A review of mechanisms generating seismic anisotropy in the upper mantle

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7 Abstract

Seismic anisotropy is a key observational tool for mapping flow in Earth's upper mantle. However, 8 interpreting patterns of anisotropy relies on a firm understanding of the microphysical mechanisms 9 that generate anisotropy. Here we discuss our current understanding of the generation of intrinsic and 10 extrinsic seismic anisotropy in upper-mantle rocks. Intrinsic anisotropy results from the elastic 11 anisotropy of the constituent minerals. We address the role of thermochemical conditions in 12 modifying the manner in which these minerals align with the deformation reference frame, controlling 13 the macroscopic anisotropy. Extrinsic anisotropy results from the composite behavior of a material 14 15 composed of multiple phases. We examine the influence of mineralogical layering and the presence of a melt phase on anisotropy, including the interaction between extrinsic and intrinsic anisotropy. 16 Finally, we compare and contrast existing methods to forward model the development of anisotropy in 17 the upper mantle and demonstrate that current predictions suggest most observed anisotropy results 18 from intrinsic anisotropy when fluids are not present. 19

20 1 Introduction

Mapping the patterns of flow in Earth's convecting mantle is an essential component of understanding the dynamics and evolution of our planet. Without the option for direct observation, we must turn to indirect means for inferring flow. Perhaps the most successful endeavour in this regard has been observations of anisotropy in the seismic properties of the upper mantle. That is, seismic wave speeds 25 can vary as a function of their propagation and/or polarization directions (e.g., Crampin, 1981).

In a critical early contribution, Hess (1964) recognized that P-waves propagating parallel to fracture 26 zones in the eastern Pacific were faster than those propagating perpendicular to fracture zones. From 27 this observation he recognized a correlation between seismic anisotropy and tectonic processes in the 28 upper mantle. This key insight opened the possibility of mapping patterns of mantle convection using 29 seismological techniques. Subsequent efforts aimed to use global maps of anisotropy in polarization 30 direction (Nataf et al., 1984) or propagation direction (Tanimoto and Anderson, 1984) to interpret 31 large-scale flow patterns, leading to a variety of new insights into upper mantle dynamics. A wide 32 range of global (e.g., Beghein et al., 2014; Chang et al., 2015; French and Romanowicz, 2014; Moulik 33 and Ekström, 2014; Schaeffer and Lebedev, 2013) and regional (e.g., Fichtner et al., 2010; Gaherty et 34 al., 1996; Nishimura and Forsyth, 1989; Russell et al., 2019; Yuan and Romanowicz, 2010) 35 tomographic models including anisotropy are now available. Many of these models have been 36 demonstrated to agree well with simulations of mantle convection (Becker et al., 2014, 2006). Besides 37 tomographic models, seismic anisotropy is frequently detected by the splitting of core-refracted shear 38 waves (SKS, SKKS), which have a much better lateral resolution than surface waves, but are lacking 39 40 in vertical resolution. Nevertheless, these teleseismic phases are demonstrated to be mostly sensitive to the anisotropy at upper mantle depths (Sieminski et al., 2008). As such, they provide important 41 information about fabrics and their relation to flow patterns within this part of the mantle (e.g., Eakin 42 et al., 2018; Long and Silver, 2008; Silver, 1996; Wolfe and Solomon, 1998). 43

Although much progress has been made in understanding mantle dynamics from seismic anisotropy,
most of this work relies on assumptions about the physical origin of that anisotropy. Seismic
anisotropy results from anisotropy in a medium's elastic properties. Considering the typical
wavelengths of teleseismic waves (>5 km), seismic anisotropy is essentially an average of the
anisotropy of features smaller than those wavelengths, including features at the grain scale (microns to
millimeters) and the outcrop scale (meters to kilometers). As illustrated in Figure 1a, crystals of all

minerals are inherently anisotropic in their elastic properties, and crystallographic alignment of many crystals in an aggregate can lead to a material that is macroscopically anisotropic, a phenomenon referred to as *intrinsic* anisotropy. The manner in which those crystals align depends on a wide range of physical and chemical variables. Additionally, as illustrated in Figure 1b, layering (or other non-random arrangements) of different materials can lead to macroscopic anisotropy, which is referred to as *extrinsic* anisotropy. The layered materials can be anything with contrasting elastic properties such as combinations of different minerals or liquids.

Observations of seismic anisotropy are therefore often linked to thermochemical conditions and the 57 history of mantle processes. These links are extremely useful for understanding modern geodynamic 58 59 systems, testing geodynamic hypotheses, and benchmarking geodynamic simulations. However, interpretations must also be made carefully, as the geometric relationships between seismic anisotropy 60 and large-scale mantle processes can change dramatically depending on the mechanism leading to 61 62 anisotropy and the ambient physical and chemical conditions, some of which are not yet fully understood (e.g., Bernard et al., 2019; Hansen et al., 2014; Jung and Karato S, 2001; Mainprice et al., 63 2005). Here we review the common mechanisms for generating anisotropy in upper mantle rocks, 64 65 describe their implementation into geodynamic simulations, and discuss first-order predictions of the distribution of anisotropy in the upper mantle. 66

67 2 Definitions of anisotropy

The terminology used to describe anisotropy is varied and may often differ between mineral physicists
and seismologists. Several reviews have recently outlined the nomenclature and physical meaning of
different descriptors of anisotropy (Almqvist and Mainprice, 2017; Long and Becker, 2010;

71 Mainprice, 2007; Skemer and Hansen, 2016) and we only briefly introduce the key terminology here.

72 The seismic anisotropy of an elastic medium can be described both in terms of P-waves and in terms

73 of S-waves. In general, P-wave anisotropy is a description of the variation in the P-wave velocity, V_P,

74 as a function of the propagation direction and is often reported as a percentage deviation from the

average $V_{\rm p}$. S-waves entering an anisotropic medium are decomposed into two orthogonally polarized S-waves with different velocities. The S-wave anisotropy is generally described by either the difference in velocity between the slow and fast S-waves, $\Delta V_{\rm s}$, or by the polarization direction of the fast wave. A full description of P-wave and S-wave anisotropy can be calculated for any elastic medium if all components of the elastic stiffness tensor, C_{ijkl} , of the medium are known (21 independent values for the most general case). In that case, one can calculate the Christoffel tensor,

$$T_{ik} = C_{iikl} d_i d_l, \tag{1}$$

81 where *d* is the direction of wave propagation (for a review, see Mainprice, 2007). The key wave
82 velocities are then given by

$$V_{\rm p} = \sqrt{\frac{\lambda_1}{\rho}}, \quad V_{\rm s1} = \sqrt{\frac{\lambda_2}{\rho}}, \quad \text{and} \quad V_{\rm s2} = \sqrt{\frac{\lambda_3}{\rho}},$$
(2)

83 where λ_1 , λ_2 , and λ_3 are the eigenvalues of T_{ik} and ρ is the density. V_{s1} and V_{s2} are the fast and slow 84 S-wave polarizations, respectively, and their difference is ΔV_s . The eigenvectors of T_{ik} represent the 85 polarization directions of the three waves, respectively.

The elastic properties of geological materials often exhibit symmetry that reduces the number of 86 87 independent values of the stiffness tensor. Two key examples are orthorhombic symmetry, found in 88 olivine and orthopyroxene, and hexagonal symmetry (also referred to as transverse isotropy)¹, found in the high-pressure phase of iron. In the former, three distinct and orthogonal directions describe the 89 maximum, intermediate, and minimum directions of anisotropy. In the latter, a single plane exists in 90 which the medium appears isotropic, while the direction normal to that plane exhibits significantly 91 different properties. General anisotropy can be decomposed into stiffness tensors with these higher 92 symmetries (Browaeys and Chevrot, 2004), allowing the overall symmetry of the elastic properties to 93 be assessed. 94

95 Due to the nature of tomographic inversions of seismic data, complete characterization of all elements

¹ For further insight into the form of the stiffness tensor for a given symmetry, see Appendix E in Nye (1985).

96 of the stiffness tensor is generally not feasible. Therefore, the anisotropy is often assumed to be of
97 reasonably high symmetry and in a favorable orientation to reduce the necessary number of
98 parameters for its description. A common descriptor of anisotropy observed in Earth is the radial
99 anisotropy, *ξ*, which is defined as the squared ratio of the horizontally polarized S-wave velocity to the

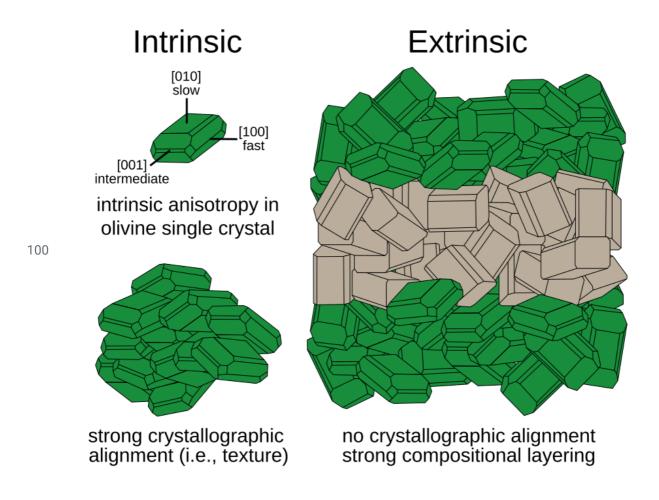


Figure 1: Schematic illustration of intrinsic and extrinsic anisotropy. Intrinsic anisotropy results from
the crystallographic alignment of crystals that are inherently anisotropic. Extrinsic anisotropy results
from the heterogeneous spatial distribution of multiple phases (e.g., compositional layering).

¹⁰⁴ vertically polarized S-wave velocity, $\left(\frac{V_{\text{SH}}}{V_{\text{SV}}}\right)^2$. This description of anisotropy effectively assumes that ¹⁰⁵ the stiffness tensor has transverse isotropy with the axis of symmetry normal to Earth's surface. ¹⁰⁶ Transverse isotropy can also be described with the Love parameters² (*A*, *C*, *F*, *L*, *N*), for which *A* and

¹⁰⁷ ² See also the relationship between the Love parameters and the Thomsen parameters (e.g., Mainprice, 2007)

108 *C* relate to the P-wave anisotropy and *L* and *N* relate to the S-wave anisotropy ($\xi = N/L$). The Love 109 parameters were expanded for more general anisotropy by Montagner and Nataf (1986). Departures 110 from radial anisotropy can be described by the azimuthal anisotropy, which is based on changes in 111 wave speed for different propagation or polarization directions within the plane parallel to Earth's 112 surface. Based on the expansion by Montagner and Nataf (1986), magnitudes of azimuthal anisotropy, 113 *G*, are often reported as a percentage of the parameter *L*.

