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Development, processing and applications of bio-sourced cellulose nanocrystal composites

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ABSTRACT

Plastic pollution concerns have catalyzed research into green materials with the specific goal of accessing new bio-derived and bio-degradable polymers with improved property profiles. One way to achieve these new materials is through the incorporation of nanofillers into bio-based polymer matrices. Cellulose nanocrystals (CNCs), which are extracted from biomass, have been investigated as one route to bio-based composites with enhanced performance. The combination of the excellent reinforcement capabilities of these bio-derived, nanosized particles along with relatively low production cost and biodegradability makes cellulose-based nanocomposites an attractive and promising approach to the next generation of green materials. Discussed herein is an overview of the use of CNCs to access reinforced bio-based nanocomposites, with particular focus on bio-available polyester and polysaccharide matrices. The characteristic changes provided by the incorporation of the nanofillers into the bio-based materials and their advantages and drawbacks are discussed. Specifically, the different parameters influencing mechanical reinforcement and barrier properties, such as the nature of processing, use of additives or CNC surface modifications are reviewed. Finally, the benefits of using CNC fillers in a number of potential future application areas, including polymer compatibilization, water purification, biomedical and electronics are outlined.

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Abbreviations: AR, aspect ratio; ATBC, acetyl tri-*n*-butyl citrate; BNA, becostat A B09 surfactant; CAB, cellulose acetate butyrate; CL, caprolactone; CNC, cellulose nanocrystal; CNF, cellulose nanofiber; CTE, coefficient of thermal expansion; DLA, D-lactic acid; DMA, dynamic mechanical analysis; DMAc, *N,N*-Dimethylacetamide; DMF, dimethylformamide; HDT, heat distortion temperature; MCC, micro-crystalline cellulose; MFC, microfibrillated cellulose; MWCNT, multi-walled carbon nanotubes; OLED, organic light emitting diode; PBAT, poly(butylene adipate terephthalate); PBS, poly(butylene succinate); PCL, polycaprolactone; PDLA, poly(D-lactic acid); PE, polyethylene; PEG, poly(ethylene glycol); PEO, poly(ethylene oxide); PHA, polyhydroxyalkanoate; PHB, poly(3-hydroxybutyrate); PLA, poly(lactic acid); PLLA, poly(L-lactic acid); PP, polypropylene; PS, polystyrene; SAXS, small-angle x-ray scattering; SEM, scanning electron microscopy; TEMPO, (2,2,6,6-Tetramethylpiperidin-1-yl)oxyl; Tg, glass transition temperature; Tm, melting temperature; WAXS, wide-angle x-ray scattering; WVP, water vapor permeability.

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1. Introduction

Ever since the existence of macromolecules was proposed 100 years ago by Hermann Staudinger, polymeric materials have played an ever-growing role in our daily life on account of their outstanding properties, which include robustness, light weight, versatility, facile processing and low cost [1]. As a consequence, there has been a meteoric rise in production of commodity plastics since the Second World War, and worldwide plastic production surpassed 340 million metric tons in 2017 (Fig. 1) [2–4]. When these materials were developed, major efforts were focused on increasing their useable lifetime and preventing degradation; however, with mass consumption of plastics, the end-of-life of these materials has become a growing concern. It is currently estimated that less than 10 % of all plastics produced are recycled, around 10 % are incinerated, with the remaining 80 % accumulating in landfills or littered into terrestrial and aquatic environments [5]. The majority of plastics produced today are petroleum-based, such as polyethylene (PE), polypropylene (PP) and polystyrene (PS), and can take hundreds of years to degrade. Furthermore, approximately ten tons of these plastics are discarded into the ocean every minute [6]. As such, unless significant changes occur, the plastic accumulation in our marine environment will continue to grow over the coming years, to the point that it has been predicted that the amount of plastic in the ocean will outweigh fish by 2050 [7]. The increase of non-biodegradable plastics in the environment is an ongoing global concern; for example, the 2019 Group of Twenty (G20) meeting on the global environment for sustainable growth proposed a framework for action to reduce marine plastic litter [8].

Considering the continued rise in plastic consumption and impending depletion of fossil fuel reserves, next generation plastic technologies need to keep the environment in mind and take necessary actions to harmonize with it. Towards this goal, the development of “sustainable” polymeric materials has attracted much attention in recent years [9–13]. By definition, these materials should be produced from non-damaging, renewable feedstocks

(a “green birth”) and be able to be easily recycled (a “green rebirth”) or quickly degraded into non-harmful components under mild environmental conditions (a “green death”) [14,15]. While such considerations are a good starting point for defining sustainability, it is important to recognize that one must also consider the wide range of factors that can play a part in the total emissions generated by a material over its entire life cycle, from initial planting to final degradation. For example, the use of pesticides during biomass growth and the energy needed to isolate the monomer/polymer from the feedstock are two factors that are not commonly considered and can push the total negative environmental impacts of bio-based materials beyond those of their fossil fuel counterparts [16]. As such, while not the focus of this review, it is important to note that any “sustainable” material system aiming for commercialization will need a full life cycle assessment to determine whether or not it is truly “more sustainable” than the existing solutions.

Additionally, while many bio-degradable polymers have been developed and commercialized as “environmentally friendly” plastics, most of these plastics are not currently sourced from renewable feedstocks. For example, polycaprolactone (PCL), poly(butylene adipate terephthalate) (PBAT) and poly(butylene succinate) (PBS) are biodegradable, but predominately use fossil fuel-based chemicals to access their monomers on a commercial scale [19]. Some small-scale operations produce a minor portion of these monomers from biomass fermentation [20], but while this is a step in the right direction, it is not yet at a scale to make the polymers’ life cycle sustainable. Increasing the percentage of these polyesters that are obtained from biomass-derived monomers is an active area of research [21] and if this can be achieved on a commercial scale, such polymers represent a significant advancement over their non-biodegradable alternatives. However, these polymers do not span the property matrix profiles that are available from the wide range of commercially available petroleum-based plastics.

Today there are two major classes of fully bio-based polymers that are commercially-viable, alkyl polyesters (predominantly poly(lactic acid) (PLA) [22] but also polyhydroxyalkonates (PHA)) [23] and carbohydrate-based [24] plastics. Unfortunately, these materials have relatively low thermal, physical and/or mechanical performance relative to their petroleum-based counterparts, which limits their use in many applications [25]. Indeed, the production percentage of bio-degradable and/or bio-based polymers was below 3 % of the total plastics market in 2017 [26]. While growing public concerns about the environment will continue to push the development and commercialization of sustainable polymers, improved material properties at a competitive cost will be a controlling factor in driving the growth of these “eco-friendly” plastics.

Among the different strategies used to improve the mechanical properties of sustainable polymers, the addition of nanofillers, such as graphene, titanium dioxide, calcium carbonate, silica, etc., appears to be a promising approach [27–30]. By controlling geometric dimensions, polymer-nanofiller interactions and particle dispersion, the incorporation of a small amount of nanofillers (usu-

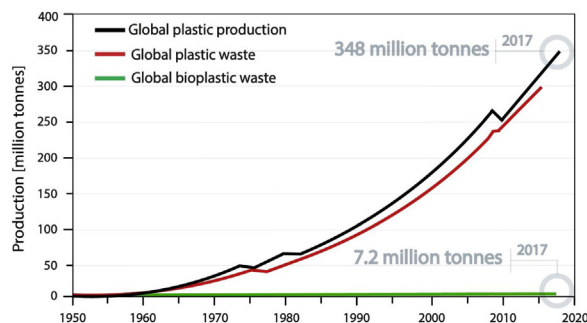


Fig. 1. Graph showing the increase in global plastic production (black), global plastic waste (red) and bio-derived plastic production (green) from 1950 to 2017 [17,18]. (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article).

ally less than 10 wt. %) has been shown to dramatically change the bulk material properties, such as improving strength, thermal resistance and gas permittivity [19,31]. However, the integration of non-bio-based or non-bio-degradable fillers into sustainable polymers diametrically opposes the material's sustainability and complicates recycling or composting processes. Thus, a focus on the development of sustainable bio-based nanofillers with renewable and degradable characteristics is of importance to achieve nanocomposite materials with sustainable lifecycles.

Among the various bio-based nanofiller materials, cellulose holds a key position as an abundant raw organic material that can be obtained from virtually inexhaustible biomass feedstocks, capable of meeting the increasing demand for green and bio-based products [32]. The use of cellulose as a material has been known since the beginning of civilization, from clothes and paper to its use in construction materials, yet over the past few decades there has been renewed interest in cellulose as a nanomaterial [33]. A variety of nanoparticles can be extracted from cellulose owing to its hierarchical structure and semi-crystalline nature (Fig. 2). Nanocelluloses are generally categorized by their size, aspect ratio and crystallinity, most often being divided into cellulose nanofibers (CNFs), which have relatively low degrees of crystallinity (ca. 60–80 %) and dimensions of nanometers in width and microns in length, and cellulose nanocrystals (CNCs) which are more crystalline (ca. > 85 %) but with aspect ratios generally less than 100. While CNFs have been employed as natural fillers for many polymer matrices including bio-based polymers, there have been a number of recent reviews that have summarized this work [34–37] and the interested reader is directed to these reviews for more information.

The focus of this review is on the other category of nanocellulose, namely cellulose nanocrystals and in particular on the use of CNCs to reinforce commercially-viable 100 % bio-based plastics. CNCs are isolated by extraction of the crystalline domains from the bio-sourced cellulosic material usually by a combination of mechanical and chemical processes [42]. Commonly, to obtain CNCs from the biomass cellulose, acid hydrolysis is carried out to degrade the amorphous connecting regions between crystals (Fig. 2). Broadly, CNCs are needle or rod-like nanoparticles that can be produced from diverse starting bio-sources (Table 1), such as wood, plants (bamboo, straw and grass, e.g. *Miscanthus x. giganteus* [43,44]) and select living organisms (e.g. bacteria, algae and sea tunicates). For clarity, a consistent naming scheme will be used throughout this review when discussing CNCs and their composites (Table 1). CNCs will be described by “*bio-source-CNC-functionality*”, so a tunicate CNC with sulfate half esters on its surface will be described as *t-CNC-SO₃⁻*.

As shown in Table 1, the length, diameter and aspect ratio of CNCs vary between 100–3000 nm, 3–50 nm and 5–200 respectively, depending on the biological source and isolation protocol [60]. Removal of the non-crystalline cellulose results in CNCs having a high degree of crystallinity, generally around 85 % or greater [61]. Depending on the bio-source and the isolation protocol, CNCs can have a tensile modulus as high as 140 GPa, a density of about 1.5 g cm⁻³ and a specific modulus around 90 GPa g⁻¹ cm³ [62]. This combination of size and strength gives the CNCs outstanding reinforcing potential and renders them competitive with other commercially available nanofillers, such as silica [63], carbon nanofibers [64] and nanoclays [65], as a strong candidate for nanocomposite applications. In fact, wood-based CNCs have already begun production on a plant scale and are commercially available [66].

The relatively high aspect ratio (AR) of CNCs when compared to spherical particles is an advantage for reinforcing polymers matrices as it defines the CNC loading required to form a percolating network throughout a material (higher AR means lower filling fractions are required for percolation) [67]. A dramatic increase in mechanical stiffness is observed when percolation is

achieved, making it an important consideration for the material's final properties. Despite these promising characteristics, there are still significant challenges to the use of CNCs in composite materials. In particular, the existence of hydroxyl groups on the surface of CNCs makes them hydrophilic in nature with a strong propensity for interparticle hydrogen bonding, causing agglomeration in polymer matrices, which significantly limits their reinforcement capability. However, it is important to note that most CNCs that are commercially available and reported in the literature are negatively charged, which enhances their dispersion in water and polar organic solvents. The surface negative charges are usually obtained during the CNC isolation procedure. As mentioned above CNCs are submitted to an acid treatment in order to remove the non-crystalline cellulose. If that acid treatment is sulfuric acid, then the surface of the CNCs will contain charged sulfate half-esters (CNC-SO₃⁻). Another common negatively charged CNC is carboxylate CNCs (CNC-CO₂⁻), usually prepared via a TEMPO/bleach oxidation process from uncharged CNCs (obtained through the use of HCl during the isolation process). The dispersibility of these charged CNCs in aqueous and polar solvents renders solvent casting a powerful strategy to optimize their dispersion in polymer matrices, and for this reason solvent casting is currently the most employed approach to prepare CNC nanocomposites [68]. In fact, CNC-based nanocomposites can be traced back to the pioneering work of Cavail , Chanzy and coworkers in the mid-1990's [69–72]. In these studies, they showed that sulfate functionalized CNCs obtained from either wheat straw or tunicin could be dispersed in an aqueous latex (of a styrene and butyl acrylate copolymer) solution and that a nanocomposite could be obtained by solution casting. The resulting film exhibited significant improvements in the mechanical strength of the material. Key to the success of this approach is both the latex and CNCs are dispersible in water, resulting in homogenous dispersions.

It is important to note that the surface hydroxyl groups of CNCs can be functionalized using various synthetic strategies making the CNCs more dispersible in hydrophobic solvents and polymers, however, one must remember that functionalization will also impact the reinforcement capability of the CNCs by altering the interactions of the nanofillers with themselves and the matrix [73].

