

Efficient Direct Recycling of Degraded LiMn_2O_4 Cathodes by One-Step Hydrothermal Relithiation

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Abstract

Due to the large demand of lithium-ion batteries (LIBs) for energy storage in daily life and the limited lifetime of commercial LIB cells, exploring green and sustainable recycling methods becomes an urgent need to mitigate the environmental and economic issues associated with waste LIBs. In this work, we demonstrate an efficient direct recycling method to regenerate degraded lithium manganese oxide (LMO) cathodes to restore their high capacity, long cycling stability and high rate performance, on par with pristine LMO materials. This one-step regeneration, achieved by a hydrothermal reaction in dilution Li-containing solution, enables reconstruction of desired stoichiometry and microphase purity, which is further validated by testing spent LIBs with different state of health (SOH). Life-cycle analysis suggested the great environmental and economic benefits enabled by this direct regeneration method compared with today's pyro- and hydrometallurgical processes. This work not only represents a fundamental understanding of the relithiation mechanism of spent cathodes but also provides a potential solution for sustainable and closed-loop recycling and re-manufacturing of energy materials.

Keywords: lithium-ion batteries, recycling, direct regeneration, lithium manganese oxide, life-cycle analysis, sustainability

Introduction

Among the state-of-art energy storage technologies, lithium-ion batteries (LIBs) have dominating applications in portable electronics, electric vehicles (EVs), and stationary energy storage^{1, 2}. The LIB industry has experienced a revolutionary development in the last decade with remarkable performance improvements, satisfying many key performance requirements such as high energy density, high power density, good cycling stability³. The global market of LIB expands dramatically as result of the significant growth in xEV market recent years, representing more than 180 GWh of worldwide LIB sales in 2018. Considering the limited service life for EVs applications (about 8-10 years) and the environmental impact of inappropriate battery disposal, there is an urgent need to develop efficient and sustainable methods for recycling/regenerating the materials out of spent LIBs^{4, 5}.

The state-of-the-art approaches in LIB recycling industry are mainly based on hydrometallurgical and pyrometallurgical processes^{6, 7}. Both methods involve energy-intensive or caustic processes such as sintering, acid leaching and chemical precipitation, which are unavoidably associated with heavy CO₂ emission and other waste generation^{8, 9}. These methods can be viable in processing Co-containing LIBs since the value of Co product (*e.g.*, CoSO₄) may compensate for the high operation cost. However, for many other LIBs, such as LiMn₂O₄ (LMO) batteries, the low intrinsic value of their elemental components (*e.g.*, Mn) poses huge challenges for recycling via traditional ways¹⁰. Nevertheless, such low-cost batteries offer unique properties for many applications. For example, LMO is an appealing cathode material due to its high thermal stability and low cost. These features make it attractive for low-cost EVs and large-scale energy storage.

On the other hand, direct regeneration without a destructive high-temperature smelting and acid leaching process is attracting considerable attentions, as it can potentially provide a cost-reduction and environment-benign solution for recycling useful materials from spent batteries. Various methodologies have been demonstrated for direct regeneration of layered oxide cathode, such as LiCoO₂ (LCO) and LiNi_xCo_yMn_zO₂ (or NCM, $x+y+z=1$). These include electrochemical treatment¹¹, hydrothermal relithiation¹², ionothermal lithiation¹³, molten salt relithiation¹⁴ and solid-state sintering¹⁵ approaches. For example, Yang *et al* have recently demonstrated a direct regeneration method of NCM, with the first discharge capacity of 158 mAh/g and the retention of 77.8% after 100 cycles at 1C via combining hydrothermal treatment and short-annealing process¹⁶. Tao *et al* successfully regenerated spent NCM via a cost-effective Li halide as Li source in ionic liquids with the advantages of low vapor pressures¹³.

Jianlin *et al* provide a promising improvement on treating the spent NCM by water process that avoids the usage of N-methyl-2-pyrrolidone (NMP)¹⁷. In spite of successful demonstration on direct regeneration of LIBs containing high-value transition elements (e.g. Co, Ni), only a few studies have been done on regenerating cathodes with low cost such as LMO^{18, 19}. The direct recycling by extraction valuable element via supercritical carbon dioxide (CO₂) has been demonstrated to be costly and not worthy in the case of LMO batteries²⁰.

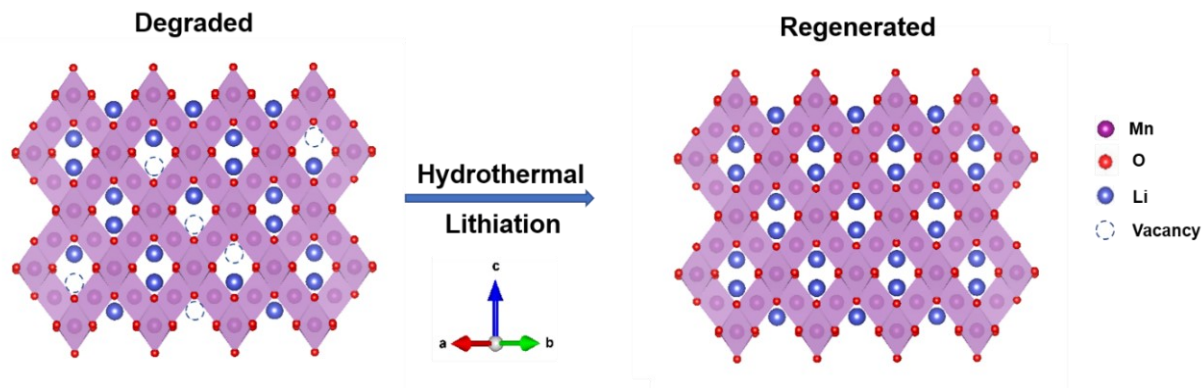


Figure 1. Illustration of the hydrothermal lithiation process in which Li^+ are re-dosed to the Li-deficient sites to recover its desired stoichiometry.

By leveraging the knowledge established in developing various synthesis methods for spinel cathode materials²¹⁻²³, in this work, we demonstrated an one-step direct regeneration method to effectively recycle spent LMO cathodes, which showed successful reconstruction of stoichiometric composition and restored crystallinity from severely degraded LMO cathode materials with different state of health (SOH). Specifically, we used a hydrothermal treatment with dilute lithium hydroxide (LiOH) solution to simultaneously relithiate degraded LMO particles and heal the microstructure defects. **Figure 1** illustrates the relithiation process highlighting the migration of lithiation inside the spinel structure along (110) direction during hydrothermal process. The reasons for capacity fading have been investigated in the last decade, which are mainly ascribed to Li loss²⁴, Mn migration²⁵ and John-Tell distortion^{26, 27}. By tuning the operation conditions, the composition and structure evolution of LMO during the regeneration process was systematically investigated via various physicochemical characterizations. The study on the kinetic mechanism combined with neutron diffraction indicates that the lithium loss and lattice distortion can be fully recovered to the original levels of the pristine materials. This work provides a new direction towards cost-effective and environment-friendly battery recycling to potentially address the sustainability issues related to LIBs.