114 **3 Generation of anisotropy**

Interpreting seismological observations of the magnitude, orientation, and symmetry of anisotropy, or forward modelling their evolution, requires an intimate understanding of the physical mechanisms leading to that anisotropy. A wide range of physical processes contribute to generating anisotropy in rocks, and here we describe the primary processes relevant to anisotropy in Earth's upper mantle.

119 3.1 Intrinsic anisotropy

All minerals are inherently anisotropic in their physical properties. As an extreme example, if grains 120 within an aggregate all share the same crystallographic orientation (i.e., they have a single 121 crystallographic preferred orientation, or CPO), then the aggregate will exhibit macroscopic 122 anisotropy identical to that of a single crystal. In a more typical example, grain orientations may not 123 be exactly the same, but grains with certain orientations have a higher probability of occurring (i.e., 124 the orientation distribution is non-uniform), in which case some anisotropy will still be imparted to 125 the macroscopic aggregate. In general, we refer to these aggregates as *textured*, which is a more 126 general term that also refers to aggregates with multiple, high-probability crystallographic preferred 127 128 orientations.

Precise calculation of the elasticity of an aggregate of anisotropic grains is nontrivial, particularly
because of the local requirements to maintain strain compatibility and stress equilibrium. Recent
reviews of this topic have been provided by Almqvuist and Mainprice (2017) and Skemer and Hansen

132 (2016). The most robust methods currently available involve explicitly discretizing the microstructural arrangement of grains and solving for the stress and strain fields using the 133 finite-element method (e.g., Zhong et al., 2014) or a Fourier-transform-based approach (e.g., Brenner 134 et al., 2009). These computationally expensive techniques can be used to benchmark simplified 135 averaging schemes, such as the Voigt and Reuss bounds, which assume every grain is subject to the 136 same strain or the same stress, respectively, or the Hill average, which takes the arithmetic mean of 137 the stiffness tensors predicted by the Voigt and Reuss bounds. Of these simplified averages, the Voigt 138 average is commonly used in the geosciences since it best approximates the magnitude of anisotropy 139 in the aggregate (Crosson and Lin, 1971; Peselnick et al., 1974; Zhong et al., 2014). 140

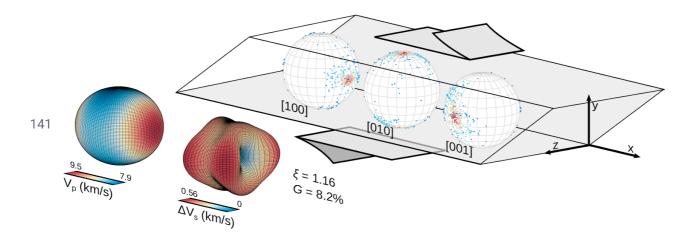


Figure 2: Demonstration of intrinsic seismic anisotropy generated from a typical CPO in an experimentally sheared olivine aggregate (sample PT0651 from Hansen et al. (2012a)). The shear direction is parallel to *x*. 3-D diagrams are given for crystallographic orientation distributions, the directional dependence of P-wave velocities, and the directional dependence on the difference in S-wave velocity between the two s-wave polarizations. Values are reported for the magnitude of radial anisotropy, ξ , and the magnitude of azimuthal anisotropy, *G*, as a percentage of *L*. 3-D projections were generated with the MTEX toolbox for Matlab[®] (Mainprice et al., 2011).

149 Figure 2 presents an example of the macroscopic elastic seismic properties calculated from a

150 distribution of orientations of olivine crystals in an experimentally deformed peridotite using the Voigt

average. This particular sample exhibits strong alignment of [100], with moderate alignment of [010] 151 and [001]. The V_p and ΔV_s anisotropies are dominated by the [100] alignment, leading to an aggregate 152 anisotropy with nearly hexagonal symmetry, even though a single crystal of olivine has orthorhombic 153 symmetry. Because intrinsic anisotropy arises from crystal orientation distributions, mechanisms for 154 producing anisotropic aggregates inherently involve grain rotations. Importantly, those grain rotations 155 need to be linked somehow to the crystallography. The two primary mechanisms for grain rotation 156 linked to crystallographic orientations are crystal-plastic deformation and rigid rotation of elongate 157 grains whose shape is crystallographically controlled. 158

159 3.1.1 Grain rotations controlled by crystal-plastic dislocation motion

Crystal plastic deformation inherently involves the motion of lattice dislocations. Dislocations are line 160 defects in a crystal whose motion results in a shear strain of the lattice (for a recent review, see 161 Kohlstedt and Hansen, 2015 and references therein)(for a recent review, see Kohlstedt and Hansen, 162 2015). This can be visualized as a lattice plane along which shearing occurs (the slip plane), whose 163 normal vector is **n**. Slip only occurs in the slip direction, which is defined by the Burgers vector, **b**. 164 The two vectors **n** and **b** define a slip system. The slip system can only operate if a shear stress is 165 166 applied on the slip plane in the direction of the burgers vector. For arbitrary stress states, the resolved shear stress describes the magnitude of the stress acting on the slip plane in the slip direction. The 167 168 Schmid tensor is defined as,

$$M_{ij} = \frac{1}{2}(b_i n_j + b_j n_i),$$
(3)

and provides a framework for determining the resolved shear stress, τ , according to $\tau = M_{ij}\sigma_{ij}$, where σ is the deviatoric stress tensor. The motion of dislocations in their slip plane (i.e., glide) produces a shear strain in the reference frame of the slip system at a given strain rate, γ , that is related to the full strain rate tensor according to $\dot{\epsilon}_{ij} = M_{ij}\gamma$.

173 In addition to strain, the glide of dislocations also produces a rotation, defined as

$$Q_{ij} = \frac{1}{2}(b_i n_j - b_j n_i), \tag{4}$$

where the rotation tensor, **Q**, defines a rotation about the axis **n**×**b**. Hence, the rotation of crystals due
to dislocation glide is inherently linked to the crystallographic directions **n** and **b**.

Crystalline materials generally have more than one slip system available. However, for the same 176 magnitude of resolved shear stress, different slip systems will produce different strain rates due to 177 differences in the ease of dislocation motion on different glide planes. Importantly, the rate of rotation 178 is given by $Q_{ij}\gamma$. Therefore, slip systems that generate faster strain rates (often referred to as "easy" 179 slip systems) contribute more to the rotation of a grain than do slip systems that generate slower strain 180 rates (often referred to as "hard" slip systems). In some minerals, such as mica, the difference in 181 strength between easy and hard slip systems is so great that the deformation and microstructural 182 evolution is effectively dominated by a single slip system. Therefore, certain mineral systems cannot 183 accommodate an arbitrary deformation if fewer than five linearly independent slip systems are 184 available, as pointed out by von Mises (1928). 185

For olivine, the (010)[100] slip system (where round brackets denote **n** and square brackets denote **b**) 186 is the easiest over a wide range of conditions (Figure 3a). It has been demonstrated experimentally 187 (Bystricky et al., 2000; Hansen et al., 2014; Zhang et al., 2000; Zhang and Karato, 1995) and 188 computationally (Hansen et al., 2016a; Kaminski and Ribe, 2001; Ribe and Yu, 1991; Tommasi et al., 189 2000) that the easy slip system controls the first-order characteristics of the CPO produced during 190 crystal plastic deformation. The key feature of these CPOs is the preferred alignment of the [100] axis 191 of olivine with the shear direction (e.g., Figure 2), which primarily occurs in simulations if the 192 (010)[100] slip system is the easiest slip system. Experimentally, this link between slip system and 193 CPO is assessed by comparing experiments on single crystals to experiments on aggregates of grains. 194 195 Figure 3 depicts the results of a series of single-crystal experiments from Bai et al. (1991).

196 The correspondence between the predicted weak (010)[100] slip system and observed CPOs with 197 [100] aligned with the shear direction suggests that transitions in CPOs as a function of thermomechanical conditions can be predicted from single crystal flow laws. The flow laws for
olivine (Figure 3) reveal the relative strength of different slip systems as a function of stress,
temperature, oxygen fugacity, silica activity, and confining pressure. All slip systems are observed to
have the same stress dependence, so a transition is not observed as a function of stress. All other
parameters, however, do lead to transitions in the easiest slip system, however relatively few of these
parameters have been investigated, as described below. In the discussion that follows, we discuss the
controls on changes in slip systems in olivine in order of most to least constrained.

205 3.1.1.1 Slip system strength as a function of temperature

206 Different activation energies for the various slip systems leads to transitions in the easiest slip system as a function of temperature (Figure 3b). Although the experiments of Bai et al. (1991) were 207 constrained to relatively high temperatures (>1200°C), Carter and AvéLallement (1970) demonstrated 208 transitions in the easiest slip system at lower temperatures in experiments extending down to~600°C. 209 In addition, based on a compilation of data, Goetze (1978) suggested that transitions occur in the easy 210 211 slip system as a function of temperature. Unfortunately, because of the necessary increase in 212 differential stress (and often confining pressure) to maintain laboratory strain rates at lower temperatures, the impact of temperature on CPO has not been rigorously deconvolved from other 213 214 effects.

215 3.1.1.2 Slip system strength as a function of oxygen fugacity

Oxygen fugacity also affects the relative strength of different slip systems (Figure 3c). The primary
role of oxygen fugacity in moderating creep strength is through its influence on point defect
concentrations and therefore on the chemical diffusion that limits the dislocation climb velocity (e.g.,
Kohlstedt and Hansen, n.d.). As evidenced by the crossing of the solid blue and dashed back lines in
Figure 3c, the most obvious transition in relative slip system strength occurs at less than two log units
below the Ni:NiO buffer. This critical oxygen fugacity is within the range of oxygen fugacities in the
upper mantle inferred from basalt chemistry (e.g., Cottrell and Kelley, 2011). However, at low

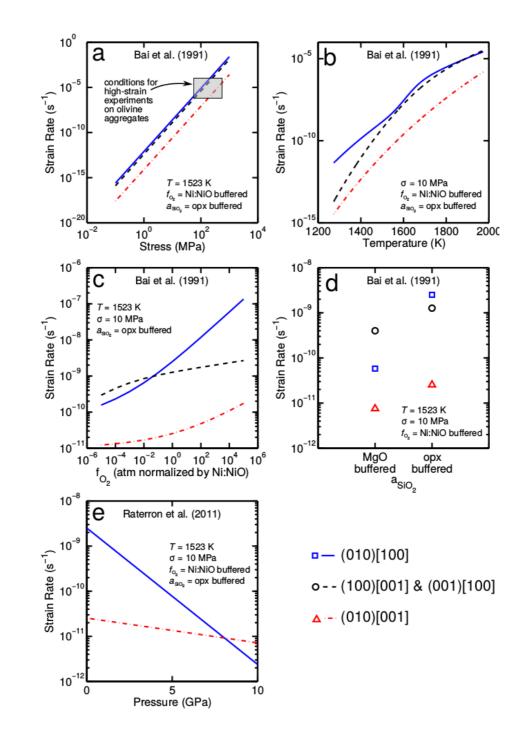


Figure 3: Predictions of strain rates in olivine single crystals as a function of (a) stress, (b)
temperature, (c) oxygen fugacity, (d) silica activity, and (e) confining pressure. Strain rates are
calculated using the flow laws from Bai et al. (1991) and Raterron et al. (2011). For each plot, the
strain rate is indicated as a function of one independent variable, and all other variables are held
constant as indicated.

fugacities in Figure 3c, whether (001)[100] or (100)[001] will dominate is unclear because these slip systems could not be distinguished in the original experiments. Therefore the predicted effect on CPO evolution is uncertain, and the impact of oxygen fugacity on CPO remains a target for future investigation. The closest approach so far comes from Keefner et al. (2011), who examined CPOs in dunites deformed at two very different oxygen fugacities. Unfortunately, the low strains in those experiments and a pre-existing CPO in the starting material make it difficult to isolate any role of oxygen fugacity in modifying the CPO.

