Broadband reduction of quantum radiation pressure noise via squeezed light injection

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The Heisenberg uncertainty principle states that the position of an object cannot be known with infinite precision, as the momentum of the object would then be totally uncertain. This momentum uncertainty then leads to position uncertainty in future measurements. When continuously measuring the position of an object, this quantum effect, known as back-action, limits the achievable precision.^{1,2} In audio-band, interferometer type gravitational wave (GW) detectors, this back-action effect manifests as quantum radiation pressure noise (QRPN) and will ultimately, but does not yet limit, sensitivity.³ Here we present the use of a quantum engineered state of light to directly manipulate this quantum back-action in a system where it dominates the sensitivity in the 10-50 kHz range. We observe a reduction of 1.2 dB in the quantum back-action noise. This experiment is a crucial step in realising QRPN reduction for future interferometric GW detectors and improving their sensitivity.

When GW detectors such as the Advanced Laser Interferometer Gravitational Wave Observatory (LIGO),⁴ Advanced Virgo, ⁵ and KAGRA, ⁶ reach their design sensitivity, quantum noise will be the dominant noise source across most of the detection band.³ Quantum noise arises from the quantum nature of the light used to probe the positions of the test masses.² The individual photons that comprise a coherent state are uncorrelated and fluctuations in their rate of arrival obey Poisson statistics. At the point of photo-detection, these fluctuations are referred to as shot noise (SN), and they limit the readout sensitivity. At the point when the photons reflect off the test mass, these fluctuations generate a fluctuating momentum transfer to the test mass and perturb its position; this is known as quantum radiation pressure noise (or sometimes, radiation pressure shot noise).

The injection of squeezed vacuum into the interferometer dark port allows the quantum noise to be

manipulated.² Phase quadrature squeezed light can reduce SN and has been demonstrated on previous generations of GW detectors at both GEO-600,^{7,8} and LIGO Hanford,⁹ and is now in routine operation in current GW detectors. The use of squeezing in the form of amplitude quadrature squeezed light to reduce the fluctuating radiation pressure force and hence QRPN has been demonstrated in a cryogenic microwave optomechanical system near the MHz-regime mechanical resonance frequency.¹⁰ Here we present a broadband audio frequency demonstration, at optical wavelength, and at room temperature.

As GW detectors approach their design sensitivity, it is important to study the effects of QRPN in relevant optomechanical systems. In addition to the injection of squeezed light, other QRPN mitigation techniques such as variational readout, ¹¹ conditional squeezing, ¹² and the use of negative mass systems, ¹³ have also been proposed to improve the low frequency sensitivity of GW detectors. The effects of QRPN were first observed with tabletop experiments. ^{10,14–17} These observations were all made at high frequencies (~MHz-GHz), around the resonance of the mechanical oscillator. This is due to the difficulty in reducing thermal and other classical noise sources below the QRPN level at low frequencies.

In contrast, GW detectors will be QRPN dominated at audio (\sim 10 Hz-kHz) frequencies over a large frequency band away from the \sim 1 Hz mechanical resonance. A direct measurement of QRPN under such conditions at room temperature has only recently been performed, ^{18,19} enabling the experiment reported here. We investigate the injection of squeezed light in a QRPN limited optomechanical system, and report the reduction of broadband QRPN at room temperature, away from the optical spring shifted mechanical resonance and at frequencies relevant to gravitational wave detectors.

The optomechanical system, shown in Figure 1, is a Fabry-Perot cavity with a micro-mechanical oscillator as one of the end mirrors. We use a low-loss single-crystal microresonator with low thermal noise to allow

