



Article Deep Learning-Based Hardness Prediction of Novel Refractory High-Entropy Alloys with Experimental Validation

Uttam Bhandari ^{1,*}, Congyan Zhang ¹, Congyuan Zeng ², Shengmin Guo ², Aashish Adhikari ³ and Shizhong Yang ^{1,*}

- ¹ Department of Computer Science, Southern University and A&M College, Baton Rouge, LA 70813, USA; congyan_zhang@subr.edu
- ² Department of Mechanical and Industrial Engineering, Louisiana State University, Baton Rouge, LA 70803, USA; czeng8@lsu.edu (C.Z.); sguo2@lsu.edu (S.G.)
- ³ School of Electrical Engineering and Computer Science, Oregon State University, Corvallis, OR 97331, USA; adhikara@oregonstate.edu
- * Correspondence: uttam.bhandari@sus.edu (U.B.); shizhong_yang@subr.edu (S.Y.)

Abstract: Hardness is an essential property in the design of refractory high entropy alloys (RHEAs). This study shows how a neural network (NN) model can be used to predict the hardness of a RHEA, for the first time. We predicted the hardness of several alloys, including the novel $C_{0.1}Cr_3Mo_{11.9}Nb_{20}$ Re₁₅Ta₃₀W₂₀ using the NN model. The hardness predicted from the NN model was consistent with the available experimental results. The NN model prediction of $C_{0.1}Cr_3Mo_{11.9}Nb_{20}Re_{15}Ta_{30}W_{20}$ was verified by experimentally synthesizing and investigating its microstructure properties and hardness. This model provides an alternative route to determine the Vickers hardness of RHEAs.

Keywords: high entropy alloys; neural networks; hardness-prediction; microstructure



Citation: Bhandari, U.; Zhang, C.; Zeng, C.; Guo, S.; Adhikari, A.; Yang, S. Deep Learning-Based Hardness Prediction of Novel Refractory High-Entropy Alloys with Experimental Validation. *Crystals* 2021, *11*, 46. https://doi.org/ 10.3390/cryst11010046

Received: 26 November 2020 Accepted: 1 January 2021 Published: 7 January 2021

Publisher's Note: MDPI stays neutral with regard to jurisdictional claims in published maps and institutional affiliations.



Copyright: © 2021 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https://creativecommons.org/licenses/by/4.0/).

1. Introduction

Refractory high entropy alloys (RHEAs) are designed by adding high melting point elements such as Cr, Mo, Nb, Ta, Ti, V, W, Re, W, Ru, Zr, Rh, Os, Ir, and Hf. RHEAs have excellent properties, such as a high hardness and high-temperature softening resistance [1–4]. Thus, application of RHEAs can be very promising candidates in the field of aerospace industry. Many studies of RHEAs such as TaNbHfZrTi, TiZrNbMoV, NbMoTaW, VNbMoTaW, Ti₂ZrHf_{0.5}MoNbx, and Al_{0.5}CoCrCuFeNi have shown excellent yield strength both at room and high temperatures [5–10]. However, the poor ductility at room temperature of RHEAs limits their industrial application. One study has shown that doping elements such as C, B, N, O, Al, Si with RHEAs could improve the mechanical properties of RHEAs and enhance their applications [11-18]. The addition of 0.1 atomic percentage (at.%) of C and 0.3 at.% of C in Mo_{0.5}NbHf_{0.5}ZrTi₁₀ has improved the plasticity and increased the compressive stress [19]. Therefore, doping with low concentrations of non-metallic elements is very important in RHEAs for improving the mechanical properties. However, predicting the mechanical properties of doped RHEAs by the first principles method is very complex. Moreover, experimental techniques are costly and tedious. Therefore, machine learning (ML) could be a promising tool to predict the mechanical properties of new complex RHEAs.

ML approaches have been used to predict the crystal structures and properties of materials [20–22] with convincing results. Islam et al. [23] trained neural network (NN) models that can analyze the phase of multi-principal element alloys (MPEAs) with 118 data samples. An NN model is a supervised machine learning prediction model that is inspired by the functionalities of the human brain. Wen et al. [24] developed a material design strategy using ML for predicting the desired properties of high entropy alloys (HEAs). George et al. [25] also utilized a machine learning model which can predict the

elasticity of high entropy alloys and included experimental validation. These studies have shown that ML methods are capable and reliable in discovering new RHEAs and predicting their phases. However, many studies focus on phase formation predictions, and a few on predicting the mechanical or functional properties of complex RHEAs.

In this study, the Vickers hardness of several complex RHEAs including $C_{0.1}Cr_3Mo_{11.9}$ Nb₂₀Re₁₅Ta₃₀W₂₀ were predicted by utilizing an NN model. We experimentally synthesized $C_{0.1}Cr_3Mo_{11.9}Nb_{20}Re_{15}Ta_{30}W_{20}$, and the phase, microstructure, and Vickers hardness were studied. The measured Vickers hardness was found to be consistent with the NN model prediction.

2. Materials and Methods

2.1. Computational Methods

The features of the alloys and the corresponding target hardness values used in this study were collected from several previous publications [6,19,26,27]. In this study, we only considered the average hardness value of HEAs present in the reference papers and did not consider the hardness value that changed with the applied load. Although a total of 380 experimental records of measured hardness were collected from the literature, the alloys that contained unwanted elements were left out, reducing the number of total available samples to 128.

A supervised machine learning task performs several steps before the actual prediction is made. An NN model requires features to train and thus make informed predictions. In this particular task, 22 relevant features that were initially picked based on the domain knowledge of which features could be helpful to predict Vickers hardness consisted of the percentage of each element in the alloy, i.e., % of Cr, % of Hf, % of Mo, % of Nb, % of Ta, % of Ti, % of Re, % of V, % of W, % of Zr, % of Co, % of Ni, % of Fe, % of Al, % of Mn, % of Cu, % of C, the entropy of the alloy (ΔS_{mix}) [28], the bulk modulus (*B*), the shear modulus (*G*), the valence electron concentration (*VEC*) [29], and the melting temperature (T_m). The HEA features were calculated using the rule of mixtures.

$$\Delta S_{mix} = -R \sum_{i=1}^{n} C_i ln C_i \tag{1}$$

$$\boldsymbol{B} = \sum_{i}^{n} (C_i B_i) \tag{2}$$

$$G = \sum_{i}^{n} (C_i G_i) \tag{3}$$

$$\boldsymbol{T}_{\boldsymbol{m}} = \boldsymbol{C}_i \ (\boldsymbol{T}_{\boldsymbol{m}})_i \tag{4}$$

$$VEC = \sum_{i=1}^{n} C_i (VEC)_i$$
(5)

