

# Influence of Intrinsic Thermal Stability on Switching Rate and Tunability of Dual-Biased Magnetic Tunnel Junctions for Probabilistic Bits

Brandon R. Zink<sup>1</sup> and Jian-Ping Wang<sup>2\*</sup>

*Department of Electrical and Computer Engineering, University of Minnesota, Minneapolis, MN 55455, USA*

*\* Fellow, IEEE*

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**Abstract**—Recently, magnetic tunnel junctions (MTJs) with superparamagnetic free layers (sMTJs) have been proposed as key components in probabilistic bits (p-bits). However, the average fluctuation rates of sMTJs are very sensitive to slight variations in the device dimensions, which creates a major obstacle to their realization in large-scale networks. One possible solution is to implement dual-biasing on p-bits to offset the effects of variations through onboard corrections. In our previous work, we demonstrated that dual-biasing has the unique capability of separate control over the high- and low-state dwell times, which adds an extra degree of tunability in the signals generated. However, these studies investigated dual-biasing on thermally stable MTJs; therefore, the maximum switching rates were lower than the gigahertz rates desired for sMTJ-based p-bit circuits. While dual-biasing on sMTJs rather than thermally stable MTJs would improve the switching rates, some of the flexibility and robustness of dual-biasing may be sacrificed due to the sensitivity of sMTJs. In this letter, we applied the dual-biasing method on 10 MTJs with varying thermal stability factors to test if sMTJs can achieve the same degree of separation between high- and low-state dwell-time tunability as thermally stable MTJs. Our results show that two degrees of tunability was achieved on all MTJs tested, thus demonstrating that dual-biased p-bits can achieve switching rates equal to or greater than single-biased sMTJs.

**Index Terms**—Spin electronics, magnetic tunnel junctions, spin torque, thermal stability, tunneling magnetoresistance.

## I. INTRODUCTION

Spintronic devices provide many unique functionalities to achieve novel computing architectures and schemes [Wang 2017]. Probabilistic spin logic (PSL) has emerged in recent years as a promising solution for various low-energy cognitive computing tasks [Camsari 2018, Faria 2018, Sutton 2017, Zand 2018]. The elementary computing units of PSL circuits are thermally unstable, stochastic devices called probabilistic bits (**p-bits**). Many p-bit designs propose magnetic tunnel junctions (**MTJs**) with a superparamagnetic free layer (**sMTJ**) as key components [Borders 2019, Faria 2017]. For sMTJs, thermal fluctuations alone can drive magnetization switching between the antiparallel (**AP**) and parallel (**P**) states due to their low intrinsic thermal stability factor ( $\Delta_0$ ). The output of a p-bit is defined by the averaged resistance of the MTJ, which can be controlled with an applied voltage or current [Ostwal 2019, Parks 2020].

A promising strategy for designing sMTJs is to use circular MTJs with in-plane anisotropy [Debashis 2018]. According to the Néel–Brown model, thermal fluctuations could drive MTJs with  $\Delta_0 \approx 0$  to switching rates of 1–10 GHz [Lopez-Diaz 2002]. However, the switching rate and transfer curves of sMTJs are extremely sensitive to variations in device dimensions, which creates a major obstacle for their implementation in large-scale p-bit networks [Abeed 2019].

One possible solution to avoid the effects of device variations is an external biasing scheme, which we refer to as “dual-biasing.” This

method generates stochastic switching signals from MTJs using an external magnetic field ( $H_{\text{bias}}$ ) and a dc voltage ( $V_{\text{bias}}$ ) with specific restrictions on their magnitudes and orientations. In our previous work, we showed that average dwell times could be tuned over four orders of magnitude with dual-biasing [Zink 2018, Zink 2019]. We also carried out a hardware feasibility demonstration of p-bits using a dual-biasing scheme [Lv 2019]. The most unique capability of dual-biasing is that the average AP- and P-state dwell times could be tuned separately with  $H_{\text{bias}}$  and  $V_{\text{bias}}$ , respectively. This two-degrees-of-tunability feature means that the average output and switching rate of these signals can be controlled separately, making dual-biasing a potential solution of avoiding the effects of variations in device sizes through onboard corrections.

Our previous work on dual-biasing only examined signals generated from thermally MTJs (where  $\Delta_0 \geq 25$ ). These studies demonstrated that dual-biasing is compatible with the existing state-of-the-art magnetoresistive random access memory technology; however, the maximum switching rates achieved were lower than the ideal gigahertz switching rates desired for p-bits. Therefore, for dual-biasing to be a realistic prospect in p-bit circuits, MTJs with lower  $\Delta_0$  will be required; however, one potential concern is that dual-biasing will not achieve the same degree of tunability on thermally unstable MTJs, due to their sensitivity to noise and defects. In this letter, we apply the dual-biasing method on 10 MTJs with  $\Delta_0$  varying from 10.5 to 35.6. For each device, we analyze the switching speed, average output, as well as the degree of separation between AP- and P-state dwell-time tunability. In our analysis, we investigate all the tradeoffs of dual-biasing on sMTJs to determine if two degrees of tunability is still achieved.

