

Event-Triggered Robust Stabilization of Nonlinear Input-Constrained Systems Using Single Network Adaptive Critic Designs

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Abstract—In this paper, we study the event-triggered robust stabilization problem of nonlinear systems subject to mismatched perturbations and input constraints. First, with the introduction of an infinite-horizon cost function for the auxiliary system, we transform the robust stabilization problem into a constrained optimal control problem. Then, we prove that the solution of the event-triggered Hamilton–Jacobi–Bellman (ETHJB) equation, which arises in the constrained optimal control problem, guarantees original system states to be uniformly ultimately bounded (UUB). To solve the ETHJB equation, we present a single network adaptive critic design (SN-ACD). The critic network used in the SN-ACD is tuned through the gradient descent method. By using Lyapunov method, we demonstrate that all the signals in the closed-loop auxiliary system are UUB. Finally, we provide two examples, including the pendulum system, to validate the proposed event-triggered control strategy.

Index Terms—Adaptive critic designs (ACDs), adaptive dynamic programming (ADP), event-triggered control (ETC), input constraints, neural network (NN), reinforcement learning (RL).

I. INTRODUCTION

ADAPTIVE critic designs (ACDs) have emerged as effective tools to solve optimal control problems over the past several decades [1]–[3]. The typical structure applied to implement ACDs is the actor-critic architecture, where the actor performs a control policy to environment (or controlled systems), and the critic offers an estimation of the value of that control policy and gives feedback information to the actor. In the computational intelligence community, adaptive dynamic programming (ADP) [4] and reinforcement learning (RL) [5] are nearly in the same spirits as ACDs (e.g., all of them have similar implementation architectures). Thus, they are often regarded as synonyms for ACDs. In this paper, we view ADP

and RL as a kind of ACDs. The early contributors to ADP and RL included Werbos [6] and Sutton and Barto [7]. After that, many scholars showed their interest in ADP and RL. Thus, all kinds of ADP and RL methods were developed, such as local value/policy iterative ADP [8], [9], goal representation ADP [10], robust ADP [11], [12], single network ACDs (SN-ACDs) [13], online RL [14], [15], off-policy RL [16], and manifold RL [17].

In recent years, applications of ACDs to study robust stabilization problems have been extensively reported [18]–[22]. In the existing literature, the robust controllers for nonlinear systems are generally obtained by solving H_∞ optimal control problems or nonlinear zero-sum games under the framework of ACDs. Nevertheless, a limitation of solving H_∞ optimal control problems or zero-sum games is that one needs to make sure the existence of saddle points. Unfortunately, it is challenging to judge whether the saddle point of nonlinear systems exists or not. To avoid this difficulty, Lin and Brandt [23] introduced an indirect method, which aimed at converting the robust control problem into an H_2 optimal control problem. Then, one was able to derive the robust controller for nonlinear systems by solving the H_2 optimal control problem. Recently, the indirect method together with ACDs was proposed by Adhyaru *et al.* [24] to design the robust controller for uncertain nonlinear input-constrained systems. After that, Mu *et al.* [25] used the indirect method and ACDs together to derive a robust tracking control strategy for nonlinear systems subject to matched uncertainties. By using a similar method as [25], Qu *et al.* [26] obtained a decentralized tracking control of large-scale nonlinear systems with matched interconnections. An important difference between [25] and [26] was that [26] did not require the initial admissible control while implementing the proposed robust control scheme. Later, Zhang *et al.* [27] extended the work of [26] to design an optimal guaranteed cost sliding mode controller for constrained nonlinear systems with matched/mismatched disturbances. In all the above mentioned literature, the robust control strategies were implemented in the time-triggering mechanism. In other words, the robust control schemes were implemented periodically. According to [28], the time-triggered control schemes often had difficulties in handling the control problems with the conditions that there were only finite computation bandwidths as well as the limited communication resources.

To overcome these difficulties, many event-triggered control (ETC) approaches have been introduced [29]–[32]. Unlike

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the time-triggered controller, the event-triggered controller is updated aperiodically. Specifically, the event-triggered controller is updated only when the deviation between the system state and the desired value crosses a prescribed threshold. Due to this characteristic, the ETC strategies can overcome the shortcomings of the time-triggered control schemes [28]. Thus, many studies on robust ETC methods were reported. Wang *et al.* [33] presented an event-based robust controller for uncertain nonlinear systems via the SN-ACD. After that, with the combination of the SN-ACD and the concurrent learning technique, Zhang *et al.* [34] developed a robust ETC of nonlinear systems with mismatched disturbances. Compared with [33], Zhang *et al.* [34] relaxed the persistence of excitation (PE) condition. Recently, by applying ACDs to solve the event-triggered H_∞ optimal control problems, Mu *et al.* [35] and Zhang *et al.* [36] obtained robust ETC strategies for nonlinear systems, respectively. Owing to the existence of the aforementioned limitation in solving H_∞ optimal control problems, these robust ETC schemes usually encountered difficulties in engineering applications. On the other hand, due to physical characteristics of actuators in engineering industries, it is necessary to take actuator saturations (i.e., input constraints) into account. To address this problem, Wang *et al.* [37] studied the constrained robust ETC problem of nonlinear input-affine systems with *matched* uncertainties using ACDs. However, to the best of our knowledge, there are few studies developing the robust ETC scheme for nonlinear input-constrained systems subject to *mismatched* perturbations, especially without using the H_∞ control theory [38]. This motivates this paper.

In this paper, a robust ETC strategy is developed for nonlinear input-constrained systems with mismatched perturbations. First, by constructing an infinite-horizon cost function for the auxiliary system, the robust stabilization problem is converted into a constrained optimal control problem. Then, it is proved that the solution of the event-triggered Hamilton–Jacobi–Bellman (ETHJB) equation, arising in the constrained optimal control problem, keeps original system states uniformly ultimately bounded (UUB). To solve the ETHJB equation, the SN-ACD is proposed. The critic network used in the SN-ACD is updated by using the gradient descent method. Finally, uniform ultimate boundedness of all the signals in the closed-loop auxiliary system is demonstrated via Lyapunov method.

The novelties of this paper include three aspects.

- 1) Different from [34] updating the augmented control in a mechanism regarded as the combination of time-triggering and event-triggering mechanisms (ETMs), this paper tunes the augmented control only in the ETM. Hence, the developed control scheme has an advantage in decreasing the computational burden.
- 2) Unlike [35] and [36] solving the event-triggered H_∞ optimal control problems, this paper obtains the robust ETC via an indirect method. Thus, the present method relaxes the requirement of judging the existence of the saddle point, which is an indispensable procedure in solving H_∞ optimal control problems.
- 3) This paper extends the work of [37] to develop a robust ETC strategy for nonlinear input-constrained systems

with *mismatched* perturbations. Generally, robust control methods for nonlinear systems with *matched* disturbances are not applicable to those systems with *mismatched* disturbances (*note*: the definitions of systems with *mismatch* disturbances and systems with *match* disturbances can refer to [23]). Furthermore, when considering input constraints, it increases the difficulty in making such an extension.

It is worth emphasizing here that the knowledge of system dynamics [i.e., $f(x)$ and $g(x)$ in system (1) (*note*: see Section II-A)] is required to be known. Actually, by using a similar fuzzy technique proposed in [39], this condition can be removed. For simplicity, in this paper we assume that the information of system dynamics is available.

The rest of this paper is structured as follows. After briefly presenting problem descriptions and preliminaries in Section II, we propose the robust ETC scheme in Section III. Then, after discussing the stability analysis in Section IV, we provide two examples to validate the established theoretical results in Section V. Finally, several concluding remarks and future works are given in Section VI.

Notation: \mathbb{R} , \mathbb{N} , and \mathbb{N}^+ denote the sets of real numbers, non-negative integers, and positive integers, respectively. \mathbb{R}^m and $\mathbb{R}^{n \times m}$ denote the spaces of real m -vectors and $n \times m$ real matrices, respectively. I_n is the identity matrix of dimension $n \times n$. \top is the transposition symbol. $\|\alpha\| = \sqrt{\sum_{i=1}^n |\alpha_i|^2}$ is the Euclidean norm of the vector $\alpha = (\alpha_1, \alpha_2, \dots, \alpha_n)^\top \in \mathbb{R}^n$. Ω is a subset of \mathbb{R}^n , i.e., $\Omega \subset \mathbb{R}^n$. $\|A\|$ denotes the Frobenius-norm of the matrix $A \in \mathbb{R}^{n \times m}$. $V_x^* = \partial V^*(x)/\partial x$ is the partial derivative of $V^*(x)$ with respect to $x \in \mathbb{R}^n$.

II. PROBLEM DESCRIPTION AND PRELIMINARIES

A. Problem Description

Consider the continuous-time nonlinear system with a mismatched perturbation given in the form

$$\dot{x}(t) = f(x(t)) + g(x(t))u(t) + k(x(t))d(x(t)) \quad (1)$$

where $x(t) \in \mathbb{R}^n$ is the state, $u(t) \in \mathcal{U}$ is the control input, $\mathcal{U} = \{(u_1, u_2, \dots, u_m) \in \mathbb{R}^m : |u_i| \leq \beta, i = 1, 2, \dots, m\}$, $\beta > 0$ is the upper bound, $f(x) \in \mathbb{R}^n$, $g(x) \in \mathbb{R}^{n \times m}$, and $k(x) \in \mathbb{R}^{n \times p}$ (*note*: $k(x) \neq g(x)$ when $p = m$) are known smooth functions, and $d(x) \in \mathbb{R}^p$ is an *uncertain* perturbation. Here, $x_0 = x(0)$ is the initial state.

Assumption 1: System (1) is controllable. Meanwhile, $x = 0$ is the equilibrium point of system (1) when letting $u(t) = 0$ and $d(x(t)) = 0$ for all $t \geq 0$.

Assumption 2: The control matrix $g(x)$ is bounded as $0 < g(x) \leq g_M$ ($\forall x \in \mathbb{R}^n$) with $g_M \in \mathbb{R}$ the positive constant. Meanwhile, there exist non-negative functions $\zeta_M(x) \in \mathbb{R}$ and $d_M(x) \in \mathbb{R}$ such that, for all $x \in \mathbb{R}^n$

$$\|g^+(x)k(x)d(x)\| \leq \ell_M(x) \quad \text{and} \quad \|d(x)\| \leq d_M(x)$$

with $g^+(x)$ the Moore–Penrose pseudo-inverse of $g(x)$. In addition, $\ell_M(0) = 0$, $d(0) = 0$, and $d_M(0) = 0$.

This paper aims at finding an appropriate state feedback controller to stabilize system (1). Owing to the existence of

190 system uncertainties, it is challengeable to design the stabiliz-
 191 ing controller directly. To address this issue, we will convert
 192 the robust control problem of system (1) into a constrained
 193 optimal control problem of the auxiliary system.

194 B. Hamilton–Jacobi–Bellman Equation Related to Auxiliary 195 Systems

196 Divide the term $k(x)d(x)$ into the following two parts:

$$197 \quad k(x)d(x) = g(x)g^+(x)k(x)d(x) + h(x)d(x) \quad (2)$$

198 with

$$199 \quad h(x) = (I_n - g(x)g^+(x))k(x). \quad (3)$$

200 According to [40], the auxiliary system corresponding to (1)
 201 can be described as

$$202 \quad \dot{x} = f(x) + g(x)u + h(x)v \quad (4)$$

203 where $u \in \mathcal{U}$ and $v \in \mathbb{R}^p$ is the auxiliary control.

