

# A single-layer urban canopy model with transmissive radiation exchange between trees and street canyons

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1    **Abstract**

2           Urban trees are one of the most effective strategies to mitigate excessive heat stress in  
3    cities. To understand the underlying mechanisms of their cooling effect and to assess their use in  
4    urban planning, the accurate simulation of how trees interact with the ambient built environment  
5    is critical and imperative. However, the representation of urban trees in existing urban canopy  
6    models (in particular single-layer ones) remains oversimplified. Here we develop a new Monte  
7    Carlo ray tracing method to explicitly resolve the canopy transmittance and evaluate its impact  
8    on radiative view factors between trees and regular building facets. The new method is highly  
9    accurate in reproducing analytical solutions. Sensitivity tests of radiative view factors suggest the  
10   importance of canopy transmittance in changing the radiation exchange. We then incorporate the  
11   ray tracing algorithm into the new version of the Arizona State University (ASU) Single-Layer  
12   Urban Canopy Model (ASLUM v3.1). In addition to radiation transmittance, ASLUM v3.1  
13   explicitly resolves the radiative shading, evapotranspiration, and root water uptake of urban trees  
14   in street canyons, with significantly improved performance in predictions (especially latent heat  
15   flux) when compared to previous versions. We further apply ASLUM v3.1 to evaluate the  
16   impacts of trees with varying characteristics on urban radiation exchange and turbulent heat  
17   fluxes. Results show that urban trees reduce the net radiation of ground and wall as well as the  
18   daytime temperature via shading and transpiration, but may slightly warm the nighttime street  
19   canyons through radiative trapping effect.

20

21    **Keywords:**

22    Urban trees; urban canopy model; Monte Carlo ray tracing; canopy transmittance; view factors;  
23    cooling effect

24        **1. Introduction**

25            Urban trees are one of the most effective and versatile nature-based solutions to improve  
26            environmental quality in cities. Especially, they alleviate daytime excessive urban heat stress  
27            during hot summers mainly through radiative shading and evapotranspiration [1]. The cooling  
28            effect of urban trees has been assessed and demonstrated in numerous field experiments and  
29            studies based on remote sensing techniques [2–5]. They are also found to efficiently improve the  
30            pedestrian thermal comfort, reduce the building energy consumption for cooling, and offset  
31            carbon emissions [6–9]. On the other hand, the efficacy of urban trees depends on many factors  
32            such as synoptic weather conditions, background climates, and tree species. Assessment is  
33            therefore necessary prior to and during the implementation of trees in urban planning and design,  
34            during which accurate numerical models are needed.

35            Extensive efforts have been made to improve urban tree modeling in micro- and local-  
36            scale numerical simulations during the past two decades. The simplest models include semi-  
37            analytical or empirical ones and those simulate trees (and other vegetation) as a separate tile. For  
38            example, Shashua-Bar and Hoffman [10] developed an empirical model (Green CTTC) and  
39            evaluated the cooling effect of urban trees as the shading partially offset by the convective heat  
40            exchange. The Surface Urban Energy and Water Balance Scheme (SUEWS) proposed by Järvi et  
41            al. [11] simulates the energy and water exchange of urban deciduous and coniferous trees as  
42            individual surface types parallel to paved surfaces and buildings. In contrast, urban canopy  
43            models address the impacts of urban geometry using the simplified two-dimensional (2D) street  
44            canyon representation [12–14], in which trees are usually modeled as a single layer [15,16],  
45            opaque elements [17–19], or porous media [20,21]. Several urban canopy models have been  
46            coupled with atmospheric models to investigate how urban trees affect the regional and

47 mesoscale land–atmosphere exchange processes [22–26]. For instance, Loughner et al. [22] and  
48 Lee et al. [23] implemented the Vegetated Urban Canopy Model (VUCM) [16] into the  
49 mesoscale Weather Research and Forecasting (WRF) model and assessed the cooling effect of  
50 urban trees in Washington–Baltimore metropolitan area and Seoul metropolitan area,  
51 respectively. Similarly, Upreti et al. [24] and Wang et al. [25] coupled a single-layer urban  
52 canopy model [27] to the WRF model to examine the impacts of shade trees on temperatures,  
53 surface energy partitioning, and human thermal comfort in the Phoenix metropolitan area and the  
54 contiguous United States, respectively. Computational fluid dynamics (CFD) models represent  
55 another model category that solves the exchange of mass, momentum, and energy between  
56 building surfaces and trees, albeit with high computational cost [28–36]. In particular, the impact  
57 of trees (as porous media) on the flow field is usually modeled as a source term in the  
58 momentum equation [29,31–33,35]. ENVI-met is probably one of the most widely used fine-  
59 scale CFD-based tools to model urban trees, although it requires detailed urban morphological  
60 input for the study area [30,34,37,38].

61       Realistically resolving vegetation (including trees) is critical to modeling urban surface  
62 energy exchange [39]. Compared to empirical, slab, and CFD models, urban canopy models are  
63 capable of simulating physical processes influenced by common 2D urban structure and trees  
64 with intermediate complexity. Urban canopy models can be broadly categorized into single-layer  
65 and multilayer models [40]. Among single-layer urban canopy models, the VUCM [16] is one of  
66 the earliest ones that consider trees, in which the energy balance of trees is modeled using the big  
67 leaf approach. Using a Monte Carlo ray tracing method, Wang’s [17] model exclusively  
68 simulates the radiative shading effect of urban trees in a single-layer urban canopy model [27].  
69 This model is reintroduced here as the Arizona State University (ASU) Single-Layer Urban

70 Canopy Model (ASLUM) v3.0 (see details in Section 2). The same ray tracing method was later  
71 adopted in the urban canopy model proposed by Ryu et al. [18]. Ryu et al.'s [18] model  
72 explicitly resolves the shading, transpiration, and root water uptake of urban trees. The Town  
73 Energy Balance (TEB) model has been refined to simulate the influence of urban trees on urban  
74 radiation exchange and airflow (TEB-SURFEX) [41]. Recently, the ecohydrological dynamics of  
75 urban trees were incorporated into the Urban Tethys-Chloris (UT&C) model proposed by Meili  
76 et al. [19]. Urban trees have also been included in a multilayer urban canopy model (BEP-tree) to  
77 evaluate their impacts on pedestrian-level micrometeorology, although this model does not  
78 include hydrological modules [20,21].

79 It is noteworthy that radiative view factors are one of the key components in resolving the  
80 shortwave and longwave radiation budget in urban canopy models [12,14], especially those with  
81 trees integrated. However, due to the complex three-dimensional (3D) nature of trees, the  
82 accurate modeling of the impact of trees on view factors is challenging. Among the single-layer  
83 family, the VUCM [16] and TEB-SURFEX [15,41] use analytically derived view factors for  
84 street canyons without trees, while the impact of trees is implicitly considered with  
85 transmissivities as ad hoc reduction factors. In contrast, the current version of ASLUM [17], Ryu  
86 et al.'s [18] model, and UT&C model [19] simulate view factors using the Monte Carlo ray  
87 tracing approach. The Monte Carlo ray tracing approach can numerically determine the view  
88 factors and radiation exchange between various (complex) surfaces using randomized energy  
89 bundles [42]. Nevertheless, in existing single-layer urban canopy models with ray tracing  
90 methods, trees are assumed to be opaque with no canopy gap fraction (gaps between leaves  
91 within tree crowns) [17–19]. Similar assumption has been made in those based on analytical  
92 view factors as well (e.g., the TUrban model [43]), which may induce large errors for sparse tree

93 canopy. In addition, the validation of view factors between trees and street canyon facets remains  
94 relatively rare, primarily due to the lack of measurements.

95 The objective of this study is twofold: (1) to develop a new Monte Carlo ray tracing  
96 method that explicitly incorporates the transmittance of foliage, and (2) to develop a new version  
97 of ASLUM (v3.1) that can simulate both radiative shading and evapotranspiration of urban trees  
98 (cf. only shading in ASLUM v3.0 [17]). The proposed models are expected to improve the  
99 representation of trees in the current versions of ASLUM and other urban canopy models. We  
100 first review the history of three generations of ASLUM in Section 2. The details of new models  
101 are introduced in Section 3. We then evaluate the performance of the proposed models with  
102 analytical solutions and field measurements (Sections 4.1, 4.2, and 4.5). In particular, the  
103 sensitivity of radiative view factors to geometry and canopy transmittance is thoroughly  
104 evaluated in Sections 4.3 and 4.4. We also apply the new ASLUM to simulate the cooling effect  
105 of trees with varying characteristics in Section 5.

106

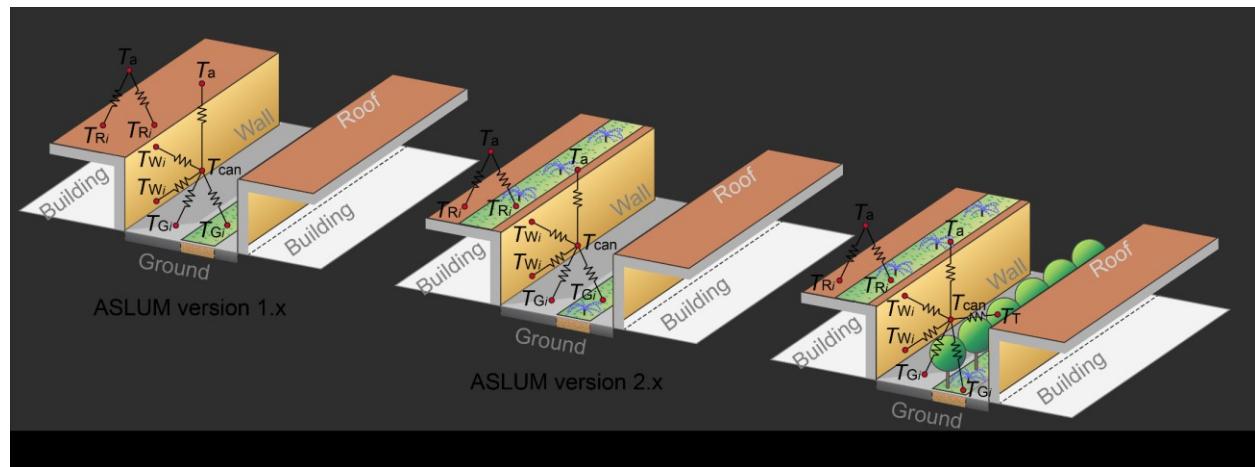
## 107 **2. Arizona State University Single-Layer Urban Canopy Model (ASLUM)**

108 The Arizona State University Single-Layer Urban Canopy Model (ASLUM) is a  
109 local/neighborhood-scale urban canopy model that physically resolves multiple processes  
110 (including the exchanges of heat, mass, and momentum) within the urban canopy layer. It  
111 represents the urban canopy layer as an infinitely long “big canyon” (2D) with specific  
112 dimensions and orientation [12,13]. ASLUM has undergone a decade of continuous development  
113 since ~2011 (see Table 1 and Fig. 1), and it is also among the earlier single-layer urban canopy  
114 models that explicitly resolve subfacet heterogeneity [44,45].