Corresponding authors: Jian-Ping Wang and Brandon R. Zink (e-mail: jpwang@umn.edu; zinkx030@umn.edu).  
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Table 1. Intrinsic Properties and Category of all MTJs Tested

| Category                               | MTJ no.  | $\Delta_0$  | $R_P$ ( $\Omega$ ) | $H_C$ (Oe) | Nominal dimensions (nm <sup>2</sup> ) |
|--|----------|-------------|--------------------|------------|---------------------------------------|
| <b>Super-paramagnetic MTJs (sMTJs)</b> | <b>1</b> | <b>10.5</b> | <b>1360</b>        | <b>NA</b>  | <b>120 x 40</b>                       |
|  | <b>2</b> | <b>11.4</b> | <b>1330</b>        | <b>NA</b>  | <b>120 x 40</b>                       |
|  | <b>3</b> | <b>12.0</b> | <b>1100</b>        | <b>NA</b>  | <b>120 x 50</b>                       |
| Thermally unstable MTJs                | 4        | 19.0        | 1290               | NA         | 130 x 45                              |
|  | 5        | 18.8        | 1015               | NA         | 120 x 50                              |
| <b>Semi-stable MTJs</b>                | <b>6</b> | <b>24.9</b> | <b>1260</b>        | <b>11</b>  | <b>130 x 45</b>                       |
|  | <b>7</b> | <b>26.4</b> | <b>1090</b>        | <b>11</b>  | <b>120 x 50</b>                       |
|  | <b>8</b> | <b>28.2</b> | <b>1250</b>        | <b>21</b>  | <b>120 x 45</b>                       |
| Thermally stable MTJs                  | 9        | 34.2        | 570                | 15         | 130 x 60                              |
|  | 10       | 35.6        | 620                | 20         | 130 x 60                              |

## II. EXPERIMENT

The MTJs tested are elliptical nanopillars with in-plane anisotropy and a stack structure of PtMn(15)/SAF/MgO(0.8)/Co<sub>60</sub>Fe<sub>20</sub>B<sub>20</sub>(2.0), where layer thicknesses are in nanometers. SAF is the synthetic antiferromagnetic fixed layer, which consists of Co<sub>70</sub>Fe<sub>30</sub>(2.5)/Ru(0.85)/Co<sub>40</sub>Fe<sub>40</sub>B<sub>20</sub>(2.4). Each MTJ has a resistance–area product of 3.5  $\Omega\cdot\mu\text{m}^2$  and a tunneling magneto-resistance (TMR) ratio between 135% and 150%.

Table 1 lists the intrinsic thermal stability factors ( $\Delta_0$ ), P-state resistances ( $R_P$ ), coercivities ( $H_C$ ), and nominal dimensions for all 10 MTJs. For each device,  $R_P$  was obtained from its resistance versus field ( $R$ – $H$ ) plots, examples of which are shown in Fig. 1(a) and (b). Additionally, for MTJs with well-defined switching fields,  $R$ – $H$  plots can be used to measure  $H_C$  as well as the stray field of the MTJ ( $H_{\text{stray}}$ ), as illustrated in Fig. 1(a). Some MTJs fluctuated randomly between AP and P-states at fields near  $H_{\text{stray}}$ , as seen in Fig. 1(b); therefore, there is no  $H_C$  for these devices.

The nominal dimensions are presented as long-axis diameter  $\times$  short-axis diameter. One approach to ensuring wide variability in  $\Delta_0$  among the MTJs tested is to vary the aspect ratio (long-axis to short axis dimension) among the devices during fabrication. However, Table 1 shows that  $R_P$  and  $H_C$  often varied significantly between MTJs with the same nominal dimensions. This indicates that the actual device dimensions deviated from their nominal ones. For this reason, we ensured variability in  $\Delta_0$  among the MTJs based on  $R_P$  and  $H_C$  measurements rather than nominal dimensions.

Switching probability ( $P_{\text{SW}}$ ) measurements were used to calculate  $\Delta_0$ . Synchronized  $P_{\text{SW}}$  measurements were used on MTJs, whose  $R$ – $H$  curves showed clear hysteresis (MTJs 6–10). For these MTJs, we obtained multiple  $P_{\text{SW}}$  distribution curves at  $H_{\text{bias}} = H_{\text{stray}}$  and pulsewidths  $\geq 500$  ns, then calculate  $\Delta_0$  from the thermal activation model as was done by Heindl [2011]. The  $R$ – $H$  curves for MTJs 1–5 showed that these devices randomly fluctuated between the AP and P-states at  $H_{\text{bias}}$  near the switching fields. Therefore,  $\Delta_0$  was calculated using asynchronous time-domain data from the random telegraphic signals generated by these devices as was done by Piotrowski [2016]. Fig. 1(b) illustrates that  $R$ – $H$  data can only provide an approximation of  $H_{\text{stray}}$  for these devices; therefore, these measurements were collected at multiple sets with slightly varying  $H_{\text{bias}}$ ; all were  $\approx H_{\text{stray}}$ .

