



Thickness-utilizing deployable hard stops for origami-based design applications

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Abstract. This work develops and presents design concepts and models of thickness-utilizing deployable hard stops (ThUDS) which can be incorporated into origami-based design applications to provide stability in specific fold states. A ThUDS, like a lamina-emergent mechanism, emerges from a flat state and can reside within a sheet. A variety of planar and spherical ThUDS configurations are developed and presented, using diagrams, equations, and prototypes. Examples of ThUDS applications are given and attributes are discussed. Considerations for the design of a ThUDS are discussed. This work outlines how a ThUDS can maintain foldability while improving stability and utilizing thickness. Parameter values for prototypes are also given for reader reproduction.

1 Introduction

Origami has found uses in numerous engineering and design applications such as small soft robots (Banerjee et al., 2018), DNA mechanisms (Su et al., 2017), transformable metamaterials (Yang and You, 2018), energy absorbers (Ma et al., 2019), and an optimized jumping mechanism (Sadeghi et al., 2019). In many applications, such as those seen in current origami-based products on the market, it is necessary to block motion and provide stability in a desired configuration (Avila et al., 2019).

Greenwood et al. (2020) developed a method for determining which techniques could be used to stabilize an origami pattern or origami-inspired device. Suggested techniques include using strain energy (Yasuda et al., 2016), compliant mechanisms (Zhang et al., 2019), and heating (Deng and Chen, 2015). Yasuda et al. (2019) recently proposed programmable structures for obtaining stability under a load. Multiple different methods were suggested by Yellowhorse and Howell (2018) for providing stiffness in origami-inspired designs. Other stiffness-based methods include using coupled origami tubes (Filipov et al., 2015, 2019), stacking origami patterns (Fang et al., 2018), and origami-tube interleaving (Cheung et al., 2014). Generally, these methods act at the joints or add increased complexity to the system.

In previous work, the authors developed two categories of deployable transcrease hard stop models that block the motion of an origami pattern in a desired fold state while maintaining the original crease locations (Andrews et al., 2019). Transcrease refers to the hard stops lying across the crease. Deployable transcrease hard stops implement cuts into the origami, making it kirigami (sometimes referred to as “pop-up origami”; Bernard et al., 2018). Since these models were developed for origami, they are based on the zero-thickness assumption of paper. Therefore, they cannot be directly implemented in origami-based applications without accommodating for thickness.

Various thickness-accommodation techniques have been developed for adapting origami designs to thicker materials (Morgan et al., 2016; Lang et al., 2018). Tachi (2011) developed an early technique that allowed for foldability while maintaining the kinematics of the original origami pattern. Chen et al. (2015) outlined equations for calculating panel thicknesses based on spherical linkages. Ku and Demaine (2016) developed algorithms to aid in developing folding patterns in thick materials. Later, Ku (2017) developed a technique that strategically removes material on both sides of a crease, allowing panels to fold to a specified angle. A technique using linkages at the joints was also recently created (Lang et al., 2020). Butler et al. (2020) developed a technique that incorporates compliant sheets. These techniques usually

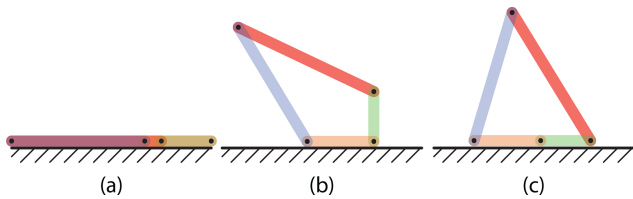


Figure 1. Theoretical diagram of ThUDS in (a) flat, (b) deploying, and (c) blocked deployed states.

involve the strategic removal or arrangement of material to enable folding.

The developments presented in this paper represent a transition from accommodating thickness to utilizing thickness. Ku (2017) started down this path by developing a technique that blocks motion at dihedral angles less than 90° through adjusting the removal of material near the joint. This paper continues to utilize thickness by illustrating thickness-utilizing deployable hard stops (ThUDS), which allow motion to be blocked at any angle and obtain stability. Two categories of ThUDS are outlined that block motion of a moving joint at a specified angle. A general form is given for each category, followed by special cases and adaptations. Diagrams and physical examples are given for each category. Finally, examples are given to show applications for ThUDS.

2 Overview

Thickness-utilizing deployable hard stops (ThUDS) are mechanisms that are designed to block motion at a desired angle using self-interference. ThUDS utilize the thickness of the material to assist with motion blocking and stability within folded systems. This primarily occurs through surface contact between contacting links, which can occur in multiple directions. Similar to lamina-emergent mechanisms (LEMs; Jacobsen et al., 2010), ThUDS originate in a flat, planar state and are deployed to be a functional, 3D structure. Because of this, ThUDS have direct applications in origami-based systems, with the ability to add necessary stability while allowing for folding.

Figure 1 depicts how this works. Figure 1a shows the mechanism in its flat, initial state, Fig. 1b shows the ThUDS deploying, and Fig. 1c shows the mechanism in its final, blocked state. The colors of each link refer to a specific portion of the mechanism, as follows:

- orange – ground link
- blue – blocked link
- red – stabilizing link
- green – interfering link.

In practice, the ground link is extended beyond the joint, such that the green interfering link comes in contact with it at the

end of its motion (typically 180°). Other angles could be used but would require additional material thickness to accommodate the decreased interference angle.

ThUDS can be separated into two categories, namely deploying strut and sector panel. The deploying strut ThUDS category has two subcategories, namely planar and spherical. They are developed from the general planar transcrease hard stop (PTHS) model for zero-thickness deployable transcrease hard stops (Andrews et al., 2019). A sector panel ThUDS is similar to self-blocking degree-4 origami vertices (Foschi and Tachi, 2018) with panels (like origami facets) rather than discrete links. They are developed from the general spherical transcrease hard stop (STHS) model for zero-thickness deployable transcrease hard stops (Andrews et al., 2019).

In the following sections the general form of each category is outlined using diagrams and examples. Examples were 3D printed and assembled with tape joints. Special cases and adaptations for each are also presented. Special cases refer to adjusting the general equations, such as for obtaining flat foldability, whereas adaptations refer to changing the general definition for various reasons, such as inverting motion.

3 Deploying strut ThUDS

Planar and spherical deploying strut ThUDS are illustrated using diagrams, equations, and examples. Parameter values for the examples are given in Appendix A in Tables A1 (planar) and A2 (spherical).

3.1 Planar deploying strut ThUDS

A planar deploying strut ThUDS is a self-interfering four-bar mechanism that blocks motion in a desired state and is defined by the following:

$$L_1 + L_2 = L_3 + L_4 \quad (1)$$

$$L_1 + d_1 i + d_2 i e^{i\rho_d} - L_2 e^{i\rho_d} - d_3 i e^{i\rho_d} + d_4 i e^{i\theta} + L_3 e^{i\theta} - d_5 i e^{i\theta} + d_6 i + L_4 = 0, \quad (2)$$

where ρ_d is the dihedral angle, θ is the strut angle, $L_1 - L_4$ are link lengths, $d_1 - d_6$ are joint offsets (positive directions shown), and $P_1 - P_4$ are joint reference planes. Dimensions and reference planes (dashed lines) are depicted in Fig. 2. Joints are denoted as J_{12} , J_{23} , J_{34} , and J_{41} , which are shown in Fig. 3 for 3D reference. Each joint offset relates a joint to a joint reference plane, with J_{41} constrained to be located on P_1 to reduce the number of joint offset parameters from 8 to 6. It can be helpful, but not necessary, to use external surfaces as joint reference planes (see Fig. 2b).

