

A Proposed New Paradigm for Understanding and Preventing

Li Metal Penetration through Solid Electrolytes

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Context & Scale

A promising future technology for higher energy-density batteries is use of Li or Na anodes with ceramic solid electrolytes (SEs). These batteries have not been practical to date, in large part because Li/Na dendrites readily penetrate through SEs, leading to short circuits, even though the Li and Na shear moduli are at least 1-2 orders of magnitude below those of the SEs. This Perspective proposes a solution to dendrite penetration that is completely new to the battery field, one that we believe will unlock new research areas for improved SEs. Our approach comes from the observation that water readily penetrates through steel and other hard solids in a process called stress corrosion cracking (SCC). The driving force for SCC is generated at the crack tip by electrochemical reactions in the presence of high tensile stress. We propose that Li penetration through SEs is analogous: via crack growth driven by Li reactions in SE regions of high tensile stress. The SCC problem was solved decades ago for metals, glasses, and ceramics by putting their surfaces into states of residual compressive stress sufficiently high to inhibit crack propagation. A

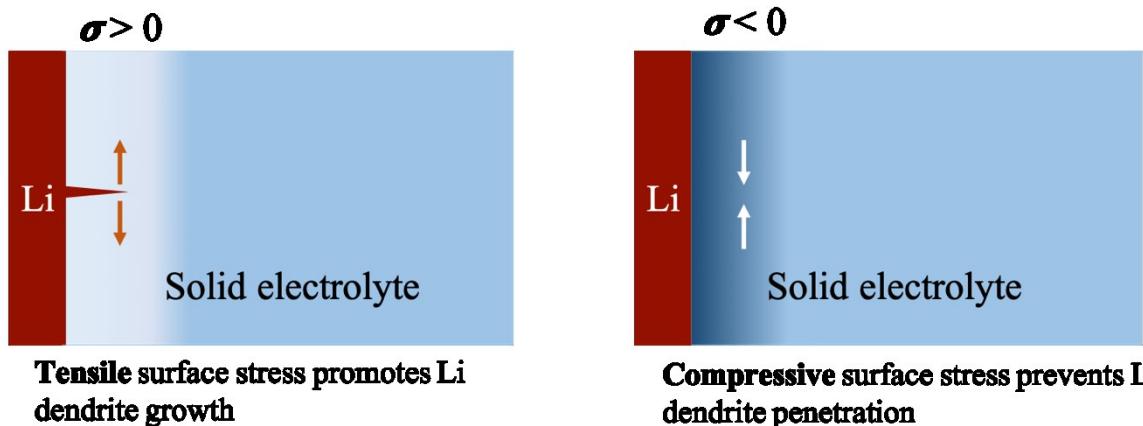
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similar approach could be viable for SEs if the required residual compressive stress does not strongly hinder Li ion diffusion. In this work we perform molecular dynamics calculations that show only a modest impact of even very high (10 GPa) compressive stresses on Li ion diffusion in a typical SE, potentially enabling our approach.

Abstract

The use of lithium (Li) or sodium (Na) metal anodes together with highly ion-conductive solid electrolytes (SEs) could provide batteries with a step improvement in volumetric and gravimetric energy densities. Unfortunately, these SEs face significant technical challenges, in large part because Li and Na dendrites can penetrate the SEs, leading to short circuits. The ability of a material with a low shear modulus (Li or Na metal) to penetrate through a ceramic is surprising from the point of view of models widely used in the Li battery field, which indicate that a SE with a shear modulus more than double that of Li or Na should prevent dendrite penetration. We introduce a concept new to the battery field for suppressing formation and penetration of lithium dendrites through SEs by putting the SE surfaces into a state of residual compressive stress. For a sufficiently high compressive stress, cracks have difficulty forming, and cracks that do form are forced to close, inhibiting dendrite penetration. This approach is widely used to solve commercially important stress corrosion cracking problems in metals and static fatigue problems in ceramics and glasses (e.g., Gorilla Glass). However, the technique will not be useful for SEs if the Li ion transport rate through a SE is substantially reduced when it is in compression. Our molecular dynamics calculations for Li ion transport through a common SE demonstrate that the introduction of even very high residual compressive stresses (~10 GPa) has only a modest effect on Li ion transport kinetics, suggesting that the approach is viable and capable of providing a new paradigm for developing high-performance and stable SEs.

TOC Graphics



Introduction

The use of Li or Na metal negative electrodes (anodes) could provide a substantial increase in the gravimetric and volumetric energy density for Li batteries. However, their use in high capacity rechargeable batteries has been precluded¹, in large part because of the growth of Li filaments (loosely called “dendrites”). These filaments provide a surface for degradation reactions, and they may become electrically isolated. For the case of dendrite penetration into solid electrolytes, which occurs readily², they can induce mechanical failure and fracture of solid electrolytes, and if they reach the positive electrode, they will cause a short circuit, potentially leading to a fire³⁻⁷.