236 3.1.1.3 Slip system strength as a function of silica activity

The silica activity of a system also modifies point defect concentrations and therefore can influence the strain rate. Figure 3d demonstrates that the relative strengths of olivine slip systems depends on the silica buffer. As with oxygen fugacity, the role of silica activity in modifying CPO has not been explored. A transition in CPO might be induced by buffering the silica activity with a silica-poor phase like MgO, but it currently seems unlikely that significant portions of the upper mantle have such low silica activity (e.g., Salters and Stracke, 2004).

243 3.1.1.4 Slip system strength as a function of pressure

244 The confining pressure may also influence the relative strengths of different slip systems in olivine. Experiments on forsterite single crystals presented by Raterron et al. (2012, 2011, 2009, 2007) and 245 illustrated in Figure 3e suggest that a slip system with a [001] Burgers vector becomes easiest at 246 confining pressures above ~8 GPa at a temperature of 1523 K (note that Table 4 in Raterron et al. 247 (2012) includes a typo, and flow laws for [011], should be in series rather than in parallel). This 248 transition in slip system strength is predicted to move to lower pressures with increased temperature. 249 Pressure-induced transitions in olivine CPO have been observed in several experiments on dry olivine 250 aggregates (Jung et al., 2009; Ohuchi et al., 2011). 251

Karato et al. (2008) suggested that care must be taken when examining CPO transitions as a functionof confining pressure as most high-pressure experiments are also characterized by high differential

stresses. These high stresses would likely cause a transition from dislocation creep to low-temperature 254 plasticity (Goetze and Poirier, 1978). Under dry conditions, low-temperature plasticity appears to 255 primarily involve [001] dislocations (Carter and Ave'lallemant, 1970; Gaboriaud et al., 1981) 256 Therefore high-pressure experiments producing CPOs with [001] aligned with the shear direction may 257 result from high differential stresses rather than high confining pressures. However, Raterron et al. 258 (2012) subsequently argued that, although involving high differential stresses, many experiments with 259 evidence for high activity of slip systems with [001] Burgers vectors still appear to be dominated by 260 dislocation creep when data are compared to published deformation mechanism maps for olivine 261 (Frost and Ashby, 1982, Chapter 15). Comparison of mechanical data from high-pressure experiments 262 263 to more recently published deformation mechanism maps (e.g., Hansen et al., 2011) confirms the argument of Raterron et al. (2012), with only the data points collected at the highest stresses plotting 264 in the low-temperature plasticity regime. There is still scope, however, for confirming that a 265 266 pressure-induced transition in CPO occurs at lower differential stresses (<300 MPa).

267 3.1.1.5 Slip system strength as a function of water fugacity

The water concentration or water fugacity of a system is also of major importance to olivine 268 deformation. Water fugacity influences point defect concentrations in olivine (e.g., Kohlstedt, 2006), 269 270 significantly impacting rates of dislocation creep. The effect of water on the relative strengths of different slip systems is not depicted in Figure 3 because insufficient flow laws have been published 271 for olivine single crystals deformed under wet conditions. Flow laws exist for the (010)[100] slip 272 273 system (Girard et al., 3/2013) and the (100)[001] and (001)[100] slip systems (Tielke et al., 2017) 274 under wet conditions. However, a complete assessment of the role of water in transitions in the easy slip system requires a flow law for the (010)[001] slip system and, ideally, all three flow laws would 275 be calibrated in the same set of experiments to rule out systematic bias between experimental 276 277 protocols. We note that all these slip systems were also investigated under hydrous conditions in the 278 experiments of Mackwell et al. (1985), however the relatively low confining pressures of those

experiments necessarily involved relatively low water fugacities, and a transition in the easiest slipsystem was not observed.

Although water-induced transitions in slip system strength have not been rigorously demonstrated, a 281 variety of experimental studies on aggregates of olivine have documented transitions in CPO 282 associated with different combinations of water concentration, temperature, and differential stress 283 (Jung et al., 2006; Jung and Karato S, 2001; Katayama et al., 2004). These results suggest that the 284 incorporation of dissociated water into the olivine lattice can lead to distinct differences in the 285 crystallographic axes that align with the shear direction. The systematics and mechanisms behind 286 these water-induced transitions in CPO were reviewed by Karato et al. (2008). However, a 287 demonstrable link between olivine CPO and the behavior of olivine single crystals under wet 288 conditions remains a clear target for future research. 289

Recent studies of naturally deformed peridotites have looked for evidence of a relationship between 290 CPO and water content. Based on analysis of water in four samples from shear zones in the Josephine 291 292 Peridotite, Skemer et al. (2013) concluded that CPO varies as a function of water content. However, Kumamoto et al. (2019) found that CPO type does not vary systematically as a function of olivine 293 water content. Bernard and Behr (2017) found that, in xenoliths from the Mojave lithospheric mantle, 294 olivine CPO does not correlate with water content, while Bernard et al. (2019) reached the same 295 conclusion in a survey of global xenoliths. All of these studies have also found that CPO does not 296 vary systematically with strain or stress, suggesting that the kinematics of deformation may be the 297 controlling factor in the type of CPO that develops. However, further studies of peridotites in settings 298 where deformation conditions can be constrained are needed to elucidate the variables controlling 299 300 olivine CPO.

301 3.1.1.6 Mechanisms for changes in slip system strength

302 The mechanisms behind changes in the relative strengths of slip systems as a function of the physical303 and chemical conditions that control dislocation motion are not yet clear. In olivine, the dislocation

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glide velocity, and therefore the induced grain-rotation rate, during dislocation creep is generally 304 thought to be limited by the dislocation climb velocity (e.g., Kohlstedt, 2006). That is, discrete 305 obstacles (e.g., dislocation dipoles) act to impede dislocation glide, and those obstacles are overcome 306 (or they are removed) by dislocation climb, which is relatively slow. The specific relationship between 307 the climb velocity and the macroscopic relationship is complex, and requires knowledge of the details 308 of the dislocation arrangement. Useful examples of this complexity in olivine are presented in the 309 discrete-dislocation dynamics simulations of Boioli et al. (2015) and Gouriet et al. (2019). Dislocation 310 climb is a non-conservative, diffusion-limited process, and therefore anything that influences diffusion 311 rates (e.g., point-defect concentrations) will influence the overall creep rate. However, for changes in 312 313 the relative velocities of different types of dislocations to occur, changes in the physical and chemical conditions must modify the climb velocities of some dislocations more than others. 314

For water, Karato et al. (2008) proposed that the density of jogs (defects essential to climb that locally 315 316 displace the dislocation line onto a neighboring slip plane) or kinks (defects essential to glide that locally displace the dislocation line within the slip plane) is modified in an anisotropic manner by the 317 318 water content. Whether this effect is directly due to OH⁻ defects or to modifications in the 319 concentrations of other point defects is not clear. Furthermore, whether this same mechanism can be responsible for transitions due to temperature, pressure, and silica activity is unclear. Future research 320 into the role of each physical and chemical parameter in modifying kink and jog densities is needed. 321 322 Another potential solution is that dislocation velocities in dislocation creep are limited by another mechanism entirely. For example, Cooper et al. (2016) suggested that olivine acts like a solid-solution 323 324 alloy, for which mobile dislocation glide velocities are often limited by interactions with solute atoms 325 rather than by dislocation climb. There are a variety of potential mechanisms by which solute atoms can interact with dislocations (for a review, see Chapter 5 in Kassner, 2015), and the macroscopic 326 327 behavior associated with these mechanisms is consistent with the behavior of many minerals. 328 Furthermore, in the context of the development of a CPO, it does appear that solute effects on dislocation velocities can be anisotropic (e.g., Akhtar and Teghtsoonian, 1969). 329

330 3.1.2 Grain rotations not controlled by dislocation motion

Grains in an aggregate may rotate by means other than the motion of lattice defects. The interfaces 331 332 between neighboring grains, the grain boundaries, can be orders of magnitude weaker than the grain interiors (e.g., Jackson and Faul, 2010), allowing grains to translate past one another. This 333 grain-boundary sliding has long been thought to modify grain rotations in deforming rocks (e.g., 334 Boullier and Gueguen, 1975), although the manner in which rotations are affected is still not agreed 335 upon. Confusion arises from the manner in which sliding on boundaries is accommodated at triple 336 junctions and other grain-boundary irregularities. If that accommodation is by the nucleation and 337 motion of lattice dislocations, the rotations association with dislocation motion can outweigh those 338 associated with grain-boundary sliding (Hansen et al., 2014, 2012b, 2011). If that accommodation is 339 340 by diffusion of material away from stress concentrations (i.e., diffusion creep), the controls on grain rotations are less clear (e.g., Sundberg and Cooper, 2008). 341

Diffusion creep is generally considered to randomize grain orientations and destroy seismic
anisotropy (e.g., Behn et al., 2009; Karato and Wu, 1993). However, several studies have
demonstrated through simulation (Wheeler, 09/2009) and experiments (Maruyama and Hiraga, 2017a;
Miyazaki et al., 2013) that CPO can be preserved and even created if diffusion creep is the dominant
deformation mechanism. In the most intuitive models for CPO generated from this mechanism,
rotations controlled by the grain shape and grain shape controlled by crystallography are both
required.