In our analysis, we divided these 10 MTJs into four categories, which were 1) sMTJs, 2) unstable MTJs, 3) semistable MTJs, and 4) stable

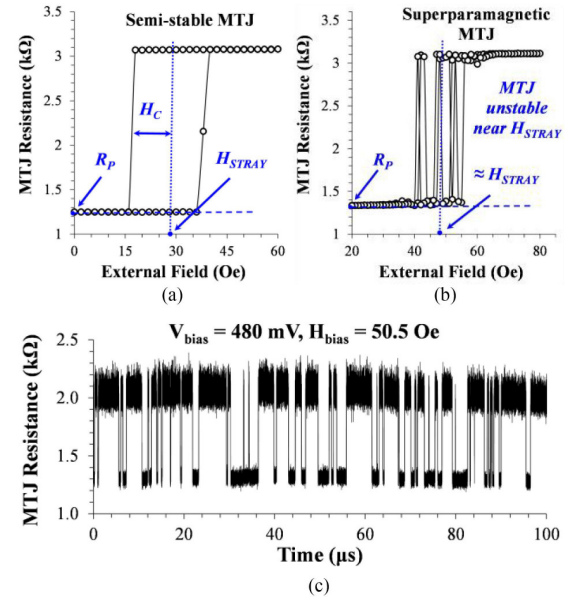


Fig. 1. Resistance versus field plots for (a) MTJ 6 and (b) MTJ 2 (see Table 1). (c) Random telegraphic switching signals generated by MTJ 2 under a bias field of 50.5 Oe (relative to  $H_{\text{stray}}$ ) and a bias voltage of 480 mV.

MTJs. The reason for choosing four categories was based on how the MTJs seemed to cluster into four groups in terms of their  $\Delta_0$  values. Even though both sMTJs and unstable MTJs exhibited superparamagnetic behavior (as shown in the asynchronous  $P_{\text{SW}}$  measurements as well as their  $R$ – $H$  plots), they are placed into separate categories because the retention time is  $\sim 2$  orders of magnitude lower for the sMTJs than for the unstable MTJs. Similarly, semistable MTJs and stable MTJs are placed into separate categories because the retention time of the semistable MTJs is  $\sim 4$  orders of magnitude higher than those for stable MTJs.

Dual-biasing measurements were collected for each MTJ using the same experimental setup described in our previous work [Zink 2018]. Note that these dual-biasing measurements are not the same as the asynchronous  $P_{\text{SW}}$  measurements used to calculate  $\Delta_0$  for MTJs 1–5 since dual-biasing has specific parameters on  $H_{\text{bias}}$  and  $V_{\text{bias}}$ . The polarity of the biases should be set so that  $H_{\text{bias}}$  favors P-state orientation and  $V_{\text{bias}}$  favors AP-state orientation. For our purposes,  $H_{\text{bias}}$  is said to increase as it moves to stronger P-state orientation, which occurs when  $H_{\text{bias}} \leq H_{\text{stray}}$  [recall Fig. 1(a) and (b)]. All  $H_{\text{bias}}$  values are presented relative to the MTJ's  $H_{\text{stray}}$ . Certain combinations of magnitudes for  $V_{\text{bias}}$  and  $H_{\text{bias}}$  produce a condition where the MTJ is never in the energetically favorable state, which causes continuous toggling between the AP- and P-states, thus generating random telegraphic switching signals, as illustrated in Fig. 1(c). The physical mechanisms which produce high levels of tunability and control are explained in greater detail in our previous work [Zink 2019].

## III. RESULTS

### A. Transfer Characteristics

In our analysis, we defined the time-averaged output as the percentage of time the MTJ spends in the AP-state, which we refer to as the AP-rate. AP-rate versus  $V_{\text{bias}}$  curves were acquired for all MTJs,