the effects of QRPN to be observed at room temperature. The system is installed on a breadboard suspended by three 150 mm wire inside a vacuum chamber at 10^{-5} Pa in order to provide passive seismic and acoustic isolation. The microresonator consists of a roughly $70 \,\mu\mathrm{m}$ diameter mirror pad suspended from a single crystal GaAs cantilever with a thickness of 220 nm, width of $8 \,\mu\text{m}$, and a length of $55 \,\mu\text{m}$. The mirror pad is comprised of 23 pairs of quarter-wave optical thickness $GaAs/Al_{0.92}Ga_{0.08}As$ layers for a transmission of T =250 p.p.m. and exhibits both low optical losses and a high mechanical quality factor.^{20–22} The microresonator has an effective mass of 50 ng, a natural mechanical frequency of $\Omega_m = 2\pi \times 876 \,\mathrm{Hz}$, and a measured mechanical quality factor of $Q_m = 16000$ at room temperature.¹⁸ The cavity has a length of $9 \pm 1 \, \text{mm}$, a finesse of $\mathcal{F} \approx 13000$ and linewidth (HWHM) of $2\pi \times 580 \, \text{kHz}$.

A 1064 nm Nd:YAG laser is used to probe the optomechanical cavity and is detuned above the cavity resonance frequency which results in a strong optical spring effect.²³ The optical spring self-locks the cavity for frequencies below the optical spring resonance, however the phase lag due to the finite cavity response results in an antidamping force, rendering the system unstable.^{24,25} The optical spring effect is stabilised by monitoring the cavity reflection and transmission field, and providing active feedback around the optical spring frequency to the laser power and frequency via an electro-optic amplitude modulator (AM) and phase modulator (PM). 18,26 In the final measurement configuration, only the reflected light and PM feedback loop is used to lock the cavity at a detuning of about 0.6 linewidths, with the optical spring increasing the mechanical resonance frequency to 140 kHz.

The squeezed vacuum state is generated from a subthreshold degenerate optical parametric oscillator (OPO) via the parametric down conversion process. The OPO is a doubly resonant bow tie cavity with a nonlinear crystal made of periodically poled potassium titanyl phosphate (PPKTP) placed within the cavity, and is pumped by light tapped from the main laser that has been frequencydoubled to 532 nm via a second harmonic generation (SHG) cavity.^{27,28} The OPO is kept on resonance with the pump light via RF reflection locking with 70 MHz sidebands generated from PM_{OPO} monitored at photodetector PD_{OPO}. Squeezed light is injected into the cavity by combining the main laser field with the squeezed vacuum state via an asymmetric 97:3 beamsplitter (BS_{SOZ}). Spatial mode mismatch is filtered out by passing the combined field through a short optical fiber before the optomechanical cavity (not shown in the experimental schematic). An intensity stabilisation servo (ISS) is used to suppress the main laser down to an out-of-loop relative intensity noise of $2.6 \times 10^{-8} \,\mathrm{Hz^{-1/2}}$. This resulted in a greater than 10 dB clearance below the shot noise level at an optical power of $25 \,\mu\mathrm{W}$ used for the final measurement.

The control of the squeezing angle with respect to the main laser is achieved with a coherent locking scheme 29,30

which utilises a coherent locking field (CLF) laser frequency shifted from the main laser by 12.5 MHz. The frequency difference between the two lasers is maintained by up-converting a small portion of the CLF laser to 532 nm and phase locking the 25 MHz beat note between the up-converted field and the OPO pump field detected at photodetector PD_{CLF-G}. The unconverted (1064 nm) CLF beam co-propagates with the squeezed vacuum field and is phase locked with the main laser after BS_{SQZ} at 12.5 MHz measured at photodetector PD_{CLF-R}. Engaging both the CLF phase locks allows the squeezing ellipse angle to track the phase of the main laser field. Rotation of the squeezed ellipse between the amplitude and phase quadrature is achieved by changing the demodulation phase between the two CLF phase locks. Figure 2 shows the performance of the squeezer, which to the best of our knowledge, is the lowest frequency at which bright squeezed light has been produced in nonlinear crystal based systems (see Supplementary Information).

