

Article MOSS: Multi-modal Best Subset Modeling in Smart Manufacturing

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Smart manufacturing, which integrates a multi-sensing system with physical Abstract: 1 manufacturing processes, has been widely adopted in the industry to support online and real-time 2 decision making to improve manufacturing quality. A Multi-sensing system for each specific 3 manufacturing process can efficiently collect the *in situ* process variables from different sensor Δ modalities to reflect the process variations in real-time. However, in practice, we usually do not 5 have enough budget to equip too many sensors in each manufacturing process due to the cost 6 consideration. Moreover, it is also important to better interpret the relationship between the sensing modalities and the quality variables based on the model. Therefore, it is necessary to model the 8 quality-process relationship by selecting the most relevant sensor modalities with the specific quality 9 measurement from the multi-modal sensing system in smart manufacturing. In this research, we 10 adopted the concept of best subset variable selection and proposed a new model called Multi-mOdal 11 beSt Subset modeling (MOSS). The proposed MOSS can effectively select the important sensor 12 modalities and improve the modeling accuracy in quality-process modeling via functional norms 13 that characterize the overall effects of individual modalities. The significance of sensor modalities can 14 be used to determine the sensor placement strategy in smart manufacturing. The selected modalities 15 can better interpret the quality-process model by identifying the most correlated root cause of quality 16 variations. The merits of the proposed model are illustrated by both simulations and a real case study in an Additive Manufacturing (i.e., fused deposition modeling) process. 18

Keywords: Data fusion; fused deposition modeling; multi-modal sensing; quality modeling; smart
 manufacturing

21 1. Introduction

Smart manufacturing integrates multi-modal sensing systems and computing resources (e.g., 22 Fog computing and Cloud computing) to support efficient real-time quality modeling, monitoring, 23 diagnosis, and control in manufacturing [1-4]. Specifically, one modality in this paper is defined 24 as a group of features extracted from the sensing signal that measures the same kind of physical 25 quantity from the same place in the manufacturing process [5]. Therefore, based on the multi-modal 26 sensing systems, different modalities of relevant variables that can reflect the status of manufacturing 27 processes are collected to effectively model the quality-process relationship in smart manufacturing [6, 28 7]. However, how to effectively design and achieve the multi-modal sensing system in smart 29 manufacturing is still an open question [8]. For example, one can equip sensors and collect 30 the corresponding process variables as many as possible to accurately model the quality-process 31 relationship in the manufacturing process. But this approach is not cost-effective, because some 32 modalities might be redundant or comparable with each other. On the other hand, with a multi-modal 33 sensing system, it is important to identify the most relevant modalities in a quality-process model to 34

effectively interpret the potential root cause of the quality variation [9]. Therefore, it is critical to find a
 quality-process model strategy that can effectively select the best subset from the multi-modal sensing

data, and rank the relevance for each modality toward the modeled quality variable. 37 Take the fused deposition modeling (FDM), which is an extruder based additive manufacturing 38 (AM) process, as an example [10]. As a promising advanced manufacturing process, FDM can efficiently 39 fabricate personalized products with a high degree of geometric complexity [11–13]. Therefore, FDM 40 has been employed in many significant applications, such as aerospace automobile and healthcare 41 field [14,15]. However, most of these applications are not yet widely deployed in practice due to the 42 quality variation of products, such as geometric deviations caused by process variations during the 43 fabrication [16,17]. Because the fabrication mechanism of the FDM process is complex, the potential 11 root cause for the geometric deviation is also diverse. For example, abnormal events during the 45 fabrication process such as irregular filament feeding, extruder vibration, and extruder temperature 46 variation might directly lead to a geometric deviation of the product. As shown in Fig. 1, in order to 47 comprehensively study the influence of these events on geometric deviations, a smart manufacturing 48 paradigm of the FDM process with a multi-modal sensing system is proposed. The data collected 49 from these sensor modalities can directly or indirectly reflect the characteristics and variations of the 50 fabrication in a FDM process. However, this design for the multi-modal sensing system might not be 51 the most cost-effective. For example, the data collected from the infrared sensor and the thermocouple 52 on the extruder might be correlated since both of them measure the thermal distribution near the 53 melting pool area [12]. In the literature, there has been a series of quality-process models to study 54 the influence from different sensor modalities on the quality variable [10,12,18,19]. However, most of 55 the existing quality-process models cannot work for nonlinear model components, and thus cannot 56 identify the significant modalities to obtain a cost-effective (e.g., without redundant or comparable 57 modalities) multi-modal sensing system. Then the budget limitation for a multi-modal sensing system might restrict the deployment of these methods in practice. Moreover, the interpretability of these 59 quality-process models might be questionable, without identifying the significant sensing modalities 60 and ranking their contributions toward a specific quality variable in a FDM process. Therefore, it is 61 important to quantify the relevance of each sensor modality toward the specific quality response in 62 quality modeling. In this way, we can provide a cost-effective multi-modal sensing system to the FDM 63 process, and also accurately pinpoint the potential root cause of a defect based on the sensor modality

selection result to reduce or avoid the product defect in the future [10].