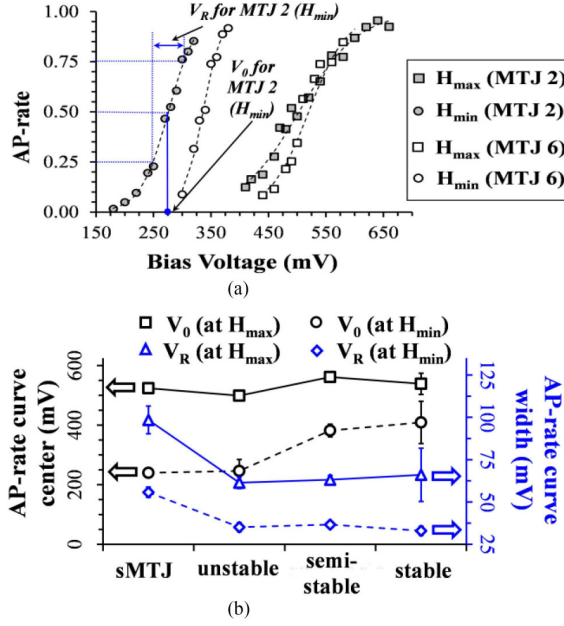


Fig. 2. (a) AP-rate versus bias voltage curves at  $H_{\min}$  and  $H_{\max}$  for a semistable MTJ and an sMTJ (MTJs 6 and 2 from Table 1).  $H_{\min} = 60$  Oe and 30.5 Oe, and  $H_{\max} = 80$  Oe and 55.5 Oe for MTJ 6 and 2, respectively. (b) Line plots showing the center ( $V_0$ ) and width ( $V_R$ ) of the voltage-dependent transfer curves for each MTJ category at  $H_{\min}$  and  $H_{\max}$ .

examples of which are shown in Fig. 2(a). These curves represent the transfer properties of the device and were characterized in terms of their center and width ( $V_0$  and  $V_R$ , respectively) where  $V_0$  is defined as  $V_{\text{bias}}$  when AP-rate = 0.5  $V_R$  is defined as the difference in  $V_{\text{bias}}$  at AP-rates of 0.75 and 0.25.  $V_0$  and  $V_R$  were obtained by fitting the AP-rate curves to a hyperbolic tangent function as was done in our previous work (see Zink [2019]).

The line plots of the average  $V_0$  and  $V_R$  measured at both minimum and maximum  $H_{\text{bias}}$  ( $H_{\min}$  and  $H_{\max}$ , respectively) are shown in Fig. 2(b) for each MTJ category. These data show that  $V_0$  increases as  $\Delta_0$  increases at  $H_{\min}$ , where  $V_0 = 240 \pm 15$  mV for sMTJs and  $409 \pm 71$  mV for stable MTJs. However, at  $H_{\max}$ ,  $V_0$  is nearly constant between all sets, where  $V_0 = 524 \pm 11$  mV for sMTJs and  $539 \pm 36$  mV for stable MTJs. This cutoff in  $V_0$  can be attributed to the rectifying properties of MTJs, where  $V_{\text{bias}}$  causes their TMR ratio to decrease. This creates an upper limit on  $V_{\text{bias}}$  for the dual-biasing method since it relies on current fluctuations caused by resistance changes [Zink 2019]. Therefore, the limiting factor for  $V_{\text{bias}}$  is the TMR ratio and not  $\Delta_0$ , which is why  $V_0$  is not dependent on  $\Delta_0$  at  $H_{\max}$  in Fig. 2(b).

For all MTJs,  $V_R$  increased from  $H_{\min}$  to  $H_{\max}$ . Note that if  $H_{\text{bias}}$  were equal among all MTJs, then  $V_R$  would decrease as  $\Delta_0$  increases. However, larger  $H_{\text{bias}}$  was needed for MTJs with larger  $\Delta_0$ , thus increasing  $V_R$ , which explains why  $V_R$  appears to be equal among unstable, semistable, and stable MTJs. However,  $V_R$  was at least two times larger for sMTJs at both  $H_{\min}$  and  $H_{\max}$ , despite smaller  $H_{\text{bias}}$ .

In terms of transfer curve characteristics, sMTJs showed superior performance to all others. Not only do they require lower minimum  $V_0$  compared to the other three categories, but they also have the same maximum  $V_0$  values, thus providing a larger tunability range. Furthermore, sMTJs had significantly wider transfer curves than the

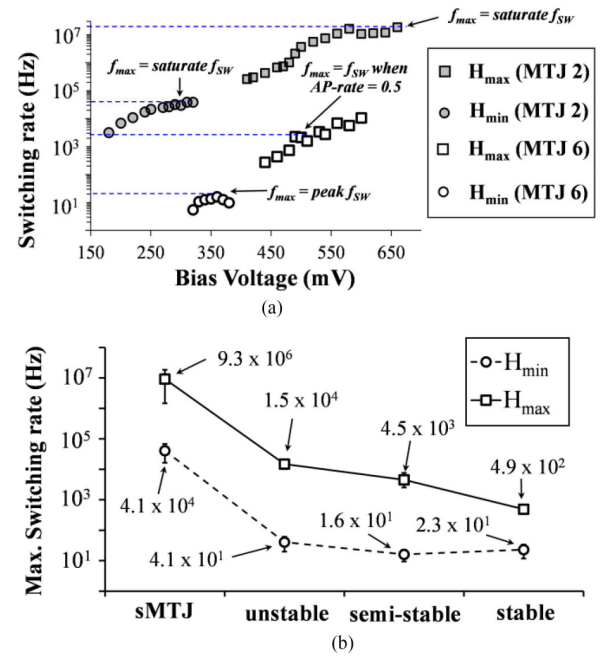


Fig. 3. (a) Dependence of average switching rate with bias voltage at  $H_{\max}$  and  $H_{\min}$  for MTJs 6 and 2 (see Table 1). (b) Maximum switching rate ( $f_{\text{max}}$ ) achieved for each MTJ category.

others, which are ideal for p-bits since output resolution and noise tolerance improve with transfer curve width.