Equation (2) is derived using a complex vector loop beginning at J_{41} and moving clockwise. This single equation results in two solvable equations by employing Euler's formula ($e^{ix} = \cos x + i \sin x$; Howell, 2001).

In practice, one would select values for the dihedral angle, two of the link lengths, and all joint offsets while the values

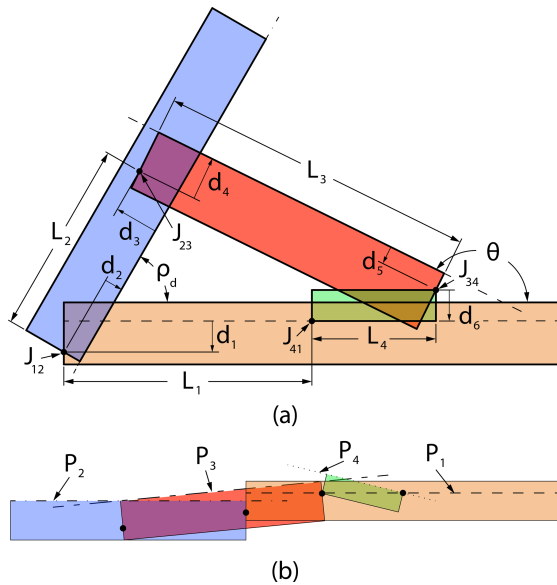


Figure 2. General diagram for a planar deploying strut ThUDS with key parameters shown. Showing side views in the (a) deployed and (b) flat states. Dashed lines designate joint reference planes. Joint offset (d) arrows denote the parameter's (P) positive direction.

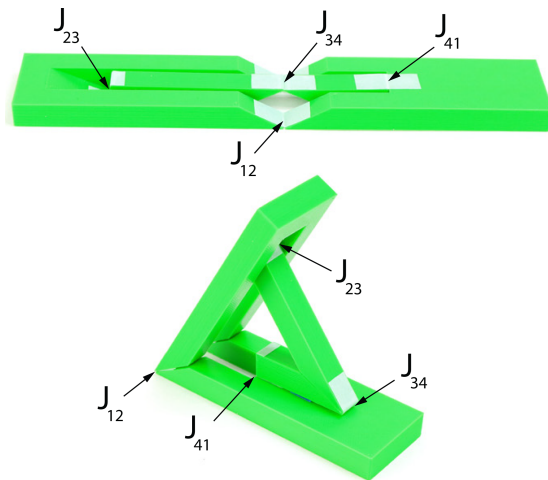


Figure 3. Example of a planar deploying strut ThUDS with joints J_{34} and J_{41} on the top surface and joints J_{12} and J_{23} on the bottom surface. Shown in flat and deployed states. Joint names shown for reference.

for the two remaining link lengths and strut angle are calculated.

Any joint offset value may be used. This can result in links 3 and 4 not being parallel to links 1 and 2 in the flat state (see Fig. 2b). Figure 4 shows an example of a 0.5 in. (12.7 mm) thick planar deploying strut ThUDS with joint offset values arbitrarily selected, such that J_{34} protrudes beyond the upper surface in the flat state.



Figure 4. Planar deploying strut ThUDS with arbitrary joint offsets. Shown in flat and deployed states.

For all links to be parallel in the flat state and reside completely within the thickness, as shown in Fig. 3, the joint offset values must form a closed loop, such that the following applies:

$$d_1 - d_2 + d_3 - d_4 + d_5 - d_6 = 0. \quad (3)$$

This would also result in parallel joint reference frames.

Joint offset values can be selected to allow for loads to be carried through the links and thus bypass the joints using the isolation principle (Guérinot et al., 2005). In this way, the material thickness is being utilized by creating surface contact between links. An example of this is shown in Fig. 3, where joints J_{12} and J_{23} are placed on the bottom surface and joints J_{34} and J_{41} are placed on the top surface. This allows link L_4 to rotate 180° before interfering with link L_1 , while also allowing for contact between all other pairs of adjacent links.

3.2 Spherical deploying strut ThUDS

A curved version of a planar deploying strut ThUDS, Fig. 5 diagrams a general spherical deploying strut ThUDS, which is defined by Eq. (3) and the following:

$$\alpha_1 + \alpha_2 = \alpha_3 + \alpha_4 \quad (4)$$

$$\beta = \alpha_1 + \alpha_4 \quad (5)$$

$$\begin{aligned} \rho_d = \cos^{-1} & \left(\frac{\cos(\phi_2) \sin(\alpha_2)}{\sin(\psi_2)} \right) \\ & + \cos^{-1} \left(\frac{\cos(\xi_3) - \cos(\xi_2) \cos(\xi_\beta)}{\sin(\xi_2) \sin(\xi_\beta)} \right) \\ & + \cos^{-1} \left(\frac{\cos(\phi_\beta) \sin(\beta)}{\sin(\psi_\beta)} \right), \end{aligned} \quad (6)$$

where ρ_d is the dihedral angle, $\alpha_1 - \alpha_4$ are the link sector angles, β is the total ground sector angle, and $d_1 - d_6$ are

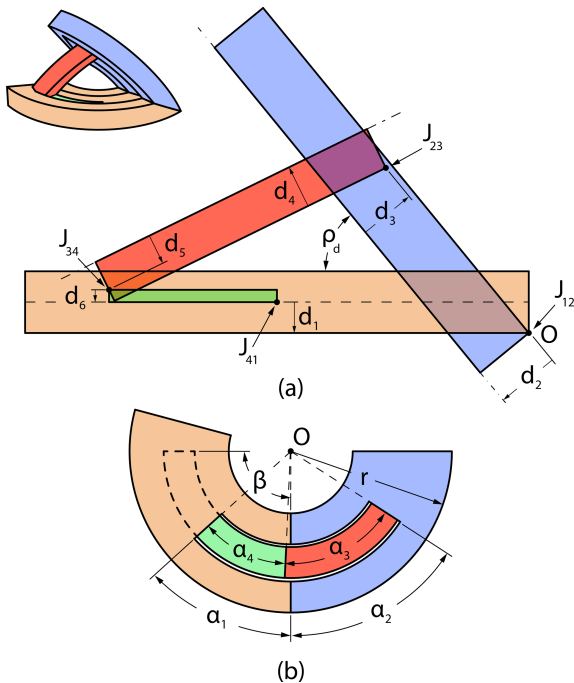


Figure 5. General diagram for a spherical deploying strut ThUDS with key parameters shown. Showing (a) the projection of the outer surface (isometric view) in the deployed state and (b) the flat state from above. Dashed lines in (b) show the position of link 4 in the deployed state. Joints rotate about O .

joint offsets. Intermediate variables ϕ_2 , ϕ_β , ξ_2 , ξ_3 , and ξ_β used in Eq. (6) are defined by the following:

$$\cos(\phi_2) = \frac{r}{\sqrt{r^2 + (d_2 - d_3)^2}} \quad (7)$$

$$\cos(\phi_\beta) = \frac{r}{\sqrt{r^2 + (d_1 + d_6)^2}} \quad (8)$$

$$\cos(\xi_2) = \frac{r \cos(\alpha_2)}{\sqrt{r^2 + (d_2 - d_3)^2}} = \cos(\alpha_2) \cos(\phi_2) \quad (9)$$

$$\cos(\xi_3) = \frac{r^2 \cos(\alpha_3) + (d_2 - d_3)(d_1 - d_6)}{\sqrt{r^2 + (d_2 - d_3)^2} \sqrt{r^2 + (d_1 - d_6)^2}} \quad (10)$$

$$\cos(\xi_\beta) = \frac{r \cos(\beta)}{\sqrt{r^2 + (d_1 + d_6)^2}} = \cos(\alpha_\beta) \cos(\phi_\beta), \quad (11)$$

where ϕ_2 and ϕ_β represent joint offset angles, and ξ_2 , ξ_3 , and ξ_β represent equivalent link sector angles. Joint reference planes are defined in the same way as in the planar sub-category (see Fig. 2b). Joints are denoted in Fig. 6 for 3D reference.

