TOPICAL REVIEW

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TOPICAL REVIEW

Distributed quantum sensing

Zheshen Zhang^{1,2,*} and Quntao Zhuang^{2,3,*}

- Department of Materials Science and Engineering, University of Arizona, Tucson, AZ 85721, United States of America
- ² James C. Wyant College of Optical Sciences, University of Arizona, Tucson, AZ 85721, United States of America
- ³ Department of Electrical and Computer Engineering, University of Arizona, Tucson, AZ 85721, United States of America
 * Authors to whom any correspondence should be addressed.

E-mail: zsz@arizona.edu and zhuangquntao@email.arizona.edu

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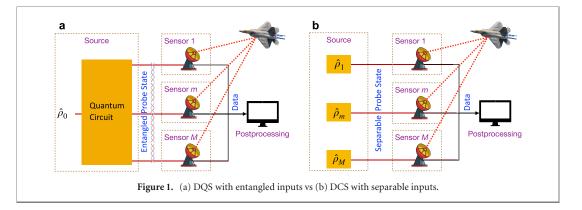
Abstract

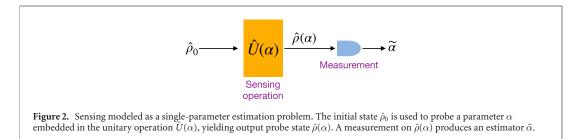
A plethora of applications hinge on a network or an array of sensors to undertake measurement tasks. A rule of thumb for sensing is that a collective measurement taken by *M* independent sensors can improve the sensitivity by $1/\sqrt{M}$, known as the standard quantum limit (SQL). Quantum resources such as entanglement and squeezed light can be harnessed to surpass the SQL. Distributed quantum sensing is an emerging subject dedicated to investigating the performance gain enabled by entangled states shared by multiple sensors in tackling different measurement problems. This review formulates distributed quantum sensing (DQS) from a quantum-information perspective and describes DQS protocols and their experimental demonstrations. The applications enabled by DQS and an outlook for future opportunities will also be discussed.

1. Introduction

The overarching goal of quantum information science and its enabled emerging quantum technologies is to demonstrate capabilities beyond what is allowed by their classical counterparts. Since the discovery of Shor's factoring algorithm [1], quantum computing has received significant interests and investments as it is widely deemed a disruptive paradigm capable of solving many classically intractable optimization [2–6], artificial intelligence [7–13], and big-data analysis problems [14–17]. A remarkable milestone for quantum computing is the accomplishment of 'quantum supremacy' on Google's 53-qubit superconducting quantum computer in solving a quantum random sampling problem [18]. Despite the tremendous recent advances in quantum computing, immense challenges arise when utilizing the available noisy intermediate-scale quantum (NISQ) hardware [19] to implement practically useful quantum algorithms due to a lack of fault-tolerant mechanism. A continued pursuit for the quantum-information community is to seek application scenarios in which quantum technologies enjoy a quantifiable advantage over their classical counterparts.

Sensing is an arena that quantum technologies can achieve advantages over classical sensing technologies for practical applications in the near term. Quantum metrology [20–24] studies the use of nonclassical resources to enhance the performance of measurements for a variety of sensing applications. As a prominent example, the Laser Interferometer Gravitational-wave Observatory (LIGO) injects nonclassical squeezed light into its Michelson interferometer to surpass the standard quantum limit (SQL) due to laser shot noise [25–27]. Apart from LIGO, quantum metrology has also been exploited in target detection [28–34], microscopy [35], biological sensing [36], and phase tracking [37] (see references [21–24, 38, 39] for comprehensive reviews of quantum metrology and references [40, 41] for a review of quantum sensing). The focus of all these quantum-metrology experiments is on utilizing quantum resources to improve the performance at a single sensor. Recent theoretical works [42–45] proposed distributed quantum sensing (DQS) protocols that enable multiple sensors to leverage their shared entangled states to boost the performance of probing *global* properties of an interrogated object. Since a multitude of real-world





applications rest upon a network or an array of sensors that work collectively to undertake sensing tasks, DQS significantly broadens the applicable scope of quantum metrology and opens a new route for achieving a quantum advantage with near-term quantum hardware.

This review first provides in section 2 an overview of DQS and compares it with distributed classical sensing (DCS). Section 3 describes DQS protocols with continuous-variables (CVs) and discrete variables (DVs). Section 4 then analyzes DQS and DCS protocols, quantifies DQS's quantum advantage, and accounts for practical nonidealities. To articulate the applications of DQS, section 5 reviews two recent DQS experiments for, respectively, optical phase sensing and radio-frequency (RF) sensing applications. An outlook for future prospects of DQS will be discussed in section 6.

2. Overview

Usual multi-parameter estimation protocols endeavor to estimate *all* unknown parameters, while some multi-parameter estimation protocols alternatively consider extracting a single parameter while regarding the rest as nuisance parameters. DQS belongs to neither cases as it is aimed at estimating a global property of multiple parameters.

A conceptual schematic for DQS is sketched in figure 1(a): a quantum circuit processes the initial quantum state $\hat{\rho}_0$ to create an entangled probe state shared by *M* sensors that jointly interrogate an object. The measurement data produced by all sensors are postprocessed to infer a global parameter of the probed object. By contrast, in DCS illustrated in figure 1(b), the quantum state at *M* sensors is in a separable form (e.g., a product form $\hat{\rho}_1 \otimes \hat{\rho}_2 \otimes \ldots \otimes \hat{\rho}_M$) to generate measurement data that are also postprocessed to infer a global property of the object. The ideal measurement sensitivity of DQS typically scales as 1/M, whereas the scaling of the measurement sensitivity of DCS is limited by the SQL of $1/\sqrt{M}$.

To quantify the advantage of DQS, a performance baseline set by a comparable DCS protocol is needed. To assess the performance of a DCS protocol, one needs to constrain its accessible resources. For example, the performance of optical sensors needs to be evaluated at a fixed probe power level as granting more probe power can always improve the performance. A commonly used resource constraint is by assuming that the compared DQS and DCS protocols use the same amount of total power at their sensors. In this case, DCS protocols are allowed to leverage separable local nonclassical resources such as squeezed light as long as the overall probe power equals that used in the compared DQS protocol. The quantum advantage is quantified as the performance disparity between the compared DQS and DCS protocols. Such a resource constraint has also been adopted by other quantum-sensing protocols such as quantum illumination [28–33], quantum reading [46] and their multi-hypothesis generalizations [47–50], and absorption spectroscopy [51]. It is worth noting that DQS protocols typically also enjoy a *practical* advantage over DCS

 Table 1. A list of protocols mentioned in this paper. PNR: photon-number-resolving. BS: beam splitter. SS: spin squeezing states. SV: squeezed vacuum states. GHZ: Greenberger–Horne–Zeilinger states. GKP: Gottesman–Kitaev–Preskill states.

Reference	Sensed parameter	Source	Measurement	Robustness	Experiments
[44]	Displacement/phase	SV + BS	Homodyne	Yes	[55, 56]
[57]	Complex displacement	GKP + BS	GKP + Gaussian	Yes	N/A
[43]	General DV parameter	GHZ type	Unspecified	Unknown	N/A
[42]	Phase	$ N\rangle + BS$	PNR detectors	Unknown	N/A
[45, 58]	Qubit phase rotation	GHZ/SS	Parity/total spin	Unknown	[59, 60]

protocols in terms of the required hardware. Specifically, a DCS protocol allowed to take advantage of local nonclassical resources such as squeezed light would need to deploy one nonclassical source at each sensor while a DQS protocol only needs one entanglement source to serve all sensors.

3. Distributed quantum sensing protocols

Prior to introducing DQS, let us first formulate quantum sensing using an example of single-parameter estimation, as shown in figure 2. Consider a parameter α embedded in a unitary operation $\hat{U}(\alpha) = \exp \left[-i\hat{H}\alpha\right]$, whose generator is the Hermitian operator \hat{H} . To sense α , one prepares an initial quantum state $\hat{\rho}_0$ and passes it through $\hat{U}(\alpha)$, obtaining the output state

$$\hat{\rho}(\alpha) = \hat{U}(\alpha)\,\hat{\rho}_0\hat{U}^{\dagger}(\alpha) \tag{1}$$

after the sensing operation. Subsequently, a suitable measurement on $\hat{\rho}(\alpha)$ gives information for building an estimator $\tilde{\alpha}$. The precision of such an estimator is characterized by the variance, i.e., the mean squared error $\delta \alpha^2 = \langle (\tilde{\alpha} - \alpha)^2 \rangle$, where $\delta \alpha$ is the standard deviation (std), i.e., the root-mean-square (rms) error. To improve the precision of estimation, one can independently use *M* probes to interrogate the same object and repeat the measurement process *M* times. In this case, the initial state is in a product form of $\hat{\rho}_0^{\otimes M}$, and the measurement on each output state $\hat{\rho}(\alpha)$ yields the estimator $\tilde{\alpha}$. Due to the i.i.d. nature of individual sensing attempts, a simple average over all estimators leads to an overall precision of $\delta \alpha_M = \delta \alpha / \sqrt{M}$, per the law of large numbers. Such a scaling is also called the SQL.