The battery community has taken several approaches to addressing the dendrite penetration problem^{8,9}. Monroe and Newman and followers¹⁰⁻¹² proposed an electrochemical-mechanical model in which a Li protrusion (proto-dendrite) is pressed conformally, or nearly conformally, against a solid polymer separator. These models compare reaction current density at the tip of the protrusion (dendrite penetration) with current density at its base and find that a separator with a shear modulus at least double that of Li metal could prevent dendrite penetration. However, neither suppression of dendrite penetration in liquid electrolyte cells under moderate stack

pressures^{13,14}, nor penetration through solid electrolytes with very high shear moduli^{2,15}—cases that do not involve solid polymer separators—can be readily explained with this paradigm. We attribute this discrepancy to a combination of the model not incorporating Li creep; ignoring internal defects in the solid electrolyte; and assuming near-conformal contact, which is not realized for interfaces between Li metal and either thin commercial separators¹³ or solid electrolytes¹⁵. Because only a small fraction of the Li metal and solid electrolyte surfaces are in physical contact, GPa-level hydrostatic pressures¹⁶ in Li cannot build up against solid electrolytes because Li relaxes, by deformation and creep, into non-contact regions that may be at a considerable distance from the contact point. Thus, we believe that contact mechanics between Li and a solid electrolyte cannot be properly modeled on a scale of a single penetrating dendrite. In addition, internal defects, such as pores, cracks, and grain boundaries in solid electrolytes can trap electrons and nucleate metallic Li, even ahead of the Li-metal front¹⁷.

Chemical and physical modifications to the Li-separator interface, such as introduction of nanostructures or coatings or by modification of the electrolyte¹⁸⁻³², have seen some success in inhibiting dendrite growth, while other approaches have focused on developing new solid electrolytes³³ and special Li hosts^{34,35} or on controlling the temperature³⁶. Nevertheless, to date there are no commercially available high capacity rechargeable Li metal batteries that operate under a current density that is comparable to that in liquid electrolytes, in significant part because of the dendrite penetration problem. This Perspective proposes a new paradigm for mitigating dendrite-induced short circuits.

New Approach to Suppress Lithium-Dendrites Induced Cracking

Our proposed approach is based on an analogy to stress corrosion cracking (SCC)³⁷⁻⁴⁰, which has been studied and largely solved in the corrosion field. SCC occurs when the surface of a component is chemically (usually electrochemically) attacked at a defect or heterogeneity⁴¹. The result is the formation or extension of an incipient crack that can grow if and only if the crack tip is in a sufficiently high state of tension. SCC crack growth occurs under the combined effect of a chemical reaction plus surface tensile stresses that are above some threshold value but below the level required for fast crack propagation^{42,43}. SCC has led to catastrophic results, such as the collapse of the Silver Bridge^{44,45} across the Ohio River. In that case, local rusting caused stress corrosion cracks that followed grain boundaries in the steel. Although SCC is often thought of as occurring primarily in metals, it can also occur in glasses, ceramics, and quartz, where the process is known as static fatigue⁴⁶⁻⁵¹.

Since the attacking medium in SCC is usually water, relative shear strength^{10,11} clearly plays no role, so the fact that soft Li metal penetrates through extremely stiff ceramic solid electrolytes is not surprising if SCC is the mechanism. Furthermore, hydrostatic pressures in the Li are not required, since the SCC driving force comes from chemical reactions in regions of tensile stress in the solid electrolyte. The proposed analogy between water penetration and Li metal penetration can be visualized in **Figure 1**. **Figure 1a** shows stainless steel that has been

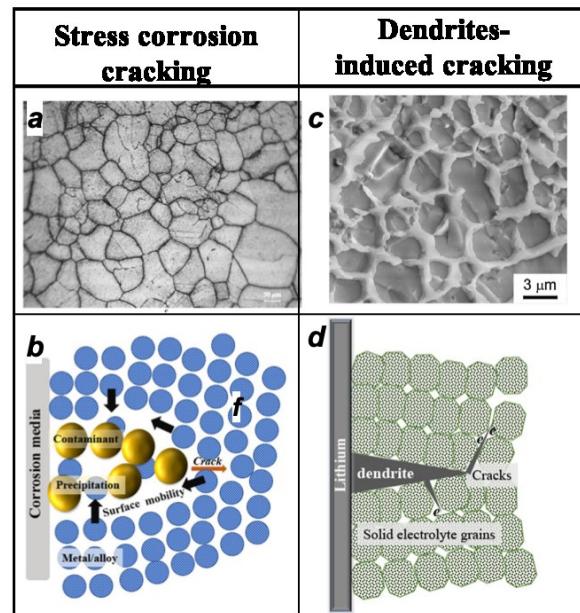


Figure 1: SEM images of (a) intergranular cracking in stainless steel (b) the intergranular penetration of LLZO by Li. Schematics of cracking propagation caused by SCC (c) and lithium plating in LLZO (d). the corresponding SCC mechanism.