CNCs by their bio-derived nature are already present in our ecosystems, albeit usually embedded in a composite structure with other components, such as lignin, amorphous cellulose and hemicelluloses. Nonetheless an important aspect that needs to be studied is their potential impact on human and environmental health. While, a complete story is not yet known and much more work remains to be done in this area to better understand their effects, this aspect of CNC research is starting to become more active. For example, Vartiainen and coworkers looked into *w-CNF* toxicity and found that no significant negative effects were observed in mouse and human cell viability tests [74]. An ecotoxicity test (*V. fischeri*) showed no effects of the *w-CNFs* below 300 mg/L and EC50 (effective concentration) values could not be obtained up to 2500 mg/L, meaning that the materials are safe unless concentrations are higher than those expected in worst-case environmental scenarios. More relevant to this review, the ecotoxicity of *w-CNC-SO₃⁻* has been investigated by Kovacs and coworkers in nine different aquatic species, with most species not being significantly affected. A greater than 25 % reduction in the reproduction in one species (the fathead minnow) was observed only at high concentrations of the *w-CNC-SO₃⁻* (> 290 mg/L) [75]. Preliminary studies into human/mammalian health have shown little-to-no oral toxicity, no dermal toxicity and generally low cytotoxicity at low concentrations. However, perhaps the biggest concern with any nanomaterial is its pulmonary toxicity [76]. Using a 3D *in vitro* triple cell coculture model of the human epithelial airway barrier, Rothen-Rutishauser and Weder observed that *c-CNC-SO₃⁻*, when

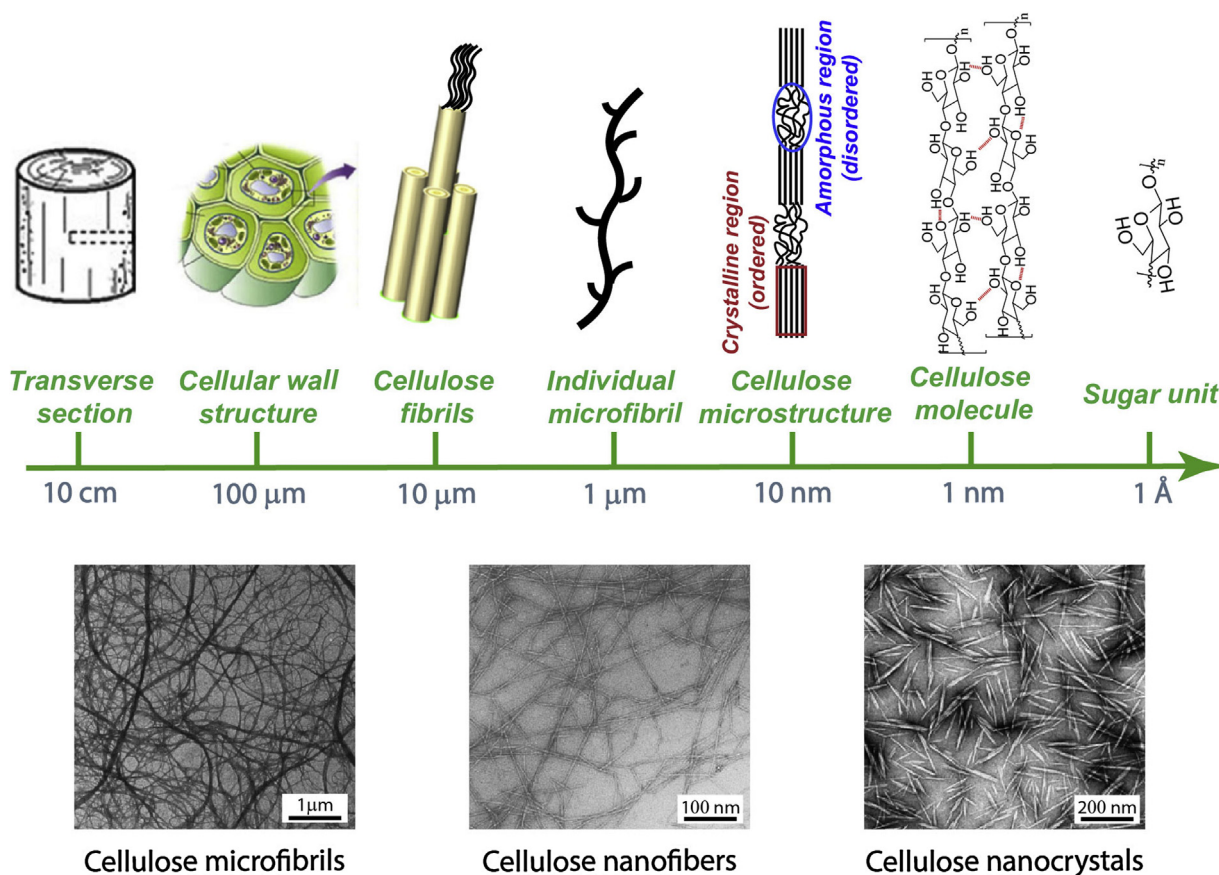


Fig. 2. Hierarchical structure of cellulose and transmission electron micrographs of cellulose microfibrils, nanofibers and nanocrystals [38–41]. Copyrights 1997, 2007, 2008, 2014, respectively. Adopted with permission from John Wiley & Sons Inc, the American Chemical Society, the Royal Society of Chemistry and Elsevier Science Ltd, respectively.

Table 1

List of common sources used to access CNCs, CNC nomenclature used in this article along with their corresponding approximate length, width and aspect ratio.

Bio-source	Abbreviation	Length	Width	Aspect Ratio	Reference
Wood	w-CNC	100–200	3–5	20–60	[45,46]
Cotton (and Filter Paper)	c-CNC	100–300	5–15	10–40	[47,48]
Ramie Fiber	rf-CNC	50–250	5–10	5–40	[40,49]
Tunicate	t-CNC	500–3000	10–30	10–200	[50,51]
Bamboo	bamboo-CNC	50–400	5–20	15–20	[52,53]
Bacteria	b-CNC	100–1000	5–50	5–200	[54,55]
Phormium tenax	ph-CNC	100–200	5–15	10–20	[56,57]
flax	f-CNC	100–500	10–30	10–50	[58,59]

delivered as an aqueous suspension, do elicit dose-dependent cytotoxicity and (pro-)inflammatory response, but at a level that is significantly lower than multiwalled carbon nanotubes or crocidolite asbestos fibers [77]. However, other studies by Shvedova and coworkers on w-CNC-SO₃[−] have shown that different and more adverse pulmonary outcomes can occur depending on whether the CNCs are in a suspension or are a freeze-dried powder [78].

Part of the challenge here is that there is not enough data at the moment to fully understand the effects of CNCs. Further complications arise as not all CNCs are created equal. For example, size and shape of the CNCs, as well as the nature of the functional groups on the CNCs will undoubtedly play a role in any ecological or biological effects. In addition, CNCs can be isolated using a range of protocols involving the use of different chemicals and different levels of purification, therefore leading to the fact that the different CNCs used in these studies may well have different levels of (toxic) contaminants. As such, there is certainly a need for more research in this area, the results of which will play an important role in the future of sustainable CNC composites.

2. CNC-reinforced bioderived polymers

2.1. Polysaccharide-based composites

Polysaccharides such as cellulose, starch, chitin, chitosan, alginates and various naturally occurring gums have attracted great interest as a source of sustainable polymers on account of their abundant supply, low cost, renewability, biodegradability and ease of chemical modification [79]. In addition, some polysaccharides and their derivatives also have good solubility in water, which readily disperses negatively charged CNCs, thus allowing for relatively facile access to composite materials.

2.1.1. Chitosan and alginate-based composites with negatively charged CNCs

Chitosan, derived from chitin the second most abundant natural polysaccharide after cellulose, is a natural linear polysaccharide consisting of (1→4)-2-amino-2-deoxy-β-D-glucan and is soluble in acidic water (Fig. 3). Chitosan has been investigated for use in

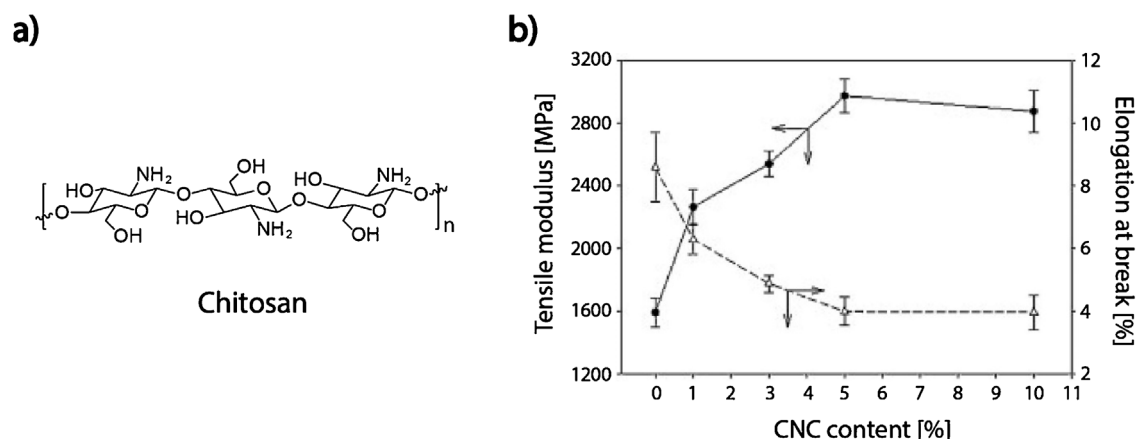


Fig. 3. a) Molecular structure of chitosan. b) Graphic showing the tensile modulus and the elongation at break of chitosan composites loaded with different $w\text{-CNC-SO}_3^-$ content [83]. Copyright 2012. Adopted with permission from Elsevier Science Ltd.

a variety of different applications including biomedical, packaging and as a thickening agent [80–82].

Chitosan/ $w\text{-CNC-SO}_3^-$ composite films have been prepared by simple aqueous mixing of a suspension of $w\text{-CNC-SO}_3^-$ with a 1 % w/v chitosan acidic solution followed by solvent casting. The resulting composites show roughly 80 % higher tensile modulus (ca. 3 vs. 1.6 GPa) and a 50 % reduction in elongation at break (4.0 vs. 8.6 %) with the inclusion of 5 wt. % $w\text{-CNC-SO}_3^-$ when compared to the neat chitosan films [83]. The increase in the mechanical strength was ascribed to the formation of strong ionic bonding interactions between the negatively charged $w\text{-CNC-SO}_3^-$ and positively charged amine groups on chitosan. In addition, the same filler content loading has been shown to lower the water vapor permeability (2.4 vs. 3.3 g·mm/m²/day/kPa) by 25 %, consistent with increased crystallinity induced by the incorporation of the CNCs. In fact, there are numerous reports that show mechanical property improvements in chitosan-based materials when CNCs are incorporated [84,85], specifically for applications in drug delivery [86], gas barrier [87] and filtration materials [88].

Alginate is another water-soluble polysaccharide (this time in basic solutions) from which CNC composites have been prepared and studied. For example, alginate/ $w\text{-CNC-SO}_3^-$ composite films prepared by solvent casting from an aqueous mixture of sodium alginate and $w\text{-CNC-SO}_3^-$ showed improved tensile strength relative to neat alginate. The tensile strength increased with $w\text{-CNC-SO}_3^-$ content up to the addition of 5 wt. % (tensile strength of ca. 80 MPa vs ca. 55 MPa for neat alginate) [89]. The presence of carboxylate moieties on the alginate means that alginate gels can be formed through the addition of Ca^{2+} ions on account of the formation of carboxylate- Ca^{2+} -carboxylate salt bridges (Fig. 4a) [90]. A number of reports in the literature investigate alginate/CNC hydrogels and aerogels crosslinked with Ca^{2+} ions [91–93]. As an example, alginate/CNC-based aerogels have been prepared by adding an aqueous Ca^{2+} solution to a lyophilized mixture of alginate and $c\text{-CNC-COOH}$ (10 wt. % CNCs) [94]. The resulting ionically crosslinked gels were then lyophilized to yield the aerogel (Fig. 4b). Mechanical properties of both the alginate/ Ca^{2+} and alginate/ $c\text{-CNC-COOH}/\text{Ca}^{2+}$ aerogels showed that the addition of CNCs enhanced the compressive strength by ca. 190 % at 70 % compressive strain (compressive strength of ca. 130 kPa vs ca. 45 kPa for alginate/ Ca^{2+} aerogel), and that carboxylic acid CNCs had a higher reinforcement effect relative to sulfated CNCs (ca. 100 kPa).

The incorporation of CNCs is not only a benefit for mechanical reinforcement but they can also be used to alter other properties of the material. For example, Tam et al. reported the use of CNC-containing alginate aerogel beads for the adsorption of the cationic

dye methylene blue [95]. Alginate/ $w\text{-CNC-SO}_3^-/\text{Ca}^{2+}$ (1 wt. % CNCs) hydrogel beads were prepared by dropping the aqueous mixture of alginate and $w\text{-CNC-SO}_3^-$ into Ca^{2+} solution followed by freeze drying to obtain the aerogel material. The adsorption of methylene blue, conducted by stirring the aerogel beads in methylene blue aqueous solutions, showed that the dye removal increased from 20 % to 60 % by adding CNCs into the aerogel, presumably (at least in part) by the increase in negative charges in the composite system.

2.1.2. Cellulose-based composites with negatively charged CNCs

As mentioned before, cellulose is the most bio-available polysaccharide and historically, numerous cellulose derivatives have been produced and sold on a commercial scale. In particular, cellulose esters and cellulose ethers, produced by chemical modification of cellulose, have found use in a wide variety of applications [96]. For example, cellulose acetate butyrate (CAB) is one of the most commonly used cellulose esters in the coatings industry on account of its enhanced solubility relative to cellulose, its chemical resistance and the fact that it is compatible with other polymers [97]. Furthermore, there is a certain amount of property tunability in these materials by altering the ratio of butyrate to acetate moieties on the cellulose backbone. Although the addition of CNC fillers may be expected to improve some of the properties of CAB, its general insolubility in water or polar solvents makes it difficult to prepare homogeneous CAB/CNC composite films.

As will be seen throughout this review, the insolubility of a polymer matrix in water or polar solvents is a recurring challenge in accessing many CNC composites. One way to tackle this difficulty is to use a solvent-exchange method. This approach involves the dispersion of the CNCs in water followed by the addition of an organic solvent that both dissolves the polymer and is miscible with water. The mixture is then centrifuged, the supernatant removed, more organic solvent is added to the remaining gel and the system agitated. This process can be repeated resulting in CNC-organic solvent dispersions that have limited temporal stability (Fig. 5). To access the nanocomposites, a solution of the polymer in the organic solvent is added to the organic solvent-suspended CNCs and the films are obtained by solution casting.

As an example, Oksman et al. reported CAB/ $w\text{-CNC-SO}_3^-$ composite films prepared via a solvent-exchange procedure (from water to acetone, a good solvent for CAB) followed by solution casting [98]. The CAB composite film with 10 wt. % $w\text{-CNC-SO}_3^-$ showed 30 times higher storage modulus (ca. 85 MPa) than that of pure CAB (ca. 3 MPa) at 155 °C, above the glass transition temperature (136 °C).

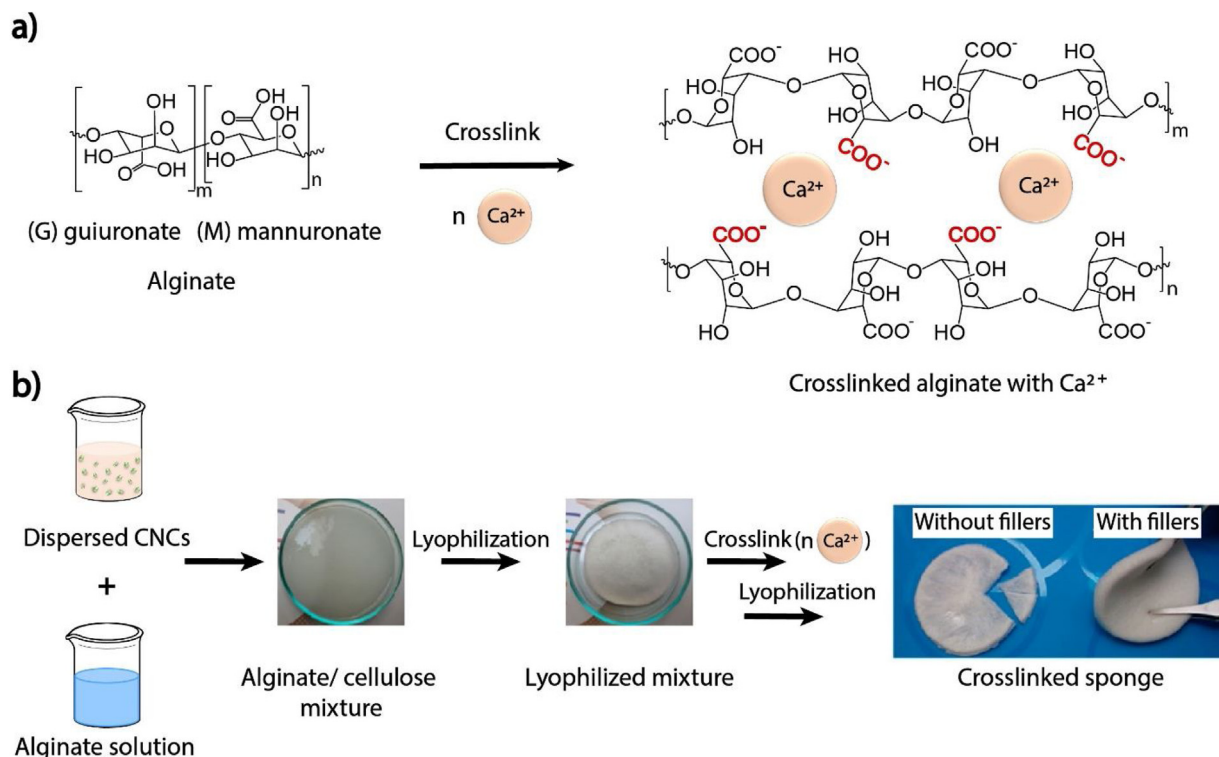


Fig. 4. **a)** Molecular structure of alginate composed of guluronate and mannuronate units and the proposed resulting crosslink structure upon addition of calcium cations. **b)** Scheme depicting the preparation of a crosslinked alginate sponge. Reproduced and adapted from references [90] Copyright 2018. Reproduced with permission from MDPI AG, and [94], Copyright 2012. Reproduced with permission from the American Chemical Society.

CNCs solvent exchange process

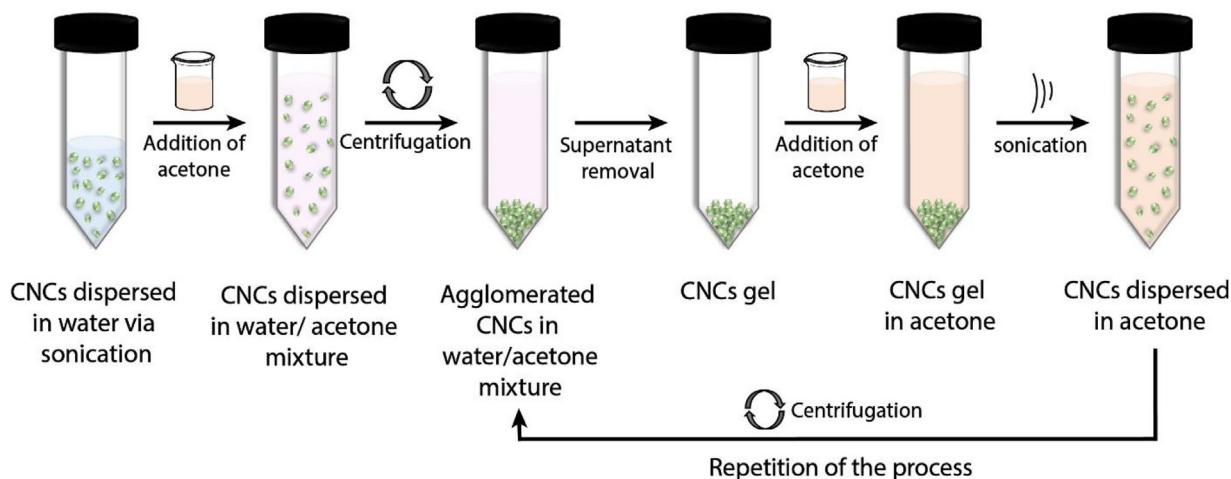


Fig. 5. Scheme depicting a standard CNC solvent exchange process from aqueous solution to a water miscible solvent such as acetone.

2.1.3. Starch-based composites with negatively charged CNCs and plasticizer

Starch is another commercially available biopolymer that can be obtained from a number of renewable plant sources, such as corn, potatoes, peas, rice, etc [99,100]. Starch is comprised of two polysaccharides, amylose (20–25 wt. %) and amylopectin (75–80 wt. %), which are the linear and branched polymers of α -glucose respectively (Fig. 6a). In its natural form, the two components combine to form a semi-crystalline, hydrogen-bonded network, resulting in an insoluble material that is difficult to reprocess. Solution processing of the natural material is difficult as starch is

insoluble in cold water and undergoes gelatinization in hot water, while melt processing is not possible as thermal decomposition starts to occur before T_m . Dried starch is brittle and mechanically weak, making it uninteresting as a replacement for any plastic [101]. While water is known to plasticize starch, the resulting material has poor properties that includes high water vapor permeability and low tensile strength [102]. In addition, starch is hygroscopic, so its water content is often difficult to control. Nonetheless starch is cheap and has generated considerable attention as a biodegradable granular filler in commodity plastics; however, such starch-based fillers generally have low reinforcing capability [103].

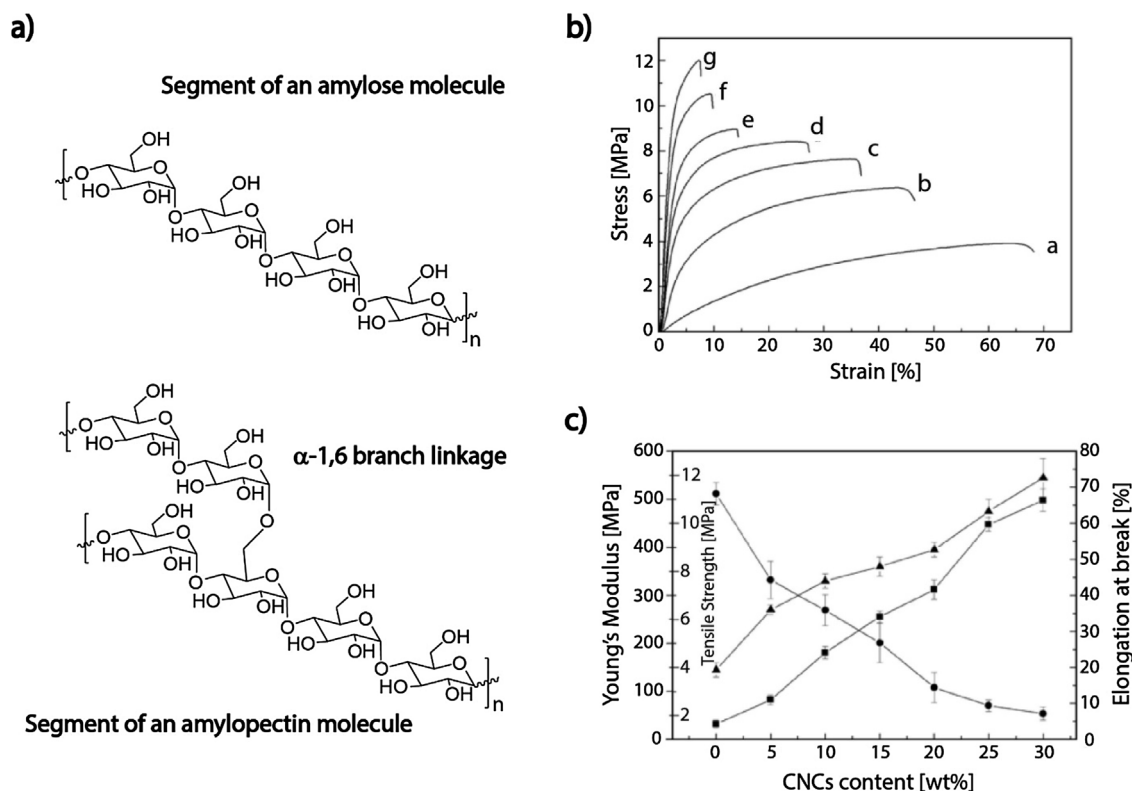


Fig. 6. a) Molecular structure of the two polymer present in starch, the linear form; amylose and the branched form; amylopectin. b) Strain-stress curves of starch/glycerol (ca. 35 wt. % of starch)/ f -CNC- SO_3^- nanocomposite film with 0 wt. % (a), 5 wt. % (b), 10 wt. % (c), 15 wt. % (d), 20 wt. % (e), 25 wt. % (f) and 30 wt. % (g) of f -CNC- SO_3^- . c) The mechanical properties of tensile strength ($\blacktriangle$), Young's modulus ($\blacksquare$) and elongation at break ($\bullet$), of the same nanocomposite film. The composite film was kept at 43 % relative humidity. [108], Copyright 2008. Adopted with permission from Express Polymer Letters.

Plasticizers other than water (such as polyols, urea, formamide, etc.) can be used to access more mechanically flexible and melt processable starch-based materials [104]. As such, these plasticized starches are able to be manufactured using traditional methods employed for synthetic plastics giving access to cheap and renewable bio-degradable materials that can be used in short-lived applications, such as packaging [105]. Unfortunately, the use of a plasticizer to improve processability comes at the cost of mechanical strength and usually does not improve water sensitivity issues. Thus, the use of a renewable filler such as CNCs as a reinforcing agent is one strategy to cope with the poor mechanical performance of plasticized starch while maintaining eco-friendly characteristics. Various reports have demonstrated a high compatibility between starch and CNC fillers, presumably as a consequence of the strong hydrogen bonding interactions between the two polysaccharide structures [106,107].

Glycerol is a commonly used plasticizer to access thermoplastic starch [109,110], although it has to be remembered that water also plays a role in such materials [111]. Interestingly, the addition of glycerol to starch yields a phase separated material (a glycerol rich and amylopectin rich phase) as highlighted by the presence of two glass transitions (ca. -50 and 40 $^{\circ}\text{C}$) [111]. Fig. 6b and c show the effect that the incorporation of f -CNC- SO_3^- has on the mechanical properties of starch/glycerol (ca. 35 wt. % of starch) composites [108]. Such CNC composites can be accessed by mixing starch granules, glycerol and f -CNC- SO_3^- in water before gelatinizing via heat treatment. Drying of the gels results in composite films which exhibit properties commonly observed in CNC reinforced materials; increases in the tensile strengths (from 4 to 12 MPa) and Young's moduli (ca. 30–500 MPa) along with decreases in the elongations at break (ca. 70 to 10 %) with varying CNC content from 0 to 30 wt. %, respectively. In comparison to multi-walled

carbon nanotubes (MWCNT), a less sustainable filler that is also often used to reinforce polymers, the starch/CNC system performs just as well, if not better. While exact comparisons are difficult to make on account of variances in source materials and processing methods, the starch/glycerol/MWCNT materials showed around 40 % increase in Young's modulus, compared to nearly 250 % increase with f -CNC- SO_3^- at the same 5 % loading [112]. An advantage the CNCs have over MWCNTs from a mechanical reinforcement perspective is they are water dispersible and as such are generally easier to process from aqueous solutions to yield composites with a more homogenous nanofiller dispersion.