Experimental Section

Commercial level pouch cell assembly. Dry pouch cells (500 mAh) made with lithium manganese oxide (LMO) as cathode active materials and graphite as anode active materials were directly supplied from Guangdong Canrd New Energy Technology Co., Ltd, China. The electrolyte was battery grade lithium hexafluorophosphate (LiPF_6) solution in ethylene carbonate (EC) and dimethyl carbonate (DEC) purchased from Sigma-Aldrich, with the composition of 1.0 M LiPF_6 in EC/DEC=50/50 (v/v) (LP40). The dry pouch cells were filled by 1 mL of electrolyte and sealed by the vacuum sealer machine (MTI Corp.) inside the glove box. After 24 h standing time, the pouch cells were activated in the voltage window of 3-4.3V by C/10 (50 mA) ($1C=148\text{ mA/g}$) under constant current - constant voltage (CC-CV) cycling with the cut-off current at C/20 (25 mA). The activated pouch cells were cycled between 3.0-4.3V at 1.5 C (750 mA) for 40 cycles, then 0.5C (250 mA) for other 160 cycles.

Homemade single-layer pouch cell assembly. Single-layer LMO-graphite pouch cells were also built in our lab to investigate the lithium distribution in the cycled cells. The pristine LMO powders (MTI Corp.) were mixed with polyvinylidene fluoride (PVDF, KYNAR 2800) and carbon black (Super P65) in NMP (Sigma-Aldrich, anhydrous, 99.5%) at a mass ratio of 8: 1: 1 to form homogeneous slurries. The slurries were casted by a doctor blade and then dried under vacuum at room temperature for 2 h followed by drying at 80 °C for 6 h. After rolling, the cathodes were cut into 4.4 cm x 5.7 cm with a mass loading of 6.8 mg/cm^2 . The pre-baked graphite (Graphite & Carbon Products, G80) was mixed with PVDF and Super P65 in NMP at a mass ratio of 90:5:5. The slurries were casted by a doctor blade and then dried under vacuum at 80 °C for 6 h. After rolling, the anodes were then cut into 4.5 cm*5.8 cm with a mass loading of 3.7 mg/cm^2 . After matching the electrodes under controlled N/P ratio (1.1-1.15), single layer pouch cells were assembled with a tri-layer membrane (Celgard 2320) as the separator and 500 ul of LP40 as the electrolyte. All the home-made pouch cells were activated in the voltage window of 3-4.3V at C/10 under CCCV cycling with the cut-off current of C/20. The cells were cycled between 3.0-4.3V at C/2 under CCCV with the cut-off current C/5 for 200 cycles.

Cathode materials harvesting. All the pouch cells were discharged to 2.8V before disassembly. The cathode strips were harvested from both the commercial and home-made pouch cells, by thoroughly rinsing with dimethyl carbonate (DMC) and then soaked in NMP for 6h under 50 °C. The active materials, binder and carbon black were removed from the aluminum substrates by sonification and scrapping. After centrifuging the NMP suspension at 3500 rpm for 5 min, active materials were precipitated. The precipitation was

washed several times by NMP. Then the active materials were collected and dried under vacuum at 80 °C overnight for regeneration.

Regeneration of cathode materials. For the hydrothermal treatment, 0.25g of cycled LMO materials were added into a 100 ml of Teflon-lined autoclave filled with 80 ml of lithium hydroxide (LiOH) solution with different concentrations. The autoclaves were consistently heated at 180 °C for different periods of time. After cooling down naturally till room temperature, the treated powders were washed by deionized water for at least 5 times till pH ~7, and then dried under vacuum at 80 °C overnight.

Characterization of regenerated materials. The compositions of cycled/regenerated LMO cathode materials were measured by an Inductively-coupled plasma quadrupole mass spectrometer (ICP-MS, Thermo Scientific™, iCAP™ RQ model). Their crystal structures were examined by X-ray powder diffraction (XRD) employing a Bruker D2 Phaser (Cu K α radiation, $\lambda=1.5406$ Å) from scanning rate of 0.58 deg/min.

Time-of-flight (TOF) powder neutron diffraction was measured at the VULCAN instrument at the Spallation Neutron Sources (SNS), Oak Ridge National Laboratory (ORNL)²⁸. The diffraction pattern was measured at the detector banks at $2\theta = \pm 90^\circ$, equipped 5 mm receiving collimators. Neutron powder diffraction patterns were collected in the high intensity mode ($\Delta d/d \sim 0.45\%$) for a duration of 2 h under the nominal 1.4 MW SNS operation, and then processed using VDRIVE software²⁹. Rietveld refinement against the neutron diffraction was performed using General Structure Analysis System (GSAS) software with EXPGUI interface^{30, 31}.

The morphology of the pristine, cycled and regenerated LMO powder was observed by Scanning Electron Microscope (SEM, FEI XL30). The particle size distribution was analyzed with the Nano Measurer software. The microstructures of the regenerated LMO powder were further confirmed by high resolution transmission electron microscopic (HR-TEM) images which were collected on JEOL-2800 at 200 kV with a Gatan OneView Camera (25 fps, full 4K resolution). The detailed structure information was measured by DigitalMicrograph (DM). X-ray photoelectron spectroscopic (XPS) measurement was conducted with an AXIS Supra by Kratos Analytical with Al K α anode source working at 15 kV and 10^{-8} Torr chamber pressure. The spectra data were processed by CasaXPS software. All spectra were calibrated with the hydrocarbon C 1s peak at 284.6 eV. The XPS depth profile analysis was carried out with a gas cluster ion source (GCIS) using focused energetic Ar ion beam.

Analysis of lithium distribution in cycled pouch cells. After cycling at 0.5C under CCCV with a cut-off current of 0.1C for 200 cycles, the home-made pouch cells were disassembled in glove box. 10 μ l of electrolyte was collected by a pipette and diluted into 10 ml of DMC. The anodes were rinsed by DMC for 2 h and then soaked in 1M HCl for 3 days. The cathode active materials were collected by the same method as harvesting commercial pouch cells described above. The compositions of electrolyte, anode electrodes and cathode electrodes were measured by ICP-MS.