204 The infinite-horizon cost function for system (4) is given by

$$205 \quad V^{u,v}(x(t)) = \int_t^\infty (\Psi(x(s)) + r(x(s), u(s), v(s)))ds \quad (5)$$

206 where $\Psi(x) = 2\ell_M^2(x) + \rho d_M^2(x)$, $\rho \in \mathbb{R}$ is a positive constant,
 207 and

$$208 \quad r(x, u, v) = x^T Q x + \mathcal{W}(u) + \rho v^T v$$

209 with $Q \in \mathbb{R}^{n \times n}$ the positive definite matrix and $\mathcal{W}(u) \in \mathbb{R}$ the
 210 semipositive definite function.

211 To overcome the bounded control, we define $\mathcal{W}(u)$ as [41]

$$212 \quad \mathcal{W}(u) = 2\beta \sum_{i=1}^m \int_0^{u_i} \psi^{-1}(\zeta/\beta) d\zeta \quad (6)$$

213 where $\psi(\cdot)$ is a bounded monotonic function with $\psi(0) = 0$.
 214 Meanwhile, $\psi(\cdot)$ is an odd function with its derivative
 215 bounded. Since $\psi^{-1}(\cdot)$ is a monotonic odd function, $\mathcal{W}(u)$
 216 given in (6) is semipositive definite. In this paper, we let $\psi(\cdot)$
 217 be the hyperbolic tangent function, i.e., $\psi(\cdot) = \tanh(\cdot)$.

218 Let $\mathcal{A}(\Omega)$ be the set of admissible control [5] defined on
 219 Ω . Then, the optimal value of (5) is formulated as

$$220 \quad V^*(x) = \min_{u,v \in \mathcal{A}(\Omega)} V^{u,v}(x). \quad (7)$$

221 If $V^*(x)$ is continuously differentiable, then its derivative
 222 satisfies

$$223 \quad (V_x^*)^T (f(x) + g(x)u + h(x)v) \\ 224 \quad + \Psi(x) + x^T Q x + \mathcal{W}(u) + \rho v^T v = 0.$$

225 According to [4], the Hamiltonian for V_x^* , u , and v can be
 226 defined as

$$227 \quad H(x, V_x^*, u, v) = (V_x^*)^T (f(x) + g(x)u + h(x)v) + \Psi(x) \\ 228 \quad + x^T Q x + \mathcal{W}(u) + \rho v^T v. \quad (8)$$

229 Then, $V^*(x)$ can be obtained by solving the Hamilton–Jacobi–
 230 Bellman (HJB) equation

$$231 \quad \min_{u,v \in \mathcal{A}(\Omega)} H(x, V_x^*, u, v) = 0 \quad (9)$$

with $V^*(0) = 0$. Based on the stationary condition 232
 [42, Th. 5.8], we can therefore derive the closed-form expres- 233
 sions of optimal control and optimal auxiliary control as 234
 follows [4]: 235

$$236 \quad u^*(x) = -\beta \tanh\left(\frac{1}{2\beta} g^T(x) V_x^*\right) \quad (10)$$

$$237 \quad v^*(x) = -\frac{1}{2\rho} h^T(x) V_x^*. \quad (11)$$

From (8)–(11), we can rewrite the HJB equation as 238

$$239 \quad (V_x^*)^T f(x) + \Psi(x) + x^T Q x + \mathcal{W}\left(-\beta \tanh\left(\frac{1}{2\beta} g^T(x) V_x^*\right)\right) \\ 240 \quad - \beta (V_x^*)^T g(x) \tanh\left(\frac{1}{2\beta} g^T(x) V_x^*\right) - \left\| \frac{1}{2\sqrt{\rho}} h^T(x) V_x^* \right\|^2 = 0 \quad (12) \quad 241$$

with $V^*(0) = 0$. According to [30], (12) is the time-triggered 242
 HJB equation. 243

244 Similar to [43], it can be proved that the robust controller for
 245 system (1) is able to be obtained by solving (12). However,
 246 owing to the use of time-triggered formulations, the robust
 247 control strategy is developed in the time-triggering mechanism.
 248 As mentioned in [44], the time-triggered control algorithms
 249 generally have low efficiency of using the limited communi-
 250 cation resources between actuators and systems. In addition,
 251 they often involve high-computational burdens. To overcome
 252 the two deficiencies, we will develop a robust ETC scheme
 253 for system (1).

254 III. ROBUST ETC STRATEGY

255 In this section, we first describe the robust stabilization of
 256 system (1) in the ETM. Specifically, we prove that the robust
 257 ETC of (1) can be obtained by solving an ETHJB equation.
 258 Then, we use the SN-ACD to solve the ETHJB equation. 259

259 A. Robust Stabilization in the ETM

260 Let $\{t_j\}_{j=0}^\infty$ (note: $t_j < t_{j+1}, j \in \mathbb{N}$) be the sequence of trig-
 261 gering instants, where t_j denotes the j th triggering instant. The
 262 system state is sampled at the triggering instant t_j , and the
 263 sampled state is written as

$$264 \quad \bar{x}_j = x(t_j) \quad j \in \mathbb{N}.$$

265 Since there generally exists an error between the sampled state
 266 \bar{x}_j and the current state $x(t)$, we define the error as follows:

$$267 \quad e_j(t) = \bar{x}_j - x(t) \quad \forall t \in [t_j, t_{j+1}). \quad (13)$$

268 From the expression $e_j(t)$ given in (13), we can judge whether
 269 an event is triggered or not. Specifically, if the event is trig-
 270 gered at instant $t = t_j$, then $e_j(t_j) = 0$. Based on the sampled
 271 state, we can obtain the ETC law $u(\bar{x}_j)$, which is executed at
 272 the triggering instant t_j . By using the zero-order hold tech-
 273 nique [28], the control sequence $\{u(\bar{x}_j)\}_{j=0}^\infty$ can generate a
 274 continuous-time input signal $\mu(\bar{x}_j, t)$, i.e.,

$$275 \quad \mu(\bar{x}_j, t) = u(\bar{x}_j) = u(x(t_j)) \quad \forall t \in [t_j, t_{j+1}).$$

Let the above mentioned ETM be applied to $u^*(x)$ given in (10). Then, the optimal ETC law for system (4) with the cost function (5) can be obtained as [30] (for all $t \in [t_j, t_{j+1})$)

$$\mu^*(\bar{x}_j, t) = u^*(\bar{x}_j) = -\beta \tanh\left(\frac{1}{2\beta} g^\top(\bar{x}_j) V_{\bar{x}_j}^*\right) \quad (14)$$

with $V_{\bar{x}_j}^* = (\partial V^*(x)/\partial x)|_{x=\bar{x}_j}$.

Similarly, applying the aforementioned ETM to $v^*(x)$ given in (11), we can derive the optimal auxiliary ETC law as

$$\vartheta^*(\bar{x}_j, t) = v^*(\bar{x}_j) = -\frac{1}{2\rho} h^\top(\bar{x}_j) V_{\bar{x}_j}^* \quad \forall t \in [t_j, t_{j+1}). \quad (15)$$

Remark 1: For brevity, in subsequent discussion we write $\mu^*(\bar{x}_j, t)$ and $\vartheta^*(\bar{x}_j, t)$ as $\mu^*(\bar{x}_j)$ and $\vartheta^*(\bar{x}_j)$, respectively.

Before continuing the discussion, we give the following assumption used in [30] and [45].

Assumption 3: $u^*(x)$ has the Lipschitz property on Ω . That is, there exists a Lipschitz constant $K_{u^*} > 0$ such that, for all $x, \bar{x}_j \in \Omega$

$$\|u^*(x) - u^*(\bar{x}_j)\| \leq K_{u^*} \|x - \bar{x}_j\| = K_{u^*} \|e_j\|.$$

Remark 2: By using Remark 1 and (14), we can write $\mu^*(\bar{x}_j) = u^*(\bar{x}_j)$. Thus, Assumption 3 implies

$$\|u^*(x) - \mu^*(\bar{x}_j)\| \leq K_{u^*} \|e_j\| \quad (16)$$

for all $x, \bar{x}_j \in \Omega$.

Theorem 1: Let Assumptions 1–3 be valid and let $V^*(x)$ be a solution of the HJB equation (12). Then, the optimal ETC law $\mu^*(\bar{x}_j)$ given in (14) can ensure the closed-loop system (1) to be stable in the sense of uniform ultimate boundedness only if $v^*(x)$ given in (11) satisfies

$$\|v^*(x(t))\|^2 \leq \lambda_{\min}(Q) \|x(t)\|^2 \quad \forall t \geq t_s \quad (17)$$

where $t_s \geq 0$ is a threshold, and provided that the triggering condition is given by

$$\|e_j\|^2 \leq \frac{(1-2\rho)\lambda_{\min}(Q)}{4K_{u^*}^2} \|x\|^2 \triangleq \|e_T\|^2 \quad (18)$$

with $0 < \rho < 1/2$ the design parameter and e_T the triggering threshold.

Proof: We take $V^*(x)$ as the Lyapunov function candidate. From the expression $V^*(x)$ given as in (7), we can deduce that $V^*(x) > 0$ for $x \neq 0$ and $V^*(x) = 0 \Leftrightarrow x = 0$, i.e., $V^*(x)$ is positive definite.

By differentiating $V^*(x)$ along the solution of $\dot{x} = f(x) + g(x)\mu^*(\bar{x}_j) + k(x)d(x)$ and using (2), we have [note: $\dot{V}^*(x)$ denotes $dV^*(x(t))/dt$]

$$\begin{aligned} \dot{V}^*(x) &= (V_x^*)^\top (f(x) + g(x)\mu^*(\bar{x}_j) + k(x)d(x)) \\ &= (V_x^*)^\top (f(x) + g(x)u^*(x) + h(x)v^*(x)) \\ &\quad + (V_x^*)^\top g(x)(\mu^*(\bar{x}_j) - u^*(x)) \\ &\quad + (V_x^*)^\top g(x)g^+(x)k(x)d(x) \\ &\quad + (V_x^*)^\top h(x)(d(x) - v^*(x)) \end{aligned} \quad (19)$$

with $h(x)$ defined as in (3).