In a distributed sensing scenario, one looks at a more general problem: consider a general unitary operation comprising a product of M unitary operations $\hat{U}(\alpha) \equiv \bigotimes_{\ell=1}^{M} \hat{U}(\alpha_{\ell})$, which, in general, entail M unknown parameters. To carry out sensing, one inputs M probes in a quantum state $\hat{\rho}_{M}$ and obtains the output quantum state

$$\hat{\boldsymbol{\rho}}_{M}\left(\boldsymbol{\alpha}\right) = \hat{U}\left(\boldsymbol{\alpha}\right)\hat{\boldsymbol{\rho}}_{M}\hat{U}^{\dagger}\left(\boldsymbol{\alpha}\right),\tag{2}$$

where the unknown parameters are $\alpha = {\{\alpha_m\}_{m=1}^M}$ instead of being a single unknown parameter as in equation (1). In a multi-parameter estimation scenario, one aims to estimate *all* unknown parameters; alternatively, one may only be interested in a single parameter while regarding the rest M - 1 parameters nuisance. Distributed sensing belongs to neither categories, as it endeavors to estimate a global parameter, e.g., a weighted average

$$\bar{\alpha} = \boldsymbol{w} \cdot \boldsymbol{\alpha} \equiv \sum_{\ell=1}^{M} w_{\ell} \alpha_{\ell}, \qquad (3)$$

where the weights, $\boldsymbol{w} = \{w_m\}_{m=1}^M$, are non-negative and sum to one without loss of generality. One can in principle consider a general analytical scalar function $f(\boldsymbol{\alpha})$, but as pointed out in reference [58], via adaptive strategies one can obtain a rough estimate for $\tilde{\boldsymbol{\alpha}}$ and then perform linear expansion around the point to obtain $f(\boldsymbol{\alpha}) \simeq f(\tilde{\boldsymbol{\alpha}}) + \sum_{\ell} \partial_{\alpha_{\ell}} f(\tilde{\boldsymbol{\alpha}}) (\alpha_{\ell} - \tilde{\alpha}_{\ell})$. By suitably dividing the number of measurements, one can reduce the problem of estimating the scalar function to estimating the weighted average in equation (3). More recent works extended the above case to multiple linear functions [52].

We point out that the special case of identical parameters $\alpha_m = \alpha$ and identical weights $w_m = 1/M$ has been considered in pioneering works of quantum metrology [20, 53, 54], which show that entanglement can beat the SQL (see section 4.2 for more details) and approach the Heisenberg limit of $\delta \alpha \propto 1/M$. A major advance made by DQS lies in the extension to a multi-parameter scenario, with an arbitrary scalar function of the parameters under estimation.

In the following, we will describe several DQS protocols and analyze their performances in the presence of imperfections. The protocols are also summarized in table 1, in terms of the source, measurement, and robustness.

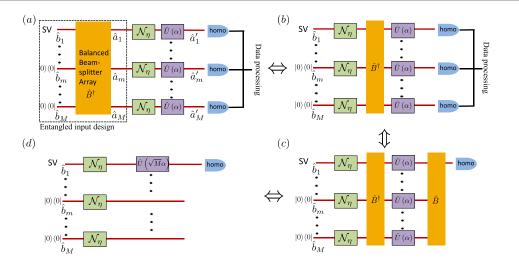


Figure 3. Distributed displacement sensing with identical displacements and weights. SV: squeezed-vacuum state with mean photon number N_S and squeezed real quadrature. N_{η} : pure-loss channel with transmissivity $0 < \eta \leq 1$. $\hat{U}(\alpha)$: field-quadrature displacement by real-valued α . Homo: homodyne measurement on the real quadrature. (a) Original protocol. (b)–(d) Equivalent protocols from reduction relations (see main text for details).

3.1. Distributed displacement sensing

This section covers single-quadrature displacement DQS protocols, with the generator being $\hat{H} = \hat{p}$. The protocol is based on entanglement generated from linear optics and single-mode squeezed vacuum states. Extension to a DQS protocol capable of simultaneous estimation of both quadrature displacements can be achieved by replacing the single-mode squeezed vacuum with a Gottesman–Kitaev–Preskill (GKP) grid state [61], as studied in reference [57].

3.1.1. Special DQS protocols

We begin with a special case of DQS with identical displacements and identical weights [44]. As shown in figure 3(a), the entangled probe state is prepared by distributing a single-mode squeezed vacuum state \hat{b}_1 on a balanced beam-splitter array. After each probe mode \hat{a}_m going through the displacement $\hat{U}(\alpha)$, one performs a homodyne measurement on the real quadrature Re (\hat{a}'_m) . Combining all measurement data $\{\tilde{a}'_m\}_{m=1}^M$ through classical data processing, one obtains an estimator $\tilde{\alpha} = \sum_{m=1}^M \tilde{a}'_m / M$. We model the imperfection in each sensor by the most common model of a pure-loss channel \mathcal{N}_η of transmissivity η , which is described by the Bogoliubov transform

$$\hat{a} \to \sqrt{\eta}\hat{a} + \sqrt{1 - \eta}\hat{e},$$
 (4)

on the input mode \hat{a} and vacuum environment mode \hat{e} . To begin with, we consider the losses to be identical across different sensors.

To analyze the performance, a sequence of reduction is utilized to simplify the problem to a single-parameter estimation situation. First, since the beam-splitter array \hat{B}^{\dagger} commutes with the identical loss channels $\mathcal{N}_{\eta}^{\otimes M}$, an equivalent protocol is devised in figure 3(b). Moreover, the data processing of equal weighted sum can be implemented by a balanced beam-splitter array \hat{B} in front of the homodyne measurements, leading to another equivalent protocol in figure 3(c), where the identical displacements are now sandwitched between two beam-splitter arrays such that a single homodyne measurement suffices to carry out the estimation. At this juncture, we can utilize a unitary reduction relation

$$\hat{B}^{\dagger}\hat{U}^{\otimes M}\left(\alpha\right)\hat{B}=\hat{U}\left(\sqrt{M}\alpha\right)\otimes\hat{U}^{\otimes (M-1)}\left(0\right)$$
(5)

to further simplify the protocol to figure 3(d), which shows that the multimode protocol is reduced to a single-mode protocol, as only \hat{b}_1 interrogates a single channel that entails information about α . A single-mode displacement is estimated after the reduction. Thus, results in section 4.3.2 immediately infer that the optimal Gaussian [62] input state for the reduced protocol depicted in figure 3(d) is a single-mode squeezed vacuum state. The resulting sensitivity obeys

$$\delta \alpha_{\eta}^{\mathrm{E}} = \frac{1}{\sqrt{I_{\mathrm{F}}^{\mathrm{Gauss, E, max}}}} = \left(\frac{\eta}{M\left(\sqrt{N_{\mathrm{S}} + 1} + \sqrt{N_{\mathrm{S}}}\right)^2} + \frac{1 - \eta}{M}\right)^{1/2},\tag{6}$$

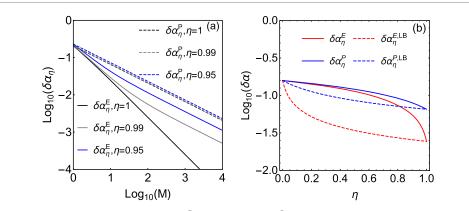


Figure 4. (a) Plots of the rms estimation errors , $\delta \alpha_{\eta}^{\text{E}}$ (solid curves) and $\delta \alpha_{\eta}^{\text{P}}$ (dashed curves), versus the number of sensor nodes, M, for various transmissivity values, from top to bottom, $\eta = 0.95, 0.99, 1$, with $n_{\text{S}} \equiv N_{\text{S}}/M$ fixed at $n_{\text{s}} = 1$. Reprinted figure with permission from [44], Copyright (2018) by the American Physical Society. (b) Comparison between bounds and performance $N_{\text{S}} = 10, M = 10, \delta \alpha_{\pi}^{\text{E}}$; performance of the optimal entangled Gaussian scheme for DQS (red). $\delta \alpha_{\eta}^{\text{P}}$: performance of optimal separable Gaussian scheme for DCS (blue). $\delta \alpha_{\pi}^{\text{E.B.}}$: lower bound of precision in equation (8) for all entangled scheme (red, dashed). $\delta \alpha_{\eta}^{\text{P.LB.}}$: lower bound of precision in equation (9) for all separable scheme. When $\eta \sim 1$, we see that $\delta \alpha_{\eta}^{\text{E}}$ beats the non-tight lower bound $\delta \alpha_{\eta}^{\text{P.LB.}}$ of separable scheme. Reprinted figure with permission from [63], Copyright (2019) by the American Physical Society.

where N_S is the total mean photon number of the probes and $I_F^{Gauss, E, max}$ is given in equation (46). We note that although the input state in the reduced protocol is a single-mode squeezed-vacuum state, the *M*-mode input $\{\hat{a}_m\}_{m=1}^M$ in the original DQS protocol illustrated figure 3(a) is in a multipartite entangled state. The sensitivity given by equation (6) is the optimum among all DQS protocols based on *Gaussian* states. Moreover, in a lossless situation ($\eta = 1$), the above DQS protocol is the optimum among *all* DQS protocols per the results introduced in section 4.2.2.