115

**Table 1.** Three generations of ASU Single-Layer Urban Canopy Model with major features.

Version	Major features	Key references
ASLUM v1.x	Basic urban energy and momentum exchanges; subfacet heterogeneity; Green's function-based surface temperatures and conductive heat fluxes	[44,46–48]
ASLUM v2.x	Detailed ground vegetation (grass) and roof vegetation (green roof); hydrological components; urban irrigation; anthropogenic heat; urban oasis effect	[27,49–51]
ASLUM v3.x	Trees (radiative shading, evapotranspiration, and root water uptake)	[8,17] and the present study



119 **Figure 1.** Schematic structures of three generations of the Arizona State University Single-Layer  
120 Urban Canopy Model with resistance networks of energy transport.  $T$  is temperature, with  
121 subscripts a, can, R, W, G, and T denoting air, canyon air, roof, wall, ground, and tree,  
122 respectively. The subscript  $i$  denotes different types of subfacets.

123 (Figure 1 is a 2-column fitting image)

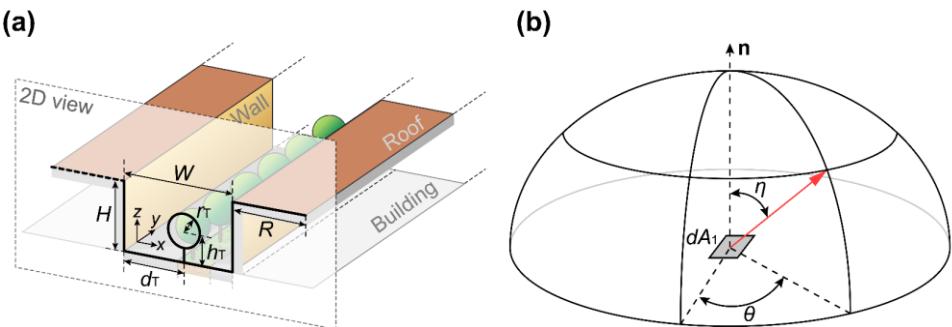
124 The first generation of ASLUM (v1.x) is developed based upon the offline version of the  
125 single-layer urban canopy model in the Weather Research and Forecasting (WRF) model  
126 [13,52]. Besides basic energy and momentum exchanges, ASLUM v1.x permits heterogeneity on  
127 each urban facet (walls, ground, and roof) [44]. For example, roofs can be a combination of  
128 conventional roofs and green roofs; ground surfaces can be composed of asphalt, concrete, bare  
129 soil, and ground vegetation (e.g., lawns); wall surfaces can consist of brick and glass. In addition,

130 ASLUM v1.x analytically resolves surface temperatures and conductive heat fluxes for solid  
131 media (walls, ground, roof, and soil) based on the Green's function approach [46–48]. The  
132 second generation of ASLUM (v2.x) features detailed ground and roof vegetation modeling [27],  
133 including a multi-layer green roof system [49–51]. ASLUM v2.x contains hydrological  
134 components to prognostically resolve soil moisture dynamics and evapotranspiration/evaporation  
135 from both natural surfaces and engineered surfaces (via a water-holding layer [27]). It  
136 incorporates some urban metabolic activities such as urban irrigation and anthropogenic heat  
137 fluxes [50]. ASLUM v2.x can also simulate the oasis effect on urban vegetation  
138 evapotranspiration [50]. The major improvement of the third generation of ASLUM (v3.x) is the  
139 numerical representation of urban trees. ASLUM v3.0 implicitly simulates the radiative shading  
140 effect of street trees via changes in radiative view factors based on a Monte Carlo ray tracing  
141 method [17]. This concise representation of urban trees enables the evaluation of the cooling  
142 effect and energy savings due to shade trees [8], but other complicated biophysical functions of  
143 urban trees (e.g., transpiration and root water uptake) are not resolved in v3.0.

144 Three generations of ASLUM have been extensively evaluated against field  
145 measurements with diverse background climates, showing good performance of reproducing  
146 different processes within the urban canopy layer (e.g., [24,27,47,50]). The sensitivity of the  
147 ASLUM to input parameters has been thoroughly evaluated using an advanced Monte Carlo  
148 simulation approach (subset simulation) (e.g., [44]). ASLUM has also been used to assess the  
149 efficacy (e.g., cooling, thermal comfort, and energy saving) of various urban heat mitigation  
150 strategies, such as white roofs, green roofs, lawns, trees, and urban irrigation (e.g., [8,17,50,53]).  
151 ASLUM is capable of being coupled to atmospheric models to simulate urban land–atmosphere  
152 interactions. ASLUM v2.x and v3.0 has been coupled to the WRF model for regional and

153 continental scales simulations (e.g., [24,25,54]). In particular, ASLUM v2.x has been included in  
 154 the public releases of the WRF model [50,55]. In addition, ASLUM v2.x and v3.0 have been  
 155 coupled with a single column atmospheric model to extend the evaluation of urban heat  
 156 mitigation strategies to the entire urban boundary layer (e.g., [56]).

157 In this study, we develop ASLUM v3.1 primarily based upon ASLUM v3.0 [8,17] and  
 158 Ryu et al.'s [18] model. ASLUM v3.1 simulate rows of street trees as circular shapes in the  
 159 cross-sectional (2D) plane (Fig. 2a). Due to the relatively small size of tree trunks as compared to  
 160 tree crowns and other urban facets, the impacts of trunks on radiation exchange are neglected  
 161 [17–19]. For illustration, here we assume one row of trees to simplify the interactions between  
 162 trees (see Section 3.3), while the proposed model can still simulate multiple rows of trees as in  
 163 ASLUM v3.0 [24,25]. The size and location of trees within the street canyon are determined by  
 164 three geometric parameters (Fig. 2a): the distance between the wall and the center of the tree  
 165 crown (“wall–tree distance”,  $d_T$ ), the height of the tree crown center (“tree height”,  $h_T$ ), and the  
 166 radius of the tree crown ( $r_T$ ). For one row of trees herein,  $d_T$  is equal to half the canyon width  
 167 (i.e., at the center of the street canyon) in a symmetric street canyon.



168  
 169 **Figure 2.** (a) Schematic structure of ASLUM v3.1 with one row of street trees and (b) the  
 170 direction of an energy bundle leaving an elemental surface area  $dA_1$  (red arrow) determined by  
 171 its zenith angle  $\eta$  and azimuth angle  $\theta$ . Note that in (a),  $H$ ,  $W$ , and  $R$  are building height, road  
 172 width, and roof width, respectively,  $d_T$  is the distance between the wall and the center of the tree

173 crown,  $h_T$  is the height of the tree crown center, and  $r_T$  is the radius of the tree crown. In (b),  $\mathbf{n}$  is  
174 the normal vector to the surface area.

175 (Figure 2 is a 1.5-column fitting image)

176

177 **3. Model description**

178 *3.1 Analytical solutions of radiative view factors*

179 A radiative view factor  $F_{12}$  describes the geometric relation of two surfaces ( $A_1$  and  $A_2$ ) as  
180 the fraction of uniform diffuse radiation leaving a surface  $A_1$  that directly reaches another surface  
181  $A_2$  [42]. In general, the direction of an energy bundle leaving an elemental surface area can be  
182 specified by the zenith angle  $\eta$  and azimuth angle  $\theta$  in a spherical coordinate system centered on  
183 it (Fig. 2b). The differential view factor between two elemental surface areas (from  $dA_1$  to  $dA_2$ ) is  
184 calculated as

185 
$$dF_{dA_1 dA_2} = \frac{\cos \eta_1 \cos \eta_2}{\pi S^2} dA_2, \quad (1)$$

186 where  $\eta_1$  ( $\eta_2$ ) is the zenith angle between the energy bundle and the surface normal of  $dA_1$  ( $dA_2$ ),  
187 and  $S$  is the length of the bundle. Integrating Eq. (1) over both surfaces gives

188 
$$F_{12} = \frac{1}{A_1} \int_{A_1} \int_{A_2} \frac{\cos \eta_1 \cos \eta_2}{\pi S^2} dA_2 dA_1. \quad (2)$$

189 For street canyons without trees in ASLUM v1.x and v2.x (Fig. 1), the view factors can  
190 be analytically determined as [57]

191 
$$F_{SG} = F_{GS} = \sqrt{1 + \left(\frac{H}{W}\right)^2} - \frac{H}{W}, \quad (3)$$

192 
$$F_{WW} = \sqrt{1 + \left(\frac{W}{H}\right)^2} - \frac{W}{H}, \quad (4)$$

193 
$$F_{GW} = \frac{1}{2}(1 - F_{GS}), \quad (5)$$

194 
$$F_{WG} = F_{WS} = \frac{1}{2}(1 - F_{WW}), \quad (6)$$

195 where the subscripts S, G, and W denote sky, ground, and wall, respectively,  $H$  is the building  
 196 height, and  $W$  is the ground (road) width (see also Fig. 2a). The ratio  $H/W$  is called canyon aspect  
 197 ratio.

198 For street canyons with one row of trees, the radiative view factor from trees (simplified  
 199 as circles in the 2D view) to one wall can also be analytically solved [58],

200 
$$F_{TW} = \frac{1}{\pi} \arctan\left(\frac{H}{2d_T}\right). \quad (7)$$

201 We can easily derive the view factor from wall to trees by applying the reciprocity relation (i.e.,  
 202  $A_1 F_{12} = A_2 F_{21}$ ),

203 
$$F_{WT} = \frac{2r_T}{H} \arctan\left(\frac{H}{2d_T}\right). \quad (8)$$

204

205 *3.2 Numerical solutions of radiative view factors with Monte Carlo ray tracing*

206 The analytical solutions in Section 3.1 were developed based on simple geometry with  
 207 opaque surfaces, and are not applicable to complex geometries such as multiple rows of trees  
 208 (e.g., two rows as in [24,25]) or, in particular, trees with transmittance considered. As an  
 209 alternative approach, the Monte Carlo method has been proposed to solve the radiation exchange  
 210 in enclosures and view factors [17,42]. In Monte Carlo ray tracing, the amount of radiative  
 211 energy can be numerically discretized into bundles (packets or rays) of energy. If equal energies  
 212 are assigned to all energy bundles, the local energy flux can be computed by counting the  
 213 number of bundles reaching a position of interest [42]. Similarly, the view factor  $F_{12}$  can be

214 determined by the proportion of rays emitted from surface  $A_1$  that are incident on surface  $A_2$   
 215 (ratio of ray numbers).