On the other hand, from (8) and (9), we obtain

$$\begin{aligned} &(V_x^*)^\top (f(x) + g(x)u^*(x) + h(x)v^*(x)) \\ &= -\Psi(x) - x^\top Qx - \mathcal{W}(u^*(x)) - \rho \|v^*(x)\|^2. \end{aligned} \quad (20)$$

Meanwhile, from (10) and (11), we find

$$\begin{cases} (V_x^*)^\top g(x) = -2\beta (\tanh^{-1}(u^*(x)/\beta))^\top \\ (V_x^*)^\top h(x) = -2\rho (v^*(x))^\top. \end{cases} \quad (21)$$

Substituting (20) and (21) into (19), it follows:

$$\begin{aligned} \dot{V}^*(x) &= -\Psi(x) - x^\top Qx - \mathcal{W}(u^*(x)) + \rho \|v^*(x)\|^2 \\ &\quad + 2\beta \underbrace{(\tanh^{-1}(u^*(x)/\beta))^\top (u^*(x) - \mu^*(\bar{x}_j))}_{\pi_1} \\ &\quad - 2\beta \underbrace{(\tanh^{-1}(u^*(x)/\beta))^\top g^+(x)k(x)d(x)}_{\pi_2} \\ &\quad - 2\rho \underbrace{(v^*(x))^\top d(x)}_{\pi_3}. \end{aligned} \quad (22)$$

By using Young's inequality $2y^\top z \leq \varrho \|y\|^2 + \|z\|^2/\varrho$ ($\varrho > 0$) and (16), we can see that π_1 in (22) implies (note: $\varrho = 1/2$)

$$\begin{aligned} \pi_1 &\leq \frac{\beta^2}{2} \left\| \tanh^{-1}(u^*(x)/\beta) \right\|^2 + 2 \|u^*(x) - \mu^*(\bar{x}_j)\|^2 \\ &\leq \frac{\beta^2}{2} \sum_{i=1}^m \left(\tanh^{-1}(u_i^*(x)/\beta) \right)^2 + 2K_{u^*}^2 \|e_j\|^2. \end{aligned} \quad (23)$$

Similarly, by using the above mentioned Young's inequality and Assumption 2, we can find that π_2 and π_3 in (22) yield (note: $\varrho = 1/2$ and $\varrho = 1$, respectively)

$$\begin{aligned} \pi_2 &\leq \frac{\beta^2}{2} \left\| \tanh^{-1}(u^*(x)/\beta) \right\|^2 + 2 \|g^+(x)k(x)d(x)\|^2 \\ &\leq \frac{\beta^2}{2} \sum_{i=1}^m \left(\tanh^{-1}(u_i^*(x)/\beta) \right)^2 + 2\ell_M^2(x) \end{aligned} \quad (24)$$

$$\pi_3 \leq \rho \|v^*(x)\|^2 + \rho \|d(x)\|^2 \leq \rho \|v^*(x)\|^2 + \rho d_M^2(x). \quad (25)$$

From [46] (note: see the proof of [46, Th. 1]), we know

$$\begin{aligned} \mathcal{W}(u^*) &= 2\beta \sum_{i=1}^m \int_0^{u_i^*(x)} \tanh^{-1}(\zeta/\beta) d\zeta \\ &= \beta^2 \sum_{i=1}^m \left(\tanh^{-1}(u_i^*(x)/\beta) \right)^2 \\ &\quad - 2\beta^2 \sum_{i=1}^m \int_0^{\tanh^{-1}(u_i^*(x)/\beta)} \tau_i \tanh^2(\tau_i) d\tau_i. \end{aligned} \quad (26)$$

Observing that $\Psi(x) = 2\ell_M^2(x) + \rho d_M^2(x)$ and using (23)–(26), we can conclude that (22) yields

$$\begin{aligned} \dot{V}^*(x) &\leq -x^\top Qx + 2\rho \|v^*(x)\|^2 + 2K_{u^*}^2 \|e_j\|^2 \\ &\quad + 2\beta^2 \underbrace{\sum_{i=1}^m \int_0^{\tanh^{-1}(u_i^*(x)/\beta)} \tau_i \tanh^2(\tau_i) d\tau_i}_{\mathcal{L}(x)}. \end{aligned} \quad (27)$$

According to the proof of [46, Th. 1], we know that $\mathcal{L}(x)$ given in (27) is a bounded function. To facilitate subsequent discussion, we denote that $\|\mathcal{L}(x)\| \leq \epsilon_M$,

where $\epsilon_M > 0$ is a constant. Then, (27) can be further rewritten as

$$\begin{aligned} \dot{V}^*(x) &\leq -\lambda_{\min}(Q)\|x\|^2 + 2\rho\|v^*(x)\|^2 + 2K_{u^*}^2\|e_j\|^2 + \epsilon_M \\ &= -2\rho\left(\lambda_{\min}(Q)\|x\|^2 - \|v^*(x)\|^2\right) + 2K_{u^*}^2\|e_j\|^2 \\ &\quad - (1 - 2\rho)\lambda_{\min}(Q)\|x\|^2 + \epsilon_M \end{aligned} \quad (28)$$

with $\lambda_{\min}(Q)$ the minimum eigenvalue of Q .

Thus, if (17) and (18) hold, then (28) yields

$$\dot{V}^*(x) \leq -\frac{(1 - 2\rho)\lambda_{\min}(Q)}{2}\|x\|^2 + \epsilon_M. \quad (29)$$

Therefore, from (29), we can find that $\dot{V}^*(x) < 0$ only when $x(t)$ is out of the following set:

$$\Omega_x = \left\{ x : \|x\| \leq \sqrt{\frac{2\epsilon_M}{(1 - 2\rho)\lambda_{\min}(Q)}} \right\}.$$

Then, uniform ultimate boundedness of the states of system (1) is guaranteed by using Lyapunov extension theorem [47]. Specifically, this indicates that $\mu^*(\bar{x}_j)$ keeps the closed-loop system (1) stable in the sense of uniform ultimate boundedness. Meanwhile, the ultimate bound is $\sqrt{2\epsilon_M/((1 - 2\rho)\lambda_{\min}(Q))}$. ■

Remark 3: According to (18), the triggering instant t_j can be calculated. Then, it is possible to obtain the minimal inter-sample time $(\Delta t_j)_{\min}$, where $\Delta t_j = t_{j+1} - t_j$, $j \in \mathbb{N}$. However, if there exists $(\Delta t_j)_{\min} = 0$, then the Zeno behavior occurs [48]. In this circumstance, $\mu^*(\bar{x}_j)$ has to be redesigned. Fortunately, $(\Delta t_j)_{\min} > 0$, $j \in \mathbb{N}$, under Assumption 1 (note: since similar proofs have been provided in [36] and [49], we omit the proof here). In this paper, simulation results provided in Section V also show that $(\Delta t_j)_{\min} > 0$, $j \in \mathbb{N}$.

To obtain the optimal ETC law $\mu^*(\bar{x}_j)$, we need to solve the ETHJB equation, which is derived by substituting (14) and (15) into (9). That is,

$$\begin{aligned} &(V_x^*)^\top f(x) - \beta(V_x^*)^\top g(x) \tanh\left(\frac{1}{2\beta}g^\top(\bar{x}_j)V_{\bar{x}_j}^*\right) \\ &\quad - \frac{1}{2\rho}(V_x^*)^\top h(x)h^\top(\bar{x}_j)V_{\bar{x}_j}^* + \Psi(x) + x^\top Qx \\ &\quad + \mathcal{W}\left(-\beta \tanh\left(\frac{1}{2\beta}g^\top(\bar{x}_j)V_{\bar{x}_j}^*\right)\right) + \left\| \frac{1}{2\sqrt{\rho}}h^\top(\bar{x}_j)V_{\bar{x}_j}^* \right\|^2 = 0. \end{aligned} \quad (30)$$

Generally, it is rather hard to solve the ETHJB equation (30) analytically [50]. To conquer the difficulty, we present the SN-ACD to approximately solve (30).

B. SN-ACD for Solving the ETHJB Equation

The approximation theorem [51] guarantees that $V^*(x)$ given in (7) can be represented via a critic network over Ω as

$$V^*(x) = \omega_c^\top \sigma_c(x) + \varepsilon_c(x)$$

where $\omega_c \in \mathbb{R}^{\tilde{n}_c}$ is the ideal weight vector, $\sigma_c(x) = [\sigma_{c1}(x), \sigma_{c2}(x), \dots, \sigma_{c\tilde{n}_c}(x)]^\top \in \mathbb{R}^{\tilde{n}_c}$ is the basis function vector, $\sigma_{c\iota}(x)$, $\iota = 1, 2, \dots, \tilde{n}_c$, are continuously differentiable

functions with $\sigma_{c\iota}(0) = 0$, $\tilde{n}_c \in \mathbb{N}^+$ is the number of basis functions, and $\varepsilon_c(x) \in \mathbb{R}$ is the approximation error.

Differentiating $V^*(x)$ at the sampled state \bar{x}_j , we have

$$V_{\bar{x}_j}^* = \nabla \sigma_c^\top(\bar{x}_j)\omega_c + \nabla \varepsilon_c(\bar{x}_j) \quad \forall t \in [t_j, t_{j+1}) \quad (31)$$

where $\nabla \sigma_c(\bar{x}_j) = (\partial \sigma_c(x)/\partial x)|_{x=\bar{x}_j}$ and $\nabla \varepsilon_c(\bar{x}_j) = (\partial \varepsilon_c(x)/\partial x)|_{x=\bar{x}_j}$.

Substituting (31) into (14), we can rewrite $\mu^*(\bar{x}_j)$ as

$$\mu^*(\bar{x}_j) = -\beta \tanh(\mathcal{A}_1(\bar{x}_j)) + \varepsilon_{\mu^*}(\bar{x}_j) \quad \forall t \in [t_j, t_{j+1}) \quad (32)$$

where

$$\mathcal{A}_1(\bar{x}_j) = \frac{1}{2\beta}g^\top(\bar{x}_j)\nabla \sigma_c^\top(\bar{x}_j)\omega_c$$

and $\varepsilon_{\mu^*}(\bar{x}_j) = -(1/2)(\mathbf{1} - \tanh^2(\xi))g^\top(\bar{x}_j)\nabla \varepsilon_c(\bar{x}_j)$ with $\mathbf{1} = [1, \dots, 1]^\top \in \mathbb{R}^m$ and ξ chosen between $\mathcal{A}_0(\bar{x}_j)$ (note: $\mathcal{A}_0(\bar{x}_j) = (1/(2\beta))g^\top(\bar{x}_j)V_{\bar{x}_j}^*$) and $\mathcal{A}_1(\bar{x}_j)$.

Similarly, by using (31), $\vartheta^*(\bar{x}_j)$ given in (15) can be represented as (for all $t \in [t_j, t_{j+1})$)

$$\vartheta^*(\bar{x}_j) = -\frac{1}{2\rho}h^\top(\bar{x}_j)\nabla \sigma_c^\top(\bar{x}_j)\omega_c + \varepsilon_{\vartheta^*}(\bar{x}_j) \quad (33)$$

with $\varepsilon_{\vartheta^*}(\bar{x}_j) = -(1/2\rho)h^\top(\bar{x}_j)\nabla \varepsilon_c(\bar{x}_j)$.