Figure 3 shows the displacement spectral density measured at $\rm PD_{\rm M}$ with 220 mW of circulating power. The broad peak at 140 kHz is the mechanical fundamental frequency shifted up by the optical spring effect. 26 The dominant noise source below 10 kHz is the thermal noise of the microresonator which follows a structural damping model between 200 Hz to 30 kHz, and falls off as $1/f^{1/2}$ compared to QRPN. 18 This $1/f^{1/2}$ difference in scaling between the QRPN and thermal noise is what allows the QRPN to dominate above 10 kHz. With 220 mW of circulating power, QRPN is the dominant noise source between 10 kHz and 50 kHz. The excess thermal noise above 30 kHz is believed to be related to thermoelastic damping. 18

The spectrum is calibrated by dividing the measured noise spectrum by the transfer function from the main laser piezo to the cavity reflection port. The laser piezo actuates on the main laser frequency and has been calibrated separately. The transfer function measures the closed loop response of the system, and undoes the effect of both the electronic feedback and the optical spring response. The optical spring effect is reintroduced in the spectrum by measuring separately the optical spring frequency and cavity detuning. A 11.2 kHz dither tone on the cavity length is used to produce a calibration line, shown in the inset of Figure 4, to ensure the calibration is constant for all the measurements. The laser piezo is calibrated in frequency which allows the spectrum to be calibrated in terms of displacement based on the cavity length.

In order to manipulate the QRPN, bright squeezed light is injected into the cavity, which affects the measured displacement spectrum as shown in Figure 4. With the injection of amplitude quadrature squeezed light, we observe a reduction of the total noise floor at frequencies where QRPN is dominant, with a maximum reduction of $1.2\,\mathrm{dB}$ at around $20\,\mathrm{kHz}$. Even though thermal noise is the dominant noise source below $10\,\mathrm{kHz}$, QRPN is still a major contributor to the total noise and the reduction in

noise due to squeezed light injection remains visible below 2 kHz. By changing the relative phase between the two CLF locks, we are able to rotate the squeezing ellipse to produce phase quadrature squeezed light, resulting in an increase of the total noise by 12.6 dB at 20 kHz. The flat and broadband nature of the increase is consistent with quantum noise being manipulated. Figure 5 shows the noise reduction and enhancement across the measurement spectrum and averaged between 19 and 23 kHz where the largest reduction occurred. The amount of noise reduction observed is currently limited by losses in the system. We estimate with a pure squeezed state injected into the cavity, the maximum noise reduction is 2.6 dB given the losses in the system. The details of the loss analysis are presented in the Supplementary Information.

We presented the reduction of quantum radiation pressure noise of a microresonator away from the optical spring shifted mechanical resonance over a broad frequency range via the injection of squeezed light. This is a step towards reducing the radiation pressure noise occuring in future interferomtric gravitational wave observatories in order to improve their sensitivity and detection range. Moreover, a radiation pressure noise limited optomechanical system provides a useful testbed for other QRPN reduction proposals^{11,19,31–33} and quantum-enhanced displacement sensing.³⁴

With the optomechanical system at room temperature, the standard quantum limit (SQL)³⁵ is currently within a factor of five of the current noise level, with the system predominately dominated by quantum and thermal noise. By cryogenically cooling the microresonator and implementing QRPN cancellation techniques¹⁹ such as utilising the optical spring,³⁶ this paves the way to reach and surpass SQL.

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AUTHOR CONTRIBUTIONS

M.J.Y., J.C., and T.C. performed the investigation and formal analysis. D.E.M. and T.C. performed the conceptualisation. M.J.Y. performed writing - original draft; J.C., T.G.M., R.L.W., D.E.M., and T.C. performed writing - review and editing. G.L.M., T.G.M., P.H., D.F., and G.D.C. provided resources; T.G.M., R.L.W., B.J.J.S., D.E.M., and T.C. provided supervision.

DATA AVAILABILITY

The data that support the plots within this paper and other findings of this study are available from the corresponding author upon reasonable request

COMPETING INTERESTS

The authors declare no competing interests.