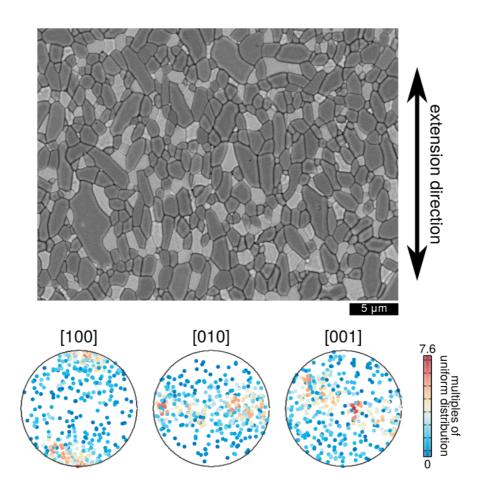
349 3.1.2.1 Influence of grain shape on grain rotations

As grain-boundaries are relatively weak, the role of grain shape in controlling grain rotations can be
evaluated by considering a rigid particle embedded in a viscous medium. The original equations of
motion were derived by Jeffery (Jeffery, 1922) and first applied to rocks in the mid 1960s
(Bhattacharyya, 1966; Gay, 1968, 1966). In this approach, elongate grains rotate freely and their rate
of rotation is controlled by both their aspect ratio and the fluid velocity gradients (Fernandez, 1987;

355 Ildefonse et al., 1992), a system that is perhaps best applied to dispersed crystals suspended in a melt. The physics of grain rotation are complex due to the interactions among neighboring grains. Ildefonse 356 et al. (1992) demonstrated with analog experiments that concentrated suspensions of elongate grains 357 will asymptotically approach steady orientation distributions due to the so-called "tiling effect". In 358 simple shear, the long axes of grains tend to align with the shear direction. In coaxial flow, the long 359 axes tend to align in the planes of maximum extension. The comparison between grain rotations in a 360 concentrated suspension and those in a dense aggregate of grains is not straightforward due to the 361 enhanced mechanical interaction among neighboring grains of the latter. However, recent experiments 362 on olivine aggregates in the diffusion creep regime by Miyazaki et al. (2013) have demonstrated 363 asymptotic alignment among elongated grains in a manner qualitatively consistent with the expected 364 result from concentrated suspensions of particles. This relationship implies that in diffusion creep, a 365 considerable amount of the total strain is taken up by sliding on grain boundaries. 366

Rotations associated with elongated grain shapes will lead to crystallographic alignment if the grain 367 368 shapes are crystallographically controlled. In two-phase aggregates, anisotropy in the interfacial energy leads to crystallographically controlled habit. This effect has been observed in aggregates of 369 forsterite + diopside and forsterite + anorthite (Miyazaki et al., 2013), leading to grains typically 370 elongated along [100]. As illustrated in Figure 4, during deformation, these elongated olivine grains 371 tend to align with their [100] axes normal to the compression direction or parallel to the tension 372 direction, respectively. Similar effects have been observed in aggregates of olivine + melt. Olivine 373 crystals in mafic melts have been observed in natural and laboratory settings to consistently have 374 grain shapes that are shortest in the [010] direction, with crystal dimensions of similar length in the 375 [100] and [001] directions (Donaldson, 1976; Drever and Johnston, 1958; Fleet, 1975; Schwindinger 376 and Anderson, 1989). Qi et. al (2018) recently observed a similar link between olivine grain shapes 377 and crystallography in sheared aggregates of olivine + basalt. They suggested that the shape preferred 378 379 orientation led to strong alignment of [010] with the shear plane and [100] and [001] axes dispersed in

- 380 the shear plane, although this pattern was complicated by additional contributions from
- 381 dislocation-based processes.



382

Figure 4: Example of CPO induced by formation of a shape-preferred orientation in a mixture of
forsterite and diopside (sample KS-14) originally presented by Miyazaki et al. (2013). A
backscattered electron image illustrates the elongate grains of forsterite (dark gray) and diopside (light
gray) that have aligned during vertical extension of the sample. The orientation distribution presents
orientations of forsterite grains, indicating alignment of [100] with the extension direction.
In addition to the first-order role of grain shape in influencing grain rotations, crystallographically

- 389 controlled grain shapes will also be linked to higher frequencies of certain types of grain boundaries.
- 390 Miyazaki et al. (2013) and Maruyama and Hiraga (2017a, 2017b) observed elongate grains in
- 391 forsterite + diopside aggregates and noted an abundance of long and straight interfaces parallel to
- 392 (010). They hypothesized that grain-boundary sliding occurs more easily on these boundaries (i.e.,

393 there is a lower grain-boundary viscosity), which will in turn additionally modify grain rotations and 394 the eventual CPO. Although direct evidence remains to be obtained for variability in the viscosity of 395 olivine grain boundaries, there is indirect evidence of variability in other physical properties of olivine 396 grain boundaries, such as electrical conductivity (Pommier et al., 2018).

Importantly, this link between grain shape, grain-boundary sliding, and CPO can apparently lead to 397 formation of seismic anisotropy in deformation regimes that exhibit very little dislocation activity. 398 The experiments of Miyazaki et al. (2013) record rheological behavior largely consistent with 399 diffusion creep as the primary deformation mechanism. This observation contradicts the conventional 400 wisdom that anisotropic regions of Earth's mantle are deforming by dislocation creep and isotropic 401 regions are deforming by diffusion creep (e.g., Karato and Wu, 1993). Numerical experiments by 402 Wheeler (09/2009) support this new perspective and demonstrate that elongate grain shapes help to 403 stabilize CPOs during deformation by diffusion creep and can even lead to macroscopic anisotropy in 404 viscosity (Wheeler, 2010). 405

406 3.2 Extrinsic anisotropy

Extrinsic anisotropy can result from the spatial arrangement of multiple phases in a rock with different
elastic properties. Thus, in the case of elastic waves with a wavelength much greater than the inherent
length scale of the spatial distribution of phases, anisotropy in the phase distribution can lead to
macroscopic seismic anisotropy, even if the individual phases are not intrinsically anisotropic.
Furthermore, extrinsic anisotropy can also result from specific spatial arrangements of different rock
types, such as layering of lithologies with very different elastic properties, whether or not the
individual rocks types are not intrinsically anisotropic.

414 3.2.1 Calculating extrinsic anisotropy

415 The simplest approach to extrinsic anisotropy is to consider a layered medium in which each layer is 416 isotropic. An early treatment of this problem was given by Backus (1962). If we consider deformation 417 parallel to the layers, then each layer will support a different stress, but each layer will undergo the same strain. If we consider deformation perpendicular to the layers, then each layer will undergo
different strains, but each layer will undergo the same stress. If the characteristic length scale of the
layering is sufficiently small compared to the wavelength of the elastic waves propagating through the
medium, this layering results in a transversely isotropic medium (i.e., hexagonal symmetry) with the
symmetry axis normal to the layering. A medium of this type is often referred to as a smooth,
transversely isotropic, long-wavelength equivalent (Fitchner et al. 2013). Azimuthal anisotropy would
not be detected by horizontally propagating waves if the layering is horizontal. There is, however,

$$\xi = \langle \mu \rangle \left\langle \mu^{-1} \right\rangle, \tag{1}$$

426 where μ is the shear modulus of an isotropic layer, and the angled brackets indicate the volume 427 average over all layers.

Further developments have been presented for cases in which the individual layers are anisotropic. If 428 the individual layers are themselves transversely anisotropic with symmetry axes normal to the 429 layering, then the elastic properties of the effective medium can be calculated using the Love 430 parameters of those layers (e.g., equations 1 and 2 in Fichtner et al. 2013). Nayfeh (1995, equation 431 15.49) presents a solution for calculating the full stiffness tensor of the effective medium if the 432 individual layers have orthotropic anisotropy (i.e., orthorhombic symmetry) with two symmetry axes 433 parallel to the layering and the third normal to the layering. Methods also exist for calculating the full 434 stiffness tensor for the effective medium if the individual layers have arbitrary anisotropy in any 435 orientation (e.g., equation 5 in Schonberg and Muir, 1982). 436

437 Extrinsic anisotropy resulting from features dispersed within a medium rather than discrete layers (
438 i.e., foliated and lineated mineral fabrics or the presence of fluid-filled cracks) is generally calculated
439 with more complex mathematical models such as the self-consistent scheme or the differential
440 effective medium (Faccenda et al., 2019; Kendall, 2000; Mainprice, 1997). These effective-medium
441 methods allow calculation of the elastic tensor of a representative volume element characterized by

the presence of ellipsoidal inclusions of one (or more for the self-consistent scheme) phase(s)dispersed in a matrix with contrasting elastic properties.

444 3.2.2 Mechanisms of producing extrinsic anisotropy

Observations from exhumed peridotite massifs indicate that a range of compositional fabrics exist in 445 the upper mantle and that these fabrics may contribute to seismic anisotropy. Nearly all massifs 446 exhibit compositional variability (e.g., Bodinier et al., 2014; Python and Ceuleneer, 2003; Quick, 447 1981), however systematic layering, characterized by alternating bands of pyroxene-rich and 448 pyroxene-poor peridotite, is less common. Examples of layering include the Josephine (e.g., Loney 449 and Himmelberg, 1976), Horoman (Niida, 1974), Erro-Tobbio (Rampone and Borghini, 2008), and 450 External Liguride (Borghini et al., 2016) peridotite massifs. The segregation of a melt phase into 451 melt-rich bands in regions of high strain rate is another possible source of extrinsic anisotropy in the 452 upper mantle (e.g., Holtzman and Kendall, 2010). In exhumed massifs, observations of foliated 453 plagioclase lherzolites include sections of the Trinity (Quick, 1981), Lanzo (Higgie and Tommasi, 454 2014), Erro-Tobbio (Piccardo and Vissers, 2007), and Othris (Dijkstra et al., 2001) massifs. The 455 elongation of individual grains can also lead to foliated and lineated fabrics that can be a source of 456 457 extrinsic anisotropy, if the contrast in isotropic elastic moduli between mineral phases is large enough (Faccenda et al., 2019). However, while the CPOs of mineral phases are often assessed in detail, the 458 role of compositional layering for extrinsic anisotropy is rarely evaluated. As an example of the 459 seismic anisotropy produced by compositional layering, in Figure 5 we calculate the contrast between 460 harzburgite and dunite, based on fabrics measured in the Josephine Peridotite. 461

Relatively few models describe the formation of mineralogical fabrics in upper mantle rocks.
Infiltration of a melt phase that is out of chemical equilibrium with the host rock can lead to
segregation and channelization of flow, typically through formation of dunitic melt channels in
peridotite (Kelemen et al., 1995). This process has been investigated through field observations (e.g.,
Kelemen et al. 2000), numerical simulations (Spiegelman et al., 2001; Weatherley and Katz, 2012),

and laboratory experiments (Daines and Kohlstedt, 1994; Pec et al., 2017, 2015). Reactive melt
transport during deformation can produce multiple, overprinting, compositional fabrics, as observed
in the Lherz massif (e.g., Le Roux et al., 2008). This interplay has been explored experimentally (D.
S. H. King et al., 2011) and numerically (Keller et al., 2017; Weatherley and Katz, 2012), but has not
been quantitatively tested against outcrop-scale observations. A useful review of geological
observations related to forming compositional heterogeneity is provided by Tommasi and Vauchez
(2015).