Electrochemical characterization. The active materials were mixed with PVDF, and Super P65 in NMP at a mass ratio of 8:1:1. Then the formed slurries were casted on an aluminum foil using a doctor blade and dried in vacuum at 80 °C for 6 h. The LMO cathodes were cut and compressed by rolling. The areal mass loading of LMO electrodes for coil cells were around 10 mg/cm². Coin cells were assembled with a Li metal disc (thickness 1.1 mm) as the counter electrode, LP40 as the electrolyte, and a tri-layer membrane (Celgard 2320) as the separator. Galvanostatic charge-discharge was carried out using a Neware battery testing system in the potential range of 3.0-4.3 V at 0.5C for 200 cycles after C/10 in the initial cycle and 0.3C in the following two cycles.

Results and Discussion

Both commercial and home-made pouch cells were used for the demonstration of our direct recycling approach. The details for assembling different pouch cells were described in the experimental section (Supporting Information). All the pouch cells were cycled in the voltage window of 3.0-4.3V until more than 20% capacity degradation was obtained (**Figure S1**). The LMO cathode materials were collected and purified by a typical procedure developed in our previous work¹⁵. The obtained cathode particles with composition and structure degradation were subject to the hydrothermal treatment (denoted as “HT”) under different conditions. The regenerated cathode particles were carefully characterized and made into new cells to evaluate the electrochemical performance. We first analyzed the cell components to identify the sources of capacity degradation associated with composition changes. For more quantitative analysis, home-made LMO/graphite single layer pouch cells with controlled cathode mass were used to investigate the Li distribution in degraded cells under room temperature. After 200 cycles in a voltage range of 3.0-4.3 V at 0.5C, 20% capacity fading appeared in our home-made pouch cells (**Figure S2**). The causes of capacity loss of the full cell are complicated, including the SEI formation on anode surface, lattice distortion caused by John-Tell effect²⁷, Mn (II) dissolution induced by Mn(III) disproportion^{32, 33}. To

identify the Li distribution, the graphite and LMO electrodes from cycled LMO pouch cell were immersed in diethyl carbonate (DEC) solution separately to wash out the residual electrolyte. Then the anode and cathode active materials were scratched off their current collectors and soaked the into hydrochloric acid to extract metal elements. A complete analysis was conducted to investigate the distribution of Li coming from the cathode side. **Figure S3** shows that 82.6% of Li was retained inside the degraded spinel cathode particles, 13.5% of Li in anode where the consumption of Li was likely associated with the formation of thick SEI during long-term cycling³⁴. Interestingly, 0.8mM Mn was detected in 1M LiPF₆ EC/DEC electrolyte. In William's work, the same level of Mn concentration was detected after the LMO powders were exposed to electrolyte. Although the appreciable Mn dissolution may cause the structure degradation, the overall loss of Li dominates the capacity fading compared with the small amount of Mn loss in the cathodes³⁵. Thus, compensation of the Li loss is a critical step to fix the degradation issues of LMO cathode for regeneration. The compositions of cycled and regenerated LMO cathode materials were measured by an inductively coupled plasma quadrupole mass spectrometer (ICP-MS) (**Table 1**). Note that the imperfect stoichiometry from the composition of commercial LMO particle are often designed for the extension of cycle life and the oxygen defects are caused by their high temperature sintering process³⁶. The cycling data of commercial pouch cells (**Figure S1**) shows that the capacity loss was more than 20% after 200 cycles under room temperature. Composition data in **Table 1** shows that the cathode material had 13% of Li loss compared with the pristine LMO even though the cells were discharged at cut-off voltage at 3.0 V.

To design an optimal regeneration process, we first investigated the relithiation kinetics during the hydrothermal treatment process in 0.1M LiOH at 180°C (**Figure 2a**). **Table S1** reveals that the Li composition can reach to the pristine level (*e.g.*, 1.06 Li per Mn) after being treated for 6h. Further extending the treatment time up to 12h does not cause continuous increase of Li concentration in the solid LMO particles, which was confirmed by the refinement XRD (**Figure 2b-d**). In addition, cell