The joint offset values are defined on the surface of a cylinder of radius, r , within which the spherical deploying strut ThUDS is defined (see Fig. 5b). It is important to note that the joint axis for each joint must pass through a single point (O) at the center of this cylinder, thus maintaining the spherical deploying strut ThUDS as a spherical mechanism.

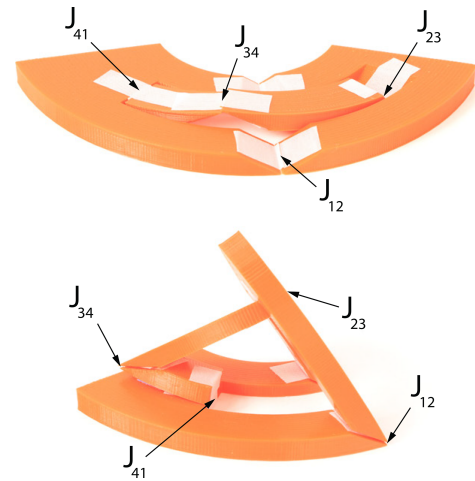


Figure 6. Example of a spherical deploying strut ThUDS. Shown in flat and deployed states. Joint names shown for reference.

Figure 6 shows a general example of a spherical deploying strut ThUDS. Joints J_{12} and J_{23} lie on the base surface, and joints J_{34} and J_{41} lie on the upper surface, which is at an angle with respect to the base surface. Contact is created between each pair of adjacent links (compare to Fig. 3).

In practice, one would select values for the dihedral angle, two of the sector angles ($\alpha_1 - \alpha_4$, β), and all joint offsets while the values for the three remaining sector angles are calculated along with the five intermediate angles. A nonlinear solver may be required.

3.3 Special case: thickened PTHS model

In some instances it is desirable to simplify a deploying strut ThUDS, such as for faster prototyping or simpler manufacturing. By placing all the joints on the same plane (setting d_1 through d_6 to be 0), Eq. (2) becomes the following:

$$L_1 - L_2 e^{i\rho_d} + L_3 e^{i\theta} + L_4 = 0, \quad (12)$$

and Eq. (6), for the spherical case, reduces to the following:

$$\cos(\rho_d) = \frac{\cos(\alpha_3) - \cos(\alpha_2)\cos(\beta)}{\sin(\alpha_2)\sin(\beta)}, \quad (13)$$

with no intermediate variables needing to be calculated.

This simplification creates this special case, which is simply a thickened version of the PTHS model (Andrews et al., 2019), with link lengths or sector angles measured on the model joint plane.

Figure 7 shows a physical example of a thickened PTHS model planar deploying strut ThUDS, which is based on the general PTHS model. A similar spherical example is shown in Fig. 8. Both examples have the same dihedral angle of 60° . In these examples, thickness is added in a single direction. Thickness can be utilized by adding material both above and beneath the joint plane, creating additional surface contact between the links.

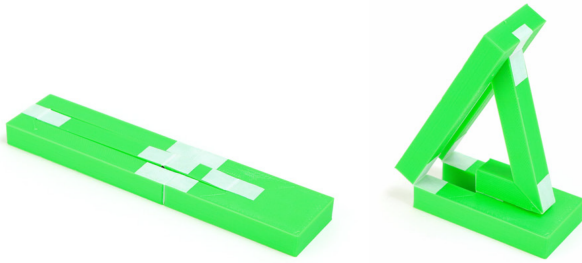


Figure 7. A simplified planar deploying strut ThUDS based on the general PTHS model (Andrews et al., 2019). Shown in flat and deployed states.

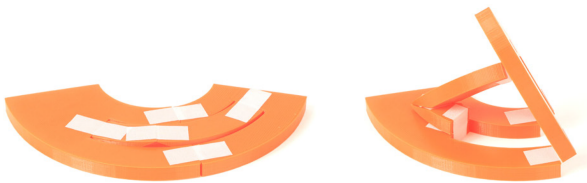


Figure 8. A simplified spherical deploying strut ThUDS based on the general PTHS model (Andrews et al., 2019). Shown in flat and deployed states.

3.4 Special case: flat-foldable, deploying strut ThUDS

In origami, a crease is flat foldable if it can obtain a fold angle of $\pm\pi$ (Lang et al., 2018). For a deploying strut ThUDS, flat foldability is possible when a set of collinear joints exist on an exterior surface, requiring that Eq. (3) be satisfied.

This special case is important because of the three particular states that are possible, namely flat folded, flat, and deployed. Three techniques for achieving these states are outlined below and illustrated in Fig. 9, with J_{added} referring to added joints. A spherical example is only given for the first technique, though the other techniques can be similarly applied.

3.4.1 Joint alignment

The simplest way of achieving flat foldability is aligning joints J_{12} and J_{34} (see Fig. 9a). For the planar subcategory, this means that $L_1 = L_4$ and $L_2 = L_3$. For the spherical subcategory, this means that $\alpha_1 = \alpha_4$ and $\alpha_2 = \alpha_3$. These joints can be aligned on either outer surface. A planar example of this flat-foldable technique is shown in Fig. 10, where the collinear joints lie on the bottom surface and flat foldability is in the opposite direction as deployment.

Two examples of flat-foldable spherical deploying strut ThUDS using joint alignment are shown in Fig. 11. Fig. 11a gives a simple version with all joints on the same plane, whereas Fig. 11b shows a more complex example with the joints offset, similar to that shown in Fig. 10, allowing for increased surface contact between the links. Flat foldability is

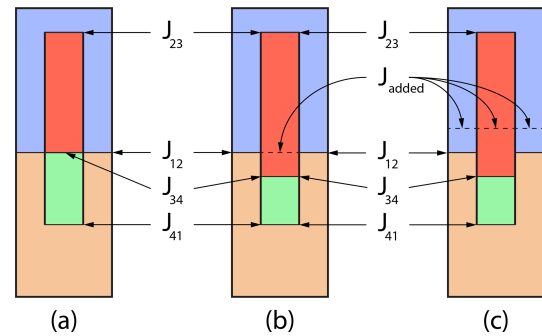


Figure 9. General diagram for techniques to achieve flat foldability with a deploying strut ThUDS: (a) joint alignment, (b) split-strut, and (c) double-split link. Joints match those shown in Figs. 2 and 5.

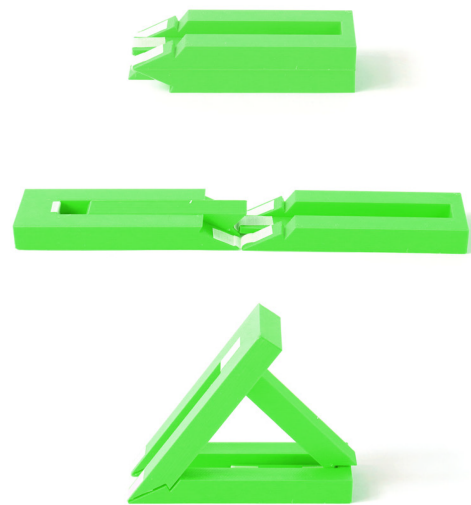


Figure 10. Flat-foldable planar deploying strut ThUDS with increased surface contact to improve load carrying. Shown in flat-folded, flat, and deployed states.

in the same direction as deployment for Fig. 11a and opposite deployment for Fig. 11b.