In contrast, a variety of models exist describing the segregation of melt into anisotropic structures in 474 partially molten rocks. At the grain scale, a melt phase will locally rearrange along olivine grain 475 boundaries in an anisotropic manner dependent on the interfacial energies (e.g., Waff and Faul, 1992) 476 or the orientation of the maximum principle stress (e.g, Daines and Kohlstedt, 1997). Typical models 477 consider the melt to reside in spherical, ellipsoidal (Faul et al., 1994; Tommasi et al., 2006; Vauchez et 478 al., 2000; Waff and Faul, 1992), or tubular pores (Mavko, 1980). All of these scenarios serve to reduce 479 seismic velocities of mantle rocks. However, if the melt pores are also aligned, they will impart 480 anisotropy in addition to any intrinsic anisotropy produced by the crystalline matrix. An analysis and 481 482 comparison of these different models is provided by Blackman and Kendall (1997). At longer length scales, melt can segregate into melt-rich bands during deformation (e.g., Holtzman et al., 2003; King 483 et al., 2010). The dynamics of melt segregation during deformation were recently reviewed by 484 Kohlstedt and Holtzman (2009) and its effect on seismic anisotropy quantified by Holtzman and 485 Kendall (2010). 486

487 3.2.3 The interplay between intrinsic and extrinsic anisotropy

To explore the interplay between extrinsic and intrinsic anisotropy (Figure 5), we first consider a natural example of mantle layering from the Josephine Peridotite in Southwestern Oregon (Hansen and Warren, 2015; Warren et al., 2008). Some sections of the Josephine Peridotite are composed of alternating, centimetric layers of dunite and harzburgite (Kelemen and Dick, 1995; Loney and

Himmelberg, 1976), each of which is intrinsically anisotropic due to the crystallographic alignment of olivine and orthopyroxene. The shape and orientation of the anisotropy is largely similar between the two layers, although the magnitude is larger in the dunites (Figure 5). The relatively small differences in seismic velocity between the two rock types primarily results from the presence of orthopyroxene in the harzburgites.

We calculated the effective anisotropy of a layered composite assuming equal volumes of dunite and 497 harzburgite and using the method of Schonberg and Muir (1982). From the prediction for the 498 combined effect of intrinsic and extrinsic anisotropy presented in the upper right panel of Figure 5, the 499 anisotropy is clearly dominated by the intrinsic anisotropy of the layers. This result is supported by 500 3-D simulations of wave propagation by Faccenda et al. (2019), which demonstrate that, for a variety 501 of compositional fabrics, the extrinsic anisotropy is only significant if the individual components have 502 large differences in elastic moduli. In perhaps the most extreme case, Tommasi and Vauchez (2015) 503 investigated the anisotropy of layered peridotites and pyroxenites, in which the pyroxenites contained 504 considerable amounts of garnet. Even then, the anisotropy is dominated by the intrinsic anisotropy, 505 and in fact, the overall anisotropy is diminished slightly because of the low anisotropy of the garnet. 506 507 Thus, it seems that compositional layering will only be the primary source of anisotropy in the absence of a CPO or aligned melt. However, the review by Tommasi and Vauchez (2015) also 508 highlights that the formation of compositional layering in nature generally involves deformation 509 (inducing a CPO) and/or the mobilization of a melt phase (leading to aligned melt pockets), and 510 therefore it seems the role of solid-state heterogeneity in observed anisotropy will be negligible. 511

As an alternative example, we consider the anisotropy of the same system modified to include an isotropic distribution of basaltic melt within the dunite layers. The role of a melt phase in moderating seismic velocity and anisotropy depends on the grain scale geometry of the melt distribution. We opted to scale the velocities of the dunites in an isotropic manner to examine the role of an isotropic melt distribution (Blackman and Kendall, 1997). An isotropic reduction in the velocity of the dunites

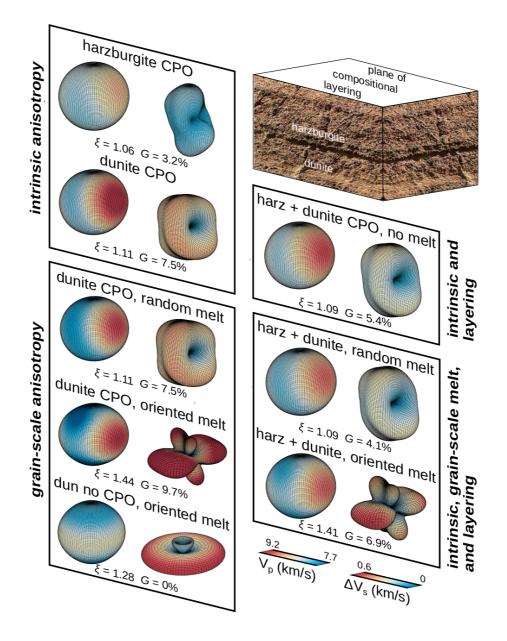


Figure 5: Demonstration of extrinsic seismic anisotropy and its interaction with typical intrinsic anisotropy in naturally deformed peridotites. Photo shows compositional layering in the Josephine Peridotite (vertical dimension is ~0.5 m). Examples of intrinsic anisotropy in a harzburgite and dunite are from Josephine Peridotite samples 3924J07 (IGSN IEJMW000D) and 3924J08 (IGSN IEJMW000E), respectively, originally described by Warren et al. (2008). CPOs from both olivine and orthopyroxene are included in calculations for the harzburgite. Three

dimensional diagrams are given for the directional dependence of P-wave velocities, and the directional dependence of the difference in S-wave velocity between the two S-wave polarizations. The local radius of each diagram is proportional to the magnitude of the velocity (or difference in velocities) for waves propagating parallel to that radius. The upper-left panel presents only the intrinsic anisotropy, and the upper-right panel presents the intrinsic anisotropy combined with the extrinsic anisotropy from layering the harzburgite and dunite. The lower-left panel presents the effect of a melt phase in the dunite for different combinations of grain-scale anisotropy and with horizontal melt pockets. The lower-right panel presents the combination of intrinsic anisotropy from a CPO and extrinsic anisotropy from a melt phase and lithological layering. Three-dimensional projections were generated with the MTEX toolbox for Matlab[®] (Mainprice et al., 2011).

will increase the contribution of extrinsic anisotropy to the overall anisotropy. Figure 5 implements a
melt fraction of 1%, which is considerably larger than most estimates of partially molten regions in
the upper mantle (e.g., Kelemen et al., 1997), even if melt is segregated into melt-rich bands
(Holtzman and Kendall, 2010). However, we present this case as only at these extreme values is the
difference between dunites and harzburgites large enough for extrinsic anisotropy to dominate the
symmetry of the overall anisotropy.

Based on these examples, the importance of extrinsic anisotropy relative to intrinsic anisotropy 524 525 depends strongly on the contrast in isotropic elastic properties of the constituent materials in the composite medium. Holtzman and Kendall (2010) numerically investigated the interplay between 526 527 intrinsic olivine anisotropy and extrinsic anisotropy from the segregation of a basaltic melt into oriented melt pockets and melt-rich bands. They found that the addition of a melt phase significantly 528 529 increases the magnitude of p-wave and s-wave anisotropy and modifies the symmetry and orientation 530 of the s-wave anisotropy. However, the addition of a melt phase does not seem to significantly affect the symmetry and orientation of the p-wave anisotropy or the general orientation of the fast s-wave 531

polarization direction. Similar results were obtained by Vauchez et al. (2000), who investigated the
combined anisotropy from olivine CPO and melt pockets in the context of continental rifts, and by
Tommasi et al. (2006), who investigated the combined anisotropy from olivine CPO, pyroxene CPO,
and melt pockets in a peridotite massif in the Canadian Cordillera.

In general in the upper mantle, a grain- or rock-scale shape preferred orientation does not generate
substantial seismic anisotropy (Faccenda et al., 2019), while the presence of preferentially aligned
fluid-filled cracks or fluid-rich bands controls the anisotropic signal even at very low porosities
(Faccenda et al., 2008; Mainprice, 1997). Therefore, care must be taken if interpreting seismological
signals in terms of the relative contributions of intrinsic and extrinsic anisotropy. In fact, synthetic
tests by Fichtner et al. (2013) revealed that most seismological data cannot definitively distinguish
between intrinsic and extrinsic anisotropy.

543 3.3 Influence of strain on anisotropy

Anisotropy in the mechanical properties of rocks is strongly linked to their deformation history. In the case of intrinsic anisotropy, grain rotations occur in parallel with ductile strain, and therefore the evolution of the distribution of crystallographic orientations depends strongly on the magnitude and geometry of strain. In the case of extrinsic anisotropy, the spatial distribution of phases also depends strongly on the magnitude and geometry of strain. The influence of strain on the development of seismic anisotropy was recently reviewed by Skemer and Hansen (2016), and so we only briefly cover this topic here.

The primary metric used to evaluate the evolution of CPO in olivine-rich rocks has been the average orientation of [100], the seismically fast axis, relative to the shear plane and shear direction during simple shear. Experiments on dry olivine (Bystricky et al., 2000; Hansen et al., 2014; Zhang and Karato, 1995) reveal that the average [100] orientation initially follows the long axis of the finite strain ellipse and then quickly aligns with the shear direction after shear strains of 1 to 2. Experiments on moderately wet olivine (several 100 ppm H/Si) reveal that the average [100] orientation is initially antithetic to the finite strain ellipse, but also eventually rotates into parallelism with the sheardirection (Jung et al., 2006; Katayama et al., 2004).