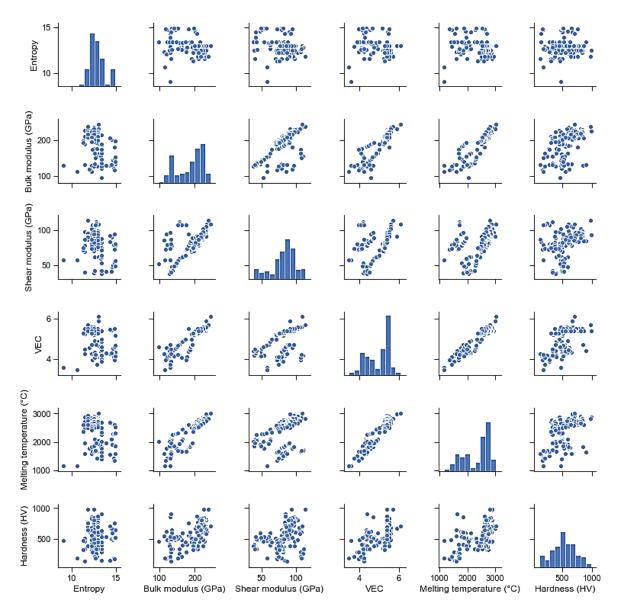
where *R* is the ideal gas constant, C_i the atomic percentages of the *i*th element, B_i is the bulk modulus of the *i*th element, G_i is the shear modulus of the *i*th element, $(T_m)_i$ is the melting point of the *i*th element, and $(VEC)_i$ is the valence electron concentration of the *i*th element.

In a typical supervised machine learning task, the dataset is split into training and testing sets before any feature engineering, visualization, analysis, or training is performed, so as to prevent any data leakage, i.e., the training should not be influenced by any information from the test data. After random shuffling, 90% of the total samples were allocated for training and validation and 10% for testing. Here, we explain the data preprocessing steps that were conducted on the training data before the NN model was trained. Firstly, the features that had zero or nominal variance were removed from the dataset. The methods adopted for feature selection and engineering in this work stem from a general class of feature engineering techniques [30]. ML models work on the basis of how close the samples are located to each other in the high-dimensional feature space. Features

that have nominal variance do not contribute much to differentiating among the samples, therefore it is better to remove such features before passing the data to an ML model to reduce space as well as time complexity. The removed feature was the "% of Re" in each sample, because all the samples in the training data had the same percentage of Re. Next, we removed the correlation among the features by two methods in succession, first, by the method of condition indices, and then by visually plotting the correlation among the features that successfully passed the condition index test.

A subset of the scatterplot of the features before the condition indices step is shown in Figure 1. There is clear association between that bulk modulus, valence electron concentration, entropy, and melting temperature, suggesting that these features are highly correlated.

Crystals 2021, 11, x FOR PEER REV The calculated Pearson's correlation of coefficient [31] between the RHEA features of 428



samples' data is shown in Table 1.

Figure 1. Scatterplot matrices of six features from the 128 samples data.

Table 1. The calculated Pearson's correlation coefficients which are related to different features of high entropy alloys (HEAs) in 128 data samples.

	$\Delta S_{ m mix}$	В	G	VEC	T_m	HV
ΔS_{mix}	1	-0.24	-0.25	-0.16	-0.12	0.044
В	-0.24	1	0.62	0.9	0.88	0.53
G	-0.25	0.62	1	0.48	0.37	0.32
VEC	-0.16	0.9	0.48	1	0.96	0.57
T_m	-0.12	0.88	0.37	0.96	1	0.56

	$\Delta S_{\rm mix}$	В	G	VEC	T_m	HV
ΔS_{mix}	1	-0.24	-0.25	-0.16	-0.12	0.044
В	-0.24	1	0.62	0.9	0.88	0.53
G	-0.25	0.62	1	0.48	0.37	0.32
VEC	-0.16	0.9	0.48	1	0.96	0.57
T_m	-0.12	0.88	0.37	0.96	1	0.56
HV	0.044	0.53	0.32	0.57	0.56	1

Table 1. The calculated Pearson's correlation coefficients which are related to different features of high entropy alloys (HEAs) in 128 data samples.

Table 1 shows that a correlation exists among the different features used. During feature removal, only those features that had minimal correlation with the target variable hardness were removed; this set of removed features included *VEC*, T_m , and B. This is a way to reduce the feature space complexity by losing minimal information from the dataset. Furthermore, visually plotting the scatterplots of the remaining features revealed some correlation among the % of Co, the % of Fe, and the % of Ni. Hence, the % of Co and the % of Fe were eliminated.

Next, Pandas library [32] was used to normalize the value of the features so that each feature came within a range of 0 and 1. Feature normalization allows all the features to scale to a similar scale, and thus makes training faster by balancing the length of the contours of the loss function across all dimensions of the parameters that are to be updated.

After that, the actual training steps began. The number of training samples is very small; therefore, k-fold cross-validation was chosen to obtain a model which performed the best on average among all the validation folds. Furthermore, because a neural network training comes with several hyperparameter choices, the hyperparameters were tuned using a randomized search. The hyperparameter grid used to sample different configurations of randomized hyperparameter search is as below:

learning rate = {0.00005, 0.0001, 0.0003, 0.0005, 0.001, 0.003, 0.005}

weight decay for regularization = $\{1 \times 10^{-5}, 5 \times 10^{-5}, 1 \times 10^{-4}, 5 \times 10^{-5}, 1 \times 10^{-3}, 5 \times 10^{-3}, 1 \times 10^{-2}, 5 \times 10^{-2}, 1 \times 10^{-1}\}$

momentum = $\{0.5, 0.75, 0.99\}$

nesterov = {True, False}

number of nodes per layer = {14, 17, 21, 24, 28, 35}

number of maximum epochs to train = {50, 75, 100, 125, 150, 175, 200, 250, 300, 325, 350, 375, 400, 425, 450, 475, 500}

dropout probability per node = $\{0, 0.3, 0.5\}$

minibatch size = $\{1, 2, 4, 8, 16, 32, 64\}$

optimizers = {torch.optim.SGD}

The training methodology followed a four-step procedure:

Step 1. Randomly selected 500 different configurations from the hyperparameter space. Step 2. Trained 500 neural networks using all of these configurations with 20-fold cross validation.

(a) The purpose of this k-fold training was to find the most generalizable set of hyperparameter configurations among the randomly chosen 500 configurations.

Step 3. After obtaining the best set of hyperparameters, we discarded all the previously trained 500 * 20 models and trained a new neural network using:

- (b) all the training data;
- (c) the best set of hyperparameters obtained from Step 2;
- (d) no cross validation. (because we had already found the hyperparameters).

Step 4: In Step 2, all intermediate models were saved at the end of each epoch. This allowed us to monitor the performance of our model on the test set at each epoch. In essence, if the model performance diverged after the nth epoch, we could discard the training epochs after the nth epoch. This gave us the "best model" corresponding to this "best set of hyperparameter configuration".

The open-source libraries PyTorch, scikit-learn, and scorch were used to train the NN model and predict the hardness of the RHEAs.

