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Receiver development for BICEP Array, a next-generation CMB polarimeter at the South Pole

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ABSTRACT

A detection of curl-type (*B*-mode) polarization of the primary CMB would be direct evidence for the inflationary paradigm of the origin of the Universe. The BICEP/Keck Array (BK) program targets the degree angular scales,

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where the power from primordial B -mode polarization is expected to peak, with ever-increasing sensitivity and has published the most stringent constraints on inflation to date. BICEP Array (BA) is the Stage-3 instrument of the BK program and will comprise four BICEP3-class receivers observing at 30/40, 95, 150 and 220/270 GHz with a combined 32,000+ detectors; such wide frequency coverage is necessary for control of the Galactic foregrounds, which also produce degree-scale B -mode signal. The 30/40 GHz receiver is designed to constrain the synchrotron foreground and has begun observing at the South Pole in early 2020. By the end of a 3-year observing campaign, the full BICEP Array instrument is projected to reach σ_r between 0.002 and 0.004, depending on foreground complexity and degree of removal of B -modes due to gravitational lensing (delensing). This paper presents an overview of the design, measured on-sky performance and calibration of the first BA receiver. We also give a preview of the added complexity in the time-domain multiplexed readout of the 7,776-detector 150 GHz receiver.

Keywords: Cosmic Microwave Background, Polarization, Instrumentation, Cosmology, B-Modes, Inflation

1. INTRODUCTION

Measurements of the polarization of the Cosmic Microwave Background (CMB) provide crucial information to further our understanding of the early Universe. The Lambda cold dark matter (Λ CDM) model predicts an E -mode polarization pattern in the CMB at the level of a few μ K as well as a B -mode polarization signal arising from gravitational lensing of E -modes by the large-scale structure of the Universe. Inflationary gravitational waves are predicted to produce an excess of B -mode power on degree angular scales that is scaled by the tensor-to-scalar ratio r . The value of r is directly tied to the energy scale of inflation.¹ While certain classes of inflation models predict extremely small values of r , a detection of primordial B -mode polarization would be direct evidence for the theory of inflation. However, polarized Galactic dust and synchrotron foregrounds hamper our ability to measure primordial gravitational waves and need to be disentangled from the degree-scale B -mode polarization signal by observing the sky at multiple frequencies with exquisite sensitivity. Additionally, the removal of B -mode power due to gravitational lensing (delensing) can lead to improved constraints on r , but it requires higher resolution observations.²

The most stringent published constraint on the tensor-to-scalar ratio is $r_{0.05} < 0.06$ at 95% confidence from BICEP/Keck Array data in conjunction with Planck and WMAP measurements⁴ (see Figure 1, which includes the most recent Planck points³). Over the past 15 years, our experimental strategy of designing small-aperture, cryogenic, refracting wide-field telescopes observing from the South Pole has proven successful in probing the degree-scale polarization of the CMB (multipoles $35 < l < 300$) with tight control of systematic errors. BICEP1 was the first polarimeter designed specifically to target the B -mode signal and operated from January 2006 through December 2008 with 49 orthogonal pairs of polarization-sensitive NTD bolometers observing at 100 and 150 GHz. BICEP2 observed the sky with 500 antenna-coupled transition-edge sensor (TES) bolometers at 150 GHz from 2010 to 2012, and reported an excess of B -mode power over the base lensed- Λ CDM model in the range $30 < l < 150$,⁵ which was later attributed to polarized dust emission.⁶ The Keck Array consisted of five BICEP2-like 260 mm aperture receivers and started observations at 150 GHz in 2012. The interchangeable Keck Array receivers allowed us to diversify the frequency coverage over the years: 95 GHz receivers were deployed in 2014, 220 GHz in 2015, and 270 GHz in 2017. The higher-throughput BICEP3 receiver replaced BICEP2 in its mount in 2015, with a 520 mm aperture and 2500 detectors all operating at 95 GHz for an on-sky instantaneous instrument sensitivity of $6.7 \mu\text{K}_{\text{cmb}}\sqrt{\text{s}}$.⁷ Figure 2 shows the progression of the BICEP/Keck Array program, to larger apertures, larger focal planes, and wider frequency coverage.

2. THE BICEP ARRAY INSTRUMENT

The latest instrument in our program is BICEP Array,^{8,9} which adopts the same interchangeable concept used in Keck Array and is comprised of four BICEP3-class receivers in six frequency bands spanning from 30 to 270 GHz (Figure 3), which are all 27% wide. The lowest (30/40 GHz) and highest (220/270 GHz) frequency receivers are dual-band receivers each featuring a checker-board of focal plane modules with single-band detectors centered at the two adjacent bands (Figure 2). Splitting the atmospheric windows this way provides more spectral information on the Galactic synchrotron and dust emission, thus improving the constraints on the foreground

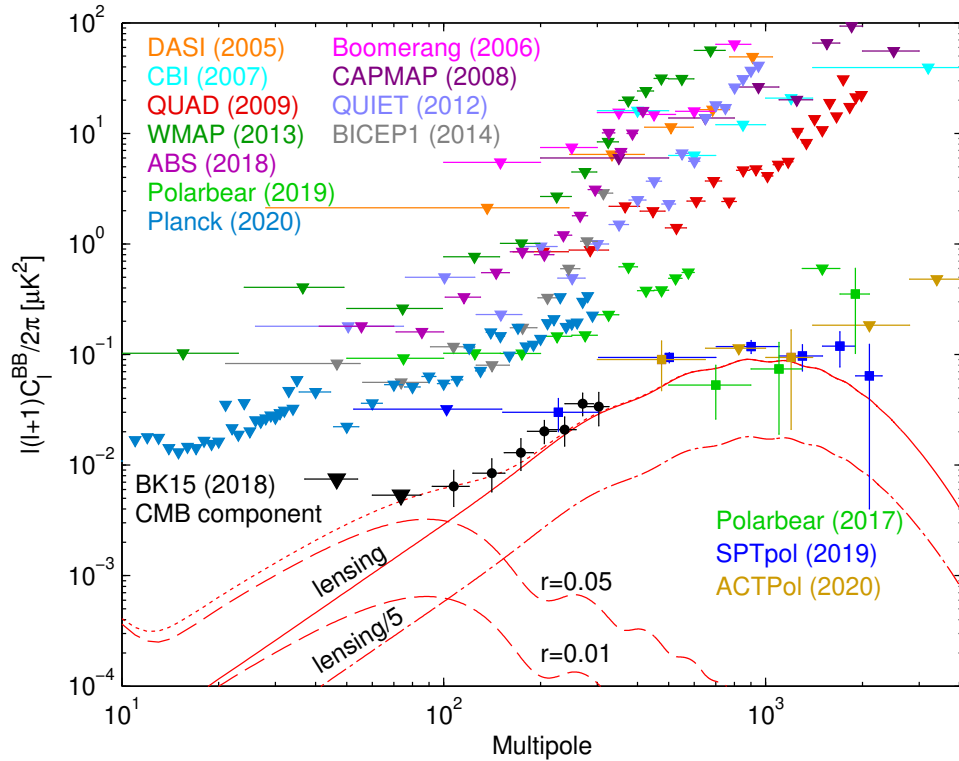


Figure 1. *B*-mode polarization measurement by different experiments as of Nov. 2020. The *Planck* points are on arXiv.³

Receiver Observing Band (GHz)	Nominal Number of Detectors	Nominal Single Detector NET ($\mu\text{K}_{\text{cmb}}\sqrt{\text{s}}$)	Beam FWHM (arcmin)	Survey Weight Per Year ($\mu\text{K}_{\text{cmb}}^{-2}\text{yr}^{-1}$)
<i>Keck Array</i>				
95	288	288	43	24,000
150	512	313	30	30,000
220	512	746	21	2,750
270	512	1,310	17	800
BICEP3				
95	2,560	265	24	240,000
BICEP Array				
< 30	192	260	76	19,500
< 40	300	318	57	20,500
95	4,056	265	24	380,000
150	7,776	313	15	455,600
< 220	8,112	746	11	58,600
< 270	12,288	1,310	9	19,200

Table 1. Receiver parameters as used in sensitivity projections. Boldface numbers are actual/achieved quantities for existing receivers. The remaining values in the survey weight column are scaled from the achieved survey weights using only the ratio of the number of detectors, plus, if necessary to change frequency, the ratio of nominal NET values squared.

model parameters. Scaling from previous on-sky performance, Table 1 shows the expected sensitivities and survey weights* of the 4 receivers, which amount to 32,000+ photon-noise limited polarization-sensitive detectors.