Similarly, subject to the resource counting of mean photon number, the optimal DCS protocol with Gaussian states for $\eta < 1$ and the general optimal DCS protocol for $\eta = 1$ is based on a product of single-mode squeezed-vacuum states and yields a sensitivity level of

$$\delta \alpha_{\eta}^{\rm P} = \frac{1}{\sqrt{I_{\rm F}^{\rm Gauss, \, \rm C, \, max}}} = \left(\frac{\eta}{M\left(\sqrt{N_{\rm S}/M + 1} + \sqrt{N_{\rm S}/M}\right)^2} + \frac{1 - \eta}{M}\right)^{1/2},\tag{7}$$

where $I_{\rm F}^{\rm Gauss, C, \max}$ is given by equation (45). The performance of the optimal DQS protocol and the optimal DCS protocol is compared in figure 4(a). At $\eta = 1$ and a fixed $n_{\rm S} \equiv N_{\rm S}/M$, equations (6) and (7) indicate that $\delta \alpha_{\eta}^{\rm E} \sim 1/M$, i.e., a Hisenberg scaling, while $\delta \alpha_{\eta}^{\rm P} \sim 1/\sqrt{M}$ is subject to the SQL, as is verified in figure 4(a). For sub-unity η , $\delta \alpha_{\eta}^{\rm E}$ deviates from the Heisenberg scaling at large $M \propto 1/(1 - \eta)$. To sustain the Heisenberg scaling at a large M, one can utilize bosonic error-correcting codes, as demonstrated in reference [57].

Now that we know the optimality of the performance in equations (6) and (7) for special cases, we can compare them with the general precision lower bounds

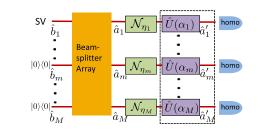
$$\delta \alpha_{\eta}^{\text{E,LB}} = \frac{1}{\sqrt{I_{\text{F}}^{\text{UB,E}}}} = \left(4\eta M \left(\sqrt{N_{\text{S}}} + \sqrt{N_{\text{S}} + 1}\right)^2 + 4\left(1 - \eta\right) M\right)^{-1/2} \tag{8}$$

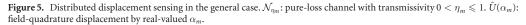
$$\delta \alpha_{\eta}^{\rm C,LB} = \frac{1}{\sqrt{I_{\rm F}^{\rm UB,C}}} = \left(4\eta M \left(\sqrt{N_{\rm S}/M} + \sqrt{N_{\rm S}/M + 1}\right)^2 + 4\left(1 - \eta\right)M\right)^{-1/2},\tag{9}$$

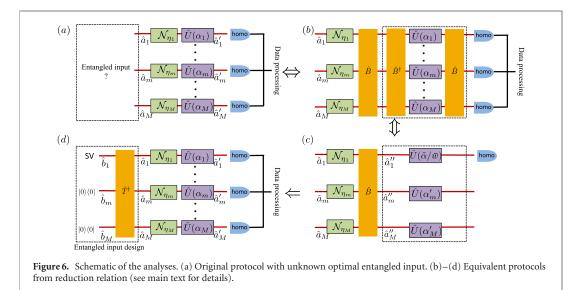
which are obtained from the Fisher information upper bounds equations (40) and (41) in section 4.3.1. We compare the above bounds and the actual protocol's performance in figure 4(b). Indeed, the lower bounds are tight at $\eta = 1$ (also trivially tight at $\eta = 0$), confirming the optimality. However, when $\eta < 1$, there is a gap between the optimal Gaussian protocol and the lower bound. It is an open question whether other protocols can beat the optimal Gaussian protocol.

3.1.2. General DQS protocols

We now extend the special DQS protocol of section 3.1.1 to a DQS protocol for estimating an arbitrary weighted average of heterogeneous displacements in the presence of heterogeneous experimental







imperfections. As shown in figure 5, the objective is to estimate a weighted average, $\bar{\alpha} \equiv \sum_{m=1}^{M} w_m \alpha_m$, of displacements $\{\alpha_m\}_{m=1}^{M}$ among M sensor nodes. Experimental imperfections are modelled by lossy channels $\{\mathcal{N}_{\eta_m}\}_{m=1}^{M}$, where the transmissivities $\boldsymbol{\eta} = \{\eta_m\}_{m=1}^{M}$ can vary across different sensor nodes. The input modes $\{\hat{a}_m\}_{m=1}^{M}$ are in an entangled state, generated from distributing a single-mode squeezed-vacuum state via a general beam-splitter array with ratios suitably optimized.

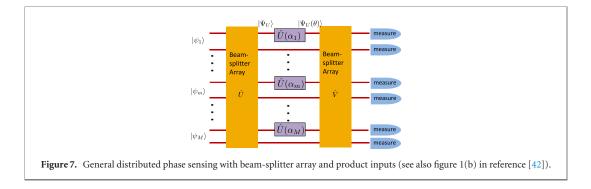
To derive the optimal entangled probe state, we again utilize equivalence relations shown in figure 6. Figure 6(a) illustrates the problem of deriving the optimal entangled probe state assuming homodyne measurements. As shown in figure 6(b), before the homodyne measurements, one can apply a beam-splitter array \hat{B} , which can be compensated in the data processing on measurement data while preserving the Fisher information. Moreover, one can insert $\hat{B}\hat{B}^{\dagger} = \hat{I}$ in between the lossy channels and the sensing displacement operations. From properties of Gaussian unitary, as shown in figure 6(c) one can suitably choose \hat{B} to obtain

$$\hat{B}^{\dagger}\left[\otimes_{m=1}^{M}\hat{U}\left(\alpha_{m}\right)\right]\hat{B}=\hat{U}\left(\bar{\alpha}/\bar{w}\right)\otimes\left[\otimes_{m=2}^{M}\hat{U}\left(\alpha_{m}'\right)\right],\tag{10}$$

where $\bar{w} \equiv \sqrt{\sum_{m=1}^{M} w_m^2}$ and all other parameters α'_m are independent of the parameter of interest $\bar{\alpha}$. As such, one only needs to measure the first output mode to estimate $\bar{\alpha}$. Now the problem becomes choosing the optimal input among $\{\hat{a}_m\}_{m=1}^M$ such that mode \hat{a}''_1 is the optimum for single-mode displacement sensing. Considering the transform \hat{B} and the lossy channels, it is easy to obtain

$$\hat{a}_1'' = \sum_{m=1}^M \frac{\mathbf{w}_m}{\bar{\mathbf{w}}} \sqrt{\eta_m} \hat{a}_m + \text{vacuum terms} = \sqrt{\bar{\eta}} \hat{b}_1 + \text{vacuum terms}, \tag{11}$$

where $\hat{b}_1 \equiv \sum_{m=1}^{M} w_m \sqrt{\eta_m} \hat{a}_m / \bar{w}, \bar{\eta} \equiv \sum_{m=1}^{M} w_m^2 \eta_m / \bar{w}^2$, and $\bar{w} \equiv \sqrt{\sum_{m=1}^{M} w_m^2 \eta_m}$. This indicates that the effective probe mode \hat{a}''_m is obtained from passing a single mode \hat{b}_1 through a pure-loss channel $\mathcal{N}_{\bar{\eta}}$. Given the energy constraint, the optimal Gaussian state is therefore obtained by applying a beam-splitter array \hat{T}^{\dagger} on a single-mode squeezed vacuum mode \hat{b}_1 and vacuum states, as shown in figure 6(d).



With the above protocol, $\tilde{\alpha} \equiv \sum_{m=1}^{M} w_m \operatorname{Re}(\hat{a}'_m)$ is an unbiased estimator of $\bar{\alpha}$ with the minimum rms error

$$\delta \alpha_{\eta}^{\rm E} = \frac{\bar{w}}{2} \left(\frac{\bar{\eta}}{(\sqrt{N_{\rm S} + 1} + \sqrt{N_{\rm S}})^2} + 1 - \bar{\eta} \right)^{1/2}.$$
 (12)

Parallel to section 3.1.1, one can compare the above DQS protocol with the optimal Gaussian DCS protocol, which, under the considered scenario, employs a product of single-mode squeezed-vacuum states, yielding a precision of

$$\delta \alpha_{\eta}^{p} = \min_{\substack{M \\ m=1}} \left[\sum_{m=1}^{M} w_{m}^{2} \left(\frac{\eta_{m}}{\left(\sqrt{N_{m} + 1} + \sqrt{N_{m}} \right)^{2}} + 1 - \eta_{m} \right) / 4 \right]^{1/2}$$
(13)

without a known closed form. One can easily check that at $\eta_m = \eta$, $\alpha_m = \alpha$, $w_m = 1/\sqrt{M}$, equations (12) and (13) converge to the simple case of equations (6) and (7). Also, we emphasize that the same optimality holds: the above DCS protocol is the optimum among all protocols based on *Gaussian* states and the optimum among *all* DCS protocols at $\eta_m = 1$ for all *m*.

3.2. Distributed phase sensing

In distributed phase sensing, equation (2) involves a phase rotation unitary operation $\hat{U}(\alpha_m) = \exp(-i\alpha_m \hat{a}_m^{\dagger} \hat{a}_m)$ at each probe \hat{a}_m . As explained in section 4.2.2, the Fisher information of phase sensing is unbounded for non-Gaussian states if only subject to a photon-number constraint. As such, previous works have been focusing on finding the optimal Gaussian protocol [64, 65], considering constraints on the photon-number variance [66, 67] or limiting to a finite photon-number cutoff [68, 69].

Through evaluating the precision limit of DQS in equation (50) for all Gaussian states (obtained from the multi-parameter CR bound, see section 4.4), reference [65] shows that the CV entangled state obtained via distributing a single-mode squeezed-vacuum state via a beam-splitter array—identical to the optimal state in the displacement case in section 3.1—is the optimal Gaussian state for estimating the weighted sum of phase.