The NN model consisted of three abstract regions, namely, the input layer, the hidden layers, and the output layer. The input layer takes in the features and passes them to the hidden layers. The output layer is the last layer of the NN model, which simply produces Crystals 2021, 11, x FOR PEER REVIEW the output based on the information passed from the last hidden layer nodes. The following

relationship can be used to calculate the output of each neuron (a_i) :

where b_i are the bias terms and W_{ij} are the weights provided for each input node. The value of a_i proceeds through an activation function. Then, the activation function will define the output of this particular neuron. The type of activation function used in this NN mbded is deally like to the value of a stick to the value of a structure to the value of a_i proceeds through an activation function. Then, the activation function will define the output of this particular neuron. The type of activation function used in this NN mbded is deally like to the value of a structure to the value of th

$$MSE = \frac{1}{n} \sum_{i=1}^{n} (Y_i - \hat{Y}_i)^2$$
(7)
$$MSE = \frac{1}{n} \sum_{i=1}^{n} (Y_i - \hat{Y}_i)^2$$
(7)

where *n* is number of data points, Y_i is the observed values, and \hat{Y}_i is the predicted values. We have \hat{Y}_i is the predicted values. \hat{Y}_i is the predicted values.

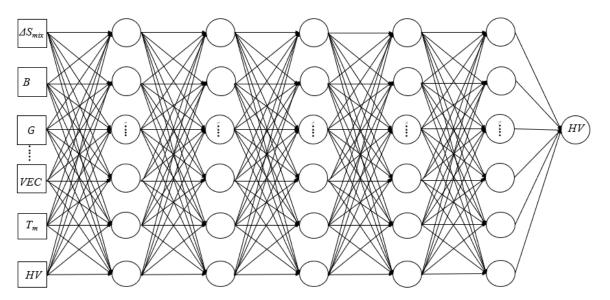


Figure 2: A schematic model of the neural network (NN) showing 5 hidden layers: The input consists of HEAs features as represented by square boxes on the left.

2.2. Experimental Methods

The C_{0.1}Cr₃Mo_{11.9}Nb₂₀Re₁₅Ta₃₀W₂₀ alloy was synthesized by vacuum arc melting method (MAM-1, Edmund Bühler, Bodelshausen, Germany) from the corresponding element mixture under a pure argon atmosphere. The powders of Cr, Mo, Nb, Re, Ta, W, and

2.2. Experimental Methods

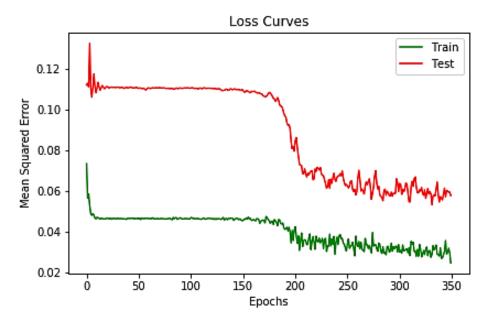
The C_{0.1}Cr₃Mo_{11.9}Nb₂₀Re₁₅Ta₃₀W₂₀ alloy was synthesized by vacuum arc melting method (MAM-1, Edmund Bühler, Bodelshausen, Germany) from the corresponding element mixture under a pure argon atmosphere. The powders of Cr, Mo, Nb, Re, Ta, W, and C were mixed inside a polystyrene mill jar for 15 min and cold pressed in a stainless steel mold using a pressure of 350 MPa and a dwelling time 30 s. The purity of each elements was more than 99.5 wt %. For the purpose of homogeneous distribution of elements, the melted ingots were flipped over and re-melted 4 times. After this, epoxy resin (a mixture of SamplKwick powder and SamplKwick liquid with the volume ratio 2:1) was applied to firmly wrap the solid ingots for easy handling. The cross section of the sample was cut using a BUEHLER low speed saw. Prior to the property tests, the cross section surface was mechanically ground with SiC papers with differing grit sizes, namely, 320, 600, 800, 1000, and 1200 mesh in sequence. After that, the ground cross section surface was polished using the MetaDiTM Supreme polycrystalline diamond suspension (1 μ m), and, finally, rinsed with deionized water and dried in air. The crystal structure of the sample was identified using an X-ray diffractometer system (Empyrean, PANalytical) provided with equipped Cu K α radiation (λ = 0.15406 nm). The 2 θ scan range from 20–120 degrees was performed with a step size of 0.026 degrees. The microstructure and chemical compositions of the $C_{0.1}Cr_3Mo_{11.9}Nb_{20}Re_{15}Ta_{30}W_{20}$ were examined using a field emission scanning electron microscope equipped with second electron (SE) and energy dispersive spectroscopy (EDS) detector (Ametek. Model: APOLLO XL, Berwyn, PA, USA). Vickers hardness was measured with a digital micro hardness tester (Clark Instrument Model CM-802AT, Novi, MI, USA). Three testing loads were used, namely, 2000, 500, and 100 gf, and the dwell time was 15 s. The Vickers hardness (HV) of C_{0.1}Cr₃Mo_{11.9}Nb₂₀Re₁₅Ta₃₀W₂₀ was tested at five different positions on the sample to ensure the consistency of the results. The intervals between adjacent testing positions were three times larger than that of the indent diagonals, which avoided the effects of work hardening.

3. Results and Discussions

3.1. Machine Learning Results

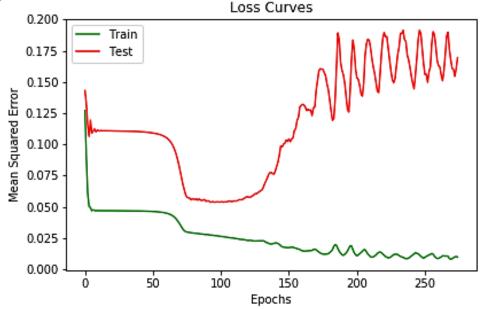
The best set of hyperparameter configurations obtained were learning rate = 0.001, weight decay for regularization = 0.001, momentum = 0.99, optimizers = stochastic gradient descent, nesterov = True, number of nodes per layer = 35, number of maximum epochs to train = 325, dropout probability per node = 0, and minibatch size = 1. The learning curves of hardness prediction are shown in Figure 3. The *y*-axis represents the mean squared error and the *x*-axis represents the number of epochs. It can be seen from the curve that the NN model was able to learn from the training data and predict the hardness of the samples for the validation data with a gradual decrease in loss over several epochs of training, starting from 0.125 and flattening out at around 0.0675. The NN model was trained on a dataset of 128 HEAs. There were also several models that diverged during training. An example case is shown in Figure 4.

the NN model was able to learn from the training data and predict the hardness of the samples for the validation data with a gradual decrease in loss over several epochs training, starting from 0.125 and flattening out at around 0.0675. The NN model v trained on a dataset of 128 HEAs. There were also several models that diverged during training. An example case is shown in Figure 4.



Crystals **2021**, *11*, x FOR PEER REVIE **Figure 3.** Learning curves of mean squared error as a function of the number of epochs. The red solid red curve represents the average 20-fold cross-validated loss scores on the validation fold, and the

Figure 3. Learning curves of mean squared error as a function of the number of epochs. The red solid red curve represents the average 20-fold cross-validated loss scores on the validation fold, and the green solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated loss score solid curve corresponds to the 20-fold cross-validated



Higuree44. Noteans squared terror assaft unot to not fit the number of the pool is: addiverging model.