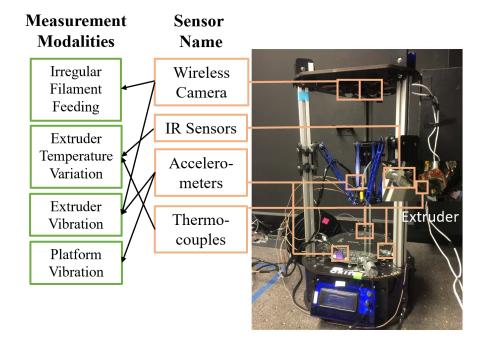


Figure 1. A Delta FDM Printer with a Multi-modal Sensing System

The objective of this research is to propose a model that can effectively select the real-time sensing 66 modalities in quality modeling to support the cost-effective multi-modal sensing system design in 67 smart manufacturing. To tackle the knowledge gap, we propose a new modeling method called 68 Multi-mOdal beSt Subset modeling (MOSS) that adopts the best subset selection idea from the best 69 subset regression [20]. The proposed MOSS can effectively select the best subset from the original 70 dataset via a two-level variable selection (i.e., among sensor modalities and within each modality) 71 effort. Specifically, two regularization norms are embedded in the quality-process model to realize 72 this effort. The first one is a functional norm that can effectively identify the relevance of each sensor 73 modality toward the quality response in model estimation. Smoothing splines framework [21] is 74 used to represent nonlinear model components, and quantify the contribution of each modality in the 75 proposed MOSS. By comparing the magnitudes of functional norms among modalities estimated from 76 the model, the rank of relevance toward the quality response can be accurately identified. The second 77 norm is an *l*-1 norm that encourages the sparsity of model coefficients corresponding to features within 78 each data modality. By comparing with the existing methods [22–26], the proposed MOSS can realize 79 the two-level variable selection simultaneously with both linear and nonlinear model components, 80 and further select the sensor modalities in smart manufacturing. To evaluate the quality prediction 81 performance and the variable selection accuracy for the proposed MOSS, both simulations and a 82 real case study are implemented. The results show the proposed MOSS can effectively select the 83 significant modalities with an accurate variable selection accuracy via the smooth spline framework 84 compared with three benchmark methods (i.e., Lasso regression [22], group Lasso [23], and hierarchical 85 Lasso [24]) 86 The rest of the paper is organized as follows. Section 2 summarizes the state-of-the-art of quality 87 improvement and modeling for FDM processes and multi-modal modeling methods. Section 3 88

⁸⁹ introduces the proposed best subset model in detail. Section 4 validates the prediction performance

⁹⁰ and the variable selection accuracy of the proposed method via a simulation study. Section 5 employs

a real case study on the FDM process to model multiple geometric quality measurements via the

proposed MOSS. Lastly, Section 6 concludes and discusses future work.

93 2. Related works

In this section, the state-of-the-art research on quality improvement and modeling for the AM 94 process is reviewed. First, to improve the product quality from the AM process, the optimized process 95 recipe (i.e., the combination of process setting variables) has been studied. For example, Fordan et 96 al. identified how the important setting variables (e.g., layer thickness) can influence the mechanical 97 property of the AM products through a design of experiment study [27]. Moreover, for the geometric 98 deviation of the product, Sood et al. employed the gray Taguchi method to study the influence of 99 five setting variables (i.e., part orientation, deposition width, layer thickness, air gap, and deposition 100 angle) on the product geometric deviation [28]. Similarly, Zhang and Peng applied the Taguchi method 101 which is combined with a fuzzy comprehensive evaluation to established empirical relations between 102 the setting variables and the geometric deviation of product [29]. Nancharaiah et al. applied an 103 ANOVA method to investigate the significant setting variables in FDM processes toward the geometric 104 deviation [30]. However, the aforementioned works mainly concentrate on the run-to-run study to 105 optimize the process recipe and identify the significant process setting variables in the AM process, 106 instead of modeling the relationship between the product quality with the process variables from the sensing system which can reflect the real-time fabrication variation. 108

To model the *in situ* sensing data with the product in an AM process, many data-driven models 109 have been proposed in the literature. For instance, Rao et al. presented an advanced Bayesian 110 nonparametric analysis method for *in situ* sensing data to identified process failures and the types 111 of failures in a FDM process in real-time [10]. Sun et al. proposed a functional quantitative and qualitative model to predict two types of quality responses via offline setting variables and in situ 113 process variables [12]. Dinwiddie et al. proposed a monitor system based on infrared cameras to 114 monitor the temperature distribution of the extrusion process in a FDM process [31]. Tlegenov et 115 al. presented a nozzle clogging monitoring system based on the *in situ* vibration data through a 116 physics-based dynamic model for a FDM process [32]. Li et al. proposed a data-driven method for in situ monitoring and process diagnosis based on the vibration sensors. The least-squares support 118 vector machine (LS-SVM) method was employed to identify the filament clogging event in real-time. 119 Liu et al. proposed a data-driven model to predict the product surface roughness based on the features 120 generated from thermocouples, infrared temperature sensors, and accelerometers [33]. Kousiatza 121 and Karalekas illustrated a geometric deviation monitoring system based on the fiber Bragg grating 122 sensors and thermocouples. The *in situ* data collected from the sensors is employed to generate the 123 temperature distribution and product profile based on a data-driven model [34]. Similarly, Fang et 124 al. proposed a strain variation monitoring system based on the embedded FBG sensors inside the 125 product [35]. Yang et al. developed an acoustic emission sensor based filament breakage monitoring 126 system. The summary statistics of the *in situ* acoustic emission signal was employed as the monitor 127 index [36]. However, the aforementioned methods typically only focus on quality-process modeling 128 instead of selecting the relevance of sensing modality. Thus, they may not provide insights on the 129 contribution of each sensing modality toward the quality variable. Therefore, the existed method 130 might be not sufficient to guide the multi-modal sensing system design in smart manufacturing. 131

On the other hand, there are many modality and variable selection modeling methods that 132 have been proposed in the literature [37]. For example, Tibshirani proposed the Lasso penalty to 133 employ the variable selection effort in an ordinary regression model by constraining the sum of 134 the absolute value of the model coefficients being less than a constant [22]. To extend the variable 135 selection efforts for the different modality of predictors, the group Lasso was proposed [38]. The group 136 Lasso proposed a group-wise penalty to encourage the group (i.e., data modality) sparsity in model 137 estimation. To effectively implement the modality selection and the variable selection within each 138 modality simultaneously, Huang et al. proposed the group bridge method to simultaneously select the important modality and also the feature within each modality at the same time via a specially designed 140 group bridge penalty [39]. However, the proposed group bridge penalty is not always differentiable 141 and tends to be inconsistent for feature selection [40]. Zhou and Zhu proposed the hierarchical Lasso 142