216 Following the definition of bundle angles in Fig. 2b, the zenith angle  $\eta$  and azimuth angle  
 217  $\theta$  for a diffuse-gray surface are randomized using two random numbers  $R_\eta$  and  $R_\theta$ ,

218 
$$R_\eta = \sin^2 \eta, \quad (9)$$

219 
$$R_\theta = \frac{\theta}{2\pi}. \quad (10)$$

220 It is straightforward that the direction of a ray can be transformed from its local spherical  
 221 coordinate system to a local Cartesian coordinate system as,

222 
$$\begin{bmatrix} \sin \eta \cos \theta \\ \sin \eta \sin \theta \\ \cos \eta \end{bmatrix} = \begin{bmatrix} \cos \theta & -\sin \theta & 0 \\ \sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \sin \eta \\ 0 \\ \cos \eta \end{bmatrix}. \quad (11)$$

223 This direction vector in the local Cartesian coordinate system is then transformed to the global  
 224 Cartesian coordinate system (Fig. 2a) via translation and rotation.

225 The emitting coordinates of rays from horizontal and vertical facets (ground, sky, and  
 226 walls) are determined by random numbers  $R_x$  and  $R_z$  [17],

227 
$$x_e = WR_x, z_e = 0 \text{ or } H, \text{ from ground or sky}, \quad (12)$$

228 
$$x_e = 0 \text{ or } W, z_e = HR_z, \text{ from walls}. \quad (13)$$

229 The emitting coordinates of rays from the surface of tree crowns are given by a random number  
 230  $R_e$ ,

231 
$$x_e = d_T + r_T \sin(2\pi R_e), \quad (14)$$

232 
$$z_e = h_T + r_T \cos(2\pi R_e). \quad (15)$$

233 Note that the above five random numbers ( $R_\eta$ ,  $R_\theta$ ,  $R_x$ ,  $R_z$ , and  $R_e$ ) are random numbers between  
 234 zero and one sampled from the standard uniform distribution. Usually these random numbers can

235 be generated by the pseudorandom number generator in MATLAB [17,19], but the ray tracing  
 236 methods using such random numbers have a slow convergence rate [59]. Instead, here we use the  
 237 Latin hypercube sampling method to generate random numbers that spread more evenly across  
 238 the sample space. The latter method is expected to speed up the convergence with smaller  
 239 discrepancies from the analytical solutions (see Section 4.1).

240 Different from the implicit method proposed by Wang [17] in ASLUM v3.0, here we  
 241 track the incident location of each ray by explicitly solving its intersections with all boundaries  
 242 in Fig. 2a. For example, the intersection of the ray with a horizontal or vertical facet (if there is a  
 243 single intersection) is  $\mathbf{l}_e + \mathbf{l}d$ . Here  $\mathbf{l}_e$  is the emitting point,  $\mathbf{l}$  is the direction vector of the ray, and  
 244  $d$  is solved by

$$245 \quad d = \frac{(\mathbf{p}_0 - \mathbf{l}_e) \cdot \mathbf{n}}{\mathbf{l} \cdot \mathbf{n}}, \quad (16)$$

246 where  $\mathbf{p}_0$  is a point on the facet, and  $\mathbf{n}$  is a normal vector to the facet as in Fig. 2b. We then  
 247 determine the actual incident point with the shortest distance from the emitting point.

248 We further consider the impact of canopy transmittance on the radiative view factors. For  
 249 simplicity, here we assume that the tree foliage is randomly distributed (spatial homogeneity),  
 250 the leaf inclination angles are spherically distributed, and the individual leaf size is much smaller  
 251 than the crown size. These assumptions have been commonly used in previous studies  
 252 (especially those on urban tree modeling) [18,20,60]. With these assumptions, the transmittance  
 253 is equivalent to the canopy gap fraction [61,62]. In the proposed ray tracing model, the  
 254 transmittance of tree crowns for both direct and diffuse radiation is a function of leaf area index  
 255 (LAI) based on the Beer–Lambert law [60,63],

$$256 \quad \tau = e^{-kLAI}, \quad (17)$$

257 where  $k$  is an empirical light extinction coefficient. We assume  $k = 0.61$  following measurements  
 258 in a deciduous forest ecosystem [63]. It is noteworthy that although this coefficient was from  
 259 photosynthetically active radiation measurements only, it is still within the ranges of extinction  
 260 coefficients for broad-leaved forests [60]. Here we use this empirical function to represent the  
 261 fraction of view unobstructed by canopy (similar to porous media; cf. transmittance of longwave  
 262 radiation assumed to be zero in e.g., Konarska et al. [64]). The transmittance  $\tau$  is then used as the  
 263 probability of a ray propagating through the tree canopy once it reaches the tree crown surface.

264

265 *3.3 Radiation exchange and turbulent heat fluxes in ASLUM v3.1*

266 The direct shortwave radiation for trees is determined by reference angles. In ASLUM  
 267 v3.1 with one row of trees, two reference angles are needed (Fig. 3a and b),

$$268 \quad \tan \theta_{ref_1} = \frac{r_T(H - h_T) + d_T \sqrt{d_T^2 + (H - h_T)^2 - r_T^2}}{(H - h_T) \sqrt{d_T^2 + (H - h_T)^2 - r_T^2} - r_T d_T}, \quad (18)$$

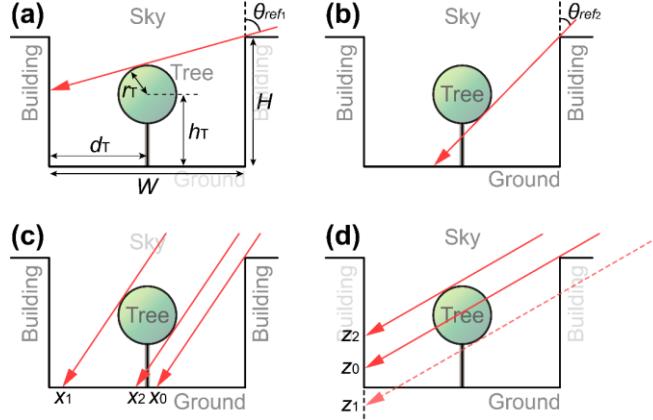
$$269 \quad \tan \theta_{ref_2} = \frac{d_T \sqrt{d_T^2 + (H - h_T)^2 - r_T^2} - r_T(H - h_T)}{(H - h_T) \sqrt{d_T^2 + (H - h_T)^2 - r_T^2} + r_T d_T}. \quad (19)$$

270 The direct shortwave radiation incident on trees is determined as [18]

$$271 \quad S_{D,T} = \begin{cases} 0 & \text{if } \xi \geq \tan \theta_{ref_1} \\ S_D [r_T \sqrt{1 + \xi^2} + d_T - (H - h_T) \xi] / (2\pi r_T) & \text{if } \tan \theta_{ref_2} \leq \xi \leq \tan \theta_{ref_1}, \\ S_D (2r_T \sqrt{1 + \xi^2}) / (2\pi r_T) & \text{if } \xi \leq \tan \theta_{ref_2} \end{cases}, \quad (20)$$

272 where  $S_D$  is the direct solar radiation received by a horizontal surface,  $\xi = \tan \theta_z \sin |\theta_n|$ ,  $\theta_z$  is the  
 273 solar zenith angle, and  $\theta_n$  is the difference between the solar azimuth angle and canyon  
 274 orientation [13,27]. Note that unlike in Ryu et al. [18], the transmittance is absent in the final

275 equations of direct shortwave radiation for trees, as the equivalent crown surface area becomes  
 276  $(1 - \tau)2\pi r_T$  here.



277

278 **Figure 3.** Determination of direct shortwave radiation in ASLUM v3.1 using (a) and (b)  
 279 reference angles and (c) and (d) reference points.  
 280 (Figure 3 is a single column fitting image)

281 Six reference points are used to determine shadows cast by wall and trees, as shown in  
 282 Fig. 3c and d. Points  $(x_0, 0)$  and  $(0, z_0)$  are the intersections of the ray passing the upper corner of  
 283 one wall with the ground and the other wall, respectively [18],

$$284 \quad x_0 = \max[W - H\xi, 0], \quad (21)$$

$$285 \quad z_0 = \max[H - W/\xi, 0]. \quad (22)$$

286 The two reference points delimiting tree shadow from the sunlit ground are

$$287 \quad x_1 = \max[d_T - h_T\xi - r_T\sqrt{1 + \xi^2}, 0], \quad (23)$$

$$288 \quad x_2 = \max[d_T - h_T\xi + r_T\sqrt{1 + \xi^2}, 0], \quad (24)$$

289 and the two reference points delimiting tree shadow from the sunlit wall are

$$290 \quad z_1 = \max[h_T - d_T\xi^{-1} - r_T\sqrt{1 + \xi^{-2}}, 0], \quad (25)$$

$$291 \quad z_2 = \max[h_T - d_T\xi^{-1} + r_T\sqrt{1 + \xi^{-2}}, 0]. \quad (26)$$

292 Here  $x_1 < x_2$  and  $z_1 < z_2$ . Then the shadow length on the ground from trees, if the shadow cast by  
 293 the wall is not considered, is  $\chi_T = x_2 - x_1$ . Similarly, the shadow length on the wall due to trees is  
 294  $\lambda_T = z_2 - z_1$ .