We also generated, for each test sample, the hardness predictions of all 500 moduls trained. Then, the uncertainty error bars were plotted using standard deviation as the metric, which are shown in Figure 5. As expected, there existed some variance among the predictions of all 500 moduls.

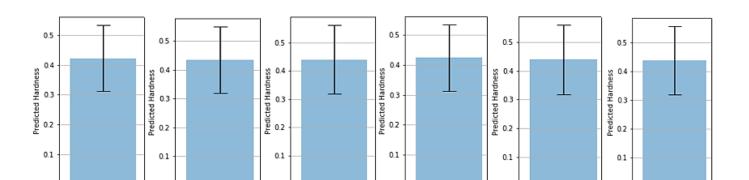


Figure 4. Mean squared error as a function of the number of epochs: a diverging model.

Crystals **2021**, 11, 46

We also generated, for each test sample, the hardness predictions of all 500 models trained. Then, the uncertainty error bars were plotted using standard deviation as the metric, which are shown in Figure 5. As expected, there existed some variance among the_{8 of 14} predictions of all 500 models.

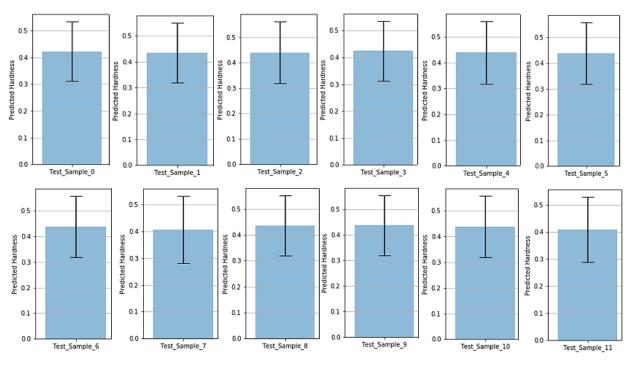


Figure 5. Error bars for the uncertainty among the trained models on test samples. Crystals **2021**, 11, x FOR PEER REVIEW

9 of 15

The R2 plots of Vickers hardness predicted by the NN on the training and test datasets are presented in Figure 6. As seen, the predictions have a trend along the y = x line. This indicates a good learnability for this task. After testing the model, the predicted hardness of tasks are presented in Figure 6. As seen, the predictions have a trend along the y = x line. Co.1 CFAMSHARAE2208045 teamabary via trunk to the testing the model, the predicted hardness of tasks are presented in Figure 6. As seen, the predictions have a trend along the y = x line. Co.1 CFAMSHARAE2208045 teamabary via trunk to the testing the model, the predicted hardness of tasks are presented in Figure 6. As seen, the predictions have a trend along the y = x line. Co.1 CFAMSHARAE2208045 teamabary via trunk to the testing the model, the predicted hardness of tasks are presented in Figure 6. As seen, the predictions the predicted that in graves the test to set the testing the finded of the prediction was chosen to digit the task and the test to set the testing the finded of the prediction was chosen to digit the test to stand the test to set the tes

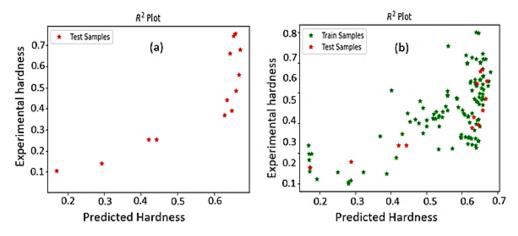


Figure 6. Hardness prediction by machine learning using the NN model for (a) the testing data and (b) both training and testing data the symbol source to predicted the random source to be predicted to be predic

Table 2. Experimental and NN model-predicted Vickers hardness of HEAs.

Test Name of Alloys Samples	Experimental Hard- ness (HV), and Refer- ence	ML Predic- tion (HV)	Error %
--------------------------------	---	-------------------------	---------

3	Nb25Ti25V25Zr25 Table 2. Experimental and NN mod	335 [36] el-predicted Vickers hardnes	s of HEAs. 481	43.5
4	M025.6Nb22.7Ta24.4W27.3	Experimenta ⁴⁵⁴ [37]	576	26.8
Test Samples 5	Name of Alloys Cr ₂₀ Co _{19.3} Fe _{19.6} M ₁₇ Ni _{19.52} V _{4.6}		ML Prediction (HV) 144	Error % 4.6
6	C _{0.4} Cr ₃ Mo _{11.9} Nb ₂₀ Re ₁₅ Ta ₃₀ W ₂₀ AI ₁₄₂ Mo222ND222TI215V _{20.95} (Nominal composition)	601 (our work 5 17 [39]	695 598	15 16 .6
7	$Cr_{1.6}Mo_{8.9}Nb_{20}Re_{15}Ta_{30}W_{20}$ (experimental composition)	601 770 [27]	686 686	141D.9
$\begin{bmatrix} 1\\ 8\\ 2 \end{bmatrix}$	$Hf_{21}Nb_{19,1}Ta_{20,1}Ti_{19,3}V_{23}Zr_{20,5}$ $Cr_{2}MB_{20}NB_{20}Ta_{20,1}Ta_{20,2}V_{13}W_{20}$	335 [34] 704 [35] 535 [37]	500 697 687	49.2 0. 99 .4
3 9 4	Nb25Ti25V25Zr25 CoMF218N5207Ca441M2732Si9.2	335 [36] 454 [37] 682 [40]	481 576 762	43.5 26181.7
5 10 6	$Cr_{20}Co_{19.3}Fe_{19.6}M_{17}Ni_{19.52}V_{4.6}$	151 [38] 517 [39] 207 [19]	144 598 263	4.6 15. @ 7
7	$Mo_{30}Nb_{10}V_{20}Ta_{20}W_{20}$	770 [27]	686	10.9
$\begin{array}{ccc} 11 & 8 \\ & 9 \end{array}$	Мо мгдАРСБУ24 15БУ24W221.1 Со _{12.9} Fe _{10.8} Ni _{10.8} Cu _{40.1} Al _{16.2} Si _{9.2}	535 [37] 498 [27] 682 [40]	687 665 762	28343.5 11.7
$12\begin{array}{c}10\\11\end{array}$	$\begin{array}{c} A Gr_{144}Co_{16.9}C_{16.9}S_{18.3} \\ A Gr_{144}Co_{16.9}C_{16.9}S_{18.3} \\ A Gr_{10} \\ M O_{40} \\ N \\ D \\ D$	207 [19] 498 [27] 535 [41]	$263 \\ 665 $ 628	²⁷ 17.3 33.5
12	Al _{14.4} Co _{16.9} Cr _{18.3} Fe _{16.8} Mn _{16.9} Ni _{16.7}	535 [41]	628	17.3