## B. Average Switching Rate

For every dataset, we measured the average AP- and P-state dwell times ( $\tau_{\text{AP}}$  and  $\tau_{\text{P}}$ , respectively) which were used to calculate the average switching rate ( $f_{\text{SW}}$ ) using  $f_{\text{SW}} = (\tau_{\text{AP}} + \tau_{\text{P}})^{-1}$ . Fig. 3(a) shows  $f_{\text{SW}}$  plotted with  $V_{\text{bias}}$  for MTJs 2 and 6 (see Table 1) at  $H_{\min}$  and  $H_{\max}$ . This figure illustrates three different behaviors of  $f_{\text{SW}}$  with  $V_{\text{bias}}$ . One is that  $f_{\text{SW}}$  reaches a maximum and then decreases, which is seen at  $H_{\min}$  for MTJ 6. The second is that  $f_{\text{SW}}$  increases with  $V_{\text{bias}}$  until reaching a saturation point, as seen at  $H_{\max}$  and  $H_{\min}$  for MTJ 2. Lastly,  $f_{\text{SW}}$  increases exponentially with  $V_{\text{bias}}$ , as seen at  $H_{\max}$  for MTJ 6.

Here, we analyze the maximum  $f_{\text{SW}}$  ( $f_{\text{max}}$ ) achieved at  $H_{\min}$  and  $H_{\max}$  for all MTJs. The method of calculating  $f_{\text{max}}$  depended on the behavior of  $f_{\text{SW}}$  versus  $V_{\text{bias}}$ . If  $f_{\text{SW}}$  peaked or saturated, then  $f_{\text{max}}$  was simply  $f_{\text{SW}}$  at the peak or saturation value. However, if  $f_{\text{SW}}$  increases exponentially with  $V_{\text{bias}}$ , then defining  $f_{\text{max}}$  was not as straightforward since  $f_{\text{max}}$  may occur when AP-rate  $> 0.9$ , which is not particularly useful for p-bit applications. Therefore, for these datasets, we defined  $f_{\text{max}}$  as  $f_{\text{SW}}$  when the AP-rate = 0.5.

Fig. 3(b) shows a line plot of  $f_{\text{max}}$  at  $H_{\min}$  and  $H_{\max}$  for all four categories. Unsurprisingly,  $f_{\text{max}}$  was the largest for sMTJs, which achieved  $f_{\text{max}} \approx 10^4$ – $10^7$  Hz. The remaining three MTJ categories showed  $f_{\text{max}} \approx 10$ – $100$  Hz at  $H_{\min}$ . This is because time-domain data were not collected if the dwell times  $> 50$  ms, due to bandwidth limitations. For sMTJs and unstable MTJs,  $f_{\text{max}}$  at  $H_{\min}$  is on the same order of magnitude as their intrinsic dwell times whereas semistable and stable MTJs required larger biases to reach 10 Hz. The upper limit of  $V_{\text{bias}}$  for all MTJs [recall Fig. 2(b)] means that  $f_{\text{max}}$  at  $H_{\max}$  is the



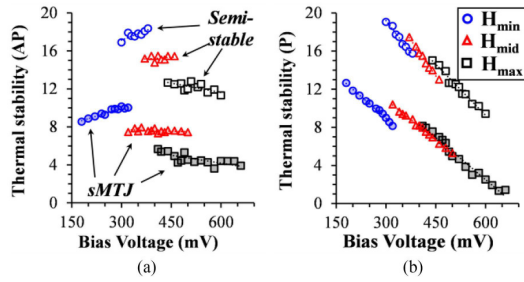


Fig. 4. Effective thermal stability factor versus bias voltage at  $H_{\max}$ ,  $H_{\min}$ , and  $H_{\text{mid}}$  for (a) AP-state and (b) P-state components for MTJs 6 and 2 (see Table 1). Note that  $H_{\text{mid}} = 70$  Oe for MTJ 6 and 45.5 Oe for MTJ 2.

upper limit of  $f_{\max}$  of the MTJ, meaning unstable MTJs and sMTJs have a broader tuning range of  $f_{\max}$  than semistable and stable MTJs.