Remark 4: The difference between $\varepsilon_{\mu^*}(\bar{x}_j)$ given in (32) and $\varepsilon_{\vartheta^*}(\bar{x}_j)$ given in (33) is caused by control constraints (note: u is constrained while v is unconstrained). To make (32) be better for understanding, we provide the detailed process of deriving $\varepsilon_{\mu^*}(\bar{x}_j)$ as follows. Let

$$\mathcal{T}(\mathcal{A}_\varpi(x)) = -\beta \tanh(\mathcal{A}_\varpi(x)), \quad \varpi = 0, 1. \quad (34)$$

Then, applying the mean value theorem [42, Th. 5.10] to $\mathcal{T}(\mathcal{A}_\varpi(x))$, we obtain (note: $\mathcal{A}_0(x) = (1/(2\beta))g^\top(x)V_x^*$)

$$\begin{aligned} \mathcal{T}(\mathcal{A}_0(x)) - \mathcal{T}(\mathcal{A}_1(x)) &= -\beta(\tanh(\mathcal{A}_0(x)) - \tanh(\mathcal{A}_1(x))) \\ &= -\frac{1}{2}(\mathbf{1} - \tanh^2(\xi))g^\top(x)\nabla \varepsilon_c(x) \end{aligned} \quad (35)$$

with ξ chosen between $\mathcal{A}_0(x)$ and $\mathcal{A}_1(x)$. By using (31), we find that (14) yields

$$\begin{aligned} \mu^*(\bar{x}_j) &= -\beta \tanh(\mathcal{A}_0(\bar{x}_j)) \\ &= \mathcal{T}(\mathcal{A}_1(\bar{x}_j)) + (\mathcal{T}(\mathcal{A}_0(\bar{x}_j)) - \mathcal{T}(\mathcal{A}_1(\bar{x}_j))) \\ &= -\beta \tanh(\mathcal{A}_1(\bar{x}_j)) - \frac{1}{2}(\mathbf{1} - \tanh^2(\xi))g^\top \nabla \varepsilon_c(\bar{x}_j). \end{aligned}$$

Hence, we can obtain the expression $\varepsilon_{\mu^*}(\bar{x}_j)$ given as in (32).

In general, the ideal weight vector ω_c is unavailable. Thus, we cannot implement $\mu^*(\bar{x}_j)$ given in (32). To handle this issue, we replace ω_c with the current estimated weight vector $\hat{\omega}_c$ in the critic network. Then, the approximation value function can be formulated as

$$\hat{V}(x) = \hat{\omega}_c^\top \sigma_c(x). \quad (34)$$

The derivative of $\hat{V}(x)$ at the sampled state \bar{x}_j is

$$\hat{V}_{\bar{x}_j} = \nabla \sigma_c^\top(\bar{x}_j)\hat{\omega}_c.$$

Replacing $V_{\bar{x}_j}^*$ in (14) with $\hat{V}_{\bar{x}_j}$, we derive the estimated value of $\mu^*(\bar{x}_j)$ as

$$\hat{\mu}(\bar{x}_j) = -\beta \tanh(\mathcal{A}_2(\bar{x}_j)) \quad \forall t \in [t_j, t_{j+1}) \quad (35)$$

where

$$\mathcal{A}_2(\bar{x}_j) = \frac{1}{2\beta} g^\top(\bar{x}_j) \nabla \sigma_c^\top(\bar{x}_j) \hat{\omega}_c. \quad (33)$$

By the same token, the estimated value of $\vartheta^*(\bar{x}_j)$ given in (33) can be obtained as

$$\hat{\vartheta}(\bar{x}_j) = -\frac{1}{2\rho} h^\top(\bar{x}_j) \nabla \sigma_c^\top(\bar{x}_j) \hat{\omega}_c \quad \forall t \in [t_j, t_{j+1}). \quad (36)$$

Substituting $\hat{V}(x)$, $\hat{\mu}(\bar{x}_j)$, and $\hat{\vartheta}(\bar{x}_j)$ into (8), we can see that the approximation Hamiltonian is

$$\begin{aligned} \hat{H}(x, \hat{V}_x, \hat{\mu}(\bar{x}_j), \hat{\vartheta}(\bar{x}_j)) \\ = \hat{\omega}_c^\top \nabla \sigma_c(x) (f(x) + g(x) \hat{\mu}(\bar{x}_j) + h(x) \hat{\vartheta}(\bar{x}_j)) \\ + \Psi(x) + x^\top Qx + \mathcal{W}(\hat{\mu}^\top(\bar{x}_j)) + \rho \|\hat{\vartheta}(\bar{x}_j)\|^2. \end{aligned} \quad (37)$$

Observe that (9) implies

$$H(x, V_x^*, \mu^*(\bar{x}_j), \vartheta^*(\bar{x}_j)) = 0.$$

Thus, the error of Hamiltonian can be formulated as

$$\begin{aligned} e_c &= \hat{H}(x, \hat{V}_x, \hat{\mu}(\bar{x}_j), \hat{\vartheta}(\bar{x}_j)) - H(x, V_x^*, \mu^*(\bar{x}_j), \vartheta^*(\bar{x}_j)) \\ &= \hat{\omega}_c^\top \phi + \Psi(x) + x^\top Qx + \mathcal{W}(\hat{\mu}(\bar{x}_j)) + \rho \|\hat{\vartheta}(\bar{x}_j)\|^2 \end{aligned} \quad (37)$$

where $\phi = \nabla \sigma_c(x) (f(x) + g(x) \hat{\mu}(\bar{x}_j) + h(x) \hat{\vartheta}(\bar{x}_j))$.

To ensure e_c given in (37) to be sufficiently small, we use the gradient descent method to minimize the target function $E = (1/2)e_c^\top e_c$. Then, the weight update rule for the critic network is obtained as

$$\begin{aligned} \dot{\hat{\omega}}_c &= -\frac{l_c}{(1 + \phi^\top \phi)^2} \frac{\partial E}{\partial \hat{\omega}_c} \\ &= -\frac{l_c \phi}{(1 + \phi^\top \phi)^2} e_c \quad \forall t \in [t_j, t_{j+1}) \end{aligned} \quad (38)$$

with e_c defined as in (37), $l_c \in \mathbb{R}^n$ the positive parameter, and $(1 + \phi^\top \phi)^{-2}$ the normalization term.

Let the weight estimation error of the critic network be $\tilde{\omega}_c = \omega_c - \hat{\omega}_c$. Then, from (38), we can see that the weight estimation error dynamics of the critic network satisfies [30]

$$\dot{\tilde{\omega}}_c = -l_c \phi \varphi^\top \tilde{\omega}_c + \frac{l_c \phi}{1 + \phi^\top \phi} \varepsilon_H \quad \forall t \in [t_j, t_{j+1}) \quad (39)$$

where $\varphi = \phi / (1 + \phi^\top \phi)^2$ and $\varepsilon_H = -\nabla \varepsilon_c^\top(x) (f(x) + g(x) \hat{\mu}(\bar{x}_j) + h(x) \hat{\vartheta}(\bar{x}_j))$ is the residual error.

From the ETM introduced in Section III-A, we can find that the closed-loop system (4) is a hybrid system. Let the augmented state be $\mathcal{X} = [x^\top, \bar{x}_j^\top, \tilde{\omega}_c^\top]^\top$. Then, we can describe the hybrid dynamical system as follows.

1) *Continuous Dynamics:*

$$\dot{\mathcal{X}}(t) = \begin{bmatrix} f(x) + \mathcal{F}(x, \bar{x}_j) \\ 0 \\ -l_c \phi \varphi^\top \tilde{\omega}_c + \frac{l_c \phi \varepsilon_H}{(1 + \phi^\top \phi)^2} \end{bmatrix} \quad \forall t \in [t_j, t_{j+1}) \quad (40)$$

where

$$\begin{aligned} \mathcal{F}(x, \bar{x}_j) &= -\beta g(x) \tanh\left(\frac{1}{2\beta} g^\top(\bar{x}_j) \nabla \sigma_c^\top(\bar{x}_j) \hat{\omega}_c\right) \\ &\quad - \frac{1}{2\rho} h(x) h^\top(\bar{x}_j) \nabla \sigma_c^\top(\bar{x}_j) \hat{\omega}_c. \end{aligned}$$

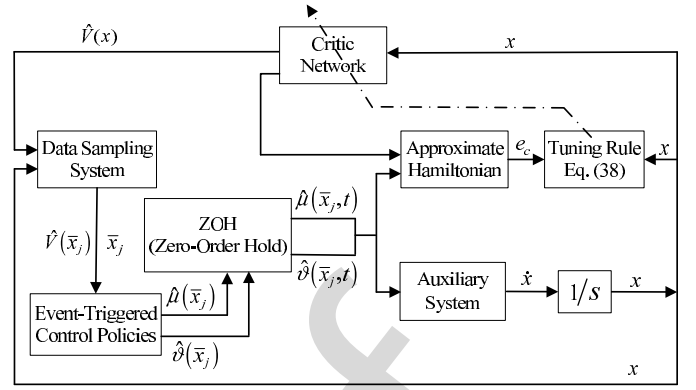


Fig. 1. Block diagram of the proposed ETC strategy.

2) *Discrete Dynamics:*

$$\mathcal{X}(t^+) = \mathcal{X}(t) + \begin{bmatrix} 0 \\ \bar{x}_j - x(t) \\ 0 \end{bmatrix} \quad t = t_{j+1} \quad (41)$$

where $\mathcal{X}(t^+) = \lim_{\eta \rightarrow 0^+} \mathcal{X}(t + \eta)$ with $\eta \in (0, t_{j+1} - t)$.

Based on the above mentioned analyses, we present the block diagram of the proposed ETC strategy in Fig. 1.

IV. STABILITY ANALYSIS

Before proving stabilities of systems (40) and (41), we provide two assumptions introduced in [4] and [52], respectively.

Assumption 4: The derivative of the basic function vector is bounded as $\|\nabla \sigma_c(x)\| \leq b_{\sigma_c}$ ($\forall x \in \Omega$), where b_{σ_c} is a positive constant. In addition, there exist positive constants $b_{\varepsilon_{\mu^*}}$, $b_{\varepsilon_{\vartheta^*}}$, and b_{ε_H} such the approximation errors $\varepsilon_{\mu^*}(\bar{x}_j)$, $\varepsilon_{\vartheta^*}(\bar{x}_j)$, and the residual error ε_H bounded as $\|\varepsilon_{\mu^*}(\bar{x}_j)\| \leq b_{\varepsilon_{\mu^*}}$, $\|\varepsilon_{\vartheta^*}(\bar{x}_j)\| \leq b_{\varepsilon_{\vartheta^*}}$, and $\|\varepsilon_H\| \leq b_{\varepsilon_H}$ ($\forall \bar{x}_j, x \in \Omega$), respectively.

Similar to (16) imposed on $u^*(x)$, we present the following assumption for $v^*(x)$.

Assumption 5: $v^*(x)$ satisfies the Lipschitz condition on Ω . That is, for all $x, \bar{x}_j \in \Omega$, there exists a Lipschitz constant $K_{v^*} > 0$ such that

$$\|v^*(x) - v^*(\bar{x}_j)\| \leq K_{v^*} \|x - \bar{x}_j\| = K_{v^*} \|e_j\|. \quad (42)$$

Let

$$G(\mathcal{A}_\kappa(x)) = \beta \tanh(\mathcal{A}_\kappa(x)), \quad \kappa = 1, 2 \quad (42)$$

where $\mathcal{A}_1(x) = (1/(2\beta))g^\top(x) \nabla \sigma_c^\top(x) \omega_c$ and $\mathcal{A}_2(x) = (1/(2\beta))g^\top(x) \nabla \sigma_c^\top(x) \hat{\omega}_c$. Then, using Taylor's theorem [42], it follows:

$$\begin{aligned} G(\mathcal{A}_1(x)) &= G(\mathcal{A}_2(x)) + \frac{\partial G(\mathcal{A}_2)}{\partial \mathcal{A}_2} (\mathcal{A}_1(x) - \mathcal{A}_2(x)) \\ &\quad + O((\mathcal{A}_1(x) - \mathcal{A}_2(x))^2) \\ &= G(\mathcal{A}_2(x)) + \frac{1}{2} (I_m - \mathcal{B}(\mathcal{A}_2(x))) g^\top(x) \\ &\quad \times \nabla \sigma_c^\top(x) \tilde{\omega}_c + O((\mathcal{A}_1(x) - \mathcal{A}_2(x))^2) \end{aligned} \quad (43)$$

with $\mathcal{B}(\mathcal{A}_2(x)) = \text{diag}\{\tanh^2(\mathcal{A}_{2i}(x))\}$, $i = 1, 2, \dots, m$, and the high-order term $O((\mathcal{A}_1(x) - \mathcal{A}_2(x))^2)$.