attacked by water via SCC⁵², where intergranular cracks were observed during aging at 550 °C. The formation of chromium carbides along the grain boundaries, which is facile at elevated temperature, results in creation of a chromium-depleted region, exacerbating the susceptibility to intergranular corrosion when tensile stresses are present. **Figure 1c** shows images of intergranular penetration of LLZO² by Li metal, forming dendrites as the crack propagates.² As illustrated in **Figures 1b** and **1d**, both processes involve corrosion/electrochemical environments together with the presence of heterogeneities⁴¹, including grain boundaries, contaminants or precipitates. We suggest that, in analogy with SCC, local residue tensile stresses promote Li dendrite propagation via crack propagation.

The approach that often solves SCC problems is putting the surface into a state of residual compressive stress. For example, the crack resistance of Gorilla Glass is due to exchanging smaller sodium atoms near the surface with larger potassium atoms⁵³.

We are not aware of any spatially resolved surface stress measurements in solid electrolytes. However, large residual stresses, both tensile and compressive, can be expected from formation processing⁵⁴, and experiment shows that when tensile, these stresses can result in highly brittle products⁵⁵. Local tensile residual stresses can also be generated from heterogeneities as well as from machining or polishing⁵⁶⁻⁵⁹. Thus, solid electrolytes may be readily susceptible to SCC (or static fatigue) as well as brittle fracture.

However, the analogy between solving SCC and solving Li dendrite penetration is imperfect because a solid electrolyte must also maintain sufficient ionic conductivity after the compression is introduced, a factor that is irrelevant for something like Gorilla Glass. Previous work has shown

that internal stresses can have a significant impact on ionic conductivity⁶⁰⁻⁶⁶, and it is possible that putting the solid electrolyte into compression could substantially hinder ion mobility.

Evaluation of the Impact of Stress on Li Diffusion

To evaluate the effect of a hydrostatic compressive stress on Li diffusion kinetics, molecular dynamics (MD) simulations were performed as described in the Methods section. Results are shown in **Figure 2, left**, which were calculated at 1100K to accelerate the diffusion process. The Li self-diffusivity, D, was fitted to the linear region of the root mean square distance (RMSD) with simulation time. The diffusivity was then plotted as a function of the average hydrostatic pressure. The simulation results at 1100K (orange dots, **Figure 2, right**) show a peak diffusivity at 2GPa tensile stress. In order to compare with experiments at room temperature, the simulated diffusivity was extrapolated to 300K based on the experimentally measured activation energy of 0.38 eV⁶⁷, a value that is insensitive to strain change according to density functional theory (DFT) calculations⁶⁸. It can be seen from the blue dots, **Figure 2, right**, that the simulated/extrapolated room temperature Li diffusivity at zero stress is $\sim 0.5 \times 10^{-12} \text{ m}^2/\text{s}$, which is within the range of

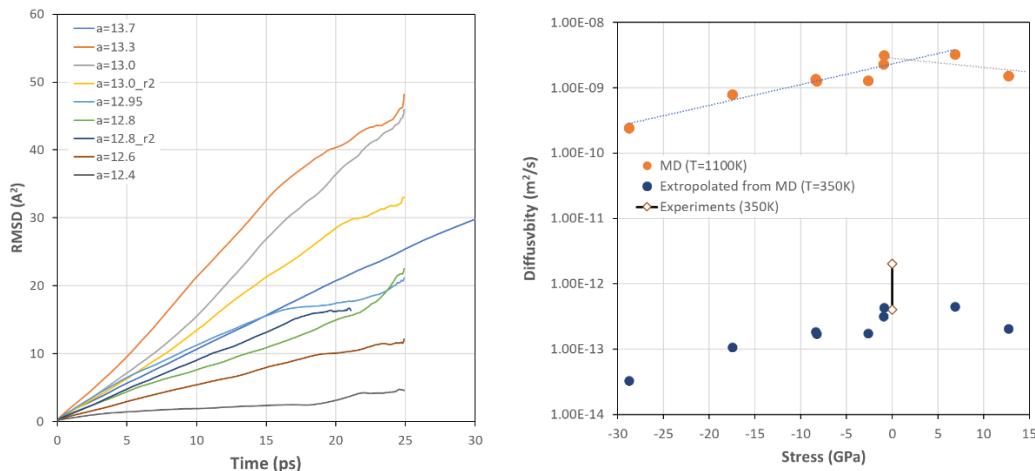


Figure 2: The simulated (left) average Li RMSD vs. simulation time with varying lattice parameters, (right) the Li self-diffusivity as a function of stress (positive means tension).

experimental values $0.4 - 2 \times 10^{-12} \text{ m}^2/\text{s}$ ⁶⁷, supporting the MD simulation results. It is not surprising to see that the Li diffusivity peaks around 2GPa tensile stress, because fast ionic conductivity in LLZO is enabled by low-barrier concerted ion migrations, which are triggered by the strong ion-ion Coulomb interactions at unique ion configurations. While compression shrinks the free volume available for Li ion mobility, high tension may also reduce the Coulomb interactions required for fast ion conductivity.