In the identical weight case, a balanced beam-splitter array is adopted and the corresponding precision

$$\delta \alpha^{\rm E} = \frac{1}{\sqrt{8N_{\rm S} \left(N_{\rm S} + 1\right)}} = \frac{1}{\sqrt{8Mn_{\rm S} \left(Mn_{\rm S} + 1\right)}},\tag{14}$$

can be easily achieved by performing homodyne measurements—again identical to the approach in the displacement DQS of section 3.1. While the optimal separable input and homodyne measurement (identical to the case of section 3.1) gives the performance

$$\delta \alpha^{\mathrm{P}} = \frac{1}{\sqrt{8Mn_{\mathrm{S}}\left(n_{\mathrm{S}}+1\right)}}.$$
(15)

We see a similar advantage from the entanglement as the case of displacement DQS discussed in section 3.1. Although the above state is the optimal for an ideal lossless situation, in the presence of loss, however, reference [55] finds that adding a non-zero displacement to the original single-mode squeezed vacuum can further improve the performance. The optimal entangled probe state in the presence of loss remains unknown, even restricting to Gaussian states.

Like the displacement DQS protocols, the resource constraint should be properly chosen to ensure an equitable comparison with DCS protocols. In this regard, the above works have adopted a resource constraint on the total mean photon number, accounting for the coherent-state portion and the squeezed-state portion, as introduced in section 2. This resource constraint is justified if the power probing

the samples has to be limited, for example, for the purpose of covertness or avoiding harming delicate biological tissues. However, coherent states are much easier to generate than squeezed-vacuum states and is often orders of magnitude higher in power as well. In applications, e.g., LIGO, that require strong coherent light, resource constraint is on the power of the coherent-state portion. In some phase DQS protocols, phase shifts transform strong coherent states into displacements so that the displacement DQS protocol introduced in section 3.1 can then be utilized, as proposed in reference [44]. A similar technique is adopted in DQS for RF-sensing applications, as detailed in section 5.2.

As we see in the above protocols for phase sensing and displacement sensing, a beam-splitter array, i.e., a linear optical network, has the power of generating multipartite entangled states that benefit the estimation of global parameters. In this regard, reference [42] systematically evaluated the use of entangled states prepared by a beam-splitter array on separable inputs $\otimes |\psi_m\rangle_{m=1}$ in DQS (figure 7).

A different resource constraint needs to be adopted for phase sensing because the precision can be unbounded under a simple mean photon-number constraint. A commonly used resource-counting scheme for phase sensing is based on the photon-number fluctuation,

$$n_j^{\rm LO} \equiv \sqrt{\langle \psi_j | \hat{n}_j^2 | \psi_j \rangle} \leqslant n_j^*, \tag{16}$$

of each two-mode product state $|\psi_j\rangle$ as an input to the beam-splitter array. For general *unnormalized* weights \boldsymbol{w}^* (max_j $|\mathbf{w}_j^*| = 1/d$, which is different from our previous definition) and photon-number fluctuation constraints $\boldsymbol{n}^* \equiv (n_1^*, \ldots, n_M^*)$, reference [42] showed that the precision of phase DQS is lower bounded by

$$\delta \bar{\alpha} \geqslant \delta \bar{\alpha}^{\text{LB}*} \equiv \frac{M |\boldsymbol{w}^{\star}|^2}{2|\boldsymbol{n}^{\star}|},\tag{17}$$

where $|\boldsymbol{w}^{\star}|^2 = \sum_j w_j^{\star 2}$ and $|\boldsymbol{n}|^2 = \sum_j n_j^{\star 2}$. To better understand the interpretation, we can consider the equal weight case, i.e., $|\boldsymbol{w}^{\star}|^2 = 1/M$, yielding

$$\delta \bar{\alpha} \ge \delta \bar{\alpha}^{\text{LB}*} = \frac{1}{2|\boldsymbol{n}^*|} \ge \frac{1}{2N_{\text{S}}^*}.$$
(18)

The second lower bound is achieved by concentrating all $N_{\rm S}^*$ photons on the same mode, so $|\mathbf{n}^*| = N_{\rm S}^* = Mn_{\rm S}^*$ saturates the Heisenberg limit. While an even distribution of photons among all input modes of the beam-splitter array leads to the SQL $\delta \bar{\alpha} \ge 1/(2n_{\rm S}^*\sqrt{M})$. As such, the benefit from entanglement only arises when photons are concentrated on a few input modes to the beam-splitter array. A protocol is also provided in reference [42] by choosing the input to the beam-splitter array as a twin-Fock state.

Now let us further compare the lower bound in equation (18) with the achievable performance in equation (14). Since $N_{\rm S}^{\star} = \sqrt{\langle \hat{n}^2 \rangle} = \sqrt{N_{\rm S} (3N_{\rm S} + 2)}$ for a single-mode squeezed-vacuum state, equation (18) yields a valid lower bound of

$$\delta \bar{\alpha}^{\text{LB}*} = \frac{1}{2\sqrt{N_{\text{S}}(3N_{\text{S}}+2)}} \leqslant \delta \alpha^{\text{E}} = \frac{1}{\sqrt{8N_{\text{S}}(N_{\text{S}}+1)}}.$$
(19)

In the $N_{\rm S} \gg 1$ limit,

$$\frac{\delta \alpha^{\rm E}}{\delta \bar{\alpha}^{\rm LB*}} \sim \sqrt{\frac{3}{2}}.$$
(20)

Note that the DV DQS protocol based on generalized twin-Fock state [42] gives $\delta \alpha^{E} = 2/\sqrt{2N_{S}(N_{S}+2)}$. Although also achieving a Heisenberg scaling, the DV DQS protocol's performance is inferior to that of the CV DQS protocols [44, 65].

4. Performance limits

In this section, we analyze the performance limits for DQS protocols. A brief review on the limits of quantum sensing, including quantum Cramér–Rao (CR) bound, SQL for separable protocols, and Heisenberg limit of entangled protocols will first be provided. Then, the quantum CR bound will be utilized to understand the performance limits of the DQS and DCS protocols in section 3, which leads to conclusions about the optimality of these protocols.

4.1. Quantum Cramér-Rao bound and the standard quantum limit

The ultimate precision of estimating a single-parameter α (without bias) from the state $\hat{\rho}(\alpha)$ is asymptotically given by the quantum CR bound [70–75]

$$\delta \alpha_M^2 \geqslant \frac{1}{M} \delta \alpha_{\rm CR}^2 \equiv \frac{1}{M I_{\rm F}[\hat{\rho}(\alpha)]},\tag{21}$$

where *M* is the number of sensing attempts and the single-parameter Fisher information [73]

$$I_{\rm F}[\hat{\rho}(\alpha)] \equiv \lim_{\epsilon \to 0} 8 \left\{ 1 - \sqrt{\mathcal{F}[\hat{\rho}(\alpha), \hat{\rho}(\alpha + \epsilon)]} \right\} / \epsilon^2$$
(22)

is given in terms of the Uhlmann fidelity [76, 77], $\mathcal{F}(\hat{\sigma}_1, \hat{\sigma}_2) \equiv \left[\text{Tr}\left(\sqrt{\sqrt{\hat{\sigma}_1} \hat{\sigma}_2 \sqrt{\hat{\sigma}_1}} \right) \right]^2$, between states $\hat{\sigma}_1$ and $\hat{\sigma}_2$. Alternatively, the Fisher information can be obtained from the symmetric logarithmic derivative (SLD) \hat{L}_{α} , which is Hermitian and satisfies

$$\frac{\hat{L}_{\alpha}\hat{\rho}_{\alpha}+\hat{\rho}_{\alpha}\hat{L}_{\alpha}}{2}=\frac{\partial\hat{\rho}_{\alpha}}{\partial\alpha}.$$
(23)

Then in general the Fisher information is defined as

$$I_{\rm F}[\hat{\rho}(\alpha)] \equiv {\rm Tr}\left[\hat{\rho}_{\alpha}\hat{L}_{\alpha}^2\right].$$
⁽²⁴⁾

In fact, for quantum states in the form of equation (1), one can easily obtain the Fisher information in both ways for pure states. The fidelity for a pure state $\hat{\rho} = |\psi\rangle\langle\psi|$ is easily devried by $\mathcal{F}(\hat{U}(\alpha) |\psi\rangle, \hat{U}(\alpha + \epsilon) |\psi\rangle) = |\langle\psi|\hat{U}(\epsilon) |\psi\rangle|^2$, and thus by taking derivatives the Fisher information reads

$$I_{\rm F}[\hat{U}(\alpha)|\psi\rangle]/4 = \operatorname{var}(\hat{H})_{\psi} \equiv \langle \psi|\hat{H}^2|\psi\rangle - \langle \psi|\hat{H}|\psi\rangle^2.$$
⁽²⁵⁾

In terms of SLD, a pure state has $\hat{\rho}_{\alpha}^2 = \hat{\rho}_{\alpha}$, it is thus easy to verify that $\hat{L}_{\alpha} = 2\partial_{\alpha}\hat{\rho}_{\alpha} = -2i\hat{H}\hat{\rho}_{\alpha} + 2i\hat{\rho}_{\alpha}\hat{H}$, and therefore equation (24) leads to equation (25). However, it is important to note that equation (25) does not in general hold for mixed states, while both equations (22) and (24) remain valid for all mixed states. Moreover, the CR bound in equation (21) is guaranteed to be asymptotically, i.e., at $M \gg 1$, achievable for a single-parameter estimation problem by adaptive strategies [78–82], in which the input state and the associated measurement setting evolve as the number of measurement increases. However, all input states are constrained to a product form.