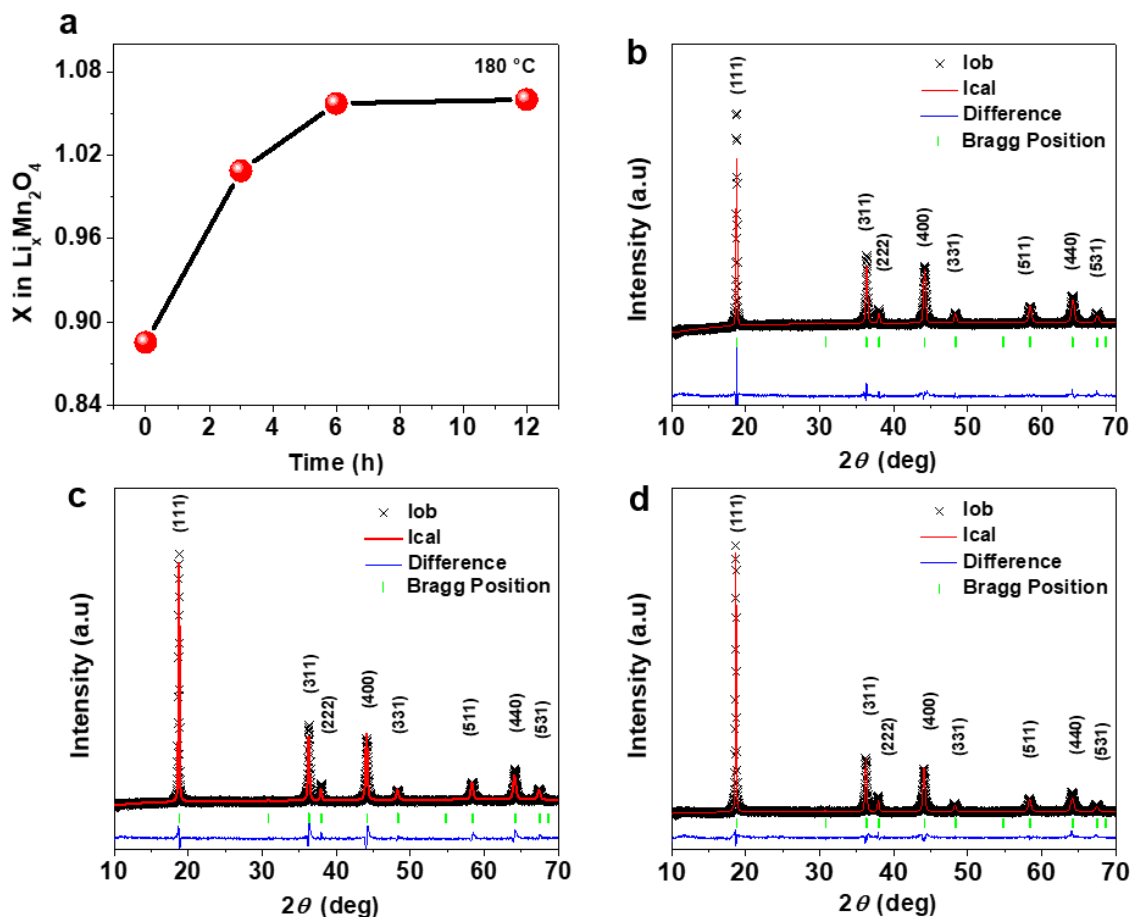


Figure 2 (a) Lithiation kinetics of degraded LIB cathode particles during hydrothermal treatment. The LMO sample regenerated in 0.1M of LiOH was named as HT-3h-LMO, HT-6h-LMO and HT-12h-LMO, respectively. Refined XRD pattern of regenerated LMO particles. (b) HT-3h LMO (c) HT-6h LMO (d) HT-12h LMO.

cycling performance (**Figure S4**) indicate that 12h treatment sample has been regenerated to the commercial reusable LMO cathode (to be discussed subsequently), which maintains high crystallinity and pure single phase.

Concentration of Li^+ in the hydrothermal solution is also an important parameter determining the relithiation behavior. With the concentration of LiOH solution changed from 0.02M to 0.2M, the degraded LMO particles can be fully recovered to reach the desired stoichiometry (~ 1.0 Li per Mn) at 180°C for 12h. As shown in **Table 1**, the composition of the regenerated LMO is sensitive to the concentration of the LiOH solution. When the LiOH concentration reached 0.4M, more Li^+ can be

inserted into the lattice forming lithium-rich Li_2MnO_3 phase, as shown in **Figure 3a** with the increased intensity of impurity peaks at 18.8, 37.0 and 44.8 degree (marked by star). These peaks are in perfect match with (001), (130) and (131) peaks of the C2/m layered phase of Li_2MnO_3 ^{37, 38}.

Table 1. Lattice parameters and ICP results of the pristine, cycled, and regenerated LMO particles. The LMO sample regenerated in 0.02, 0.1 and 0.2M of LiOH for 12h was named as 0.02M HT-LMO, 0.1M HT-LMO and 0.2M HT-LMO, respectively.

Sample	a/Å	$R_{wp}/\%$	$R_p/\%$	Composition
Pristine LMO	8.2275(2)	3.93	2.05	$\text{Li}_{1.058}\text{Mn}_{1.951}\text{O}_{3.932}$
Cycled LMO	8.1930(4)	3.53	1.90	$\text{Li}_{0.885}\text{Mn}_{1.943}\text{O}_{3.942}$
0.02M HT-LMO	8.2218(3)	3.51	3.00	$\text{Li}_{1.033}\text{Mn}_{1.945}\text{O}_{3.939}$
0.1M HT-LMO	8.2272(2)	3.39	2.63	$\text{Li}_{1.060}\text{Mn}_{1.942}\text{O}_{3.944}$
0.2M HT-LMO	8.2274(3)	2.76	1.65	$\text{Li}_{1.067}\text{Mn}_{1.933}\text{O}_{3.944}$

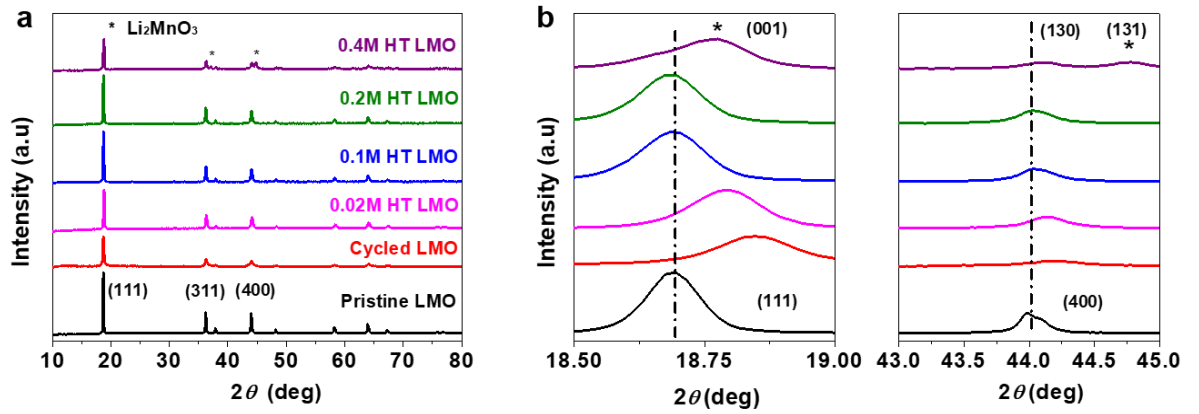


Figure 3. XRD patterns of pristine, cycled, and regenerated (a) LMO particles by hydrothermal treatment under 0.02M, 0.1M, 0.2M and 0.4M LiOH solution; (b) enlargement of the regions in the range of 18.5-19.0° and 43-45 °.

It is also critical to further investigate the evolution of the crystal structure of degraded LMO during the hydrothermal reaction. X-ray diffraction (XRD) patterns of cycled, pristine and regenerated LMO are shown in **Figure 3**. The standard pattern of spinel phase with $Fd\bar{3}m$ space group was validated in all samples³⁹. Although no additional impurity peaks exist, the peaks became broader and less intense in

cycled LMO compared to pristine LMO. A shift of the major (111) spinel peaks to higher angles can also be clearly found in **Figure 3b**, corresponding to the lattice parameter shrinkage from 8.23 Å to 8.19 Å. It indicates that, although the spinel structure was retained, the more Li^+ removed from their tetrahedral sites, the more decrease of unit-cell dimension are observed⁴⁰. Thus, it is reasonable that the extent of Li^+ loss can be reflected on the right shift of (111) peaks which allows us to validate the effectiveness of our regeneration method. For example, after hydrothermal treatment in 0.1M LiOH for 12h, the (111) peak shifts back to lower angles and with intensity recovered to the pristine level. These results suggest the successful reconstruction of the crystal structure and high crystallinity of the regenerated LMO product.

Table 2. Neutron diffraction refinement results of pristine, cycled, and regenerated LMO.