Although the Li diffusivity decreases under compression, even at 10GPa compression the diffusivity is still 40% of its value at zero stress. This difference is even less than the variation of the experimental data at zero stress. Consistent with our results, we note that the experimentally measured Li ion conductivity in LLZO showed minimal changes under compressive residual stresses between 12.5Mpa and 50Mpa⁶⁹. Therefore, we conclude that even very large compressive stresses will not have a large impact on Li ion diffusion over short distances.

Methods for Applying Compressive Stress

As mentioned above, SCC can only occur when the surface is in tension, so a highly successful and widely used strategy for preventing SCC has been to put the component's surface into compression. If this residual compressive stress is high enough, cracks are difficult to form and grow, and cracks that exist are forced to close. Among the most widely used techniques to introduce a surface residual compressive stress in metals is shot peening⁷⁰⁻⁷³, which is a cold working process where large numbers of small hard particles (metallic, ceramic or glass) impinge on the component with sufficient force to deform it plastically and put the surface into compression^{74,75}. For brittle materials such as ceramics and glasses, other techniques have been developed for commercial application. Among them are laser shock peening (LSP), which can

give compressive stresses of up to 500 MPa in aluminum oxide⁷⁶; ion implantation^{77,78}; and ion exchange^{47,79} (which is used to make Gorilla Glass⁵³). The latter techniques can introduce compressive residual stresses as high as 10 GPa in aluminum oxide⁷⁸. We next consider each of these approaches, except for shot peening, for use with LLZO.

LSP introduces laser plasma-driven shock-waves into a material, typically using a plasma-confining medium (e.g., glass or water) to increase the peak pressure of the shock wave. A sacrificial layer is often used to protect the treated sample from laser ablation. Shukla et al⁷⁶ demonstrated that his LSP-treated a-Al₂O₃ had a biaxial compressive residual stress of several hundred MPa that extended to a depth of up to 1.2 mm from the surface.

Ion exchange⁸⁰ has also been used to introduce compressive stresses at the surface by exchanging alkali (or sometimes alkaline-earth) ions in the original glass/glass-ceramic with larger ones from a molten salt bath. The introduction of large ions near the surface induces a volume increase, generating a compressive stress in the ion-exchange region. The final mechanical properties are dependent on the stress level at the surface and the depth of penetration of the larger ions.

Unfortunately, the uses of these strengthening strategies for preventing Li dendrite penetration through solid electrolytes face potentially severe constraints. In the case of ion exchange, only a limited selection of ions can be introduced near the SE surface in a wet process. Also, ion exchange strongly favors the exchange of monovalent ions—replacing the Li in this case—which would change the chemical identity of the solid electrolyte and, likely, inhibit Li ion mobility in the exchanged region. While LSP avoids these problems, it generally creates heterogeneous surface damage that could increase the interface resistance; it can also create local tensile stresses⁷⁶.

Furthermore, the range of stresses introduced by LSP, up to hundreds of MPa, is much lower than what is possible with other techniques.

The better alternative, in our estimation, is ion implantation, which can be used to introduce residual surface compressive stresses with control of stress level, depth profile, crystallinity, and chemistry in the near-surface region (10 to 1,000 nm). It has been used commercially to strengthen polymers, glasses and ceramics for decades to solve stress corrosion cracking (SCC) or static fatigue, but it has not been applied to SEs, to our knowledge. An advantage of ion implantation is the large number of chemical, structural, and physical states that can be created, including metastable and non-equilibrium states, for nano/mesoscale tailoring the surface structure of SEs.

Energetic implanted ions can include transition metal ions, halide ions, rare gas ions, and even lithium ions, which can modify the surface structure—including creating local disorder—leading new mechanical properties for solid electrolytes, as illustrated schematically in

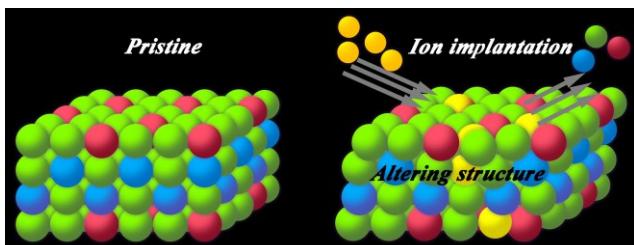


Figure 3: Scheme of using ion implantation to alter structure of solid electrolytes.