One can generalize the above protocol to using an arbitrary separable input state across M measurements and allowing an arbitrary joint measurement [20]. However, the CR bound in equation (21) holds true, and the $\delta \alpha_M \propto 1/\sqrt{M}$ scaling is usually referred to as the SQL.

4.2. Beating the standard quantum limit

Entanglement between the input states across different measurements is needed to beat the SQL. Early works of quantum metrology [20, 53, 54] found that the so-called Heisenberg scaling of precision, $\delta \alpha_M \propto 1/M$, can be approached if the input states across M measurements are in a multipartite entangled form. To analyze this setting, we consider applying a joint operation on an M-probe pure state $|\psi_M\rangle$:

$$\hat{\boldsymbol{\rho}}_{M}\left(\alpha\right) = \hat{U}^{\otimes M}\left(\alpha\right) \left|\boldsymbol{\psi}_{M}\right\rangle \left\langle\boldsymbol{\psi}_{M}\right| \hat{U}^{\dagger \otimes M}\left(\alpha\right),\tag{26}$$

where $\hat{U}^{\otimes M}(\alpha) = \exp\left[-i\alpha \sum_{\ell} \hat{H}_{\ell}\right]$, with $\{\hat{H}_{\ell}\}$ being identical generators applied on different probes. Then, the Fisher information is derived using equation (25) as

$$I_{\rm F}[\hat{U}^{\otimes M}(\alpha)|\psi_M\rangle]/4 = \operatorname{var}\left(\sum_{\ell}\hat{H}_{\ell}\right)_{\psi_M} \equiv \langle\psi_M|\left(\sum_{\ell}\hat{H}_{\ell}\right)^2|\psi_M\rangle - \langle\psi_M|\sum_{\ell}\hat{H}_{\ell}|\psi_M\rangle^2.$$
(27)

For a product state $|\psi_M\rangle = \bigotimes_{\ell=1}^M |\psi_\ell\rangle$ (not necessarily identical), $\langle \psi_M | (\sum_\ell \hat{H}_\ell)^2 |\psi_M\rangle = \sum_\ell \langle \psi_\ell | \hat{H}_\ell^2 | \psi_\ell \rangle + \sum_{\ell \neq \ell'} \langle \psi_\ell \hat{H}_\ell | \psi_\ell \rangle \langle \psi_{\ell'} | \hat{H}_{\ell'} | \psi_{\ell'} \rangle$, which, after some simple algebra, shows additivity for Fisher information between product states:

$$I_{\mathrm{F}}[\hat{U}^{\otimes M}(\alpha) \otimes_{\ell=1}^{M} |\psi_{\ell}\rangle]/4 = \sum_{\ell} I_{\mathrm{F}}[\hat{U}(\alpha) |\psi_{\ell}\rangle]/4.$$
(28)

Combining the convexity property of the Fisher information, we conclude that any separable input state will have Fisher information upper bounded by M times the maximum Fisher information for the individual states, therefore giving the SQL of $\delta \alpha_M \propto 1/\sqrt{M}$. Equation (28), however, does not hold for entangled states. The disparity between the SQL performance and sub-SQL performance demonstrates a provable quantum advantage enabled by entanglement, as elaborated below by a few examples.

4.2.1. Finite-dimensional probes

For *d*-dimensional probe states, e.g., DV systems such as atoms, NV centers etc, or CV systems with a finite photon-number cutoff, one can simply consider the eigenstates $\{|\lambda_n\rangle\}_{n=1}^d$ of the generator, i.e. $\hat{H}|\lambda_n\rangle = \lambda_n|\lambda_n\rangle$, as discussed in reference [54]. Suppose the minimum and maximum eigenvalues are λ_{\min} and λ_{\max} , each term $I_{\rm F}[\hat{U}(\alpha) |\psi_\ell\rangle]/4 = \operatorname{var}(\hat{H})_{\psi_\ell} \leq (\lambda_{\max} - \lambda_{\min})^2/4$. Equation (28) then provides the following bound for a separable input

$$I_{\rm F} \leqslant I_{\rm F}^{\rm max,C} \equiv M (\lambda_{\rm max} - \lambda_{\rm min})^2.$$
⁽²⁹⁾

In contrast, with an entangled input, $\hat{H}_M = \sum_{\ell} \hat{H}_{\ell}$ is regarded as a global generator, and the minimum and maximum eigenvalues then become $M\lambda_{\min}$ and $M\lambda_{\max}$, leading to the Fisher information

$$I_{\rm F} \leqslant I_{\rm F}^{\rm max, \rm E} \equiv M^2 (\lambda_{\rm max} - \lambda_{\rm min})^2, \tag{30}$$

achievable by the superposition state $|\psi_M\rangle = (|\lambda_{\max}\rangle^{\otimes M} + |\lambda_{\min}\rangle^{\otimes M})/\sqrt{2}$. The above Fisher information follows $\propto M^2$, corresponding to an optimal Heisenberg scaling of $\delta \alpha_M \propto 1/M$ [83].

4.2.2. Infinite-dimensional probes

For infinite-dimensional probe states, e.g., in a CV system, the eigenvalues of the generator can be unbounded. In this case, additional constraints, such as the mean occupation number (the mean photon number in the context of quantum optics) $N_{\rm S} = \sum_{\ell=1}^{M} \langle \hat{a}_{\ell}^{\dagger} \hat{a}_{\ell} \rangle$, are necessary to ensure a physical input state.

The Fisher information for CV states needs to be calculated on a case-by-case basis. For example, in single-mode phase sensing with $\hat{H} = \hat{a}^{\dagger}\hat{a}$ being the number operator, one can construct an input state $|\psi\rangle = \sqrt{1 - N_{\rm S}/S}|0\rangle + \sqrt{N_{\rm S}/S}|S\rangle$, with mean photon number $N_{\rm S}$ bounded but the variance $\operatorname{var}(\hat{H})_{\psi} = N_{\rm S}(S - N_{\rm S})$ can be arbitrarily large, and therefore, the Fisher information can be unbounded. Hence, further constraints, such as restricting to Gaussian input states or fixing the photon-number fluctuation, are required to operate in a physically allowed regime.

Another important scenario is displacement sensing with a generator of $\hat{H} = \hat{p}$. First considering a single probe, the Fisher information reads $I_{\rm F}[\hat{U}(\alpha) |\psi\rangle]/4 = \operatorname{var}(\hat{p})_{\psi}$. To achieve the optimal precision, we need to maximize $\operatorname{var}(\hat{p})_{\psi}$, subject to the energy constraint $N_{\rm S} = \langle \hat{a}^{\dagger} \hat{a} \rangle \equiv \left(\operatorname{var}(\hat{p})_{\psi} + \operatorname{var}(\hat{q})_{\psi} \right)/4 - 1/2$. Here, zero-mean input states are chosen because displacement does not enhance the precision. Taking into account the uncertainty principle, $\operatorname{var}(\hat{p})_{\psi} \cdot \operatorname{var}(\hat{q})_{\psi} \ge 1$, and the energy constraint, it shows that $\operatorname{var}(\hat{p})_{\psi}$ is maximized when the input is in a squeezed-vacuum state, with the optimal Fisher information

$$I_{\rm F}[\hat{U}(\alpha)|\psi\rangle]/4 = \left(\sqrt{N_{\rm S}} + \sqrt{N_{\rm S}+1}\right)^2.$$
(31)

We now consider *M* probes with a total energy constraint N_S . For separable input states, the Fisher information is additive (equation (28)). Since the single-mode Fisher information in equation (31) is concave with respect to the energy N_S , the Fisher information for *M* separable probes becomes

$$I_{\rm F} \leqslant I_{\rm F}^{\rm max,C} \equiv 4M \left(\sqrt{N_{\rm S}/M} + \sqrt{N_{\rm S}/M + 1}\right)^2 \simeq 16N_{\rm S},\tag{32}$$

whose maximum is achieved with the input being in an i.i.d. product of single-mode squeezed vacuum states. Asymptotically, it is independent of the number of probes *M*.

With an entangled input state, we need to consider the overall Fisher information of equation (27):

$$I_{\rm F}[\hat{U}^{\otimes M}(\alpha) | \psi_M \rangle]/4 = M \cdot \operatorname{var}(\hat{P})_{\psi_M},\tag{33}$$

where $\hat{P} = \sum_{\ell} \hat{p}_{\ell} / \sqrt{M}$ is defined as a global momentum quadrature, with the corresponding global position quadrature defined as $\hat{Q} = \sum_{\ell} \hat{q}_{\ell} / \sqrt{M}$. Because \hat{P} and \hat{Q} satisfy the canonical commutation relation and can be obtained by applying a passive linear transform on the original single-mode quadrature operators, they can be regarded as being effectively produced by sending the original input modes through a balanced beam-splitter array. As energy is preserved under a beam-splitter transform, it is clear that concentrating all the energy on the global mode of \hat{P} and \hat{Q} is optimal, as the other global modes are all in vacuum states. At this juncture, we have reduced the multimode problem to a single-mode problem, and the Fisher information

$$I_{\rm F} \leqslant I_{\rm F}^{\rm max,E} \equiv 4M \left(\sqrt{N_{\rm S}} + \sqrt{N_{\rm S} + 1}\right)^2 \simeq 16MN_{\rm S} \tag{34}$$

is achieved by an entangled input state whose corresponding global mode is in a single-mode squeezed-vacuum state. This sub-SQL performance is achieved in a specific DQS protocol, as explained in section 3.1.2.