3.2. Experimental Results

The XRD pattern of C_{0.1}Cr₃Mo_{11.9}Nb₂₀Re₁₅Ta₃₀W₂₀ with the log intensity *y*-axis is 3.2. Experimental Results shown in Figure 7. According to the image, each diffraction peak indicates most likely one The XRD pattern of C_{0.1}Cr₃Mo_{11.9}Nb₂₀Re₁₅Ta₃₀W₂₀ with the log intensity *y*-axis is single body-centered cubic (BCC) phase. No obviously distinguished peaks can be obshown in Figure 7. According to the image, each diffraction peak indicates most likely served. This indicates the existence of a single-phase BCC phase be obconcrating to the wavelength of the X-ray is 1.5406 Å. With the help of served. This indicates the existence of a single-phase BCC phase in C_{0.1}Cr₃Mo_{11.9}Nb₂₀Re₁₅ a₃₀W₂₀. The wavelength of the X-ray is 1.5406 Å. With the help of Bragg's law [42], described as $2d \cdot sin\theta = n \cdot \lambda$ (8)

$$2a \cdot \sin\theta = n \cdot \lambda \tag{8}$$
$$2d \cdot \sin\theta = n \cdot \lambda \tag{8}$$

where d, θ , n, and λ are interplanar spacing, half of the diffraction angle, positive integer, where d, θ , n, and λ are interplanar spacing, half of the diffraction angle positive integer, where d, θ , n and λ are interplanar spacing, half of the diffraction angle positive integer, where d, θ , n and λ are interplanar spacing, half of the diffraction angle positive integer, where d, θ , n and λ are interplanar spacing, half of the diffraction angle positive integer, where d, θ , n and λ are interplanar spacing, half of the diffraction angle positive integer, where d, θ , n and λ are interplanar spacing, half of the diffraction angle positive integer, where d, θ , n and λ are interplanar spacing, half of the diffraction angle positive integer, where d, θ , η are interplanar spacing, half of the diffraction angle positive integer, where d are interplanar spacing positive integers and θ are integers and θ .

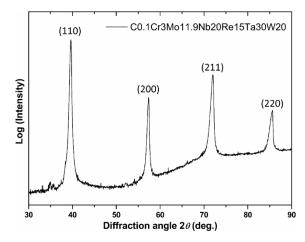


Figure 7. Image showing the XRD ptime of the law with the war is and way is indication in the diffraction angle and log function of intensity respectively.

The microstructure information of the has easted for Svi Mps Nb holes and the microstructure information of the has easted for Svi Mps Nb holes and the second second and the second and t

areas are seen, the XRD results only show a single BCC phase structure. The two areas The two BEC stabathes Chatructure and beneral marticle patical lattice dose paterna lattice dose paterna la se energhetbetyther are bereardthurdeterione baribetebee Bederioniusader, thise tardee Tor shaptar REtheredaskes arequire, incer wartierets martic (with press (with the viral of revendues) enconstaps bradestrip thap so idnit to a so id to be for a prime of the prime of th tenerofneieropnate movels or ved streach down pretition test two pelforpretormal Erosh Elos Figo uxt.Bushibits.charaisserveralsdectad.combosition.position.characterization to ensuability raliable liter utsthance subtecompleting composition in la neutricom it alisted. Watable de Gaubron velee monlisted in the list of the list of the list of the second istoirage and storages. Bisodosseel Carebos when it is a basolid bed aboth bad bishted posts he discut the face monothed suggest and starting and the starting and t oasthallosycostsaldorsisten tooritsisteen horitim the comprisitions it positions. Wildowed one with evaluate obstheratiole of tisedidologiered discoveretested the costed Cis contenteisabousiotered by a whee thamithed nontientl contemptationsphenomenon explained by the following heasing reased: 143,441a hosiyacan oxisteed iexibee argon latrace phenentup hereastial lay-cautadow as intervitably invidized dovidized example sizing resizing Coriscess efficial beneficial tion excitation entrance by sisteration densecting dense to 200 and the standard provident in the second second second second second second and sepreted to be someter over coldification of the store of the start of the second s entivated diffusion ad Cardusion the card making processo and principles of the content of the c templeion the paliphed surface solished surface.

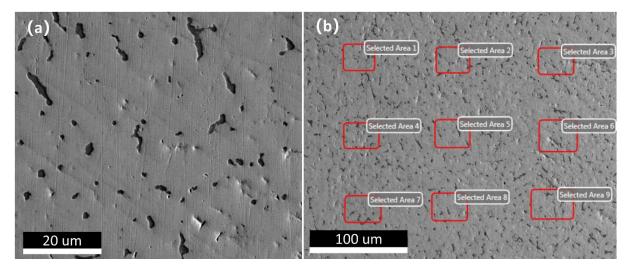


Figure 8. (a) SEM image of sample surface after polishing; (b) energy dispersive spectroscopy (EDS) testing areas on the sample surface:

Table 3: EBS t	esting results	of the polished	sample surface.
----------------	----------------	-----------------	-----------------

T1	N.11.	N.C.	<u> </u>	TT -	TAT	D .
Element		INIO	Çr	<u>r</u> a	VV VV	ĸe
Liement	Nb	Mo	Cr	la	VV	Ke
——Nominal (at.%)	20.00_	<u> </u>			-20.00	-15.00
Nominal (at %)	20.00	11 00	3.00	30.00	20.00	15.00
Tested (at %)	^{20.40} 31	118,00	1.06	31.47	22.66	16.20
	17.01	0.70	1.00	01.1/		10.07
Stand Tester (at: %) on (at %)	19.34 71	8.80 0	1.06-	<u>31,47</u>	22-66	1659
<u>Standard Deviation (at.%)</u>	0.71	0.19	0.15	0.17	0.51	0.29
Standard Deviation (at %)	0.71	0.19	0.15	0.17	0.51	0.29

Standard Deviation (at.%) 0.71 0.19 0.15 0.17 0.51 0.29 In addition, the difference of vapor pressure among the metal elements is another reason for the variation. As shown in Figure 9, the vapor pressure of the six elements from room the indefinition of the difference of wather interview in the reason of the six elements is another transfer interview in the difference of the six elements from the six elements is the pressure of the six elements in the six elements is another room the indefinition of the arc melting process, Cr and Mo were more volatile than the other elements, especially Cr.

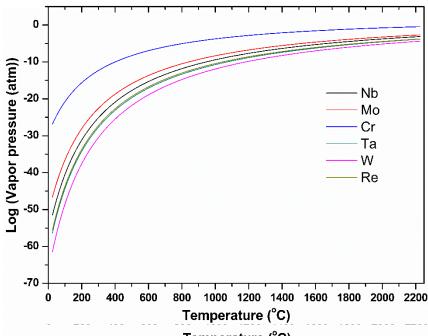


Figure 9. Image indicating the vap Jeppe (atura d'gG) a function of temperature (from room temperature to around 2200 °C). Figure 9. Imaggendition graphicapapt pressuse in log log actuaction to be of premipre (from term

An EDS mapping test was also performed to determine the composition distribution

in the areogen alberts also performed to determine the completences distribution in the areogen alberts also performed to determine the completences distribution in the areogen of the determined of the provided and the performance of the second of provide the determined of the provided and the performance of the second of the provided and the second of the performance of the second of the second of the provided and the second of the performance of the second of the provided and the second of the secon