508 *Lemma 1:* The high-order term given in (43) is bounded as

$$509 \quad \left\| O\left(\mathcal{A}_1(x) - \mathcal{A}_2(x)\right)^2 \right\| \leq 2\sqrt{m} + g_M b_{\sigma_c} \|\tilde{\omega}_c\|. \quad (44)$$

510 *Proof:* From (43), we can find

$$511 \quad \left\| O\left(\mathcal{A}_1(x) - \mathcal{A}_2(x)\right)^2 \right\| \leq \|G(\mathcal{A}_1(x))\| + \|G(\mathcal{A}_2(x))\| \\ 512 \quad + \frac{1}{2} \|I_m - \mathcal{B}(\mathcal{A}_2(x))\| \|g(x)\| \\ 513 \quad \times \|\nabla\sigma(x)\| \|\tilde{\omega}_c\|. \quad (45)$$

514 Since $\|\tanh(x)\| \leq 1$ for all $x \in \mathbb{R}^n$, we can conclude that
515 $\|G(\mathcal{A}_\kappa(x))\| = (\sum_{i=1}^m \tanh^2(\mathcal{A}_{\kappa i}(x)))^{1/2} \leq \sqrt{m}$, $\kappa = 1, 2$, and
516 $\|I_m - \mathcal{B}(\mathcal{A}_2(x))\| \leq 2$. Then, using Assumptions 2 and 4, we
517 can see that (45) yields (44). ■

518 *Theorem 2:* Consider auxiliary system (4) associated with
519 the ETHJB equation (30). Let Assumptions 1–5 be valid
520 and take the control policies proposed as in (35) and (36).
521 Suppose that the initial control for system (4) is admissible
522 and the weight tuning rule for the critic network is described
523 as (38). Then, the closed-loop system (4) and the weight esti-
524 mation error $\tilde{\omega}_c$ are UUB only if the following event-triggering
525 condition holds:

$$526 \quad \|e_j\|^2 \leq \frac{(1-2\gamma)\lambda_{\min}(Q)}{4K_{\max}^2} \|x\|^2 \triangleq \|\bar{e}_T\|^2 \quad (46)$$

527 where $K_{\max} = \max\{K_{u^*}, K_{v^*}\}$, $0 < \gamma < 1/2$ is a design
528 parameter, and \bar{e}_T is the triggering threshold, and provided
529 that the following inequality holds:

$$530 \quad \frac{l_c}{2} \lambda_{\min}(\varphi\varphi^\top) - (16g_M^2 + h_M^2/\rho^2)b_{\sigma_c}^2 > 0 \quad (47)$$

531 where $\lambda_{\min}(\varphi\varphi^\top)$ denotes the minimum eigenvalue of $\varphi\varphi^\top$, φ
532 satisfies the PE condition, and h_M is the bound of $h(x)$.

533 *Proof:* We take the Lyapunov function candidate as

$$534 \quad L(t) = \underbrace{V^*(\bar{x}_j)}_{L_1(t)} + \underbrace{V^*(x(t))}_{L_2(t)} + \underbrace{(1/2)\tilde{\omega}_c^\top \tilde{\omega}_c}_{L_3(t)}.$$

535 Since the closed-loop system (4) is a hybrid system, we present
536 the stability analysis from following two circumstances.

537 *Situation I:* Events are not triggered, i.e., $t \in [t_j, t_{j+1})$, $j \in \mathbb{N}$.
538 Then, we have $\dot{L}_1(t) = \dot{V}^*(\bar{x}_j) = 0$.

539 Taking the derivative of $L_2(t)$ and using the trajectory
540 generated from $\dot{x} = f(x) + g(x)\hat{\mu}(\bar{x}_j) + h(x)\hat{\vartheta}(\bar{x}_j)$, we have

$$541 \quad \dot{L}_2(t) = (V_x^*)^\top \left(f(x) + g(x)\hat{\mu}(\bar{x}_j) + h(x)\hat{\vartheta}(\bar{x}_j) \right) \\ 542 \quad = (V_x^*)^\top \left(f(x) + g(x)u^*(x) + h(x)v^*(x) \right) \\ 543 \quad + (V_x^*)^\top g(x)(\hat{\mu}(\bar{x}_j) - u^*(x)) \\ 544 \quad + (V_x^*)^\top h(x)(\hat{\vartheta}(\bar{x}_j) - v^*(x)). \quad (48)$$

545 Substituting (20) and (21) into (48), it follows:

$$546 \quad \dot{L}_2(t) = -\Psi(x) - x^\top Qx - \rho \|v^*(x)\|^2 - \mathcal{W}(u^*(x)) \\ 547 \quad + \underbrace{2\beta \left(\tanh^{-1}(u^*(x)/\beta) \right)^\top (u^*(x) - \hat{\mu}(\bar{x}_j))}_{\Xi} \\ 548 \quad + 2\rho (v^*(x))^\top (v^*(x) - \hat{\vartheta}(\bar{x}_j)). \quad (49)$$

Applying Young's inequality $2y^\top z \leq \|y\|^2 + \|z\|^2$ to Ξ in (49),
we obtain

$$549 \quad \Xi \leq \beta^2 \left\| \tanh^{-1}(u^*(x)/\beta) \right\|^2 + \|u^*(x) - \hat{\mu}(\bar{x}_j)\|^2 \\ 550 \quad = \beta^2 \sum_{i=1}^m \left(\tanh^{-1}(u_i^*(x)/\beta) \right)^2 + \|u^*(x) - \hat{\mu}(\bar{x}_j)\|^2. \quad (50)$$

Then, by using (26), we can see that

$$- \mathcal{W}(u^*(x)) + \Xi \leq \mathfrak{L}(x) + \|u^*(x) - \hat{\mu}(\bar{x}_j)\|^2 \quad (50)$$

with $\mathfrak{L}(x)$ defined as in (27). As indicated in the proof
of Theorem 1, $\mathfrak{L}(x)$ is bounded as $\|\mathfrak{L}(x)\| \leq \epsilon_M$. Thus,
combining (49) and (50), we have

$$558 \quad \dot{L}_2(t) \leq -\Psi(x) - x^\top Qx - \rho \left\| \hat{\vartheta}(\bar{x}_j) \right\|^2 + \epsilon_M \\ 559 \quad + \underbrace{\|u^*(x) - \hat{\mu}(\bar{x}_j)\|^2}_{\Lambda_1} + \rho \underbrace{\|v^*(x) - \hat{\vartheta}(\bar{x}_j)\|^2}_{\Lambda_2}. \quad (51)$$

Applying the inequality $\|y+z\|^2 \leq 2\|y\|^2 + 2\|z\|^2$ to Λ_1 in (51)
and using Assumption 3 as well as (32) and (35), it follows:

$$562 \quad \Lambda_1 = \left\| (u^*(x) - \mu^*(\bar{x}_j)) + (\mu^*(\bar{x}_j) - \hat{\mu}(\bar{x}_j)) \right\|^2 \\ 563 \quad \leq 2\|u^*(x) - \mu^*(\bar{x}_j)\|^2 + 2\|\mu^*(\bar{x}_j) - \hat{\mu}(\bar{x}_j)\|^2 \\ 564 \quad \leq 2\|G(\mathcal{A}_2(\bar{x}_j)) - G(\mathcal{A}_1(\bar{x}_j)) + \varepsilon_{\mu^*}(\bar{x}_j)\|^2 + 2K_{u^*}^2 \|e_j\|^2 \\ 565 \quad (52)$$

where $G(\mathcal{A}_\kappa(\bar{x}_j)) = G(\mathcal{A}_\kappa(x))|_{x=\bar{x}_j}$ with $G(\mathcal{A}_\kappa(x))$ defined
as in (42). By using (43) and Lemma 1 as well as Young's
inequality, we derive

$$569 \quad 2\|G(\mathcal{A}_2(\bar{x}_j)) - G(\mathcal{A}_1(\bar{x}_j)) + \varepsilon_{\mu^*}(\bar{x}_j)\|^2 \\ 570 \quad \leq 2\left(2g_M b_{\sigma_c} \|\tilde{\omega}_c\| + 2\sqrt{m} + b_{\varepsilon_{\mu^*}}\right)^2 \\ 571 \quad \leq 16g_M^2 b_{\sigma_c}^2 \|\tilde{\omega}_c\|^2 + 4a_0^2 \quad (53)$$

with $a_0 = 2\sqrt{m} + b_{\varepsilon_{\mu^*}}$.

Thus, combining (52) and (53), it follows:

$$574 \quad \Lambda_1 \leq 2K_{u^*}^2 \|e_j\|^2 + 16g_M^2 b_{\sigma_c}^2 \|\tilde{\omega}_c\|^2 + 4a_0^2. \quad (54)$$

Similar to the process of calculating Λ_1 , we obtain

$$576 \quad \Lambda_2 = \left\| (v^*(x) - \vartheta^*(\bar{x}_j)) + (\vartheta^*(\bar{x}_j) - \hat{\vartheta}(\bar{x}_j)) \right\|^2 \\ 577 \quad \leq 2\|\vartheta^*(\bar{x}_j) - \hat{\vartheta}(\bar{x}_j)\|^2 + 2\|v^*(x) - \vartheta^*(\bar{x}_j)\|^2 \\ 578 \quad \leq 2\left\| -\frac{h^\top(\bar{x}_j)}{2\rho} \nabla\sigma_c^\top(\bar{x}_j)\tilde{\omega}_c + \varepsilon_{\vartheta^*}(\bar{x}_j) \right\|^2 + 2K_{v^*}^2 \|e_j\|^2 \\ 579 \quad \leq 2K_{v^*}^2 \|e_j\|^2 + \left(h_M^2 b_{\sigma_c}^2 / \rho^2 \right) \|\tilde{\omega}_c\|^2 + 4b_{\varepsilon_{\vartheta^*}}^2. \quad (55)$$

Note that $\Psi(x)$ given in (5) and $\rho\|\hat{\vartheta}(\bar{x}_j)\|^2$ are non-negative
functions. Then, from (51), (54), and (55), we get

$$582 \quad \dot{L}_2(t) \leq -\lambda_{\min}(Q)\|x\|^2 + 4K_{\max}^2 \|e_j\|^2 \\ 583 \quad + \left(16g_M^2 + h_M^2/\rho^2\right) b_{\sigma_c}^2 \|\tilde{\omega}_c\|^2 + 4a_0^2 + 4b_{\varepsilon_{\vartheta^*}}^2 + \epsilon_M \\ 584 \quad (56)$$

with $K_{\max} = \max\{K_{u^*}, K_{v^*}\}$.