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approach to effectively remove insignificant modality and implement the variable selection within 143 each modality by penalizing the coefficients using two levels of l-1 penalty [24]. Paynabar et al. [25] 144 and Sun et al. [26] proposed a hierarchical nonnegative garrote method to achieve these two-level 145 variable selection efforts in linear regression models. Fan and Li developed the smoothly clipped 146 absolute deviation (SCAD) penalty to effectively select variables and estimate linear model coefficients 147 simultaneously [41]. However, the aforementioned methods mainly focus on selecting linear functional 148 model components, and cannot deal with the nonlinear model components. For the nonlinear model 149 components, Lin and Zhang proposed the component Selection and Smoothing Operator (COSSO) 150 method to regularize the data modality as the summation of component norms based on the smooth 151 spline method [42]. Ravikumar et al. proposed the sparse additive model (SpAM) to regularize the 152 data modality based on an empirical functional norm via a non-parametric smoother [43]. However, 153 these methods do not involve the variable selection effort within each modality among the nonlinear 154 model components. Therefore, it is important to propose a model that can handle the nonlinear model 155 components with the capability that can simultaneously select both the significant modalities and the 156 variables within each modality in model estimation. 157

158 3. Methodology

In order to clarify the scope of this study, we assume that an additive model structure is sufficient to model the quality-process relationship. This assumption is validated in Appendix.A1. Moreover, quality measurement of Product *i* is treated as the quality variable in modeling, denoted as y_i and i = 1, ..., n. The model can be expressed as:

$$y_i = \alpha + \sum_{r=1}^d f_r \quad \boldsymbol{x}_{ir}^{\mathrm{T}} \boldsymbol{\beta}_r \quad + \boldsymbol{\epsilon}_{it},$$
(1)

where α is an unknown intercept, f_r s are unknown smooth functions, $x_{ir} = (x_{ir1}, \ldots, x_{irpr})^T$ is the feature vector generated from modality r for product i with p_r number of features, and $\beta_r = (\beta_{r1}, \ldots, \beta_{rpr})^T$ is the vector of weight coefficients for the predictor vector x_{ir} . It is worth to mention that the data can be aligned based on the dynamic time warping [44]. To guarantee that model Eq.(1) is estimable, in this paper, we shall use the constraints $f_r = 0, r = 1, \ldots, d$ [45]. Therefore the quality-process relationship in Eq.(1) can be expressed as an additive model where each modality is represented by an additive component function f_r . This model structure can help better interpret the contribution of each modality component [9]. Moreover, to estimate component function f_r , f_r is formulated in a reproducing kernel Hilbert space (RKHS) framework. Specifically, the whole mean response function ($\alpha + \sum_{r=1}^d f_r$) in Eq.(1) is assumed to reside in an RKHS \mathcal{F} of functions. The space has a tensor sum decomposition $\mathcal{F} = 1$ \mathcal{F}_1 with $\mathcal{F}_1 = \int_{r=1}^d \mathcal{F}^r$, where $\mathcal{F}^1, \ldots, \mathcal{F}^d$ are d orthogonal subspaces of \mathcal{F} such that f_r \mathcal{F}^r to indicate d modalities. To estimate the model parameters (f_r, α, β_r), a penalized least square optimization formulation is proposed as:

$$\underset{f_r,\boldsymbol{\beta}_r}{\operatorname{argmin}}\sum_{i} \quad y_i - \alpha - \sum_{r=1}^{d} f_r \quad \boldsymbol{x}_{ir}^{\mathrm{T}}\boldsymbol{\beta}_r \quad \overset{2}{} + \lambda_1 \sum_{r} \quad \boldsymbol{\beta}_{r-1} + \lambda_2 \sum_{r=1}^{d} \quad f_{r-2}, \quad (2)$$

where the first term $\sum_{i} y_{i} - \alpha - \sum_{r=1}^{d} f_{r} x_{ir}^{T} \beta_{r}^{2}$ represents the least-square loss for model estimation; $\sum_{r} \beta_{r-1} = \sum_{r} \sum_{j=1}^{p_{r}} \beta_{rj}$ is the *l*-1 regularization term which implements the variable selection effort within each modality [22]; λ_{1} is the tuning parameter to control the sparsity of the β_{r} ; $\sum_{r=1}^{d} f_{r-2} = \sum_{r=1}^{d} f_{r}^{2}$ is the *L*-2 functional norm regularization to determine the sparsity among data modalities [39]. Therefore, the proposed MOSS can effectively and simultaneously select the significant sensing modalities for nonlinear function components, and also identify the important predictors within each modality. To effectively estimate the functional norm for each modality, modality а

¹⁶⁶ inputs $x_{ir}^{T}\beta_{r}$, i = 1, ..., n, are all standardized to [0, 1] within each modality. Therefore, by comparing ¹⁶⁷ the magnitude of functional norms, the best subset of modalities toward the quality response can be ¹⁶⁸ effectively identified. It is worth to mention that, once the significant modalities and the important ¹⁶⁹ features within each modality are identified, the raw sensor features can be used to interpret the root ¹⁷⁰ cause of the product defects. Moreover, by choosing the different tuning parameter λ_2 , the number of ¹⁷¹ selected modalities in the best subset can be controlled.

To estimate the model parameters in Eq.(2), a block updating algorithm is developed to break down the proposed optimization problem into two simpler optimization problems as follow:

$$\underset{\alpha,f_r}{\operatorname{argmin}}\sum_{i} y_i - \alpha - \sum_{r=1}^{d} f_r \quad \boldsymbol{x}_{ir}^{\mathrm{T}}\boldsymbol{\beta}_r \quad \overset{2}{+} \lambda_2 \sum_{r=1}^{d} f_{r-2}, \qquad (3)$$

and

$$\operatorname{argmin}_{\boldsymbol{\beta}_{r}} \sum_{i} y_{i} - \alpha - \sum_{r=1}^{d} f_{r} \mathbf{x}_{ir}^{\mathrm{T}} \boldsymbol{\beta}_{r}^{2} + \lambda_{1} \sum_{r} \boldsymbol{\beta}_{r-1}.$$
(4)