4.3. Precision limits in the presence of noise

The above analyses assume pure states so that the Fisher information has a simple form represented in equations (25) and (27). However, experimental imperfections are in general inevitable, rendering the output state mixed and the evaluation of the Fisher information more challenging. Although an exact optimization of the Fisher information is difficult, one can obtain upper bounds on the Fisher information [66]. One can also focus on certain specific classes of input states, such as the Gaussian states [62], to make the problem tractable.

Here, we consider the CV example of displacement estimation introduced in section 4.2.2 and explain the above two approaches. We consider the most common noise in photonic sensing—loss, i.e. the vacuum noise Suppose pure loss occurs before the probing process, the input–output relation for a single mode is

$$\hat{\rho}(\alpha) = \hat{U}(\alpha) [\mathcal{N}_n(\hat{\rho})] \hat{U}^{\dagger}(\alpha), \tag{35}$$

which augments a lossy channel into the sensing model described equation (1). Similar to equation (26), the output *M*-mode state is

$$\hat{\boldsymbol{\rho}}_{M}(\alpha) = \hat{U}^{\otimes M}(\alpha) \left[\mathcal{N}_{\eta}^{\otimes M}(\hat{\boldsymbol{\rho}}_{M}) \right] \hat{U}^{\dagger \otimes M}(\alpha) \,. \tag{36}$$

4.3.1. General upper bounds

Several general upper bounds for the DQS and DCS protocols will be presented (details in reference [63]). The probe state after loss is in general mixed, expressed as $\hat{\rho}_M = \sum_{\ell} c_{\ell} |\psi_{\ell}\rangle \langle \psi_{\ell}|$, where $\sum_{\ell} c_{\ell} = 1$ are positive eigenvalues and ψ_{ℓ} 's are the eigenstates. Per convexity of the Fisher information, we have

$$I_{\rm F}[\hat{\boldsymbol{\rho}}_M(\alpha)] \leqslant \sum_{\ell} c_{\ell} I_{\rm F}[\hat{U}(\alpha)^{\otimes M} |\psi_{\ell}\rangle].$$
(37)

For each pure state, similar to equation (27), we can explicitly express $I_{\rm F}[\hat{U}(\alpha)^{\otimes M}|\psi_{\ell}\rangle] = 4 \operatorname{var}\left(\sum_{k} \hat{p}'_{k}\right)_{\psi_{\ell}}$, where \hat{p}'_{k} is the momentum quadrature of the *k*th probe after the lossy channel. Combining the above with equation (37), we have

$$I_{\rm F}[\hat{\rho}_M(\alpha)]/4 \leqslant \left\langle \left(\sum_k \hat{p}'_k\right)^2 \right\rangle_{\hat{\rho}_M(\alpha)} - \sum_{\ell} c_{\ell} \left\langle \left(\sum_k \hat{p}'_k\right) \right\rangle_{\psi_{\ell}}^2 \leqslant \operatorname{var}\left(\sum_k \hat{p}'_k\right)_{\hat{\rho}_M(0)},\tag{38}$$

where the inequality $\sum_{\ell} c_{\ell} x_{\ell}^2 \ge \left(\sum_{\ell} c_{\ell} x_{\ell}\right)^2$ and the invariance of quadrature variances under displacement are used. Because the pure-loss channel transforms $\hat{p}'_k = \sqrt{\eta} \hat{p}_k + \sqrt{1-\eta} \hat{p}_{e_k}$, where \hat{p}_{e_k} and \hat{p}_k are the momentum quadratures of the environment and the mode before the loss, we immediately have

$$I_{\rm F}[\hat{\boldsymbol{\rho}}_M(\alpha)]/4 \leqslant \eta \operatorname{var}\left(\sum_k \hat{p}_k\right) + (1-\eta)M,\tag{39}$$

where the variance is evaluated before the pure-loss channel. Combining with the analyses in equation (34), an upper bound (UB) for the Fisher information is derived as

$$I_{\rm F} \leqslant I_{\rm F}^{\rm UB,E} \equiv \eta I_{\rm F}^{\rm max,E} + 4 \, (1 - \eta) \, M.$$
 (40)

At $\eta = 1$, the UB recovers equation (34) and is therefore achievable. However, it is unclear whether equation (40) is achievable at $\eta < 1$. One also finds that the method utilizing purification to reduce to pure states calculations 66 gives the same UB as equation (40).

Similarly, the Fisher information UB in DCS is derived as

$$I_{\rm F} \leqslant I_{\rm F}^{\rm UB,C} \equiv \eta I_{\rm F}^{\rm max,C} + 4 \, (1 - \eta) \, M,$$
(41)

which recovers equation (32) at $\eta = 1$, while its achievability remains unknown for $\eta < 1$.

4.3.2. Optimal Gaussian states

Now we discuss the optimal Gaussian states for the DQS and DCS protocols [44]. In the following, we first show that a single-mode squeezed-vacuum state is the optimal Gaussian probe for single-mode sensing.

The Gaussian input state $\hat{\rho}$ in equation (35) is fully characterized [62] by its quadratures' mean vector \boldsymbol{a} and covariance matrix \mathbf{V} , where the quadratures are defined as $\operatorname{Re}(\hat{a})$ and $\operatorname{Im}(\hat{a})$. Then, writing $\hat{\rho}$ as the Gaussian state $\hat{\rho}_{G}(\boldsymbol{a}, \mathbf{V})$, we get $\hat{\rho}_{G}(\sqrt{\eta} \boldsymbol{a} + \alpha, \eta \mathbf{V} + (1 - \eta)\mathbf{I}/4)$ for a Gaussian state $\hat{\rho}(\alpha)$, where $\boldsymbol{\alpha} \equiv [\alpha, 0]$ and \mathbf{I} is the 2 × 2 identity matrix. Thus, $\hat{\rho}_{G}(\sqrt{\eta} \boldsymbol{a} + \alpha + \epsilon, \eta \mathbf{V} + (1 - \eta)\mathbf{I}/4)$ for the Gaussian state

 $\hat{\rho}(\alpha + \epsilon)$, where $\epsilon \equiv [\epsilon, 0]$. The quadrature covariance matrix of an arbitrary $\hat{\rho}_{\rm G}(\boldsymbol{a}, \mathbf{V})$ can always be written in the form of $\mathbf{V} = \mathbf{R}_{\theta} \mathbf{V}_{\rm diag} \mathbf{R}_{\theta}^{\rm T}$, where $\mathbf{V}_{\rm diag} = {\rm Diag}[(2n+1)e^{-r}/4, (2n+1)e^{r}/4]$ with $r \ge 0, n \ge 0$, and

$$\mathbf{R}_{\theta} = \begin{bmatrix} \cos(\theta) & \sin(\theta) \\ -\sin(\theta) & \cos(\theta) \end{bmatrix}.$$
(42)

With this **V** representation, reference [84] shows how to evaluate the Uhlmann fidelity between $\hat{\rho}_{G}(\sqrt{\eta} a + \alpha, \eta \mathbf{V} + (1 - \eta)\mathbf{I}/4)$ and $\hat{\rho}_{G}(\sqrt{\eta} a + \alpha + \epsilon, \eta \mathbf{V} + (1 - \eta)\mathbf{I}/4)$ (see reference [85] for a general method of calculating fidelity between Gaussian states). Using the result of that evaluation in equation (22) gives

$$I_{\rm F}[\hat{\rho}(\alpha)] = \frac{4\{e^r(1-\eta) + (2n+1)\eta[e^{2r}\cos^2(\theta) + \sin^2(\theta)]\}}{(e^r(1-\eta) + (2n+1)\eta)[(2n+1)\eta e^r + 1 - \eta]}.$$
(43)

This expression's maximum over θ and n occurs when $\theta = n = 0$, in which case $\max_{\theta,n} I_F[\hat{\rho}(\alpha)] = 4/(\eta e^{-r} + 1 - \eta)$ with mean the photon-number constraint $N_S = \mathbf{a}^T \mathbf{a} + [\cosh(r) - 1]/2$. From this result it is clear that $\mathbf{a} = \mathbf{0}$ is optimal, so the UB

$$I_{\rm F}^{\rm Gauss} \leqslant I_{\rm F}^{\rm Gauss,\,max} \equiv \left(\frac{\eta}{4(\sqrt{N_{\rm S}+1}+\sqrt{N_{\rm S}})^2} + \frac{1-\eta}{4}\right)^{-1},$$
 (44)

is achieved by a single-mode squeeze-vacuum state.

One can then solve the separable Gaussian input case, via considering the power distribution $\{N_m\}_{m=1}^M$ across different modes. Optimization over the additive Fisher information gives the UB

$$I_{\rm F}^{\rm Gauss,C} \leqslant I_{\rm F}^{\rm Gauss,\,C,\,max} \equiv \left(\frac{\eta}{M\left(\sqrt{N_{\rm S}/M + 1} + \sqrt{N_{\rm S}/M}\right)^2} + \frac{1-\eta}{M}\right)^{-1},\tag{45}$$

which is achievable by an i.i.d. product of single-mode squeezed-vacuum state. At $\eta = 1$, equation (45) reduces to equation (32), confirming that in a lossless case the Gaussian state is the optimum. For the entangled input, as we explained in section 3.1.2, one can reduce the *M*-probing problem to a single probing and obtain

$$I_{\rm F}^{\rm Gauss,E} \leqslant I_{\rm F}^{\rm Gauss, E, \max} \equiv \left(\frac{\eta}{M\left(\sqrt{N_{\rm S}+1}+\sqrt{N_{\rm S}}\right)^2} + \frac{1-\eta}{M}\right)^{-1},\tag{46}$$

which is achievable by an entangled input designed in section 3.1.2. Similarly, at $\eta = 1$, equation (46) reduces to equation (34), affirming that in the lossless case the Gaussian state is optimal.