MATERIALS AND CORRESPONDENCE

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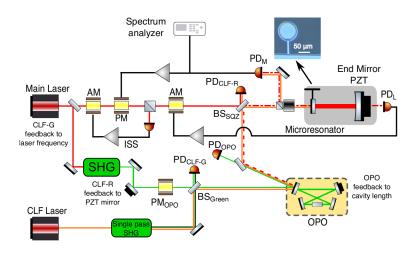


FIG. 1. Schematic of the experiment. Squeezed vacuum (dashed red) is generated from an Optical Parametric Oscillator (OPO) pumped by an optical field (green) at twice the main laser frequency from a Second Harmonic Generator (SHG). The squeezed vacuum state is then combined with the main laser (red) using a 97:3 beamsplitter (BS_{SQZ}) to produce a bright squeezed state (dotted dashed red). The bright squeezed state is injected into the in-vacuum optomechanical cavity which consists of the microresonator (shown in the inset) and a macroscopic end mirror. The reflected (transmitted) cavity field detected by photodetector PD_M (PD_L) is used to actively stabilise the optomechanical cavity. A secondary Coherent Locking Field (CLF) laser (orange and dark green) is used to control the squeezing quadrature via feedback to the main laser frequency and the OPO pump phase.

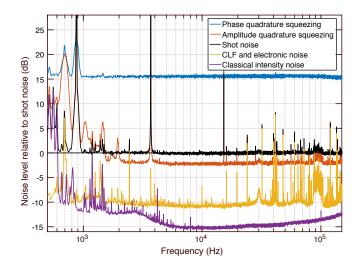


FIG. 2. Low frequency squeezed light. Squeezed light noise spectrum measured at the reflection port of the optomechanical cavity, with the cavity highly detuned. The out-of-loop classical laser intensity noise measured at PD_{CLF-R} is projected onto the same plot, showing a greater than 10 dB clearance from shot noise. Low frequency roll up of the amplitude quadrature squeezed spectrum is due to feedback noise coupling from the CLF locking loop.

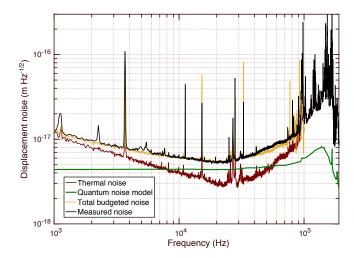


FIG. 3. **Noise budget.** Displacement spectral density of the microresonator with a 140 kHz optical spring resonance with contribution from various noise sources. The dominant noise sources are thermal noise (brown trace), and quantum noise (green trace) which is dominated by QRPN below the optical spring resonance. The thermal noise measurement was taken with low intracavity power, and closely follows a structural damping model. The quantum noise trace also takes into account the electronic dark noise level of the photodetector. The quadrature sum of the two noise sources (yellow trace) is overlaid with the measured displacement spectrum (black trace) with no squeezed light injection.

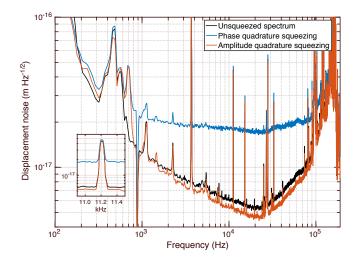


FIG. 4. Manipulation of QRPN with squeezed light. Calibrated displacement noise spectrum of the microresonator with the injection of squeezed light. Reference trace (black) is measured by tuning the OPO to its anti-resonance to ensure no squeezed light is generated. Injection of amplitude quadrature squeezed light (red) results in a maximum noise reduction of 1.2 dB at 20 kHz. Rotating the squeezed ellipse to the phase quadrature (blue) increased the total noise of the system. Inset: 11.2 kHz calibration line used in the three measurements.

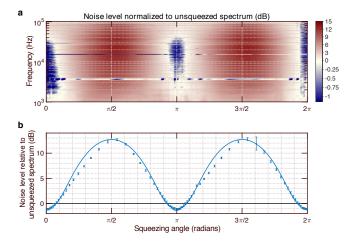


FIG. 5. Noise level as a function of squeezing angle. Displacement noise spectrum as a function of the squeezing phase, normalized to the reference spectrum $\bf a$, across the measurement frequency band and $\bf b$, averaged between 19 and 23 kHz. Horizontals lines at 3.7 kHz, 15 kHz and 28 kHz corresponds to the higher order mechanical modes of the microresonator. Phase quadrature squeezing occurs at $\pi/2$ radians, while amplitude quadrature squeezing occurs at π radians. The error bars represent the standard deviation of the noise level.