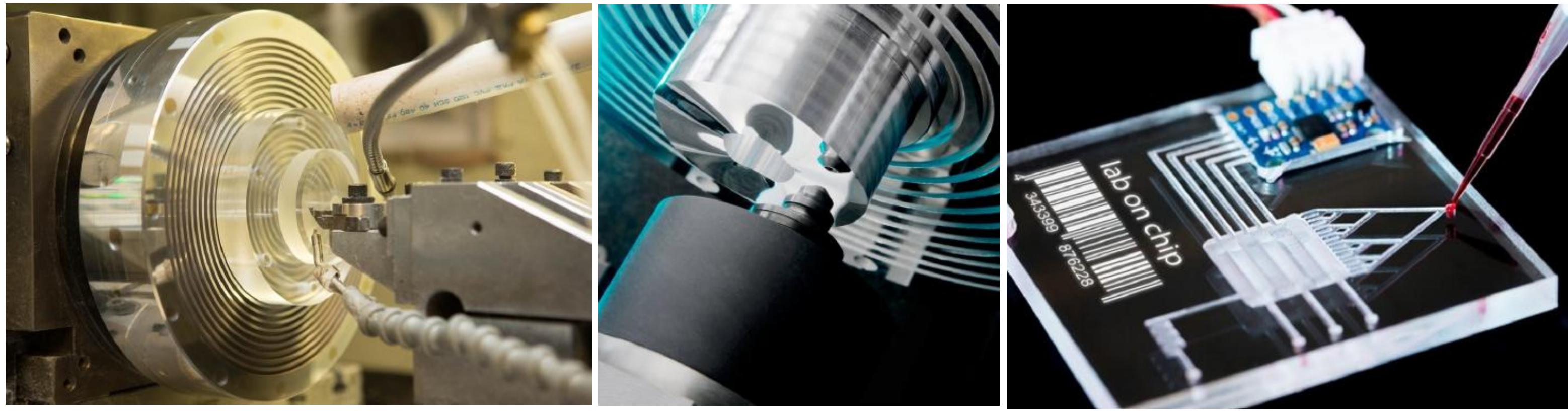


High-Resolution Characterization of Machining-Induced Residual stress In Single-Crystal Sapphire