*Survey Weight is a single number representing the total raw experimental sensitivity achieved, and is defined as $W = 2A/N^2$ where A is the map area and N is the noise level in the Q/U maps. Survey weight is useful because it scales linearly with integration time, number of detectors, and statistical sensitivity to r .¹⁰

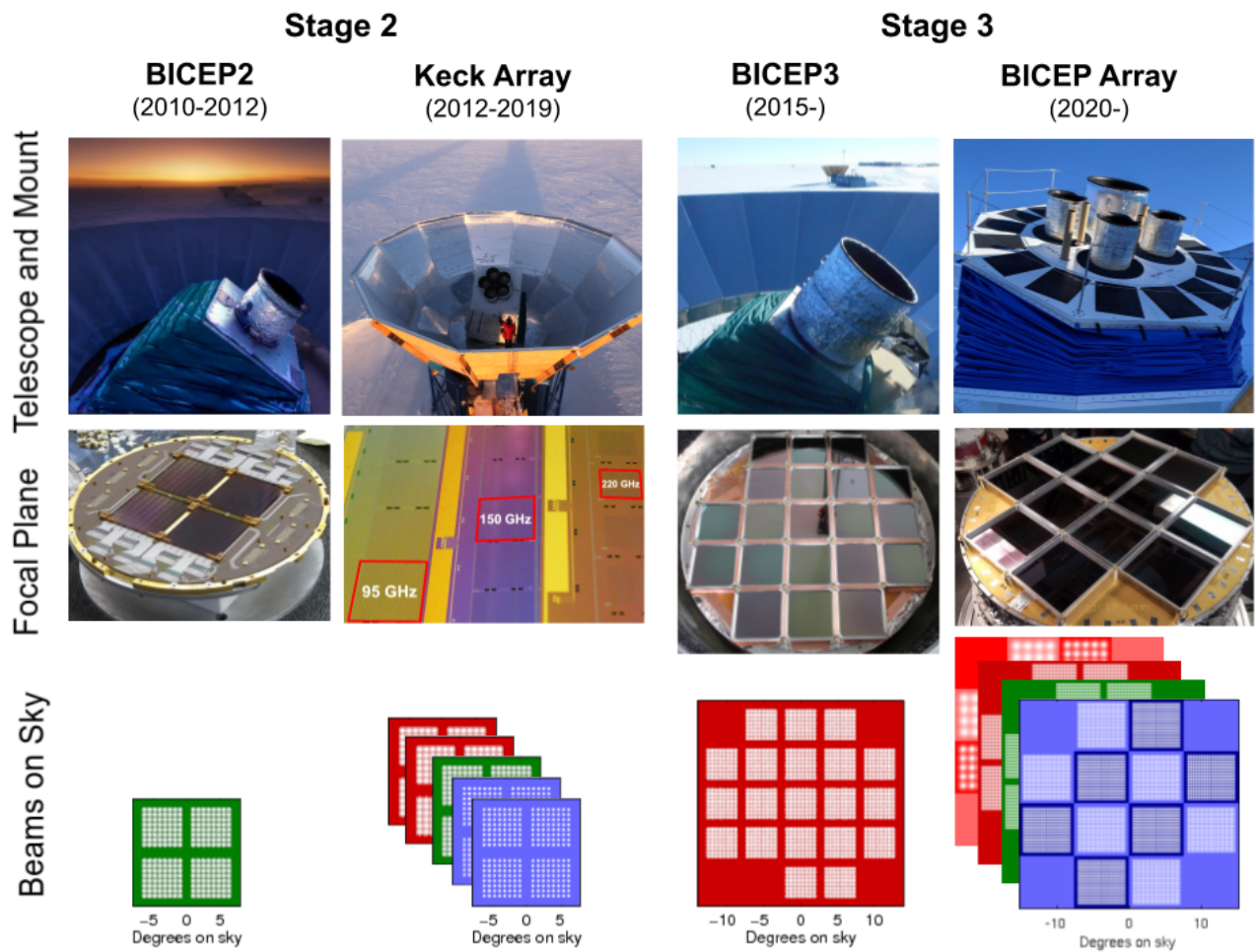


Figure 2. The progression of the BICEP/Keck Array program leading to the BICEP Array. Bottom row: the beam patterns of the focal planes on the sky shown on a common scale. Each square represents a single receiver, and the colors indicate different observing frequencies: light red for 30/40 GHz, red for 95 GHz, green for 150 GHz, and blue for 220/270 GHz.

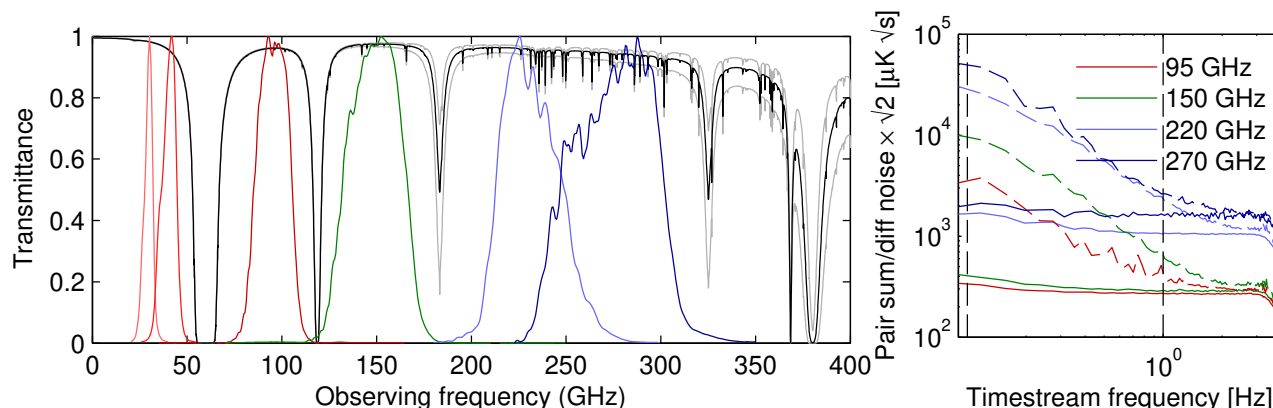


Figure 3. *Left:* Comparison of atmospheric transmission at the South Pole with the bandpasses of BICEP/Keck Array and BICEP Array. Median atmospheric transmission during the observing season is shown in black, bracketed by the 10th and 90th percentiles. Transmission drops only slightly across 200–300 GHz, making dust observations in the upper part of this window effective, with similar dust sensitivity to the 220 GHz band. *Right:* Minimally processed timestream pair-sum and pair-difference noise spectra from Keck Array. The stable Antarctic atmosphere enables observations at all of these frequencies that are low-noise across the indicated science band from 0.1–1 Hz, corresponding to $25 \lesssim \ell \lesssim 250$.

At the end of 2019, the *Keck Array* telescope mount has been replaced by the new BICEP Array mount,¹¹ which provides bore-sight rotation about the optical axis, in addition to rotation in Azimuth and Elevation, following the *Keck Array* and BICEP3 designs. During the same Austral Summer, we also deployed the first 30/40 GHz BICEP Array receiver, equipped with a full complement of detector modules to fill the focal plane, which has now observed for an entire season. The other BICEP Array receivers will be installed in the new mount with a staged approach over the next few years[†]. In the meantime, we are continuing observations with a subset of the *Keck Array* receivers installed in open slots until they are filled by available BICEP Array receivers. The observations will continue to focus on the deep BICEP/Keck Array sky patch so that the new low-frequency data can be combined with existing multi-frequency observations. An updated project timeline is shown in Figure 12.

