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Simultaneous Sulfite Electrolysis and Hydrogen Production Using Ni Foam-Based Three-Dimensional Electrodes

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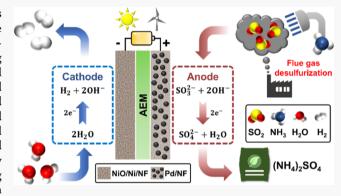
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ABSTRACT: The electrochemical oxidation of sulfite ions offers encouraging advantages for large-scale hydrogen production, while sulfur dioxide emissions can be effectively used to obtain value-added byproducts. Herein, the performance and stability during sulfite electrolysis under alkaline conditions are evaluated. Nickel foam (NF) substrates were functionalized as the anode and cathode through electrochemical deposition of palladium and chemical oxidation to carry out the sulfite electro-oxidation and hydrogen evolution reactions, respectively. A combined analytical approach in which a robust electrochemical flow cell was coupled to different *in situ* and *ex situ* measurements was successfully implemented to monitor the activity and stability during electrolysis. Overall, satisfactory sulfite conversion and hydrogen



production efficiencies (>90%) at 10 mA·cm⁻² were mainly attributed to the use of NF in three-dimensional electrodes with a large surface area and enhanced mass transfer. Furthermore, stabilization processes associated with electrochemical dissolution and sulfur crossover through the membrane induced specific changes in the chemical and physical properties of the electrodes after electrolysis. This study demonstrates that NF-based electrocatalysts can be incorporated in an efficient electrochemical flow cell system for sulfite electrolysis and hydrogen production, with potential applications at a large scale.

■ INTRODUCTION

Sulfur dioxide (SO₂) emissions produced from coal, heavy oil, and diesel combustion have led to severe effects on human health, climate change, and the global environment. East Asia is the most threatened region by anthropogenic SO₂ emissions because of China's high dependence on coal. To mitigate the current situation, flue gas desulfurization (FGD) technologies have been implemented in order to capture SO₂ from gas streams in power plants. In particular, wet-type technologies with high removal efficiencies are preferred, in which SO₂ becomes sulfite (SO₃²⁻). Then, by exposing the resulting solution to strong oxidants, such as ozone, disposals can be transformed into useful byproducts. Notably, the use of aqueous ammonia as an absorbent with subsequent oxidation yields ammonium sulfate, which has potential use as a fertilizer.

Electrochemical technologies have been extensively used for environmental remediation because of their exceptional removal efficiencies and superior performance. Additionally, electrochemistry offers promising advantages for sustainable interconversion of chemical energy and electrical work because they can be supplied by green electrons from solar and wind power. In the research field of FGD, recent studies have demonstrated that replacing typical chemical oxidation with

electrochemical steps has great potential for harvesting profitable byproducts from disposals, thus lowering overall costs. $^{13-16}$ In particular, the electrochemical oxidation of ammonium sulfite at slightly alkaline pH yields high-purity hydrogen (H_2) and ammonium sulfate simultaneously, as recently demonstrated by our previous work. 13

Figure 1 shows the ammonia-based FGD process, in which the oxidation step is performed *via* the electrochemical oxidation of sulfite. Extensive research has been done regarding the absorption step, including process simulation, scrubber design, and absorption models.^{7,17–19} However, while absorption units and product handling technologies are commercially available,²⁰ the electrochemical step still leaves much to be improved and only preliminary studies and proofs of concept are available in the literature. Aspects such as sulfite speciation due to the pH,¹³ the kinetics on Pd and Pt electrodes,^{21,22} and preliminary hydrogen production measure-

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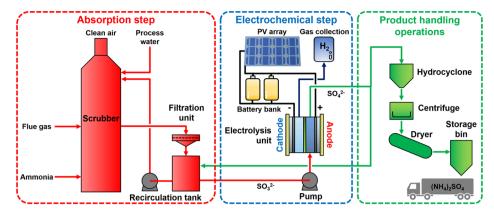


Figure 1. Schematic illustration of the ammonia-based FGD process with an electrochemical sulfite oxidation step.