295 Then the total shadow length on the ground due to wall and trees is

$$296 \quad \chi_{\text{shadow}} = \begin{cases} W - x_0 + \chi_T & \text{if } x_2 \leq x_0 \\ W + \chi_T - x_2 & \text{if } x_1 \leq x_0 < x_2, \\ W - x_0 & \text{if } x_0 < x_1 \end{cases} \quad (27)$$

297 and the shadow length on the ground due exclusively to trees is

$$298 \quad \chi_{\text{trees}} = \begin{cases} \chi_T & \text{if } x_2 \leq x_0 \\ \chi_T - (x_2 - x_0) & \text{if } x_1 \leq x_0 < x_2. \\ 0 & \text{if } x_0 < x_1 \end{cases} \quad (28)$$

299 The total shadow length on the wall due to wall and trees is

$$300 \quad \lambda_{\text{shadow}} = \begin{cases} \max[z_0, z_2] & \text{if } z_1 \leq z_0 \\ \lambda_T + z_0 & \text{if } z_0 < z_1, \end{cases} \quad (29)$$

301 and the shadow length on the wall due exclusively to trees is

$$302 \quad \lambda_{\text{trees}} = \begin{cases} 0 & \text{if } z_2 \leq z_0 \\ z_2 - z_0 & \text{if } z_1 \leq z_0 < z_2. \\ \lambda_T & \text{if } z_0 < z_1 \end{cases} \quad (30)$$

303 The direct shortwave radiation incident on the ground is calculated as

$$304 \quad S_{D,G} = S_D (W - \chi_{\text{shadow}} + \tau \chi_{\text{trees}}) / W, \quad (31)$$

305 and the direct shortwave radiation incident on walls is

$$306 \quad S_{D,W} = S_D \xi (H - \lambda_{\text{shadow}} + \tau \lambda_{\text{trees}}) / (2H). \quad (32)$$

307 The term  $\tau \lambda_{\text{trees}}$  and  $\tau \chi_{\text{trees}}$  represent the sunflecks under trees at a particular solar angle. Note that  
 308 different from Ryu et al. [18] and Meili et al. [19], one row of trees in the proposed model  
 309 involves no interference between trees in the  $x$ - $z$  plane (Fig. 2a), so that the redistribution of

310 energy excess or deficit (due to the neglection of interference, as in previous studies) is  
 311 unnecessary.

312 The net shortwave radiation for each facet (ground, walls, roof, and tree crowns) is the  
 313 absorption of the direct and reflected shortwave radiation. We assume Lambertian surfaces as in  
 314 Kusaka et al. [13]. The subfacet heterogeneity is also resolved following Wang et al. [27]. Here  
 315 we only show equations related to tree crowns, and solutions for other facets are similar to those  
 316 detailed in Wang et al. [27]. For trees, the net shortwave radiation is

317 
$$S_T = (1 - \alpha_T)[S_{D,T} + S_Q F_{TS} + 2(S_{D,W} + S_Q F_{WS})\bar{\alpha}_W F_{TW} + (S_{D,G} + S_Q F_{GS})\bar{\alpha}_G F_{TG}], \quad (33)$$

318 where  $\alpha_T$  is the albedo of trees,  $\bar{\alpha}_W$  and  $\bar{\alpha}_G$  are the equivalent albedos of walls and ground with  
 319 subfacets, respectively, and  $S_Q$  is the diffuse solar radiation received by a horizontal surface.

320 The net longwave radiation absorbed by trees also considers both direct and reflected  
 321 radiation,

322 
$$L_{T,direct} = \varepsilon_T (L^{\downarrow} F_{TS} + 2\bar{\varepsilon}_W \sigma \bar{T}_W^4 F_{TW} + \bar{\varepsilon}_G \sigma \bar{T}_G^4 F_{TG} - \sigma T_T^4), \quad (34)$$

323 
$$L_{T,reflected} = \varepsilon_T [2F_{TW}(1 - \bar{\varepsilon}_W)(L^{\downarrow} F_{WS} + \bar{\varepsilon}_W \sigma \bar{T}_W^4 F_{WW} + \bar{\varepsilon}_G \sigma \bar{T}_G^4 F_{WG} + \varepsilon_T \sigma T_T^4 F_{WT}) + F_{TG}(1 - \bar{\varepsilon}_G)(L^{\downarrow} F_{GS} + 2\bar{\varepsilon}_W \sigma \bar{T}_W^4 F_{GW} + \varepsilon_T \sigma T_T^4 F_{GT})], \quad (35)$$

324 where  $\varepsilon_T$  is the emissivity of trees,  $\bar{\varepsilon}_W$  and  $\bar{\varepsilon}_G$  are the equivalent emissivities of walls and ground  
 325 with subfacets, respectively,  $\sigma$  is the Stefan–Boltzmann constant,  $T_T$  is the tree temperature,  $\bar{T}_W$   
 326 and  $\bar{T}_G$  are the equivalent temperatures of walls and ground, respectively, and  $L^{\downarrow}$  is the  
 327 downward longwave radiation.

328 The turbulent heat fluxes (sensible and latent heat fluxes) from walls, ground, and roof  
 329 are determined via resistance networks (Fig. 1), as detailed in Wang et al. [27]. ASLUM v3.1  
 330 also considers water-holding capacity of engineered pavements, and calculates the latent heat

331 flux from natural surfaces with reduction factor and stomatal resistance as in previous versions  
 332 [27,50]. For trees, the transpiration per unit of leaf plan area for a single, hypostomatous leaf is  
 333 given as [18,65]

$$334 E_{\text{leaf}} = \frac{sR_n + 0.93\rho c_p D_a / r_a}{L_v[s + 0.93\gamma(2 + r_s / r_a)]}, \quad (36)$$

335 where  $s$  is the slope of the saturation vapor pressure curve at the ambient air temperature,  $\rho$  is the  
 336 density of air,  $c_p$  is the specific heat capacity of air at a constant temperature,  $D_a$  is the vapor  
 337 pressure deficit of air,  $r_a$  and  $r_s$  are boundary layer resistance and stomatal resistance of the leaf,  
 338 respectively,  $L_v$  is the latent heat of vaporization, and  $\gamma$  is the psychrometric constant. Note that  
 339 the leaf boundary layer resistance follows the empirical relation in Green [65]. The net radiation  
 340 of the leaf,  $R_n$ , is the sum of net shortwave radiation ( $S_{\text{leaf}}$ ) and net longwave radiation ( $L_{\text{leaf}}$ ),

$$341 S_{\text{leaf}} = \frac{S_T 2\pi r_T (1 - \tau)}{2r_T \text{LAI}}, \quad (37)$$

$$342 L_{\text{leaf}} = \frac{L_T 2\pi r_T (1 - \tau)}{2r_T \text{LAI}}, \quad (38)$$

343 where  $L_T = L_{T,\text{direct}} + L_{T,\text{reflected}}$ , and  $2r_T \text{LAI}$  is the total leaf plan area. The latent heat flux per unit  
 344 leaf plan area is then  $LE_{\text{leaf}} = L_v E_{\text{leaf}}$ .

345 The sensible heat flux per unit leaf plan area is given as

$$346 H_{\text{leaf}} = \frac{\rho c_p (T_T - T_{\text{can}})}{\text{RES}_{\text{leaf}}}, \quad (39)$$

347 where  $T_{\text{can}}$  is the street canyon air temperature, and the aerodynamic resistance  $\text{RES}_{\text{leaf}} = 1.27r_a$   
 348 [18,66].

349 ASLUM v3.1 simulates the root water uptake by vegetation as a sink term in the Richards  
 350 equation using an empirical model developed by Jarvis [67]. This method takes into account the

351 effects of vertical distributions of roots and soil water content, and we assume the total root  
 352 water uptake to be equal to the total transpiration. More details of root water uptake calculation  
 353 can be found in Ryu et al. [18]. Note a tree fraction parameter (e.g., Eq. (21) in Ryu et al. [18]) is  
 354 not needed here, as ASLUM assumes homogeneity in the along-canyon axis (2D street canyon).

355 The canyon air temperature can be diagnostically solved as

$$356 T_{\text{can}} = \frac{\frac{2H}{W} \frac{\overline{T_w}}{\text{RES}_w} + \frac{\overline{T_g}}{\text{RES}_g} + \frac{2r_t \text{LAI}}{W} \frac{\overline{T_t}}{\text{RES}_{\text{leaf}}} + \frac{\overline{T_a}}{\text{RES}_{\text{can}}}}{\frac{2H}{W} \frac{1}{\text{RES}_w} + \frac{1}{\text{RES}_g} + \frac{2r_t \text{LAI}}{W} \frac{1}{\text{RES}_{\text{leaf}}} + \frac{1}{\text{RES}_{\text{can}}}}, \quad (40)$$

357 where  $\text{RES}_w$ ,  $\text{RES}_g$ , and  $\text{RES}_{\text{can}}$  are aerodynamic resistances of wall, ground, and street canyon,  
 358 and  $T_a$  is the air temperature at the reference height. This approach has been used in Masson [12]  
 359 and Wang et al. [27], although not for urban trees. Similarly, the canyon air specific humidity  
 360 can be diagnostically solved as

$$361 q_{\text{can}} = \frac{\frac{\rho L_v \overline{q_g}}{\text{RES}_g} + \frac{\rho L_v q_a}{\text{RES}_{\text{can}}} + \frac{2r_t \text{LAI}}{W} LE_{\text{leaf}}}{\frac{\rho L_v}{\text{RES}_{\text{can}}} + \frac{\rho L_v}{\text{RES}_g}}, \quad (41)$$

362 where  $\overline{q_g}$  is the equivalent specific humidity of ground, and  $q_a$  is the specific humidity at the  
 363 reference height.