This approach is similar to the flat-foldable planar transcrease hard stop (FF-PTHS) model developed previously (Andrews et al., 2019), which works for dihedral angles less than 90° . By utilizing the material thickness, flat foldability can be obtained with dihedral angles of 90° or more. This is accomplished by offsetting joints J_{23} and J_{41} , thus changing the deploying strut ThUDS kinematics.

For example, joint J_{41} in Figs. 10 and 11b is offset from the bottom surface, whereas the other joints are all on the bottom surface. Additionally, these examples highlight strategically locating the joints and the material thickness to increase surface contact, thus increasing ThUDS stability.

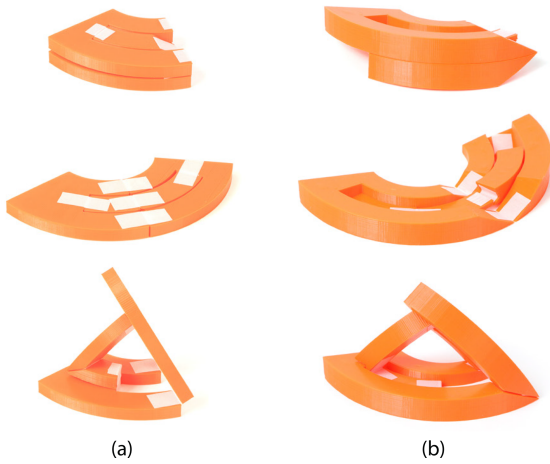


Figure 11. Flat-foldable spherical deploying strut ThUDS; (a) a simple example and (b) a more complex example with surface contact. Shown in flat-folded, flat, and deployed states.

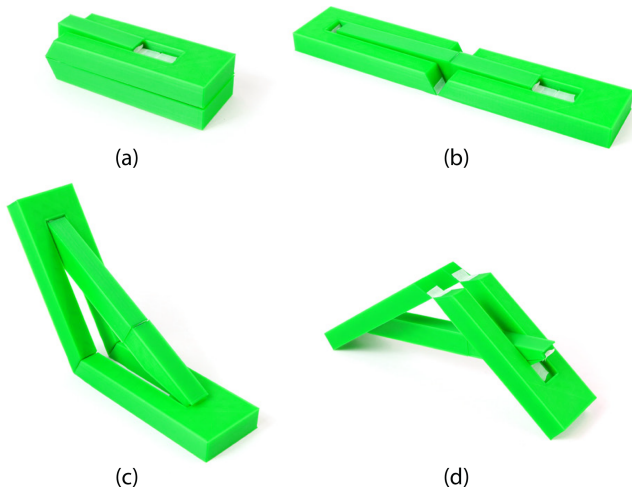


Figure 12. Flat-foldable planar deploying strut ThUDS with strut (link 3) split. Shown as (a) flat folded, (b) flat, (c) deployed, and (d) in an undesired state due to the added degree of freedom.

3.4.2 Split strut

By splitting the strut and introducing an additional joint collinear with J_{12} (see Fig. 9b), dihedral angles of $\geq 90^\circ$ can be easily obtained. The primary trade-off of this technique is the addition of a degree of freedom and, thus, reduced stability. By strategically placing the joints, the material thickness can be utilized to return some stability.

Figures 12 and 13 show examples of this technique using a planar deploying strut ThUDS. The first has collinear joints on the bottom surface, a dihedral angle of 120° , and folds flat opposite the direction of deployment. The second has collinear joints on the top surface, a dihedral angle of 90° , and folds flat in the same direction as deployment.

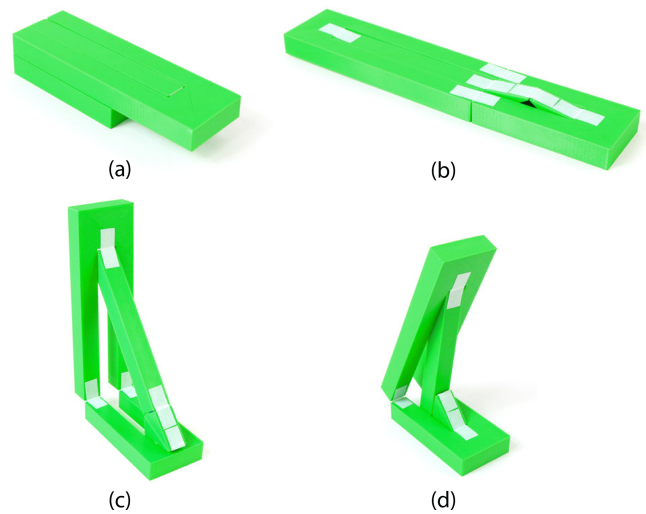


Figure 13. Flat-foldable planar deploying strut ThUDS with strut (link 3) split. Shown as (a) flat folded, (b) flat, (c) deployed, and (d) in an undesired state due to the added degree of freedom.

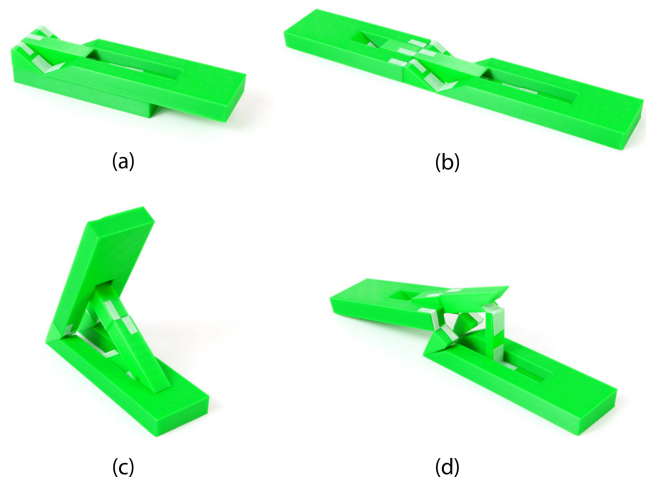


Figure 14. Flat-foldable planar deploying strut ThUDS with links 2 and 3 split. Shown (a) flat folded, (b) flat, (c) deployed, and (d) in an undesired state due to the added degrees of freedom.

3.4.3 Double-split link

The third technique for obtaining flat foldability is to add two collinear joints by splitting links L_2 and L_3 . This technique is limited by the addition of multiple degrees of freedom. Stability is further reduced from the split-strut technique. As before, material thickness can be utilized to aid with locking at the additional joint.

An example of this technique is depicted in Fig. 14. Here the collinear joints lie on the bottom surface, the dihedral angle is 60° , and the prototype folds flat opposite the direction of deployment.

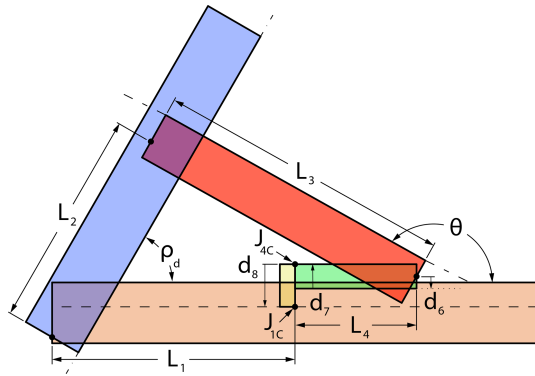


Figure 15. Diagram of a planar deploying strut ThUDS with offset crease joint added to depict key parameters, excluding $d_1 - d_5$ (see Fig. 2). Dashed lines designate joint reference planes.