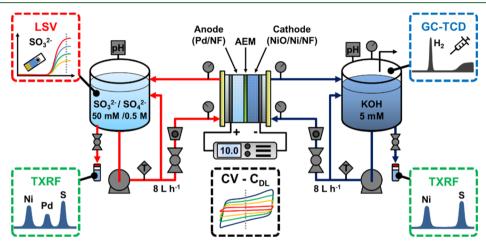


Figure 2. Schematic illustration of the flow cell system and the analytical techniques used to monitor electrolysis tests.

ments have been reported using typical three-electrode cells and planar electrodes. 13,23 Therefore, further improvement on electrode design, catalyst stability, and cell performance is required to improve the robustness of the step. In this sense, the use of nickel foam (NF) as a three-dimensional (3D) substrate for electrocatalysts offers promising advantages for novel technologies, as demonstrated in water electrolysis, because of its high conductivity, large surface area, and great stability in alkaline media. 24–26 Moreover, by depositing catalysts onto NF, costs can be effectively reduced, while mass transfer and the surface area are greatly improved. In spite of these features, its use in electrochemical technologies for environmental applications is scarce and its potential in other approaches has not been fully tested. 28,29

Herein, sulfite electrolysis using surface-modified NF electrodes in a novel electrochemical reactor design, as a pioneering electrochemical oxidation approach for FGD, is addressed. In brief, this article covers the performance and stability assessment of the electrodes during alkaline electrolysis in a robust electrochemical flow cell, which provides a more realistic and reproducible testing environment at the lab scale. Through a series of experiments, the performance in terms of $\rm H_2$ production and $\rm SO_3^{2-}$ conversion as well as the physicochemical stability of the electrochemical step shown in Figure 1 because the remaining steps in FGD are well known and can be effectively adapted to specific flue gas compositions and flow rates. Still, the improvement of the electrochemical step offers important advantages, namely, (1)

the production of high-purity H_2 and ammonium sulfate while SO_2 emissions are exploited, (2) the use of NF as an improved and cost-effective 3D substrate to increase the surface area of deposited electrocatalysts, and (3) the use of an easily scalable flow cell with superior performance. Further development should be aimed to successfully integrate this electrochemical step in FGD processes for validation at a large scale.

EXPERIMENTAL SECTION

Two different electrodes, namely, NiO/Ni/NF and Pd/NF, were fabricated. For comparison, bare NF and Pd/C/NF electrodes were also prepared and tested (Figure S1). NiO/Ni/NF electrodes were prepared by a simple chemical oxidation method using $K_2S_2O_8$ as previously reported by He et al.³⁰ Pd/NF electrodes were prepared by a one-step electrochemical plating method as previously reported by Wang et al.³¹ A Pd loading of 0.49 \pm 0.06 mg·cm⁻² was obtained. The electrodes were characterized before and after electrolysis by X-ray diffraction (XRD), scanning electron microscopy (SEM), energy-dispersive X-ray spectroscopy (EDX), and X-ray photoelectron spectroscopy (XPS). The redox behavior and the electrochemically active surface area (ECSA) were estimated through electrochemical measurements. Details are given in the Supporting Information.

Sulfite electrolysis was performed during a 24 h period in a 3D-printed filter-press electrochemical flow cell as described in a previous work.²⁷ A schematic diagram of the one-unit flow cell system and the set of analytical techniques is shown in Figure 2. Electrodes were placed in each chamber (Figure S2):

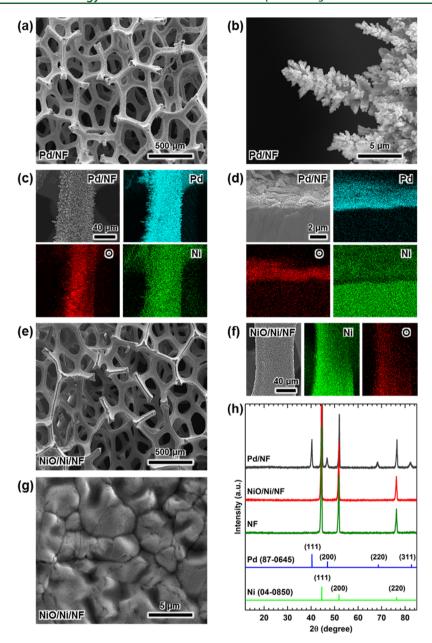


Figure 3. Electrode characterization: SEM images for the (a) Pd/NF porous network and (b) Pd dendrite, (c) elemental mapping for the Pd/NF branch, (d) elemental mapping for the Pd/NF cross section, (e) NiO/Ni/NF porous network, (f) elemental mapping for the NiO/Ni/NF branch, (g) NiO/Ni/NF surface, and (h) XRD results.