2.1 Receiver Overview

BICEP Array is largely based on the successful design of BICEP3.^{12–15} Each receiver is housed in a custom-designed vacuum cryostat¹¹ 2.1 m tall and 0.9 m in diameter (excluding the additional envelopes of the multi-channel readout electronics and the pulse-tube cooler). Figure 4 shows a cross-section of the receiver, along with the optical diagram for reference. The vacuum and 50 K shells are designed with a short base-stage, and long cylinders for the main section, which allow users to lift off the outer shells from the base plate without undoing the cabling, thermal joints and sub-Kelvin truss structure. The vacuum window is made out of HDPE for the 30/40 GHz receiver, while thinner solutions for the higher frequencies are actively being pursued.¹⁶

The 4 K shell is divided into two lengthwise segments for ease of access during integration; the top optics section houses the objective lens and baffle rings designed to minimize reflections within the tube. The lower optics section holds the nylon filter and the field lens. The 4 K plate supports the fridge space and the sub-Kelvin thermo-mechanical truss structure. The 50 K volume is supported by G-10 truss legs, providing robust structural support while maintaining low thermal conductivity between temperature stages. The truss legs for the 4 K and sub-Kelvin structures are instead made out of carbon fiber, owing to its superior room-temperature elastic modulus to low-temperature thermal conductivity ratio at ≤ 4 K.¹⁷

2.2 Thermal Architecture

All BICEP Array receivers (see Figure 4) use a Cryomech PT415[‡] pulse tube with nominal cooling capacity of 40 W and 1.5 W at the 50 K and 4 K stages, respectively. The pulse tube is driven by a remote stepper motor that

[†]Due to the COVID-19 pandemic, no crew will deploy at the end of 2020 and the instrument will remain unchanged.

[‡]<https://www.cryomech.com/products/pt415/>

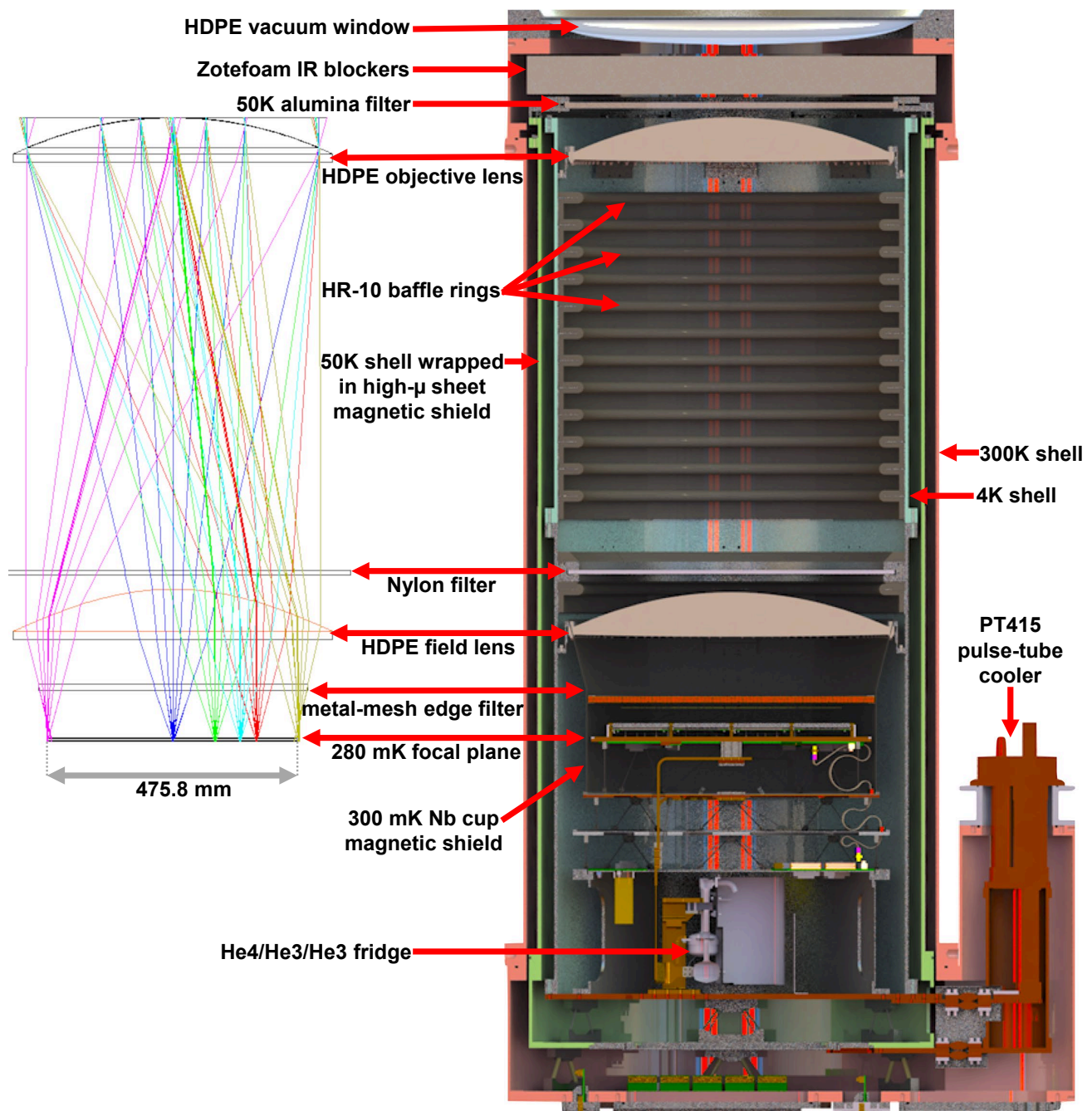


Figure 4. BICEP Array optical diagram and cross-section of the cryogenic receiver. All optical components, except for the Zotefoam filters, are anti-reflection coated to minimize in-band reflections. The HDPE lenses, nylon filter, and aperture stop are precision-mounted in the receiver and cooled to 4 K to reduce detector loading. The focal plane assembly, which houses 12 detector modules, is cooled to 280 mK by a sorption fridge and surrounded by a superconducting Nb magnetic shield. The focal plane is actively temperature-controlled to achieve detector baseline stability over timescales of hours. The radially-symmetric receiver design allows well-matched beams for orthogonally polarized detectors at the focal plane.

Truss structure conducted load budget			
	2 K (μ W)	300 mK (μ W)	250 mK (nW)
18 100-way NbTi cables (TDM)	84.1	18.8	82.2
4 25-way Manganin cables (HK)	1.9	0.5	2.8
Cernox cables (HK)	6.6	1.2	2.4
Heater cables (HK)	2.8	0.5	1.8
Carbon fiber trusses (M)	33.6	12.9	47.1
Aluminized mylar RF shield (M)	48.7	21.5	97.8
Total	177.7	55.5	234.1

Table 2. Sub-Kelvin loading from conduction for BICEP Array. This calculation^{24,25} is based on the maximum detector readout NbTi cable count for the highest-frequency TDM receiver (150 GHz, see Table 3). The housekeeping (HK) and miscellaneous (M) entries are common to all BICEP Array receivers. More details on RF shielding are given in Section 2.6.

is physically detached and electrically/mechanically isolated from the cold head. Residual mechanical vibrations induced by the fittings connecting the head and the motor are damped by a spring bellows connecting the cold head to the cryostat shell. We also use e-beam welded heat straps with flexible sections of ropelay stranded copper in order to minimize the rigidity and the transmission of vibration to the cryostat stages.

The optical filtering follows the successful BICEP3 scheme.¹² Behind the 560 mm-aperture vacuum window, which lets > 100 W of thermal radiation into the receiver, a stack of 12 1/8"-thick layers of Zotefoam HD-30[§] with 1/10" spacers provides infrared filtering,^{18,19} in conjunction with a 10 mm-thick IR-absorptive alumina filter,²⁰ which is installed at the top of the 50 K stage. The lower 4 K optics section holds an absorptive 7.45 mm-thick nylon filter, to prevent any short-wavelength radiation let through by the alumina filter above from reaching the focal plane. Finally a low-pass metal-mesh filter^{21,22} installed at 300 mK defines the upper edge of the band.