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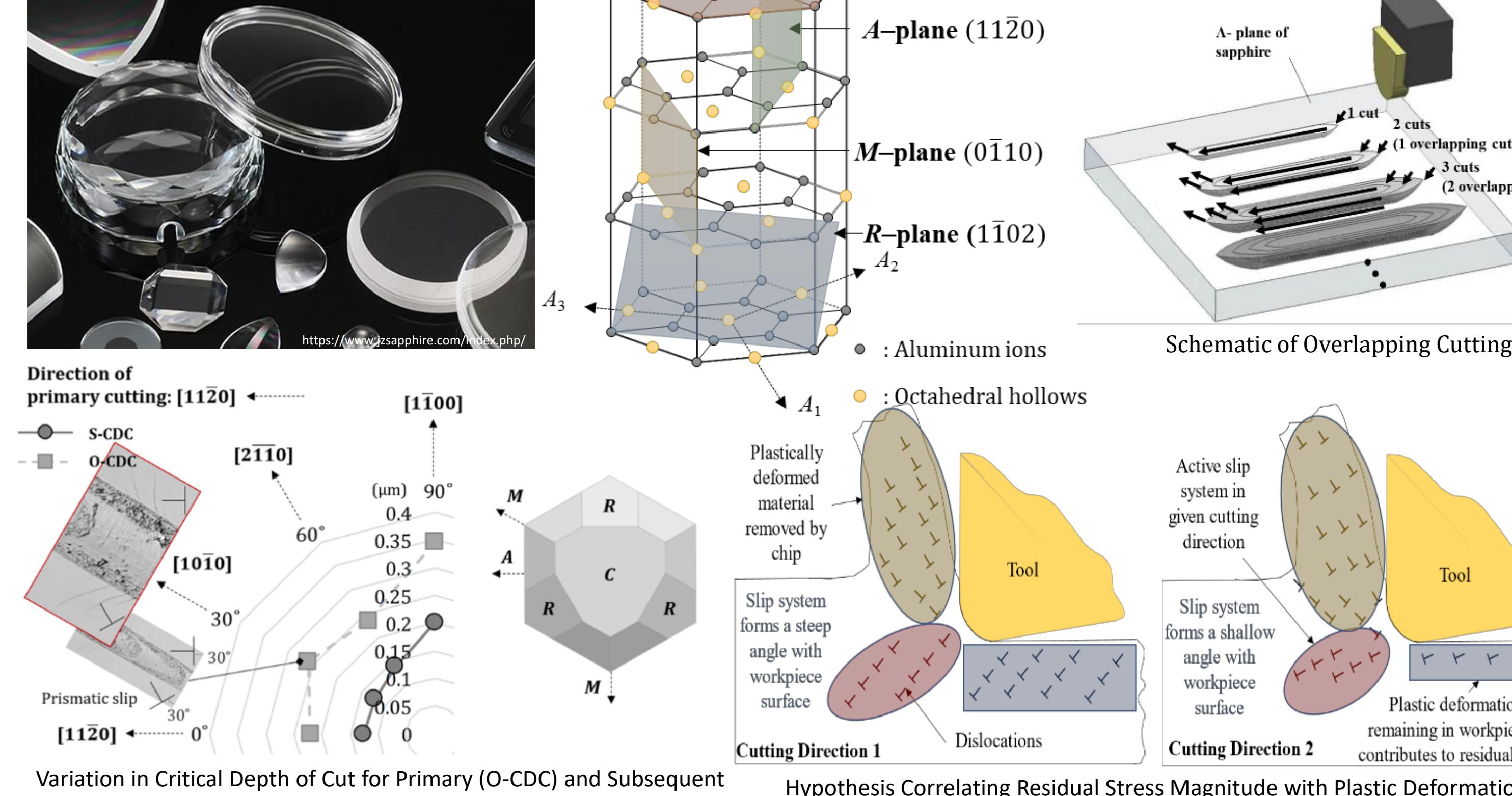
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Project Objectives and Goals