NiO/Ni/NF as the cathode and Pd/NF as the anode. Nicoated stainless-steel plates were used as current collectors. A 5 mM KOH solution (pH \sim 12) was recirculated in the cathodic section of the cell, while a fresh 50 mM (NH₄)₂SO₃ in 0.5 M $(NH_4)_2SO_4$ solution, as the supporting electrolyte, was loaded into the anodic section. The latter acted as a simulated electrolyte coming from a flue gas absorption step as used by previous studies.⁵ For further details on the properties of the effluents from ammonia-based FGD, please refer Table S1 in the Supporting Information. A volume of 250 mL was used for each section. Importantly, KOH solutions were purified by using a previously reported method to remove Fe impurities to avoid incidental activity enhancement for the oxygen evolution reaction (OER) during tests.³² Note that the anion exchange membrane (AEM) delimited both sections. The flow rate was maintained at 8 L h⁻¹ using peristaltic pumps and calibrated

rotameters. Electrolytes were degasified with ultrahigh purity Ar for 30 min before any tests.

Electrolysis was performed as chronopotentiometric runs at 10 mA·cm $^{-2}$ using an Interface 1000 potentiostat/galvanostat (Gamry). Tests were carried out in a three-electrode configuration using an Ag/AgCl reference electrode. Anodic linear sweep voltammetry (LSV) scans between 0.0 and 1.3 V versus Ag/AgCl, at a scan rate of 10 mV·s $^{-1}$, were recorded before and after each test. For the cathode, LSV scans were recorded from -0.48 to -1.5 V versus Ag/AgCl at 10 mV·s $^{-1}$. All the potentials were converted into the reversible hydrogen electrode scale. The ECSA fluctuation along time was estimated by checking the double-layer capacitance ($C_{\rm DL}$). Liquid samples (50 μ L) were taken from the anolyte and analyzed to determine the sulfite concentration. The concentrations of Ni, Pd, and S in the electrolytes were

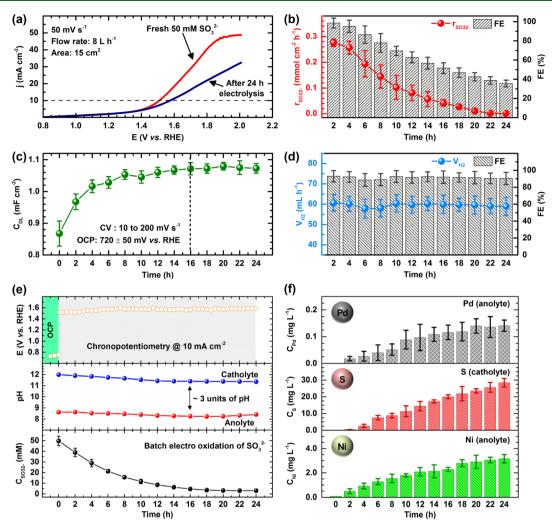


Figure 4. Electrolysis performance results: (a) anodic i-V curves before and after electrolysis, (b) SO_3^{2-} consumption rates with the corresponding FEs, (c) double-layer capacitance of the anode with time, (d) H_2 production rates and the corresponding FEs, (e) electrode potential, pH, and SO_3^{2-} concentration with time, and (f) concentration of dissolved Pd, S, and Ni in the corresponding electrolytes with time.

assessed by means of total-reflectance X-ray fluorescence (TXRF). Samples were analyzed using an S2 PICOFOX spectrometer (Bruker Nano GmbH) by using an internal standard (Y, 5 mg L $^{-1}$). Finally, the evolved H $_2$ gas was estimated by means of gas chromatography. The faradaic efficiencies (FEs), reaction rates, and performance metrics were calculated. Details are given in the Supporting Information. Note: electrolysis tests were performed by triplicate.

RESULTS AND DISCUSSION

Electrode Characterization. SEM images of Pd/NF anodes are shown in Figures 3 and S4. For comparison, SEM and elemental mappings of pristine NF are shown in Figure S5. In both materials, interconnecting pores with diameters below $500~\mu m$ are distributed along a consistent 3D structure. However, while pristine NF exhibits a rather smooth surface, Pd/NF is covered with a dense layer of Pd microstructures. Remarkably, dendrite-like microstructures can be seen, especially near the edges of NF branches (Figure 3b). The diameter of the spikes protruding from these dendrites is estimated to be in the 50-500~nm range (Figure S4). Additional SEM images display Pd deposits deep within the porous substrate (Figure S6). Other tight spaces may not