Combining measurements with a thermal model, the total loading on the 50 K and 4 K stages with the receiver on-sky is estimated to be about ~ 40 W and ~ 0.5 W, respectively. Table 5 reports the median BICEP Array system temperatures during CMB observations in 2020.

Sub-Kelvin cooling for the detectors is provided by a three-stage helium (4He/3He/3He) sorption fridge from CEA Grenoble,²³ with heat intercepts at 2 K (4He stage), 300 mK (intermediate cooler, or IC), and 250 mK (ultra cooler, or UC). With a design total loading of 70 and 15 μ W at the 300 and 250 mK stages, respectively, the fridge has sufficient cooling capacity to maintain a 3-day uninterrupted observing schedule between thermal cycles. With the telescope on-sky during observations, we have achieved a minimum fridge hold time of 2.5 days, after which other scheduling constraints become relevant.

The sub-Kelvin structure is located on top of the 4 K base plate, above the sorption fridge. It is separated into three thermal, "wedding-cake" carbon-fiber truss stages at 2 K, 300 mK, and 280 mK. Each stage provides radiative shielding and room for cable heat-sinking to the respective fridge stages, allowing low-loading environment for the focal plane and detectors. The detector modules and copper focal plane plate are heat-sunk to the fridge UC stage via a flexible high-purity copper-foil heat strap. The strap connects to the focal plane through a stainless steel block. The temperature of the strap is actively regulated, and the block serves as a passive low-pass thermal filter to attenuate thermal noise from the control circuit. The estimated conductive loading on the 2 K, IC, and UC stages is ~ 178 , ~ 55 , and 0.234μ W, respectively, from heat-sinking of cables and the mechanical truss structure, but not including radiative contributions (see Table 2).

2.3 Optics

Following the same concept as in previous small-aperture telescopes in the BICEP/Keck Array series, the BICEP Array receivers are simple diffraction-limited two-lens refractors, which provide a telecentric and flat focal surface with minimum aberrations over a wide field of view (see Figure 4 for the optical diagram). The telescope has a mean f -ratio of $f/1.57$ at the center of the focal plane, which has a diameter of 475.8 mm. The HDPE lenses

[§]<https://www.zotefoams.com/wp-content/uploads/2016/02/HD30-December-2017.pdf>

are 650 mm in diameter, with a clear aperture of 550 mm and a field of view of 29.6 degrees. The lenses and nylon filter are cooled to 4 K to minimize loading on the detectors and are anti-reflection coated to minimize in-band reflections. The 4 K space between the objective and the field lens is lined with baffle rings coated with Eccosorb[®] HR-10 microwave absorber to suppress far-sidelobe reflections. The same Eccosorb[®] is also used to define the 550 mm optical stop for the system, which is located just above (sky side) the objective lens. The detector beams are designed to terminate on the cold stop with an edge taper ranging from -10 to -13 dB with respect to the main lobe, depending on the frequency. Following the approach of previous optical designs in the BICEP/Keck Array telescope series, we take advantage of the excellent directivity provided by the uniform illumination of the planar phased-array antennas and maintain a conservative edge taper at the aperture stop.²⁶

The current material for the vacuum window is 1"-thick HDPE at 30/40 GHz, where HDPE has negligible in-band emission. At higher frequencies, thinner windows are being pursued, which will reduce the in-band optical loading and thereby significantly improve mapping speed.¹⁶

2.4 Detector Modules and Readout

The BICEP Array receivers are equipped with state-of-the-art dual-polarization antenna-coupled TES arrays, fabricated on 150 mm diameter silicon wafers.^{26,27} The detector arrays are based on planar in-phase combined slot antennas that provide higher pixel packing density than feedhorns, given a chosen edge taper[†]. The readout architecture is based on Time-Domain Multiplexing (TDM^{28,29}), developed by the University of British Columbia and NIST, with two stages of SQUIDs driven using a Multi-Channel Electronics (MCE) system that provides SQUID/TES bias voltages, controls SQUID addressing, and digitizes detector signals. The readout chain is based on numerous previous successful experiments,^{30,31} with the detector modules at 280 mK carrying the first-stage SQUIDs on a PCB located behind the $\lambda/4$ backshort (see Figure 5), which then connect to a custom focal plane distribution board and through superconducting NbTi wires to a stage of Series Array SQUIDs at 4 K (see Figure 6). In the design of these PCBs and the architecture of the cables, we paid particular attention to pairing signal and return in order to minimize cross-talk among channels. Moreover, the SQUIDs and TES detectors are carefully shielded from sources of magnetic fields, including the Earth's field (see Section 2.5 for more details).

Twelve detector modules are tiled onto the focal plane, each containing 32 to 2048 detectors, depending on the observing frequency (see Table 1). The module is based on the successful BICEP3 design,¹⁴ except the detectors are now fabricated on 6" silicon wafers, instead of the previous 4" wafers to expedite lithographic fabrication with higher detector count per module. The first-stage SQUID readout multiplexing chips are housed in a FR4 circuit board inside the module with superconducting tin-copper traces (BICEP3 and BICEP Array 30/40 GHz used aluminum traces on alumina substrates instead). The housing is constructed with superconducting niobium and aluminum, which, along with a high- μ A4K sheet inside the module, are designed to achieve high magnetic shielding performance (Section 2.5). Figure 5 shows the exploded view of the module design at 150 GHz.

Electromagnetic interactions between the edge antennas and the metal frame around the module can cause polarized beam mismatch on the edge pixels, resulting in potential temperature-to-polarization leakage in the CMB maps. We designed corrugated walls to minimize this effect. The 30/40 GHz module implements a novel broadband corrugation design that mitigates the differential ellipticity caused by the metal frame over 57% bandwidth, from 25 GHz to 45 GHz.^{32,33}

The first 30/40 GHz receiver (BA1) in its final configuration will be populated with 6 modules at each frequency in a checker-board arrangement. The design for the two frequencies is similar, with appropriate dimensions of the antenna scaled accordingly to frequency.³⁴ Due to the COVID-19 pandemic, no crew will deploy at the end of 2020 and the instrument will observe the sky for two full seasons in the configuration it was first deployed at the end of 2019, with the following breakdown of modules: 4 at 30 GHz, 7 at 40 GHz, plus one prototype dual-band 30/40 GHz module with 16 dichroic optical pixels (64 detectors; Shiu et al. in prep. [‡]).

The design of the two BICEP Array receivers at 95 and 150 GHz is at an advanced level of development and is based on the same TDM architecture and TES detector arrays. Table 3 shows the multiplexing factors and cabling arrangement for each receiver. We are currently in the process of validating the 150 GHz module design,

[†]See https://cmb-s4.org/wiki/images/2019_10_16_CMBS4_DetectorTechUpdate_V01.pdf#page=6.

[‡]<https://microdevices.jpl.nasa.gov/interactivepdfs/index.html?pdf=2020-MDL-Annual-report.pdf>, page 61.