### C. Degree of Separation Between $\Delta_{\text{AP}}$ and $\Delta_{\text{P}}$ Tunability

For this analysis,  $\tau_{\text{AP}}$  and  $\tau_{\text{P}}$  were used to calculate the AP- and P-state components of the effective thermal stability factors ( $\Delta_{\text{AP}}$  and  $\Delta_{\text{P}}$ , respectively) using the Néel-Arrhenius equation,  $\tau_{\text{AP(P)}} = \tau_0 \exp(\Delta_{\text{AP(P)}})$ , where the inverse attempt frequency ( $\tau_0$ ) was assumed to be 1 ns [Lopez-Diaz 2002]. Fig. 4(a) and (b) shows  $\Delta_{\text{AP}}$  and  $\Delta_{\text{P}}$  plotted with  $V_{\text{bias}}$  for MTJs 6 and 2 (see Table 1) at  $H_{\min}$ ,  $H_{\max}$ , and a bias field between  $H_{\min}$  and  $H_{\max}$ , referred to as  $H_{\text{mid}}$ . For both MTJs,  $\Delta_{\text{AP}}$  increases with  $V_{\text{bias}}$  and decreases with  $H_{\text{bias}}$  whereas  $\Delta_{\text{P}}$  decreases with  $V_{\text{bias}}$  and increases with  $H_{\text{bias}}$ . However, two-degrees-of-tunability capability of dual-biasing is revealed when investigating the relative changes in  $\Delta_{\text{AP}}$  versus  $\Delta_{\text{P}}$  with both  $V_{\text{bias}}$  and  $H_{\text{bias}}$ . At  $H_{\min}$ , changes in  $\Delta_{\text{P}}$  with  $V_{\text{bias}}$  are  $\sim 3.5 \times$  larger than changes in  $\Delta_{\text{AP}}$  for MTJ 6 and  $\sim 2 \times$  larger for MTJ 2. At  $H_{\max}$ , changes in  $\Delta_{\text{P}}$  with  $V_{\text{bias}}$  are  $\sim 6 \times$  and  $4.5 \times$  larger than the changes in  $\Delta_{\text{AP}}$  for MTJs 6 and 2, respectively. In fact,  $\Delta_{\text{AP}}$  appears to decrease slightly with  $V_{\text{bias}}$  as  $H_{\text{bias}}$  increases, which was observed for all devices tested and explained in our previous work [Zink 2019]. This means that P-state pulsewidths will decrease by 2–3 orders of magnitude while AP-state pulsewidths do not even change by 1 order. On the other hand, at the minimum voltages ( $V_{\min}$ ), changes in  $\Delta_{\text{AP}}$  with  $H_{\text{bias}}$  are  $\sim 1.5 \times$  and  $2.5 \times$  larger than changes in  $\Delta_{\text{P}}$  and at  $V_{\max}$ ,  $\sim 9.5 \times$  and  $2 \times$  for MTJs 2 and 6, respectively. This means that that AP-state pulsewidths decrease with  $H_{\text{bias}}$  by  $\approx 2$ –2.5 orders of magnitude while P-state pulsewidths increase by less than 1. The influences of  $H_{\text{bias}}$  and  $V_{\text{bias}}$  on  $\Delta_{\text{AP}}$  and  $\Delta_{\text{P}}$  observed in Fig. 4(a) and (b) were also observed in our previous work [Zink 2018, 2019], which demonstrates the reproducibility of dual-biasing.

Note that  $\Delta_{\text{AP}}$  and  $\Delta_{\text{P}}$  are influenced by both  $V_{\text{bias}}$  and  $H_{\text{bias}}$  to some degree; therefore, the two-degrees-of-tunability feature can be quantified. In our analysis, this is done using a metric we refer to as the degree of separation in  $\Delta_{\text{P}}$  and  $\Delta_{\text{AP}}$  tunability, which we divided into  $V_{\text{bias}}$  dependence and  $H_{\text{bias}}$  dependence components ( $D_V$  and  $D_H$ , respectively).  $D_V$  and  $D_H$  are expressed using slopes of  $\Delta_{\text{P}}$  and  $\Delta_{\text{AP}}$  with  $V_{\text{bias}}$  and  $H_{\text{bias}}$ , respectively, as seen in (1).  $D_V$  represents the order of magnitude decrease in  $\tau_{\text{P}}$  for every 1 order of magnitude increase in  $\tau_{\text{AP}}$  with  $V_{\text{bias}}$ . Similarly,  $D_H$  represents the order of magnitude decrease in  $\tau_{\text{AP}}$  for every 1 order of magnitude increase in  $\tau_{\text{P}}$  with  $H_{\text{bias}}$ . According to the Néel-Brown model [Li 2004],  $\Delta_{\text{AP(P)}}$  is proportional

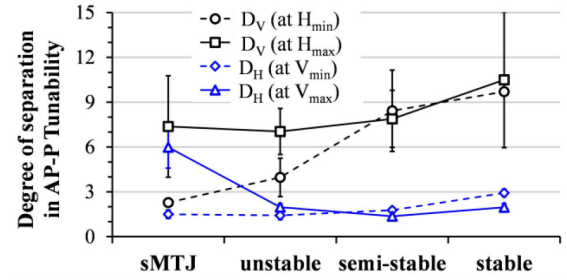


Fig. 5. Degree of separation between  $\Delta_{\text{AP}}$  and  $\Delta_{\text{P}}$  tunability with voltage and field ( $D_V$  and  $D_H$ , respectively) for each MTJ category.  $D_V$  represents the order of magnitude decrease in  $\tau_{\text{P}}$  for every 1 order of magnitude increase in  $\tau_{\text{AP}}$ , and  $D_H$  represents the order of magnitude decrease in  $\tau_{\text{AP}}$  for every 1 order of magnitude increase in  $\tau_{\text{P}}$ .