allow dendritic growth, which could explain Pd agglomeration (Figure S6a). EDX elemental mapping reveals that Pd uniformly covered the NF branches (Figure 3c), which demonstrates the high quality of Pd electrodeposition using a flow cell. A detailed analysis of a cross-sectional view of Pd/ NF (Figure 3d) shows a thin Pd layer (~300 nm). The presence of oxygen on the surface is evident in EDX elemental mappings and atomic compositions (Table S2), suggesting that some Pd oxides could be formed by exposure to air. Still, only cubic Pd metal (ICDD PDF# 87-0645) and cubic Ni metal (ICDD PDF# 04-0850), which correspond to the as-deposited Pd and the NF substrate, respectively, can be seen in XRD patterns (Figure 3h).³¹ Additionally, XPS measurements (Figure S9) confirmed the presence of Pd, Ni, and O. Overall, these results demonstrate that high-quality anodes were synthesized using a one-step electrodeposition method in a flow cell. The Pd electrocatalyst was distributed uniformly over the NF substrate and the observed dendrite-like morphology confers a large ECSA, which increases the number of exposed active sites for sulfite electro-oxidation. Therefore, superior Pd anodes can be obtained using a simple preparation method without requiring several synthetic steps.

For comparison, Pd/C/NF electrodes were prepared by spray coating. SEM images and elemental mapping are shown

in Figure S8. In contrast to Pd/NF, the distribution of Pd is not homogeneous, and some portions of the NF substrate were exposed. Moreover, the catalyst severely agglomerates, creating flakelike microstructures which are stacked randomly. This suggests that Pd/C/NF electrodes prepared by spray coating are not useful because agglomeration decreases catalyst utilization, increases the inactive surface area (e.g., the carbon support and binder material), and ultimately results in a lower ECSA and higher cell resistance, as has been reported for Pt/ C. 33,34 Therefore, binder-free Pd/NF anodes prepared by electrodeposition are a better alternative for sulfite electrooxidation

SEM images of the as-prepared NiO/Ni/NF cathodes are shown in Figures 3 and S9. Note that when compared with pristine NF (Figure S5), the NiO/Ni/NF electrode exhibits a slightly roughened surface which confers a larger surface area. This is more evident at the highest magnification (500 nm) as some nanostructures can be seen (Figure S9). Moreover, a significant presence of NiO nanoclusters was not evident, which suggests that the Ni surface was not substantially oxidized.30° Although elemental mapping in Figure 3f shows both nickel and oxygen distributed along the NF branch, NiO peaks were not seen in the XRD patterns (Figure 3h), and only planes of the Ni metal are obvious. XPS analysis (Figure S10) showed only the presence of Ni, O, and C signals, which suggest that the NF surfaces of the as-obtained samples might be slightly oxidized. 30,35 This further demonstrates that only amorphous NiO clusters could be isolated over the cathode. Such an electrode composition favors the hydrogen evolution reaction (HER) because NiO promotes the cleavage of the H-OH bond, while contiguous metallic Ni preferentially adsorbs H, enhancing the overall recombination into H_2 and decreasing the overpotential.³⁰

Additional electrochemical characterization was performed to compare the surface area and electrode activity. The ECSA was estimated through the C_{DL} method (Figure S11), while cyclic voltammetry (CV) was used to elucidate the redox behavior (Figure S12). Pd/NF displayed the highest ECSA, which is attributed to the dendrite-like microstructures produced by the well-controlled electrodeposition method. For NiO/Ni/NF, the noticeable improvement is attributed to an etching process via $K_2S_2O_8$ oxidation.³⁰ The removal of Ni roughened the surface, which may also improve bubble removal during the HER.²⁴ Regarding redox behavior, only Pd/NF and Pd/C/NF electrodes exhibited activity toward SO₃²⁻ electro-oxidation, while a higher HER activity is evident for NiO/Ni/NF compared to that for pristine NF. Indeed, this confirms the suitability of Pd/NF and NiO/Ni/NF electrodes for sulfite electro-oxidation and HER, respectively.

Performance and Stability Results. The sulfite electrolysis results are shown in Figure 4. From i-V curves (Figure 4a), it is evident that SO_3^{2-} was fully consumed after 24 h. The initial curve exhibits an increase in the current density until it reaches the mass transfer-limited region close to 50 mA·cm⁻². After electrolysis, the curve no longer resembles that of SO₃²⁻ oxidation, and the potential at 10 mA·cm⁻² shifts to ca. 80 mV. Figure 4b shows the sulfite electro-oxidation rates calculated from sulfite concentration profiles (Figure 4e) and the corresponding FEs. The electro-oxidation rates decrease with time since the availability of $SO_3^{\ 2^-}$ dropped due to batch oxidation.¹³ Moreover, the FEs are not constant and decrease as well. This implies that once SO_3^{2-} begins to be scarce in the electrolyte, simultaneous reactions proceeded because of a