586 Taking the time derivative of $L_3(t)$ and using the weight
587 estimation error dynamics (39), it follows:

$$588 \quad \dot{L}_3(t) = -l_c \tilde{\omega}_c^\top \varphi \varphi^\top \tilde{\omega}_c + l_c \frac{\tilde{\omega}_c^\top \varphi}{1 + \phi^\top \phi} \varepsilon_H. \quad (57)$$

589 Noticing that $1 + \phi^\top \phi \geq 1$ and using the above men-
590 tioned Young's inequality, we develop the last term in
591 (57) as

$$592 \quad \frac{l_c}{1 + \phi^\top \phi} \tilde{\omega}_c^\top \varphi \varepsilon_H \leq \frac{l_c}{2(1 + \phi^\top \phi)} \left(\tilde{\omega}_c^\top \varphi \varphi^\top \tilde{\omega}_c + \varepsilon_H^\top \varepsilon_H \right) \\ 593 \quad \leq \frac{l_c}{2} \tilde{\omega}_c^\top \varphi \varphi^\top \tilde{\omega}_c + \frac{l_c}{2} \varepsilon_H^\top \varepsilon_H.$$

594 Then, (57) yields

$$595 \quad \dot{L}_3(t) \leq -\frac{l_c}{2} \tilde{\omega}_c^\top \varphi \varphi^\top \tilde{\omega}_c + \frac{l_c}{2} \varepsilon_H^\top \varepsilon_H \\ 596 \quad \leq -\frac{l_c}{2} \lambda_{\min}(\varphi \varphi^\top) \|\tilde{\omega}_c\|^2 + \frac{l_c}{2} b_{\varepsilon_H}^2. \quad (58)$$

597 By using (56) and (58), we can see that

$$598 \quad \dot{L}(t) \leq -2\gamma \lambda_{\min}(Q) \|x\|^2 - (1 - 2\gamma) \lambda_{\min}(Q) \|x\|^2 \\ 599 \quad - \left(\frac{l_c}{2} \lambda_{\min}(\varphi \varphi^\top) - (16g_M^2 + h_M^2/\rho^2) b_{\sigma_c}^2 \right) \|\tilde{\omega}_c\|^2 \\ 600 \quad + 4K_{\max}^2 \|e_j\|^2 + 4a_0^2 + 4b_{\varepsilon_{\theta^*}}^2 + \epsilon_M. \quad (59)$$

601 If the condition (46) holds, then (59) yields

$$602 \quad \dot{L}(t) \leq -2\gamma \lambda_{\min}(Q) \|x\|^2 + 4a_0^2 + 4b_{\varepsilon_{\theta^*}}^2 + \epsilon_M \\ 603 \quad - \left(\frac{l_c}{2} \lambda_{\min}(\varphi \varphi^\top) - (16g_M^2 + h_M^2/\rho^2) b_{\sigma_c}^2 \right) \|\tilde{\omega}_c\|^2.$$

604 Under the condition (47), we can find that $\dot{L}(t) < 0$
605 only if we can ensure one of the following inequalities
606 holds:

$$607 \quad \|x\| > \sqrt{\frac{4a_0^2 + 4b_{\varepsilon_{\theta^*}}^2 + \epsilon_M}{2\gamma \lambda_{\min}(Q)}} \triangleq c_1 \quad (60)$$

608 OR

$$609 \quad \|\tilde{\omega}_c\| > \sqrt{\frac{8a_0^2 + 8b_{\varepsilon_{\theta^*}}^2 + 2\epsilon_M}{l_c \lambda_{\min}(\varphi \varphi^\top) - (32g_M^2 + 2h_M^2/\rho^2) b_{\sigma_c}^2}} \triangleq c_2. \quad (61)$$

610 Then, uniform ultimate boundedness of both $x(t)$ and $\tilde{\omega}_c$
611 is obtained by using Lyapunov extension theorem [47].
612 Meanwhile, the ultimate bounds of $x(t)$ and $\tilde{\omega}_c$ are c_1 given
613 in (60) and c_2 given in (61), respectively.

614 *Situation II:* Events are triggered, i.e., $t = t_j, j \in \mathbb{N}$. Then,
615 we take the difference of Lyapunov function candidate $L(t_j)$
616 into account, that is

$$617 \quad \Delta L(t_j) = V^*(\bar{x}_{j+1}) - V^*(\bar{x}_j) + \Pi(x(t_j^+), \bar{x}_j)$$

618 where $x(t_j^+) = \lim_{\eta \rightarrow 0^+} x(t_j + \eta)$ with $\eta \in (0, t_{j+1} - t_j)$, and

$$619 \quad \Pi(x(t_j^+), \bar{x}_j) = V^*(x(t_j^+)) - V^*(x(t_j)) \\ 620 \quad + \frac{1}{2} \tilde{\omega}_c^\top(t_j^+) \tilde{\omega}_c(t_j^+) - \frac{1}{2} \tilde{\omega}_c^\top(t_j) \tilde{\omega}_c(t_j).$$

Suppose that $x(t) \notin E_{c_1} = \{x(t) \in \mathbb{R}^n \mid \|x(t)\| \leq c_1\}$ 621
or $\tilde{\omega}_c \notin E_{c_2} = \{\tilde{\omega}_c \in \mathbb{R}^n \mid \|\tilde{\omega}_c\| \leq c_2\}$. Then, from 622
Situation I, we have $dL(t)/dt < 0 \forall t \in [t_j, t_{j+1})$. That is, 623
 $L(t)$ is strictly monotonically decreasing on $[t_j, t_{j+1})$. Thus, it 624
implies 625

$$L(t_j) > L(t_j + \eta) \quad \forall \eta \in (0, t_{j+1} - t_j). \quad (62) \quad 626$$

Taking $\eta \rightarrow 0^+$ over both sides of (62), we can conclude 627

$$L(t_j) \geq \lim_{\eta \rightarrow 0^+} L(t_j + \eta) = L(t_j^+). \quad 628$$

Thus, we have 629

$$V^*(x(t_j)) + \frac{1}{2} \tilde{\omega}_c^\top(t_j) \tilde{\omega}_c(t_j) \geq V^*(x(t_j^+)) + \frac{1}{2} \tilde{\omega}_c^\top(t_j^+) \tilde{\omega}_c(t_j^+). \quad 630 \quad (63) \quad 631$$

From (63), it follows: 632

$$\Pi(x(t_j^+), \bar{x}_j) \leq 0. \quad (64) \quad 633$$

On the other hand, the uniform ultimate boundedness of the 634
state $x(t)$ in Situation I implies 635

$$V^*(\bar{x}_{j+1}) \leq V^*(\bar{x}_j). \quad (65) \quad 636$$

Therefore, under the condition that $x(t) \notin E_{c_1} = \{x(t) \in \mathbb{R}^n \mid \|x(t)\| \leq c_1\}$ (or $\tilde{\omega}_c \notin E_{c_2} = \{\tilde{\omega}_c \in \mathbb{R}^n \mid \|\tilde{\omega}_c\| \leq c_2\}$), we can conclude that $\Delta L(t_j) < 0$ based on (64) and (65). According to [53], uniform ultimate boundedness of $x(t)$ and $\tilde{\omega}_c$ is guaranteed. Meanwhile, the ultimate bounds of $x(t)$ and $\tilde{\omega}_c$ are c_1 given in (60) and c_2 given in (61), respectively. ■ 643

V. SIMULATION STUDY 644

This section presents two examples to show the effec- 645
tiveness and applicabilities of the established theoretical 646
results. 647

A. Example 1: Nonlinear Plants 648

We study the continuous-time nonlinear system with a 649
mismatched perturbation given by 650

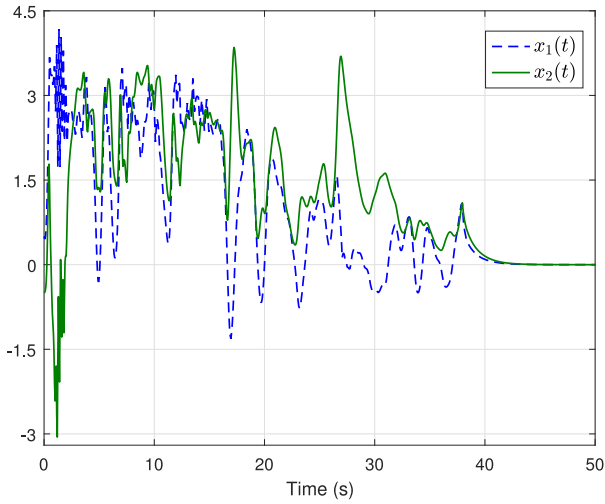
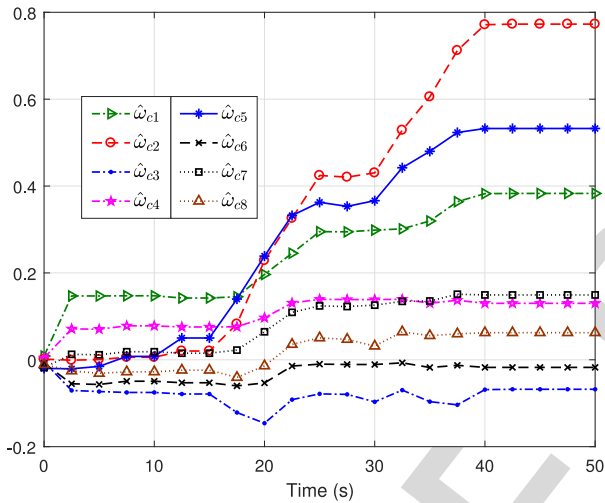
$$\dot{x}_1 = -x_1 + x_2 + \delta_1 x_1 \cos\left(\frac{1}{x_2 + \delta_2}\right) + \delta_3 x_2 \sin(x_1 x_2) \quad 651 \\ \dot{x}_2 = -0.5(x_1 + x_2) + 0.5x_2 \sin^2(x_1) + \sin(x_1)u \quad (66) \quad 652$$

where $x = [x_1, x_2]^\top \in \mathbb{R}^2$ is the state, $u \in \{u \in \mathbb{R} \mid |u| \leq \beta\}$ is 653
the control input, and $\delta_\varsigma, \varsigma = 1, 2, 3$, are unknown parameters. 654
In this example, we set $\beta = 2$ and randomly choose $\delta_1 \in$ 655
 $[-\sqrt{2}/2, \sqrt{2}/2]$, $\delta_2 \in [-100, 100]$, and $\delta_3 \in [-\sqrt{2}/2, \sqrt{2}/2]$. 656
The initial state is $x_0 = [0.5, -0.5]^\top$. 657

The mismatched perturbation in system (66) is 658

$$d(x) = \delta_1 x_1 \cos\left(\frac{1}{x_2 + \delta_2}\right) + \delta_3 x_2 \sin(x_1 x_2). \quad 659$$

After making some computations, we obtain $\|d(x)\| \leq \|x\|$. 660
Hence, we can let $d_M(x) = \|x\|$. Since $g(x) = [0, \sin(x_1)]^\top$ 661
and $k(x) = [1, 0]^\top$, we have $g(x)g^+(x)k(x) = 0$. Then, 662


 Fig. 2. Evolution of auxiliary system states $x_1(t)$ and $x_2(t)$ in Example 1.

 Fig. 3. Convergence of critic network weight vector \hat{w}_c in Example 1.

based on (4), the auxiliary system related to (66) can be proposed as

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -x_1 + x_2 \\ -0.5(x_1 + x_2 - x_2 \sin^2(x_1)) \end{bmatrix} + g(x)u + k(x)v \quad (67)$$

with $g(x) = [0, \sin(x_1)]^T$, $k(x) = [1, 0]^T$, and $v \in \mathbb{R}$.