In addition to the orientation distribution of [100], the [010] and [001] distributions also reveal 559 systematic evolutions until a steady-state texture is reached. For dry olivine aggregates (Bystricky et 560 al., 2000; Hansen et al., 2014; Zhang and Karato, 1995), the average [010] orientation eventually 561 aligns with the shear-plane normal. For moderately wet olivine aggregates (Jung et al., 2006; 562 Katayama et al., 2004), the average [001] orientation eventually aligns with the shear plane normal. 563 These combinations of [100] parallel to the shear direction and either [010] or [001] normal to the 564 shear plane helped support the interpretation that weak slip systems control the final texture, with 565 [100](010) or [100](001) being dominant in either case, respectively. However, Hansen et al. (2014) 566 noted that, during torsion of dry olivine aggregates, the [010] and [001] axis distributions undergo a 567 protracted evolution in which they initially form girdles normal to the shear direction before finally 568 forming distinct clusters. The evolution appears to require shear strains of ~10 before steady-state 569 CPOs are reached. Hansen et al. (2014) interpreted the slow evolution of the girdled fabrics to result 570 from the comparable activity of the (010)[100] and (001)[100] slip systems (e.g., Bai et al., 1991). 571 572 Importantly, the girdled CPOs at moderate strain result in seismic anisotropy that has hexagonal symmetry, with a symmetry axis parallel to the shear direction. Because this hexagonal anisotropy 573 evolves to orthorhombic symmetry at high strain, seismologically detecting transitions in the 574 symmetry of anisotropy may provide a means to, at least qualitatively and in conjunction with the 575 magnitude of anisotropy, map low- strain domains in the upper mantle. 576

These experimental results are in broad agreement with observations in naturally deformed
peridotites. In a few outcrop-scale shear zones in ultramafic massifs, strain markers are present that
allow the CPO to be correlated with the magnitude of strain (Hansen and Warren, 2015; Kumamoto et
al., n.d.; Warren et al., 2008; Webber et al., 2010). The general observation is that the average [100]
orientation reorients much slower (about a factor of 2 in shear strain) in naturally deformed aggregates

than in experimentally deformed aggregates (see Figure 3 in Skemer and Hansen, 2016). Hansen and Warren (2015) additionally looked at the degree of girdling in [010] and [001] distributions and noted that naturally deformed dunites exhibit girdling that evolves on a similar strainscale to those deformed in the laboratory.

In addition to the dependence of anisotropy on the magnitude of strain, significant differences arise in 586 anisotropy as a function of the geometry of strain. Tommasi et al. (1999) generated a wide variety of 587 texture types by numerically simulating olivine CPOs formed in a range of coaxial and non-coaxial 588 flows. Relatively few experimental studies have examined CPO evolution in geometries other than 589 simple shear. Hansen et al. (2011) deformed aggregates in axial compression and observed a 590 transversely isotropic anisotropy with [010] axes parallel to the loading direction and which define the 591 symmetry axis, a result that was expected based on the simulations of Tommasi et al. (1999). Hansen 592 et al. (2016c) also investigated experimentally a complementary deformation geometry, axial 593 extension, which was not investigated numerically by Tommasi et al. (1999). They found distinct 594 small-circle girdles of [100] around the extension direction, which they hypothesized resulted from 595 the near identical strengths of the (010)[100] and (001)[100] slip systems at the conditions of the 596 597 experiments.

The effect of strain geometry on CPO in naturally deformed rocks has been evaluated in a few studies.
Chatzaras et al. (2016) and Bernard et al. (2019) both used the shape-preferred orientation of spinel
grains as a proxy for strain geometry in naturally deformed peridotite xenoliths. These studies
concluded that the olivine CPO correlates with the strain geometry. Kumamoto et al. (2019)found that
CPO evolution in outcrop-scale transects of shear zones in the Josephine Peridotite are best explained
by a combination of simple shear and extension.

⁶⁰⁴ So far, we have considered the evolution of anisotropy from a uniform³ initial texture. However, the

⁶⁰⁵ ³ Many authors erroneously refer to very weak textures as "random". In the context of orientation distributions,

⁶⁰⁶ random simply means that orientations are drawn at random from a particular distribution, but that distribution

⁶⁰⁷ could actually describe a very strong CPO. In contrast, "uniform" refers to a uniform distribution, for which all

⁶⁰⁸ orientations are equally probable (i.e., there is no distinct preferred orientation).

deformation history of mantle rocks can be long and complicated, and therefore, the deformation 609 process of interest is often superimposed on an already textured rock. Several authors have examined 610 the role of initial CPOs on the subsequent evolution of anisotropy. Boneh and Skemer (2014), in 611 particular, conducted triaxial compression experiments on samples of natural olivine with a strong 612 initial texture and systematically varied the orientation of the initial texture relative to the loading 613 axes. Each initial texture orientation resulted in a different evolution of CPO and thus seismic 614 anisotropy. Hansen et al. (2016c) conducted experiments on dry olivine aggregates in which 615 deformation was initially imposed in extension and subsequently imposed in torsion. Hansen et al. 616 (2016a) identified differences in the CPO evolution through comparison of these experiments to 617 618 experiments conducted solely in torsion. The evolutionary paths of anisotropy in experiments on initially uniform samples and samples with strong initial CPOs tend to converge at high strains (>5 619 shear strain for the case of simple shear). Thus, considering the full history of CPO evolution is 620 621 primarily important in regions of the upper mantle that have undergone relatively little recent strain in 622 the current strain geometry.

Unfortunately, very little information is available for the evolution of extrinsic anisotropy with
increasing strain, which will likely depend on the mechanisms leading to compositional layering.
Holtzman and Kendall (2010) demonstrated that the degree of melt segregation in the olivine + melt
system is quantitatively linked to seismic anisotropy. The link between the degree of melt segregation
and the total strain is complex but has been parameterized in an empirical model by King et al.
(Holtzman et al., 12/2012). Further investigation of the evolution of extrinsic anisotropy is a clear
target for future research.

630 4 The longevity of anisotropy

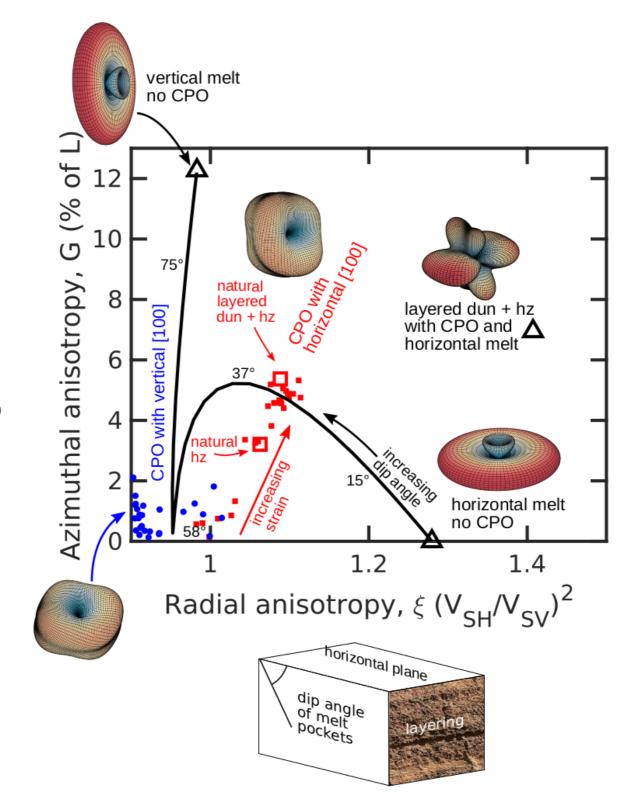
A variety of geodynamic settings involve portions of the upper mantle in which anisotropy is assumed
to be preserved from previous formation and deformation events. These settings include "freezing in"
of upper mantle to create the oceanic lithosphere (Becker et al., 2014; e.g., Beghein et al., 2014;

Hansen et al., 2016b; Russell et al., 2019), construction of continental interiors (e.g., Conrad et al.,
2007; Marone and Romanowicz, 2007; Silver and Chan, 1988; Yuan and Romanowicz, 2010), and
rifting of continental margins (e.g., Tommasi and Vauchez, 2001).

These interpretations rely on a lack of modification of the anisotropy once the anisotropy-forming 637 process has ceased. However, Boneh et al. (2017) demonstrated that grain growth during annealing of 638 pre-deformed olivine aggregates will modify existing CPOs, weakening and rotating the intrinsic 639 anisotropy. Similar observations have been made for other mineral systems, including quartz (e.g., 640 Heilbronner and Tullis, 2002), calcite (Ghosh et al., 2017), and ice (e.g., Montagnat et al., 2015). 641 Unfortunately, the timescales of this modification are not yet well quantified. Relaxation of extrinsic 642 anisotropy associated with mineralogical layering likely requires subsequent deformation to induce 643 phase mixing, the mechanisms and timescales of which are still the subject of active debate (Bercovici 644 and Skemer, 2017; Cross and Skemer, 2017; Tasaka et al., 2017). Relaxation of extrinsic anisotropy 645 associated with the segregation of a melt phase into melt-rich bands has been better quantified, with 646 heterogeneity on the scale of 1 m relaxing over ~1 Ma and heterogeneity on the scale of 10 m relaxing 647 over ~300 Ma (Daniel S. H. King et al., 2011). Subsequent loading in an orientation different to the 648 649 original loading direction, however, may reorganize the melt significantly faster than static annealing (Pendleton et al., 2012). 650

651 4.1 Summary of systematics in anisotropy

The above discussion illustrates that seismic anisotropy of the upper mantle is influenced by a
wide-range of intrinsic and extrinsic variables. In Figure 6, we attempt to summarize systematic
variations in anisotropy as a function of these variables. We consider two specific aspects of
anisotropy, radial and azimuthal, in a typical geographic reference frame (i.e., with the third direction
parallel to Earth's radius). For shearing parallel to Earth's surface in dry, melt-free olivine (red
squares), horizontal alignment of [100] is expected. Experimental samples reveal that azimuthal and
radial anisotropy increase with increasing strain until values of approximately 5% and 1.1 are reached,



660 Figure 6: Systematics of azimuthal and radial anisotropy for olivine aggregates with CPO,

661 compositional layering, and/or oriented melt pockets. Only a simple set of situations are presented:

662 red data represent anisotropy with horizontal [100] maxima, blue data represent anisotropy with

vertical [100] maxima, and black data represent anisotropy of rocks including a melt phase. Solid data points are from the compilation of experimentally deformed samples in Hansen et al. (2014) assuming a mixture of 60% olivine and 40% pyroxene. Open data points are based on data from naturally deformed peridotites presented in Figure 5. Projections in 3-D represent examples of the directional dependence of ΔV_s for each scenario, as depicted in Figure 5. The block diagram presents the reference frame for layering and dipping melt pockets.

respectively. Natural samples (open red squares) fall on the same trend, even for the example of
horizontal layering of different mineral assemblages. For shear parallel to Earth's radius in dry,
melt-free olivine, [100] should be vertically aligned. In contrast to horizontal alignment of [100],
vertical alignment results in low magnitudes of azimuthal anisotropy, even if large strains have been
accumulated. In addition, the magnitudes of radial anisotropy are less than unity.