Figure 3. With its control of dopant species, concentration, and spatial distribution (implantation depth), ion implantation has also been widely used in modifying electronic properties of semiconductors for the microelectronics industry, as well as strengthening of metals and non-conducting ceramics⁸¹. Recent work has shown a positive impact of using ion beam modification on the ionic conductivity of polymer electrolyte films due to increased charge carries and dielectric constant.

Finally, we note that introduction of compressive residual surface stresses would be expected to make any SE less brittle and, thus, easier to handle in a commercial environment. We expect that implantation of solid electrolytes will create materials with new properties that can be tailored to improve those of solid-state ion-conducting materials.

Conclusion and Perspective

In summary, we have proposed a new paradigm for inhibiting dendrite penetration through solid electrolytes: putting the SE surfaces into a state of residual compressive stress, which can suppress the crack formation that accompanies dendrite penetration. We have performed MD simulations to demonstrate that the introduction of even very high (~ 10 GPa) hydrostatic compressive stresses into LLZO has only a modest impact on Li diffusion kinetics, enabling our proposal. Our approach is based on its success in solving stress corrosion cracking and static fatigue problems in metals, ceramics, and glasses in commercial products. In addition to inhibiting dendrite penetration in solid electrolytes, compressive stresses on the order of GPa will improve their fracture toughness and will tend to suppress lithium plating inside of solid electrolytes because of an increased overpotential. While there are a number of techniques that can be used commercially to introduce compressive residual stresses, we suggest that ion implantation will be the most useful for this purpose, as it may provide a new avenue for developing high-performance and stable solid electrolytes.

METHODS

A periodic cubic cell of $\text{Li}_{24}\text{La}_{24}\text{Zr}_{16}\text{O}_{96}$ was simulated using GULP software and implemented in Materials Studio with a force-field including the long-range Coulombic potential, the short-range Buckingham potential, and a core–shell polarizable potential for O atoms following the parameters

provided in⁸². The simulation cell length was varied from 12.4 Å to 13.7 Å, and the root mean square displacement (RMSD) of Li⁺ ions was tracked during NVT (fixed cell) dynamics.

AUTHOR CONTRIBUTIONS

S.J.H. and C. B. proposed the idea and concepts. Y.Q. did the calculations. All authors contributed equally to the writing of the manuscript.

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References:

- 1 Lin, D., Liu, Y. & Cui, Y. Reviving the lithium metal anode for high-energy batteries. *Nature nanotechnology* **12**, 194 (2017).
- 2 Cheng, E. J., Sharafi, A. & Sakamoto, J. Intergranular Li metal propagation through polycrystalline Li_{6.25}Al_{0.25}La₃Zr₂O₁₂ ceramic electrolyte. *Electrochimica Acta* **223**, 85-91 (2017).
- 3 Cheng, X.-B., Zhang, R., Zhao, C.-Z. & Zhang, Q. Toward safe lithium metal anode in rechargeable batteries: a review. *Chemical reviews* **117**, 10403-10473 (2017).
- 4 Feng, X. *et al.* Thermal runaway mechanism of lithium ion battery for electric vehicles: A review. *Energy Storage Materials* **10**, 246-267 (2018).

5 Bieker, G., Winter, M. & Bieker, P. Electrochemical in situ investigations of SEI and dendrite formation on the lithium metal anode. *Physical Chemistry Chemical Physics* **17**, 8670-8679 (2015).

6 Harris, S. J., Timmons, A. & Pitz, W. J. A combustion chemistry analysis of carbonate solvents used in Li-ion batteries. *Journal of Power Sources* **193**, 855-858 (2009).

7 Porz, L. *et al.* Mechanism of lithium metal penetration through inorganic solid electrolytes. *Advanced Energy Materials* **7**, 1701003 (2017).

8 Tikekar, M. D., Choudhury, S., Tu, Z. & Archer, L. A. Design principles for electrolytes and interfaces for stable lithium-metal batteries. *Nature Energy* **1**, 16114 (2016).

9 Wu, B. *et al.* The role of the solid electrolyte interphase layer in preventing Li dendrite growth in solid-state batteries. *Energy & Environmental Science* **11**, 1803-1810 (2018).

10 Monroe, C. & Newman, J. Dendrite growth in lithium/polymer systems a propagation model for liquid electrolytes under galvanostatic conditions. *Journal of The Electrochemical Society* **150**, A1377-A1384 (2003).

11 Monroe, C. & Newman, J. The effect of interfacial deformation on electrodeposition kinetics. *Journal of The Electrochemical Society* **151**, A880-A886 (2004).

12 Barai, P., Higa, K. & Srinivasan, V. Effect of initial state of lithium on the propensity for dendrite formation: a theoretical study. *Journal of The Electrochemical Society* **164**, A180-A189 (2017).

13 Zhang, X. *et al.* Rethinking How External Pressure Can Suppress Dendrites in Lithium Metal Batteries. *Journal of The Electrochemical Society* **166**, A3639-A3652 (2019).