3.5 Adaptation: addition of offset crease joint

As outlined in Sect. 2, the interfering link (link 4) is constrained to rotate 180° . For some types of joints, it is infeasible to obtain full 180° rotation. This challenge can be overcome by replacing joint J_{41} with two joints and a link. This is referred to as an offset crease joint (Ku and Demaine, 2016).

Figure 15 diagrams the addition of an offset crease joint to a planar deploying strut ThUDS. Equations (1) and (2) must be adapted to account for this extra joint, which gives the following:

$$L_1 + L_2 = L_3 + L_4 + d_8, \quad (14)$$

and the updated loop-closure equation is as follows:

$$L_1 + d_1i + d_2ie^{i\rho_d} - L_2e^{i\rho_d} - d_3ie^{i\rho_d} + d_4ie^{i\theta} + L_3e^{i\theta} - d_5ie^{i\theta} + d_6i + L_4 - d_7i + d_8i = 0, \quad (15)$$

where d_7 and d_8 are joint offsets accounting for the offset crease, and joints J_{1C} and J_{4C} refer to the two joints of the offset crease joint. Joint reference planes are defined in the same way as in Fig. 2b. The material of the link portion of the offset crease joint further helps with blocking the motion.

Figure 16 shows a planar deploying strut ThUDS with an incorporated offset crease joint. In this example, all joints lie on the same plane, parallel to the exterior surfaces, for easier assembly. Adding the offset crease joint allows for surface contact between each pair of connected links, while maintaining simplicity.

Following the principles in Sect. 3.4, a deploying strut ThUDS with an offset crease joint can be flat foldable. Figure 17 depicts a flat-foldable ThUDS with an offset crease joint with joint alignment.

3.6 Adaptation: inverted motion

A deploying strut ThUDS is designed to move from a flat, unfolded state to block motion before reaching a flat-folded

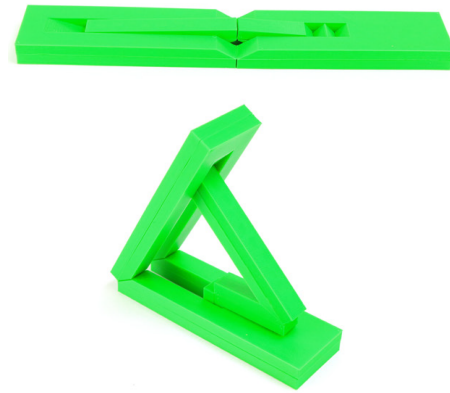


Figure 16. Planar deploying strut ThUDS with offset crease joint. All joints lie on the center plane. Shown in flat and deployed states.

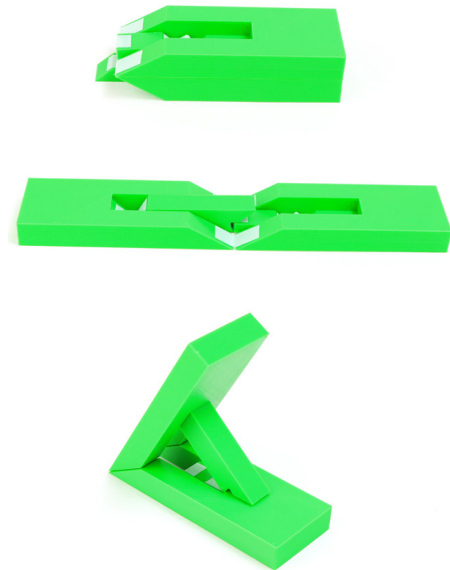


Figure 17. Flat-foldable planar deploying strut ThUDS with offset crease joint. Flat foldability is in the opposite direction of deployment. All joints lie on the bottom plane. Shown in flat-folded, flat, and deployed states.

state. Motion can be inverted such that a deploying strut ThUDS deploys from a flat-foldable state rather than a flat state. For the planar subcategory, this is done by replacing Eqs. (1) and (2) with the following:

$$L_1 + L_4 = L_2 + L_3, \quad (16)$$

and the adjusted loop-closure equation as follows:

$$-L_1 + d_1i + L_2e^{i\rho_d} + d_2ie^{i\rho_d} - L_3e^{i\theta} + d_3ie^{i\theta} + L_4 + d_4i = 0, \quad (17)$$

with parameters depicted in Fig. 18. Unlike the general case, only four joint offset values are used. This is because the upper surface of link 2 is established as the corresponding

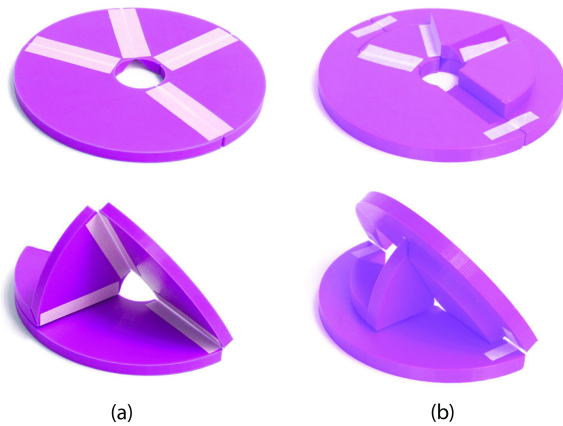


Figure 21. Sector panel ThUDS examples with (a) thickness added only beneath the joint plane and (b) thickness added both above and beneath the joint plane. Shown in flat and deployed states.

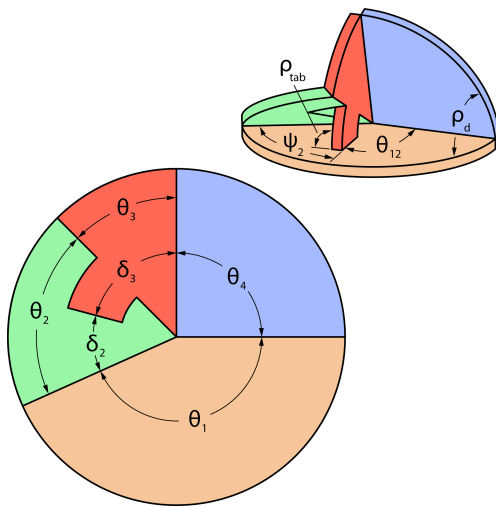


Figure 22. General diagram for a tabbed sector panel ThUDS with key parameters shown.

4.1 Adaptation: tabbed sector panel ThUDS

For a sector panel ThUDS, motion is blocked by self-interference between panels 1 and 3 (see Fig. 20). This requires that panel 2 is able to rotate 180° around joint J_{12} , specifying that J_{12} must reside on the upper surface of panels 1 and 2. This constraint reduces the possible surface contact within the system by constraining the possible positions of the remaining joints.