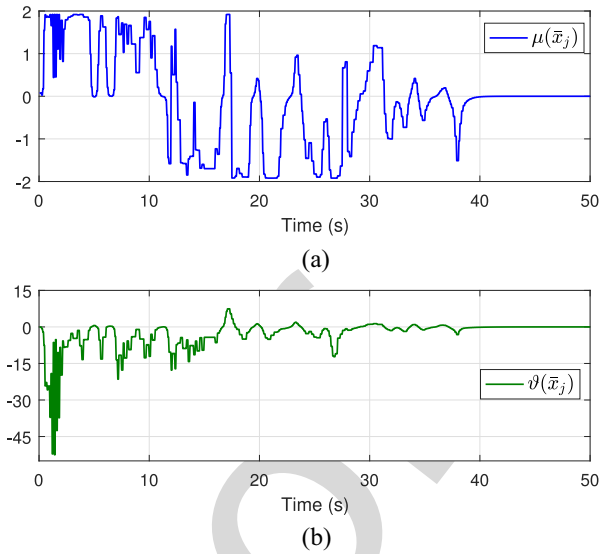
Since $\|g^+(x)k(x)d(x)\| = 0$, we choose $\ell_M(x) = 0$. Let $\rho = 0.25$ and $Q = I_2$. Then, based on (5), the cost function for system (67) can be given as

$$V^{u,v}(x_0) = \int_0^\infty (1.25\|x\|^2 + \mathcal{W}(u) + 0.25v^T v) dt$$

where

$$\begin{aligned} \mathcal{W}(u) &= 2 \int_0^u \beta \tanh^{-1}(\zeta/\beta) d\zeta \\ &= 2\beta u \tanh^{-1}(u/\beta) + \beta^2 \ln(1 - u^2/\beta^2). \end{aligned} \quad (68)$$

To obtain the optimal ETC, we employ the critic network (34). The parameters used in the critic network and the event-triggering condition (46) are given as follows:


 Fig. 4. (a) ETC $\mu(\bar{x}_j)$. (b) Auxiliary ETC $\vartheta(\bar{x}_j)$.

$l_c = 0.5$, $\tilde{n}_c = 8$, $\gamma = 0.3$, and $K_{\max} = 3.5$. The basic function vector used in the critic network is

$$\sigma_c(x) = [x_1^2, x_2^2, x_1 x_2, x_1^4, x_2^4, x_1^3 x_2, x_1^2 x_2^2, x_1 x_2^3]^T. \quad (680)$$

The weight vector in the critic network is written as $\hat{w}_c = [\hat{w}_{c1}, \hat{w}_{c2}, \dots, \hat{w}_{c8}]^T$. Furthermore, to ensure φ to be persistently exciting, we add the exploration noise $n_e(t) = 12e^{-0.05t}[\sin^2(t)\cos(t) + \sin^2(2t)\cos(0.1t) + \sin^2(-1.2t)\cos(0.5t) + \sin^5(t) + \sin^2(1.12t) + \cos(2.4t)\sin^3(2.4t)]$ into the control at the first 38 s.

Remark 5: Choosing appropriate basic function vectors for critic networks is a challenging issue. Because the number of the elements in the basis function vector is closely associated with the number of neurons in the critic network. In this example, the basic function vector is determined via computer simulations. We find that selecting the basic function vector as the above mentioned $\sigma_c(x)$ can lead to desirable results. In Example 2, the basic function vector is also determined by using computer simulations.

The evolution of auxiliary system states is illustrated in Fig. 2. As displayed in Fig. 2, the auxiliary system states $x_1(t)$ and $x_2(t)$ turn out to be asymptotically stable. The convergence of the critic network weight vector \hat{w}_c is shown in Fig. 3. It can be seen that, after the first 40 s, the critic network weight vector converges to $\hat{w}_c^{\text{final}} = [0.383, 0.773, -0.068, 0.130, 0.533, -0.018, 0.149, 0.062]^T$. Fig. 4(a) and (b) describes the ETC $\mu(\bar{x}_j)$ and the auxiliary ETC $\vartheta(\bar{x}_j)$. The validity of condition (17) is verified by presenting Fig. 5. As indicated in Fig. 5, (17) holds only if $t \geq 40$ s (i.e., $t_s = 40$ s). Fig. 6(a) and (b) shows the two norms (i.e., the norm of the event-triggering condition $\|e_j\|$ and the norm of the event-triggering threshold $\|\bar{e}_T\|$) and the sampling period T_s , respectively. Observing Fig. 6(b), we can find that $\min T_s = 0.1$ s. Actually, there are 289 state samples in Fig. 6(b), which indicates that only 289 state samples are necessary to implement the ETC algorithm. Nevertheless, under the same

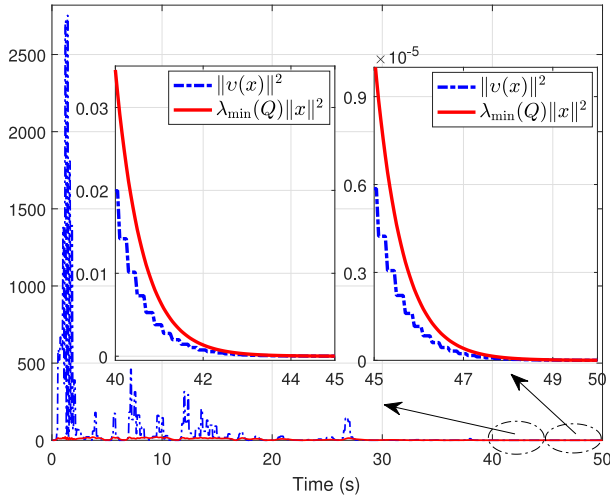
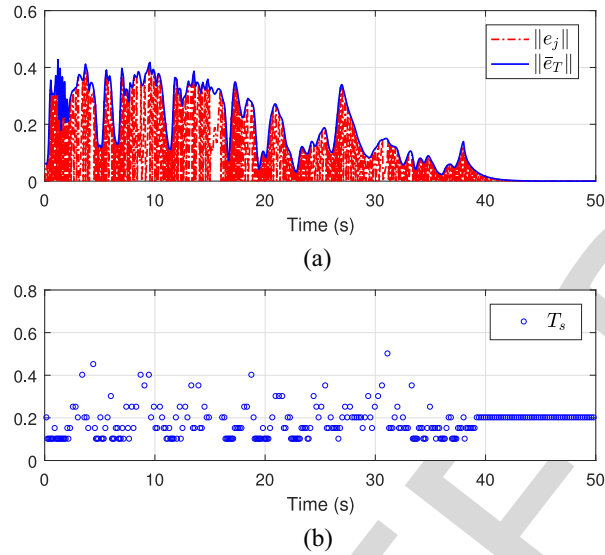


Fig. 5. Verification of condition (17) in Example 1.

Fig. 6. (a) Norm of the event-triggering condition $\|e_j\|$ and norm of the event-triggering threshold $\|\bar{e}_T\|$. (b) Sampling period T_s in Example 1.

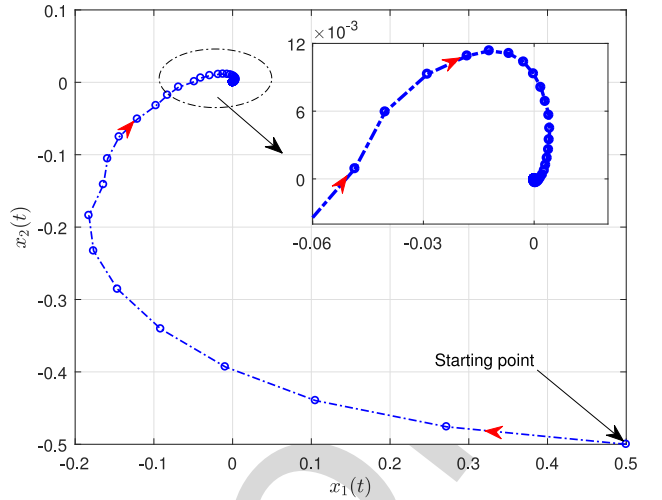
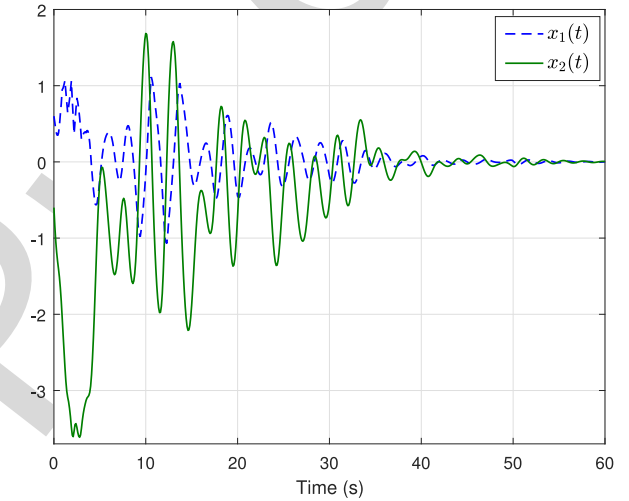
714 condition, there are 1000 state samples utilized to imple-
 715 ment the time-triggering control algorithm. Consequently, the
 716 present ETC strategy reduces the controller updates up to
 717 71.1%. In this sense, the computational burden is remarkably
 718 decreased. Substituting the above obtained weight vector $\hat{\omega}_c^{\text{final}}$
 719 to (35), we derive the approximate optimal ETC. Fig. 7 dis-
 720 plays the states of closed-loop system (66). From Fig. 7, we
 721 can see that the states of system (66) are stable under the
 722 approximate ETC.

723 B. Example 2: Application to the Pendulum System

724 We consider the pendulum system given in [19] as

$$725 \begin{cases} \frac{d\theta}{dt} = v + d \\ J \frac{dv}{dt} = u - Mgl \sin(\theta) - f_d \frac{d\theta}{dt} \end{cases} \quad (69)$$

726 with the current angle position of the pendulum $\theta \in \mathbb{R}$, the
 727 angular velocity $v \in \mathbb{R}$, the perturbation $d \in \mathbb{R}$, the control
 728 $u \in \{u \in \mathbb{R} : |u| \leq 1\}$ (note: $\beta = 1$), the mass of the pendulum

Fig. 7. States $x_1(t)$ and $x_2(t)$ of closed-loop system (66).Fig. 8. Evolution of auxiliary system states $x_1(t)$ and $x_2(t)$ in Example 2.

729 $M = 4/3$ kg, the acceleration of gravity $g = 9.8$ m/s², the
 730 length of the pendulum $l = 3/2$ m, the rotary inertia $J =$
 731 $4/3MI^2$ kg \cdot m², and the frictional factor $f_d = 0.2$. We assume
 732 that $d = \delta_1 \theta \sin(\delta_2 v)$ with δ_1 and δ_2 randomly chosen within
 733 the intervals $[-\sqrt{2}/2, \sqrt{2}/2]$ and $[-2, 2]$, respectively.