14 Louli, A. J. *et al.* Exploring the Impact of Mechanical Pressure on the Performance of Anode-Free Lithium Metal Cells. *Journal of The Electrochemical Society* **166**, A1291-A1299, doi:10.1149/2.0091908jes (2019).

15 Zhang, X., Wang, Q. J., Harrison, K. L., Roberts, S. A. & Harris, S. J. Pressure-Driven Interface Evolution in Solid-State Lithium Metal Batteries. *Cell Reports Physical Science* **1**, 100012 (2020).

16 Klinsmann, M., Hildebrand, F. E., Ganser, M. & McMeeking, R. M. Dendritic cracking in solid electrolytes driven by lithium insertion. *Journal of Power Sources* **442**, 227226 (2019).

17 Tian, H.-K., Liu, Z., Ji, Y., Chen, L.-Q. & Qi, Y. Interfacial Electronic Properties Dictate Li Dendrite Growth in Solid Electrolytes. *Chemistry of Materials* **31**, 7351-7359 (2019).

18 Cheng, X. B. *et al.* Dendrite-free lithium deposition induced by uniformly distributed lithium ions for efficient lithium metal batteries. *Advanced Materials* **28**, 2888-2895 (2016).

19 Zhang, R. *et al.* Conductive nanostructured scaffolds render low local current density to inhibit lithium dendrite growth. *Advanced Materials* **28**, 2155-2162 (2016).

20 Li, W. *et al.* The synergetic effect of lithium polysulfide and lithium nitrate to prevent lithium dendrite growth. *Nature communications* **6**, 7436 (2015).

21 Liu, Y. *et al.* Lithium-coated polymeric matrix as a minimum volume-change and dendrite-free lithium metal anode. *Nature communications* **7**, 10992 (2016).

22 Khurana, R., Schaefer, J. L., Archer, L. A. & Coates, G. W. Suppression of lithium dendrite growth using cross-linked polyethylene/poly (ethylene

oxide) electrolytes: a new approach for practical lithium-metal polymer batteries. *J Am Chem Soc* **136**, 7395-7402 (2014).

23 Ding, F. *et al.* Dendrite-free lithium deposition via self-healing electrostatic shield mechanism. *J Am Chem Soc* **135**, 4450-4456 (2013).

24 Ren, Y., Shen, Y., Lin, Y. & Nan, C.-W. Direct observation of lithium dendrites inside garnet-type lithium-ion solid electrolyte. *Electrochemistry Communications* **57**, 27-30, doi:10.1016/j.elecom.2015.05.001 (2015).

25 Zhang, Y. *et al.* Dendrite-free lithium deposition with self-aligned nanorod structure. *Nano letters* **14**, 6889-6896 (2014).

26 Zhou, W. *et al.* Plating a dendrite-free lithium anode with a polymer/ceramic/polymer sandwich electrolyte. *J Am Chem Soc* **138**, 9385-9388 (2016).

27 Brousse, T., Retoux, R., Herterich, U. & Schleich, D. Thin-film crystalline SnO₂-lithium electrodes. *Journal of The Electrochemical Society* **145**, 1-4 (1998).

28 Dudney, N. J. Addition of a thin-film inorganic solid electrolyte (Lipon) as a protective film in lithium batteries with a liquid electrolyte. *Journal of power sources* **89**, 176-179 (2000).

29 Yang, C.-P., Yin, Y.-X., Zhang, S.-F., Li, N.-W. & Guo, Y.-G. Accommodating lithium into 3D current collectors with a submicron skeleton towards long-life lithium metal anodes. *Nature communications* **6**, 8058 (2015).

30 Lin, D. *et al.* Layered reduced graphene oxide with nanoscale interlayer gaps as a stable host for lithium metal anodes. *Nat Nanotechnol* **11**, 626 (2016).

31 Kozen, A. C. *et al.* Next-generation lithium metal anode engineering via atomic layer deposition. *ACS nano* **9**, 5884-5892 (2015).

32 Zeng, S. *et al.* Robust interface layers with redox shuttle reactions suppress the dendrite growth for stable solid-state Li metal batteries. *Journal of Energy Chemistry* (2020).

33 Zhao, C.-Z. *et al.* An anion-immobilized composite electrolyte for dendrite-free lithium metal anodes. *Proceedings of the National Academy of Sciences* **114**, 11069-11074 (2017).

34 Chi, S. S., Liu, Y., Song, W. L., Fan, L. Z. & Zhang, Q. Prestoring lithium into stable 3D nickel foam host as dendrite-free lithium metal anode. *Advanced Functional Materials* **27**, 1700348 (2017).

35 Zheng, G. *et al.* Interconnected hollow carbon nanospheres for stable lithium metal anodes. *Nat Nanotechnol* **9**, 618 (2014).

36 Ishikawa, M., Kanemoto, M. & Morita, M. Control of lithium metal anode cycleability by electrolyte temperature. *Journal of power sources* **81**, 217-220 (1999).