A tabbed sector panel ThUDS alters panels 2 and 3, removing the 180° constraint on panel 2 by adding a tab to panel 3, as shown in Fig. 22. The governing equations for this adaptation are Eq. (18) as follows:

$$\delta_2 + \delta_3 = \theta_2 + \theta_3 \quad (21)$$

$$\theta_{12} = \theta_1 - \psi_2 \quad (22)$$

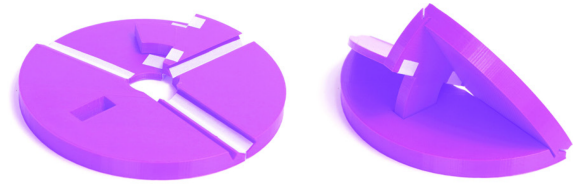


Figure 23. Tabbed sector panel ThUDS with tab lock groove and panel contact. Shown in flat and deployed states.

$$\cos(\rho_d) = \frac{\cos(\delta_3) - \cos(\theta_{12})\cos(\theta_4)}{\sin(\theta_{12})\sin(\theta_4)} \quad (23)$$

$$\cos(\rho_{\text{tab}}) = \frac{\cos(\theta_2) - \cos(\psi_2)\cos(\delta_3 - \theta_3)}{\sin(\psi_2)\sin(\delta_3 - \theta_3)}, \quad (24)$$

where ψ_2 is the projection of panel 2 on panel 1, δ_3 is the overall stiffener sector angle, δ_2 is the tab offset from joint J_{12} , and ρ_{tab} is the stiffener angle (see Fig. 22). Other parameters are the same as those defined above. The tabs here are cut along a radial line for convenience, though this does not need to be the case; any shape could be used, as long as the point where δ_3 is defined stops parallel to the ground panel plane.

Figure 23 shows an example of a tabbed sector panel ThUDS with a dihedral angle of 60° , which matches that of the examples in Fig. 21. Material is trimmed on either side of joints J_{12} and J_{34} to allow for increased surface contact. Additionally, panel 2 is thinner than the other panels since it is not load-bearing. A notch was added in panel 1 to lock the ThUDS in the blocked state.

Because of solving nonlinearity, the examples shown in Figs. 23 and 24 were designed such that $\rho_{\text{tab}} = \theta_4 = \theta_{12} = 90^\circ$. To aid in design, spherical kinematic equations, such as those given by McCarthy and Soh (2011), can be used in conjunction with the z -direction coupler point equation from Bowen et al. (2014) to determine at what angle the tab will interfere with panel 1.

4.1.1 Special case: flat-foldable sector panel ThUDS

As with a deployable strut ThUDS, flat foldability can be achieved for a sector panel ThUDS if, and only if, a pair of collinear joints exist on an exterior surface. This can be stated symbolically as follows:

$$\theta_1 + \theta_2 = \theta_3 + \theta_4 = \pi. \quad (25)$$

In general, this can only occur for a dihedral angle of 90° with $\theta_3 = \theta_4 = \frac{\pi}{2}$, thus allowing either θ_1 , θ_2 , or θ_{12} to be selected and the other two calculated.

Unlike the general case, which can only be flat foldability for one dihedral angle, a tabbed sector panel ThUDS can achieve flat foldability for a wider range of dihedral angles, specifically $90^\circ < \rho_d < 180^\circ$. This is possible because the support panel's sector angle is based on δ_3 instead of θ_3 and

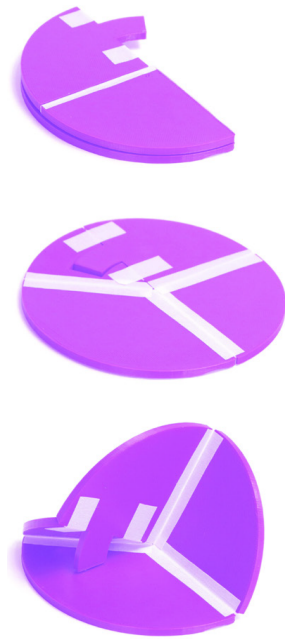


Figure 24. Flat-foldable sector panel ThUDS with flat foldability in the same direction as deployment. Shown in flat-folded, flat, and deployed states.

$\delta_3 > \theta_3$. Figure 24 shows an example of a flat-foldable tabbed sector panel ThUDS with a dihedral angle of 120° .

4.2 Adaptation: slider sector panel ThUDS

Another adaptation of the sector panel ThUDS is replacing panel 2 with a sliding joint. This can be defined using Eq. (18) and the following:

$$\theta_2 + \theta_{12} = \theta_3 + \theta_4 \quad (26)$$

$$\cos(\rho_d) = \frac{\cos(\theta_{12})\cos(\theta_4) - \cos(\theta_3)}{\sin(\theta_{12})\sin(\theta_4)}, \quad (27)$$

where θ_2 is the slider angle and θ_{12} is measured opposite θ_1 rather than along θ_1 . Other parameters are the same as defined above. The slider angle tracks an angle of θ_2 (such that $\theta_1 + 2\theta_2 + \theta_5 = 2\pi$). An example of this is shown in Fig. 25 in various states, with a slider larger than θ_2 to allow for constrained motion.

4.3 Adaptation: inverted motion

A sector panel ThUDS is designed from a flat, unfolded state to block motion before reaching a flat-foldable state. Motion can be inverted such that a sector panel ThUDS deploys from a nondevelopable, flat-foldable state instead of a flat, developable state. This is done by replacing Eqs. (18) through (20) with the following:

$$\theta_1 - \theta_2 + \theta_3 - \theta_4 = 0, \quad (28)$$

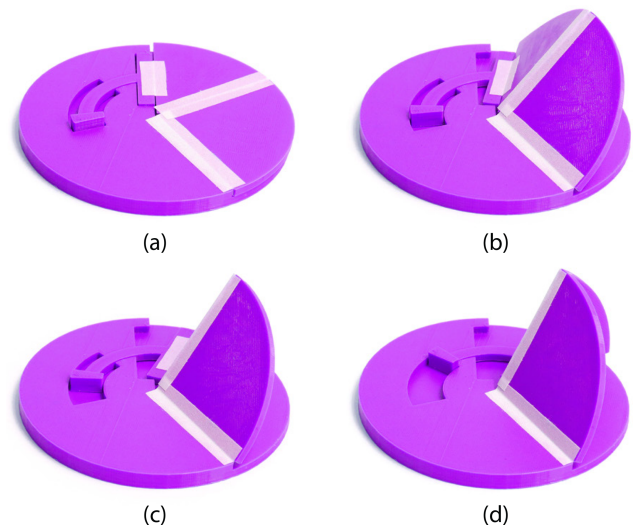


Figure 25. Slider sector panel ThUDS in (a) flat, (b–c) deploying, and (d) deployed states.

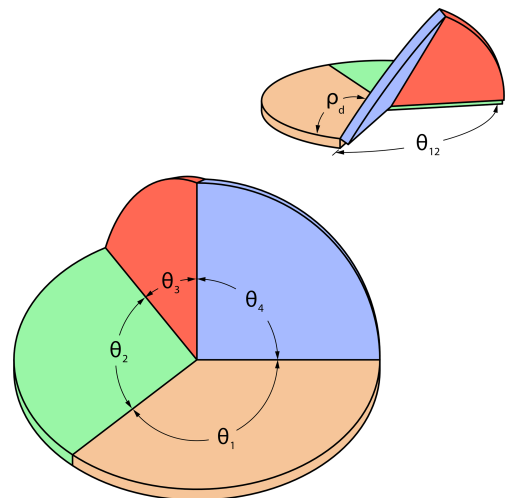


Figure 26. General diagram for a sector panel ThUDS with inverted motion depicting key parameters.

$$\theta_1 + \theta_2 + \theta_{12} = 2\pi, \quad (29)$$

and replacing Eq. (27) with the parameters depicted in Fig. 26. Note that for this adaptation θ_{12} is also opposite θ_1 instead of along θ_1 , as specified for the slider adaptation above.

Figure 27 is a physical example of this adaption. Each panel is shifted as needed, using the offset panel technique for thickness accommodation to allow for flat foldability (Lang et al., 2018).