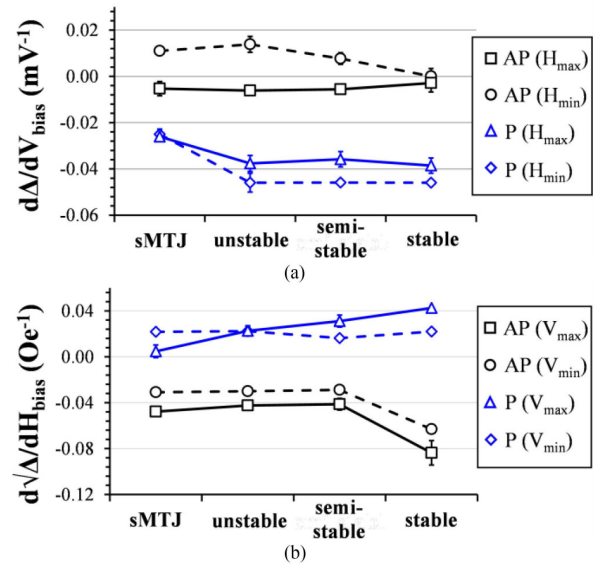


Fig. 6. Slopes  $\Delta_{\text{AP}}$  and  $\Delta_{\text{P}}$  with respect to (a)  $V_{\text{bias}}$  and (b)  $H_{\text{bias}}$  for each MTJ category.

to  $H_{\text{bias}}^2$ ; therefore, we defined  $D_H$  in terms of changes in  $\sqrt{\Delta_{\text{AP(P)}}}$

$$D_V = \left| \frac{d\Delta_{\text{P}}/dV_{\text{bias}}}{d\Delta_{\text{AP}}/dV_{\text{bias}}} \right| \quad D_H = \left| \frac{d\sqrt{\Delta_{\text{AP}}}/dH_{\text{bias}}}{d\sqrt{\Delta_{\text{P}}}/dH_{\text{bias}}} \right|. \quad (1)$$

The line plots in Fig. 5 show  $D_V$  and  $D_H$  for all four MTJ categories.  $D_V$  is calculated at both  $H_{\min}$  and  $H_{\max}$ , and  $D_H$  is calculated at both  $V_{\min}$  and  $V_{\max}$ . This plot shows that  $D_V$  clearly improves as  $\Delta_0$  increases at  $H_{\min}$ . However, the influence of  $\Delta_0$  on  $D_V$  at  $H_{\max}$  is unclear due to the large error bars. One key observation is that  $D_V$  improves from  $H_{\min}$  to  $H_{\max}$  for sMTJs and unstable MTJs, whereas  $D_V$  does not change significantly with  $H_{\text{bias}}$  for semistable and stable MTJs. Fig. 6 shows that dual-biasing on stable MTJs achieves better degree of separation in tunability with  $V_{\text{bias}}$  since  $D_V$  maintains a value above 6 from  $H_{\min}$  to  $H_{\max}$ . It should be noted that  $D_V > 2$  for sMTJs at  $H_{\min}$ , meaning that the two-degrees-of-tunability capability is still present.

The  $D_H$  curves in Fig. 5 shows that the MTJ category, which produces the largest  $D_H$ , is dependent on  $V_{\text{bias}}$ . These curves show that stable MTJs have the largest  $D_H$  at  $V_{\min}$  whereas sMTJs have the largest  $D_H$  at  $V_{\max}$ . This result demonstrates that even though the degree of separation in  $\Delta_{\text{P}}$  tunability with  $V_{\text{bias}}$  is reduced in sMTJs, two degrees

of tunability is not sacrificed since their degree of separation in  $\Delta_{AP}$  tunability with  $H_{bias}$  improves.