The inclusion of melt pockets leads to additional complexity. The black curve indicates the range of 668 anisotropies attainable depending on the orientation of the melt pockets and no mineral CPO. 669 Horizontal melt pockets result in high radial anisotropy and no azimuthal anisotropy. Vertical melt 670 pockets result in high azimuthal anisotropy and values of radial anisotropy just less than unity. The 671 small amount of radial anisotropy results from the fact that polarized S-waves will interact with the 672 melt pockets differently depending on propagation direction, regardless of the polarization direction. 673 That is, S-waves propagating normal to the pockets induce shear parallel to the pockets, for all 674 polarization directions, and S-waves propagating parallel to the pockets induce shear normal to the 675 pockets, for all polarization directions. Interestingly, melt-pocket orientations near 58° also result in 676 very low azimuthal anisotropy because shearing is consistently oblique to the pockets, regardless of 677 the propagation direction. 678

Clearly, the melt-pocket orientation, CPO, and mineral layering can all simultaneously contribute to
the anisotropy, resulting in a large parameter space to explore. For simplicity, we investigate a single
case involving all three contributions, in which melt pockets are horizontal, mineral layering is

32

horizontal, and [100] axes are horizontal. This case produces high values of both azimuthal radialanisotropy and does not fall on any of the trends previously explored.

The models in Figure 6 suggest that a combination of azimuthal and radial anisotropy constraints can be used to rule out certain mechanisms as contributing to upper mantle seismic anisotropy . Values of radial anisotropy less than unity likely cannot be explained by horizontal shearing. Radial anisotropy </br/>686radial anisotropy less than unity likely cannot be explained by horizontal shearing. Radial anisotropy687<1 combined with high azimuthal anisotropy likely cannot be explained by CPO or layering in</td>688melt-free rocks. Exceedingly high values of radial anisotropy (>1.1) also cannot easily be explained689by CPO or layering in melt-free rocks. Very high values of both azimuthal and radial anisotropy, if690observed, would likely require a combination of CPO, mineral layering, and melt.

5 5 Forward modeling the development of anisotropy

692 5.1 General approach to forward modeling

As described above, the development of anisotropy not only depends on the mechanistic details of the 693 particular process producing anisotropy, but also on the history and geometry of deformation. 694 695 Therefore, the most popular methods of forward modelling anisotropy rely on models that track and 696 allow interaction between the microphysical mechanisms associated with anisotropy and the larger scale kinematics. A variety of models have been developed for predicting intrinsic anisotropy, and we 697 698 briefly review these here. Unfortunately, very little development has occurred in the context of 699 simulating the development of extrinsic anisotropy and this remains a key topic for future research efforts. 700

Figure 201 Equations 3 and 4 above illustrate that the glide of lattice dislocations generates strain and rotation of
individual grains. To predict the elastic properties of an aggregate of grains, the rotations of a
population of grains must be tracked. Although tracking the rotation of a single crystal with known
boundary conditions is relatively straightforward, the interactions among neighboring, anisotropic
crystals in an aggregate lead to significant difficulties in tracking rotations within a population of

706 grains. For a recent review of models simulating the deformation of aggregates, see Pokharel et al.707 (2014).

Some of the most rigorous simulations include an explicitly defined microstructure (i.e., an array of
grains and grain boundaries) and track the full stress and displacement fields (e.g., Lebensohn, 2001).
Full-field simulations constrain the calculation to ensure that stress equilibrium and strain
compatibility are maintained throughout the model volume. That is, cavities cannot open and
neighboring grains cannot become interpenetrating. Although rigorous and essential for examining
heterogeneities in the stress and strain fields below the grain scale, these methods are computationally
expensive and are not generally used to evaluate deformations larger than a few percent strain.

715 To reduce the computational complexity, mean-field models ignore heterogeneity within grains and employ one of a variety of homogenization schemes to address interactions between grains in an 716 average sense. The simplest homogenization schemes assume that either the stress or the strain rate is 717 718 the same in every grain, referred to as the Sachs model (Sachs, 1928) or the Taylor (or 719 Taylor-Bishop-Hill) model (Bishop and Hill, 1951; Taylor, 1938). In the former, stress is 720 homogeneous, but grains have no strain compatibility requirement (i.e., cavities can open or grains can intersect one another). In the latter, strain is homogeneous, but stress equilibrium is not 721 maintained (i.e., the stress can be different between two neighboring material points). Because these 722 723 end-member models allow the deformation (and therefore rotation) to be directly calculated for each grain, they are computationally efficient, if not perfect representations of the microphysics. Some 724 more sophisticated approaches are discussed in the next section. 725

For geological materials, the Taylor model can be difficult to adapt since many minerals have too few
slip systems to accommodate an arbitrary strain tensor. According to the von Mises criterion (Mises,
1928), five linearly independent slip systems are required to produce any arbitrary deformation since
symmetry and volume conservation reduce the strain tensor to five independent components. Olivine,
for example, has only four dominant slip systems at high temperature (see the compilation in

Tommasi et al., 2000). These slip systems can be further reduced to three, as [100](001) and
[001](100) produce the same Schmid tensor and are therefore linearly dependent. However, Tielke et
al. (2016) observed mechanical differences between these slip systems in experiments on olivine
single crystals, suggesting that they may be independent.

735 5.2 Models of geologic materials

736 One of the major models for simulating CPO evolution in olivine and pyroxene was developed by 737 Kaminski and Ribe (2001) and Kaminski et al. (2004) and is commonly referred to as D-Rex. This 738 model is largely based on the Taylor model and finds the closest possible strain rate tensor for each grain given its orientation and available slip systems. Any mismatch between the best-fitting strain 739 rate and the imposed, macroscopic strain rate necessarily means that strain incompatibilities arise in 740 741 the microstructure. However, Kaminski and Ribe (2001) suggested that this approach is applicable to real aggregates if any incompatibilities are assumed to be relieved by the activation of 742 743 non-dislocation-based mechanisms (e.g., grain-boundary sliding), which are assumed to not affect the 744 grain rotations. Kaminski and Ribe (2001) also included a mechanism for dynamic recrystallization to affect the CPO evolution. Grains subject to higher stresses are presumed to have higher dislocation 745 densities and therefore higher strain energies, resulting in these grains being gradually consumed by 746 747 grains with low strain energy according to a tuneable rate parameter.

Viscoplastic-self-consistent modelling (VPSC) offers an alternate approach to modeling CPO 748 evolution by taking a mean-field approach that attempts to account for grain interactions without 749 imposing the Sachs or Taylor end members (Lebensohn and Tomé, 1993; Molinari et al., 1987). In 750 these models, each grain is assumed to act as an inclusion in a homogeneous effective medium, 751 equivalent to the elastic inclusion problem (Eshelby, 1957). The properties of the effective medium 752 are characterized by the mechanical properties of the aggregate, but this approach inherently requires 753 the effective medium to have a linear relationship between stress and strain rate (i.e., Newtonian). 754 However, because plastically deforming crystals tend to have non-Newtonian rheological behavior, a 755

linearization scheme must be imposed. The primary difference among the various implementations of
the VPSC model is the method for linearization, several of which are reviewed in application to
olivine by Castelnau et al. (2008). The second-order method (Ponte Castañeda, 2002) is perhaps the
most accurate linearization scheme available, as it closely approximates the mechanical response
determined by full-field methods by enforcing both strain strain and stress compatibility at the grain
scale, although increased accuracy comes at the cost of decreased computational efficiency.

The VPSC method requires that enough slip systems are available to fulfill the von Mises criterion,
similar to the Taylor model. For VPSC models of olivine, additional fictitious slip systems are
generally implemented for this purpose. The relative strengths of these fictitious slip systems are set
to high values, which prevents significant contribution to grain rotations and CPO evolution.
However, depending on the linearization scheme, the strength of the fictitious slip systems
dramatically affects the predicted mechanical properties, with the second order method again being
the best approximation of full-field models (Castelnau et al., 2008).

Although VPSC is computationally more efficient than full-field models, incorporation into larger scale simulations is still cumbersome. In a major advancement, Goulding et al. (2015) developed ANPAR, an analytical approach to VPSC. This approach parameterizes an analytical function for the spin of a grain of any orientation, which is then calibrated using the second-order linearization of VPSC. This method can reproduce the results of second-order VPSC for a wide variety of deformation geometries, with an increase in computational speed of 10⁴.

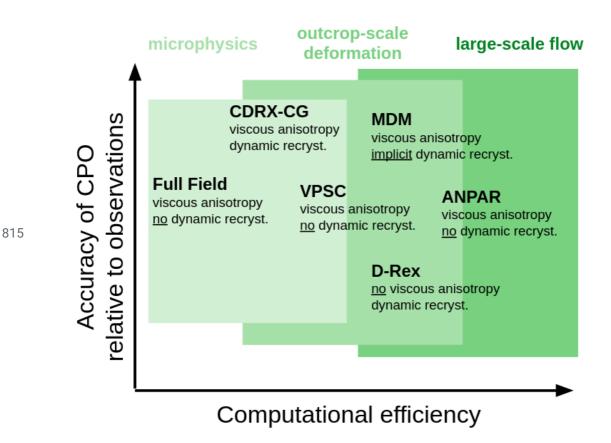
A key limitation of the models described above is their poor applicability to high degrees of
deformation. Full-field simulations are too computationally inefficient to model CPO evolution to
strains larger than a few tens of percent. D-Rex and VPSC reasonably reproduce the average CPO
orientation and symmetry observed in experiments and naturally deformed rocks up to shear strains of
~6, but they tend to overestimate the texture strength, and therefore the strength of the anisotropy,
after strains of ~1 (Hansen et al., 2016a; Warren et al., 2008). Although a more complete investigation

of the full range of model parameters could in the future yield a better prediction of the mantle fabrics
and associated anisotropy using D-Rex and VPSC, two recent studies have sought to overcome these
limitations in strain in an alternative way.

In the first model, Signorelli and Tommasi (2015) developed a version of VPSC that includes effects 784 related to subgrain rotation recrystallization (CDRX-CG). By tracking individual subgrain 785 orientations and the distribution of stored strain energy among all grains and subgrains, the 786 formulation allows subgrains to become new grains according to a set of criteria based on the total 787 strain and the strain energy of the parent grain. Grain interactions are simulated according to typical 788 789 methods for VPSC simulation, whereas subgrain interactions are assumed to follow the Sachs model, implying that subgrains are not subject to the same strain compatibility requirements as the rest of the 790 aggregate. Subgrains of slightly different orientation to their parent grain are considered new grains 791 and contribute to the CPO once a threshold misorientation is reached. These new grains introduce a 792 randomization effect that prevents texture strengths from reaching the extreme values typical of VPSC 793 simulation at high strain, and comparison between model and experimental observations appears 794 reasonable up to shear strains of at least 20. 795

796 The second model designed for application to high strains was proposed by Hansen et al. (2016a) and is referred to here as the modified director method (MDM). This approach is more phenomenological 797 in nature than other models, as grain rotations are decoupled from the mechanical response of the 798 aggregate. Grain rotations are controlled by equation 4 and the available slip systems, but the rotation 799 rate is calculated based on the crystallographic orientation relative to the flow kinematics, scaled by a 800 tuning parameter that is unique to each slip system. Scaling rotation rate by the orientation of a vector 801 in a flow is similar to the director method used to predict viscous anisotropy in geodynamic 802 simulations (Lev and Hager, 2008a, 2008b; e.g., Moresi et al., 2003). This formulation results in the 803 need for only one model parameter per slip system to track the CPO evolution. The mechanical 804 805 response is dealt with separately using a modified Taylor model, and again, one tuning parameter per

slip system. The benefit of this approach is the dramatic gain in computational efficiency, especially 806 because individual grains are tracked separately, which allows easy parallelization on a multicore 807 computer. Because of this gain in efficiency and the relatively small number of model parameters, 808 Hansen et al. (2016a) were able to devise an optimization routine to find the best-fit model parameters 809 that reproduce a large dataset of experimentally derived CPOs and the associated mechanical response 810 from experiments conducted in a variety of loading geometries and to large strains. Simulations with 811 this model reasonably reproduce the CPO orientations and texture strengths observed in experiments 812 and natural samples to shear strains greater than 20 as well as in a variety of more complicated 813 814 loading paths.