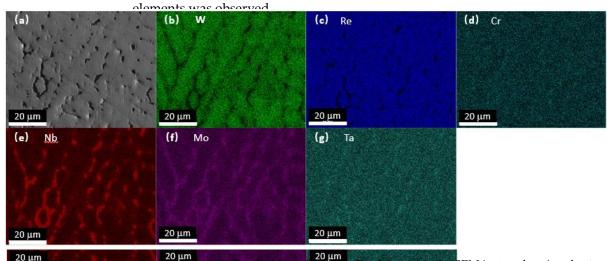


Figure 10. BO mapping results of the sample Co. Gov Mapping Result of the sample Co. Gov Mapping Results of the sample Co. CraMon. No. CraMon Mapping Results of the sample Co. CraMon. No. CraMon Mapping Results of the sample Co. CraMon. No. CraMon Mapping Results of the sample Co. CraMon. No. CraMon Mapping Results of the sample Co. CraMon. No. CraMon Mapping Results of the sample Co. CraMon. No. CraMon Mapping Results of the sample Co. CraMon. No. CraMon Mapping Results of the sample Co. CraMon. No. CraMon Mapping Results of the sample Co. CraMon. No. CraMon Mapping Results of the sample Co. CraMon. No. CraMon Mapping Results of the sample Co. CraMon. No. CraMon Mapping Results of the sample Results of the sample Co. CraMon. No. CraMon Mapping Results of the sample Results of the sample Co. CraMon. No. CraMon Mapping Results of the sample Results of the sample Co. CraMon. No. CraMon Mapping Results of the sample Results of the sample Co. CraMon. No. CraMon Mapping Results of the sample Results of the sample Results of the sample Co. CraMon Mapping Results of the sample Results of the same Results of the sample Results of the sa

A Vickers hardness test was carried out and the results are listed in Table 4. Based on the results, the average hardness was approximately 600 HV. Meanwhile, it was also determined that with the increase in testing load, the obtained average hardness decreases. This phenomenon is ascribed to indentation size effect [47], and similar observations were also reported by other researchers [48,49].

Table 4. Vickers hardness test results of $C_{0.1}Cr_3Mo_{11.9}Nb_{20}Re_{15}Ta_{30}W_{20}$.

Load (gf)	Average Hardness (HV)	Standard Deviation (HV)
2000	587.10	21.56
500	595.44	21.35
100	622.60	13.05

The ML studies on mechanical and physical properties of HEAs were verified by comparing with the experiments [21–26,50–52]. The predicted Vickers hardness of $C_{0.1}Cr_3Mo_{11.9}$ Nb₂₀Re₁₅Ta₃₀W₂₀ with nominal composition and experimental composition were 695 H_V and 686 H_V, respectively. The experimentally measured Vickers hardness of $C_{0.1}Cr_3Mo_{11.9}Nb_{20}Re_{15}Ta_{30}W_{20}$ agreed with the machine learning prediction, with an error below 15%. Moreover, the calculated Vickers hardness of $C_{0.1}Cr_3Mo_{11.9}Nb_{20}Re_{15}Ta_{30}W_{20}$ was found to be 900 H_V using the rule of mixture and Chen's model [53]. This predicted value of hardness had an error % of 64, which is not reliable. The hardness predictions from the current model seem very promising because they were studied with small training datasets. The close agreements between predictions and experiments validate the reliability of the current NN model. The prediction accuracy can be further improved with sufficiently larger datasets. A similar neural NN model could be used in predicting properties of future RHEAs, such as yield strength, ductility, and tensile strength, etc.

4. Conclusions

In this study, an NN model consisting of five hidden layers was introduced and the hardness of the novel alloy $C_{0.1}Cr_3Mo_{11.9}Nb_{20}Re_{15}Ta_{30}W_{20}$ was predicted. The microstructure study showed a single BCC phase existing in $C_{0.1}Cr_3Mo_{11.9}Nb_{20}Re_{15}Ta_{30}W_{20}$. The predicted hardness of $C_{0.1}Cr_3Mo_{11.9}Nb_{20}Re_{15}Ta_{30}W_{20}$ by the NN model was 695 HV, which agreed with the experiment. The current NN method will allow researchers to synthesize virtual RHEAs to achieve the expected hardness without any experimental trial and error method. Therefore, provides a promising scope in accelerating RHEAs designs with the desired hardness.

Author Contributions: Conceptualization, U.B., C.Z. (Congyan Zhang) and S.Y.; methodology, U.B. and A.A; software, U.B; C.Z. (Congyuan Zeng), A.A.; validation, C.Z. (Congyan Zhang), S.G. and S.Y.; formal analysis, C.Z. (Congyuan Zeng), and S.G; investigation, U.B., and C.Z. (Congyan Zhang); resources, S.Y.; data curation, A.A., and U.B.; writing—original draft preparation, U.B., C.Z. (Congyuan Zeng) and S.Y; writing—review and editing, S.G. and S.Y; visualization, S.Y.; supervision, S.Y.; project administration, S.Y.; funding acquisition, S.Y. All authors have read and agreed to the published version of the manuscript.

Funding: This research was partially supported by the NSF EPSCoR CIMM project under Award No. 1541079, DOE award No. DE-NA0003979, and DoD support under contract No. W911NF1910005. CZ(Congyuan Zeng) and SG are supported by the US National Science Foundation under grant number OIA-1946231 and the Louisiana Board of Regent for the Louisiana Material Design Alliance (LAMDA). The computational simulations were supported by the Louisiana Optical Network Infrastructure (LONI) with the supercomputer allocation loni_mat_bio15 and 16.

Institutional Review Board Statement: Not applicable.

Informed Consent Statement: Not applicable.

Data Availability Statement: All data and codes used in this study will be made available upon the reasonable request to the corresponding authors.

Conflicts of Interest: The authors declare no conflict of interest.