galvanostatic mode. It is evident that the secondary reaction which occurred at the anode is the OER because (1) bubble generation at the anode was observed especially after 6 h, (2) the i-V curve after electrolysis closely resembles that of the OER, and (3) headspace samples from the anolyte container analyzed using a gas chromatograph and a thermal conductivity detector (TCD) demonstrate that evolved O₂ increased with time (Figure S13). Although this may appear to be unfavorable, we consider the OER to be beneficial because O₂ bubbles may enhance SO_3^{2-} oxidation in the bulk, in a similar way strong oxidants such as O3 are bubbled in FGD disposals for the same purpose. Furthermore, O2 could be used as another byproduct in the overall process because the membrane avoids H2 and O2 from mixing.

As a benchmark, the performance of Pd/C/NF and NF electrodes was evaluated. The electro-oxidation rates were reduced notably after 8 h for Pd/C/NF (Figure S14), while pristine NF electrodes exhibited low FEs and i-V curves resembling only OER activity (Figure S15). Evidently, pristine NF is not active toward SO_3^{2-} oxidation, as previously shown in the redox behavior characterization (Figure S12). The disadvantageous performance of the Pd/C/NF electrode is attributed to the reduced number of exposed Pd sites caused by catalyst agglomeration during spray coating, as previously described in the characterization section. Hence, even though both Pd/NF and Pd/C/NF electrodes had an equal catalyst loading, in the latter, less Pd active sites were in contact with sulfite ions. This further demonstrates the superior features of the Pd/NF anode.

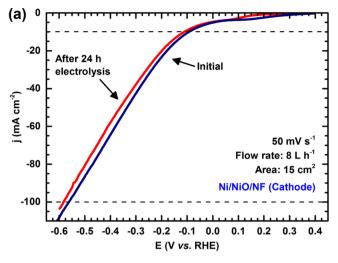
An interesting behavior can be seen in Figure 4c, in which the $C_{\rm DL}$ at the anode stabilizes following an asymptotic trend. We attribute this behavior to a change in the ECSA as the reaction progresses, which implies that the initial surface condition may not be constant throughout electrolysis. Similar trends have been reported for OER electrocatalysts, in which the oxidation of the surface induced morphology and/or composition changes during OER.³⁶ In fact, this increase and stabilization of the ECSA throughout the OER has been previously seen.³⁷ This effect is discussed in detail in the following sections by comparing the electrodes before and after tests. Note that a similar effect was seen in bare NF (Figure S15), which can be attributed to Ni oxidation during the OER.³⁸

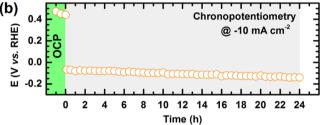
The H₂ production rates and FEs are shown in Figure 4d. The hydrogen production rate was 0.252 ± 0.007 mmol h⁻¹ cm⁻² after averaging all the measurements during 20 h, which corresponds to approximately 60 mL of H₂ gas produced every 2 h using just one electrolysis unit. The FE was 91.3 \pm 2.5% throughout electrolysis, and its fluctuation below 100% is attributed to the saturation of the electrolyte and bubbles attached to the walls of the catholyte container. Note that contrary to the anode, the FEs are constant because the HER is the dominant event. Overall, the results suggest that satisfactory FEs and H2 production rates were achieved by more efficient bubble removal derived from the combination of NF and the flowing electrolyte, as compared to our previous work in a stagnant electrolyte and Pd foil electrode. 13 Furthermore, no other gas product was detected at the cathodic container, which proves that high-purity H₂ was produced during electrolysis and the AEM prevented O2 migration from the anode.

Figure 4e shows that the electrode potential increases slightly with time. Still, this increment is only close to 8% of the initial potential, and it is associated to the OER occurring because of the depletion of the sulfite ion in the anode. Furthermore, a constant pH gradient is clearly seen between both sections, which is attributed to a constant flow of OHions from the cathode to the anode. 13 Moreover, a constant ionic migration demonstrates an adequate stability of the membrane. The pH at the cathode fluctuated between 12 and 11.5, while at the anode, it was stable with a value around 8.5. These values of pH are advantageous for both electrodes, and severe basic conditions were effectively avoided. Sulfite electrooxidation is promoted above pH 8, while ammonia migration to the gas phase is decreased below pH 9.21 Moreover, stable nickel oxides/hydroxides are expected in the pH range between 8.5 and 12.6 according to the Pourbaix diagram, which should decrease the dissolution rates of NF.³⁹ Finally. the sulfite concentration decreased with time, until it stabilized below 5 mM after 18 h. This validates the decrease of FEs and oxidation rates as the sulfite ion is depleted with time because of batch electrolysis.