A direct optimization of Eq.(3) is difficult due to the functional norm regularization term. Inspired by the COmponent Selection and Smoothing Operator (COSSO) [42], an equivalent formulation of Eq.(3) is proposed as follow:

$$\operatorname{argmin}_{\alpha, f_r, \theta_r} \sum_{i} y_i - \alpha - \sum_{r=1}^d f_r \quad \boldsymbol{x}_{ir}^{\mathrm{T}} \boldsymbol{\beta}_r \overset{2}{\longrightarrow} + \lambda_0 \sum_{r=1}^d \theta_r^{-1} \quad f_r \stackrel{2}{\xrightarrow{}}_2 + \lambda_2 \sum_{r=1}^d \theta_r, \tag{5}$$

where λ_0 is a tuning constant and $\theta_r \ge 0$ is the constrained weight coefficients for each sensor modality. By the representer theorem for smooth splines [21], the solution of f_r has the form $f_r(x) = \sum_{i=1}^{n} c_i \theta_r R_r \ \mathbf{x}_{ir}^{\mathrm{T}} \boldsymbol{\beta}_r, x$, where c_i s are unknown coefficients and R_r is the reproducing kernel function of \mathcal{F}^r . Let R_r^* be the $n \times n$ matrix with the (i, j)-th element being $R_r((\mathbf{x}_{ir}^{\mathrm{T}} \boldsymbol{\beta}_r), (\mathbf{x}_{jr}^{\mathrm{T}} \boldsymbol{\beta}_r)), i = 1, ..., n$, j = 1, ..., n. Define $R_{\theta} = \sum_{r=1}^{d} \theta_r R_r$ and the matrix $R_{\theta}^* = \sum_{r=1}^{d} \theta_r R_r^*$. For fixed θ_r s, we can find the estimates of the intercept α and the coefficient vector $\mathbf{c} = (c_1, ..., c_n)^{\mathrm{T}}$ by

$$\underset{\alpha,c}{\operatorname{argmin}} \left(\boldsymbol{y} - \alpha \boldsymbol{1}_n - R_{\theta}^* \boldsymbol{c} \right)^{\mathrm{T}} \left(\boldsymbol{y} - \alpha \boldsymbol{1}_n - R_{\theta}^* \boldsymbol{c} \right) + n \lambda_0 \boldsymbol{c}^{\mathrm{T}} R_{\theta}^* \boldsymbol{c}, \tag{6}$$

which is a standard smoothing spline problem [21] and can be solved, including the tuning of λ_0 , by standard smoothing splines software [45]. By fixing α and c, defining $\mathbf{g}_r = R_r^* c$ and letting G be the $n \times r$ matrix with the *r*-th column being \mathbf{g}_r , we can efficiently solve $\boldsymbol{\theta} = (\theta_1, ..., \theta_d)^T$ by

$$\underset{\boldsymbol{\theta}}{\operatorname{argmin}} \left(\boldsymbol{z} - \boldsymbol{G} \boldsymbol{\theta} \right)^{\mathrm{T}} \left(\boldsymbol{z} - \boldsymbol{G} \boldsymbol{\theta} \right) + n\lambda_2 \sum_{r=1}^{d} \theta_r, \quad \text{subject to } \theta_r \ge 0, r = 1, \dots, d, \tag{7}$$

where $\mathbf{z} = \mathbf{y} - (1/2)n\lambda_0\mathbf{c} - \alpha \mathbf{1}_n$. Therefore, by iterating Eq.(6) and Eq.(7), the intercept α and the functional components f_r can be estimated via the penalized constrained least squares fitting framework in [46,47].

¹⁷⁵ Next, to estimate the Eq.(4), we can fix α and f_r and the problem will be reduced to a linear ¹⁷⁶ regression model with a Lasso penalty. It can be efficiently solved by the coordinate descent algorithm ¹⁷⁷ as shown in [48]. Therefore, an alternately updating strategy is proposed to find the solution of ¹⁷⁸ the proposed model as shown in Algorithm 1. To select the optimal tuning parameters, the 5-fold ¹⁷⁹ cross-validation is employed [22,45]. The selection procedures are shown in Algorithm 1. The root ¹⁸⁰ mean square errors (RMSEs) from the cross-validation is used to select *lambda*₁ and *lambda*₂.

Algorithm 1 Block Updating Algorithm

Input: data $(x_{i1}, x_{i2}, ..., x_{id}, y_i), i = 1, ..., n$; where $x_{ir} = (x_{ir1}, ..., x_{irp_r})^T$ is the *r*-th modality for product *i* with p_r number of features **Initialization:** $\theta = \mathbf{1}_d$; λ_0 : solving the smoothing spline problem as [45], and tuning λ_0 according to cross-validation; β_r : initialized via ridge regression, r = 1, ..., d.

Repeat

Select the tuning parameter λ_2 based on cross-validation **Repeat until** α , *c*, and θ coverage:

Step 1: argmin $\boldsymbol{y} - \alpha \mathbf{1}_n - R_{\theta}^* \boldsymbol{c}^{\mathrm{T}} \boldsymbol{y} - \alpha \mathbf{1}_n - R_{\theta}^* \boldsymbol{c} + n\lambda_0 \boldsymbol{c}^{\mathrm{T}} R_{\theta}^* \boldsymbol{c}$ Step 2: argmin $(\boldsymbol{z} - \boldsymbol{G}\boldsymbol{\theta})^{\mathrm{T}} (\boldsymbol{z} - \boldsymbol{G}\boldsymbol{\theta}) + n\lambda_2 \sum_{r=1}^{d} \theta_r$, subject to $\theta_r \ge 0, r = 1, \dots, d$.

Select the tuning parameter λ_1 based on cross-validation **Repeat until** β_r coverage:

Step 1:argmin
$$\sum_{i} y_i - \alpha - \sum_{r=1}^{d} f_r x_{ir}^{T} \beta_r^{2} + \lambda_1 \sum_{r} \beta_{r-1}$$

181 4. Simulation

182 4.1. Simulation Setting

The objective of this simulation study is to evaluate the statistical performance of the proposed 183 model compared with other benchmark models. In total, there are eight different simulation settings 184 that are summarized in Table 1. Specifically, the sample size for each simulation case represents 185 how many samples are generated. In each sample, the multi-modal data and the corresponding 186 model response are generated based on a pre-defined model structure. The Decibels signal-to-noise 187 ratio (SNR) is defined as $SNR_{dB} = 10 \log_{10} \frac{M_{signal}}{M_{noise}}$, where M_{signal} is the mean of signal power for 188 multi-modality data, and M_{noise} is the power for the noise. The sparsity represents the ratio between 189 the total significant variables and the total number of variables in the model. Finally, we chooses linear 190 and nonlinear structures to test the robustness of the proposed methods to model a nonlinear system. 191

Case No.	Sample Size	Sparsity Signal-to-noise Ratio (db) (Total Signi cant Variables Model in All Modalities)				
1	100	1	0.1 (6)	Linear		
2	100	0.6	0.25 (16)	Nonlinear		
3	100	1	0.1 (6)	Nonlinear		
4	100	0.6	0.25 (16)	Linear		
5	300	1	0.1 (6)	Nonlinear		
6	300	0.6	0.25 (16)	Linear		
7	300	1	0.1 (6)	Linear		
8	300	0.6	0.25 (16)	Nonlinear		

Table 1. Simulation Settings

To explicate the advantages of the proposed method, in each simulation, four modalities of data are generated as the raw signals. The summary of these four data modalities and the number of their corresponding features are shown in Table.2. Specifically, Modality 1 and Modality 2 are time series signals generated respectively from AR(2) model with $\phi_1 = [0.9, -0.2]^T$ and AR(3) model with $\phi_2 = [-0.7, 0.3, 0.1]^T$ [49]. Moreover, the *i.i.d* noise for both AR models is generated from N(0,0.5). In practice, the features generated from the raw signal are widely used in modeling to reduce the data dimension and decrease the computation intensity [26]. Therefore, to effectively generate the

signal features from Modality 1 and Modality 2, the discrete wavelet analysis is employed because 199 it can effectively extract the features from both time and frequency domain [50]. Moreover, x_1 and 200 x_2 are the features that are the Level1 and Level2 db4 detailed wavelet coefficients from Modality 1. 201 Similarly, x₃ and x₄ are Level1 and Level2 db4 detailed wavelet coefficients extracted from Modality 202 2. Moreover, since there might be a 2-D image signal in the smart manufacturing system, such as a 203 thermal distribution image, we also generate the 2-D image as Modality 3 in each sample. Specifically, 204 the 2-D image is generated from a multivariate normal distribution, and the covariance function 205 defined by inverse exponential squared Euclidean distance: $\Sigma(z, z) = \exp(-z - z^2)$ [51]. *z* is an 206 arithmetic sequence from 0 to 2 with 10 elements. An example of the image generated in the simulation 207 is shown in Fig.2. Moreover, x_5 and x_6 are Level1 (i.e., high-resolution image features) and Level2 208 (i.e., low-resolution image features) 2-D sym4 wavelet coefficients extracted from Modality 3. As 209 the disturbance, we also generate Modality 4 as the uncorrelated signal to validate the robustness of 210 variable selection performance for the proposed model. The corresponding feature x_7 for Modality 4 is 211 generated from a Gaussian distribution N(0, 1). 212

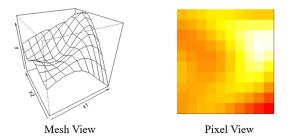


Figure 2. The simulated thermal distribution Signal

Table 2. Data Summary in Simulation (number of features is shown in parenthesis)

Data	ta Modality 1		Modality 2		Modality 3		Modality 4
Features	High-resolution time-series features (8)	Low-resolution time-series features (4)	High-resolution time-series features (8)	Low-resolution time-series features (4)	High-resolution image features (25)	Low-resolution image features (4)	Noise generated from Normal Distribution (11)

After generating the features from each data modality, we need to determine the significant modalities and corresponding significant features in each sample. The significant modalities and the features will be randomly selected from Modalities 1 to 3 following a uniform distribution. Moreover, for each significant variable $x_{i,j}$ (i.e., jth variable from ith modality), the corresponding model coefficients $\beta_{i,j}$ is generated through a uniform distribution as Unif(-3, 3). Therefore, for the simulation that has a linear model structure, the response y for each sample can be generated as:

$$y = \sum_{i} \sum_{j} \beta_{i,j} x_{i,j} + \xi.$$
(8)

Moreover, for the simulation that has a nonlinear model structure, the response is generated as:

$$y = \sum_{i} \sum_{j} \beta_{i,j} \exp\left(x_{i,j} + \xi\right), \tag{9}$$

where $\xi \sim N(0, \gamma^2)$, and the magnitude of γ^2 is determined by the signal-to-noise ratio from the simulation setting.

For each simulation setting shown in Table.1, 100 replicates are simulated. The proposed MOSS is compared with three benchmark models to evaluate its prediction performance and also the variable

selection accuracy: (1) the Lasso regression which can only implement the variable selection efforts 217 without the concept of data modality [22]; (2) the group Lasso which can implement the variable 218 selection in modality level but cannot select the variable within each modality [39]; and 3) the hierarchical Lasso which can implement the variable selection in both among modalities and within 220 each modality [24]. These three benchmarks can help to comprehensively validate the performance of 221 the MOSS for both variable selection and prediction accuracy. To evaluate the prediction accuracy, in 222 each replication of the simulation, 80% samples are used as the training dataset, and the remaining 223 20% of samples are used as the testing dataset. To fairly compare the variable selection accuracy, the significant variables for each simulation case are the same among each replication. Moreover, the 225 number of modalities selected from the MOSS is fixed as the maximum number of modalities selected 226 among benchmarks in each replication. Based on this scenario, we can validate whether the proposed 227 MOSS can effectively guide the multi-modal sensing system design with a limited budget (i.e., limited 228 sensor modalities) by selecting the most relevant sensor modalities compared with benchmarks. 229