816 Figure 7: Schematic comparison of available models in terms of accuracy and computational

- 817 efficiency. Here, accuracy refers to the ability of a model to reproduce observations in laboratory
- 818 experiments and natural samples. Three fields are denoted that roughly indicate the context for which
- 819 each model is best suited. All acronyms are defined in the main text.

The qualitative characteristics of the models described above are compiled in Figure 7 to help the 820 reader distinguish which method is best suited for their purposes. In general, there is a clear tradeoff 821 between the level of physical detail captured in the model and the computational efficiency. More 822 detailed, physically-based models are limited to only predicting outcomes based on the physics 823 included in the model, and are therefore probably best for testing hypotheses about microphysical 824 processes through comparison to observations of individual textures formed under known (or 825 estimated) conditions. More phenomenological models, which may be tuned to fit observed textures 826 in naturally and/or experimentally deformed rocks, are better suited to large-(time or spatial) scale 827 simulations because (1) they tend to exhibit increased computational efficiency and (2) their 828 829 calibration inherently captures the effects of all the relevant microphysical phenomena. This last benefit must be treated with care, however, since calibration in this manner does not necessarily 830 capture the proper scaling relationships for the underlying mechanisms to allow robust extrapolation 831 832 across time and spatial scales.

833 6 Predictions of the distribution of anisotropy

Here we summarize predictions of seismic anisotropy in the upper mantle based on current knowledge 834 835 of the underlying physical processes and on existing tools for forward modelling the development of anisotropy. Figure 8 presents calculations of azimuthal and radial anisotropy from intrinsic and 836 extrinsic sources for the oceanic upper mantle. Calculations of intrinsic anisotropy were made with 837 VPSC (Tommasi, 1998), D-Rex (Hedjazian et al., 2017), and MDM (Hansen et al., 2016b). In all 838 cases, a flow field was calculated along with the strain-dependent development of CPO. The VPSC 839 calculation assumes that a single deformation mechanism operates. The D-Rex calculation includes a 840 competition between dislocation creep and diffusion creep. The MDM calibration assumes that a CPO 841 associated with the presence of a melt is generated in the partially molten region beneath a spreading 842 center and that a CPO associated with dislocation-based processes is generated elsewhere. 843

844 All models predict low anisotropy at the topmost and bottommost portions of upper mantle, with a

several-hundred-km thick region of higher anisotropy at intermediate depths. However, all models 845 also predict that the region of high anisotropy is thinner for radial anisotropy than for azimuthal 846 anisotropy. Both Hansen et al. (2016b) and Hedjazian et al. (2017) noted that the depth profile of 847 radial anisotropy in these calculations is relatively age independent, in agreement with geophysical 848 observations (Beghein et al., 2014; Burgos et al., 2014). Hansen et al. (2016b) suggested that this age 849 independence results from the radial anisotropy being set primarily in the partially molten region 850 beneath mid-ocean ridges. Hedjazian et al. (2017) suggested that it results from a transition from 851 852 dislocation to diffusion creep with increasing depth. Geophysical observations suggest that depth profiles of azimuthal anisotropy do exhibit an age dependence (Beghein et al., 2014; Burgos et al., 853 854 2014; Schaeffer et al., 2016), which is predicted by the model of Hansen et al. (2016b), as well as the 855 VPSC model of Tommasi (1998). In contrast, the transition in deformation mechanisms in the model of Hedjazian et al. (2017) results in age-independent azimuthal anisotropy. 856

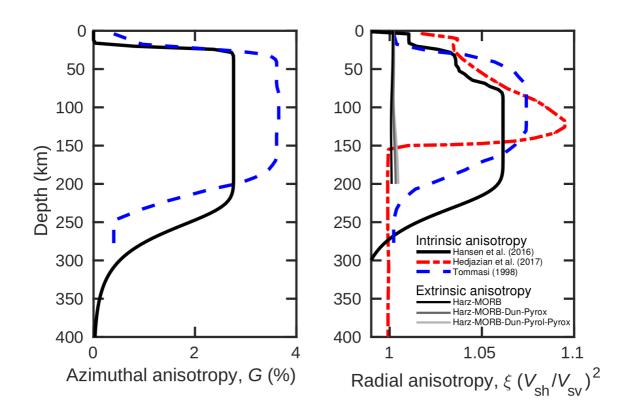


Figure 8: Synthetic profiles of anisotropy predicted for the upper mantle. Both azimuthal and radial anisotropy are presented as a function of depth. Models of intrinsic anisotropy are taken

from previously published work. Models for extrinsic anisotropy are derived in the present work and described in detail in the main text.

We also explore predictions of anisotropy from extrinsic mechanisms. In this calculation, the 857 distribution of mafic and ultramafic lithologies in ophiolites, orogenic massifs, and seafloor samples 858 provides the basis for our compositional model of oceanic lithosphere. The Oman Ophiolite, an ~20 859 km thick sequence of oceanic lithosphere, provides constraints on lithospheric structure at relatively 860 fast spreading rates (e.g., Nicolas and Boudier, 2000). The exposed sequence consists of extrusive 861 lavas (0.5-2 km), sheeted dikes (1-1.5 km), gabbros (0.5-6 km) and up to 12 km of the uppermost 862 lithospheric mantle (e.g., Bodinier et al., 2014; Lippard, 1986). The mantle section consists 863 predominantly of harzburgite, with more fertile facies (i.e., more clinopyroxene rich peridotite) near 864 865 the based of the mantle section (e.g., Godard et al., 2000; Takazawa et al., 2003). Dunites occur as ~5–15% of the mantle section (Boudier and Coleman, 1981; e.g., Lippard, 1986), where they are 866 interpreted as the channels by which melt is transported out of the mantle (Kelemen et al., 1995). 867 Observations at slower spreading rates indicate that some melt is trapped in the upper mantle, 868 resulting in thinner crust overlying a zone of crust-mantle mixture (e.g., Cannat, 1996; Dick et al., 869 2003; Sleep and Warren, 2014). Hence, our generic model for the upper oceanic lithosphere is a 870 mixture of 45% harzburgite, 10% dunite, and 45% MORB over a 20 km depth. 871

Various models (Hofmann, 1988; Ringwood, 1975; Salters and Stracke, 2004; Workman and Hart,
2005) are available for the composition of the upper mantle below the plate. Here, we use pyrolite, an
approximate composition for the upper mantle first developed by Ringwood (1975). Our model
includes 5% pyroxenite, which is garnet bearing below 60 km, as suggested by field observations of
peridotites (Bodinier et al., 2014) and the geochemistry of mid-ocean ridge basalts (Hirschmann and
Stolper, 1996).

Based on this view of upper-mantle composition, we present three separate calculations for extrinsicanisotropy in the right panel of Figure 8. In the first case, as an end member, we assume that the upper

100 km of the upper mantle is interlayered harzburgite and basalt in equal proportions. In the second 880 case, we assume the same thickness also contains layers of dunite and pyroxenite in the proportions 881 45:20:15:10 for harzburgite, dunite, basalt, and pyroxenite, respectively. In the third case, which we 882 consider to be the most realistic, the uppermost 20 km is assumed to be layers of harzburgite, basalt, 883 and dunite in the proportions 45:45:10, and the remaining 80 km is assumed to be layers of pyrolite 884 and pyroxenite in the proportions 95:5, respectively. In all cases, we assume that compositional 885 layering is normal to Earth's radius, and therefore the azimuthal anisotropy is zero. This orientation of 886 layering should also produce the most extreme radial anisotropy (Figure 6). Of the three cases, the 887 third results in the most radial anisotropy, but overall, the degree of anisotropy is substantially smaller 888 889 than for predictions of intrinsic anisotropy, consistent with the predictions of Faccenda et al. (2019). 890 Therefore, most anisotropy in the upper mantle is likely the result of intrinsic mechanisms.

891 7 Summary and outlook

We have presented a summary of the current state of knowledge concerning the generation of
anisotropy in Earth's upper mantle based on laboratory experiments, field observations, and models.
We describe the mechanisms associated with forming anisotropy, which may be derived from intrinsic
or extrinsic sources, and routes to forward modelling the generation of anisotropy.

Our discussion highlights several key outstanding issues. The development of intrinsic anisotropy is 896 well studied in experimental and natural samples, but further effort is needed to understand the 897 microphysics that links changes in slip-system activity to physical and chemical conditions. The role 898 of dislocation kink and jog densities in moderating dislocation velocity are of particular interest, 899 especially in their relationship to the role of water in crystal plastic deformation. Furthermore, the role 900 of pyroxene in decreasing the seismic anisotropy of upper mantle aggregates and changing the 901 deformation mechanism as strain and phase mixing increases (e.g., Tasaka et al., 2017) needs to be 902 better understood. Forward models of the development of intrinsic anisotropy are prevalent, but the 903 904 most popular models do poorly at high strains and are computationally intensive. Newer generations

905 of models are primed to allow major improvements in forward modelling anisotropy by increasing906 both accuracy and efficiency at the expense of capturing the physics of the implicit processes.

907 The development of extrinsic anisotropy is less well studied and more observations are needed of the 908 evolution of extrinsic anisotropy, as well as physical models that can be used to forward model this 909 evolution. However, although less well investigated, recent evaluations of the relative contributions of 910 different types of anisotropy suggest that extrinsic anisotropy plays a minor role throughout most of 911 the upper mantle, unless preferentially-oriented fluid-filled cracks are present. This conclusion is 912 supported by our comparison of forward models for predicting uppermost mantle anisotropy, which 913 demonstrate that fitting geophysical observations of anisotropy requires a significant contribution 914 from intrinsic anisotropy with extrinsic anisotropy playing a minor role.

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Declaration of interests

^I The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

□The authors declare the following financial interests/personal relationships which may be considered as potential competing interests: