



Influence of the order of fabrication sequences on the thermoelectric properties of skutterudite $\text{CoSb}_3-\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanocomposites

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ARTICLE INFO

Article history:

Received 25 November 2019

Received in revised form

19 June 2020

Accepted 22 June 2020

Available online 30 June 2020

Keywords:

Hydrothermal synthesis

$\text{Cu}_{0.6}\text{Ni}_{0.4}$ nano alloy

Cobalt skutterudite

Fabrication sequences

Nanocomposite

Thermoelectric properties

Bipolar effect

ABSTRACT

Nanocomposite samples of $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ ($x = 1, 3.5, 6$, and 9 wt%) were fabricated through two different approaches to understand the influence of fabrication processes on the thermoelectric properties of CoSb_3 skutterudite. CoSb_3 matrix and $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloy were synthesized separately via hydrothermal procedures. The mixtures of as-hydrothermally synthesized powders were prepared and annealed in the first method, while in the second fabrication route, CoSb_3 powders were initially annealed, followed by mixing with $\text{Cu}_{0.6}\text{Ni}_{0.4}$ and annealing of the composite at the same conditions. The results showed improved electrical conductivity of CoSb_3 compounds, which is consistent with the systematic increase of the carrier concentration upon increasing the $\text{Cu}_{0.6}\text{Ni}_{0.4}$ content. The grain boundary potential barrier mechanism was used to describe the influence of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloy on the height of the energy barrier of $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$, as compared with that of pristine CoSb_3 synthesized using the similar hydrothermal method. The onset of bipolar thermopower reduction is shifted to higher temperatures; however, the room temperature thermopower is reduced upon increasing the content of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoinclusions. The sample containing 1 wt% of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ fabricated through the first fabrication procedure showed the highest zT value at ~ 550 K.

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1. Introduction

Conversion of waste heat to electrical energy using thermoelectric (TE) generators has become more prevalent in both research and industrial applications for clean energy technologies [1–3]. Conventionally, the thermal to the electrical conversion efficiency of a TE material is evaluated via its dimensionless figure-of-merit, $zT = S^2T/\rho\kappa$; thereat, T , S , ρ and $\kappa = \kappa_e + \kappa_L$ are absolute temperature, thermopower (Seebeck coefficient), electrical resistivity, and total thermal conductivity, respectively. The total thermal conductivity of semiconductor material includes electronic (κ_e) and lattice (κ_L) thermal conductivity components [4]. Various

strategies have been investigated to improve the zT of TE materials, including nanostructuring and electronic structure tuning via solid solution and elemental doping on ionic sites of pristine materials [5–13]. It is known that decoupling the interdependent thermopower and electrical resistivity could be an efficient approach for boosting the power factor (S^2/ρ) [14]. Hence, decoupling the electronic parameters can be a practical strategy to achieve high zT values; however, it could be a challenging task for a single-phase thermoelectric material. Obtaining composite materials could improve the transport properties of TE materials via inducing multi-mode phonon scattering from hierarchical structures. Uniform distribution of a small amount of appropriate nano inclusion in a TE material could improve the corresponding zT value through enhancing the power factor and/or reducing κ_L [14–19]. Cobalt skutterudite is one of the promising TE materials that is extensively explored by adopting strategies such as doping, cage filling, nanostructuring, and fabricating composite compounds, aiming to improve its zT value [20–27]. It is known that the pristine CoSb_3

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system possesses relatively low electrical conductivity and simultaneously significant Seebeck coefficients at temperatures below the onset of the bipolar effect [28,29]. Existing intrinsic vacancies in crystal-cell is one of the attractive features of skutterudites, providing the possibility of tuning the transport properties via incorporating elements from alkali, alkaline earth group, rare-earth metals or other metals such as gallium, indium, and thallium in the cell vacancies [20,22,27]. The lattice thermal conductivity of partially-filled CoSb_3 is reduced due to frequent scattering of phonon on the loosely bonded void fillers [26,27]. The use of composite structures to enhance the TE properties of CoSb_3 has recently received more attention [30–35]. The influence of various materials such as MoS_2 [36], SiC [37], reduced graphene oxide [38], WTe_2 [39], and FeSb_2 [40], as an additive on the thermoelectric properties of pristine or partially-filled CoSb_3 have been studied. Furthermore, the role of in situ formed extra crystal phases, such as Sb_2O_3 [19], CoSb_2O_4 [19], and InSb [41], on enhancing phonons scattering in CoSb_3 structure have been studied.

In the present study, the influence of composite structures and the order of fabrication sequences on the thermoelectric properties of $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites are investigated. Both CoSb_3 powder and $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloy were separately synthesized through hydrothermal processes. Hydrothermally synthesized single-phase CoSb_3 system possesses a relatively low electrical conductivity [39,42]; therefore, pristine CoSb_3 were mixed with relatively high electrically conductive materials ($\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloy) to enhance the electrical conductivity [43]. $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ ($x = 1, 3.5, 6$, and 9 wt%) nanocomposite samples were prepared through two separate procedures (P1 and P2) and all annealed in a vacuum atmosphere under the same conditions. The crystal structure, microstructure, and transport properties were characterized for all the samples. The peak power factor of $6.33 \mu\text{Wcm}^{-1}\text{K}^{-2}$ is obtained for the sample containing 1 wt% of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloy. It is found that the total thermal conductivity of $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ samples is not the same for both sets of samples. The peak zT value of 0.23 is obtained for the sample containing 1 wt% of $\text{Cu}_{0.6}\text{Ni}_{0.4}$, while higher percentages of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloy deteriorates power factor due to significantly reduced thermopower.

1.1. Experimental procedure

1.1.1. Synthesis of CoSb_3 powder

CoSb_3 powder was synthesized using a hydrothermal procedure, reacting Sb powder with a stoichiometric amount of $\text{CoCl}_2\cdot6\text{H}_2\text{O}$ precursor to obtain the ratio of Sb to Co elements of 3:1. The reaction was performed in a Teflon-lined autoclave. The solution was heated from room temperature to 255°C at a heating rate of $2.5^\circ\text{C}/\text{min}$ and hold for 12 h, followed by cooling to room temperature at the same rate. The obtained precipitate was then washed using ethanol and deionized water in sequences and dried at 80°C for 3 h in an Argon atmosphere in a tube furnace. The final single CoSb_3 phase was attained upon annealing partially cold-pressed (about 3 MPa) bulks of the as-synthesized powder at 585°C for 5 h at about 10^{-5} Torr vacuum atmosphere. More details on the hydrothermal synthesis of CoSb_3 could be found elsewhere [42].

1.1.2. Synthesis of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ powder

$\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloy was also synthesized using a hydrothermal procedure [43]. 5.36 mmol $\text{CuCl}_2\cdot2\text{H}_2\text{O}$, 3.57 mmol $\text{NiCl}_2\cdot6\text{H}_2\text{O}$, and 5 mL Glycerol were added to 150 mL deionized (DI) water in a Teflon cup. Glycerol was added to prevent the oxidation of Cu and/or Ni elements. The solution was then stirred for 15 min, while it was heated on a hot plate at about 50°C . The NaBH_4 chemical was

then used to reduce the solution. The Teflon cup containing the solution was then heated in an autoclave at 170°C for 12 h. The obtained precipitate was then washed using DI water and ethanol in sequences and dried with the same method used for drying CoSb_3 .

1.1.3. Fabrication of $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites

Nanocomposite samples of $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ with $x = 1, 3.5, 6$, and 9 wt% were fabricated through two different procedures. For the first set of samples that were produced through procedure number one (P1), $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites with $x = 1, 3.5, 6$, and 9 wt% are labeled as sample #1 to #4, respectively. For the second set of samples that were produced through procedure number two (P2), the $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites with $x = 1, 3.5, 6$, and 9 wt% were labeled as sample #5, to #8, respectively. The first fabrication route (P1) includes mixing stoichiometric ratios of as-hydrothermally synthesized $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloys with CoSb_3 powder and suspended in 10 mL ethanol by ultrasonication. The obtained suspension was partially dried at about 45°C in the air followed by drying at 80°C under argon atmosphere for 3 h. The final dried powder was then partially cold-pressed at a pressure of about 3 MPa and sealed in Pyrex ampoule under 10^{-5} Torr. The sealed samples were then annealed at 585°C for 5 h.

To fabricate the second set of the samples with the same compositions through P2, we first cold-pressed the as-hydrothermally synthesized CoSb_3 powder and annealed it at 585°C for 5 h in an evacuated-and-encapsulated Pyrex ampoule. The annealed CoSb_3 was then powdered using an agate mortar and pestle and mixed with a stoichiometric ratio of as-hydrothermally synthesized $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloys. To obtain a uniform suspension, we suspended the mixture in 10 mL ethanol by ultrasonication. The samples were dried using the same method used in P1. The obtained powders through both P1 and P2 were then cold-pressed into parallelepiped and disc shape samples at 17 MPa. The compacted samples were then annealed at 585°C for 5 h in a vacuum-sealed Pyrex ampoule.

Our motivation for producing $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ composites through P1 was to improve the intergrain joints of $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ particles via thermodynamically providing conditions for localizing Co and Sb ions into crystal sites of CoSb_3 structure and simultaneous formation of CoSb_3 grains with the least boundaries with that of CuNi grains, e.g., to reduce Kapitza resistance. The formation of CoSb_3 particles using P1 could be regarded as the in-situ formation of an extra phase inside the microstructure of the host material.

The structure of the obtained samples was analyzed using x-ray diffraction pattern (XRD). The micro-morphology of the samples was characterized using field emission scanning electron microscopy (FESEM, MIRA3-TESCAN-XMU). The thermopower (Seebeck coefficient), electrical conductivity, room temperature charge carrier concentration, and mobility measurements were carried out using a standard 4-point probe method using Linseis equipment under Helium environment. The thermopower was measured for five temperature differences at a given temperature, and each measurement was then repeated four times and then averaged. The thermopower was determined using the slope method in quasi-steady-state mode with temperature differences of 1–5 K. The temperature dependence of magnetic moment under the applied magnetic field of 10^4 emu (~ 0.1 T) was explored between 2 K and 400 K using vibrating sample magnetometer (PPMS, Quantum Design DynaCool). The thermal conductivity ($\kappa = D \times C_p \times \rho$) was obtained using the measured thermal diffusivity (D), specific heat capacity (C_p), and bulk density (ρ). The thermal diffusivity measurement was carried out between room temperature and 800 K in vacuum using a Laser Flash apparatus (Netzsch LFA 457 Micro

Flash) [44]. The specific heat capacity was estimated using the Dulong-Petit limit, $C_p = 3nR$; wherein n is the number of atoms per formula unit and R the universal gas constant [45]. For CoSb_3 matrix, $C_p = 0.235 \frac{J}{g\text{K}}$ was calculated, herein, $n = 32$ is the number of atoms per CoSb_3 cell. The C_p values $0.397 \frac{J}{g\text{K}}$ and $0.433 \frac{J}{g\text{K}}$ was inserted, respectively, for Cu and Ni elements [46]. The combination C_p of $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites could be calculated using the Kopp-Neumann rule, expressed using Eq. (1) [47].

$$C_p = \sum_{i=1}^N f_i C_{pi} \quad (1)$$

Where i index gets values 1 and 2 for CoSb_3 and $\text{Cu}_{0.6}\text{Ni}_{0.4}$ phases, respectively, and f_i being the weight percentage of a component having a specific heat capacity of C_{pi} . The bulk density of the samples was measured using the Archimedes' method.

The measurement errors for electrical conductivity, Seebeck coefficient, and thermal diffusivity are within 10%.

2. Results and discussion

2.1. Structural and morphology characterization

The XRD pattern of as-hydrothermally synthesized $\text{Cu}_{0.6}\text{Ni}_{0.4}$ -nanoalloy in Fig. 1a shows that the sample formed of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ phase and traces of Cu_2O phase with its most intense peak at around $2\theta \approx 38^\circ$. The primary reflections correspond to a face-centered cubic structure with a space group of $\text{Fm}\bar{3}m$ (#225) [43]. A single phase of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloy was obtained by annealing the powder at 560°C for 5h (Fig. 1b). The Cu_2O phase might have been reduced by residual remnant Glycerol that might have remained in the $\text{Cu}_{0.6}\text{Ni}_{0.4}$ precipitate.

Fig. 2a shows the XRD pattern of as-hydrothermally synthesized powder of CoSb_3 , indicating that the precipitate contains Sb, CoSb, and CoSb_2 phases. Only traces of CoSb_3 phases (labeled by + symbol) could be identified in the XRD pattern of the hydrothermally synthesized precipitate, similar to previous studies [23]. Annealing the powder at 585°C for 5h results in a single phase of CoSb_3 (Fig. 2b).

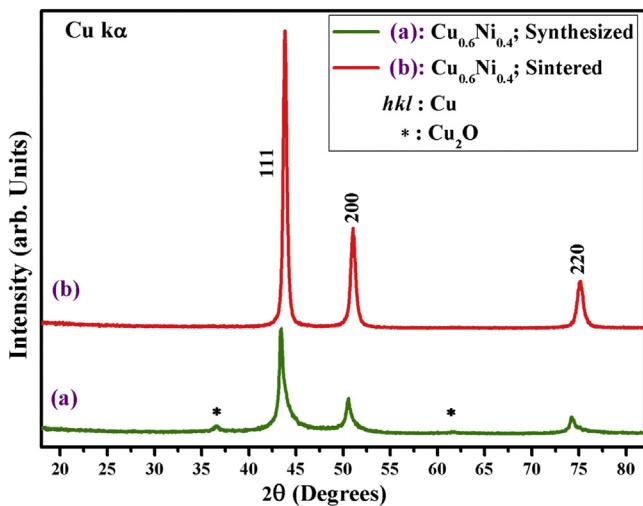


Fig. 1. XRD patterns of as-hydrothermally synthesized $\text{Cu}_{0.6}\text{Ni}_{0.4}$ powders (a); asterisk symbol (*) denotes Cu_2O phase. XRD of annealed $\text{Cu}_{0.6}\text{Ni}_{0.4}$ powders at 560°C for a duration of 5h inside an evacuated ampoule (b). The (hkl) Miller indices represent that of the face-centered cubic copper structure, space group $\text{Fm}\bar{3}m$ (#225).

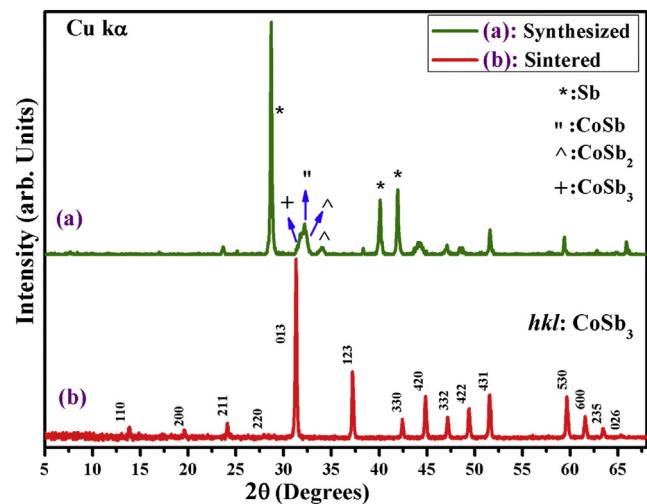


Fig. 2. XRD patterns of as-hydrothermally synthesized CoSb_3 powders (a); (*) (**) (+) symbols represent Sb, CoSb, CoSb_2 and CoSb_3 phases, respectively. XRD of annealed CoSb_3 powders at 585°C for a duration of 5h inside an evacuated ampoule (b). The (hkl) Miller indices indicate cobalt skutterudite structure.

Fig. 3 illustrates the XRD patterns of $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ of all nanocomposite samples with $x = 1, 3.5, 6$, and 9 wt\% . The major crystalline phase in all samples is CoSb_3 ; albeit, samples #1 to #4, fabricated by the first method, show higher purity. The impurity peaks are identified as CoSb_2 , NiSb , and NiCoSb phases (labeled in Fig. 3). The intensity of impurity peaks is increased at higher concentrations of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloy, especially for the first set of samples. The impurity phases in the present composite samples could cause Ni deficiencies in the crystal structure of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ (Fig. 3). No Cu_2O peak is detected in the XRD pattern of the $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites, indicating that $\text{Cu}_{0.6}\text{Ni}_{0.4}$ phase remains stable at the present fabrication conditions despite the formation of Ni deficiencies. The lattice parameter of all the $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ composites is refined with respect to the cell parameter of pure CoSb_3 . The obtained results show the lattice parameter of the different samples varies between 9.031 \AA and 9.037 \AA (see

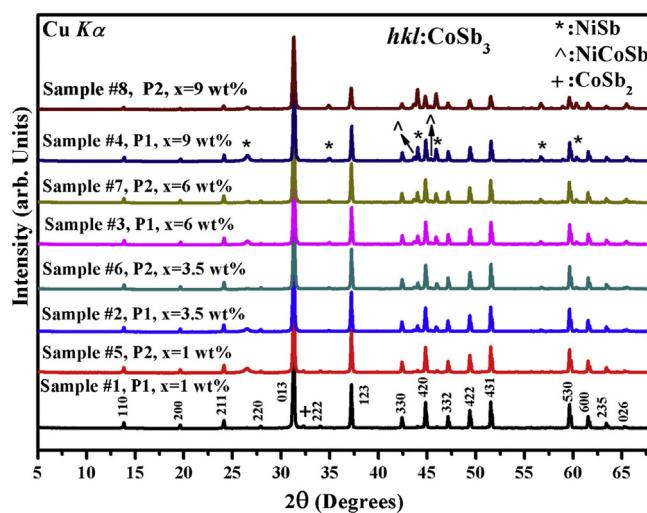


Fig. 3. XRD patterns of $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites with $x = 1, 3.5, 6$ and 9 wt\% fabricated through P1 (samples #1 through #4) and P2 (samples #5 through #8). (*) (^) (+) symbols represent traces of NiSb , NiCoSb , and CoSb_2 impurity phases, respectively. The (hkl) Miller indices indicate cobalt skutterudite structure.

supplementary), indicating that the host phase remains pure, as compared with other reports for pure cobalt skutterudite system [23,24,28,41,42].

The bulk density of the samples ranges between 63% and 73% of the theoretical density indicating a highly porous structure (Table 1). The relative bulk density of the samples fabricated through P1 is relatively lower than that of those samples fabricated through P2. The relative bulk density is reduced by the $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloy ratio, especially for the second set of the samples.

The FE-SEM image of as-hydrothermally synthesized $\text{Cu}_{0.6}\text{Ni}_{0.4}$ powder is illustrated in Fig. 4. It shows the agglomeration of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nano-particles. The FE-SEM images of the fractured surfaces of $\text{CoSb}_3\text{-}x\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanocomposites from samples #2 and #6 in Fig. 5a and b, respectively, show CoSb_3 grains with 300–600 nm in size (Fig. 5a), which co-exist with smaller size particles that appeared on the grains and interfaces of the larger CoSb_3 grains. These smaller particles that are pointed to with the red color arrow symbols might be $\text{Cu}_{0.6}\text{Ni}_{0.4}$. The $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoinclusions range between 50 and 150 nm in size (Fig. 5a). According to the SEM micrographs, the size of CoSb_3 particles fabricated through P2 is comparatively larger than the size of CoSb_3 particles fabricated through P1 for the same amount of x. Moreover, the size of CoSb_3 particles fabricated through P1 is reduced with the increase in the content of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloy. In addition, Fig. 5 show that the first fabrication method (Fig. 5a) resulted in a more evenly embedded $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoinclusions within the microstructure of the composite compared to the second fabrication method (Fig. 5b). This microstructure is promising for enhancing TE properties of CoSb_3 . As Fig. 5b shows, $\text{CoSb}_3\text{-}x\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanocomposites that were fabricated through P2 led aggregation of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ particles on the grains of CoSb_3 crystals unevenly. The EDS analysis of a randomly selected area of sample #2 (Fig. 5c), together with a quantitative atomic percentage, are tabulated in Fig. 5d. The results confirm the presence of Co, Sb, Cu, and Ni element in the composites (Fig. 5d). The elemental maps for samples #2 and #6 (Fig. 5e and f) indicate a more uniform distribution of elements for sample #2, which was prepared through P1 process than that of sample #6 prepared through P2 fabrication process. Also, the SEM micrographs show that $\text{CoSb}_3\text{-}x\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanocomposites are relatively porous, which is in agreement with their low relative bulk densities (Table 1).

2.2. Measurement of magnetic moment, charge carriers concentration and mobility

Fig. 6 displays the inverse magnetic moment of samples #1, 2, 3, and #4 as a function of temperature between 2 K and 400 K, under the applied auxiliary magnetic field of about 0.1 T. The magnetization of all samples is decreased with temperature and increased with the concentration of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ phase. Magnetization data shown in Fig. 6 suggested that $\text{CoSb}_3\text{-}x\text{Cu}_{0.6}\text{Ni}_{0.4}$ samples are diamagnetic at around room temperature and has a weak Curie-

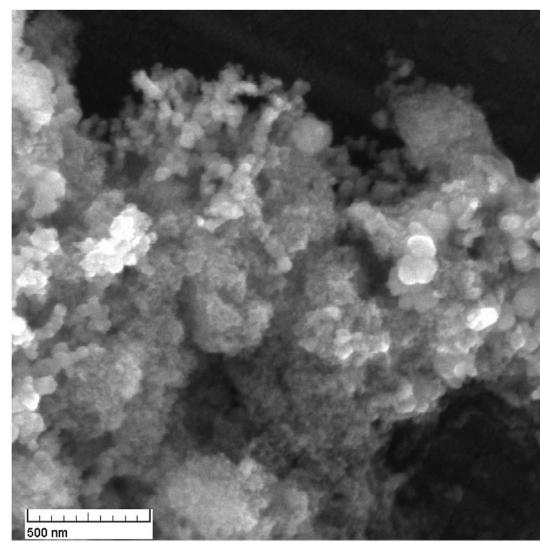


Fig. 4. FE-SEM image of as-hydrothermally synthesized powders of agglomerated $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoparticles.

Weiss contribution at low temperature, which agrees with previous reports [48,49]. Diamagnetization is caused by the zero-spin electron configuration of Co^{3+} . With the increase in $\text{Cu}_{0.6}\text{Ni}_{0.4}$, an increase in magnetization might originate from the low spin configuration of Ni ions [48].

The Hall effect and mobility of $\text{CoSb}_3\text{-}x\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanocomposites are measured at room temperature, and results are presented in Table 1. The Hall charge carrier concentrations are negative for all the samples, indicating electron as the majority charge carrier. The electron concentration is increased with the concentration of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloy in both sets of samples. The maximum electron concentrations of $n = 1 \times 10^{20} \text{ cm}^{-3}$ and $8 \times 10^{20} \text{ cm}^{-3}$ were obtained for samples #4 and #8, respectively. The significant difference in electron concentration between sample #4 and #8 might be due to uneven distribution of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloys in the CoSb_3 matrix of samples prepared by the second fabrication method (Fig. 5). The Hall mobility of electrons fluctuates between 15 and $5 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$ for all the samples (Table 1). The mobility remains less sensitive to the content of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloy for the first set of samples compared to the second set. This suggests that embedded $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoparticles have an insignificant influence on the electron mobility reduction, presumably due to the formation of a dense structure of $\text{CoSb}_3\text{-}x\text{Cu}_{0.6}\text{Ni}_{0.4}$ composite. Hall data of sample #8 shows that electrons mobility correlates with the charge carrier concentration (Table 1). The relatively low electron mobility in conjunction with its relatively high carrier concentration of sample #8 might originate from the increased electron

Table 1

Physical properties obtained for $\text{CoSb}_3\text{-}x\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanocomposite samples fabricated through procedures P1 and P2.

Physical Property	Relative Bulk Density (%)	Electron Concentration (10^{19} cm^{-3})	Mobility ($\text{cm}^2/\text{s.V}$)	E_b (meV) $312 \leq T/K < 605$	E_b (meV) $655 < T/K \leq 800$
Samples					
Sample #1; P1; x = 1 wt%	65	1.9	15	36	156
Sample #2; P1; x = 3.5 wt%	63	2.8	15	33	135
Sample #3; P1; x = 6 wt%	63	5	14	30	125
Sample #4; P1; x = 9 wt%	65	10	11	24	102
Sample #5; P2; x = 1 wt%	73	2	13	41	234
Sample #6; P2; x = 3.5 wt%	68	2.7	14	35	155
Sample #7; P2; x = 6 wt%	66	4	10	33	138
Sample #8; P2; x = 9 wt%	66	80	5	11	51

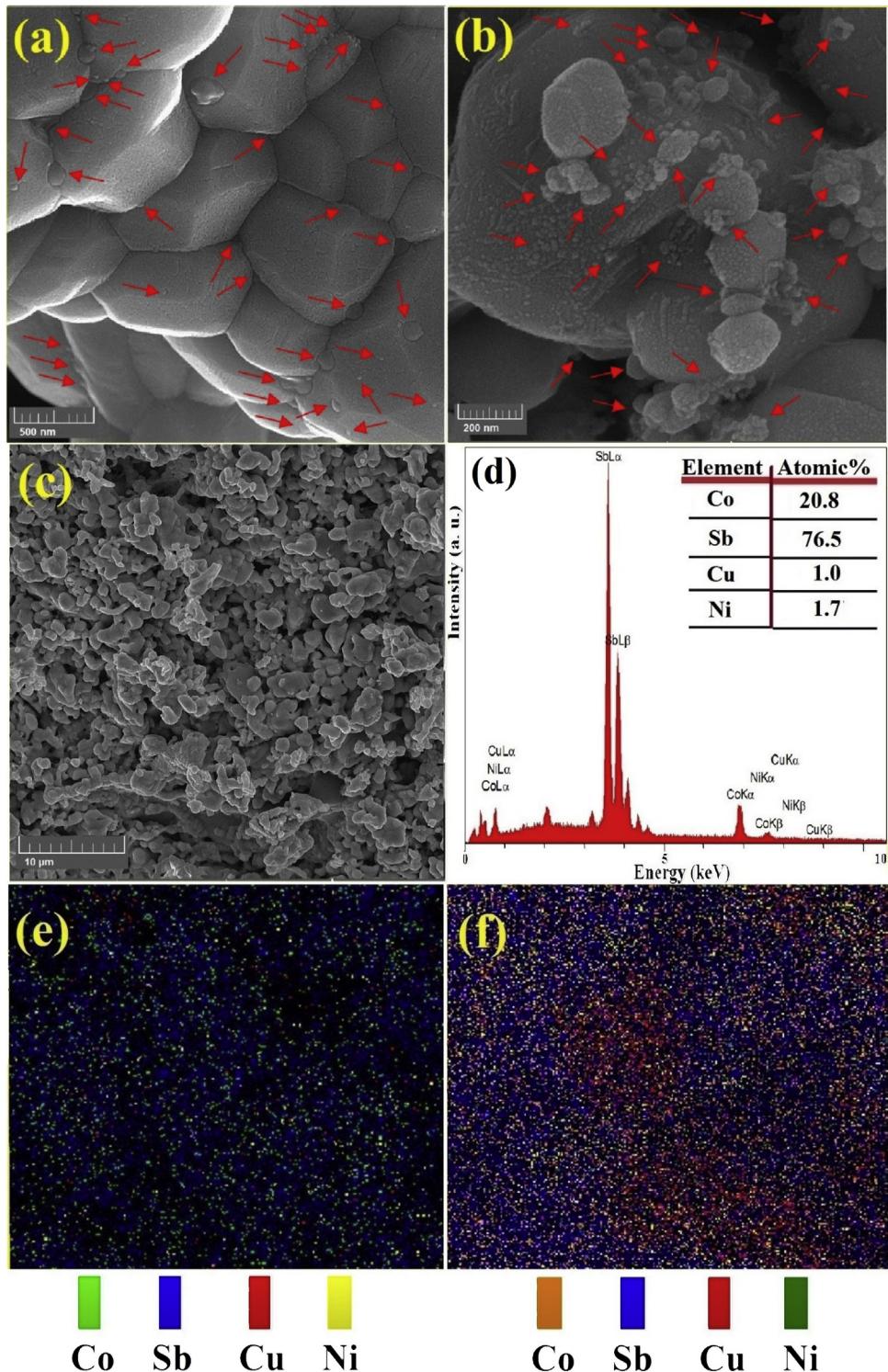


Fig. 5. FE-SEM images from the fractured surface of $\text{CoSb}_3\text{-}x\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanocomposites representatively taken for samples #2 with $x = 3.5$ wt%, fabricated through P1 (a), and sample #6 with $x = 3.5$ wt%, fabricated through P2 (b); the quantitative EDX composition analysis (d) is randomly obtained from a selected area of sample #2 (c); the EDX elemental mapping representatively checked for samples #2 (e) and sample #6 (f).

scattering from those unevenly distributed electron pockets related to $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloys and traces of other impurity phases (Fig. 3).

2.3. Measurement and analysis of thermoelectric properties

The electrical conductivity of $\text{CoSb}_3\text{-}x\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanocomposites

with $x = 1, 3.5, 6$ and 9 wt% is enhanced with $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloy concentrations (Fig. 7). It is worth to mention that the electrical conductivity of hydrothermally synthesized $\text{Cu}_{0.6}\text{Ni}_{0.4}$ alloy displayed almost temperature-independent behavior from 300 K to 550 K with an average value of $7 \times 10^5 \Omega^{-1}\text{m}^{-1}$ [43]. Compared with that of CoSb_3 material synthesized using the same

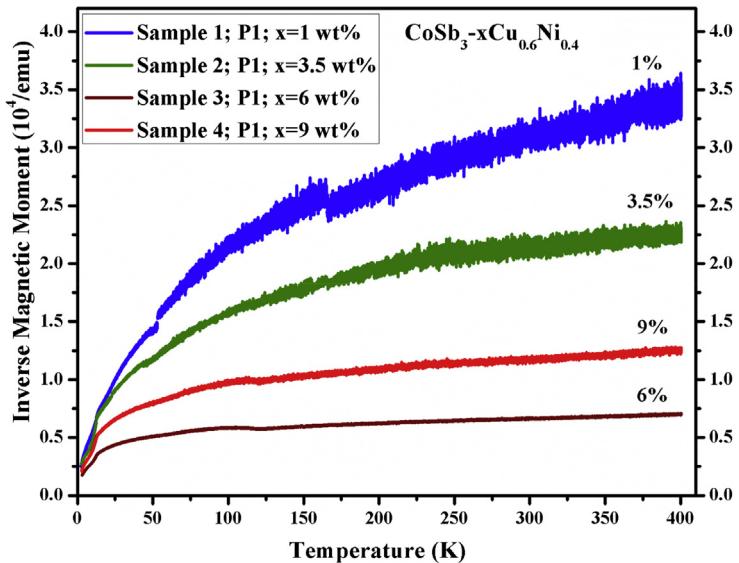


Fig. 6. Inverse magnetic susceptibility of $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites with $x = 1, 3.5, 6$, and 9 wt% (samples #1 through #4 fabricated using P1) as a function of temperature between 2 K and 400 K, under the applied auxiliary magnetic field of about 0.1 T.

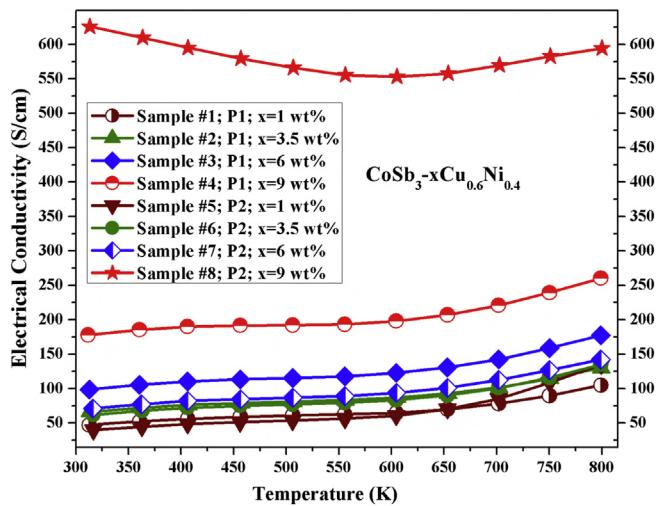


Fig. 7. The temperature dependence of electrical conductivity of $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites with $x = 1, 3.5, 6$, and 9 wt% between 312 K and 800 K; samples #1 through #4 were fabricated using P1 and samples #5 through #8 were fabricated using P2.

hydrothermal procedure and possessing comparable bulk density [39], the least enlargement of the electrical conductivity of the present composites is over four-times. All the electrical conductivity curves similarly display nonmetallic temperature dependence between room temperature and 800 K, except sample #8. The temperature dependence of the electrical conductivity of sample #8 decreases with increasing temperature below 600 K, resembles metallic behavior, and it switches to nonmetallic behavior for $600 < T/K \leq 800$. Commonly, the electrical conductivity of semiconductor materials such as pristine CoSb_3 displays strong temperature dependence. However, the relatively weak temperature dependence of the electrical conductivity of $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites might arise from the high porosity of samples. Similar weak temperature dependence of electrical conductivity was also reported for CoSb_3 samples fabricated using melting quenching-annealing-plasma activated sintering and

hydrothermal synthesis followed by annealing procedures [21,39]. The relatively low electrical conductivity values of samples might be due to high porosity in conjunction with a high concentration of grain boundaries, which features nanostructures. Highly porous structures could trap charge carriers, and a high concentration of grain boundaries could expedite scattering of charge carriers. Single-phase CoSb_3 samples fabricated via similar hydrothermal procedure showed a relatively low electrical conductivity as well [39,42]. For both sets of samples, the electrical conductivity is increased with the content of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloys. As seen on the micrograph images (Figs. 4 and 5), nanosized $\text{Cu}_{0.6}\text{Ni}_{0.4}$ particles connect CoSb_3 grains to its nearest neighbors; these highly conductive particles increase the electrical conductivity of the composite. The samples with $x = 1$ and 3.5 wt% showed almost the same electrical conductivity values, over the temperature range for both fabrication methods (Fig. 7). The electrical conductivity of samples with $x = 6$ wt% show similar behavior over the whole temperature range; however, the sample fabricated by the first method has slightly higher electrical conductivity values, mainly due to its higher electron mobility (Table 1). The significantly enhanced electrical conductivity of sample #8 might be attributed to its 10-times larger carrier concentration, compared to that of sample #4 and the rest of the samples. The relatively high carrier concentration and hence the significantly increased electrical conductivity of sample #8 could arise from a kind of short-range percolation as a result of inhomogeneous distribution of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ within CoSb_3 matrix.

The secondary phase of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloy could tune interfacial energy barriers to facilitate electron transition within grain boundaries. The influence of a second phase on the electron transport at grain boundaries of the matrix material can be studied by applying a potential barrier model [50,51]. The electrical conductivity correlates to the height of the potential energy barrier through Eq. (2):

$$\sigma \propto T^{-0.5} e^{-\frac{E_b}{k_B T}} \quad (2)$$

Where σ is electrical conductivity at temperature T ; E_b and k_B are the height of potential energy barrier and the Boltzmann constant, respectively. Fig. 8 shows the results of fitting the electrical

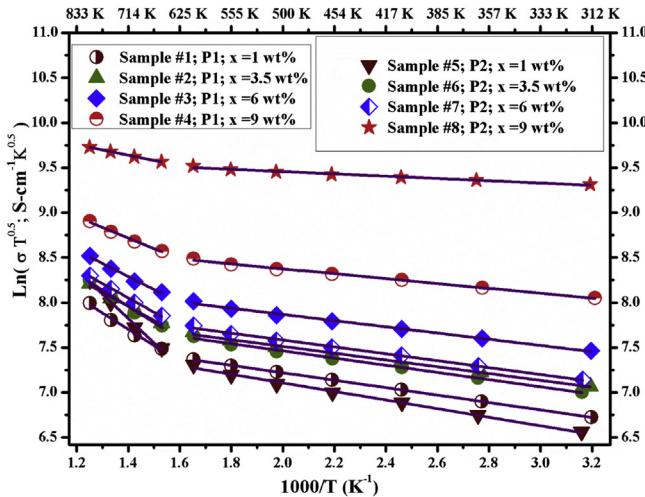


Fig. 8. Linear fitting of $\ln(\sigma T^{0.5})$ versus T^{-1} for $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites within two temperature regions of $312 \leq T/K < 605$ and $655 < T/K \leq 800$. The slopes of fitted curves are used to estimate the height of the grain boundary potential barrier (E_b); samples #1 through #4 were fabricated using P1, and samples #5 through #8 were fabricated using P2.

conductivity curves with Eq. (2). For each curve, the appropriate fitting is obtained within temperature intervals of $312 \leq T/K < 605$ and $655 < T/K \leq 800$. The estimated E_b values obtained at both temperature regions are presented in Table 1. The lower temperature region corresponds to smaller E_b values (Fig. 8), while the higher temperature region corresponds to larger E_b values (Table 1). At both temperature ranges, E_b is reduced systematically with the concentration of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloy for both sets of samples. The estimated E_b values using Eq. (2) for the second set of samples are slightly larger than that of the first set, except sample #8. At lower temperature range, the highest E_b value is 41 meV, and the lowest E_b value is 11 meV, respectively for sample #5 and #8. E_b is increased at $655 < T/K \leq 800$ region and its magnitudes vary between 234 meV and 51 meV for sample #5 and #8, respectively (Table 1). The significantly increased E_b values at $655 < T/K \leq 800$ might be due to the height of the potential barrier that holes carriers encounter during transition through grain boundaries. In other words, the selectively filtering of the lower energy holes carriers via the grain boundary could have correlated with the increased height of the potential barrier at higher temperature regions. The mentioned mechanism is schematically described in Fig. 9, thereat, the minority impurity states at a lower temperature (part 1) is declined the barrier height that electrons encounter, while at the higher temperature region (part 2) the depletion of impurity states in conjunction with contribution of holes carriers from valence band is increased the height of the potential barrier (E_b). The depletion of impurity electronic states with increasing

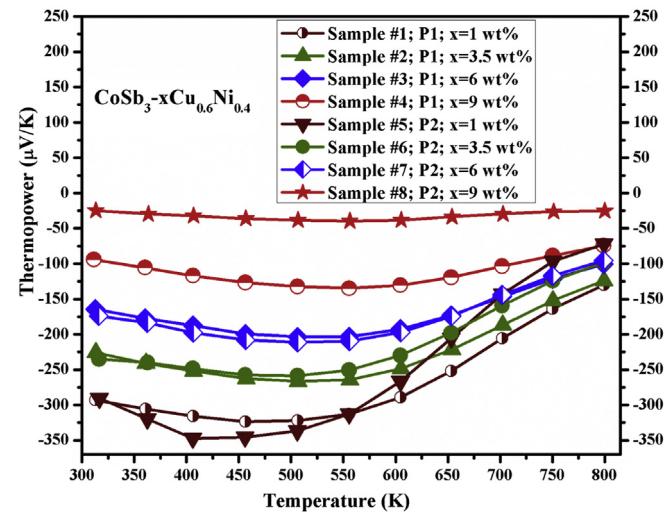


Fig. 10. The temperature dependence of thermopower of $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites with $x = 1, 3.5, 6$, and 9 wt% between 312 K and 800 K; samples #1 through #4 were fabricated using P1 and samples #5 through #8 were fabricated using P2.

temperature would lead to the activation of intrinsic states at higher temperature regions. This mechanism would emerge the bipolar effect in CoSb_3 structure thereat both electron and holes would contribute to transport properties [29,52,53]. The obtained data from fitted curves to the electrical conductivity values using Eq. (2) show that the estimated values of E_b is reduced at $655 < T/K \leq 800$ with the concentration of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloys. The direct contribution of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ electron states to the transport properties of CoSb_3 system could have presumably led to the mentioned mechanism.

The thermopowers of the $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites (Fig. 10) are negative, demonstrating n-type semiconductors. The room temperature absolute thermopower values of samples are reduced systematically with increasing the content of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloy (Fig. 10). The largest absolute thermopower value was obtained for composite samples with $x = 1$ wt%, and the lowest value corresponds to the sample #8. On the other hand, nanocomposites having the same content of $x = 3.5$ and 6 wt% display almost the same thermopower values below 525 K. The thermopower of sample #8 varies slightly at 25–40 $\mu\text{V/K}$ over the measured temperature range. The thermopower values as a function of electron concentration for sample #8 resembles the metallic behavior where thermopower is a function of electron concentration (n) $^{-\frac{2}{3}}$. Compared with that of CoSb_3 material synthesized using the same hydrothermal procedure [39], the absolute thermopower value of present $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites is enhanced up to about 20% for the sample with $x = 1$ wt% (Fig. 10).

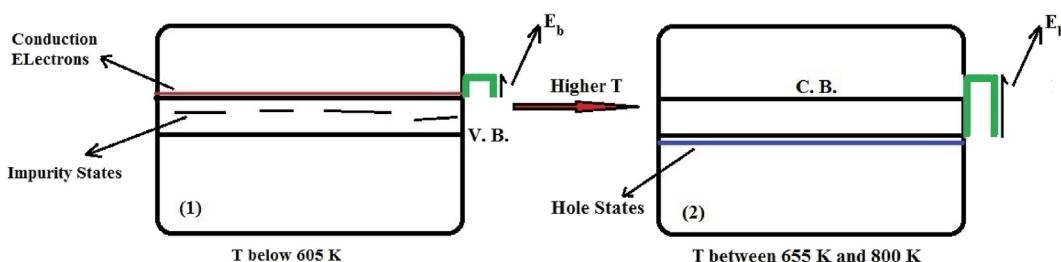


Fig. 9. A schematic to explain the influence of holes carriers to the enlarged E_b values at $655 < T/K \leq 800$ temperature region as compared with that of the contribution of impurity states to the electronic properties below 605 K.

Furthermore, the reduction of thermopower due to the bipolar effect that is discussed in the following discussion is partially suppressed, and the slope of its curve as a function of temperature is decreased as a result of compositing with $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloy.

Considering a partial contribution of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ and in situ formation of the impurity phase, the total thermopower of $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites could be expressed using Eq. (3),

$$S = \sum_i \frac{\sigma_i S_i}{\sigma} = \frac{\sigma_m S_m + \sigma_a S_a + \sigma_{ip} S_{ip}}{\sigma_m + \sigma_a + \sigma_{ip}} \quad (3)$$

where S , S_i , σ_i and $\sigma = \sigma_m + \sigma_a + \sigma_{ip}$ denote total thermopower, partial thermopower, partial electrical conductivity, and total electrical conductivity, respectively. In Eq. (3), m , a and ip indices represent CoSb_3 matrix, $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloy, and in situ formed impurity phases, respectively. The thermopower of hydrothermally synthesized CoSb_3 is usually negative below 400 K [39,41]. The absolute thermopower of n-type $\text{Cu}_{0.6}\text{Ni}_{0.4}$ alloy was shown to increase with temperature from about $-44 \mu\text{V/K}$ at 300 K to about $-62 \mu\text{V/K}$ at 550 K [43]. The relatively reduced room temperature thermopower of the composites might arise from an increased $\frac{\sigma_i}{\sigma}$ ratio at a higher concentration of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ and impurity phases. The reduced values of S with $\text{Cu}_{0.6}\text{Ni}_{0.4}$ concentration imply that impurity traces presumably could have been p-type semiconductors (Fig. 3); hence it could have led to further reduction of thermopower at room temperature (Fig. 10). Above 400 K, the probable contribution of the thermally activated intrinsic holes carriers from CoSb_3 matrix has compensated the corresponding thermopower component (S_m) due to the bipolar effect [29,39,41].