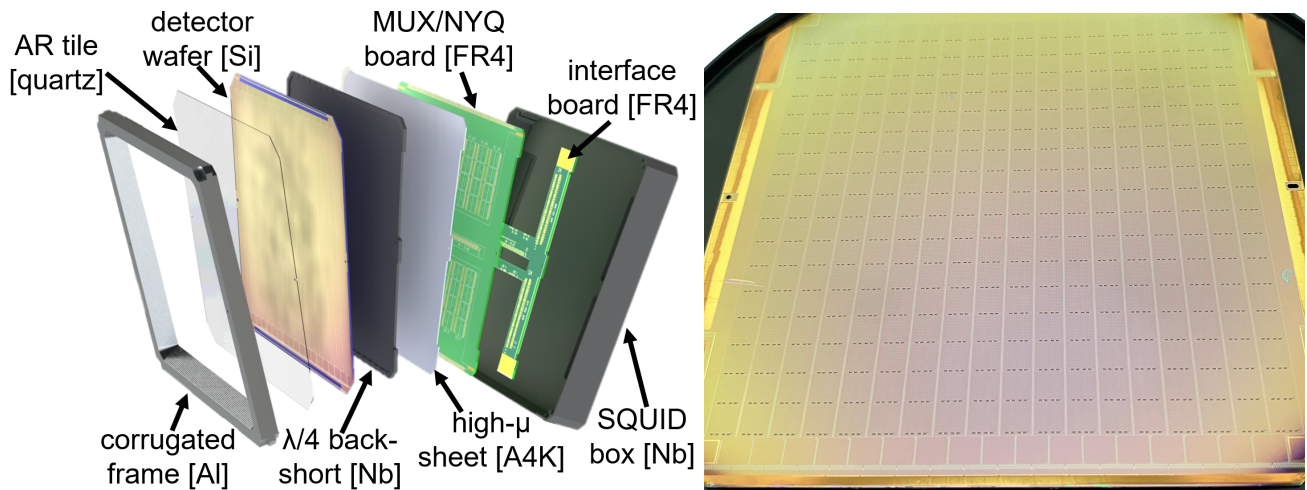


Figure 5. *Left*: An exploded view of the BICEP Array 150 GHz module. The design is based on BICEP3¹⁴ but scaled to house a larger detector wafer. The SQUIDs are mounted on the “MUX/NYQ” board and completely enclosed in a superconducting Nb box for magnetic shielding. The “interface” board allows for four flexible copper cables to route the TDM row and column signals out of thin slots in the Nb box and into the focal plane distribution board (see Figure 6). The “MUX/NYQ” board for the BA 95 and 150 GHz receivers is made out of FR4 with superconducting tin-copper traces, while BICEP3 and BICEP Array 30/40 GHz used aluminum traces on alumina substrates instead. *Right*: photo of a BICEP Array 150 GHz wafer with an 18x18 grid of phased-array slot antennas, each with dual-polarization detectors (648 total).

Frequency	30/40 GHz	95 GHz	150 GHz
# Detector Tiles	12	12	12
# Detectors	192 + 300	4,056	7,776
# Detectors/Tile	32 + 50	288	648
# SQUID MUX11 chips/Tile	6	32	64
# MCE	1	3	6
# Columns/MCE	24	32	32
# Rows (multiplexing factor)	33	43	41
# SQUID series array (SSA) modules	4	12	24
# Manganin cables (300 K - 4 K)	5	15	30
# NbTi cables (4 K - 280 mK)	3	9	18

Table 3. Time-domain multiplexing (TDM) scheme for the 30/40, 95, and 150 GHz receivers in BICEP Array. The fourth 220/270 GHz receiver will use microwave μ MUX^{35,36} or TKIDs,^{37,38} which both promise higher multiplexing factors.

which allows an 18x18 pixel tile (see Figure 5) to be read out. The large number of MCEs needed at 150 GHz required a relatively minor mechanical redesign of the MCE boxes in order to fit within the space constraints imposed by the telescope mount. In the context of CMB-S4,¹⁹ our team has developed ambitious preliminary designs of TDM modules that can read up to 1,920 detectors, without requiring superconducting flex cables.

The last BICEP Array receiver at 220/270 GHz will eventually feature over 20,000 detectors, and will be read out using RF-multiplexing schemes, which promise higher multiplexing factors than TDM. One possible implementation is the microwave SQUID readout (μ Mux³⁵) system that has been already been operated with our current TES detectors for a year as an on-sky demonstrator.³⁶ In this system, the TES detectors are unchanged and are multiplexed by coupling each TES to its own superconducting microwave resonator through an RF-SQUID. Alternatively, Thermal Kinetic Inductance Detectors (TKID^{37,38}) offer on-wafer RF multiplexing to greatly simplify wafer hybridization, and are currently being developed and tested within the collaboration.

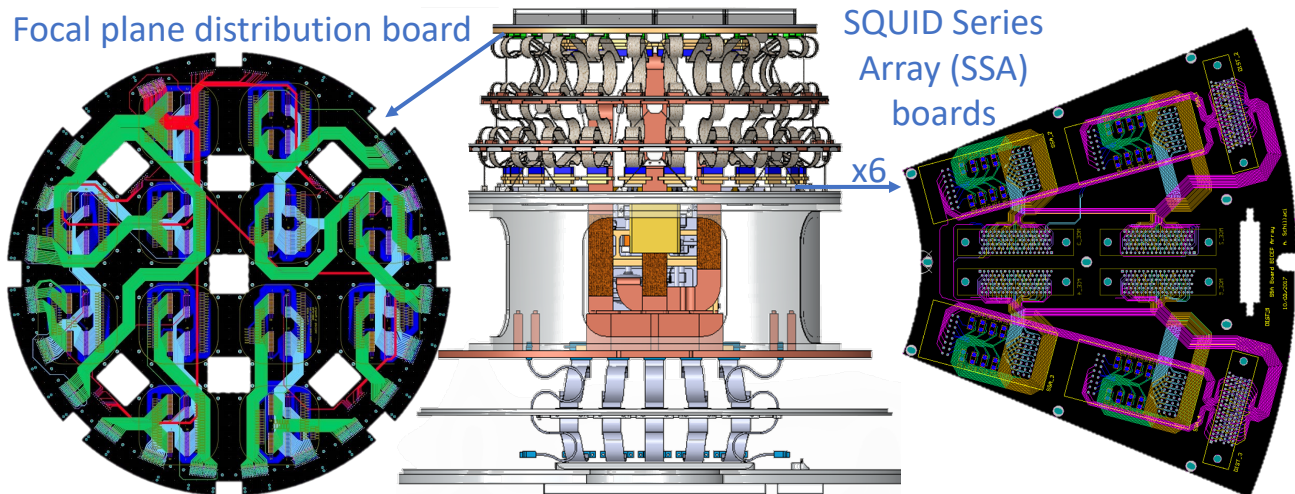


Figure 6. The focal plane distribution board gathers all the readout cabling from warmer stages and distributes them to the corresponding detector module at 280 mK. The SSA board is located at 4 K, and houses the SQUID Series Arrays (SSA). Each MCE connects to a single SSA board via five 100-way cables. The 30/40, 95, and 150 GHz receivers have one, three and six SSA boards, respectively. Shown above is the 150 GHz configuration.

Parts	Axial Residual Flux	Transverse Residual Flux
50K and 4K shields (combined)	0.24%	0.52%
Detector module (as a whole)	0.12%	0.20%

Table 4. Simulated magnetic shielding performance in BICEP Array, listed as separate sub-system contributions.

2.5 Magnetic Shielding

The SQUID/TES readout system is known to be susceptible to external magnetic fields^{39,40} and BICEP Array's magnetic shielding architecture is designed to minimize the level of spurious signals generated as the telescope moves along the Earth's magnetic field lines. We studied multiple configurations using COMSOL Multi-Physics software,⁴¹ which allowed us to simulate the Meissner behavior of a superconducting material (see Figure 7). We selected an architecture with a 1 mm-thick cylindrical A4K high magnetic permeability (μ) sheet wrapped around the 50 K cryostat shell, combined with a 2 mm-thick Niobium superconductive flared cup at 300 mK, which provide a shielding factor of 200 or better at the focal plane. Slotted mounting holes on the 50 K shield allow sufficient thermal expansion mismatch between the aluminum and A4K. The sub-Kelvin Niobium shield required a continuous base in addition to the flared cylinder to enhance the shielding performance. The Niobium base is not electrically connected to the copper base plate to avoid potential superconductor-metal interactions at the contact surface.

The TESs and the SQUIDs are then further shielded inside the focal plane modules, each of which features a superconducting aluminum detector frame, a superconducting Niobium SQUID box and a 0.020"-thick sheet of high- μ A4K material to provide a combined shielding factor of about 500 or better. Simulation shows the biggest field leakage comes from the slots for the readout cables. An additional Niobium sheet (not shown in Figure 7 for simplicity), with cable slots that are offset with respect to those in the SQUID box, is mounted on the back side of the module Niobium housing to minimize the leakage. Table 4 shows the simulated magnetic shielding performance of the receiver and module, listed separately. The combined system shielding performance is less straightforward to simulate due to interaction among the shields, and is beyond the scope of this paper.