The starch/ f -CNC- SO_3^- composites also exhibited two glass transitions (T_g s) (similar to the unreinforced matrix) with both transitions shifting to slightly higher temperatures with higher CNC content. Wide-angle x-ray scattering (WAXS) measurements showed the appearance of a new amylopectin crystal peak in the starch/glycerol/ t -CNC- SO_3^- composite materials, implying that the CNCs also act as a nucleating agent. It was suggested that the glycerol (and water) rich phase would localize near the CNC surfaces [50,113] potentially leading to a two-fold effect: (1) the local plasticization of amylopectin chains near the CNCs, aiding in transcrystallization, and (2) antiplasticization of the amylopectin phase, reducing the overall material ductility.

The use of sorbitol in place of glycerol as a plasticizer for starch yields materials that only exhibit one T_g , which has been ascribed to a decrease in mobility of the sorbitol. Starch/sorbitol (ca. 30 wt. % of starch) composite films containing t -CNC- SO_3^- have been prepared by solvent casting. Interestingly, these materials do not exhibit transcrystallization of amylopectin nor show a significant antiplasticizing effect, suggesting that sorbitol does not accumulate near the CNCs [114]. Compared to pure plasticized starch/sorbitol films, a starch/sorbitol/ t -CNC- SO_3^- (ca. 25 wt. %) composite film

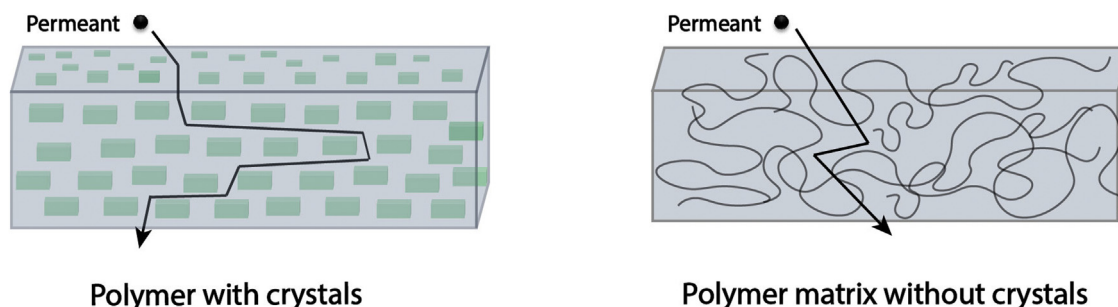


Fig. 7. The presence of non-permeable crystals (e.g. CNCs) in the polymer matrix (left) increases the permeant tortuosity/path length thus reducing permeability of water vapor and oxygen relative to an amorphous polymer matrix (right) [131]. Copyright 2004. Reproduced with permission from Elsevier Science Ltd.

showed an increase in tensile strength from ca. 5 MPa to 40 MPa and Young's modulus from ca. 50 MPa to 750 MPa (measured at 43 % relative humidity), while elongation at break of films with and without CNCs were low (below 10 %) [115]. Overall the starch/sorbitol/*t*-CNC-SO₃[−] materials showed better mechanical reinforcement than the starch/glycerol/*t*-CNC-SO₃[−] composites. It was suggested that the absence of sorbitol accumulation near the CNCs allows more effective stress transfer between CNCs and the starch matrix, leading to composites that exhibit a more significant increase in the modulus and tensile strength relative to pure glycerol-plasticized materials.

2.2. Poly(lactic acid)-based composites

Poly(lactic acid) (PLA) (most commonly the *L*-lactide enantiomer, PLLA) is currently one of the most commercially relevant bio-based polymers on account of its easy, and relatively cheap, access on a large scale as well as its overall eco-friendly properties such as bio-degradability, renewability, non-toxicity and compostability [116–118]. PLA can be prepared via ring opening polymerization of lactide monomers, which can be obtained via distillation from corn, sugar cane and other fermentation crops, giving access to large scale production at competitive costs relative to petroleum-based polymers [119]. Additionally, unlike other bio-sourced polymers, PLA can be melt-processed by extrusion, thermoforming, or injection molding to be shaped into fibers, films, or other functional forms [120].

While PLA has the potential to be a promising replacement for some commodity petroleum-based plastics, as with other bio-based polymers, it is limited in its mechanical and thermal properties. For example, its heat distortion temperature (HDT, the temperature at which the polymer deforms under a specific load) is low (55 °C) which, along with its brittleness (strain at break ~2.5 %) and poor impact resistance (impact strength ~2.6 kJ/m²), limits its utilization in a range of applications [116]. Nonetheless, PLA has already been used in some commercial applications, including packaging material e.g. corn chip bags. However, the poor barrier properties of the neat material (oxygen transmission rate over 30 cm³/m²/day compared to most commercial materials with less than 15 cm³/m²/day) prevent application in air and water-tight systems [121,122]. Since plastic packaging was a \$260bn market in 2013, it is clear why improving these properties could make a major impact in the industry [7].

A range of strategies have been developed to overcome these issues and improve PLA's overall properties, such as copolymerization, stereocomplexation, polymer blending and addition of plasticizers and/or nanofillers [123–126]. While all of these approaches result in the enhancement of either thermomechanical or barrier properties of PLA, some of them require the addition of unsustainable components to the sustainable matrix, reducing the eco-friendly aspects of the material. The use of cellulose nanocrystals

as a nanofiller, on the other hand has the potential to address the material drawbacks while maintaining the green nature of the material.

2.2.1. Poly(lactic acid)-based composites with negatively charged CNCs

As discussed above, solution processing is the most common way to access CNC composites. Unfortunately, PLA is not soluble in water and as such, direct mixing with aqueous CNC suspensions is not possible. The most common solvent used for solution processing PLA in the literature is chloroform, however, good dispersion of CNCs in this solvent is difficult. As discussed in Section 2.1.2, solvent exchange processes (Fig. 5) can be used to access dispersions of CNCs in organic solvents. As chloroform is not miscible with water, the aqueous dispersion of CNCs needs to be first solvent exchanged into a water miscible organic solvent (e.g. acetone) and then exchanged to chloroform. Lagaron et al. investigated if such a solvent exchange process aids the dispersion of CNCs in PLLA matrix [127]. To do this, chloroform dispersed *w*-CNC-SO₃[−] were prepared either by the solvent exchange process or by adding in freeze-dried *w*-CNC-SO₃[−] (from water) directly to chloroform followed by sonication. The two different chloroform CNC suspensions were independently mixed with PLA in chloroform and cast to furnish nanocomposites loaded with 1, 2, 3 and 5 wt. % *w*-CNC-SO₃[−].

No matter how the CNCs were dispersed in the chloroform the modulus and tensile strength of the composites were reduced relative to neat PLLA suggesting inhomogeneous dispersion [127] and that solvent exchange into chloroform does not appear to be a viable route to homogeneously dispersed CNCs in PLA. Nonetheless, the incorporation of CNCs by either route did result in an increase in the crystallinity of the PLLA (e.g. from ca. 9 % for neat PLLA to 15 % with 1 wt. % of freeze-dried *w*-CNC-SO₃[−]) as well as to an increase in water and oxygen barrier properties (from 1.37 × 10^{−17} m³·m/s·m²·Pa of O₂ for neat PLLA down to 0.23 × 10^{−17} m³·m/s·m²·Pa with 1 wt. % of freeze-dried CNCs), suggesting that the CNCs act as a nucleating agent for PLLA [128].

These latter observations have been made in a number of studies and as such, the ability of CNCs to enhance the barrier properties is one of the advantages of the PLA/CNC composites. It has been shown that the degree of barrier improvement for PLA-based CNC nanocomposites depends on the surface modification of the CNCs and the processing methods [129,130]. In addition, it was also reported that the type of CNC polymorph (cellulose I vs. cellulose II) employed can play a role in barrier properties. Dhar et al. showed that the incorporation of 3 wt. % *bamboo*-CNC-SO₃[−] (either in the cellulose I or cellulose II form) into PLLA by solvent exchange into chloroform (via acetone) and casting, resulted in films with different oxygen permeation properties; 14.0 cm³/m²/day for cellulose I CNC composites and 7.8 cm³/m²/day for cellulose II CNC composites [121]. A common hypothesis used to explain why CNCs improve

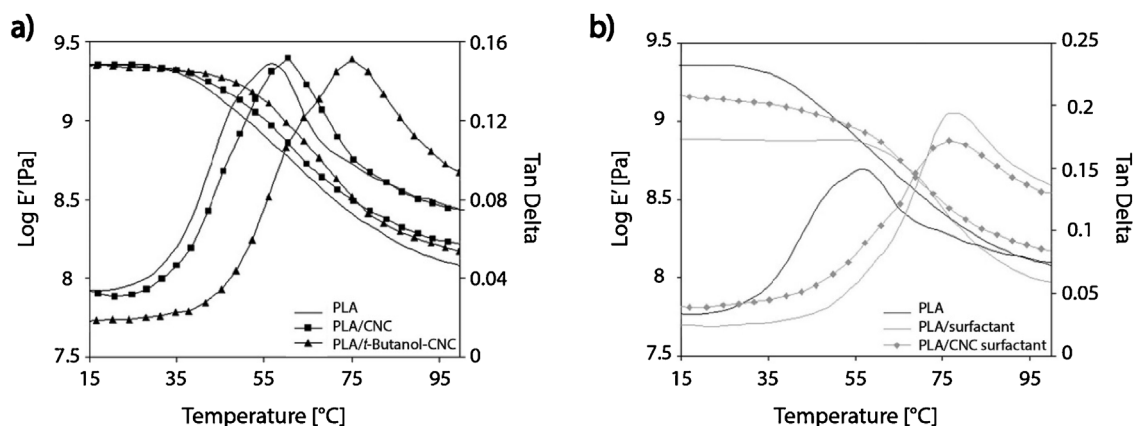


Fig. 8. Storage modulus and tan delta curves determined by DMA measurements of **a)** a comparison of neat PLA, PLA/CNC composite and PLA composite with tert-butanol CNCs. **b)** and BNA surfactant. Reproduced and adapted with permission from Ref. [138], Copyright 2007. Adopted with permission from Elsevier Science Ltd.

barrier properties is that the addition of these non-permeable crystals results in a more tortuous pathway for transport of gas or water molecules through the film, whereas the matrix without crystals does not hinder this transport (Fig. 7) [131]. In addition, the increased PLLA crystallinity induced by the nucleating effect of the CNCs reduces free volume between chains and creates more internal impermeable barriers that further limit the diffusion of small molecules [132]. It is worthy to note that improved barrier properties have been observed upon incorporating CNCs into other bio-based matrices such as alginate, polyhydroxybutyrate (PHB) and starch [133–137].

Petersson et al. investigated a slightly different protocol to access PLA/CNC composites. In this case the *w*-CNC-SO₃[−] were solvent transferred from water to *t*-butanol and the *t*-butanol CNC dispersion was then freeze-dried. Those freeze-dried CNCs were then dispersed in chloroform by ultrasonication [138]. *t*-Butanol has a melting point of 23–25 °C, which was expected to accelerate the freezing of the suspension and thereby limit the aggregation of the CNCs during the freezing process. The mechanical properties of PLA/CNC composites prepared from chloroform suspensions of either *t*-butanol freeze-dried *w*-CNC-SO₃[−] or water freeze-dried *w*-CNC-SO₃[−] showed that there is indeed a better mechanical reinforcement when using the *t*-butanol freeze-dried *w*-CNC-SO₃[−] (Fig. 8a). At 60 °C there is 64 % increase in storage modulus, *E'* for 5 wt. % *t*-butanol freeze-dried *w*-CNC-SO₃[−] relative to a 23 % increase when using water freeze-dried *w*-CNC-SO₃[−]. In addition, there is a shift to higher temperatures in the tan δ peak by 15 °C with the *t*-butanol freeze-dried *w*-CNC-SO₃[−] films (compared to the films made with water freeze-dried *w*-CNC-SO₃[−]), indicating a more pronounced effect on the segmental motion of PLA chains in these composites (Fig. 8b) which is consistent with a better dispersed nanofiller.

Petersson et al. also investigated the use of surfactants as an alternative to improve the dispersion of the CNCs in PLA. It was assumed that the surfactant would hinder the hydrogen bonding between the CNCs during the freeze-drying process and result in a better distribution within the matrix. The selected surfactant, Beycostat A B09 (BNA), a phosphoric ester of polyoxyethylene(9)nonylphenyl ether, had been employed earlier by Heux et al. as a coating for *c*-CNC-SO₃[−] and *t*-CNC-SO₃[−] to yield birefringent toluene suspensions [48]. The surfactant coated *w*-CNC-SO₃[−] also showed birefringence when dispersed in chloroform (which was not observed with the *t*-butanol freeze-dried *w*-CNC-SO₃[−] discussed above), highlighting the benefit of the surfactant to improve the dispersion of the nanofillers. The composites were made by simple solution casting resulting in a transparent film upon melt pressing, consistent with good dispersion of the CNCs in the

matrix. Comparison of dynamic mechanical analysis (DMA) curves of PLA/surfactant composites with the PLA/surfactant/*w*-CNC-SO₃[−] composites showed that the CNC composite materials had an 83 % greater storage modulus at 20 °C. However, it is important to note that both materials show reduced modulus relative to neat PLA at this temperature. In fact, while there is a shift in tan δ of ca. + 20 °C for the surfactant containing materials relative to PLA, there is only a small increase in modulus for the PLA/*w*-CNC-SO₃[−]/surfactant composites relative to PLA observed above 55 °C. Overall, while these CNCs may be well dispersed in the matrix, the mechanical studies are consistent with the surfactant coating on the CNCs preventing direct interactions between the PLA and the CNCs. As such, while it is important to obtain well dispersed CNCs in a matrix, this in and of itself is not enough to obtain good mechanical reinforcement. Ensuring good interfacial adhesion between the filler and matrix and/or good filler-filler interactions are also important considerations.

One application-focused benefit of surfactant addition is the blocking of hydrophilic groups on the CNC surfaces, which can reduce water uptake and transport. Reduced water vapor permeability (WVP) has been shown to prevent bacterial growth in packaging materials and the hydrophilic nature of negatively charged CNCs can be antithetical to this goal [139]. In one study, Fortunati and coworkers showed that the reduction in WVP caused by increased tortuosity and crystallinity in a PLA matrix was offset entirely by the hydrophilicity of *w*-CNC-SO₃[−] at 1 wt. % loading [140]. Adding surfactant (Beycostat A B09) blocked the hydrophilic surface groups from associating with water molecules and decreased WVP by 34 % relative to the negatively charged *w*-CNC-SO₃[−] composites at the same 1 wt. % loading.

Water uptake of PLA-based materials can have significant effects on their material properties. The degradation rate of PLA has been shown to be influenced by the relative humidity of the surrounding environment, with more humid environments causing PLA to degrade more quickly [141]. More rapid degradation of PLA/cellulose fiber composites has been observed with both macrocellulose (wood pulp and wood fibers) [142] as well as nanocellulose [143] composites, where the rate changes are attributed to the increased water uptake caused by the hydrophilic cellulose. To further back up this hypothesis, the use of surfactant-coated CNCs at a 1:1 surfactant to CNC weight ratio resulted in a reduced PLA degradation rate under composting conditions with 5 wt. % *w*-CNC-SO₃[−]/surfactant in a PLA matrix [143]. While not extensively investigated in many matrices, it may be possible to somewhat tune the degradation rate of CNC sustainable composites through the hydrophilic or hydrophobic modification of the nanocrystal surface, broadening

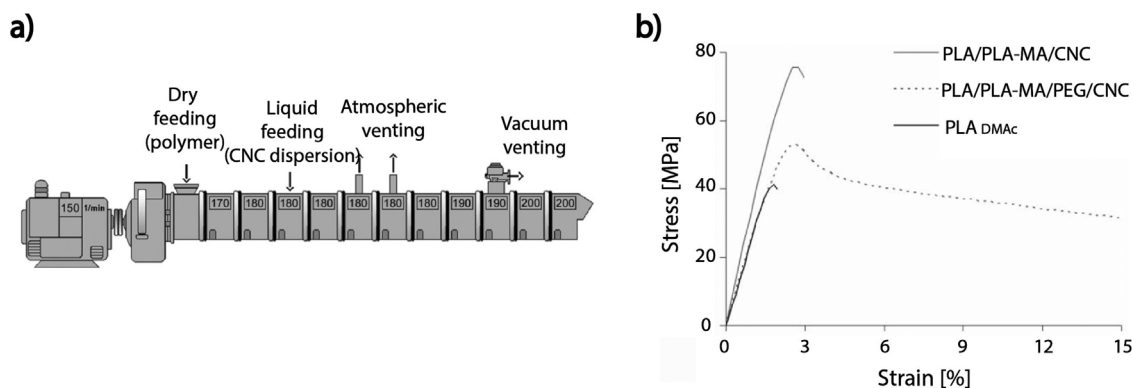


Fig. 9. **a)** Scheme showing the different compartments (feeding zone, venting zone and vacuum zone) of an extruder used to process CNC composites. **b)** The comparison of the measured tensile stress strain curves of PLA/PLA-MA/CNC, PLA/PLA-MA/PEG/CNC and PLA_{DMAc} [145]. Copyright 2006. Adopted with permission from Elsevier Science Ltd.

the application window for bio-based CNC composite packaging materials.

The future of packaging materials is trending toward more active materials which, for example, have antimicrobial characteristics built into the packaging, reducing the likelihood of bacterial build up over the lifetime of the product. Unmodified negatively charged CNCs have few to no antimicrobial properties, but the addition of other additives, such as silver nanoparticles, can impart these desired effects [140]. Unfortunately, the same hydrophobic surface modifications that have been used to reduce water uptake have also been shown to have negative effects on antibacterial nanoparticle migration and leaching. Fortunati and coworkers showed enhanced leaching in PLA films filled with *w*-CNC-SO₃⁻ coated with an ethoxylated nonylphenol surfactant and silver nanoparticles [144], presumably on account of increased mobility in the hydrophobic surfactant layer. In some cases, as much as 10 times increase in the amount of nanoparticle leaching was observed relative to the neat PLA films or PLA loaded with unmodified *mcc*-CNC-SO₃⁻.

Surfactants are not the only additives that have been investigated to access improved PLA/CNC composites. Oksman et al. studied the use of *N,N*-dimethylacetamide (DMAc) with LiCl for the preparation of CNC-based PLA nanocomposites [145]. It is important to note that DMAc/LiCl mixtures with high LiCl content dissolve cellulose and allow access to individual cellulose macromolecules [146,147]. However, DMAc containing a lower amount of LiCl (0.5 wt. %) can be utilized to separate individual *w*-CNC-SO₃⁻ from microcrystalline cellulose (MCC) with ultrasonication and allow access to relatively concentrated *w*-CNC-SO₃⁻ suspensions (10–17 wt. %). Oksman et al. investigated melt mixing of PLA with the concentrated DMAc/LiCl/*w*-CNC-SO₃⁻ suspensions. The CNC suspensions (enough to obtain 5 wt. % CNCs in the final composite) were pumped directly into an extruder containing molten PLA at 170–200 °C. The extruder was equipped with several venting systems that allowed the removal of vapors upon heating (Fig. 9a) [145]. However, using this melt processing technique resulted in brown/degraded materials. To address this issue processing aids, such as polyethylene glycol (PEG1500) (15 wt. %) or maleated PLA (PLA-MA, 2.2 % maleic anhydride) (10 wt. %), were incorporated into the molten PLA to decrease the viscosity or act as a coupling agent, respectively.

Fig. 9b shows the stress-strain curves of three different compositions of the melt processed PLA using this technique. PLA_{DMAc} is the film formed by simply injecting a DMAc/LiCl solution (i.e. no CNCs) into molten PLA and shows stress at break and strain at break similar to neat PLA. Adding in the DMAc/LiCl/*w*-CNC-SO₃⁻ suspension to a molten mixture of PLA and PLA-MA results in a film that exhibits almost double the tensile strength relative the PLA_{DMAc} (ca.

78 and 40 MPa, respectively) and an increase in Young's Modulus (3.9 vs. 2.9 MPa). These values compare well with PLA composites containing maleic anhydride-modified multi-walled carbon nanotubes (MA-MWCNT) [148]. The PLA/MA-MWCNT material showed a tensile strength of around 76 MPa at a similar 4 parts per hundred loading, showing that the CNC-based composites offer a competitive, renewable alternative to MWCNTs in this case.

Interestingly the addition of PEG (1500 g/mol) to the melt processed PLA/PLA-MA/PEG/*w*-CNC-SO₃⁻ films yields a more ductile material that exhibits an eight times increase in the strain at break (up to 18 %) while also showing a slight increase maximum tensile strength relative to PLA_{DMAc}. No explanation was provided on why the PEG improved the ductility of this PLA/PLA-MA/PEG/*w*-CNC-SO₃⁻ composite. However, similar effects have been previously observed in other PEG/CNC containing composites and has been attributed to the interactions between the low molar mass PEG and CNCs, reducing the CNC-CNC interactions and improving their dispersion in the matrix [149]. While the use of DMAc/LiCl/*w*-CNC-SO₃⁻ does allow access to melt processable PLA/CNC composites, the DMAc/LiCl appears to result in the degradation of the *w*-CNC-SO₃⁻ at high temperatures [145], as was suggested by the brown-colored composites obtained. As such, optimization in the compounding process would require the use of a feed medium which does not cause CNC (or PLA) degradation at the high temperatures required for processing. Additionally, this study highlights how the addition of a coupling/compatibilizing agent (in this case the PLA-MA) into the polymer melt can be used to prevent/inhibit the re-aggregation of the CNCs upon removal of the dispersing medium [150,151].

The use of plasticizers has been investigated as a way to access more flexible PLA/CNC composites. For example, the natural compound limonene has been shown to plasticize PLA (20 wt. % blended into PLA drops the *T_g* from 58 to 42 °C), lower its crystallinity and improve its barrier properties, which are important factors in packaging films. To access PLA/limonene/CNC composites, the PLA and limonene were melt blended (15–25 wt. % of the plasticizer at ca. 180 °C) prior the direct addition of 1 or 3 wt. % of *ph*-CNC-SO₃⁻ (dried at 40 °C overnight) to the molten polymer [57,152]. The resulting films were transparent and exhibited a single *T_g* (DSC) at ca. 34 (1 wt. %) or 32 °C (3 wt. %). The DSC also revealed a decrease in the cold crystallization temperature (*T_{cc}*) of PLA in the composites consistent with the dispersed *ph*-CNC-SO₃⁻ promoting the crystallization of the matrix in the plasticized PLA [153]. The PLA/limonene/*ph*-CNC-SO₃⁻ composites revealed high values of elongation at break 288 % (1 wt. % CNC) and 272 % (3 wt. % CNC) primarily as a consequence of the plasticization effect of the limonene (PLA/limonene has an elongation of break ca. 250 %).

As such, adding *ph*-CNC-SO₃⁻ (up to 3 wt. %) to the PLA/limonene system appears to not have a significant effect on the mechanical properties.

The above discussion shows that it is possible to utilize different processing techniques and/or additives to enhance the dispersion of the CNCs in PLA. However, to date the amount of mechanical reinforcement in such composites appears not to have been optimized. The use of plasticizers/surfactants may enhance the mobility of PLA chains in the matrix, benefiting elongation at break, but they can also block CNC-CNC interactions along with filler-matrix interactions. As such, while the organization of such agents at the CNC surfaces may improve dispersion, it can also reduce the ability for stress transfer from the matrix to the filler, limiting mechanical reinforcement. Thus, a key challenge here is how does one effectively quantify the level of dispersion of the CNCs within the matrix. Does one method provide better dispersion than another? Given that the different processes discussed above add in a variety of different components it is hard to isolate the simple effect of the added component versus the effect of CNC dispersion on the material properties. Instead, one must rely on less objective evidence, like birefringence in solution and transparency of materials, but neither of these provide a quantifiable level of homogeneity. In the end what is important is how well does a given processing technique improve the properties of the composite but there is certainly an argument to be made for the development of more comprehensive methods for measuring the CNC filler dispersion.

2.2.2. Poly(lactic acid)-based composites with polymer grafted CNCs

Given the challenges of dispersing CNCs in PLA, primarily on account of the differences in polarity of the filler and matrix, covalent functionalization of the CNCs is an alternative strategy to adding additives to aid their dispersion in PLA. Most of the work in this area has focused on grafting polymers to the CNCs and investigating the resulting PLA composites. It has been demonstrated that the grafting of polymer chains to the CNC surface can not only improve the dispersion of the CNCs within the matrix but can also enhance the interfacial adhesion between the filler and matrix [154]. Grafting of polymers to the CNCs prevents aggregation of the nanocrystals through steric hindrance and the nature of the interactions between the grafted polymer and matrix can be used to facilitate dispersion within the matrix.

Polymer grafting to the CNCs can be achieved by either a "grafting-to", where a preformed polymer chain is reacted with functional groups on the CNC surface, or "grafting-from" method, where an initiating site on the surface is used to polymerize the monomer directly from the CNCs. For PLA specifically, the "grafting-from" approach has generally been employed in the preparation of the modified fillers, predominantly through the use of the surface -OH groups as initiating sites for ring opening polymerization (ROP) [155–158]. Not surprisingly, the most common polymer grafted from the CNCs in this context is PLA (Fig. 10a). This is most commonly achieved using tin(II)-based catalysts and through the variation of the monomer concentration, time and/or the addition of "free" OH groups, the molecular weight of the grafts can be somewhat controlled [159].

Generally, it is expected that grafted chains with higher molecular weight will penetrate deeper into a polymer matrix, assuming a constant matrix molecular weight and neutral or favorable interactions between the polymer graft and the matrix [160]. This should enhance the interfacial adhesion between the matrix and filler and result in better stress transfer from the matrix to the nanomaterial when load is applied. To the best of our knowledge detailed studies focusing on this aspect have yet to be carried out with CNC-based composites. However, Lönnberg et al. have shown that polycaprolactone (PCL) composites (matrix *M_n* ca. 80,000 g/mol) containing

10 wt. % PCL-grafted microfibrillated cellulose (MFC-g-PCL) exhibited better mechanical reinforcement with MFC-g-PCL that have longer grafts (Young's Modulus ca. 325 MPa for graft with *M_n* ca. 2200 g/mol and 290 MPa for graft with *M_n* ca. 700 g/mol). This compares to a Young's modulus of 190 MPa for the neat PCL and 260 MPa for the PCL reinforced with unmodified MFC [161]. However, this increase in stiffness does come at a cost of ductility, where the neat material had an elongation at break of roughly 900 % while all of the 10 wt. % composite materials fractured at less than 25 % strain.

Goffin et al. prepared *rf*-CNC-g-PLLA by carrying out the ROP of L-lactide in toluene-dispersed *rf*-CNC-SO₃⁻, obtained via a solvent exchange process. The polymer-grafted *rf*-CNC-g-PLLA were shown to result in more stable chloroform suspensions after 3 days than the unmodified *rf*-CNC-SO₃⁻ or a blend of PLLA with *rf*-CNC-SO₃⁻, thus highlighting the benefits of the polymer modification for compatibility with non-polar media [156]. Composites were prepared by melt blending *rf*-CNC-g-PLLA in PLLA with up to 8 wt. % filler, which resulted in nearly colorless materials with varying degrees of transparency depending on the CNC content (more CNCs resulted in hazier materials). Comparatively, materials prepared with *rf*-CNC-SO₃⁻ showed the expected thermal degradation upon melt processing at the same temperatures, 185–200 °C, suggesting that the polymer grafting aids the thermal stability of the CNCs. As seen in Section 2.1.3 with negatively charged CNCs, these functionalized CNCs are also capable of acting as nucleating agents in semi-crystalline matrices [162]. DSC analysis of the PLLA/*rf*-CNC-g-PLLA composites showed an increased in crystallinity and a decreased crystallization half-time (the time at which the extent of crystallization reaches 50 % completion) with the addition of *rf*-CNC-g-PLLA. At room temperature, no reinforcing effect is observed; however, reinforcement above *T_g* is seen and is primarily attributed to the increased PLLA crystallinity restricting the polymer chain mobility [163]. Interestingly, DMA showed a drop in the glass transition temperature at 8 wt.% loading, suggesting that the filler may also have a plasticizing effect on the matrix.

Braun et al. have investigated the use of CNCs with a lower polymer grafting density [155,164]. This was achieved by acetylation of freeze-dried CNCs (*w*-CNC-Ac) resulting in blocking/protecting many of the possible -OH initiation sites. This procedure gave access to *w*-CNC-Ac with up to 60–70 % of the OH groups functionalized according FTIR (Fig. 10b). The group conducted grafting-from ROP reactions from freeze-dried *w*-CNC-Ac in either toluene solution or in the bulk monomer (L-lactide) to yield the polymer grafted acetylated CNCs (*w*-CNC-Ac-g-PLLA). The acetylation and PLLA grafting were confirmed by the appearance of characteristic ester carbonyl peaks at 1736 cm⁻¹ for the acetate and 1760 cm⁻¹ for the polymer (Fig. 11a). PLA/*w*-CNC-Ac-g-PLLA composites were prepared by mixing a PLA solution in chloroform with a chloroform suspension of *w*-CNC-Ac-g-PLLA to create films with up to 25 wt. % *w*-CNC-Ac-g-PLLA. After evaporation of the solvent, the resulting composites were compression molded and resulted in highly transparent materials, suggestive of a good dispersion of the modified fillers within the matrix (Fig. 11b). Composites prepared with the solution functionalized *w*-CNC-Ac-g-PLLA had a substantially greater increase in the heat distortion temperature reaching 150 °C at a filler loading of 15 wt. % compared to 115 °C for the composite made with the bulk-functionalized *w*-CNC-Ac-g-PLLA. This is compared to 70 °C for the neat PLA and 80 °C for the PLA/*w*-CNC-Ac composites (Fig. 11c). The difference between the two *w*-CNC-Ac-g-PLLA nanocomposites highlights the importance in considering the polymer grafting methodology, which will impact the amount and molecular weight of the grafted polymer, factors that can play a significant role in the final properties of the composites.

As before, the crystallization half-time of the PLA composites with 5 wt. % *w*-CNC-Ac-g-PLLA quenched at 110 °C from the melt

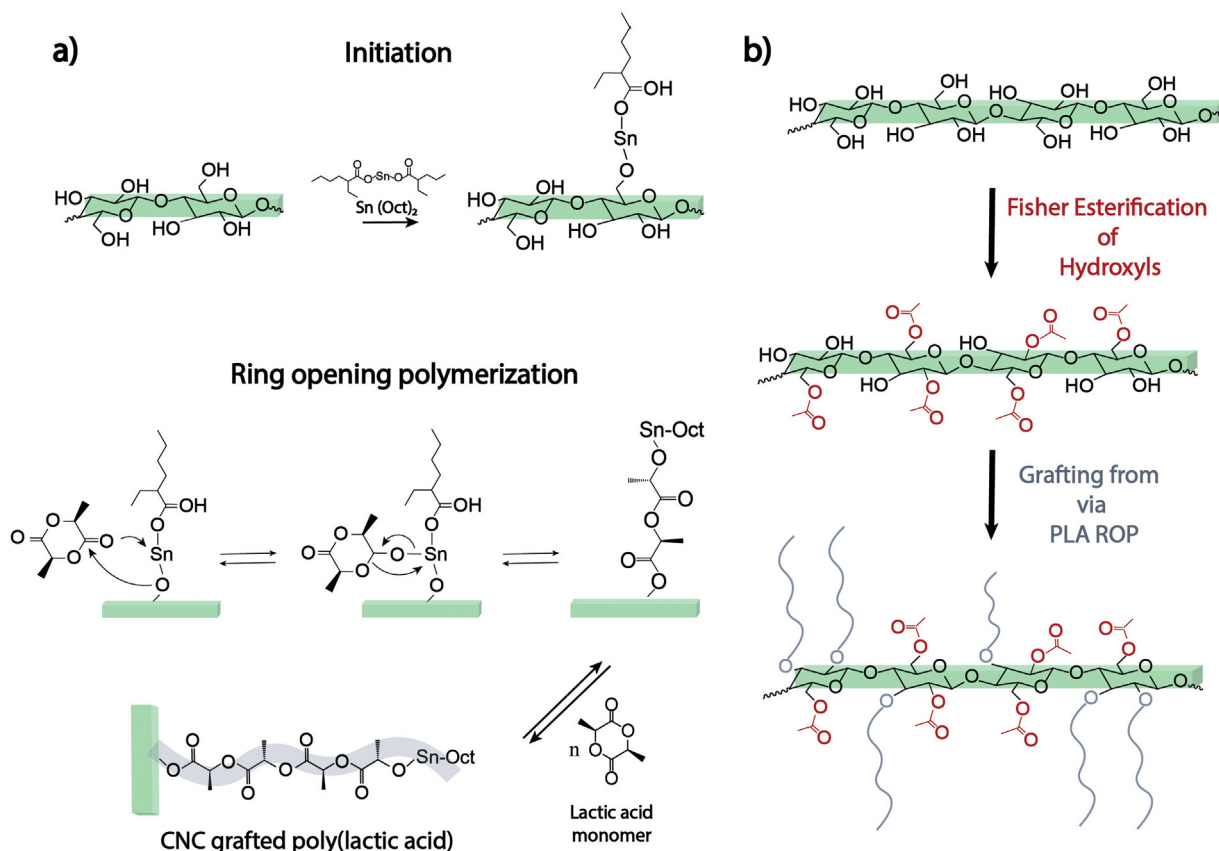


Fig. 10. a) Synthetic path of a ring opening polymerization of poly(lactic acid) initiated on the surface of the CNC and in presence of catalyst, the tin(II) 2-ethylhexanoate (Sn(Oct)₂). b) Scheme illustrating acetylation procedure to partially functionalize the surface of the CNCs [155]. Copyright 2012. Reproduced with permission from the American Chemical Society.

was 45 s compared to 90 s for neat PLA (Fig. 11d). A further reduction of the crystallization half-time down to 15 s was observed upon increasing the CNC loading to 15 and 20 wt. % (Fig. 11d). This is a useful result as one of the challenges of PLA from an industrial perspective is its slow crystallization time [165].

An aspect of PLA that we have not yet touched upon is its ability to form stereocomplexes [166]. PLLA has a melting point of 170–190 °C and a T_g of 50–65 °C, while racemic PLA is amorphous with a T_g ca. 50–60 °C. PDLA/PLLA blends form semi-crystalline stereocomplexes that have a melting point at 220–240 °C and a T_g ca. 65–70 °C, showing thermal improvements over the individual components [166]. Thus, conceptually one can envision grafting one stereoisomer (e.g. D-lactide) from the CNC and incorporate it in a matrix of the other (e.g. L-lactide) to obtain a material with enhanced properties. Zhang and coworkers employed this approach and obtained transparent PLLA/c-CNC-g-PDLA composite films by solvent casting from chloroform, which suggested that the modified filler had good dispersion within the matrix [167]. The composites also exhibited significant improvements in heat distortion resistance (40 % strain for the 10 wt. % composite after 10 min at 80 °C with a load of 50 g vs. 220 % for neat PLLA under the same conditions), but T_g shifted to lower temperatures as c-CNC-g-PDLA content increased from 0 to 10 wt. %.

Another key challenge for PLA is to develop ways to improve its toughness. While toughness improvements can be achieved by blending soft, ductile polymers, such as natural rubber or poly(butylene succinate) (PBS), into the matrix [168], an alternative approach has utilized PLA's stereocomplex characteristics [166]. Muiruri et al. grafted a random copolymer block of ϵ -caprolactone (CL) and D-lactide (DLA) on w-CNCs in toluene followed by a homo-D-lactide block to act as a compatibilizing block between the filler

and the matrix [169]. The inclusion of CL into the grafted polymer was intended to act as a rubbery phase to absorb deformation energy and improve toughness of the composite material. The nanocomposites were prepared by solution casting a mixture of PLLA and 2.5 wt. % w-CNC-g-P(CLDLA-*b*-DLA) in chloroform and subsequently melt processing by injection molding. The stereocomplexation of the grafted D-lactide chains with the L-lactide matrix, enhanced filler–matrix interactions and inclusion of 2.5 % of the filler increased the toughness by 20 times, but decreased the tensile strength and modulus on account of plasticization. Scanning electron microscopy (SEM) and small-angle X-ray scattering (SAXS) measurements showed the major toughening mechanisms to be fibrillation and crazing during deformation of the nanocomposites. Such a biodegradable and tough CNC-filled PLA nanocomposites could open up new application avenues for PLA based materials [169].

2.3. Poly(3-hydroxybutyrate)-based composites with negatively charged CNCs

Poly(3-hydroxybutyrate) (PHB) is a thermoplastic polyester belonging to the family of polyhydroxyalkanoates which can be produced by bacteria or from sources, such as plants, sugar cane, etc [170]. As a result of its similar properties to petroleum-based polymers like PP (such as melting temperature ca. 180 °C and tensile strength ca. 30 MPa) combined with biodegradability and biocompatibility, PHB has been widely studied with a specific focus in biomedical [171,172] and food packaging applications [173]. However, material brittleness and a narrow processing window (low degradation temperature ca. 220 °C) still remain as challenges for broader implementation. One approach to overcome these issues is

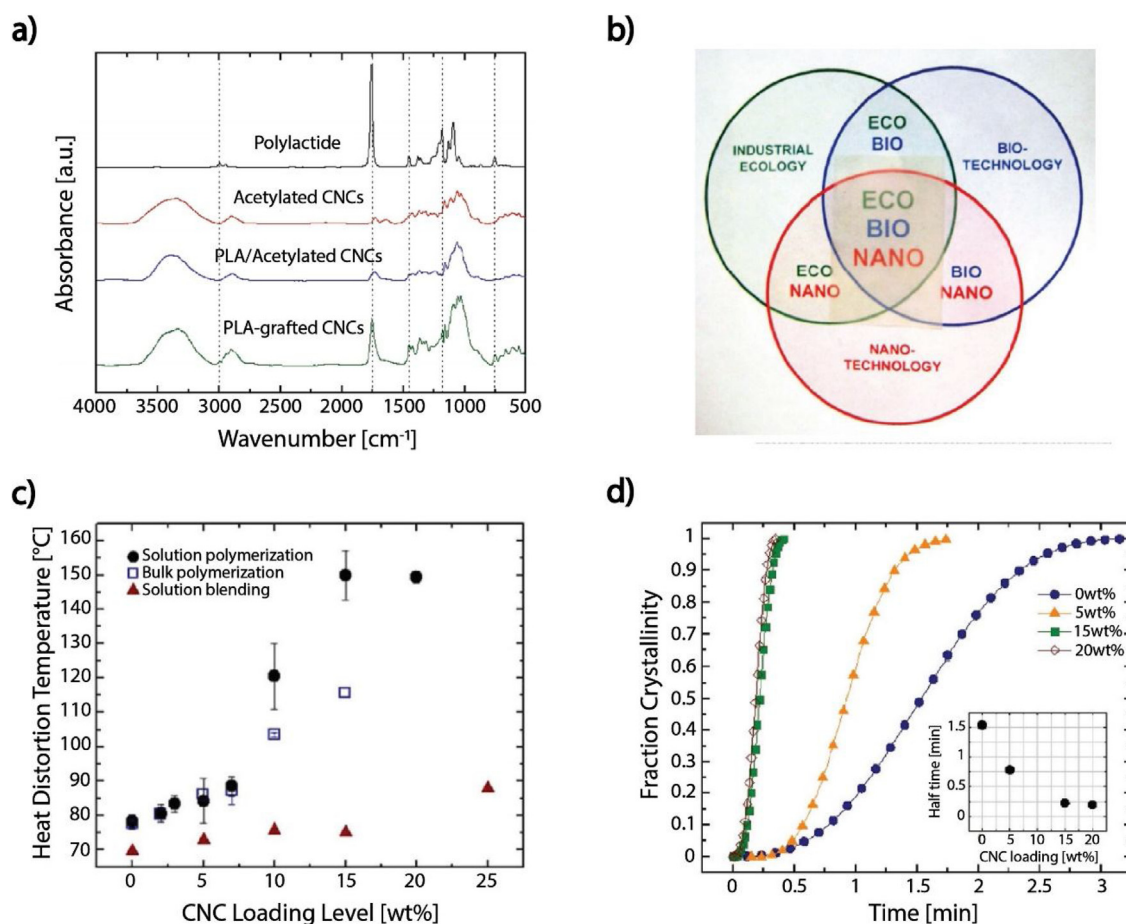


Fig. 11. a) Comparison of FTIR spectra of PLA (black), w-CNC-Ac (red), PLA/w-CNC-Ac (blue) and w-CNC-Ac-g-PLLA (green). Dotted lines indicate PLA signals that do not overlap with peaks originating from the CNCs. b) Melt-pressed films of PLA/w-CNC-Ac-g-PLLA nanocomposite with 10 wt% w-CNC-Ac-g-PLLA loading. c) Comparison of the obtained heat distortion temperature for nanocomposites prepared by in situ polymerization in solution and in bulk compared with solution-blended nanocomposites, as a function of CNC weight loading. d) Comparison of the fraction of crystallinity over time for PLA composites with solution polymerized w-CNC-Ac-g-PLLA when the materials are quenched from the melt to 110 °C. The crystallization half-time as a function of the content of CNC is plotted in the inset [155]. Copyright 2012. Adopted with permission from the American Chemical Society. (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article).

the addition of plasticizers and fillers, such as CNCs, to tune the thermal and physical properties of PHB composites without altering the overall material biodegradability [174–176].