It is commonly known that the bipolar effect mainly arises from the intrinsic band structure of the materials and hence can affect thermoelectric transport properties, including electrical conductivity, thermal conductivity, and thermopower. Typically, the bipolar effect reduces the thermopower but enhances both thermal conductivity and electrical conductivity. All nanocomposite samples (Fig. 10) show the bipolar effect. However, the temperature corresponds to the maximum thermopower is increased with the concentration of $\text{Cu}_{0.6}\text{Ni}_{0.4}$.

Fig. 11 displays the thermoelectric power factor of $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ with $x = 1, 3.5, 6$, and 9 wt% between room temperature

and 800 K. The maximum power factor of about $6.33 \mu\text{Wcm}^{-1}\text{K}^{-2}$ is obtained for sample #1 around 506 K, slightly improved compared to the previous reports for pristine CoSb_3 [24,29,41,52]. The peak of power factor is shifted to higher temperatures, while the values are reduced with the ratio of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloys, mainly due to the significant reduction of the total thermopower (Fig. 10).

The total thermal conductivities of $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites between 312 K and 800 K are illustrated in Fig. 12.

Microstructural analysis (Fig. 5) indicated that the size of the skutterudite grains is larger than the calculated phonon mean-free-path (135 nm) for CoSb_3 structure and therefore larger than the value predicted by kinetic theory ($\sim 4\text{nm}$). Also, considering the fact that the transport properties measurement is performed well above 50 K, the special phonon confinement effects on the specific heat capacity of the composites are negligible [54,55]. Hence, by assuming grain size-independent specific heat capacity, we may consider a constant C_{pi} for each component and apply Eq. (1) to estimate C_p of the samples. The largest total thermal conductivity values are obtained for sample #8, and the smallest values were obtained for sample #1 (Fig. 12). For the first set of samples, κ values are significantly lower than that of the second set, except for the samples #3 and #7 ($x = 6$ wt%). The κ of all samples is decreased with temperature for $312 \leq T/\text{K} \leq 600$, albeit at different rates; for $600 < T/\text{K} \leq 800$, κ is increased with temperature for all samples except sample #8 that κ almost plateau remains roughly constant above 555 K. This is due to the large carrier concentration of this sample (Table 1). Compared with that of CoSb_3 material synthesized using the same hydrothermal procedure [39], the measured total thermal conductivity of present $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites is enlarged over two-times and increased upon increasing the content of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ within the same temperature interval. The measured total thermal conductivity of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ alloy showed a relatively small increase with temperature from about $3 \text{ Wm}^{-1}\text{K}^{-1}$ at 300 K to about $3.5 \text{ Wm}^{-1}\text{K}^{-1}$ at 550 K [43].

The lattice phonon component of the total thermal conductivity could be estimated by subtracting the electronic contribution from the overall thermal conductivity $\kappa_L = \kappa - \kappa_e - \kappa_{bi}$. In the absence of the bipolar effect κ_{bi} , the electronic contribution (κ_e) to the thermal conductivity could be estimated using the Wiedemann-Franz law, $\kappa_e = \sigma LT$; thereat $L = \frac{\pi^2 (k_B)}{e^2} \approx 2.45 \times 10^{-8} \text{ W}\Omega\text{K}^{-2}$ (for metals or

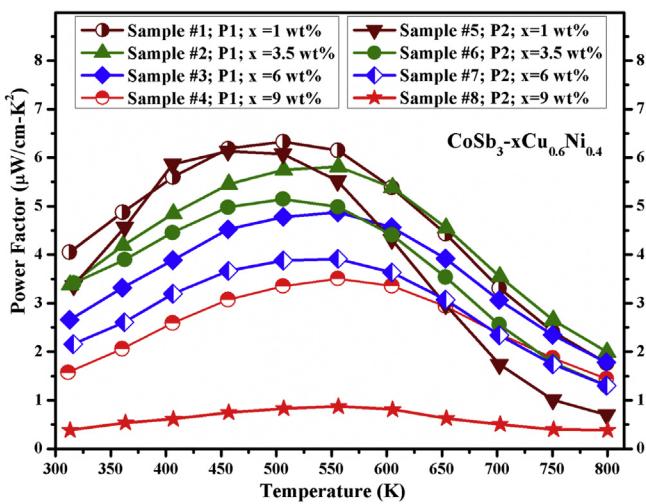


Fig. 11. The thermoelectric power factor of $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites with $x = 1, 3.5, 6$, and 9 wt% as a function of temperature between 312 K and 800 K; samples #1 through #4 were fabricated using P1 and samples #5 through #8 were fabricated using P2.

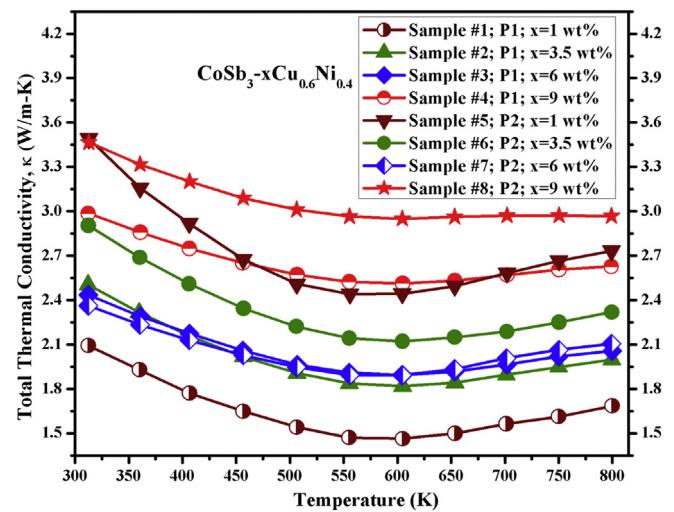


Fig. 12. The total thermal conductivity (κ) of $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites with $x = 1, 3.5, 6$, and 9 wt% as a function of temperature between 312 K and 800 K; samples #1 through #4 were fabricated using P1 and samples #5 through #8 were fabricated using P2.

degenerate semiconductors), where L is the Lorenz number, and σ is the electrical conductivity at absolute temperature T . The contribution of σLT is estimated, and the obtained results show the corresponding magnitudes varies from $0.036 \text{ Wm}^{-1}\text{K}^{-1}$ to $0.51 \text{ Wm}^{-1}\text{K}^{-1}$ for $312 \leq T/K \leq 800$ for all the samples, except sample #8 ($x = 9 \text{ wt\%}$). The magnitudes of σLT for sample #8 varies from $0.48 \text{ Wm}^{-1}\text{K}^{-1}$ to $1.16 \text{ Wm}^{-1}\text{K}^{-1}$ for $312 \leq T/K \leq 800$, which is in agreement with the corresponding relatively high electrical conductivity of the title composite (Fig. 7). By disregarding the deviation of L for composite samples from that of a single-phase metal or degenerate semiconductor, and in the presence of the bipolar effect κ_{bi} , the electronic contribution to the total thermal conductivity could be estimated by $\sigma LT + \kappa_{bi}$; in which the bipolar contribution κ_{bi} could be estimated using Eq. (4) [53].

$$\kappa_{bi} = \frac{\sigma_e \sigma_h}{\sigma_e + \sigma_h} (S_e - S_h)^2 T \quad (4)$$

where, $\sigma_{e,h}$ and $S_{e,h}$ represents electrons (holes) contribution to the electrical conductivity and thermopower, respectively.

The temperature dependence of $\kappa - \sigma LT$ for all samples is represented in Fig. 13. All samples present a bipolar effect curvature except for sample #8, which has much higher charge carrier concentration.