37 Eliaz, N., Shachar, A., Tal, B. & Eliezer, D. Characteristics of hydrogen embrittlement, stress corrosion cracking and tempered martensite embrittlement in high-strength steels. *Engineering Failure Analysis* **9**, 167-184 (2002).

38 Raja, V. & Shoji, T. *Stress corrosion cracking: theory and practice*. (Elsevier, 2011).

39 Zeng, R.-c. *et al.* Review of studies on corrosion of magnesium alloys. *Transactions of Nonferrous Metals Society of China* **16**, s763-s771 (2006).

40 Anderson, O. L. & Grew, P. C. Stress corrosion theory of crack propagation with applications to geophysics. *Reviews of Geophysics* **15**, 77-104 (1977).

41 Harris, S. J. & Lu, P. Effects of Inhomogeneities—Nanoscale to Mesoscale—on the Durability of Li-Ion Batteries. *The Journal of Physical Chemistry C* **117**, 6481-6492, doi:10.1021/jp311431z (2013).

42 Pereira, H. B., Panossian, Z., Baptista, I. P. & Azevedo, C. R. d. F. Investigation of stress corrosion cracking of austenitic, duplex and super duplex stainless steels under drop evaporation test using synthetic seawater. *Materials Research* **22** (2019).

43 Rao, A. U., Vasu, V., Govindaraju, M. & Srinadh, K. S. Stress corrosion cracking behaviour of 7xxx aluminum alloys: a literature review. *Transactions of Nonferrous Metals Society of China* **26**, 1447-1471 (2016).

44 Lichtenstein, A. G. The silver bridge collapse recounted. *Journal of performance of constructed facilities* **7**, 249-261 (1993).

45 *Silver Bridge*, <https://en.wikipedia.org/wiki/Silver_Bridge> (

46 Wiederhorn, S. & Bolz, L. Stress corrosion and static fatigue of glass. *Journal of the American Ceramic Society* **53**, 543-548 (1970).

47 Gy, R. Stress corrosion of silicate glass: a review. *Journal of non-crystalline solids* **316**, 1-11 (2003).

48 Lade, P. V. & Karimpour, H. Static fatigue controls particle crushing and time effects in granular materials. *Soils and foundations* **50**, 573-583 (2010).

49 Purnell, P. & Beddows, J. Durability and simulated ageing of new matrix glass fibre reinforced concrete. *Cement and Concrete Composites* **27**, 875-884 (2005).

50 Teoh, S. Fatigue of biomaterials: a review. *International journal of fatigue* **22**, 825-837 (2000).

51 Seaman, J. H., Blanchet, T. A. & Tomozawa, M. Origin of the static fatigue limit in oxide glasses. *Journal of the American Ceramic Society* **99**, 3600-3609 (2016).

52 *Different types of corrosion*, WebCorr Corrosion Consulting Services, <https://www.corrosionclinic.com/types_of_corrosion/intergranular_corrosion_cracking.htm> (

53 Li, X., Jiang, L., Zhang, X. & Yan, Y. Influence of residual compressive stress on nanoindentation response of ion-exchanged aluminosilicate float glass on air and tin sides. *Journal of non-crystalline solids* **385**, 1-8 (2014).

54 Yamada, H. in *Solid Electrolytes for Advanced Applications* 91-110 (Springer, 2019).

55 Garcia-Mendez, R., Smith, J. G., Neuefeind, J. C., Siegel, D. J. & Sakamoto, J. Correlating Macro and Atomic Structure with Elastic Properties and Ionic Transport of Glassy Li₂S-P₂S₅ (LPS) Solid Electrolyte for Solid-State Li Metal Batteries. *Advanced Energy Materials* (2020).

56 Trail, S. & Bowen, P. Effects of stress concentrations on the fatigue life of a gamma-based titanium aluminide. *Materials Science and Engineering: A* **192**, 427-434 (1995).

57 Liu, D., Shi, Y., Lin, X. & Xian, C. Study on improving surface residual stress of polished blade after polishing based on two-stage parameter method. *The International Journal of Advanced Manufacturing Technology* **100**, 1491-1503 (2019).

58 Marshall, D. & Lawn, B. R. Residual stress effects in sharp contact cracking. *Journal of materials science* **14**, 2001-2012 (1979).

59 Wu, D., Wang, H., Zhang, K. & Lin, X. Research on flexible adaptive CNC polishing process and residual stress of blisk blade. *The International Journal of Advanced Manufacturing Technology* **103**, 2495-2513 (2019).

60 Pan, J. *et al.* Effects of stress on lithium transport in amorphous silicon electrodes for lithium-ion batteries. *Nano Energy* **13**, 192-199 (2015).