4.4. Multiparameter quantum Cramér-Rao bound

In distributed sensing, although a single scalar function is being estimated, one in general needs a multi-parameter quantum CR bound to analyze the performance limit of an unbiased estimation. Here, we generalize the analyses in section 4.1.

Consider the estimation of parameters α of the state $\hat{\rho}_M(\alpha) = \hat{U}(\alpha) \hat{\rho}_M \hat{U}^{\dagger}(\alpha)$ given in equation (2). For distributed sensing, it suffices to consider $\hat{U}(\alpha) = \exp\left(-\sum_{m=1}^M \hat{H}_m \alpha_m\right)$, with generators \hat{H}_m commuting. In a general multi-parameter estimation scenario, one performs measurement and obtains an estimator $\tilde{\alpha} = (\tilde{\alpha}_1, \dots, \tilde{\alpha}_M)$. The precision is characterized by the covariance matrix with elements

$$\boldsymbol{V}_{mn} = \langle \left(\tilde{\alpha}_m - \alpha_m \right) \left(\tilde{\alpha}_n - \alpha_n \right) \rangle. \tag{47}$$

Similar to equation (23), we introduce the SLD \hat{L}_{α_m} for each parameter. Then, the Fisher information matrix has elements

$$\boldsymbol{H}_{mn} = \operatorname{tr}\left[\hat{\boldsymbol{\rho}}_{M}\left(\boldsymbol{\alpha}\right)\frac{\hat{L}_{\alpha_{m}}\hat{L}_{\alpha_{n}} + \hat{L}_{\alpha_{n}}\hat{L}_{\alpha_{m}}}{2}\right].$$
(48)

For an arbitrary weight matrix *G*, we have the CR bound

$$\operatorname{Tr}\left[\boldsymbol{G}\boldsymbol{V}\right] \geqslant \operatorname{Tr}\left[\boldsymbol{G}\boldsymbol{H}^{-1}\right]. \tag{49}$$

For distributed sensing, we focus on the estimation of $\bar{\alpha} \equiv \sum_{\ell=1}^{M} w_{\ell} \alpha_{\ell}$ in equation (3) and therefore one can choose $\boldsymbol{G} = \boldsymbol{w}^{\mathrm{T}} \boldsymbol{w}$ in equation (49) to obtain the ultimate limit of distributed sensing in estimating $\bar{\alpha}$ as

$$\delta \alpha^2 \equiv \operatorname{tr} \left[\boldsymbol{w}^{\mathrm{T}} \boldsymbol{w} \boldsymbol{V} \right] \geqslant \operatorname{tr} \left[\boldsymbol{w}^{\mathrm{T}} \boldsymbol{w} \boldsymbol{H}^{-1} \right].$$
(50)

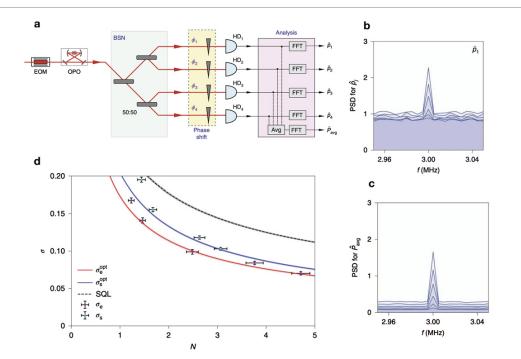


Figure 8. DQS experiment for optical phase sensing using CV multipartite entanglement. (a) Experimental diagram. OPO: optical parametric oscillator; EOM: electro-optic modulator; BSN: beam-splitter network; HD: homodyne detector; FFT: fast Fourier transform. (b) The frequency-domain measurement data acquired by the first sensor, showing a signal peak at 3 MHz and a noise floor. (c) The averaged measurement data in the frequency domain. The averaged data show a higher signal-to-noise ratio than the measurement data acquired at a single sensor due to the entanglement-enabled cancellation of measurement noise from different sensors. (d) Comparison of the measurement sensitivities of the DQS scheme and the DCS scheme. σ_e^{opt} : optimal measurement sensitivity for DQS; σ_s : experimental measurement sensitivity for DCS. Copyright © 2019, The Author(s), under exclusive licence to Springer Nature Limited [55].

An alternative bound from the right logarithmic derivative can be obtained similarly. For multiple-parameter estimation, the readers can refer to references [86-91].

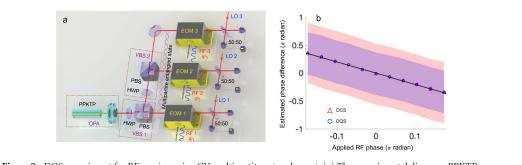
Evaluating the Fisher information matrix in equation (48) is in general challenging, but can be done for Gaussian states [65], as the fidelity can be evaluated by the method in reference [75].

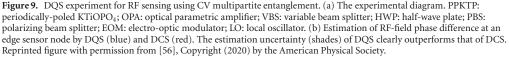
5. Applications of distributed quantum sensing

DQS has been demonstrated in two experiments based on CVs [55, 56], and very recently, in two other experiments based on DVs [59, 60]. We next introduce the two CV DQS experiments and discuss their applications in optical phase and RF sensing.

5.1. Optical phase sensing

Guo *et al* verified the principle of DQS in a CV quantum-optics platform. Figure 8(a) illustrates the experimental setup. An electro-optic modulator (EOM) creates 3 MHz sidebands of a 1550 nm beam, which is subsequently injected into an optical parametric oscillator (OPO) cavity as the seed. The OPO cavity is pumped below the oscillation threshold and produces displaced squeezed light at the 3 MHz sidebands at its output. The displaced squeezed light is then split into four arms by a beam-splitter network (BSN) comprising three 50:50 beam splitters. Each arm serves as a sensor node to probe an optical phase shift controlled by wave plates. The objective of the sensing task is to measure a global parameter, the average phase shift, across the sensor network. To this end, a homodyne detector (HD) measures the quadrature displacement at each sensor. The measurement data from four sensors are postprocessed to derive the average phase shift. The frequency-domain data acquired by a single sensor are plotted in figure 8(b), where the signal peak at 3 MHz and the measurement-noise floor can be clearly identified. The spectrum of the signal averaged over four sensors is depicted in figure 8(c). Due to the quantum correlation between the measurement noise at different sensors, the noise power after averaging is significantly reduced, leading to a higher signal-to-noise ratio than that at a single sensor. In figure 8(d), the performance of DQS (red solid curve) is compared with that of DCS (blue solid curve) and the SQL (black dashed curve). The





DCS experiment employs separable displaced squeezed states at the sensors subject to the same total mean photon number as the DQS experiment based on entangled probe states. The derivation of the SQL assumes that the sensors utilize classical coherent light to estimate the average optical phase shift. DQS outperforms both the DCS and SQL at all mean photon-number levels. The DCS performs better than the SQL due to single-mode squeezed light used by each sensor. This DQS experiment demonstrated an entanglement-enabled quantum advantage over *all* DCS protocols using the same probe power.

5.2. RF sensing

In addition to optical phase sensing, DQS can enhance a wide range of sensing applications by introducing transducers that covert the probed physical parameters into modulations on the entangled probe state in the optical domain. Xia *et al* [56] recently reported an experiment of DQS for RF sensing, as sketched in figure 9(a). Squeezed light is produced from an optical parametric amplifier (OPA) cavity in which a type-0 periodically-poled KTiOPO₄ (PPKTP) crystal is embedded. The OPA cavity is seeded with 1550 nm light such that its output consists of a strong classical coherent state at the central wavelength and phase squeezed vacuum state residing at the sidebands. Two variable beam splitters (VBSs), each composed of a half-wave plat (HWP) and a polarizing beam splitter (PBS), constitute a quantum circuit that configures the multipartite entangled state. As we discuss below, one needs to tailor the structure of the multipartite entangled state to achieve the optimal performance for a specified RF-sensing task such as average RF-field amplitude estimation or angle-of-arrival estimation via RF-field phase difference measurements. In the experiment, a three-mode entangled state is generated for probing a global property of the RF field observed at three RF-photonic sensors. The RF field at the *m*th RF-photonic sensor can be represented as

$$\mathcal{E}_m(t) = E_m \cos(\omega_c t + \varphi_m),\tag{51}$$

where A_m is the RF amplitude, ω_c is the RF carrier frequency, t is time, and φ_m is the RF phase. Under the weak-field limit, an EOM converts the RF field into a displacement

$$\alpha_m \propto E_m \varphi_m \tag{52}$$

on the phase quadrature. A balanced homodyne detector measures the quadrature displacement, yielding an estimator $\tilde{\alpha}_m$. Postprocessing on the $\tilde{\alpha}_m$'s from all three sensors leads to an estimation on the RF-field property of interest.