References

- Soni, V.K.; Sanyal, S.; Sinha, S.K. Phase evolution and mechanical properties of novel FeCoNiCuMox high entropy alloys. *Vacuum* 2020, 174, 109173. [CrossRef]
- Bhandari, U.; Zhang, C.; Yang, S. Mechanical and Thermal Properties of Low-Density Al_{20+X}Cr_{20-X}Mo_{20-Y}Ti₂₀V_{20+y} Alloys. *Crystals* 2020, 10, 278. [CrossRef]
- 3. Tan, X.R.; Zhao, R.F.; Ren, B.; Zhi, Q.; Zhang, G.P.; Liu, Z.X. Effects of Hot Pressing Temperature on Microstructure, Hardness and Corrosion Resistance of Al₂NbTi₃V₂Zr High-Entropy Alloy. *Mater. Sci. Technol.* **2016**, *32*, 1582–1591. [CrossRef]
- 4. Senkov, O.N.; Scott, J.M.; Senkova, S.V.; Miracle, D.B.; Woodward, C.F. Microstructure and Room Temperature Properties of a High-Entropy TaNbHfZrTi Alloy. *J. Alloy. Compd.* **2011**, *509*, 6043–6048. [CrossRef]
- Wu, Y.D.; Cai, Y.H.; Chen, X.H.; Wang, T.; Si, J.J.; Wang, L.; Wang, Y.D.; Hui, X.D. Phase Composition and Solid Solution Strengthening Effect in TiZrNbMoV High-Entropy Alloys. *Mater. Des.* 2015, *83*, 651–660. [CrossRef]
- Han, Z.D.; Chen, N.; Zhao, S.F.; Fan, L.W.; Yang, G.N.; Shao, Y.; Yao, K.F. Effect of Ti Additions on Mechanical Properties of NbMoTaW and VNbMoTaW Refractory High Entropy Alloys. *Intermetallics* 2017, 84, 153–157. [CrossRef]
- Qiao, D.X.; Jiang, H.; Jiao, W.N.; Lu, Y.P.; Cao, Z.Q.; Li, T.J. A Novel Series of Refractory High-Entropy Alloys Ti₂ZrHf_{0.5}VNb_x with High Specific Yield Strength and Good Ductility. *Acta Metall. Sin. Engl. Lett.* 2019, *32*, 925–931. [CrossRef]
- 8. Brechtl, J.; Chen, S.Y.; Xie, X.; Ren, Y.; Qiao, J.W.; Liaw, P.K.; Zinkle, S.J. Towards a Greater Understanding of Serrated Flows in an Al-Containing High-Entropy-Based Alloy. *Int. J. Plast.* **2019**, *115*, 71–92. [CrossRef]
- 9. Bhandari, U.; Zhang, C.; Guo, S.; Yang, S. First-Principles Study on the Mechanical and Thermodynamic Properties of MoNbTaTiW. *Int. J. Miner. Metall. Mater.* **2020**, *27*, 1398–1404. [CrossRef]
- 10. Wang, Z.; Lu, W.; Raabe, D.; Li, Z. On the Mechanism of Extraordinary Strain Hardening in an Interstitial High-Entropy Alloy under Cryogenic Conditions. J. Alloy. Compd. 2019, 781, 734–743. [CrossRef]
- Malinovskis, P.; Fritze, S.; Riekehr, L.; von Fieandt, L.; Cedervall, J.; Rehnlund, D.; Nyholm, L.; Lewin, E.; Jansson, U. Synthesis and Characterization of Multicomponent (CrNbTaTiW) C Films for Increased Hardness and Corrosion Resistance. *Mater. Des.* 2018, 149, 51–62. [CrossRef]
- 12. Zhang, H.; Hedman, D.; Feng, P.; Han, G.; Akhtar, F. A High-Entropy B₄(HfMo₂TaTi)C and SiC Ceramic Composite. *Dalt. Trans.* **2019**, *48*, 5161–5167. [CrossRef] [PubMed]
- 13. Castle, E.; Csanádi, T.; Grasso, S.; Dusza, J.; Reece, M. Processing and Properties of High-Entropy Ultra-High Temperature Carbides. *Sci. Rep.* **2018**, *8*, 1–12. [CrossRef] [PubMed]
- 14. Guo, L.; Ou, X.; Ni, S.; Liu, Y.; Song, M. Effects of Carbon on the Microstructures and Mechanical Properties of FeCoCrNiMn High Entropy Alloys. *Mater. Sci. Eng. A* 2019, 746, 356–362. [CrossRef]
- 15. Huang, T.; Jiang, L.; Zhang, C.; Jiang, H.; Lu, Y.; Li, T. Effect of Carbon Addition on the Microstructure and Mechanical Properties of CoCrFeNi High Entropy Alloy. *Sci. China Technol. Sci.* **2018**, *61*, 117–123. [CrossRef]
- 16. Seol, J.B.; Bae, J.W.; Li, Z.; Han, J.C.; Kim, J.G.; Raabe, D.; Kim, H.S. Boron doped ultrastrong and ductile high-entropy alloys. *Acta Mater.* **2018**, *151*, 366–376. [CrossRef]
- 17. Lei, Z.; Liu, X.; Wu, Y.; Wang, H.; Jiang, S.; Wang, S.; Hui, X.; Wu, Y.; Gault, B.; Kontis, P.; et al. Enhanced strength and ductility in a high-entropy alloy via ordered oxygen complexes. *Nature* **2018**, *563*, 546–550. [CrossRef]
- Bagdasaryan, A.A.; Pshyk, A.V.; Coy, L.E.; Konarski, P.; Misnik, M.; Ivashchenko, V.I.; Kempiński, M.; Mediukh, N.R.; Pogrebnjak, A.D.; Beresnev, V.M.; et al. A new type of (TiZrNbTaHf)N/MoN nanocomposite coating: Microstructure and properties depending on energy of incident ions. *Compos. Part B Eng.* 2018, 146, 132–144. [CrossRef]
- Guo, N.N.; Wang, L.; Luo, L.S.; Li, X.Z.; Chen, R.R.; Su, Y.Q.; Guo, J.J.; Fu, H.Z. Microstructure and Mechanical Properties of In-Situ MC-Carbide Particulates-Reinforced Refractory High-Entropy Mo0. 5NbHf0. 5ZrTi Matrix Alloy Composite. *Intermetallics* 2016, 69, 74–77. [CrossRef]
- 20. Agarwal, A.; Rao, A.K.P. Artificial Intelligence Predicts Body-Centered-Cubic and Face-Centered-Cubic Phases in High-Entropy Alloys. *JOM* 2019, *71*, 3424–3432. [CrossRef]
- 21. Zhang, Y.; Wen, C.; Wang, C.; Antonov, S.; Xue, D.; Bai, Y.; Su, Y. Phase Prediction in High Entropy Alloys with a Rational Selection of Materials Descriptors and Machine Learning Models. *Acta Mater.* **2020**, *185*, 528–539. [CrossRef]
- Zhou, Z.; Zhou, Y.; He, Q.; Ding, Z.; Li, F.; Yang, Y. Machine Learning Guided Appraisal and Exploration of Phase Design for High Entropy Alloys. NPJ Comput. Mater. 2019, 5, 1–9. [CrossRef]
- Islam, N.; Huang, W.; Zhuang, H.L. Machine Learning for Phase Selection in Multi-Principal Element Alloys. Comput. Mater. Sci. 2018, 150, 230–235. [CrossRef]
- 24. Wen, C.; Zhang, Y.; Wang, C.; Xue, D.; Bai, Y.; Antonov, S.; Dai, L.; Lookman, T.; Su, Y. Machine Learning Assisted Design of High Entropy Alloys with Desired Property. *Acta Mater.* **2019**, *170*, 109–117. [CrossRef]
- Kim, G.; Diao, H.; Lee, C.; Samaei, A.T.; Phan, T.; de Jong, M.; An, K.; Ma, D.; Liaw, P.K.; Chen, W. First-Principles and Machine Learning Predictions of Elasticity in Severely Lattice-Distorted High-Entropy Alloys with Experimental Validation. *Acta Mater.* 2019, 181, 124–138. [CrossRef]