5 Applications of ThUDS

ThUDS were implemented in origami-based designs to demonstrate their benefit in products and systems. Several

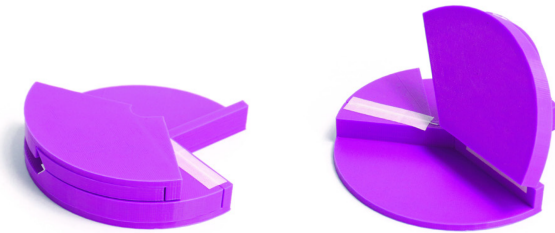


Figure 27. Inverted sector panel ThUDS with thickness added and removed to allow for flat foldability. Shown in flat-folded and deployed states.

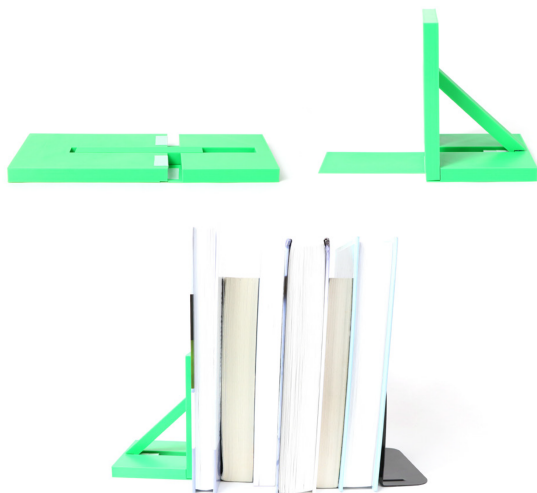


Figure 28. Collapsible bookend with planar deploying strut ThUDS. Shown in flat state, deployed state, and in functional use.

of these were selected and are shown with increasing levels of complexity.

5.1 Collapsible bookend

Bookends are often difficult to store due to their shape. By making them collapsible, they can be easily stored, while being able to maintain their function when deployed.

By implementing a 90° planar deploying strut ThUDS, the collapsible bookend shown in Fig. 28 was developed, which closely resembles a typical metal bookend. The bookend has a flat state, such that it can be stored in a box or even on the bookshelf between books. Then, it can be quickly deployed for use and maintain stability with books resting against it. See Table A1 in Appendix A for parameter values.

Additionally, the thickness of the links is utilized by design to create surface contact, placing the strut link in compression when in use. This allows loads to be transmitted through the strut and ground links to the shelf, while still allowing for folding.

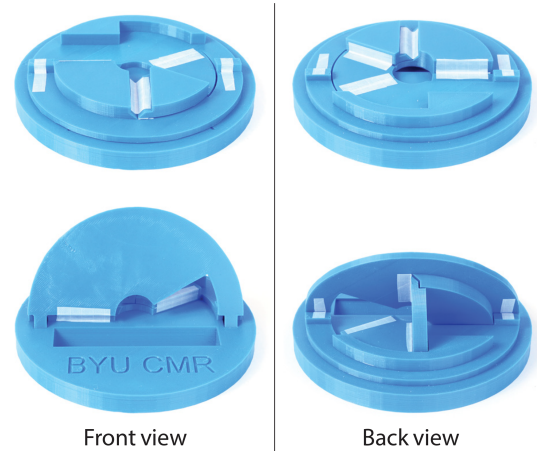


Figure 29. Desk mobile phone holder in stowed and deployed states.

5.2 Desk mobile phone holder

An origami-based desk mobile phone holder, shown in Fig. 29, was designed using a sector panel ThUDS. It has a flat state for easy storage and can be deployed for holding a mobile phone. A dihedral angle of 60° was selected for simplicity but could be designed for other angles.

This design utilizes the material thickness in multiple ways. Tabs and corresponding slots were added to isolate loads from the joints. A ridge was also added to help lock panels 2 and 3 in place, further removing the load from the joints. Additionally, a groove was designed in panel 1 for panel 2 to sit in. Together, these features constrain the motion of the ThUDS and improve stability, while maintaining desired functionality and foldability.

5.3 Side table

Furniture is often cumbersome and bulky, thus being difficult to move and store. Folding allows for easier movement and reduces the required storage space. An origami-based foldable side table was created by replacing joints between the legs and table top with flat-foldable planar deploying strut ThUDS, as shown in Fig. 30. The equations in Sect. 3.1 were used to determine the ThUDS dimensions (see Table A1 in Appendix A).

Because flat-foldable ThUDS were used, the side table is able to collapse to a completely flat position, as shown in Fig. 30. Thus, stowability is increased while functionality is maintained. Joints were offset to utilize the link thickness to create surface contact, helping to remove loads from the joints.

5.4 Flat-foldable unit cell

Square or rectangular structures are common in a variety of origami-based applications. With this in mind, a square unit



Figure 30. Flat-foldable side table example. The planar deploying strut ThUDS used are similar to those shown in Fig. 10.



Figure 31. Flat-foldable square unit cell in flat, deployed, and locked states.

cell was created that is able to be folded flat, then deployed, and locked in a square stable state. Figure 31 shows the unit cell in its flat, deployed, and locked states. This unit cell can be used as a building block for other applications.

This design was created by placing a pair of planar deploying strut ThUDS in two opposing corners and a pair of inverted planar deploying strut ThUDS in the other two opposing corners. Each has a dihedral angle of 90° . Locking is enabled through the motion-blocking capability of ThUDS and the bistable nature of inverted planar deploying strut ThUDS.

Additionally, this configuration transfers loads through a ThUDS, rather than a joint via the strut link, through link contact with the sides. This adds to the stability of the system and potential load-carrying capacity.

6 Discussion

When selecting and designing a ThUDS configuration for a particular application, it is important to address the trade-offs tied to the type used and parameters chosen. The strategic utilization of material thickness to allow for surface contact

and increased stability comes with increased complexity. On the other hand, the simpler the design, the less the material thickness can be utilized for functionality, such as reducing loading on the joints.

One key benefit of a ThUDS is the ability to adapt them to nearly any material, and thus, they can be used in a wide variety of applications. By assuming near-zero thickness, ThUDS simplify to transcrease hard stops and can be directly incorporated within an origami pattern (Andrews et al., 2019). When applied to thick materials, surface contact can be used for increased stability and load-bearing.

The examples herein show the possibility of using flexible joints, such as tape or fabric, when contact is exhibited between links. This is because loads are able to pass predominately through the links, reducing the stress on the joints. These examples also show that ThUDS can become degenerate in their flat states. Remedies for this include adding material beneath the joint plane (see Fig. 16) and residing on a thickened plane (see Figs. 25 and 27).

Furthermore, ThUDS can be embedded in any system built from a flat sheet, whether this is an origami pattern or a thick folding system. For example, the origami-based folding side table shown in Fig. 30 has 3D-printed polylactic acid (PLA) ThUDS embedded in a wooden structure.

Finally, ThUDS can be used in series, parallel, or a combination of both. The examples in Sect. 5.1 and 5.2 exhibit only a single ThUDS. The side table has four ThUDS in series (see Fig. 30), and the flat-foldable unit cell shown in Fig. 31 has a series of four pairs of parallel ThUDS.

7 Conclusions

This work has focused on methods for blocking motion and incorporating stability in origami-based systems through the development of thickness-utilizing deployable hard stops (ThUDS), which have both flat and deployed states. Methods used to design the ThUDS were presented using diagrams, equations, and examples. These were separated into two categories, namely deploying strut ThUDS and sector panel ThUDS. Special cases, such as obtaining flat foldability and adaptations, such as inverted motion, were presented for each.