The behavior of  $D_V$  and  $D_H$  can be explained using the line plots in Fig. 6(a) and (b), which show the slopes of  $\Delta_{AP}$  and  $\Delta_P$  with  $V_{bias}$  and  $H_{bias}$ , respectively. Fig. 7(a) shows that  $d\Delta_{AP}/dV_{bias}$  is  $\sim 10\times$  larger for sMTJs and unstable MTJs than for stable MTJs at  $H_{min}$ , which clearly illustrates why  $D_V$  is significantly smaller in sMTJs compared to stable MTJs. Furthermore,  $|d\Delta_P/dV_{bias}|$  is  $\sim 2\times$  lower for sMTJs than for all other categories at both  $H_{min}$  and  $H_{max}$ , which also contributes to a reduction in  $D_V$  for sMTJs. The key observation from Fig. 7(a) is that  $d\Delta_{AP}/dV_{bias}$  changes sign from  $H_{min}$  to  $H_{max}$  for all MTJs. This was also observed in one of our previous studies where we attributed this sign change to the influence of  $H_{bias}$  on the AP- and P-state components of the intrinsic critical switching voltage ( $V_{CO}$ ), where increasing  $H_{bias}$  caused  $dV_{CO}/dV_{bias}$  to increase in the AP-state but not in the P-state [Zink 2019]. This sign change suggests that each MTJ, regardless of  $\Delta_0$ , has a bias field where  $d\Delta_{AP}/dV_{bias} \approx 0$ , resulting in a near infinite  $D_V$ . Note that this change in sign in  $d\Delta_{AP}/dV_{bias}$  explains the large error bars for  $D_V$  at  $H_{max}$  in Fig. 5.

This result may seem like an exciting prospect for complete independent tuning of  $\Delta_P$  and  $\Delta_{AP}$ . However, the dual-biasing method requires tuning of both  $V_{bias}$  and  $H_{bias}$ , meaning that optimum control over  $\Delta_P$  and  $\Delta_{AP}$  occurs when  $d\Delta_{AP}/dV_{bias}$  has minimal dependence on  $H_{bias}$  over a large range of bias fields. Our results show that the stable MTJs had the largest  $D_V$  values and smallest variation in  $d\Delta_{AP}/dV_{bias}$  from  $H_{min}$  to  $H_{max}$ . It should be noted that the VCMA efficiency increases as MTJ size decreases [Piotrowski 2016]. In this letter, sizes of the stable MTJs are larger than the sMTJs, as seen in the  $R_p$  values in Table 1. Therefore, the weak dependence of  $d\Delta_{AP}/dV_{bias}$  on  $H_{bias}$  seen in stable MTJs may be a result of device size and not  $\Delta_0$ .

Fig. 6(b) shows that  $|d\sqrt{\Delta_P}/dH_{bias}|$  is  $\sim 2-3\times$  larger for stable MTJs than all other MTJs at both  $V_{min}$  and  $V_{max}$ . Since  $d\sqrt{\Delta_P}/dH_{bias}$  is nearly constant among all MTJs at  $V_{min}$ ,  $D_H$  is largest for stable MTJs at  $V_{min}$ . However, each MTJ category had showed different responses of  $d\sqrt{\Delta_P}/dH_{bias}$  with  $V_{bias}$ . From  $V_{min}$  to  $V_{max}$ ,  $d\sqrt{\Delta_P}/dH_{bias}$  decreased significantly for sMTJs, remained constant for unstable MTJs, and increased for semistable and stable MTJs. The change in  $d\sqrt{\Delta_P}/dH_{bias}$  from  $V_{min}$  to  $V_{max}$  is partially due to the influence of  $V_{bias}$  on the anisotropy field ( $H_K$ ) and  $V_{CO}$ . Previous experimental work has shown that VCMA efficiency increases as the MTJs thermal stability factor increases [Piotrowski 2016], which explains the differences in responses of  $d\sqrt{\Delta_P}/dH_{bias}$  since the influence of  $V_{bias}$  on  $d\sqrt{\Delta_P}/dH_{bias}$  in stable MTJs is primarily characterized by  $dH_K/dV_{bias}$  and  $dV_{CO}/dV_{bias}$ . This discrepancy in the behavior of  $d\sqrt{\Delta_P}/dH_{bias}$  with  $V_{bias}$  explains why  $D_H$  is largest for sMTJs at  $V_{max}$ .

#### IV. CONCLUSION

A major challenge in realizing p-bits in large-scale PSL circuits is that any deviations in  $\Delta_0$  between MTJs will result in significant differences in their transfer curves and switching rates, resulting in computation errors and bottlenecks. Dual-biasing is a promising solution for correcting these variations as it provides a method for tuning the center and width of the p-bits transfer curve as well as its switching rate. In our previous studies, the dual-biasing technique was applied to thermally stable MTJs, therefore sacrificing switching rate

for two degrees of tunability. However, in this letter, we demonstrated that dual-biasing can achieve two degrees of tunability for both sMTJs and stable MTJs. Even though sMTJs did not achieve the same degree of separation in low-state tunability with voltage, the capability for two degrees of tunability was not sacrificed. Additionally, dual-biased sMTJs improved several other performance metrics such as larger degree of separation in high-state tunability with field, enhanced control over average output and switching rate, and better noise immunity in transfer curves.

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