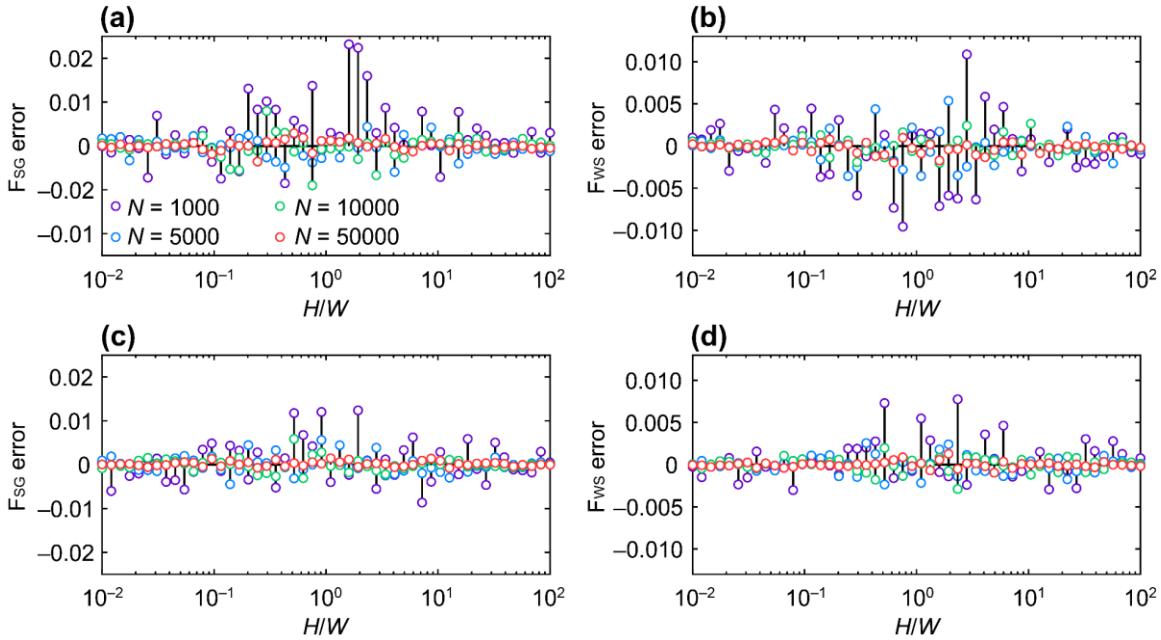
364

#### 365 **4. Model evaluation**

366 *4.1 Monte Carlo simulations and analytical solutions of radiative view factors in street canyons  
 367 without trees*

368 We compare the estimated view factors using the Monte Carlo ray tracing method against  
 369 analytical solutions based on Eqs. (3)–(6) in street canyons without trees (ASLUM v1.x and

370 v2.x). Results of  $F_{SG}$  and  $F_{WS}$  using different random number generators and sample sizes (for  
 371 each urban facet) are shown as the deviations from analytical solutions (“errors”) in Fig. 4. For  
 372 both (pseudo)random number generators, the accuracy of Monte Carlo ray tracing increases with  
 373 the sample size  $N$ . The estimated results with relatively higher errors usually occur within the  
 374  $H/W$  range of 0.1–10. With a sample size of 50000, the ray tracing methods using both random  
 375 number generators yield results with high accuracies: the values of mean absolute error (MAE)  
 376 are below 0.001. On the other hand, the ray tracing algorithm using the Latin hypercube  
 377 sampling method converges much faster than that using the default pseudorandom number  
 378 generator. For example, when the sample size is 100 (not shown here), the MAE of the estimated  
 379  $F_{SG}$  with the Latin hypercube sampling method is 0.008, much lower than that with the default  
 380 generator (0.02). In the subsequent simulations, we use the Latin hypercube sampling method  
 381 with a sample size of 10000 in the Monte Carlo ray tracing algorithm. This ensures both high  
 382 accuracy ( $MAE < 0.001$ ) and computational efficiency when estimating view factors.



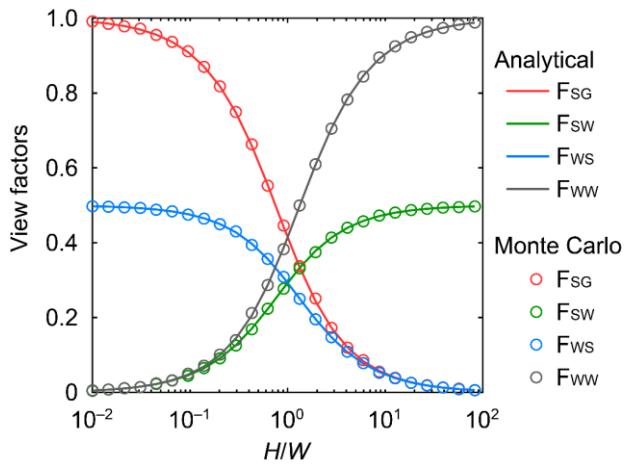
383

384 **Figure 4.** Numerical errors of view factors  $F_{SG}$  and  $F_{WS}$  with varying canyon aspect ratio  $H/W$   
 385 estimated using the Monte Carlo ray tracing method as compared to analytical solutions in street  
 386 canyons without trees. In Monte Carlo simulations, (a) and (b) use the default pseudorandom  
 387 number generator in MATLAB, whereas (c) and (d) use the Latin hypercube sampling method.

388 Note that  $N$  is the sample size for each urban facet.

389 (Figure 4 is a 2-column fitting image)

390 Figure 5 shows the comparison between the estimated view factors using the Monte  
 391 Carlo ray tracing method and their analytical solutions as functions of the canyon aspect ratio.  
 392 The proposed ray tracing method reproduces analytical solutions with nearly negligible  
 393 discrepancies. In particular, radiative view factors drastically change when the canyon aspect  
 394 ratio is in the range of 0.1–10. This partially explains the relatively high errors within the same  
 395 range observed in Fig. 4. This range is also similar to that for real cities (0.05–5 in Harman et al.  
 396 [57]; 0.2–10 in Wang [17]), suggesting that it is critical to accurately estimate view factors in  
 397 realistic urban street canyons.



398  
 399 **Figure 5.** View factors  $F_{SG}$ ,  $F_{sw}$ ,  $F_{ws}$ , and  $F_{ww}$  with varying canyon aspect ratio  $H/W$  estimated  
 400 using the Monte Carlo ray tracing method and their analytical solutions in street canyons without  
 401 trees. The sample size  $N = 10000$ .

402 (Figure 5 is a single column fitting image)

403

404 *4.2 Monte Carlo simulations and analytical solutions of radiative view factors in street canyons*  
405 *with trees*

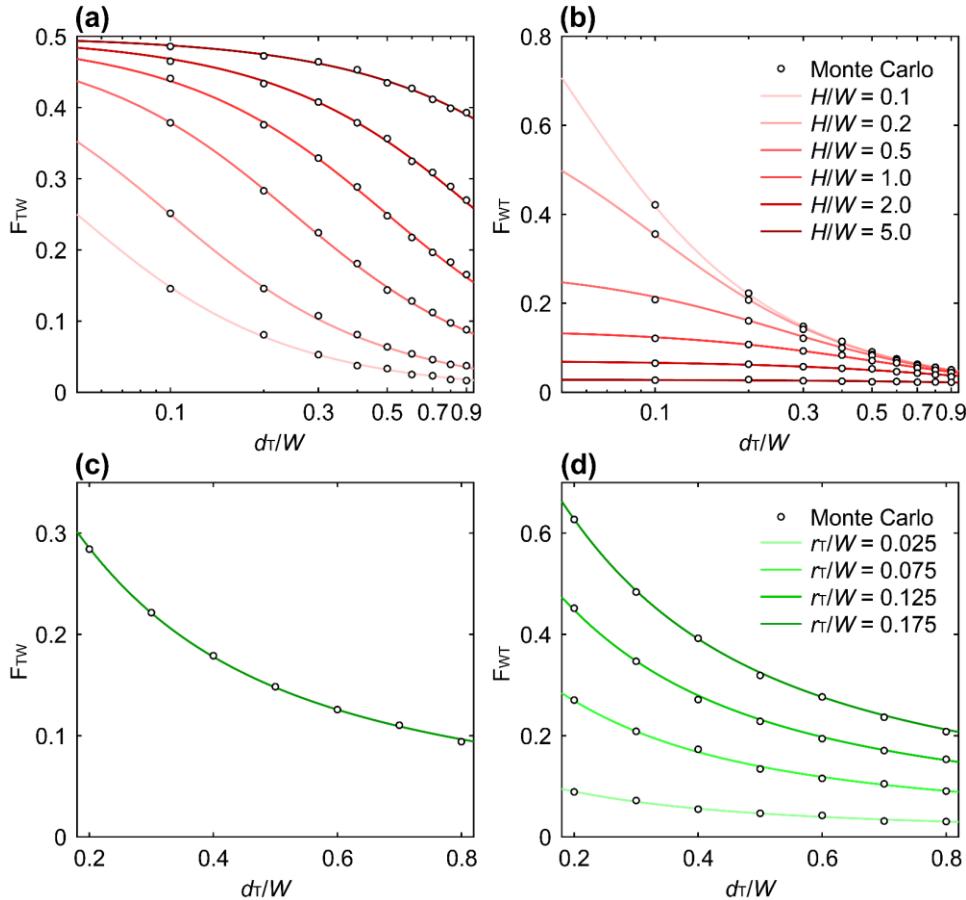
406 We evaluate the estimated view factors between one wall and trees using the Monte Carlo  
407 ray tracing method against their analytical solutions using Eqs. (7) and (8) in street canyons with  
408 one row of trees (ASLUM v3.x). Results are shown in Fig. 6 as functions of canyon aspect ratio,  
409 normalized tree crown radius ( $r_T/W$ ), and normalized wall-tree distance ( $d_T/W$ ). Across the entire  
410 spectrum of  $d_T/W$ , both radiative view factors estimated by Monte Carlo simulations are in good  
411 agreement with analytical solutions. In general, both  $F_{TW}$  and  $F_{WT}$  increase as the wall-tree  
412 distance decreases, because the hemispherical envelope of an element on the wall tends to be  
413 more occupied by trees when  $d_T$  is smaller. Deeper canyons with higher aspect ratio reduce the  
414 view factor  $F_{WT}$  as the dimension of wall increases (Fig. 6b); meanwhile, greater  $F_{TW}$  values are  
415 observed based on the reciprocity relation (Fig. 6a).  $F_{TW}$  is not affected by varying tree crown  
416 radius (see also Eq. (7)). As an example, Figure 6c shows  $F_{TW}$  for  $r_T/W = 0.175$ . In contrast, the  
417 view factor  $F_{WT}$  estimated by Monte Carlo simulations linearly declines with tree crown radius  
418 (Fig. 6d), consistent with the analytical solution based on Eq. (8). Figure 6 suggests that the  
419 proposed Monte Carlo ray tracing method can accurately predict tree-related view factors for  
420 varying geometries of both street canyons and trees.

421 We also compare the proposed method with the previous algorithm in ASLUM v3.0 [17].

422 Here we assume that  $H/W = 0.3$ ,  $r_T = 0.09W$ ,  $h_T = 0.5H$ , and  $d_T = 0.5W$  for demonstration.

423 Results are summarized in Table 2. Considering that the proposed ray tracing method is robust  
424 and accurate (Figs. 4–6), here we treat its results as the “ground truth” in comparison. Although

425 both methods can accurately predict view factors in street canyons without trees [17], clear  
 426 discrepancies are found for street canyons with trees. In particular, with a simplified and implicit  
 427 representation of tree crowns, Wang's [17] method underestimates  $F_{TW}$  by over 51% when  
 428 compared to the proposed method. This comparison, as an example, highlights the improved  
 429 performance of the proposed method when compared to its previous version [17].