Four origami-based examples were also shown, all of which have flat storage states and stable, functional deployed states. Through these examples, it has been shown that a ThUDS can be applied in functional ways to items with practical use. How a ThUDS utilizes thickness is also illustrated and discussed. Thickness-utilizing deployable hard stops maintain foldability and improve stability, while utilizing thickness, and are able to be completely contained within the thickness of a design.

Appendix A

Table A1. Parameter values for planar deploying strut ThUDS examples. Lengths are in inches (millimeters). Parameters marked “–” are not part of the technique used to create that prototype. Whether flat foldability (FF) is possible is denoted in the last column.

| Example | ρ_d | L_1 | L_2 | L_3 | L_4 | d_1 | d_2 | d_3 | d_4 | d_5 | d_6 | d_7 | d_8 | FF |
|-----------|----------|-----------------|-----------------|-----------------|----------------|-----------------|----------------|----------------|-----------------|----------------|-----------------|---------------|---------------|----|
| Figure 3 | 60° | 2 (50.8) | 3.288 (83.5) | 3.288 (83.5) | 2 (50.8) | 0.5 (12.7) | 0.5 (12.7) | 0.5 (12.7) | 0.5 (12.7) | 0 | 0 | – | – | N |
| Figure 4 | 60° | 2 (50.8) | 4.164 (106) | 4.164 (106) | 2 (50.8) | 0.1 (2.54) | 0.3 (7.62) | 0.5 (12.7) | 0.2 (5.08) | 0.4 (10.2) | 0 | – | – | N |
| Figure 7 | 60° | 1.125 (28.6) | 3.6 (91.4) | 3.225 (81.9) | 1.5 (38.1) | – | – | – | – | – | – | – | – | N |
| Figure 10 | 60° | 2 (50.8) | 3.56 (90.4) | 3.56 (90.4) | 2 (50.8) | 0.15 (3.81) | 0.5 (12.7) | 0.5 (12.7) | 0.5 (12.7) | 0.5 (12.7) | 0.15 (3.81) | – | – | Y |
| Figure 12 | 120° | 2.5 (63.5) | 3.113 (79.1) | 5.113 (130) | 0.5 (12.7) | 0.35 (8.89) | 0.5 (12.7) | 0.5 (12.7) | 0.5 (12.7) | 0.55 (14.0) | 0.2 (5.08) | – | – | Y |
| Figure 13 | 90° | 0.5 (12.7) | 1 (25.4) | 1.25 (31.8) | 0.25 (6.35) | – | – | – | – | – | – | – | – | Y |
| Figure 14 | 60° | 2 (50.8) | 2.342 (59.5) | 2.842 (72.2) | 1.5 (38.1) | 0.2 (5.08) | 0.5 (12.7) | 0.5 (12.7) | 0.5 (12.7) | 0.5 (12.7) | 0.2 (5.08) | – | – | Y |
| Figure 16 | 60° | 2.25 (57.2) | 3.34 (84.8) | 3.34 (84.8) | 1.75 (44.5) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.5 (12.7) | N |
| Figure 17 | 60° | 1.4 (35.6) | 1.914 (48.6) | 1.914 (48.6) | 1 (25.4) | 0.2 (5.08) | 0.5 (12.7) | 0.5 (12.7) | 0.5 (12.7) | 0.5 (12.7) | 0.2 (5.08) | 0.2 (5.08) | 0.4 (10.2) | Y |
| Figure 19 | 60° | 2 (50.8) | 1.404 (35.7) | 1.596 (40.5) | 1 (25.4) | 0.25 (6.35) | 0.5 (12.7) | 0.25 (6.35) | 0 | – | – | – | – | Y |
| Figure 28 | 90° | 2 (50.8) | 3.083 (78.3) | 4.083 (104) | 1 (25.4) | 3/16 (4.76) | 7/16 (11.1) | 7/16 (11.1) | 7/16 (11.1) | 3/8 (9.53) | 1/8 (3.18) | – | – | N |
| Figure 30 | 52.52° | 2 (50.8) | 3.051 (77.5) | 3.051 (77.5) | 2 (50.8) | 0.125 (3.18) | 0.5 (12.7) | 0.5 (12.7) | 0.5 (12.7) | 0.5 (12.7) | 0.125 (3.18) | – | – | Y |
| Figure 31 | 90° | 0.5 (12.7) | 0.6 (15.2) | 0.85 (21.6) | 0.25 (6.35) | 0.1 (2.54) | 0.25 (6.35) | 0.25 (6.35) | 0.25 (6.35) | 0.25 (6.35) | 0.1 (2.54) | – | – | N |
| Figure 31 | 90° | 1 (25.4) | 0.307 (7.80) | 0.943 (24.0) | 0.25 (6.35) | 0.125 (3.18) | 0.25 (6.35) | 0 | 0.125 (3.18) | – | – | – | – | Y |

Table A2. Parameter values for spherical deploying strut ThUDS examples. Lengths are in inches (millimeters). Parameters marked “–” are not part of the technique used to create that prototype. Whether flat foldability (FF) is possible is denoted in the last column.

| Example | ρ_d | α_1 | α_2 | α_3 | α_4 | β | d_1 | d_2 | d_3 | d_4 | d_5 | d_6 | FF |
|------------|----------|------------|------------|------------|------------|---------|-----------------|----------------|----------------|----------------|---------------|-----------------|----|
| Figure 6 | 60° | 45° | 40.60° | 55.60° | 30° | 75° | 0.25 (6.35) | 0.25 (6.35) | 0.25 (6.35) | 0.25 (6.35) | 0 | 0 | N |
| Figure 8 | 60° | 45° | 43.63° | 58.63° | 30° | 75° | – | – | – | – | – | – | N |
| Figure 11a | 60° | 30° | 49.11° | 49.11° | 30° | 60° | – | – | – | – | – | – | Y |
| Figure 11b | 60° | 45° | 59.86° | 59.86° | 45° | 90° | 0.125 (3.18) | 0.5 (12.7) | 0.5 (12.7) | 0.5 (12.7) | 0.5 (12.7) | 0.125 (3.18) | Y |

Table A3. Parameter values for sector panel ThUDS examples. Parameters marked “–” are not part of the technique used to create that prototype. Whether flat foldability (FF) is possible is denoted in the last column.

| Example | ρ_d | θ_1 | θ_2 | θ_3 | θ_4 | θ_{12} | δ_2 | δ_3 | ψ_2 | ρ_{tab} | FF |
|--------------|----------|------------|------------|------------|------------|---------------|------------|------------|----------|--------------|----|
| Figure 21a–b | 60° | 150° | 60° | 60° | 90° | 90° | – | – | – | – | N |
| Figure 23 | 60° | 165° | 77.37° | 27.63° | 90° | 90° | 45° | 60° | 75° | 90° | N |
| Figure 24 | 120° | 130.89° | 49.11° | 90° | 90° | 90° | 19.11° | 120° | 40.89° | 90° | Y |
| Figure 25 | 120° | 150° | 60° | 60° | 90° | 90° | – | – | – | – | N |
| Figure 27 | 120° | 150° | 120° | 60° | 90° | 90° | – | – | – | – | Y |
| Figure 29 | 60° | 150° | 60° | 60° | 90° | 90° | – | – | – | – | N |

Data availability. All of the pertinent data are provided in the text of the publication.

Author contributions. DWA was the lead author and performed or directed the modeling and prototyping represented in the paper. SPM initially structured the paper, guided the direction of the research presented, and provided editorial input. LLH guided the direction of the research, made contributions on presentation approaches for the mechanisms, and provided reviews of the paper.

Competing interests. The authors declare that they have no conflict of interest.

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