- 26. Gorsse, S.; Nguyen, M.H.; Senkov, O.N.; Miracle, D.B. Database on the Mechanical Properties of High Entropy Alloys and Complex Concentrated Alloys. *Data Br.* 2018, *21*, 2664–2678. [CrossRef]
- 27. Zheng, S.; Wang, S. First-Principles Design of Refractory High Entropy Alloy VMoNbTaW. Entropy 2018, 20, 965. [CrossRef]
- Zhang, Y.; Zhou, Y.J.; Lin, J.P.; Chen, G.L.; Liaw, P.K. Solid-solution Phase Formation Rules for Multi-component Alloys. *Adv. Eng. Mater.* 2008, 10, 534–538. [CrossRef]
- 29. Guo, S.; Ng, C.; Lu, J.; Liu, C.T. Effect of Valence Electron Concentration on Stability of Fcc or Bcc Phase in High Entropy Alloys. J. *Appl. Phys.* **2011**, *109*, 103505. [CrossRef]
- 30. A Practical Guide to Dimensionality Reduction Techniques. Available online: https://www.youtube.com/watch?v= ioXKxulmwVQ&ab_channel=PyData (accessed on 12 December 2020).
- 31. Kelleher, J.D.; Mac Namee, B.; D'arcy, A. Fundamentals of Machine Learning for Predictive Data Analytics: Algorithms, Worked Examples, and Case Studies; MIT Press: Cambridge, MA, USA, 2015.
- 32. McKinney, W. Python for Data Analysis: Data Wrangling with Pandas, NumPy, and IPython; O'Reilly Media Inc.: Sevastopol, CA, USA, 2012.
- 33. Maas, A.L.; Hannun, A.Y.; Ng, A.Y. Rectifier Nonlinearities Improve Neural Network Acoustic Models. Proc. ICML 2013, 30, 3.
- Juan, C.C.; Tseng, K.K.; Hsu, W.L.; Tsai, M.H.; Tsai, C.W.; Lin, C.M.; Chen, S.K.; Lin, S.J.; Yeh, J.W. Solution strengthening of ductile refractory HfMoxNbTaTiZr high-entropy alloys. *Mater. Lett.* 2016, 175, 284–287. [CrossRef]
- 35. Zhang, B.; Gao, M.C.; Zhang, Y.; Guo, S.M. Senary refractory high-entropy alloy CrxMoNbTaVW. *Calphad* **2015**, *51*, 193–201. [CrossRef]
- 36. Senkov, O.N.; Senkova, S.V.; Miracle, D.B.; Woodward, C. Mechanical properties of low-density, refractory multi-principal element alloys of the Cr–Nb–Ti–V–Zr system. *Mater. Sci. Eng. A* 2013, *565*, 51–62. [CrossRef]
- 37. Senkov, O.N.; Wilks, G.B.; Scott, J.M.; Miracle, D.B. Mechanical properties of Nb₂₅Mo₂₅Ta₂₅W₂₅ and V₂₀Nb₂₀Mo₂₀Ta₂₀W₂₀ refractory high entropy alloys. *Intermetallics* **2011**, *19*, 698–706. [CrossRef]
- Stepanov, N.D.; Shaysultanov, D.G.; Salishchev, G.A.; Tikhonovsky, M.A.; Oleynik, E.E.; Tortika, A.S.; Senkov, O.N. Effect of V content on microstructure and mechanical properties of the CoCrFeMnNiVx high entropy alloys. J. Alloy. Compd. 2015, 628, 170–185. [CrossRef]
- Chen, S.Y.; Yang, X.; Dahmen, K.A.; Liaw, P.K.; Zhang, Y. Microstructures and crackling noise of Al_xNbTiMoV high entropy alloys. Entropy 2014, 16, 870–884. [CrossRef]
- 40. Zhuang, Y.X.; Liu, W.J.; Chen, Z.Y.; Xue, H.D.; He, J.C. Effect of elemental interaction on microstructure and mechanical properties of FeCoNiCuAl alloys. *Mater. Sci. Eng. A* 2012, 556, 395–399. [CrossRef]
- 41. He, J.Y.; Liu, W.H.; Wang, H.; Wu, Y.; Liu, X.J.; Nieh, T.G.; Lu, Z.P. Effects of Al addition on structural evolution and tensile properties of the FeCoNiCrMn high-entropy alloy system. *Acta Mater.* **2014**, *62*, 105–113. [CrossRef]
- 42. Cullity, B.D. Elements of X-ray Diffraction; Addison-Wesley Publishing: Boston, MA, USA, 1956.
- 43. Trindade, V.B.; Krupp, U.; Wagenhuber, P.E.G.; Christ, H.J. Oxidation Mechanisms of Cr-Containing Steels and Ni-Base Alloys at High-Temperatures–. Part I: The Different Role of Alloy Grain Boundaries. *Mater. Corros.* **2005**, *56*, 785–790. [CrossRef]
- Tsai, S.C.; Huntz, A.M.; Dolin, C. Growth Mechanism of Cr₂O₃ Scales: Oxygen and Chromium Diffusion, Oxidation Kinetics and Effect of Yttrium. *Mater. Sci. Eng. A* 1996, 212, 6–13. [CrossRef]
- Kuhn, B.; Talik, M.; Niewolak, L.; Zurek, J.; Hattendorf, H.; Ennis, P.J.; Quadakkers, W.J.; Beck, T.; Singheiser, L. Development of High Chromium Ferritic Steels Strengthened by Intermetallic Phases. *Mater. Sci. Eng. A* 2014, 594, 372–380. [CrossRef]
- 46. Alcock, C.B.; Itkin, V.P.; Horrigan, M.K. Vapour pressure equations for the metallic elements: 298–2500K. *Can. Metall. Q.* **1984**, 23, 309–313. [CrossRef]
- 47. Uzun, O.; Karaaslan, T.; Keskin, M. Hardness Evaluation of Al-12Si-0.5 Sb Melt-Spun Ribbons. J. Alloy. Compd. 2003, 358, 104–111. [CrossRef]
- Uzun, O.; Karaaslan, T.; Gogebakan, M.; Keskin, M. Hardness and Microstructural Characteristics of Rapidly Solidified Al-8-16 Wt.% Si Alloys. J. Alloy. Compd. 2004, 376, 149–157. [CrossRef]
- 49. Xu, B.; Tian, Y. Ultrahardness: Measurement and Enhancement. J. Phys. Chem. C 2015, 119, 5633–5638. [CrossRef]
- 50. Chang, Y.J.; Jui, C.Y.; Lee, W.J.; and Yeh, A.C. Prediction of the composition and hardness of high-entropy alloys by machine learning. *JOM* **2019**, *71*, 3433–3442. [CrossRef]
- 51. Bhandari, U.; Rafi, M.R.; Zhang, C.; Yang, S. Yield strength prediction of high-entropy alloys using machine learning. *Mater. Today Commun.* **2020**, 101871. [CrossRef]
- 52. Zhao, Q.; Yang, H.; Liu, J.; Zhou, H.; Wang, H.; Yang, W. Machine learning-assisted discovery of strong and conductive Cu alloys: Data mining from discarded experiments and physical features. *Mater. Des.* **2020**, *197*, 109248. [CrossRef]
- Tian, Y.; Xu, B.; Zhao, Z. Microscopic theory of hardness and design of novel superhard crystals. *Int. J. Refract. Met. Hard Mater.* 2012, 33, 93–106. [CrossRef]