Metal dissolution is caused by different factors such as electrode potential, pH, electrolyte composition, and surface oxidation/reduction, among others. 40-42 This unfavorable process may lead to a decrease in catalyst loading, which is detrimental to the performance and reaction rates with time. 42 Figure 4f shows the concentrations of Pd, S, and Ni in different electrolytes with time. We used the flow cell coupled to TXRF as a powerful approach to carefully measure the presence of elements in the electrolytes and assess electrode stability. For Pd and Ni, it is evident that some dissolution occurs at the anode. However, note that the metal concentration almost stabilizes after ca. 18 h. This implies that the dissolution rates decrease with time and are controlled. Metal dissolution in the Pd/C/NF electrode (Figure S14) was similar to that in Pd/ NF, with a final Pd concentration close to 0.125 ± 0.087 mg· L⁻¹. Because both electrodes exhibited different ECSA trends, this suggests that Pd dissolution occurred until stabilization in the electrolyte and it was not related to the number of exposed Pd sites on each electrode. Moreover, the Ni-to-Pd ratio in the electrolyte was around 20:1, suggesting that the NF substrate was also etched until stabilization. Finally, the Ni concentration in the catholyte was low (<1 mg·L⁻¹) and stable, suggesting that the reductive potentials kept Ni as metallic.

Sulfur detection at the cathode was used to estimate the sulfur diffusion through the membrane, a serious problem in SO₂ electrolyzers which reduces the efficiency at the cathode as S(IV) can be reduced to elemental sulfur or metallic sulfides. 43,44 From Figure 4f, note that the sulfur concentration at the cathode increases with time, which is attributed to the high concentration of sulfur at the anode and the high pressure drop due to porous NF, which may displace sulfite/sulfate ions through the AEM into the cathode.²⁷ Therefore, the effects on the cathode were evaluated. Figure 5 displays a series of electrochemical measurements to evaluate the activity and stability of the NiO/Ni/NF electrode. From Figure 5a, we observe that i-V curves before and after electrolysis exhibit a similar HER behavior. The overpotential at 10 mA·cm⁻² is ~90 mV at the beginning and shifts near 20 mV. A similar trend can be seen from the chronopotentiometry curve (Figure 5b). Finally, ECSA fluctuation with time is subtle (Figure 5c), and a noticeable trend is not as evident as in Pd/NF (Figure 4c). This suggests that the electrode was stable and no serious poisoning due to S(IV) diffusion occurred. Still, post-analysis of the electrodes was performed to confirm these results.





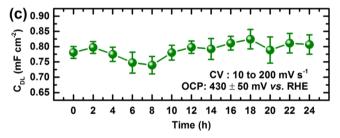


Figure 5. Electrochemical results for the NiO/Ni/NF cathode: (a) i-V curves before and after electrolysis, (b) chronopotentiometric curve, and (c) double-layer capacitance with time.

Electrode Postanalysis. Figure \$16 shows the morphology, EDX, and XRD comparisons before and after electrolysis using the Pd/NF anode. The cross section reveals a thick surface film (Figure S16a) mainly composed of Pd according to EDX (Figure S17). Dendrites exhibited a compressed, cauliflower-like structure as if sharp edges from the fresh electrode were removed (Figure S16b). This can be seen in more detail in additional SEM images (Figure S18). Overall, Pd deposits became rounded (Figure S16c), and higher magnifications (500 nm) revealed solid deposits (Figure S18) which are different from those in fresh Pd/NF (Figure S4). Also, Pd characteristic peaks from XRD were broadened (Figure S16f), which possibly indicates that the mean size of Pd crystallites was reduced. 45 Elemental mapping of the NF branches confirm that Pd was still dispersed uniformly throughout the material; however, the oxygen content was reduced (Figures S16d and S19). This is evident from EDX spectra, as the oxygen peak decreases (Figure S16e). This indicates that surface oxides were removed from the surface during electrolysis. Finally, note that no sulfur was detected, which suggests that the anode was not poisoned by the dithionate ion, a common anion which strongly adsorbs onto

noble metals during sulfite electro-oxidation.^{21,46} This further confirms the superior features of the Pd/NF electrode.