Three RF-sensing tasks were investigated in the experiment: RF-field average amplitude estimation, phase-difference estimation at a central sensor node, and phase-difference estimation at an edge sensor node. The same RF-sensing tasks were carried out by DCS as a performance benchmark. In DCS that defines the SQL, the sidebands were in vacuum states after turning off the entangled states while the strong coherent state remains at the central wavelength was retained. Figure 9(b) compares the estimation uncertainty of DQS (blue shade) and DCS (red shade) under the task of measuring the phase difference at an edge node. DQS enjoys an appreciable advantage over DCS by virtue of the multipartite entangled state shared by the three sensors. The DCS experiment used ~100 μ W of optical power, whereas the DQS experiment further introduced entangled sidebands at a sub-nW power level to beat the SQL. As such, the DQS and DCS protocols *in practice* used almost the same amount of probe power. The performance of the demonstrated DQS protocol can also be compared with a DCS protocol based on local separable squeezed states with the same total mean photon number as that of the entangled states employed in the DQS

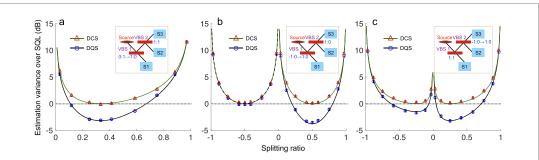
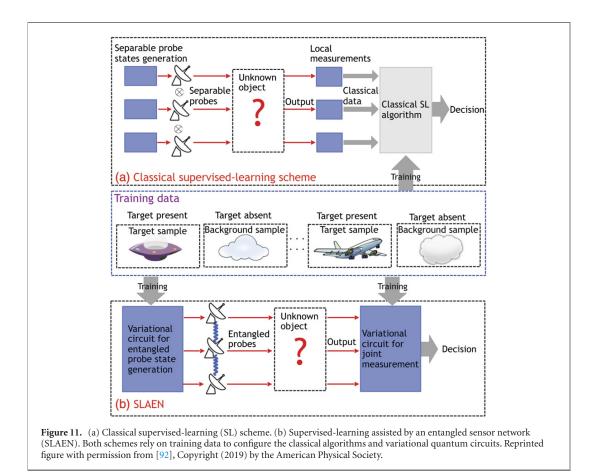


Figure 10. Optimization of multipartite entangled state for (a) RF-field average amplitude estimation, (b) phase-difference estimation at a central sensor node, and (c) phase-difference estimation at an edge sensor node. Insets show the tuning ranges of the splitting ratios for VBSs. Circles: DQS experimental data; triangles: DCS experimental data; solid curves: theory. Reprinted figure with permission from [56], Copyright (2020) by the American Physical Society.



protocol. Like the phase-sensing experiment [55], the DQS protocol only needs one squeezed-light source in contrast to three separate squeezed-light sources required by the DCS protocol, thereby enjoying a substantially reduced implementation complexity. Nonetheless, the DQS protocol still demonstrated a \sim 10% signal-to-noise-ratio advantage over the DCS protocol based on separable squeezed states [56].

The entangled senor network is reconfigurable in that the multipartite entangled state can be tailored by the quantum circuit to minimize the estimation uncertainty for a specified RF-sensing problem. To build a connection between the structure of the multipartite entangled state and the performance of a RF-sensing problem, Xia *et al* optimized the multipartite entangled state by tuning the parameters of the quantum circuit and measured the variance of estimation under different settings [56]. The theoretical predictions (solid curves) and experimental data for DQS (circles) and DCS (triangles) are depicted in figure 10. Entanglement optimization for three RF-sensing problems are studied: RF-field average amplitude estimation (figure 10(a)), phase-difference estimation at a central sensor node (figure 10(b)), and phase-difference estimation at an edge sensor node (figure 10(c)). In all cases, the splitting ratio of one VBS

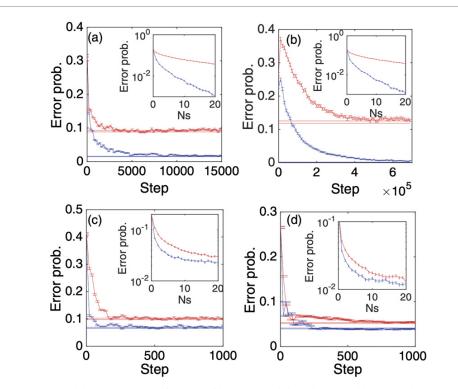


Figure 12. Error probability vs training steps for SLAEN (blue curves) and classical supervised learning (red curves). (a), (b), (c), and (d) assume different source brightness and system efficiencies in their simulations. Insets: the scaling of the error probability with respect to the source brightness. Reprinted figure with permission from [92], Copyright (2019) by the American Physical Society.

of the quantum circuit is tuned while the other VBS's splitting ratio is fixed. In the optimization of the multipartite entangled state for phase-difference estimation, the phase of one arm of the quantum state is flipped between 0 and π as an additional knob. The largest advantage of DQS over DCS is only achieved at an appropriately chosen beam-splitter ratio and phase, highlighting the necessity of tailoring the entangled probe state for different RF-sensing tasks. Notable, a consequence of the quantum correlations between the measurement noise at different sensors, the DQS estimation variances show asymmetric behaviors as the phase is flipped [56].

5.3. Machine-learning applications

Quantum machine learning [7–13] has recently spurred broad interest as it creates new opportunities to harness the power of quantum resources to reduce the complexity of many data-processing problems. At present, however, large-scale fault-tolerant random access quantum memories and NISQ devices with sufficient circuit depths remain elusive to allow many quantum machine-learning schemes to achieve an advantage over classical machine-learning schemes.

Many real-world applications rely on sensors to acquire data for classical machine-learning algorithms to perform further processing, e.g., classification or compression. A conventional classical supervised-learning scheme is illustrated in figure 11(a) using a target classification example. Sensors in separable quantum states probe an object, generating local measurement data that are processed by a classical supervised-learning algorithm. The classical supervised-learning algorithm is first trained using known objects such that it becomes capable of processing data acquired from interrogating unknown objects once the training completes. The involvement of sensors opens a window to leverage DQS to achieve quantum-enhanced performance in data processing. In particular, as machine-learning applications often only requires the acquisition of a global property, such as the class of the sample, it is natural that DQS can be utilized to benefit. Supervised learning assisted by an entangled sensor network (SLAEN) [92], illustrated in figure 11(b) is a recently developed hybrid quantum–classical machine-learning scheme that reaps such benefits from DQS. In SLAEN, a variational quantum circuit is trained by a classical supervised-learning algorithm to generate entangled states shared by the sensors. After interrogating the object, a second variational quantum circuit processes the quantum state prior to measurements. The measurement data are fed to a classical algorithm to complete data processing. Like the classical supervised-learning scheme,

SLAEN also rest upon training data to configure the variational quantum circuit and the classical algorithm to achieve the optimal performance and largest quantum advantage.

The error probabilities of SLAEN (blue curves) and the classical supervised-learning scheme (red curves) during the training process are plotted in figure 12 for different physical parameters. It is evident that SLAEN achieves a quantum advantage over the classical supervised-learning scheme by enabling a reduced error probability in solving data-classification problems. Since sensors are ubiquitous for data collection, SLAEN and DQS would pave a distinct and broad route for quantum-enhanced data processing in the NISQ era, as demonstrated in a recent experiment for the classification of RF signals [93].

6. Outlook

As a new paradigm for quantum metrology, DQS endows new quantum-enhanced capabilities for applications built upon a network of sensors. Yet, a few fundamental questions about DQS remain unanswered. First, although section 3.1 has elucidated the optimal DQS scheme for displacement sensing in the absence of loss and the optimal Gaussian scheme in the presence of loss, and section 3.2 provided the optimal Gaussian DQS scheme for phase sensing, a general optimal DQS scheme remains unknown and warrants future investigations. Second, it is well known that non-Gaussian resources such as the GKP state [61] lead to universality in CV quantum computing [94]. It is shown that the GKP state can improve the performance of DQS by compensating for loss [57], but it calls for further studies to assess the utility of non-Gaussian probe states and measurements in DQS. Third, DV DQS protocols are useful for a variety of applications such as magnetic and stress sensing, but they are less explored than CV DQS protocols. In particular, it would be worthwhile to conduct a systematic analysis on the performance of DV DQS protocols subject to practical nonidealities. Also, scalable creation of DV entangled states and distributing them to DV sensors need additional research.

From an application perspective, DQS can be exploited to address sensing and data-processing problems in different physical domains. For example, a recent theoretical proposal envisages use of DQS to boost the performance of fiber gyroscopes for navigation applications [95]. The idea is to inject multimode entangled light, like what was utilized in the DQS RF-sensing experiment [56], into to an array of fiber gyroscopes to improve the scaling of the measurement noise. Such a configuration would also be applicable to enhancing the readout signal-to-noise ratio of an array of optomechanical transducers used in inertial sensing [96] and atomic force microscopes [97]. With the recently developed SLAEN framework, it would be foreseeable that an array of entangled sensor can be trained to benefit physical-layer data processing tasks such as biological molecular identification and object tracking [36, 98]. More generally, a quantum network of clocks [99] can also be considered as a DV DQS system in which the entanglement shared by distributed quantum-network nodes can boost the stability of accuracy of synchronizing remote atomic clocks.

The experimental demonstrations of DQS so far are all based on table-top quantum-optics platforms. Recent advances in on-chip generation of squeezed light [100–103] and entangled photons [104, 105], in conjunction with efficient on-chip transducers [106], have promised a more scalable and cost-effective solution for the widespread deployment of CV DQS protocols. On the DV front, large-scale integration of color centers with photonic circuits has been recently achieved [107], opening a route for utilizing DQS to benefit chip-scale magnetic and electric-field sensing applications.

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ORCID iDs

Zheshen Zhang ⁽¹⁾ https://orcid.org/0000-0002-8668-8162 Quntao Zhuang ⁽¹⁾ https://orcid.org/0000-0002-9554-3846

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