Sample	a/Å	Mn-O bond length/Å	Oxide State	Composition
Pristine LMO	8.2307(2)	1.954	+3.52	$\text{Li}_{1.058}\text{Mn}_{1.942}\text{O}_{3.944}$
Cycled LMO	8.1955(2)	1.943	+3.60	$\text{Li}_{0.896}\text{Mn}_{1.942}\text{O}_{3.944}$
0.1M HT-LMO	8.2280(3)	1.953	+3.54	$\text{Li}_{1.066}\text{Mn}_{1.934}\text{O}_{3.952}$

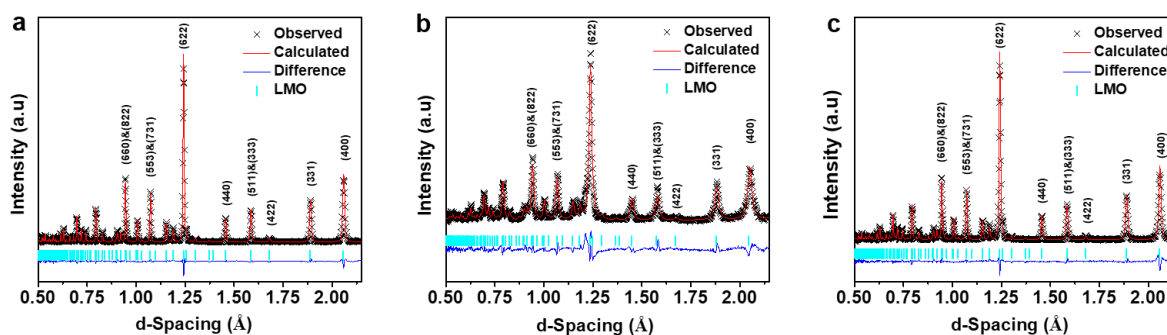


Figure 4. Rietveld refinement results of neutron diffraction patterns of (a) pristine, (b) cycled, and (c) regenerated LMO particles from 0.1M of LiOH.

Rietveld refinement was performed on all the XRD patterns using the General Structure Analysis System (GSAS) software (**Figure S5**). Both R_B (Bragg factor) and R_{wp} (weighted profile R -factor) are less than 5% which indicates the reliability of the refinement results. The lattice parameters of all the samples are compared in **Table 1**. The results further validate that not only the Li loss is compensated but also the structure can be repaired after simple hydrothermal treatment. For the purpose of demonstration,

hydrothermal relithiation with 0.1M of LiOH at 180 °C for 12 h was selected to treat the degraded LMO cathode particles for the next step.

To further quantify the occupancy of Li sites inside the lattice, neutron diffraction measurement was conducted on the pristine, cycled, and regenerated LMO from 0.1M of LiOH (**Figure 4**). As we expected, it evidently indicates that Li, Mn and O are located on the 8a (tetrahedral), 16d (octahedral), and 32e Wyckoff sites, respectively^{41, 42}. The Rietveld refinement results are listed in **Table 2**. The average Mn oxidation state increased from 3.52 to 3.60 during the long-term cycling because the Li vacancies appear inside the spinel lattice. After hydrothermal treatment, the average Mn oxidation state decreased back to 3.54 and the lattice parameter of face-centered cubic (FCC) conventional unit cell increased from 8.1955(2) Å to 8.2280(3) Å due to the complement of Li into the vacancies. The decrease of Mn-O bond length in cycled LMO is ascribed to the reduction of Mn radius, whereas the radius of Mn⁴⁺ (0.530 Å) is smaller than that of Mn³⁺ ion (0.645 Å)⁴³. After regeneration, the bond length was resumed to the pristine value. In addition, the changes of the composition were also consistent with the structure parameters (**Table 2**), which further confirms that the degraded LMO cathode was successfully regenerated in 0.1M LiOH solution.

The SEM images and size distribution of the pristine, cycled and regenerated LMO particles are displayed in **Figure S7**. The pristine LMO sample has random particle morphology with peak sizes of about 1.2 µm. After long term cycling, the peak size of LMO particles increased to 1-2 µm possibly due to aggregation. After hydrothermal treatment, the spent LMO particles become more uniform and maintain a narrow distribution similar to the pristine LMO sample. To obtain more insights in the microstructure, the regenerated cathode materials were carefully examined by high-resolution transmission electron microscope (HRTEM) (**Figure 5a-b**). The interplanar spacings of regenerated LMO were measured to be 0.48 nm and 0.25 nm, which corresponds to the orientation of (111) and (311) atom plane found in typical LMO, respectively⁴⁴⁻⁴⁶. The fast Fourier transform (FFT) patterns are indexed to the diffraction of the <011> and <010> zone axes⁴⁷. Thus, the HRTEM images also confirm the reconstruction of the spinel structure in the regenerated LMO. Additional HRTEM images of cycled LMO particles in the surface and bulk regions are shown in **Figure S8**.

X-ray photoelectron spectroscopic (XPS) measurement was performed on cycled and regenerated LMO to investigate the changes of the valence status (**Figure 5c-d**). Peak fitting was conducted on the Mn 2p_{3/2} spectrum to provide detailed distribution of the valence information of Mn in both samples (**Table**.

S2&S3) ^{48, 49}. **Figure 5c** shows a board shoulder in the region of high bonding energy, which can be ascribed to the high Mn^{4+} composition. **Figure 5d** shows a clear shoulder in low bonding energy region indicating the Mn^{3+} contribution. Quantitative analysis reveals that 51.7% and 48.3% of Mn can be assigned to Mn^{3+} Mn^{4+} , respectively, in the regenerated cathode, which is in good agreement with the valence distribution of Mn in typical LMO. By comparison, 34.9% Mn^{3+} and 65.1% Mn^{4+} were found in cycled cathode. The increase of the average valence state of Mn can be attributed to the Li loss inside lattice. Therefore, the more dominant contribution of Mn^{4+} in the cycled cathodes and its disappearance in regenerated cathodes further support that the Li-deficient spinel phases formed after cycling was recovered into well-defined, less defective structure after regeneration.