The results suggest that Pd electrodissolution occurred and surface oxides were removed until a stable condition was achieved: (i) the ECSA increased with time until it was constant; (ii) the Pd concentration in the electrolyte increased until it was stabilized according to TXRF; (iii) oxygen on the surface from EDX was decreased; and (iv) morphological changes suggest that sharp edges and spikes in Pd microstructures were removed. According to the literature, the anodic dissolution of Pd causes surface morphology changes, and oxide growth/reduction leads to an increase of surface defects. 40 Furthermore, Pd oxide transitions (e.g., from PdO to PdO₂) trigger dissolution in alkaline media.⁴⁷ Nevertheless. note that the Pd/NF anode still exhibited a high surface area, Pd was well dispersed after electrolysis, and dissolution was not severe. In fact, it has been found that Pd exhibits lower anodic dissolution rates than most noble metals in alkaline media.⁴ This is attributed to the stabilization provided by adsorbed OH^{-.40} Therefore, it is likely that initial Pd surface oxides were etched until fresh metallic Pd was exposed. In contrast, anodic Ni dissolution is attributed to pH because soluble Ni²⁺ is expected below pH ~ 8.3 . Therefore, pH control is crucial. Still, it seems that only small amounts of exposed Ni were dissolved, as shown by EDX (Figure 5e) and a stable Ni concentration after 20 h (Figure 3f).

SEM, EDX, and XRD measurements of the NiO/Ni/NF electrode are shown in Figure S20. The morphology remained unchanged (Figure S21): a rough surface with nanostructures is evident. This agrees with the constant ECSA trend (Figure 4c). From XRD, we observe that characteristic peaks of metallic Ni remained unchanged. However, elemental mappings and EDX spectra revealed that the oxygen and sulfur contents increased after electrolysis (Figure S21b,c and Table S2). We performed XPS analysis to elucidate the chemical states of Ni, O, and S (Figure S22). The surface was mainly composed of Ni metal, NiO, and Ni(OH)2. The presence of reduced Ni is discussed in the Supporting Information. Peaks typical of a metal-sulfur bond in the range of 160.5-163.8 eV were not seen, which suggests that SO₄²⁻ ions arising from sulfur diffusion were not reduced and only adsorption occurs. 48-50 This further confirms the robustness of the NiO/Ni/NF electrode; the efficiency was not decreased because of sulfur reduction, and the HER is the main reaction, which agrees with FEs.

Performance, Energy, and Environmental Implications. The performance metrics and relevant operational parameters are shown in Table 1. Our approach exhibited reasonable performance at 10 mA·cm⁻² with high SO₃²⁻ conversions (>90%) and a constant H₂ production rate (~ 0.25 mmol h⁻¹ cm⁻²). Considering the energy inputs and outputs, a rough energy efficiency can be estimated. One electrolysis unit requires about 0.11 kW·h·mol⁻¹ H₂ produced, while the energy output as hydrogen can be set as 0.08 kW·h· mol⁻¹ (see the Supporting Information).⁵¹ Thus, the energy efficiency of the electrolyzer is about 73%. When pumping is considered, the efficiency drops drastically (<5%). The use of a membrane also contributes to a higher cell voltage (~2.0 V). Note however that these features improve the overall performance: AEM-separated streams allow a safe way to collect gas and liquid products, 52 while forced convection and recirculation enhance bubble removal, ion migration, and mass transfer. 27,53,54 Future studies should be aimed to reduce

Table 1. Performance Metrics for the ${\rm SO_3}^{2-}$ Electrolysis Approach Proposed Here

H_2 productivity (mmol·cm ⁻² ·h ⁻¹)	0.252 ± 0.007^{c}
H ₂ productivity (mmol·cm ⁻³ ·h ⁻¹)	0.015 ± 0.001^{c}
H ₂ purity (%)	$32.0 \pm 1.2^{a,c}$
H ₂ average FE (%)	91.3 ± 2.5^{c}
initial SO ₃ ²⁻ oxidation rate (mmol·cm ⁻² ·h ⁻¹)	0.276 ± 0.014^{b}
initial SO_3^{2-} oxidation rate (mmol·cm ⁻³ ·h ⁻¹)	0.017 ± 0.001^{b}
final ${\rm SO_3}^{2-}$ concentration (mM)	1.96 ± 0.79^{b}
SO ₃ ²⁻ conversion (%)	96.8 ± 1.6^{b}
cell voltage (V)	2.03 ± 0.12
energy yield (mol·kW·h ⁻¹)	9.19 ± 0.58
energy consumption (kW·h·mol ⁻¹)	0.11 ± 0.01

 $^a Remaining$ gases were Ar and $H_2 O.$ No other gas was produced at the cathode. $^b Value$ from averaging different electrolysis tests. $^c Value$ from averaging measurements for 20 h.

energy consumption, and energy assessments should consider the entire FGD process because pumping is also required for fluid transportation.