The onset temperature for bipolar effect can be estimated by observing the bipolar trends shown by the transport properties. In this work, the onset temperature of the bipolar effect for each sample is compared with respect to their corresponding thermal conductivity κ . The relatively small magnitudes of σLT (less than 17% of the total κ) could be attributed to the relatively weak electrical conductivity of the present $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ composites. Fig. 13 shows the sum of the lattice and bipolar thermal conductivity, i.e., $\kappa - \sigma LT = \kappa_L + \kappa_{bi}$. κ_L generally has a reducing trend with temperature due to the increase of the 3-phonon scattering. But κ_{bi} slope versus temperature is positive due to the increase in the population of the thermally excited carriers. As such, at low temperatures, lattice contribution is dominant, and at high temperatures, the bipolar contribution controls the trend of $\kappa - \sigma LT$. It can be seen that for all samples, except sample 5, the curvature changes at approximately 550–600 K. The same trend is observed for the thermopower versus temperature (Fig. 10). The exact onset temperature of seeing the bipolar effect may be somewhat different for

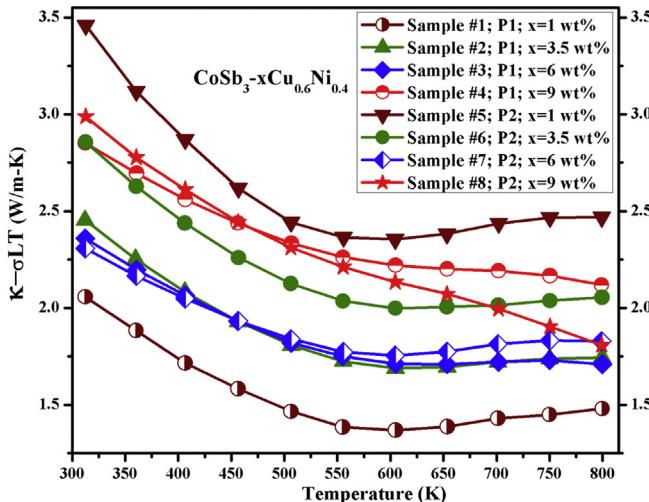


Fig. 13. The temperature dependence of $\kappa - \sigma LT$ calculated for $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites with $x = 1, 3.5, 6$ and 9 wt\% between 312 K and 800 K thereat the σLT term was estimated using the Wiedemann-Franz law.

the thermal conductivity and the thermopower depending on the relative strength of their various components. Sample 5 shows a smaller κ_{bi} onset temperature for both the thermal conductivity and thermopower, which is attributed to its smaller carrier concentration.

Fig. 14 displays the dimensionless TE figure of merit (zT) for $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites with $x = 1, 3.5, 6$, and 9 wt\% between room temperature and 800 K . The maximum zT of about 0.23 is achieved at 555 K for sample #1. In general, the first set of samples show higher zT values than the second set (for the same amount of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloy). The obtained zT value of 0.23 is higher than that of unfilled pristine CoSb_3 synthesized using the hydrothermal procedure, or previous reports used other fabrication methods [19,36,37,39,41]. Hence, the fabrication of potential TE composites using the first procedure (P1) in conjunction with the appropriate choice of nanoinclusions seems a promising route to enhance zT of corresponding materials beyond its current values.

3. Conclusion

CoSb_3 and $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloy were separately synthesized through hydrothermal procedures. The influence of fabrication sequences of composite materials on the formation of the desired crystal phase and transport properties of the final composite materials was studied. The obtained samples were highly porous in nature, and traces of impurity phases, including CoSb_2 , NiSb , and NiCoSb were identified in the final compounds.

Nanoinclusions vary in size between 50 nm and 150 nm , while CoSb_3 particles are between 300 nm and 600 nm . The EDX mapping shows a more uniform distribution of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloy in the first set of samples.

The magnetization of the first set of samples increased with the concentration of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloys, while it is decreased with temperature. The electrical conductivity of $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites is enhanced with the content of $\text{Cu}_{0.6}\text{Ni}_{0.4}$. The electrical conductivity demonstrates weak temperature dependence, probably due to the relatively high porosity of the samples. The electrical conductivity of all samples displays nonmetallic temperature dependence behavior, except sample with $x = 9 \text{ wt\%}$, which has much higher carrier concentration than the other samples. The obtained results from the applied potential barrier model

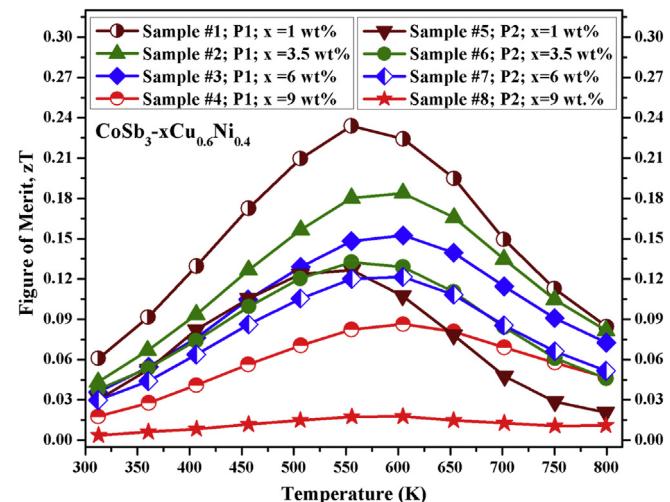


Fig. 14. The zT as a function of temperature for $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ nanocomposites with $x = 1, 3.5, 6$, and 9 wt\% between 312 K and 800 K ; samples #1 through #4 were fabricated using P1 and samples #5 through #8 were fabricated using P2.

showed that the height of the energy barrier was reduced with increasing content of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoinclusions for both sets of samples.

The temperature-dependent thermopower values displayed that the onset of bipolar effect is shifted to higher temperatures with the concentration of $\text{Cu}_{0.6}\text{Ni}_{0.4}$.

The first set of samples possesses lower total thermal conductivity than the samples fabricated by a second fabrication method, presumably due to their relatively high porosity. On the other hand, the higher carrier concentration of sample #8 is an exception that displays a high contribution of the electronic component to its total thermal conductivity.

The maximum zT value was obtained at 555 K for the sample with $x = 1$ wt%, fabricated by the first method. The zT of present $\text{CoSb}_3\text{-xCu}_{0.6}\text{Ni}_{0.4}$ is higher than pristine CoSb_3 , synthesized by the same hydrothermal method. In general, the zT values of samples fabricated by the first method are larger than those made by the second method for samples with the same amount of $\text{Cu}_{0.6}\text{Ni}_{0.4}$ nanoalloys.

CRediT authorship contribution statement

Ahmad Gharleghi: Conceptualization, Formal analysis, Investigation, Methodology, Supervision, Resources, Writing - original draft, Writing - review & editing. **Md Mobarak Hossain Polash:** Formal analysis. **Rasoul Malekfar:** Funding acquisition. **Sima Aminorroaya Yamini:** Writing - review & editing. **Daryoosh Vashaee:** Funding acquisition, Investigation, Supervision, Resources, Writing - review & editing.

Declaration of competing interest

There is no conflict of interest to declare.

Acknowledgments

This work was partially supported by the National Science Foundation, United States under grant numbers ECCS-1351533, ECCS-1515005, and ECCS-1711253. AG acknowledges the supports from I. R. Iran's National Elite Foundation-3321.

Appendix A. Supplementary data

Supplementary data to this article can be found online at <https://doi.org/10.1016/j.jallcom.2020.156188>.

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