61 Fluri, A., Pergolesi, D., Roddatis, V., Wokaun, A. & Lippert, T. In situ stress observation in oxide films and how tensile stress influences oxygen ion conduction. *Nature communications* **7**, 10692 (2016).

62 Bucci, G., Talamini, B., Renuka Balakrishna, A., Chiang, Y.-M. & Carter, W. C. Mechanical instability of electrode-electrolyte interfaces in solid-state batteries. *Physical Review Materials* **2**, doi:10.1103/PhysRevMaterials.2.105407 (2018).

63 De Souza, R. A., Ramadan, A. & Hörner, S. Modifying the barriers for oxygen-vacancy migration in fluorite-structured CeO₂ electrolytes through strain: a computer simulation study. *Energy & Environmental Science* **5**, 5445-5453 (2012).

64 Chen, B. *et al.* Strain tunable ionic transport properties and electrochemical window of Li₁₀GeP₂S₁₂ superionic conductor. *Computational Materials Science* **153**, 170-175 (2018).

65 Atkinson, A. & Ramos, T. Chemically-induced stresses in ceramic oxygen ion-conducting membranes. *Solid State Ionics* **129**, 259-269 (2000).

66 Liu, W., Liu, H., Ou, G. & Pan, W. Residual stress-dependent electric conductivity of sputtered co-doped CeO₂ thin-film electrolyte. *Journal of Applied Physics* **109**, 084321 (2011).

67 Hayamizu, K., Terada, Y., Kataoka, K., Akimoto, J. & Haishi, T. Relationship between Li⁺ diffusion and ion conduction for single-crystal and powder garnet-type electrolytes studied by ⁷Li PGSE NMR spectroscopy. *Physical Chemistry Chemical Physics* **21**, 23589-23597 (2019).

68 Moradabadi, A. & Kaghazchi, P. Effect of lattice and dopant-induced strain on the conductivity of solid electrolytes: application of the elastic dipole method. *Materialia* **9**, 100607 (2020).

69 Yamada, H., Ito, T., Basappa, R. H., Bekarevich, R. & Mitsuishi, K. Influence of strain on local structure and lithium ionic conduction in garnet-type solid electrolyte. *Journal of Power Sources* **368**, 97-106 (2017).

70 Hammond, D. & Meguid, S. Crack propagation in the presence of shot-peening residual stresses. *Engineering Fracture Mechanics* **37**, 373-387 (1990).

71 Kobayashi, M., Matsui, T. & Murakami, Y. Mechanism of creation of compressive residual stress by shot peening. *International journal of fatigue* **20**, 351-357 (1998).

72 Meguid, S., Shagal, G., Stranart, J. & Daly, J. Three-dimensional dynamic finite element analysis of shot-peening induced residual stresses. *Finite elements in analysis and design* **31**, 179-191 (1999).

73 Wang, S., Li, Y., Yao, M. & Wang, R. Compressive residual stress introduced by shot peening. *Journal of Materials Processing Technology* **73**, 64-73 (1998).

74 Mochizuki, M. Control of welding residual stress for ensuring integrity against fatigue and stress-corrosion cracking. *Nuclear Engineering and Design* **237**, 107-123 (2007).

75 Mahmoudi, A., Ghasemi, A., Farrahi, G. & Sherafatnia, K. A comprehensive experimental and numerical study on redistribution of residual stresses by shot peening. *Materials & Design* **90**, 478-487 (2016).

76 Shukla, P. P., Swanson, P. T. & Page, C. J. Laser shock peening and mechanical shot peening processes applicable for the surface treatment of technical grade ceramics: a review. *Proceedings of the Institution of Mechanical Engineers, Part B: Journal of Engineering Manufacture* **228**, 639-652 (2014).

77 Burnett, P. & Page, T. F. An investigation of ion implantation-induced near-surface stresses and their effects in sapphire and glass. *Journal of materials science* **20**, 4624-4646 (1985).

78 McHargue, C., O'hern, M., White, C. & Lewis, M. Ion implantation in ceramics-residual stress and properties. *Materials Science and Engineering: A* **115**, 361-367 (1989).

79 Abouelleil, M. M. Ion exchange in glasses and crystals. *Annual Review of Materials Science* **23**, 255-268 (1993).

80 Chen, W. W. & Wang, Q. J. Thermomechanical analysis of elastoplastic bodies in a sliding spherical contact and the effects of sliding speed, heat partition, and thermal softening. *Journal of Tribology* **130**, 041402 (2008).

81 Conrad, J. R., Radtke, J. L., Dodd, R. A., Worzala, F. J. & Tran, N. C. Plasma source ion-implantation technique for surface modification of materials. *Journal of Applied Physics* **62**, 4591-4596 (1987).

82 Klenk, M. & Lai, W. Local structure and dynamics of lithium garnet ionic conductors: tetragonal and cubic Li₇La₃Zr₂O₇. *Physical Chemistry Chemical Physics* **17**, 8758-8768 (2015).