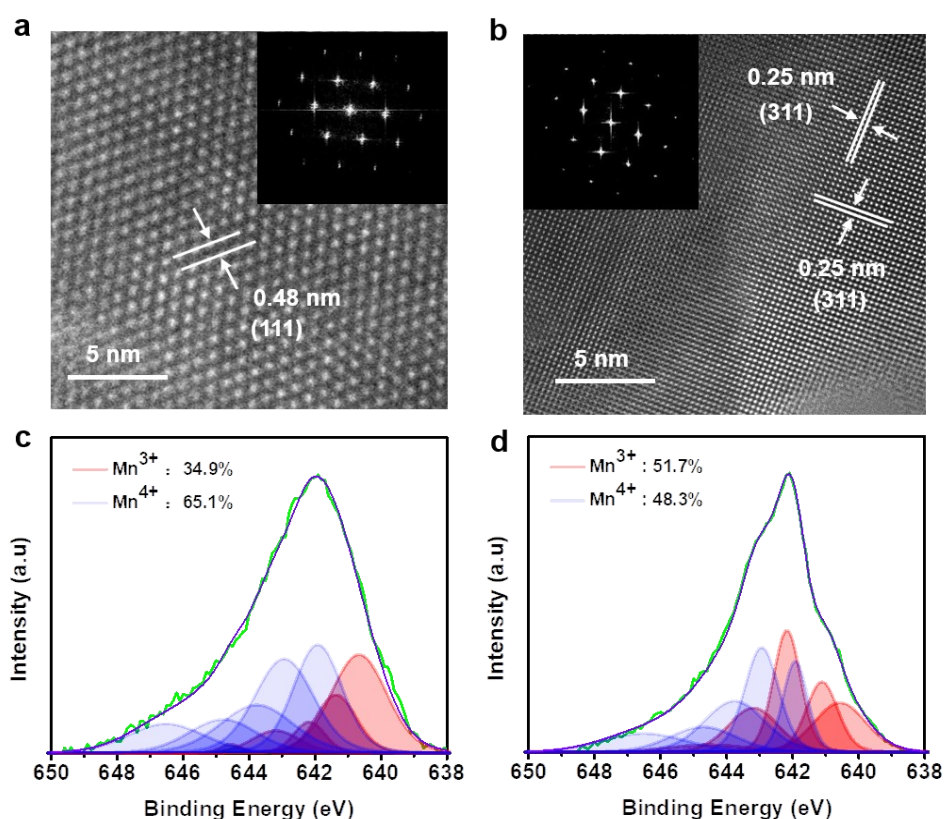


Figure 5. (a) HRTEM images and FFT patterns of regenerated LMO particles in the bulk region and (b) surface region. (c) XPS spectra of cycled LMO and (d) regenerated LMO particles.

To evaluate the electrochemical performance of the pristine, cycled and regenerated LMO samples, galvanostatic charge/discharge test was conducted in a voltage range of 3.0-4.3 V. To compare the different electrochemical performance achieved with LMO regenerated in LiOH solution with different concentrations, differential capacity plots (dQ/dV) at the first cycle at 0.1C were also acquired (**Figure**

6a). Unlike the broad peak of 0.02M regenerated sample, the LMO regenerated in 0.1M of LiOH displayed sharp intrinsic reduction peaks at 4.16 V and 4.03 V (labeled as R₁ and R₂) and oxidation peaks at 4.11 V and 3.97 V (labeled as O₁ and O₂), which can be ascribed to the two-step mechanism of the electrochemical Li⁺ intercalation and extraction from tetrahedral sites in spinel structure^{50, 51}. The peak separations between charge and discharge scan are 57 mV and 61 mV, respectively, which is good indication of high reversibility of the electrochemical reaction, with small polarization and favorable reaction kinetics⁵².