230 4.2. Results and discussion

	Lasso Regression	Group Lasso	Hierarchical Lasso	MOSS (Proposed)
Case 1	8.72%	8.35%	8.37%	7.58%
	(0.04)	(0.02)	(0.02)	(0.02)
Case 2	9.42%	9.10%	8.82%	7.71%
Case 2	(0.07)	(0.01)	(0.02)	(0.01)
Casa 2	15.75%	14.97%	13.24%	11.92%
Case 3	(0.05)	(0.03)	(0.05)	(0.02)
	9.94%	9.51%	8.42%	7.93%
Case 4	(0.05)	(0.02)	(0.02)	(0.02)
	13.41%	12.75%	12.69%	10.46%
Case 5	(0.06)	(0.04)	(0.05)	(0.02)
Case 6	7.81%	7.04%	7.15%	6.67%
Case 0	(0.07)	(0.01)	(0.01)	(0.01)
Case 7	8.65%	8.17%	7.81%	7.23%
Case /	(0.06)	(0.01)	(0.04)	(0.02)
Case 8	12.89%	10.61%	10.17%	8.82%
	(0.08)	(0.01)	(0.02)	(0.02)

Table 3. Normalized RMSE (Standard Error) of Each Simulation Case

The average of the normalized root-mean-squared error (RMSE) and the corresponding standard 231 error for eight simulation cases are shown in Table. 3. The values shown in bold are the smallest 232 prediction errors and the corresponding standard error obtained from different models in each simulation case. From the results, the proposed MOSS yields the best prediction accuracy in most 234 of the cases with both linear and nonlinear model structures. It is because the proposed MOSS can 235 deal with the nonlinear model components, and can effectively implement the variable selection for 236 both among the modalities and within each modality compared with the benchmarks via the function 237 norm and *l*-1 norm simultaneously. For the Lasso regression, it can be observed that the standard error is relatively large than other methods. It is because without considering the variable relationships 239 among modalities, the variable selection result might not be stable among replications. Moreover, 240

since the group Lasso cannot effectively implement the variable selection within each modality, more insignificant variables are included in the model and the prediction accuracy is relatively low. For the hierarchical Lasso, it has a comparable result with the proposed MOSS method, but for the nonlinear model components, the proposed MOSS has a better prediction accuracy since the functional norm can work with both linear and nonlinear model components.

	Lasso Regression	Group Lasso	Hierarchical Lasso	MOSS (Proposed)
Case 1	51.2%	56.2%	61.2%	64.8%
Case 2	54.3%	57.1%	62.3%	68.7%
Case 3	55.1%	60.8%	63.3%	61.9%
Case 4	48.2%	52.4%	62.9%	68.7%
Case 5	60.2%	54.1%	70.4%	75.4%
Case 6	63.4%	58.7%	68.6%	73.2%
Case 7	66.1%	59.2%	67.3%	71.5%
Case 8	63.2%	53.8%	70.6%	73.6%

 Table 4. Average Variable Selection Recall of Each Simulation Case

On the other hand, to evaluate the variable selection accuracy of each method, the Recall =246 Number of Significant Variables Selected Tetel Number of Selected Variables is employed as the performance measurement since it can reasonably 247 reflect the cost-effective of variable selection results. The results are shown in Table.4. The proposed 240 MOSS yields the best cost-effective performance in all simulation settings. It shows the merits of the 249 proposed MOSS that can efficiently select the significant modalities and variables simultaneously. 250 Moreover, the group Lasso has good precision for most simulation cases. The Lasso regression almost 25: has the worst variable selection performance on all simulation settings since it cannot address the 252 modality structure among variables, and can only consider the variables that are independent in 253 variable selection. Moreover, it is not surprising since the group Lasso does not implement the variable 254 selection within each modality, therefore the number of selected variables for group Lasso is much 255 higher than other methods. The recall for the group Lasso also proves this idea. The hierarchical 256 Lasso usually has a comparable variable selection precision with the MOSS since it can also implement 257 the variable selection for both modalities and within each modality. But limited by its linear model component assumption, the proposed MOSS can be more flexible compared with the hierarchical 259 Lasso. 260

261 5. A Real Case Study

262 5.1. Experiment Setup

In order to evaluate the performance of the proposed model, we apply the proposed method 263 to the data sets collected from a real FDM process [12]. Specifically, we predict the corresponding geometric deviation features based on the *in situ* process data collected from different sensors. In this 265 data sets, the FDM product is fabricated under different combinations of process setting variables 266 based on the design of the experiment method. The selected process setting variables in the experiment 267 are shown in Table.5. In total, there are four setting variables in two levels: extruder speed, extruder 268 temperature, temperature disturbance, and platform vibration disturbance. The extruder speed and the extruder temperature are both the significant setting variables that can directly influence the product 270 quality [52]. To introduce extra disturbance to the system, two types of process noise are involved in 271

	Extruder travel speed	Extruder temperature	Temperature disturbance	Vibration disturbance
Level 1	40 <i>mm</i> /s	225°	On	On
Level 2	70 <i>mm</i> / <i>s</i>	245°	Off	Off

Table 5. Setting Variables in the Experiment [12]

the experiment. The disturbances are introduced by a fan near the extruder, which can significantly 272 change the thermodynamic in the near area, and a vibrator on the printing bed. These disturbances are 273 employed to validate whether the proposed method can identify the disturbance in variable selection 274 results. A full factorial design with three replications of each experiment treat is executed in this case 275 study. In total, 48 products are fabricated. The full design of the experiment table is attached in the 276 Appendix. A1. In the experiment, the modified national aerospace standard 979 test part design (as 277

shown in Fig.3) is selected as the product design [10]. 278

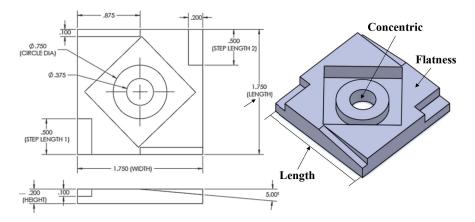


Figure 3. Standard drawing of NAS 979 part [10]