430  
 431 **Figure 6.** View factors  $F_{TW}$  and  $F_{WT}$  estimated using the Monte Carlo ray tracing method and  
 432 their analytical solutions in street canyons with trees as functions of (a) and (b) canyon aspect  
 433 ratio  $H/W$  and normalized wall-tree distance  $d_T/W$  ( $r_T = 0.045W$ ), and (c) and (d) normalized tree  
 434 crown radius  $r_T/W$  and  $d_T/W$  ( $H = 0.5W$ ). The tree height  $h_T$  is  $0.5H$ .  
 435 (Figure 6 is a 1.5-column fitting image)  
 436

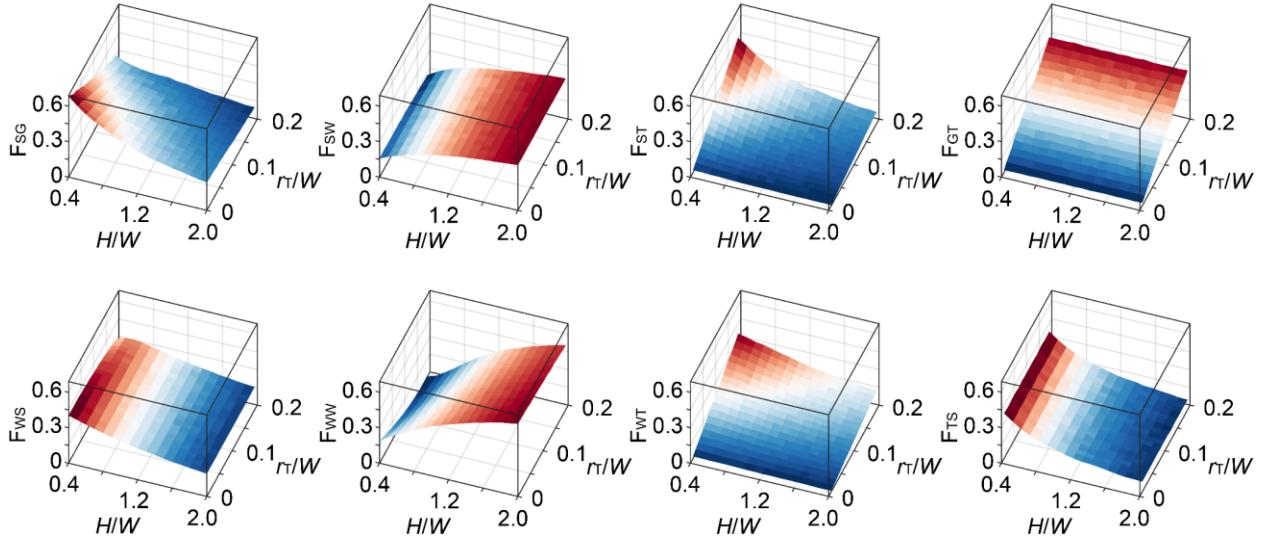
437 **Table 2.** Comparison of view factors estimated using two Monte Carlo ray tracing methods.

	$F_{SG} = F_{GS}$	$F_{SW} = F_{GW}$	$F_{ST} = F_{GT}$	$F_{WS} = F_{WG}$	$F_{WW}$	$F_{WT}$	$F_{TS}$	$F_{TG}$	$F_{TW}$
Wang [17]	0.525	0.043	0.242	0.337	0.027	0.203	0.477	0.477	0.141
The proposed method	0.531	0.120	0.229	0.399	0.024	0.177	0.410	0.404	0.093
Error	-0.006	-0.077	0.014	-0.062	0.004	0.026	0.067	0.073	0.048

438

439 *4.3 Sensitivity of radiative view factors to street canyon and tree geometry*

440 In this section, we thoroughly evaluate the sensitivity of radiative view factors to the  
 441 geometry of street canyon and trees. Note that  $d_T = 0.5W$  follows the setting in ASLUM v3.1  
 442 (Section 2). Figure 7 shows the radiative view factors as functions of canyon aspect ratio and  
 443 normalized tree crown radius. Here we set  $W = 20$  m and  $h_T = 4$  m, and calculate view factors  
 444 with changing building height (8–40 m) and tree crown radius (0–3.8 m). When  $r_T = 0$ , the  
 445 estimated view factors are identical to those in street canyons without trees, and the results of  $F_{TS}$   
 446 for  $r_T/W$  is not shown in Figs. 7 (same for Fig. 8). Among the eight view factors in Fig. 7,  $F_{SW}$ ,  
 447  $F_{WS}$ ,  $F_{WW}$ , and  $F_{TS}$  are relatively more sensitive to canyon aspect ratio than to tree crown radius.  
 448 In contrast,  $F_{GT}$  is more sensitive to tree crown radius. Other view factors ( $F_{SG}$ ,  $F_{ST}$ , and  $F_{WT}$ )  
 449 exhibit high sensitivity in shallow street canyons ( $H/W < \sim 1.2$ ). This is because the size of the  
 450 tree (especially the largest one) is relatively comparable to that of walls in shallow canyons, and  
 451 the radiation exchange between sky and ground can be largely intercepted by trees. However, the  
 452 impacts of trees diminish as street canyons deepen. Due to similar reason, a local minimum of  
 453  $F_{WS}$  is observed with the shallowest street canyon and the largest tree crown radius in Fig. 7.  
 454 With a constant canyon aspect ratio, view factors  $F_{ST}$ ,  $F_{GT}$ , and  $F_{WT}$  linearly increase with tree  
 455 crown radius, while  $F_{TS}$  remains intact (analogous to  $F_{TW}$  and  $F_{WT}$  in Fig. 6). Although the  
 456 patterns of these view factors are in general consistent with those in Wang et al. [25], some  
 457 minor discrepancies still exist, primarily because this previous study uses two rows of trees (cf.  
 458 one row herein).



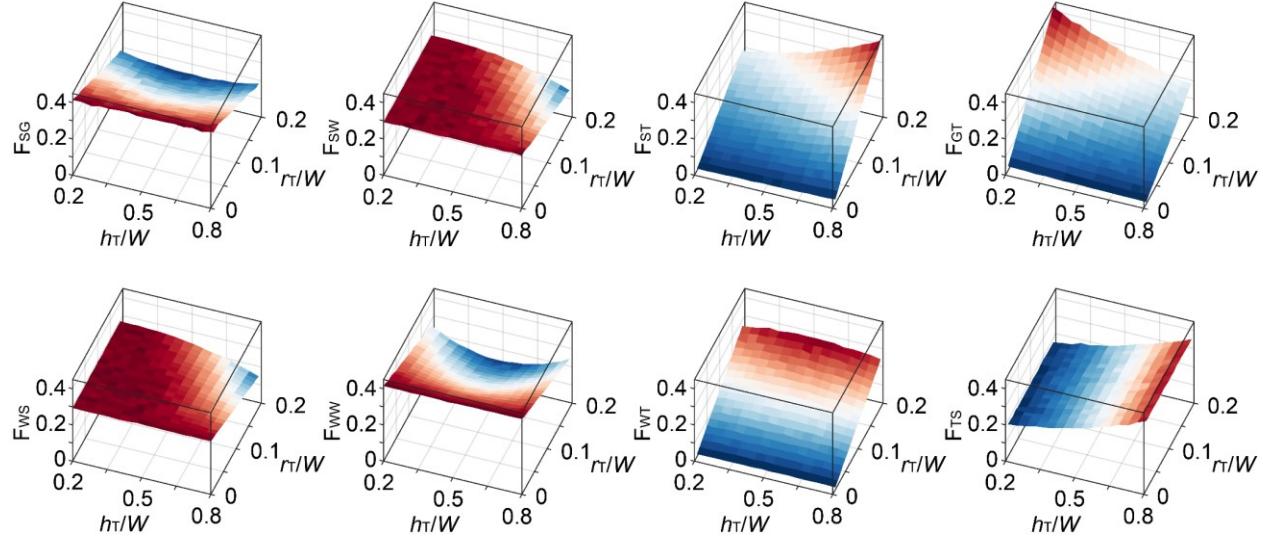
459

460 **Figure 7.** Sensitivity of radiative view factors to varying canyon aspect ratio ( $H/W$ ) and  
 461 normalized tree crown radius ( $r_T/W$ ) in ASLUM v3.1. The wall-tree distance  $h_T$  equals  $0.5W$ .  
 462 Results are color coded such that red is for high values and blue is for low values.

463 (Figure 7 is a 2-column fitting image)

464 Figure 8 shows the radiative view factors as functions of normalized tree height and  
 465 normalized tree crown radius. Here we set  $W = 20$  m and  $H = 20$  m, and calculate view factors  
 466 with changing tree height (4–16 m) and tree crown radius (0–3.8 m). A canyon aspect ratio of 1.0  
 467 retains sufficiently nonlinear sensitivity of some view factors ( $F_{SG}$ ,  $F_{ST}$ , and  $F_{WT}$ ) to the  
 468 normalized tree crown radius. As observed in Wang et al. [25], view factors between basic facets  
 469 of the street canyon enclosure, i.e.,  $F_{SG}$ ,  $F_{SW}$ ,  $F_{ws}$ , and  $F_{ww}$ , are relatively insensitive to tree  
 470 height.  $F_{sw}$  and  $F_{ws}$  are also nearly intact with varying tree crown radius when tree crowns are  
 471 close to the ground ( $h_T/W < \sim 0.5$ ), but slightly decrease when tree crowns become bigger and  
 472 higher. View factors between two parallel facets ( $F_{SG}$  and  $F_{ww}$ ) gradually drop as the tree crown  
 473 size increases. Analogous to the view factor from one wall to trees with changing wall-tree  
 474 distance (see Section 4.2), the view factors from ground/sky to trees nonlinearly change with tree

475 height but linearly increases with tree radius (see Eq. (8)). Similarly, with constant tree height  
 476 and wall-tree distance, the relationship between  $F_{WT}$  and tree crown size remains linear, which is  
 477 in line with analytical solutions in Section 3.1. The view factor from trees to sky ( $F_{TS}$ ) is  
 478 independent of tree crown radius with a given tree height. It is noteworthy that the nonlinearity  
 479 of view factors with varying geometry is not unusual (in fact is fairly common). This indicates  
 480 that the generalized linear relationships between view factors and geometric parameters (e.g.,  $H$ ,  
 481  $r_T$ , and  $h_T$ ) in Ryu et al. [18] are only applicable within certain ranges of geometry, and therefore  
 482 need be used with caution.

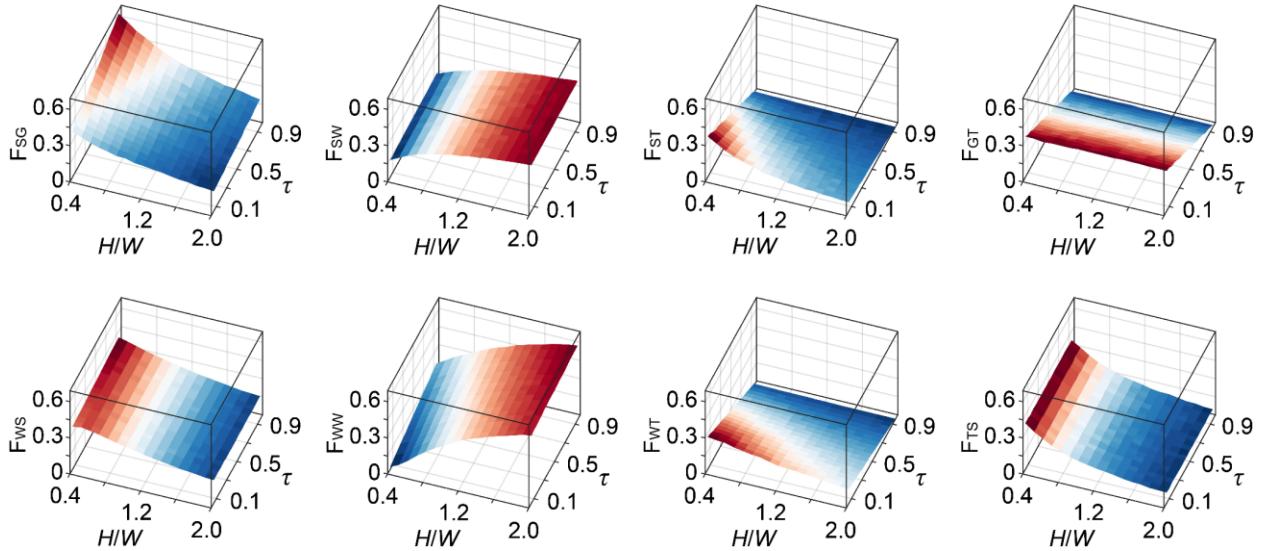


483  
 484 **Figure 8.** Same as Fig. 7 but for sensitivity to varying normalized tree height ( $h_T/W$ ) and  
 485 normalized tree crown radius ( $r_T/W$ ).  
 486 (Figure 8 is a 2-column fitting image)

#### 488 4.4 Sensitivity of radiative view factors to canopy transmittance

489 We further investigate the impacts of canopy transmittance on view factors. A set of  
 490 geometric parameters is prescribed:  $W = 20$  m,  $h_T = 4$  m,  $d_T = 10$  m ( $0.5W$ ),  $r_T = 3$  m, and

491 changing  $H$  (8–40 m). Rather than using Eq. (17) with an empirical light extinction coefficient,  
492 here we manually set transmittance to range from 0.05 (very dense tree canopy) to 0.95 (very  
493 sparse tree canopy, e.g., induced by defoliation during cold seasons). Results of eight view  
494 factors are summarized in Fig. 9. In general, all view factors are nonlinearly dependent on the  
495 building height (or aspect ratio) except for  $F_{GT}$ , which is independent of varying  $H$ . This is in line  
496 with those shown in Fig. 7. For view factors between parallel canyon facets,  $F_{SG}$  and  $F_{WW}$   
497 drastically increase with transmittance when the size of tree crown is comparable to the building  
498 height (shallow canyons). For example,  $F_{SG}$  increases by 0.283 when  $\tau$  rises from 0.05 to 0.95.  
499 Similar but relatively mild increase with transmittance is observed for  $F_{SW}$  and  $F_{WS}$ . However,  
500 these distinct changes only occur in shallow street canyons, and the dependence of  $F_{SG}$ ,  $F_{SW}$ ,  
501  $F_{WS}$ , and  $F_{WW}$  on transmittance rapidly diminishes as canyons become deeper. Among the four  
502 tree-related view factors,  $F_{TS}$  is the only one independent of transmittance, as the proportion of  
503 hemispherical envelope of tree crowns occupied by sky does not depend on the equivalent crown  
504 surface area (see also Eq. (20)).  $F_{ST}$ ,  $F_{GT}$ , and  $F_{WT}$  gradually decrease in shallow street canyons  
505 as tree canopy becomes sparser. All eight view factors become closer to their no-tree  
506 counterparts (Section 4.3) when the transmittance drops toward zero. The considerable impact of  
507  $\tau$  on view factors, especially those related to trees, highlights that canopy transmittance plays an  
508 important role in the radiation exchange among urban facets. This also suggests that the seasonal  
509 variation of foliage should be considered in long-term simulations with street trees [19,25].



510

511 **Figure 9.** Same as Fig. 7 but for sensitivity to varying canyon aspect ratio ( $H/W$ ) and canopy  
512 transmittance ( $\tau$ ).

513 (Figure 9 is a 2-column fitting image)

514

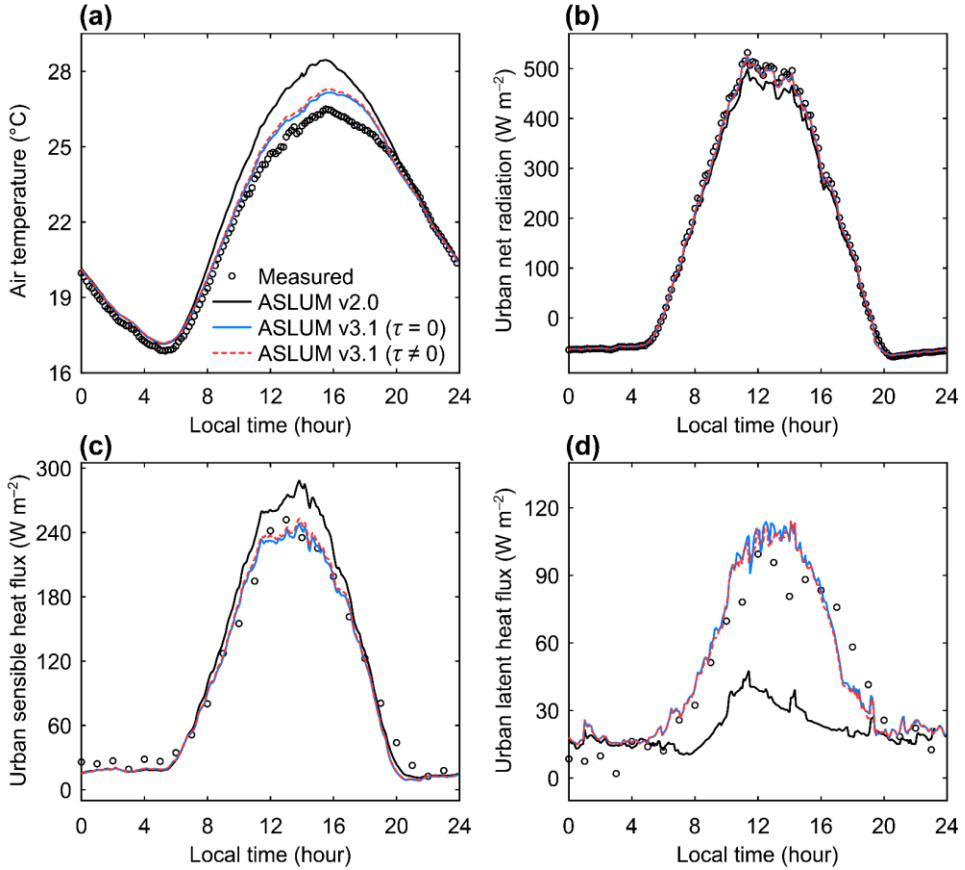
515 *4.5 Evaluation of simulations against field observations*

516 In this section, we evaluate the performance of the new ASLUM v3.1 and its previous  
517 version (ASLUM v2.0, basic v2.x) using field measurements from the Basel UrBan Boundary  
518 Layer Experiment (BUBBLE) campaign in Basel, Switzerland [68]. Specifically, we use  
519 observations from the urban Basel-Sperrstrasse site ( $47.57^\circ$  N,  $7.60^\circ$  E) with the period of  
520 observations from June 10 to July 9, 2002 (30 days). A one-day spin-up period (June 9, 2020) is  
521 used. Details of the site and instruments employed during the experiment can be found in Rotach  
522 et al. [68]. The input parameters used in simulations with different versions of ASLUM are  
523 primarily from two previous studies [18,69] (Table 3). Note that Ryu et al. [18] use two rows of  
524 street trees (tree crown radius is 1.5 m) with a tree fraction of 0.8. In ASLUM v3.1 with only one  
525 row of trees, the equivalent tree crown radius, after taking into account transmittance (LAI = 4),

526 is 3.4 m. Besides ASLUM v2.0 and v3.1, we also test a simplified version of ASLUM v3.1, in  
 527 which the transmittance is neglected. Figure 10 shows the diurnal variations in observed and  
 528 simulated street canyon air temperature, urban net radiation, urban sensible heat flux, and urban  
 529 latent heat flux averaged over 30 days. To analyze the model performance, we calculate the  
 530 coefficient of determination ( $R^2$ ), root-mean-square error (RMSE), and mean bias error (MBE)  
 531 following an international model comparison project [39,40]. The statistics are summarized in  
 532 Table 4.

533 **Table 3.** Model parameters in simulations in Section 4.4.