PHB is insoluble in water, making the processing of well dispersed PHB/CNC materials a challenge, similar to most other CNC composite systems. As such, solvent casting is most often done from organic solvents that can dissolve PHB, like DMF or chloroform [176]. Simple composites of PHB with CNCs have been investigated, but the expected increase in brittleness without improving thermal stability was observed, which is why the use of other additives is also necessary [176]. For example, Orefice et al. were able to achieve a birefringent dispersion of w-CNC-SO₃⁻ in a PHB matrix by using low molar mass PEG (200 Da) as a dispersing agent and plasticizer [177]. At first, w-CNC-SO₃⁻ were dispersed in PEG by evaporating the water from a PEG/w-CNC-SO₃⁻ solution (Fig. 12 inset), then the PEG/CNC blend was dissolved in a chloroform solution containing 5 w/v % PHB. Homogeneous PHB/PEG/w-CNC-SO₃⁻ (constant 15 wt.% PEG relative to PHB) composite films, as visualized under SEM, were obtained with varying CNC content by casting the mixture, evaporating off the solvent at room temperature followed by drying at 40 °C. These PHB/PEG/w-CNC-SO₃⁻ nanocomposite films exhibited a significant increase of the elongation at break (50 times greater than neat PHB and 25 times greater than PHB/PEG blends). While there was no significant loss of tensile strength (ca. 15–20 MPa), these composite materials did exhibit a substantial decrease in modulus (from > 600 to < 100 MPa from 0 wt. % to 0.45 wt. %)

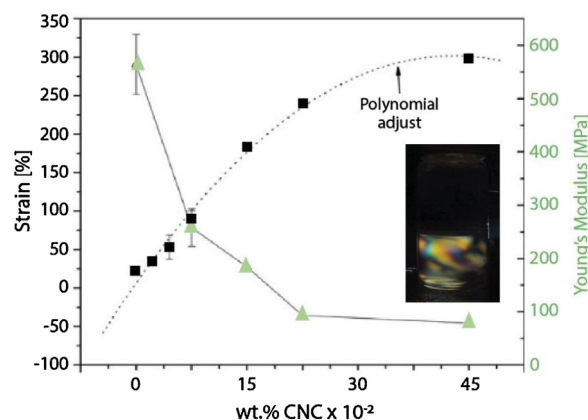


Fig. 12. The strain and Young's Modulus of PEG/PHB composite with low CNC content. (Inset: PEG/CNC dispersion at 1 wt. % concentration, observed between crossed polarizers) [177]. Copyright 2013. Adopted with permission from John Wiley & Sons Inc.

(Fig. 12). In addition to these mechanical changes, thermal stability was shown to be enhanced in the PHB/PEG/w-CNC-SO₃⁻ systems when compared to the PHB/PEG materials. The inclusion of CNCs was able to delay thermal degradation to be comparable to neat PHB, with degradation onset around 270 °C, which is around 40 °C better than the PHB/PEG system. All of these changes support the

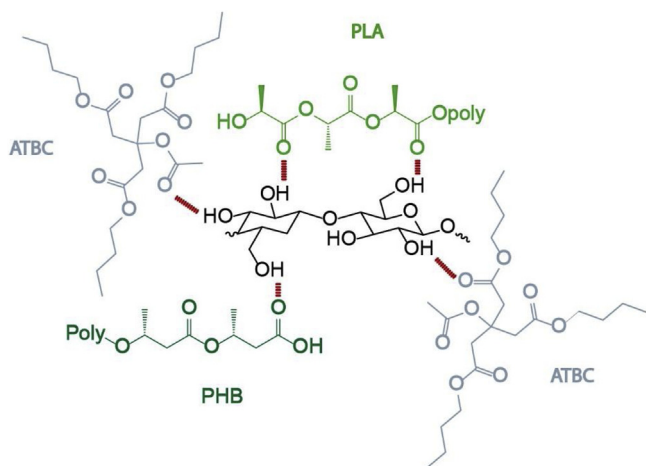


Fig. 13. The suggested molecular interaction on the CNCs with PLA, PHB and ATBC in the composite [179]. Copyright 2015. Adopted with permission from Elsevier Science Ltd.

ability of CNCs to enhance the processing and application window of PHB.

PHB and PLA can be blended together to expand their property profile resulting in improvements in both mechanical and barrier properties [178]. As such, CNC composites of these blended materials are also of interest [140]. Fortunati et al. melt mixed 5 wt. % $w\text{-CNC-SO}_3^-$ or freeze-dried surfactant (STEPFAC 8170, nonylphenol phosphate ester) coated $w\text{-CNC-SO}_3^-$ in 1:1 (w/w) with melt blended PLLA/PHB (75:25 wt. %) plasticized with 15 wt. % (relative to the PLLA/PHB blend) of acetyl tri-*n*-butyl citrate (ATBC) [179]. The ATBC was added to enhance the PLLA and PHB chain mobility and promote the dispersion of the CNCs within the matrix [180]. The transparency of the resulting materials suggested a good dispersion of the CNCs within the matrix for the composites made with either unmodified or surfactant-coated CNCs. However, transmission electron microscope images revealed some flakes within the PLLA/PHB/ $w\text{-CNC-SO}_3^-$ system, while the surfactant-modified CNCs did not show the formation of such agglomerates. SEM micrographs of the fractured cross-sections revealed rough surfaces and the formation of voids in the PLLA/PHB/ATBC materials, while the incorporation of either unmodified $w\text{-CNC-SO}_3^-$ or surfactant-coated $w\text{-CNC-SO}_3^-$ eliminated these voids. The authors suggest that the ATBC plasticizer resulted in a reduction of viscosity in the system, which facilitated processing and ultimately promoted the dispersion of CNCs in the polymer blend. However, the ATBC plasticizer does have side effects, as noticed in the barrier properties of the films. The PLLA/PHB/ $w\text{-CNC-SO}_3^-$ transmitted $13\text{ cm}^3/\text{m}^2/\text{day}$ of oxygen while the plasticized PLLA/PHB/ATBC/ $w\text{-CNC-SO}_3^-$ showed a rate of $23\text{ cm}^3/\text{m}^2/\text{day}$ (c.f. neat PLA ca. $30\text{ cm}^3/\text{m}^2/\text{day}$). A T_g increase from 31 to ca. 45°C with the incorporation of the CNCs into PLLA/PHB/ATBC suggests good filler matrix interactions (Fig. 13). In addition, two melting peaks are observed for the plasticized blends, one for PLLA (149°C) and one for PHB (172°C). However, there is only one melting peak at 147°C in the PLLA/PHB/ATBC/ $w\text{-CNC-SO}_3^-$ composites, suggesting a drop of the overall crystallinity in this material, possibility as a result of the $w\text{-CNC-SO}_3^-$ increasing compatibility between the PLA and PHB. The incorporation of the $w\text{-CNC-SO}_3^-$ to PLLA/PHB/ATBC resulted in almost no changes to the Young's modulus but did significantly reduce the elongation at break (27 vs. 90 %). However, the incorporation of surfactant modified $w\text{-CNC-SO}_3^-$ into the polymeric blends resulted in an increase in the elongation at break (147 %) allowing access to more ductile materials. These composite films showed a clear increase in degradation rate when CNCs and/or plasticizer were included in the blend, cutting degradation time in half

for some samples. This is most likely attributable to the presence of more water within the matrix making hydrolysis more likely.

3. Other potential applications of sustainable cellulose nanocomposites

As covered in the previous sections, the ability for cellulose nanocrystals to positively impact properties of bio-based polymers has received significant attention in the past decade. While understanding the structure-property-processing relationships in these sustainable composites is an important goal, a parallel question to be addressed is where are the potential applications for such materials? The following section aims to highlight selected application areas in which CNCs, and their bio-based composites, may show promise that go beyond the mechanical reinforcement and packaging applications that have been touched upon in the prior sections.

3.1. Compatibilization of immiscible polymers

Most polymers are immiscible and as such, when they are blended together, the result is a macrophase separated material with poor physical properties. Compatibilization is the process of stabilizing the interface between the two immiscible polymers, thus creating a more homogenous material with improved properties. Compatibilizers include the use of surfactant-like molecules or block copolymers that are able to organize at the interface and lower the surface energy between the two phases. From a recycling perspective, the use of compatibilizers is attractive as it potentially offers a more facile route to processing of recycled polymers by reducing the need for costly separations [181]. Given that CNCs can be used to reinforce polymer matrices, if they can be used as a compatibilizer as opposed to say molecular/polymer based surfactants, then the resulting recycled blended material may show even more enhanced mechanical properties. This would create a potential opportunity for the upcycling of plastic waste, which is when the regenerated material has the same or more value than the virgin supply [182].

Habibi and coworkers reported an early example an immiscible polymer blends being compatibilized by $rf\text{-CNC-SO}_3^-$ in a PLLA/PCL system [183]. The ternary composites of the PLLA/PCL blend along with either $rf\text{-CNC-SO}_3^-$ or $rf\text{-CNC-g-PLLA-b-PCL}$ showed a 2 or 3 order of magnitude increase in the storage modulus (over 1000 MPa) when compared to the binary PLLA/PCL system (ca. 5 MPa). The composites microstructure appeared much more homogenous compared to the blend without CNCs (Fig. 14). Similar compatibilization effects of CNCs have also been observed in less sustainable matrices, such as poly(vinyl alcohol)/PEO blends [184]. Such observations suggest that it may be possible to utilize CNC-based fillers to combine the previously mentioned mechanical, thermal and barrier property improvements with compatibilization expanding the capabilities of both virgin and recycled blends.

3.2. Water filtration

As discussed above, hydrophilic CNCs enhance the diffusion of water into polymer matrices, begging the question of whether these systems would be viable as membranes and filters for water purification. If the CNCs are also functionalized with a binding motif, then such systems could be tailored for selective filtration and toxin removal. Saito and Isogai were the first to show that TEMPO-oxidized $c\text{-CNC-COOH}$ were capable of metal ion adsorption from aqueous solutions by association of the metal ions with the deprotonated carboxylate groups [185]. From that point, the field has expanded tremendously with work towards enhancing uptake of targeted ions, such as lead, through functionalization

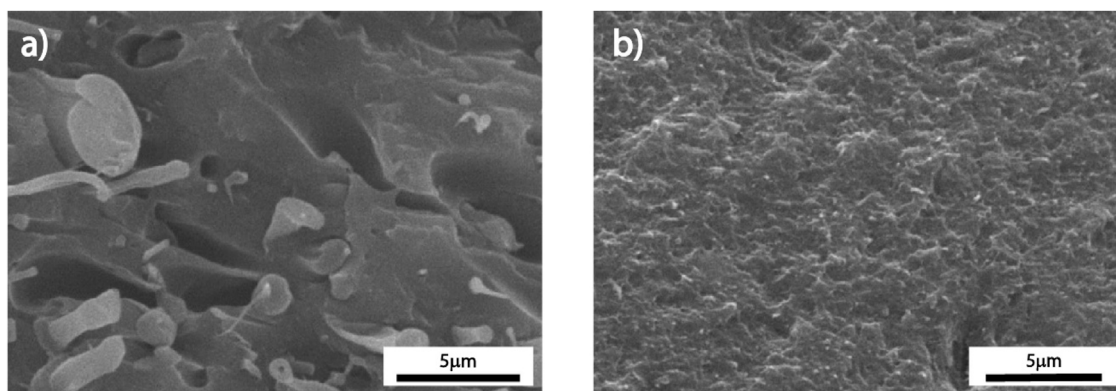


Fig. 14. a) SEM image of PLLA/PCL (1:1) polymer blend showing clear phase inhomogeneity between the two polymeric materials and b) a PLLA/PCL (1:1) blend with 2 wt. % of *rf*-CNC-SO₃[−] showing a much more homogenous morphology [183]. Copyright 2012. Adopted with permission from the American Chemical Society.

of the CNCs with specific binding motifs and towards stripping the sequestered material in order to recover and reuse the filtration material [186–188]. In one example, Mathew and coworkers made a bio-based high flux membranes by vacuum filtration of a 1:1 gelatin/w-CNC-PO₃[−] solution on a cellulose microfiber support followed by melt pressing at 80 °C [189]. The resulting uniform membrane was capable of high flux (almost 3000 L/h/m² at 1 bar) and high capacity uptake of metal ions such as Cu²⁺ (358 mg/g of CNC in the filter) and Fe³⁺/Fe²⁺ (512 mg/g). For comparison, carbon nanotubes have a Cu²⁺ sorption capacity of 67.8 mg/g of filtration material.