We have performed direct measurements of the system to validate the COMSOL simulations by applying an external field that is modulated at a known frequency, including the use of cryogenic flux gate sensors installed at the location of the SQUIDs and TES. The results of these measurements will be published in a dedicated study (Schillaci, Basu Thakur et al, in prep.)

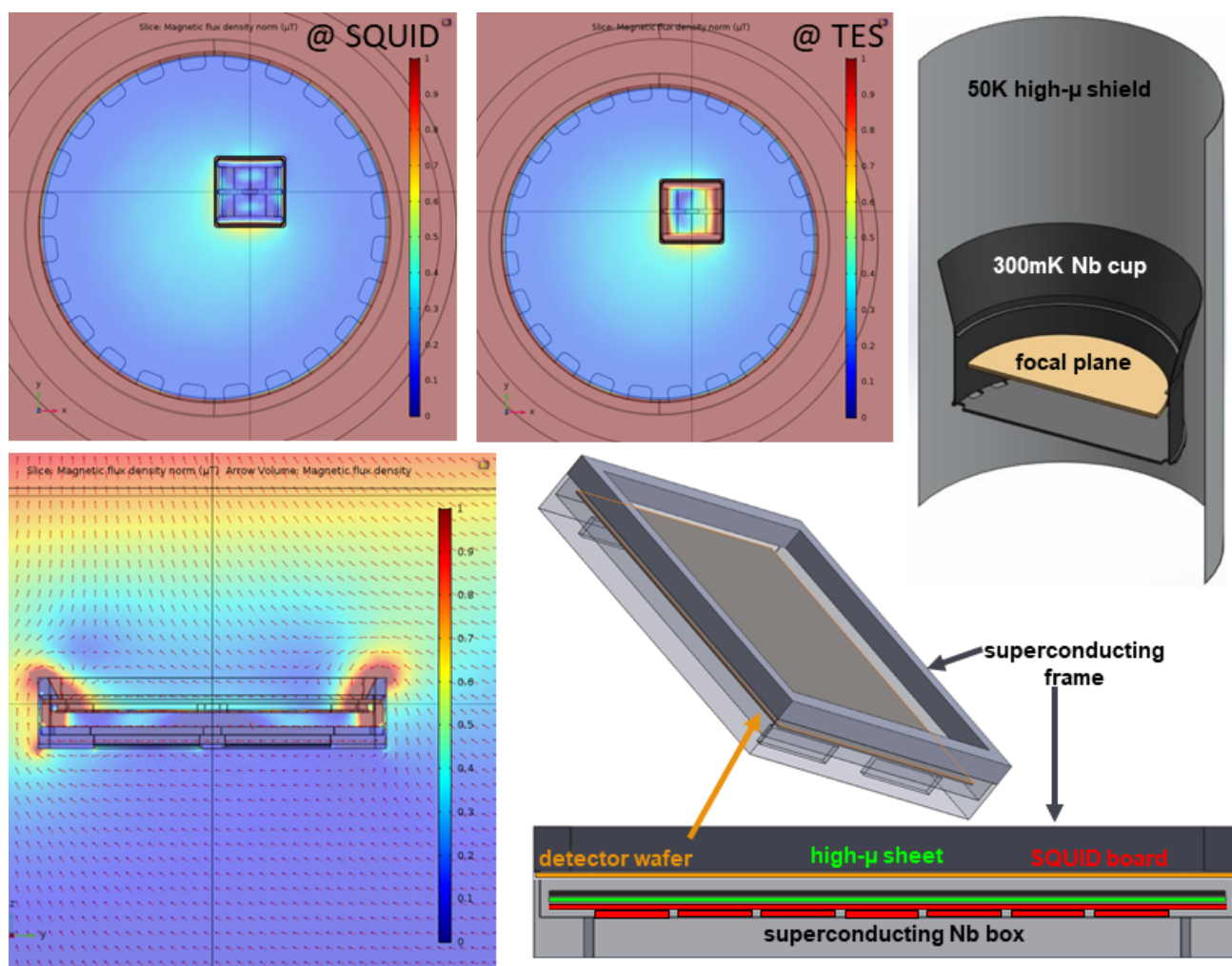


Figure 7. BICEP Array magnetic shielding. *Top left and center:* Comsol simulation of the residual total magnetic flux density when a purely axial $100\ \mu\text{T}$ external magnetic DC field is applied. Two horizontal slices of the receiver are shown, at the SQUID and TES planes, respectively. Color bar units are in μT . *Bottom left:* same as above but for a vertical slice at the detector module. *Top Right:* A 1 mm thick, high- μ A4K sheet is wrapped around the 50 K stage. A superconducting niobium flared cup shield is mounted at the 300 mK stage, surrounding the focal plane. *Bottom right:* The modules provide an additional level of shielding for the SQUIDS and the detectors. The various components made out of different materials are highlighted in color for clarity, and their respective labels are colored accordingly.

2.6 RF Shielding

Following the successful electromagnetic interference (EMI) mitigation strategy of previous small-aperture telescopes in the BICEP/*Keck Array* series,⁴² the detectors and SQUID readout chain are enclosed in a radio frequency (RF) shield. The RF shield begins on the top of the focal plane plate and extends down to the 4 K insert volume. Circular clamps at each temperature stage hold an aluminized Mylar shroud that drapes over the “wedding-cake” truss structure (a photo showing this has been published in a previous conference proceeding⁹). The continuous Mylar sheet is used to create a conductive path that surrounds the stages at different temperatures without thermally linking them (see Table 2 for an estimate of the thermal loading due to the Mylar). The ring on the stage at the bottom of the truss connects to the aluminum walls of the fridge volume and the 4 K base plate, which then connects to the optics tube. Filter connectors (micro-D saver PI filtered, model no. C48-00063-01 ^{**}) at the 4 K base plate protect the cold electronics from RF interference picked up in wiring outside the cryostat.

3. BICEP ARRAY 30/40 GHz RECEIVER PERFORMANCE

The 30/40 GHz BA1 cryostat was successfully integrated with the new BICEP Array mount and cooled to base temperatures in January 2020. Table 5 reports the median system temperatures in BA1 during CMB observations in 2020, demonstrating adequate cryogenic performance achieved already during the first season. The exact focal plane configuration that was deployed is described in Section 2.4 and will remain unchanged for two full observing seasons due to the COVID-19 pandemic.

An extensive detector calibration campaign was conducted over the first several months of 2020, by a combination of the Austral Summer crew and winter-over Nathan Precup. Figure 8 shows FTS spectra for all the single-band detectors in BA1, demonstrating well-behaved band-passes at both frequencies and high end-to-end optical efficiency from the combination of detectors and optical train.

Another major check of the optical system is provided by taking beam maps with a source in the far-field of the telescope.^{43,44} Figure 9 shows band-averaged far-field beam map (FFBM) composites, obtained by coadding all per-detector FFBM composites in a frequency band (not including the prototype dual-band detectors mentioned in Section 2.4). Per-detector FFBM composites are made by coadding all individual FFBMs for a detector, which are taken at different boresight angles. The band-averaged composites demonstrate in-focus imaging and FWHM beam sizes in line with the design values of 76 and 57 arcmin at 30 and 40 GHz, respectively (see Table 1).

Finally, Figure 10 shows a preliminary BICEP Array 40 GHz temperature map covering 570 deg², obtained from 3,187 50-minute scansets from the 2020 observing season, and compared to the *Planck* 44 GHz⁴⁵ reobserved temperature map. Besides the variable⁴⁶ QSO [HB89] 0208-512 ^{††} visible at [RA, Dec] = [32.6925, -51.0172] deg in the BICEP Array field, the maps look very similar. Further analysis is beyond the scope of this paper.

4. OBSERVING STRATEGY AND PROJECTED SENSITIVITY

BICEP Array focuses its CMB observations on the same sky patch as BICEP3, spanning right ascension $-60 \text{ deg} < \text{RA} < 60 \text{ deg}$ and declination $-70 \text{ deg} < \delta < -40 \text{ deg}$, with an effective area of $\sim 600 \text{ deg}^2$ (larger than *Keck Array*'s $\sim 400 \text{ deg}^2$, but colocated). With the full BICEP Array sensitivity (see Figure 11), we expect to achieve and surpass the *Planck* map depths at all frequencies after only a few months of observations.

The parameters of the *Keck Array*, BICEP3, and BICEP Array are given in Table 1. The BICEP Array sensitivity estimates are based on achieved survey weight per year of the *Keck Array*. This procedure accounts for all real-world observing imperfections such as detector yield, cryogenic efficiency, data cuts, ground subtraction, temporal filtering, and other unexpected events that decrease the final sensitivity compared to the ideal case. Figure 12 shows the projected sensitivity of the ongoing and planned BICEP program. We expected to reach $\sigma(r) \sim 0.003$ at the end of the program, depending on the level of delensing that can be achieved using higher-resolution data from the South Pole Telescope. A demonstration of the delensing technique was just published.⁴⁷

^{**}https://portal.cristek.com/admin/client-data/cristek-web-links/cwl_links/4/FILTRRevD.PDF

^{††}[https://ned.ipac.caltech.edu/byname?objname=\[HB89\]%200208-512](https://ned.ipac.caltech.edu/byname?objname=[HB89]%200208-512)

Thermometer	Temperature (K)	Thermometer	Temperature (K)
50 K pulse tube head	41.803	4 K heat strap cold side	3.562
50 K heat strap cold side	43.664	4 K heat strap warm side	3.689
50 K heat strap warm side	49.036	Fridge bracket	3.943
50 K plate	50.251	Field lens	4.434
50 K tube bottom	58.737	Nylon filter	4.896
50 K tube top	63.268	Objective lens	5.183
50 K alumina filter	63.624	SQUID Series Array (SSA) board	4.002
He-4 switch	22.154	2 K plate	2.457
He-3 switch	23.191	Niobium cup (flared section)	0.373
He-4 pump	5.006	IC heat strap	0.322
He-3 pump	4.895	IC plate	0.321
He-4 condenser	3.781	Edge filter	0.321
He-4 evaporator	2.492	UC plate side	0.303
Intercooler (IC) evaporator	0.318	UC plate center	0.302
Ultracooler (UC) evaporator	0.274	UC heat strap	0.279

Table 5. Median BICEP Array system temperatures during CMB observations in 2020. See Figure 4 for locations.

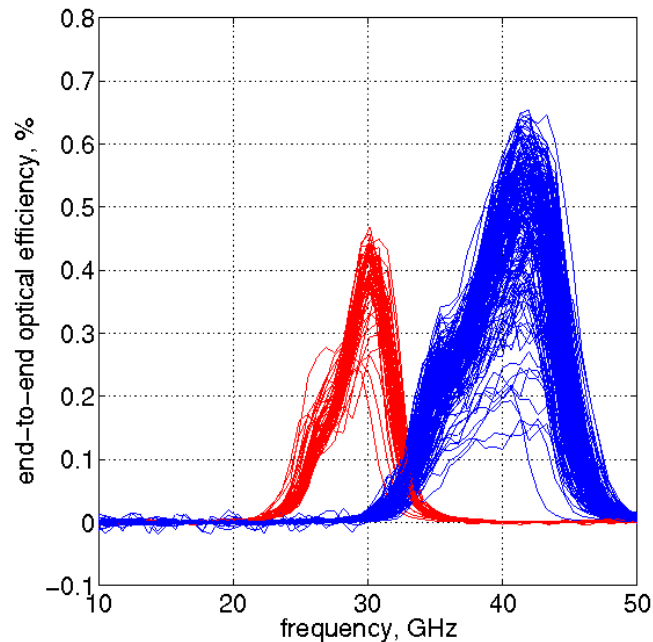


Figure 8. FTS spectra, normalized to the per-detector end-to-end optical efficiency.

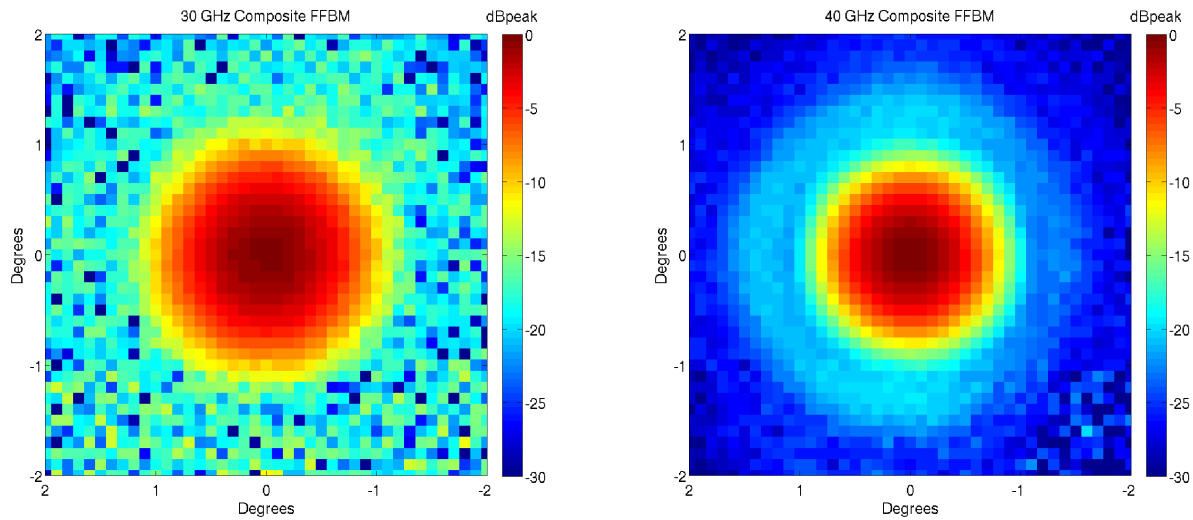


Figure 9. Band-averaged far-field beam map (FFBM) composites, made by coadding all per-detector FFBM composites in a frequency band. Per-detector FFBM composites are made by coadding all individual FFBM for a detector, which are taken at a range of boresight angles to get maximum coverage of the source. *Left:* 30 GHz. *Right:* 40 GHz.

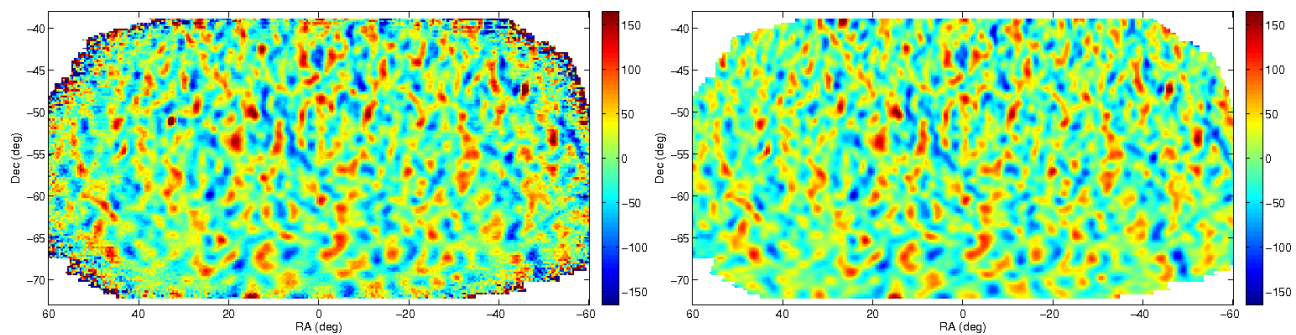


Figure 10. *Left:* BICEP Array 40 GHz temperature map covering 570 deg^2 , obtained from 3,187 50-minute scansets from the 2020 observing season. *Right:* Planck 44 GHz⁴⁵ reobserved temperature map, for comparison. Color bar units: μK .

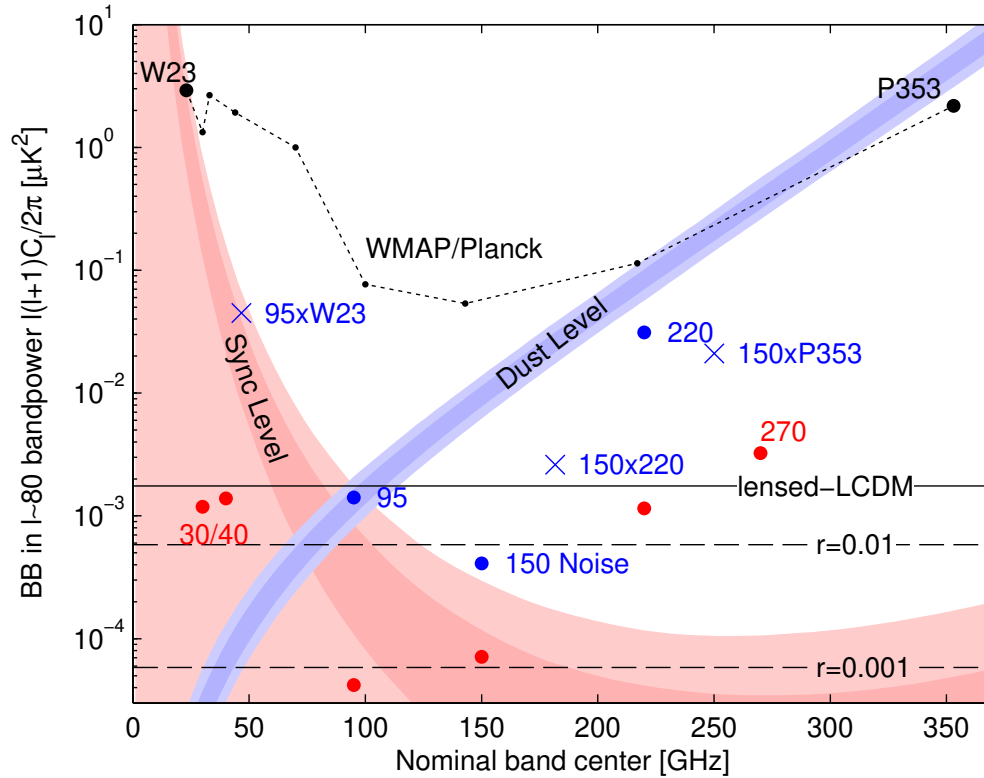


Figure 11. Noise uncertainty compared to signal level in the crucial $\ell = 80$ BB bandpower in the BICEP/Keck Array sky patch. The horizontal black lines show the expected signal power of lensed- Λ CDM, $r = 0.01$ and $r = 0.001$. The black circles show the noise uncertainty in the BK field of WMAP (23 & 33 GHz) and *Planck* (seven bands spanning 30–353 GHz) auto-spectra. The blue circles and crosses show the noise uncertainties published in BK15⁴ for auto- and cross-spectra, respectively. The constraints on the dust and synchrotron signal levels set in BK15 are shown by the shaded regions. Dust emission is detected with high signal-to-noise, while synchrotron has not been detected to date. The projected BICEP Array sensitivities by the end of the 2024 season are shown in red (see Figure 12 for a timeline).

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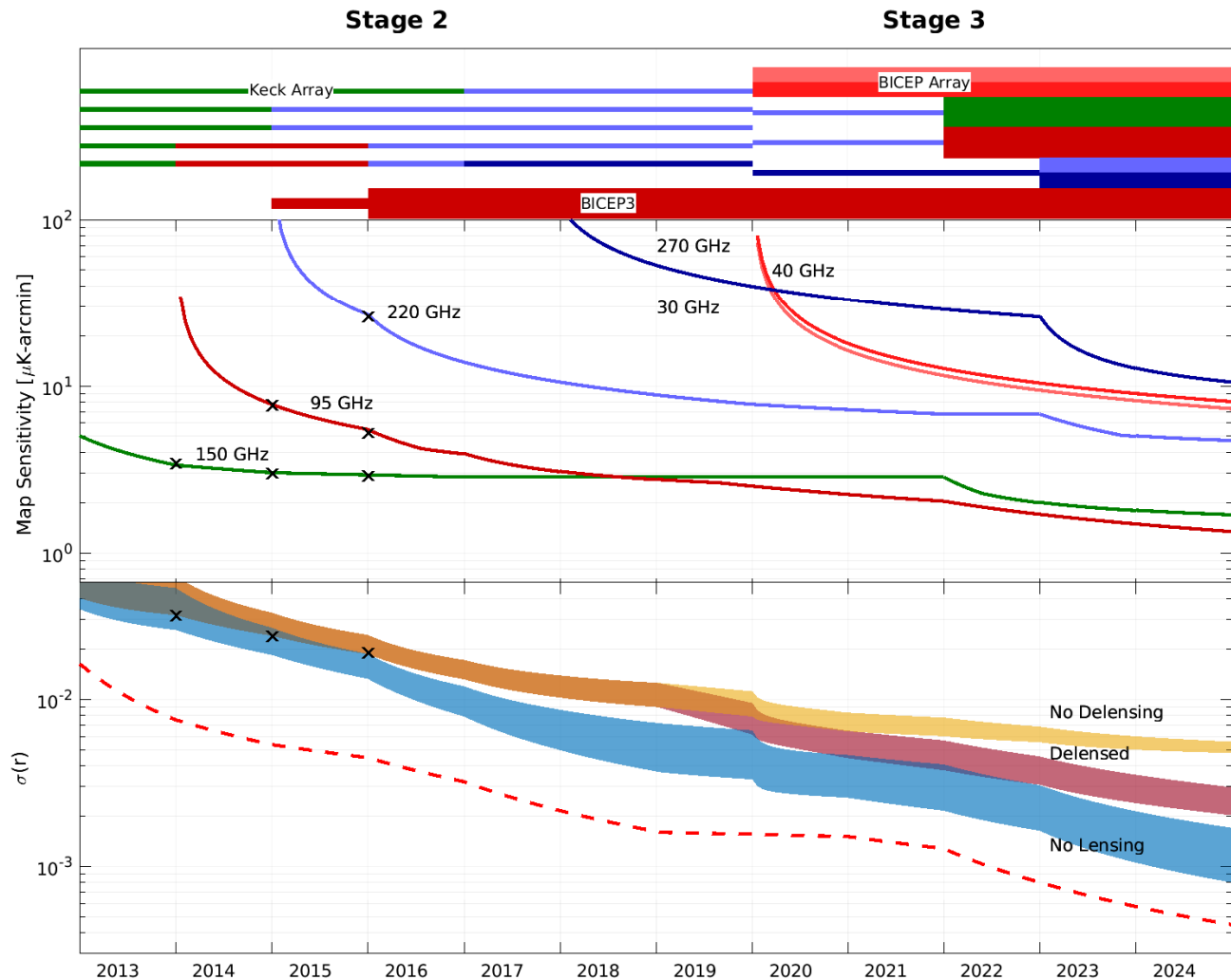


Figure 12. Projected sensitivity of the ongoing and planned BICEP/Keck Array observational program. BICEP Array will provide the sensitivity necessary to sustain the current rapid progress in constraining inflation. Note that these projections involve direct scalings from published end-to-end analyses and hence include all real-world inefficiencies, and removal of dust and synchrotron foregrounds. The X's mark the sensitivities achieved in the BK13,⁶ BK14⁴⁸ and BK15⁴ papers. Top panel: Schematic representation of the program showing the frequency bands covered by the various receivers through each observing season. Middle panel: Map depth at each frequency as a function of time. Bottom panel: Sensitivity to r after marginalizing over seven foreground parameters, as well as the “no foreground” raw sensitivity (red dash). The shaded regions show different levels of assumed delensing efficiency (including a “no lensing” case) that we can achieve by working with SPT-3G^{47,49} under the umbrella of the newly-founded South Pole Observatory.⁵⁰ The width of the shaded regions is due to a combination of varying the foreground amplitudes 1σ low/high from the BK15 maximum likelihood model, and turning frequency decorrelation (i.e., spatially varying spectral indices) in the foreground modeling on/off.

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