The multi-modal sensing system for the FDM process in the experiment is equipped with 279 two tri-axis accelerometers, two thermocouples, and one infrared (IR) sensor as shown in Fig.1(a). 280 All signals are measured at a sampling frequency of 1 Hz via a data acquisition system built by 281 Ni-cRIO-9073. Such a senor selection and frequency combination has shown to be effective to reflect 282 the real-time FDM process condition [10,12]. For the vibration sensor, it contains the vibration signals 283 from the three-axis, and each axis is considered as one separate data modality. It is because the signal 284 from each axis can reflect different types of process variation for a FDM process, and can further help 285 to accurately identify the significant modality in the process. The wavelet analysis is used to compactly 286 represent the *in situ* signals collected from these sensors in this case study. Specifically, the Level4 287 detail wavelet coefficients generated based on the db4 basis are employed as signal features in this 288 case study. Finally, there are 47 features extracted from each data modality, and there are nine data 289 modalities in total. After the product fabrication, the coordinate measuring machine is used to measure 290 the corresponding geometric quality variables (i.e., length, flatness, and concentric). 29:

5.2. Results and Discussion 292

Quality Measurements (from CMM)	Lasso	Group Lasso	Hierarchical Lasso	MOSS (Proposed)
Length	20.15%	17.65%	16.14%	14.57%
Flatness	12.43%	11.44%	9.79%	7.91%
Concentric	11.06%	9.83%	9.02%	7.86%

Table 6. Average of Normalized RMSEs

To evaluate the prediction performance of the proposed model, a 5-fold CV training-testing 293 strategy is employed. Similar to the simulation study, the Lasso, group Lasso, and hierarchical Lasso 294 are used as the benchmark methods. The average of normalized RMSEs for testing from 5-fold CV is shown in Table.6. It can be observed that the proposed MOSS yields the best prediction accuracy for 296 all three quality measurements. It is because the proposed method can properly identify the significant 297 data modalities based on the smooth spline functional norm and also the important features within 298 each modality. The Lasso regression has the worst prediction accuracy since it does not to consider 299 the modality structure among each variable. This issue might lead to an inaccurate variable selection result. Similarly, the group Lasso has comparable results with the Lasso regression since it can only 301 consider the variable selection among modalities. Moreover, the hierarchical Lasso has a better result 302 compared with Lasso and group Lasso since it can implement the variable selection on two-levels 303 simultaneously. However, due to it might usually restrict on a local optimal when estimating the 304 model coefficients, the proposed method could be more effective to identify the significant modalities. 305

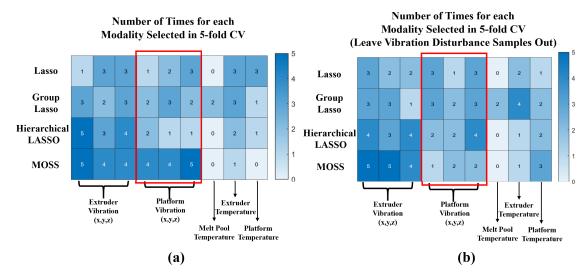


Figure 4. (a) Number of Times for each Modality Selected in 5-fold CV; (b) Number of Times for each Modality Selected in 5-fold CV after Leaving Vibration Disturbance Samples Out

On the other hand, to evaluate the modality selection results, the number of times that each modality is selected in the 5-fold CV for product flatness is shown in Fig.4. Specifically, the modality 307 selection results for two scenarios are studied: (1) the modality selection results with all samples 308 collected from the experiments; and (2) the modality selection results for the samples that do not 309 have the vibration disturbance on the printing bed. The motivation of this sensitivity analysis is to 310 evaluate whether the proposed method and the benchmarks can accurately identify the significant data 311 modalities in model estimation. From the Fig.4, it can observe that when the printing platform has the 312 vibration disturbance, the proposed MOSS method can effectively identify the influence of extruder 313 and platform vibration in the model estimation, which are the most relevant modalities for product 314 flatness [12]. Once the vibration disturbance is removed, the number of selection times for platform 315 vibration is significantly reduced. It is because the contribution of platform vibration is decreasing 316 without the vibration disturbance during the fabrication process. On the other hand, other benchmarks 317 cannot always select these important modalities in model estimation. Moreover, after removing the 318 samples that have the vibration disturbance, the proposed MOSS method can also effectively identify 319 the most relevant modalities (i.e., extruder vibration) on this scenario and have a better selection 320 accuracy compared with other benchmarks in a 5-fold CV. Therefore, it can be concluded that the 321 proposed MOSS can effectively select the sensing modalities in a quality model. This result can further 322 guide the multi-modal sensing system design and support the root cause analysis to improve the 323 product quality and the process reliability of the FDM. 324

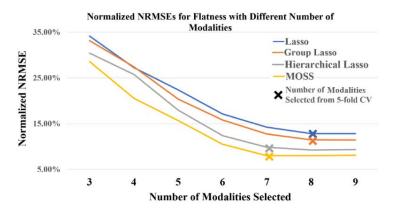


Figure 5. Normalized NRMSEs for Flatness with Different Number of Modalities

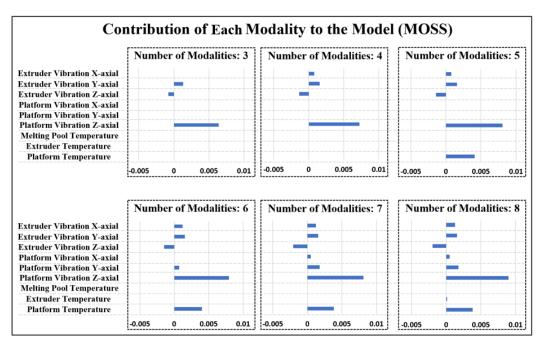


Figure 6. Contribution of each Modality for Flatness Prediction with Different Numbers of Modalities in MOSS