3.3. Biomedical CNC-containing bio-based materials

CNCs have been investigated in a wide range of different biomedical materials. In this regard there are a few biomedical application areas for which fully bio-based composites have received some attention [190,191].

One area where CNC-containing bio-based hydrogels have been investigated is as drug delivery vehicles. For example, Dufresne and coworkers blended *c*-CNC-SO₃[−] into a crosslinked alginate core and subsequently adsorbed additional alginate onto the surface to create double-layer hydrogel particles (Fig. 15) [192]. The pure alginate outer layer showed relatively rapid degradation and drug release while longer-term sustained release of the active pharmaceutical ingredient was observed from the inner alginate/ *c*-CNC-SO₃[−] sphere, which degraded at a slower rate. It was also suggested that the CNCs may cause slower diffusion of the drug within the matrix.

Bio-based nanocomposites have also attracted interest in tissue engineering applications. For instance, CNCs have been shown to delay implant degradation, increasing the amount of time cells that can grow into the scaffold before losing mechanical support. For example, it has been shown that while cell proliferation in alginate/*c*-CNC-SO₃[−] gel composites was slowed (relative to alginate gels), the improved mechanical strength and slower degradation rate made the material a promising candidate for bone stents for which rapid cellular growth is not required, but mechanical strength is needed [193]. In a related example, Yang et al. created hydroxyapatite/gelatin/*b*-CNC-COOH hydrogel composites where the amount of CNCs incorporated into the composite could be used to control the gel's degradation rate in simulated bodily fluid while maintaining the tensile strength [194].

CNC-based materials have also been investigated as antimicrobial agents. For example, CNCs have been grafted with a variety of molecules, such as rosin [195], porphyrin [196] and polyrhodanine [197] to create films and particles that have shown considerable success in reducing bacterial colony survival. While not composites, these functionalized CNC nanomaterials have been

proposed to be incorporated into fabrics, papers, and coatings for the biomedical, food service and packaging industries to access more sustainable and biocompatible alternatives to the current solutions.

The future role of CNCs in the biomedical industry relies on the continued investigation of biological interactions with the many different forms of CNCs and in a wide range of environments. While some *in vitro* studies have been undertaken with CNC-based systems [198], we have only scratched the surface and a much better understanding of *in vivo* interactions is necessary. Additionally, further degradation studies need to be undertaken so that the long-term impact of CNCs on the body can be better understood.

3.4. Electronics

CNCs have been investigated in a range of electronic applications further highlighting their versatility as a nanomaterial. While not all of the materials used with the CNCs in this section are sustainable, the key goal is to replace actively toxic materials that are traditionally used in systems like batteries and solar cells, and as such, reducing the non-trivial contamination issues upon disposal [199,200].

In battery applications, nanocellulose based materials are interesting on account of their mechanical strength and permeability [201]. Accordingly, studies have investigated the potential of CNC composites as separators, electrolytes [202] and electrodes [203] in next-generation battery technologies. Dufresne and coworkers combined the needs of a separator and electrolyte by solvent casting *t*-CNC-SO₃[−]s into a PEO film to create a robust, conductive nanocomposite [202]. The material exhibited less than half an order of magnitude loss in ionic conductivity at 60 °C when compared to neat PEO, while also achieving an order of magnitude increase in mechanical strength.

The complexity of electronic systems is one factor that makes fully sustainable devices difficult to design, but CNCs provide a foundation that can be built upon. Okahisa and coworkers used cellulose nanofiber mats dipped in various acrylic resins to create substrates with low coefficients of thermal expansion (CTE) for deposition of organic light-emitting diodes (OLEDs) [204]. The low CTE, 12.1 ppm/K in the best case, showed a 94 % decrease over the neat resin and was essential to prevent delamination during thermal cycles encountered in regular use. This idea was advanced by Kippelen and coworkers, who used a glycerol/w-CNC-SO₃[−] substrate to create a fully recyclable OLED [205]. Building on this work, the same group went on to employ the same optically clear composite of glycerol and w-CNC-SO₃[−] as a substrate for recyclable solar cells (Fig. 16), on top of which was deposited successive layers of silver, ethoxylated polyethylenimine, photoactive material, molyb-

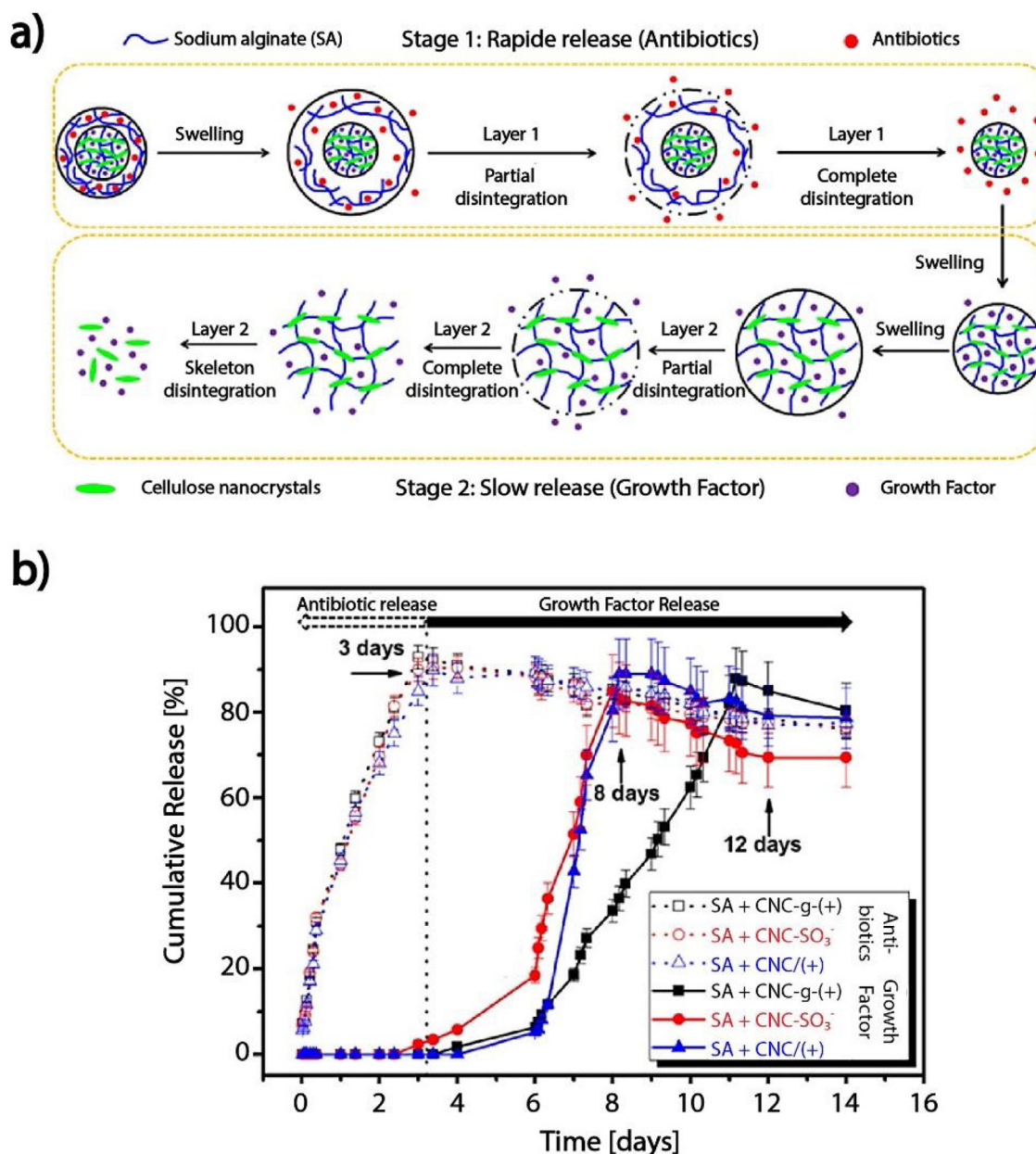


Fig. 15. a) Drug release schematic for the release of the antibiotic ceftazidime hydrate loaded into the sodium alginate (SA) outer layer and human epidermal growth factor in the SA/CNC inner layer from double membrane alginate hydrogel particles. b) Graph of drug release times showing rapid release of the antibiotic from the outer layer, and a delayed onset release of growth factor. CNCs used were neat w-CNC-SO₃⁻, CNCs modified by chemical grafting of a positively charged small molecule (CNC-g-(+)), and CNCs modified by physical adsorption of a positively charged polyelectrolyte polymer (CNC/(+)) [192]. Copyright 2016. Adopted with permission from the American Chemical Society.

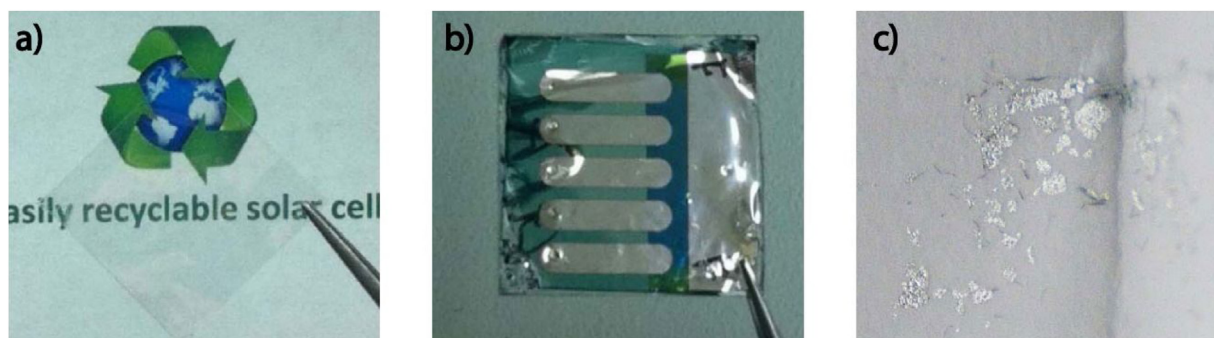


Fig. 16. a) Transparent w-CNC-SO₃⁻ film used as the substrate for the recyclable solar cell, b) the fully assembled and recyclable solar cell on the CNC substrate and c) the solid remains (mainly consisting of Ag and MoO₃) after dissolving the solar cell into its constituent components through a series of washes in deionized water and chlorobenzene [206]. Copyright 2013. Adopted with permission from the Nature Group.

denum oxide (MoO_3) and finally another layer of silver [206]. While the achieved power conversion efficiency of 2.7 % is nowhere near to the state-of-the-art solar cells, ca. 25 %, these cells were able to be completely recycled, showing that fully-recyclable solar cells are a legitimate possibility.

4. Conclusion

The incorporation of bio-based cellulose nanocrystals into sustainable polymer matrices allows access to improvements in a number of important material properties, from mechanical strength and thermal resistance to barrier properties, without detracting from the materials sustainability. Although, it is important to note that while CNCs are components of many natural systems (in particular within trees and plants), more work is needed to better understand the environmental and biological impacts of isolated and functionalized CNCs. This critical aspect aside, the key to improved materials properties is the ability to access composites where the CNCs are well-dispersed within the host matrix. If the polymer matrix is soluble in water (or even polar organic solvents such as DMF), e.g. alginate and chitosan, then it is relatively easy to access CNC composites that show greatly enhanced properties by standard solution casting processes. The real challenge comes when the polymer matrix in question is not soluble in a solvent that disperses the CNCs. Numerous methods have been tried to get around this problem, including transferring the CNCs into less polar solvents, to limited success. Additives (e.g. surfactants or dispersing agents) can be used to enhance CNC dispersion in the matrix. However, such molecules usually facilitate the dispersion by localizing at the CNC surfaces and as such, stress transfer between the CNCs themselves as well as between CNCs and the matrix is diminished, reducing the effectiveness of the reinforcement. To improve stress transfer, covalent grafting of the dispersing agent, usually a short-chain polymer, to the CNC surface has been conducted. The resulting materials exhibit some of the best properties of any CNC composites currently reported. Nonetheless, improvements in the large-scale synthesis and processing of such materials need to be made before commercial implementation will be achieved.

Solvent casting-based processes are currently the most frequently employed because they offer the advantage of maximizing dispersion of the CNCs. However, such processing involves large amounts of solvent and, from a sustainability and commercialization point of view, any solution-based processing is not ideal. Unfortunately, melt processing of CNC composites is a major challenge, as it is with most nanocomposites, given their tendency to aggregate/phase separate and the fact that they can start to decompose at high temperatures. Most of the aforementioned strategies (functionalization of CNCs, addition of surfactants and plasticizers) are viable options, but as of yet, a scalable, cost effective process still needs to be developed.

The possibilities of commercialization are diverse, and work has been done in the areas of packaging, compatibilization, water purification, biomedical and electronics (amongst others). The sustainability and ability to functionalize the CNC's surface with a wide variety of chemistries are part of what makes their appeal so broad. For example, grafting of binding sites allows sequestration of ions in contaminated water, attachment of antibacterial agents helps to prevent disease in biomedical applications and grafting of conductive materials improves electronic or ionic conduction, opening the door to potentially accessing wholly sustainable systems that can impact fields ranging from energy storage to flexible bio-electronics. As such, while there are still unresolved challenges that need to be addressed, the potential of CNCs (and other nanocelluloses) to help expand the sustainable materials portfolio is clear.

Authors contribution

All the authors contributed in surveying the literature and writing this review.

Declaration of Competing Interest

None.

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