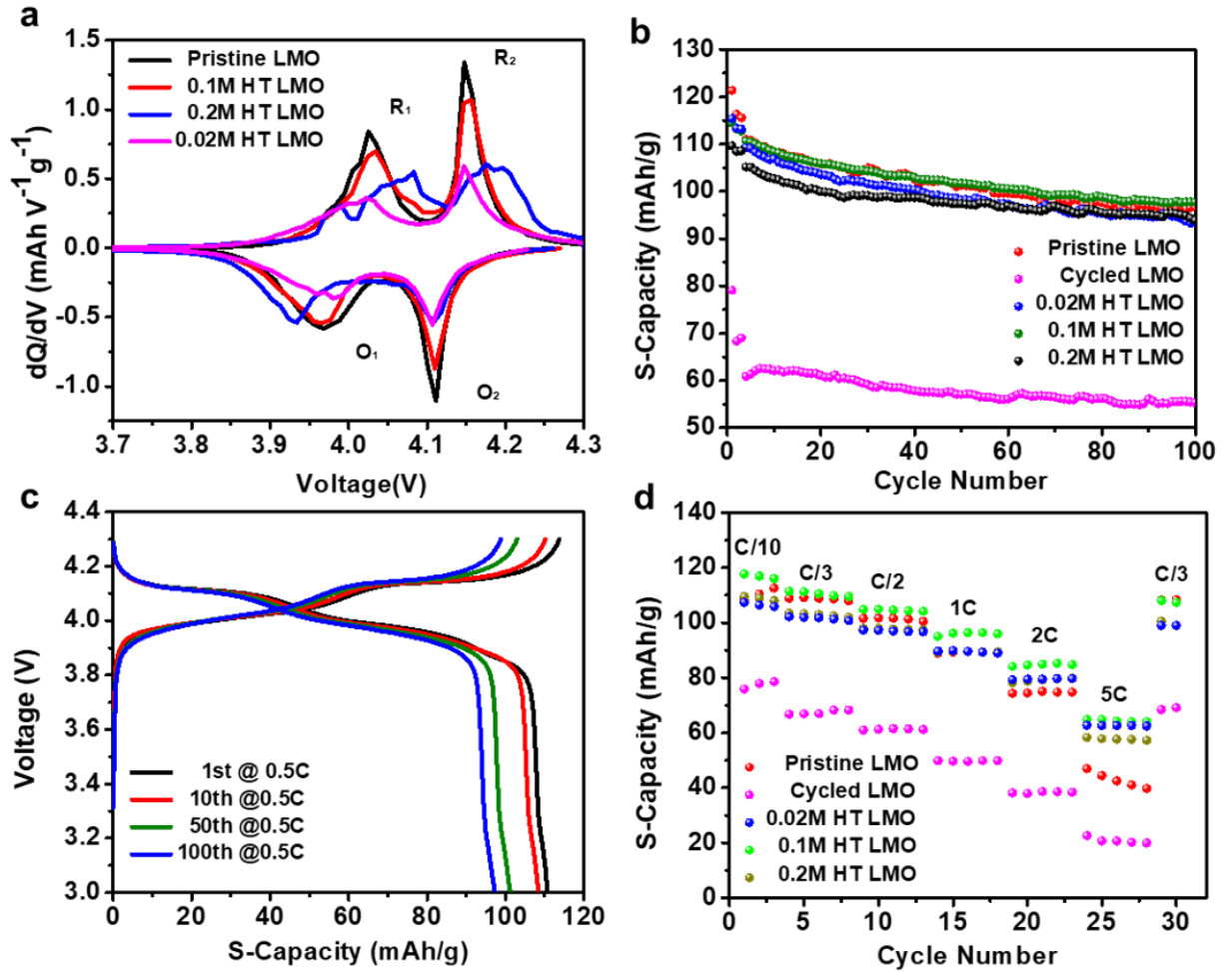


Figure 6. (a) dQ/dV plots of pristine and regenerated LMO samples at 0.1C. (b) Cycling performance of pristine, non-treated and regenerated LMO samples at 0.5C; (c) Charge/discharge curve of LMO regenerated in 0.1M of LiOH at the 1st, 10th, 50th and 100th cycle at 0.5C. (d) Rate performance of different LMO samples. HT-LMO: hydrothermal treatment at 180 °C for 12 h in LiOH solution with different concentrations.

For LMO regenerated from 0.2 M of LiOH, two tiny split peaks were obtained instead of only one reduction peak (R_1), indicating the unexpected side reaction at the initial activation cycle. It also caused a relatively lower initial columbic efficiency (82%) compared with 90% of LMO obtained in 0.1M LiOH. Furthermore, the larger peak separation suggests more severe polarization and poorer reversibility.

As shown in **Figure 6b**, the pristine LMO cathode showed a discharge capacity of 112 mAh/g at the first cycle at 0.5C ($1C = 148$ mAh/g) and 97 mAh/g after 100 cycles, corresponding to a capacity retention of 86.6%. The cycled LMO cathode (harvested from spent cells without any treatment) showed a discharge capacity of only 61 mAh/g at first cycle at 0.5C and 55 mAh/g after 100 cycles, which is expected again due to the Li^+ loss and irreversible lattice distortion. By hydrothermal treatment at 180 °C for 12 h, the electrochemical properties were fully recovered: a discharge capacity of 109, 111 and 105 mAh/g at the first cycle at 0.5C and 94, 98 and 94 mAh/g after 100 cycles were obtained by LMO treated in 0.02, 0.1 and 0.2M LiOH, respectively. In addition, the cycling stability of LMO was also recovered. For example, with the hydrothermal treatment in 0.1M LiOH solution, the cycling stability of regenerated LMO was fully recovered to 88% capacity retention after 100 cycles, which was slightly improved even compared with the pristine LMO. Interestingly, both LMO samples obtained in 0.02M and 0.2M LiOH showed slightly lower initial capacity compared with the sample regenerated in 0.1M LiOH solution. That can be ascribed to the remaining Li deficiencies in 0.02M HT LMO and phase impurity in 0.2M HT LMO samples, which is consistent with the structure information described earlier.

In addition, compared with cycled LMO and LMO regenerated in 0.1M of LiOH, the sharp peak indicates that the well-defined spinel structure with remarkable electrochemistry activity and high crystallinity was obtained by 0.1M HT treatment. Two distinguished plateaus in the charge/discharge curves at 1st, 10th, 50th and 100th cycles are shown in **Figure 6c**, corresponding to two sharp peaks in differential capacity plots (**Figure 6a**), indicating the good cycling and crystalline stability⁵³. The rate performance of the pristine, cycled and regenerated LMO cathodes materials is shown in **Figure 6d**. The 0.1M HT LMO showed an improved capacity at high rates compared with pristine LMO particles. For example, the 0.1M HT LMO electrode delivered a specific capacity of, 95, 84 and 65 mAh/g at 1, 2, and 5C ($1C = 1.48$ mA/cm²) respectively, in contrast to 89, 74, and 47 mAh/g for the pristine LMO. It indicates that hydrothermal treatment can eliminate the lattice defects and enhance the lithium diffusion kinetics inside the cycled and commercial particles⁵⁴.

Considering that spent LMO cells may have different SOHs, we also examined our regeneration approach using cells with a much higher degree of degradation. For example, a cell with 60% of capacity fading was obtained by cycling in a voltage range of 3.0-4.3V for 500 cycles. Using the same regeneration protocol developed above, LMO cathode with Li deficiency of up to 40% was fully recovered to the desired stoichiometry, which was supported by the compositions of cycled and regenerated LMO particles as shown in **Table S4**. In addition, the undesired Li deficient phases were also converted back to the original spinel phase with the efficient relithiation process. Similar to the other samples, the electrochemical performance was also resumed to the same level of pristine LMO cathodes (**Figure S6**). The successful demonstration of direct regeneration of heavily degraded LMO cathode strongly suggests that our developed method can be applied to different cases of spent LMO cells.

Compared with traditional pyrometallurgical recycling and hydrometallurgical recycling, our direct regeneration method for closed-loop LMO recycling shows potential economic and environmental benefits, which were analyzed by the EverBatt model developed by Argonne National Laboratory⁵⁵ (see detailed methods in Supporting Information).

In this model, by assuming 10,000 tons of spent LMO batteries annual processing capacity, the life-cycle analysis of the three different recycling methods was performed in terms of energy consumption, greenhouse gas (GHG) emission, operation cost and overall profit. The flow chart for each recycling process was mentioned in **Figure S9-11**. In the pyrometallurgical process, the high-temperature smelting process not only consumes a large amount of energy but also generates exhaust gas. The following gas treatment process is necessary but expensive^{56, 57}. In the hydrometallurgical process, most of the energy use comes from the upstream production of the strong acid/base/ consumed for leaching and precipitation treatment. **Figure 7a** shows that a total energy consumption of 18.5 and 30.7 MJ per kg of spent cells is required in pyrometallurgical and hydrometallurgical process, respectively. By comparison, the total energy consumption for direct recycling is only 4.1 MJ per kg of spent cells. Consistently, high GHG emission values generated from burning fuels in both pyro- and hydrometallurgical processes (**Figure 7b**). In comparison, our direct regeneration process only accounts for around 20% of the GHG emission caused in the two traditional methods.