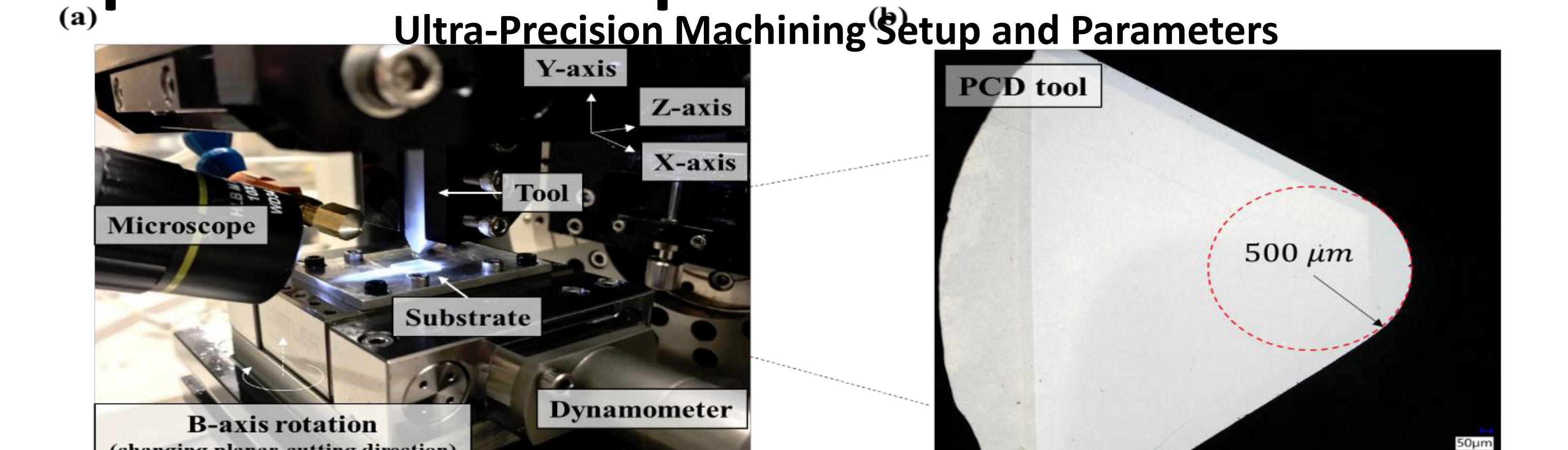


- Address machining challenges by investigating the effects of sapphire's high hardness, brittleness, and crystallographic anisotropy on material removal
- Quantify residual stress and that contribute to crack initiation and degradation of machining performance
- Utilize Raman spectroscopy to evaluate residual stress providing insights for process modeling and optimization
- Employ X-ray nanobeam diffraction microscopy, enabling high-resolution correlation between deformation mechanisms and stress evolution

Background



Experimental Setup

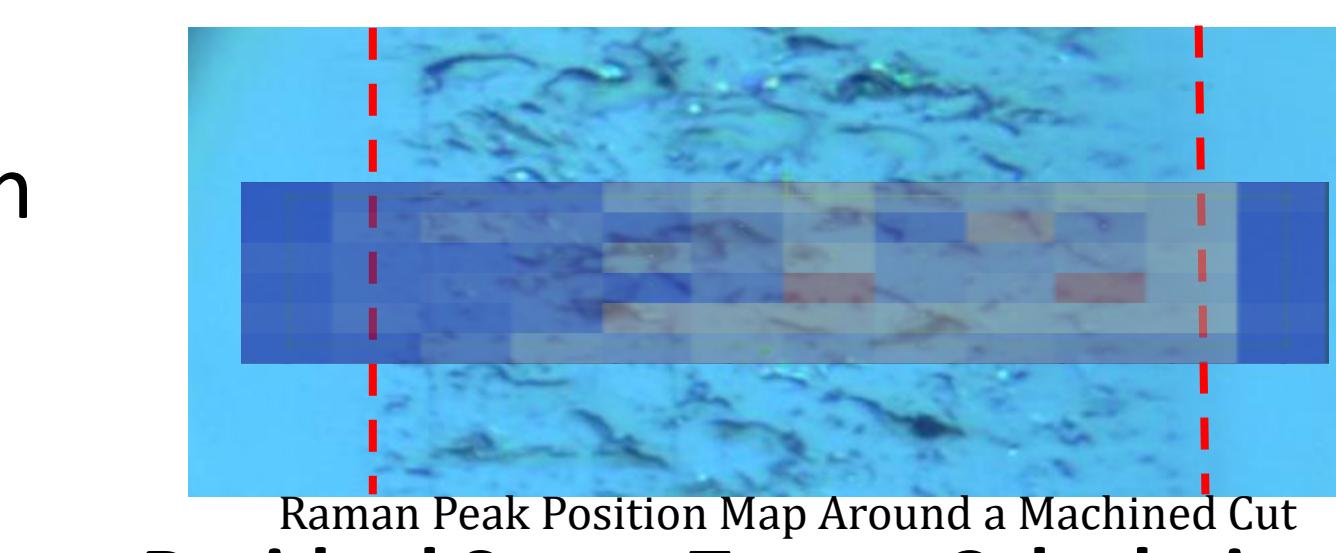


| Parameter | Description |
|--------------|---|
| Machine Tool | ROBONANO α-0iB, FANUC Corp., Japan |
| Cutting Tool | Binderless Nano-PCD Tool, 500 μm nose radius, 0° rake angle (A.L.M.T. Corp., Japan) |
| Substrate | Sapphire, Czochralski growth; 3 mm x 5 mm x 0.5 mm (MTI Corp., U.S.A.) |
| Dynamometer | Type 9119AA1 (Kistler Instrument Corp., Switzerland) |
| Cutting oil | Mineral oil based (JX Nippon Oil & Energy, Japan) |
| Feed rate | 5 mm/min |