Moreover, to identify whether the proposed MOSS can effectively identify the best subset of 325 modalities when modeling the quality-process relationship, the prediction results for product flatness 326 with a different number of selected modalities are shown in Fig.5, Fig.6, and Fig.7. The number of 327 modalities selected represents the maximum number of modalities that the method can select in model 328 estimation. To guarantee the modeling performance, the number of selected modalities is started 329 from three. It can be observed that in Fig.5 the proposed MOSS method yield the best prediction 330 accuracy in all scenarios compared with benchmarks. It is because that the proposed MOSS method 331 can accurately selecting the significance of the sensing modality. To validate this point of view, we 332 also summarized the selected modalities in detail. Due to the limited space, we mainly showed the 333 selected modalities for MOSS and Hierarchical Lasso in Fig.6 and Fig.7 for the number of modalities 334 from three to eight. Since the hierarchical Lasso has the closest prediction accuracy with the MOSS. 335 Based on the modality selection result, it can be observed that the proposed MOSS can accurately 336 select the modalities in a proper order compared with the benchmark. For example, when the number 337 of selected modalities increased to four, the MOSS selected x-axial extruder vibration as the additional 338 modality, and the hierarchical Lasso selected platform temperature as the additional modality. For the 339 flatness of the product, as discussed above, the variation of platform temperature is not significant 340

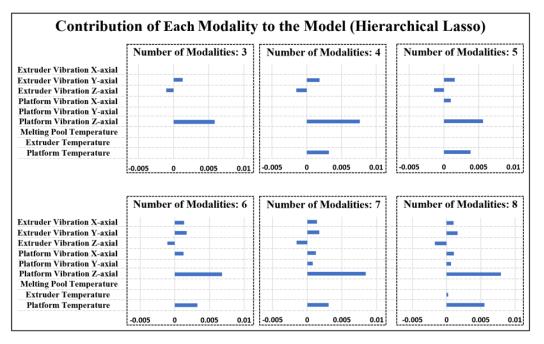


Figure 7. Contribution of each Modality for Flatness Prediction with Different Numbers of Modalities in Hierarchical Lasso

³⁴¹ compared with the vibration on the extruder. This modality selection result also explains why the

prediction accuracy for Moss is much better than hierarchical Lasso when the number of selected 342 modalities is four. On the other hand, it can also be found that even though the selected modalities are 343 the same for both MOSS and hierarchical Lasso, the prediction accuracy of Moss is still slightly better than the hierarchical Lasso. One possible explanation is the MOSS can better leverage the selection 345 efforts between the modalities and the variables within each modality based on the smooth spline 346 non-parametric estimation. Moreover, the hierarchical Lasso usually yields a local optimal due to 347 the modeling estimation restriction [25]. The MOSS also has the flexibility to control the number of 348 modalities selected in the model estimation, and further guide a cost-effective multi-modal sensing 349 system design. Therefore, when there are limited resources and have to select the best subset of 350 modalities, the MOSS can still select the most relevant modalities, and while estimating an accurate 351 quality-process model. 352

353 6. Conclusion

Smart manufacturing integrates the multi-modal sensing system and the computation capability 354 to effectively support real-time data analytics. However, how to design a multi-modal sensing 355 system with a cost-effective consideration for the manufacturing process is a challenging question. 356 Because it is difficult to accurately identify the relevance and contribution of each sensor modality 357 toward the specific quality response. Therefore, in this research, we proposed a new model called 358 MOSS, which can effectively rank the significant sensor modalities and simultaneously identify the 359 important features within each modality in model estimation. It can guide the sensing system design 360 in smart manufacturing, and also provides a way to identify the contribution of each modality to 361 potentially guide the diagnosis for the quality variation [10]. The MOSS can be easily extended to 362 other applications and domains, such as other manufacturing processes or healthcare applications 363 which usually need to model the data with a multi-modal format [53,54]. 364

This research also leads to several future research directions. First, we can generalize the MOSS so that multiple quality responses can be jointly modeled. One possible extension of the MOSS is to multiple response regression under the non-parametric estimation framework [55]. Next, the spatial process variables and quality responses, such as the thermal video and 3d profile of the product, can Version December 15, 2020 submitted to Sensors

- ³⁶⁹ be incorporated into the MOSS to reasonable quantify the spatio-temporal relationship contained in
- both process variables and quality variables [56]. Finally, the monitoring and control strategy can also
- ³⁷¹ be integrated with the MOSS in a real-time manner to effectively detect the anomaly event during the
- ³⁷² fabrication process, and further improve process reliability and reduce process variation [57].

373 Appendix A.

Run Number	Number	Extruder Speed Level	Extruder Temperature Level	Temperature Disturbance Level	Vibration Disturbance Level
44	1	0	0	0	0
43	2	0	0	0	1
7	3	0	0	1	0
48	4	0	0	1	1
20	5	0	1	0	0
21	6	0	1	0	1
6	7	0	1	1	0
29	8	0	1	1	1
12	9	1	0	0	0
26	10	1	0	0	1
30	11	1	0	1	0
24	12	1	0	1	1
14	13	1	1	0	0
22	14	1	1	0	1
3	15	1	1	1	0
38	16	1	1	1	1
10	17	0	0	0	0
28	18	0	0	0	1
33	19	0	0	1	0
41	20	0	0	1	1
32	21	0	1	0	0
8	22	0	1	0	1
15	23	0	1	1	0
45	24	0	1	1	1
19	25	1	0	0	0
36	26	1	0	0	1
42	27	1	0	1	0
35	28	1	0	1	1
11	29	1	1	0	0
31	30	1	1	0	1
5	31	1	1	1	0
4	32	1	1	1	1
16	33	0	0	0	0
1	34	0	0	0	1
13	35	0	0	1	0
40	36	0	0	1	1
2	37	0	1	0	0
39	38	0	1	0	1
46	39	0	1	1	0
25	40	0	1	1	1
34	41	1	0	0	0
23	42	1	0	0	1
17	43	1	0	1	0
37	44	1	0	1	1
27	45	1	1	0	0
47	46	1	1	0	1
18	47	1	1	1	0
9	48	1	1	1	1

Table A1. Design of Experiment Table for Case Study [12]

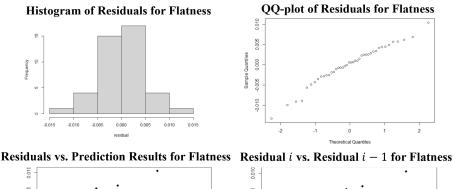




Figure A1. Residual Plot and Assumption Check for the Proposed MOSS in Case Study

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