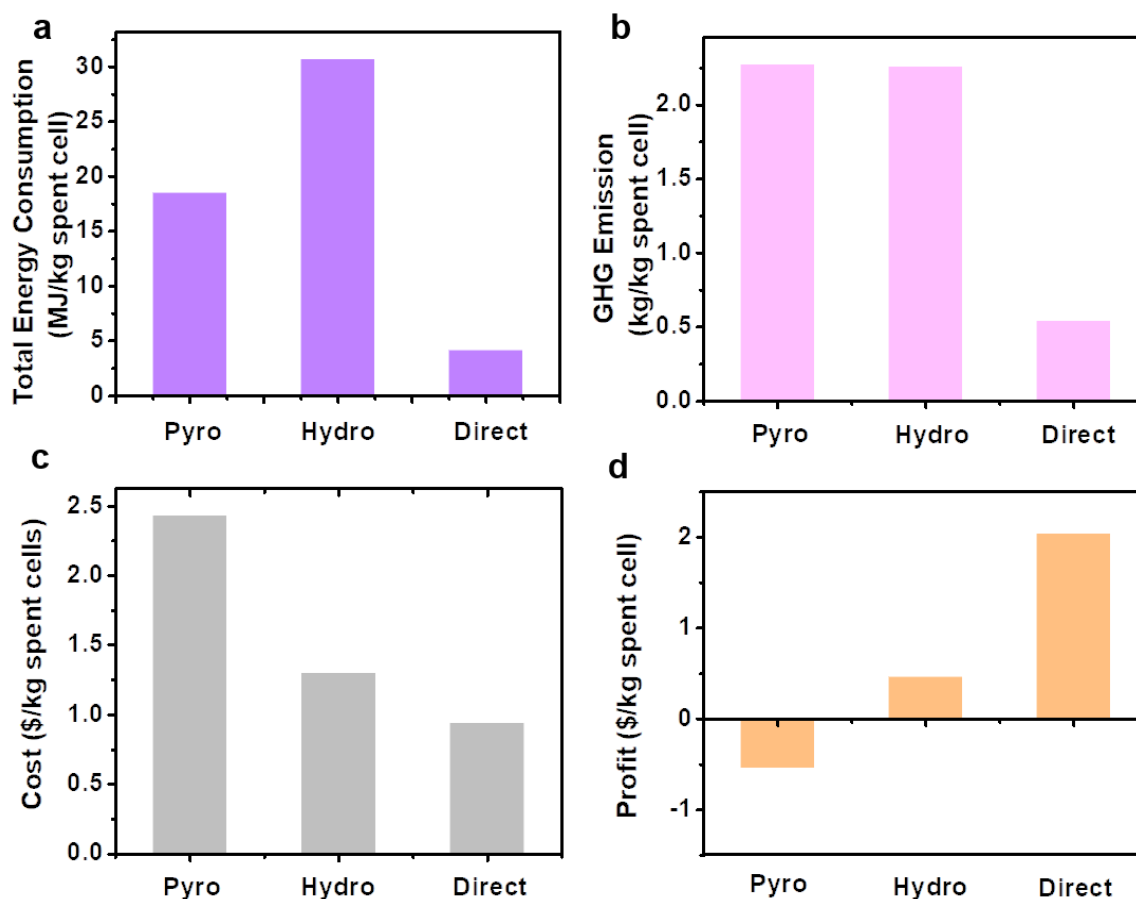


Figure 7. Life-cycle analysis based on EverBatt model. (a) Total energy consumption and (b) GHG emissions per kg of recycled cells from pyrometallurgical, hydrometallurgical and direct recycling, respectively. (c) Recycling cost and (d) Profit per kg of spent LMO batteries obtained from pyrometallurgical, hydrometallurgical and direct recycling, respectively.

The cost and profit were also modeled and the results are compared in **Figure 7c and d**. Compared with LCO and NCM cathodes, LMO has not been recycled on an industrial scale due to the low profit (or even economic loss)⁵⁸. The total cost of pyrometallurgical, hydrometallurgical, and direct recycling of LMO batteries was estimated to be \$2.43, \$1.3 and \$0.94 per kg of spent battery cells processed, respectively. It is worth to be mentioned that the only hydrometallurgical method collecting manganese as manganese sulfate and manganese dioxide, while high-quality LMO cathode powder is obtained in the direct regeneration method. Since the current market value of LMO (\$7.00/kg) is much higher than that of Mn in product (\$1.43/kg), an economic benefit with a potential profit of \$2.03 per kg of spent cells can be obtained in the direct recycling process. In comparison, the expected profit in pyrometallurgical method

is calculated negatively. As the result of the significant reductions in total energy use, GHG emissions and processing cost, as well as the potential increase of overall profit, the non-destructive, one-step aqueous direct regeneration method may be a preferable option for closed-loop LIB recycling. While the EverBatt model might have oversimplified the actual processing steps in the LIB recycling, we believe the side-by-side comparison among the three recycling approaches can provide valuable guidance to select and improve the next-generation LIB recycling strategies.

Conclusion

In summary, we have successfully demonstrated complete regeneration of degraded LMO cathodes with different SOHs using a simple direct recycling approach. Particularly, the perfect reconstruction of desired stoichiometry and phase purity enabled by the one-step hydrothermal treatment in dilute Li-containing solutions provides the regenerated LMO particles with high capacity, long cycling stability and high rate performance, on par with commercial pristine LMO materials. The understanding on the mechanism of the hydrothermal relithiation process provides a potential solution for sustainable and closed-loop re-manufacturing of energy materials. The life-cycle analysis further suggests that our work represents a simple yet efficient approach to re-functionalize high-performance LMO cathodes, with distinct environmental and economic advantages over traditional pyrometallurgical and hydrometallurgical methods. Continuous improvement of the direct recycling method towards automated electrode separation and process intensification will pave the way for its practical application.

■ ASSOCIATED CONTENT

Supporting Information

The Supporting Information is available free of charge on the ACS Publications website. Experimental section, supplementary tables and supplementary figures (Electrochemical data, ICP data, Rietveld refinement of the XRD patterns, XPS fitting parameters, TEM images and EverBatt Model).

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Notes

A Patent was filed for this work through the UCSD Office of Innovation and Commercialization.

■ ACKNOWLEDGEMENTS

This work was supported by US National Science Foundation via Award CBET-1805570, U.S. Department of Energy (DOE) via ReCell Center, and the start-up fund support from the Jacob School of Engineering at UC San Diego. Part of this work used the UCSD-MTI Battery Fabrication Facility and the UCSD-Arbin Battery Testing Facility. Neutron diffraction work was carried out at the Spallation Neutron Source (SNS), which is the U.S. DOE user facility at the Oak Ridge National Laboratory, sponsored by the Scientific User Facilities Division, Office of Basic Energy Sciences (BES). The electron microscopy work by Q.Y. and J.L. was supported as part of the Center for Synthetic Control Across Length-scales for Advancing Rechargeables (SCALAR), an Energy Frontier Research Center funded by the US DOE, Office of Science, BES under Award No. DESC0019381.

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