Data and Results—Raman Spectroscopy

Raman Spectroscopy Parameter

| Parameter | Description |
|----------------------------|---------------------------------|
| Raman Instrument and Model | Horiba LabRAM HR Evolution |
| Laser Wavelength | 633 nm |
| Grating Density | 1800 grooves/mm |
| Spectral Acquisition Time | 10 s/position, 2 scans per spot |
| Raman map spacing | ~10 μm intervals |



Raman Peak Position Map Around a Machined Cut

Residual Stress Tensor Calculation

Based on the relationship between peak shift ($\Delta\nu$) and stress tensor (σ_{ij})

$$\Delta\nu = \Pi_{ij}\sigma_{ij} = \begin{vmatrix} \Pi_{11} & \Pi_{12} & \Pi_{13} \\ \Pi_{21} & \Pi_{22} & \Pi_{23} \\ \Pi_{31} & \Pi_{32} & \Pi_{33} \end{vmatrix} \begin{vmatrix} \sigma_{xx} & \sigma_{xy} & \sigma_{xz} \\ \sigma_{yx} & \sigma_{yy} & \sigma_{yz} \\ \sigma_{zx} & \sigma_{zy} & \sigma_{zz} \end{vmatrix} \quad (1)$$

Π_{ij} is the piezo spectroscopic coefficient

Accounting for the crystal orientation in the lab frame

$$\begin{vmatrix} \sigma_{x'x'} & \sigma_{x'y'} & \sigma_{x'z'} \\ \sigma_{y'x'} & \sigma_{y'y'} & \sigma_{y'z'} \\ \sigma_{z'x'} & \sigma_{z'y'} & \sigma_{z'z'} \end{vmatrix} = \Phi_{xyz} \begin{vmatrix} \sigma_{xx} & \sigma_{xy} & \sigma_{xz} \\ \sigma_{yx} & \sigma_{yy} & \sigma_{yz} \\ \sigma_{zx} & \sigma_{zy} & \sigma_{zz} \end{vmatrix} \tilde{\Phi}_{xyz} \quad (2)$$

Φ_{xyz} is rotation matrix and $\tilde{\Phi}_{xyz}$ is the transpose of the rotation matrix.

Considering the crystal symmetries of sapphire, Eq. 1 reduces to

$$\Delta\nu = \begin{vmatrix} \Pi_a^{(n)} & 0 & 0 \\ 0 & \Pi_b^{(n)} & 0 \\ 0 & 0 & \Pi_c^{(n)} \end{vmatrix} \Phi_{xyz} \begin{vmatrix} \sigma_{xx} & \sigma_{xy} & \sigma_{xz} \\ \sigma_{yx} & \sigma_{yy} & \sigma_{yz} \\ \sigma_{zx} & \sigma_{zy} & \sigma_{zz} \end{vmatrix} \tilde{\Phi}_{xyz} \quad (3)$$

Reducing to plane strain condition and simplifying Eq. 3,

$$\begin{pmatrix} \sigma_{xx} \\ \sigma_{xy} \\ \sigma_{yy} \end{pmatrix} = \begin{pmatrix} A_{11} & A_{12} & A_{13} \\ A_{21} & A_{22} & A_{23} \\ A_{31} & A_{32} & A_{33} \end{pmatrix}^{-1} \begin{pmatrix} \Delta\nu_1 \\ \Delta\nu_2 \\ \Delta\nu_3 \end{pmatrix} \quad (4)$$

Basal slip Rhombohedral twinning

Ductile

Basal slip

Prismatic slip

A_{1g} Phonon Peak in Sapphire

X1 R1 TW X2 R2 TW X3 R3 TW

X C TW1 X C TW2 X C TW3

● C SL1 ● C SL2 ● C SL3 ● C SL4 ● C SL5 ● C SL6

+ A1 SL1 + A2 SL1 + A3 SL1

+ A1 SL2 + A2 SL2 + A3 SL2

+ A1 SL1 + A2 SL1 + A3 SL1

+ A1 SL2 + A2 SL2 + A3 SL2

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