734 Let $x_1 = \theta$ and $x_2 = v$. Observing that $g(x) =$
 735 $[0, 0.25]^T$ and $k(x) = [1, -0.2]^T$, we obtain $h(x) =$
 736 $(I_2 - g(x)g^+(x))k(x) = [1, 0]^T$. Then, according to (4), the
 737 auxiliary system related to (69) can be proposed as

$$738 \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} x_2 \\ -4.9 \sin(x_1) - 0.2x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 0.25 \end{bmatrix} u + \begin{bmatrix} 1 \\ 0 \end{bmatrix} v. \quad (70)$$

739 The initial state is $x_0 = [0.6, -0.6]^T$. Since $d(x) =$
 740 $\delta_1 x_1 \sin(\delta_2 x_2)$, we have that $\|d(x)\| \leq \sqrt{2}/2 \|x\|$ and
 741 $\|g^+(x)k(x)d(x)\| \leq 0.4\sqrt{2} \|x\|$. Therefore, we choose $d_M(x) =$
 742 $(\sqrt{2}/2) \|x\|$ and $\ell_M(x) = 0.4\sqrt{2} \|x\|$ to satisfy Assumption 2.
 743 Selecting $\rho = 0.4$, $Q = I_2$, and using (5), we can present the
 744 cost function for system (70) as follows:

$$745 V^{u,v}(x_0) = \int_0^\infty (1.84 \|x\|^2 + \mathcal{W}(u) + 0.4v^T v) dt$$

746 with $\mathcal{W}(u)$ defined as in (68).

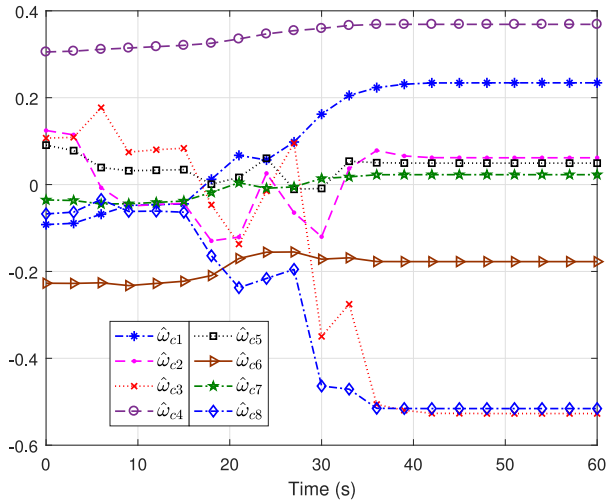
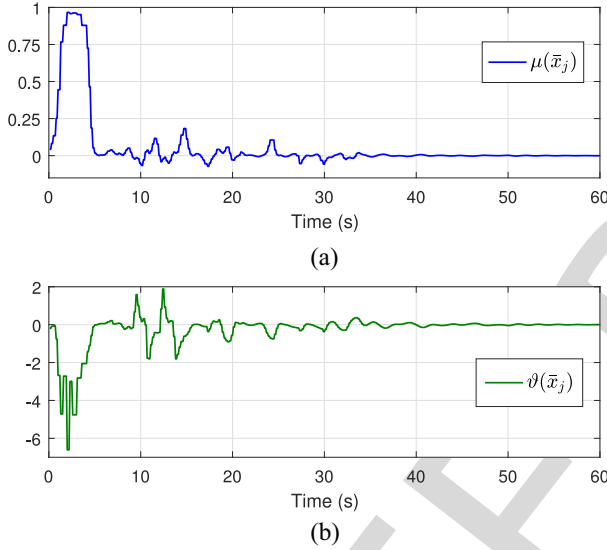
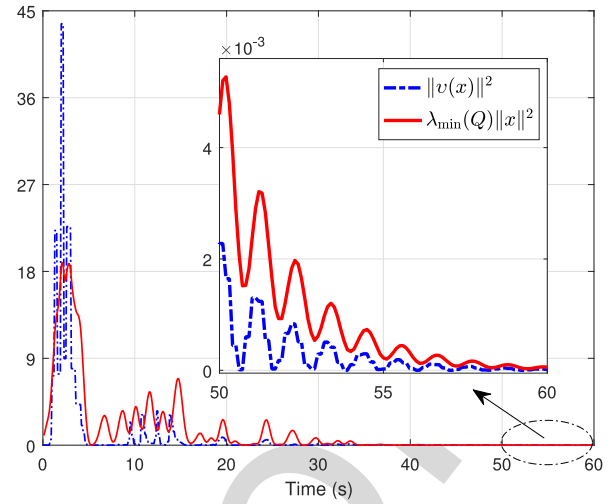
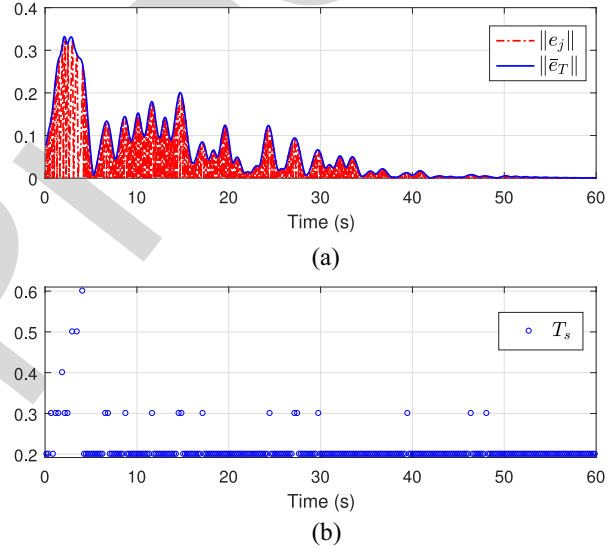

 Fig. 9. Convergence of critic network weight vector $\hat{\omega}_c$ in Example 2.

 Fig. 10. (a) ETC $\mu(\bar{x}_j)$. (b) Auxiliary ETC $\vartheta(\bar{x}_j)$.


Fig. 11. Verification of condition (17) in Example 2.


 Fig. 12. (a) Norm of the event-triggering condition $\|e_j\|$ and norm of the event-triggering threshold $\|\bar{e}_T\|$. (b) Sampling period T_s in Example 2.

747 The critic network given as in (34) is applied to derive the
 748 optimal ETC law for system (70). The parameters employed
 749 in the critic network and the event-triggering condition (46)
 750 are the same as in Example 1. The basic function vector used
 751 in the critic network is

$$752 \quad \sigma_c(x) = [x_1^2, x_2^2, x_1x_2, x_1^4, x_2^4, x_1^3x_2, x_1^2x_2^2, x_1x_2^3]^\top$$

753 and the weight vector in the critic network is denoted
 754 as $\hat{\omega}_c = [\hat{\omega}_{c1}, \hat{\omega}_{c2}, \dots, \hat{\omega}_{c8}]^\top$. To ensure φ to be persis-
 755 tently exciting, we add the following exploration noise
 756 $n_e(t) = 3e^{-0.15t}[\sin^2(t)\cos(t) + \sin^2(2t)\cos(0.1t) +$
 757 $\sin^2(-1.2t)\cos(0.5t) + \sin^5(t) + \sin^2(1.12t) +$
 758 $\cos(2.4t)\sin^3(2.4t)]$ into the control at the first 50 s.

759 The evolution of auxiliary system states is displayed in
 760 Fig. 8. As illustrated in Fig. 8, the auxiliary system states
 761 $x_1(t)$ and $x_2(t)$ are UUB. The convergence of the weight vec-
 762 tor $\hat{\omega}_c$ is depicted in Fig. 9. It can be observed that, after
 763 the first 50 s, the critic network weight vector converges to
 764 $\hat{\omega}_c^{\text{final}} = [0.234, 0.062, -0.527, 0.369, 0.049, -0.177, 0.023,$

$-0.516]^\top$. Fig. 10(a) and (b) indicates the ETC $\mu(\bar{x}_j)$ and the
 765 auxiliary ETC $\vartheta(\bar{x}_j)$. The validity of condition (17) is veri-
 766 fied through Fig. 11. As shown in Fig. 11, (17) holds only if
 767 $t \geq 50$ s (i.e., $t_s = 50$ s). Fig. 12(a) and (b) describes the two
 768 norms (i.e., the norm of the event-triggering condition $\|e_j\|$
 769 and the norm of the event-triggering threshold $\|\bar{e}_T\|$) and the
 770 sampling period T_s , respectively. From Fig. 12(b), we can see
 771 that $\min T_s = 0.2$ s. In fact, there are 284 state samples in
 772 Fig. 12(b), which shows that only 284 state samples are neces-
 773 sary to implement the ETC algorithm. Nonetheless, under
 774 the same condition, there are 600 state samples required to
 775 implement the time-triggering control algorithm. Accordingly,
 776 the present ETC strategy reduces the controller updates up to
 777 52.67%. In this sense, the computational burden is remarkably
 778 decreased. Substituting the above derived weight vector $\hat{\omega}_c^{\text{final}}$
 779 to (35), we obtain the approximate optimal ETC. Fig. 13 dis-
 780 plays the states of closed-loop system (69). Observing Fig. 13,
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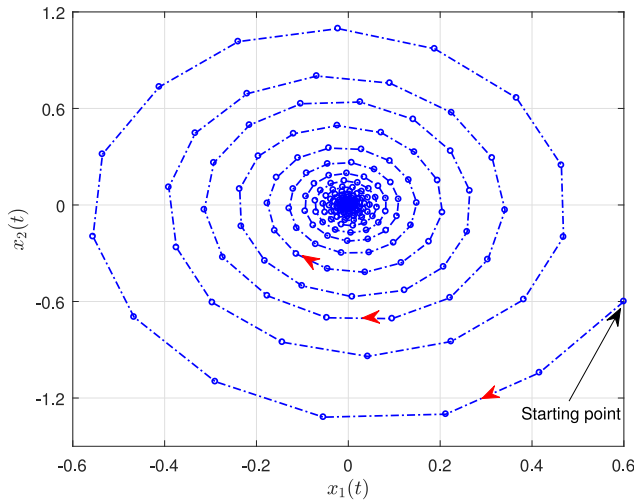


Fig. 13. States $x_1(t)$ and $x_2(t)$ of closed-loop system (69).

we can find that the approximate optimal ETC keeps the states of system (69) stable.

VI. CONCLUSION

This paper has presented a robust ETC method for nonlinear input-constrained systems with mismatched perturbations. By using an SN-ACD, the robust ETC law was obtained via solving the H_2 optimal control problem. Thus, the proposed control method can avoid the difficulty in judging the existence of saddle points, which arises in H_∞ optimal control problems. However, the developed robust ETC approach has to calculate the Moore–Penrose pseudo-inverse of the control matrix function and offer its upper bounded function. Indeed, this is a limitation when applying the present control strategy to nonlinear systems with complicated structures. Hence, how to relax this condition is one subject of our future studies.

On the other hand, this robust ETC approach is developed for a unique agent system. In recent years, ACDs have been utilized to study optimal regulations of multiagent systems [54], [55]. It is well-known that multiagent plants exist widely in engineering applications, such as the coordination of unmanned aerial vehicles. In addition, packet loss is an important issue arising in multiagent systems, especially networked multiagent systems. Recently, Lu *et al.* [56] proposed an effective model predictive tracking control strategy for networked systems subject to random packet loss and uncertainties. Accordingly, how to extend the SN-ACD to develop robust ETC schemes for multiagent systems with random packet loss and uncertainties is also one direction in our future research.

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