Most of the approaches in the literature only oxidize sulfite and lack the profitable by-products proposed herein. Studies focused only on SO₂ removal reported higher conversions. An ozonation method assisted by Mn²⁺ achieved almost a 99% conversion,⁶ while gas/solid oxidation on MnO₂ reached nearly 100%. 55 However, a fair comparison is difficult because configurations were not strictly the same. Furthermore, some electrochemical systems with simultaneous SO_3^{2-} oxidation and H₂ production have been reported. The photo-electrochemical system reported by Han et al., which relied on Pt (cathode) and Mo-doped BiVO₄ (photoanode), reported similar conversions (~97%) and FEs (94%) but lower H_2 production rates (<60.26 μ mol·cm⁻²·h⁻¹) at 3.42 mA·cm⁻². ¹⁴ Huang reported a H₂ production of 3.63 mmol·cm⁻²·h⁻¹ with Pt/C electrodes (0.5 mg·cm⁻²). However, large current densities (~180 mA·cm⁻²) and a concentrated ammonium sulfite electrolyte (2 M) were required.²³ A method reported by Yang et al., which allowed the recovery of H₂SO₄, NaOH, and H_2 in a parallel-plate reactor, exhibited a lower FE (\sim 87%) and a higher energy consumption ($\sim 0.2 \text{ kW} \cdot \text{h} \cdot \text{mol}^{-1} \text{ H}_2$) when operating at a low current density (5.92 mA·cm⁻²) and a higher cell voltage (3.6 V). Finally, the use of a flow cell and forced convection greatly improved H2 production from our previous approach (0.05 mmol·cm⁻²·h⁻¹).¹³

Besides performance, other important technical aspects should be highlighted. First, the use of a 3D-printed electrolyzer proves that 3D printing may accelerate electrolysis with a reduction in costs and weight. 56 Pilot plant-scale electrolyzers with stacked units using 3D-printed components should be assessed because of the unique advantages of 3D printing for scale-up.²⁷ Additionally, coupling the system to high-efficiency triple-junction solar cells is highly recommended as it has been previously used to increase solar-tohydrogen efficiencies in polymer electrolyte membrane (PEM) electrolyzers. 57,58 Moreover, note that extra purification steps are required, especially when flue gas contains other chemicals, such as heavy metals. For instance, filtration using membranes or molecular sieves can be used. Furthermore, hydrocyclones and centrifuges coupled to recirculation steps are required to concentrate and purify resultant product streams and subsequently generate solid ammonium sulfate. These purification technologies are commercially available.²⁰

Furthermore, this approach carries important environmental and sustainability implications. First, note that the atom economy of the process is greatly improved. That is, more atoms involved in the process are included in the final products, i.e., ammonium sulfate and hydrogen. Typical FGD is mostly focused on SO₂ removal from flue gas to satisfy environmental regulations. However, by making this process more profitable, environmental treatment of flue gas may become a ubiquitous process. Also, ammonia-based FGD requires fewer and easier steps than analogous processes such as limestone-based FGD, which requires more complex unit operations after the oxidation step. ²⁰ Additionally, by using an electrochemical step and aqueous electrolytes, the use of homogeneous catalysts, solvents, ionic liquids, and ozone for oxidation is avoided. Still, some issues must be effectively solved to enhance the approach. In particular, long-term electrode stability and metal dissolution must be carefully addressed because Pd and Ni toxicity may become an issue, especially if the oxidized solution is discharged in water after FGD.⁵⁹ Of course, microfiltration systems could be employed to capture dissolved metals for reuse.⁶⁰ Other aspects such as the use of greener materials for 3D printing, research on earthabundant electrocatalysts for sulfite electro-oxidation and HER, AEM development, and coupling to renewable energy sources should be assessed to increase the sustainability of the approach. Ultimately, this may lead to profitable, efficient, and environmentally friendly SO₂ exploitation technologies capable of being integrated into coal-fired power plants in the future.

ASSOCIATED CONTENT

Supporting Information

The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/acs.est.0c04190.

Detailed experimental section, additional electrochemical and physicochemical characterization results before and after experiments, electrochemical testing setup, oxygen evolution plots with time, and additional post-analysis results (PDF)

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Notes

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ABBREVIATIONS

NF Ni foam Pd/C Pd on carbon

Pd/NF Pd electrodeposited onto Ni foam Pd/C/NF Pd/C spray-coated onto Ni foam

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