Variables	Value	Versions
<i>Street canyon and tree geometries</i>		
Building height (m)	14.6	v2.0 and v3.1
Road (ground) width (m)	18.2	v2.0 and v3.1
Roof width (m)	21.4	v2.0 and v3.1
Reference height of atmospheric measurements (m)	31.7	v2.0 and v3.1
Thickness of roof (m)	0.3	v2.0 and v3.1
Thickness of wall (m)	0.3	v2.0 and v3.1
Distance between tree crown center and wall (m)	9.1	v3.1
Height of tree crown center (m)	7.3	v3.1
Tree crown radius (m)	3.4	v3.1
Leaf area index	4	v3.1
Fraction of subfacets on ground (asphalt, grass)	0.65, 0.35	v2.0 and v3.1
<i>Roughness length</i>		
Roughness length for momentum for canyon (m)	1.46	v2.0 and v3.1
Roughness length for momentum for roof (m)	0.15	v2.0 and v3.1
Roughness length for heat for canyon (m)	0.146	v2.0 and v3.1
Roughness length for heat for roof (m)	0.015	v2.0 and v3.1
<i>Thermal properties</i>		
Ground surface albedo (asphalt, grass)	0.10, 0.20	v2.0 and v3.1
Roof surface albedo	0.15	v2.0 and v3.1
Wall surface albedo	0.25	v2.0 and v3.1
Leaf surface albedo	0.20	v3.1
Ground surface emissivity (asphalt, grass)	0.95, 0.93	v2.0 and v3.1
Roof surface emissivity	0.95	v2.0 and v3.1
Wall surface emissivity	0.95	v2.0 and v3.1
Leaf surface emissivity	0.95	v3.1
Thermal conductivity of ground ( $\text{W m}^{-1} \text{K}^{-1}$ ) (asphalt, grass)	1.2, 2.0	v2.0 and v3.1
Thermal conductivity of roof ( $\text{W m}^{-1} \text{K}^{-1}$ )	0.94	v2.0 and v3.1
Thermal conductivity of wall ( $\text{W m}^{-1} \text{K}^{-1}$ )	0.94	v2.0 and v3.1
Volumetric heat capacity of ground ( $\text{MJ K}^{-1} \text{m}^{-3}$ ) (asphalt, grass)	1.8, 1.3	v2.0 and v3.1
Volumetric heat capacity of roof ( $\text{MJ K}^{-1} \text{m}^{-3}$ )	1.4	v2.0 and v3.1
Volumetric heat capacity of wall ( $\text{MJ K}^{-1} \text{m}^{-3}$ )	1.4	v2.0 and v3.1



534

535 **Figure 10.** Simulated (a) street canyon air temperature, (b) urban net radiation, (c) urban sensible  
 536 heat flux, and (d) urban latent heat flux using ASLUM v2.0 (without trees), v3.1 with  $\tau = 0$ , and  
 537 v3.1 with  $\tau \neq 0$  evaluated against measurements.

538 (Figure 10 is a 1.5-column fitting image)

539 On average, ASLUM v2.0 slightly overestimates the canyon air temperature (MBE =  
 540  $0.86^{\circ}\text{C}$ ) and the urban sensible heat flux (MBE =  $5.19 \text{ W m}^{-2}$ ) while underestimates the urban  
 541 net radiation (MBE =  $-11.38 \text{ W m}^{-2}$ ). However, the discrepancy in the simulated latent heat  
 542 fluxes is relatively large (MBE =  $-20.62 \text{ W m}^{-2}$ ), primarily due to the omission of  
 543 evapotranspiration from urban trees. The differences between simulations and observations of  
 544 turbulent heat fluxes are even greater during the day (RMSE =  $\sim 47 \text{ W m}^{-2}$ ) than over the diurnal  
 545 cycle (Fig. 10c and d) as the daytime surface energy balance is dominated by solar radiation.

546 Nevertheless, the performance of ASLUM v2.0 is in general consistent with and even better than  
547 the median performance of 32 urban land surface models in Grimmond et al. [39].

548 **Table 4.** Summary of performance statistics using different versions of ASLUM. Note that units  
549 are for RMSE and MBE, and the number of data points  $n = 8641$  for each variable.

	$R^2$	RMSE	MBE
<i>ASLUM v2.0 (without trees)</i>			
Street canyon air temperature (°C)	0.98	1.25	0.86
Urban net radiation (W m <sup>-2</sup> )	1.00	19.01	-11.38
Urban sensible heat flux (W m <sup>-2</sup> )	0.87	40.73	5.19
Urban latent heat flux (W m <sup>-2</sup> )	0.24	40.34	-20.62
<i>ASLUM v3.1 (with trees and <math>\tau = 0</math>)</i>			
Street canyon air temperature (°C)	0.99	0.63	0.34
Urban net radiation (W m <sup>-2</sup> )	1.00	7.95	-2.56
Urban sensible heat flux (W m <sup>-2</sup> )	0.86	36.83	-4.80
Urban latent heat flux (W m <sup>-2</sup> )	0.56	30.69	1.00
<i>ASLUM v3.1 (with trees and <math>\tau = 0.087</math>)</i>			
Street canyon air temperature (°C)	0.99	0.69	0.40
Urban net radiation (W m <sup>-2</sup> )	1.00	8.36	-3.13
Urban sensible heat flux (W m <sup>-2</sup> )	0.87	36.85	-3.27
Urban latent heat flux (W m <sup>-2</sup> )	0.56	30.28	0.23

550

551 After including trees into ASLUM v3.1, clear improvement is observed in all three  
552 statistics of all four model outputs (Fig. 10 and Table 4). The most significant improvement is in  
553 latent heat flux (Fig. 10d), of which the RMSE decreases from 40.34 W m<sup>-2</sup> to 30.28 W m<sup>-2</sup>. The  
554 considerable underestimate of latent heat flux in ASLUM v2.0 is largely mitigated by the  
555 inclusion of trees: the MBE in latent heat flux in ASLUM v3.1 is 0.23 W m<sup>-2</sup>. As a result, the  
556 systematic overestimate in sensible heat flux predicted by ASLUM v2.0 is also reduced via the  
557 changes in energy partitioning, especially during the daytime (Fig. 10c). Despite the minor  
558 overestimation, the predicted daytime air temperature is lower than that in ASLUM v2.0,  
559 showing the cooling effect of urban trees from shading and transpiration. The difference in the  
560 performance of ASLUM v2.0 and v3.1 highlights that the vegetation modeling plays an essential  
561 role in the simulation of urban surface energy flux exchanges [39]. It is noteworthy that the

562 performance of ASLUM v3.1 is relatively better than that of Ryu et al.'s [18] model, which can  
563 be attributable to the more accurate ray tracing algorithm, the iteratively determined canyon air  
564 temperature and humidity, and the absence of artificial energy deficit/excess redistribution for  
565 tree-tree interactions in the ASLUM v3.1.

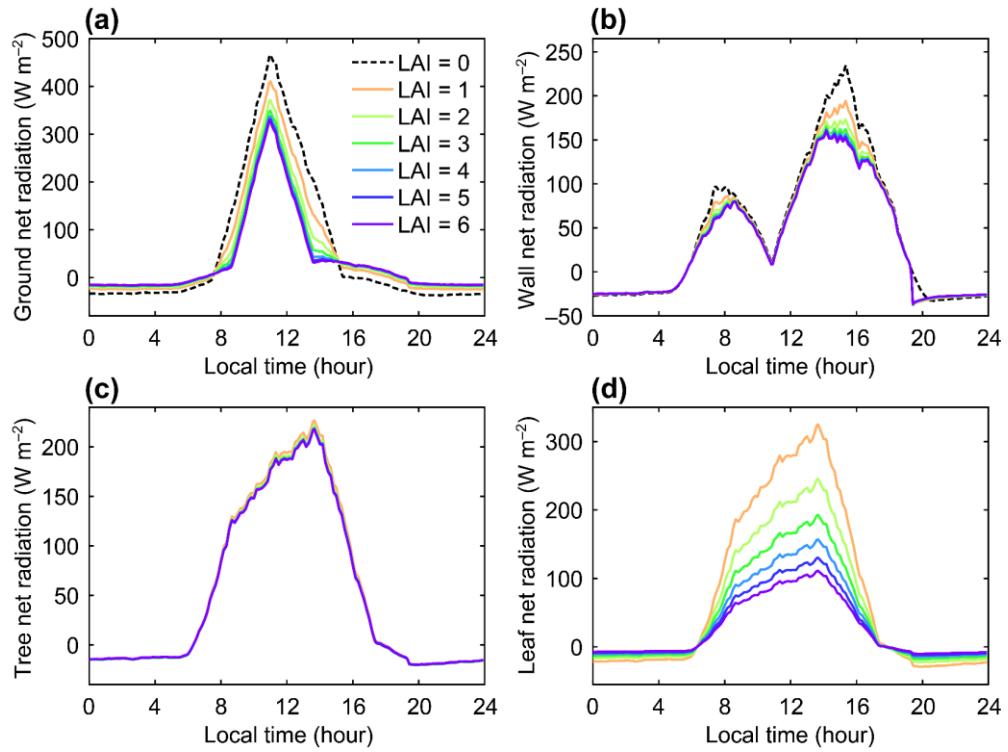
566 On the other hand, the impact of transmittance on the performance of ASLUM v3.1 with  
567 the input parameters in Table 3 is relatively weak, owing to the small transmittance of the dense  
568 tree canopy ( $\tau = 0.087$ ) during summer. The statistics of the simulations using two versions of  
569 ASLUM v3.1 are quite close. Nevertheless, discrepancies in the simulated latent and sensible  
570 heat fluxes are still recognized. In particular, assuming the tree crowns to be opaque ( $\tau = 0$ )  
571 results in slightly overestimated urban latent heat flux (see Eq. (37) and (38)). For example,  
572 including transmittance can reduce the MBE of daytime urban latent heat flux from  $2.37 \text{ W m}^{-2}$   
573 to  $1.19 \text{ W m}^{-2}$ . Such difference/improvement can be much greater when the transmittance of tree  
574 crowns is higher (Section 5.1).

575

## 576 **5. Model applications and discussion**

### 577 *5.1 Radiation exchange and turbulent heat fluxes influenced by leaf area index*

578 In this section, we evaluate the impacts of varying leaf area index and the associated  
579 transmittance on urban radiation exchange and turbulent heat fluxes. The input parameters are  
580 identical to those in Table 3 except for the LAI of trees (0–6 herein). We use ASLUM v2.0 for  
581 the case with LAI = 0 (without trees; reference case) and ASLUM v3.1 for the other five cases  
582 (LAI = 1–6). The simulated radiation budgets for different facets are shown in Fig. 11, and the  
583 simulated air temperature, net radiation, and turbulent heat fluxes are shown in Fig. 12. Note that  
584 tree net radiation is converted to leaf net radiation using Eqs. (37) and (38).



585

586 **Figure 11.** Simulated net radiations of (a) ground, (b) wall, (c) tree, and (d) leaf with varying

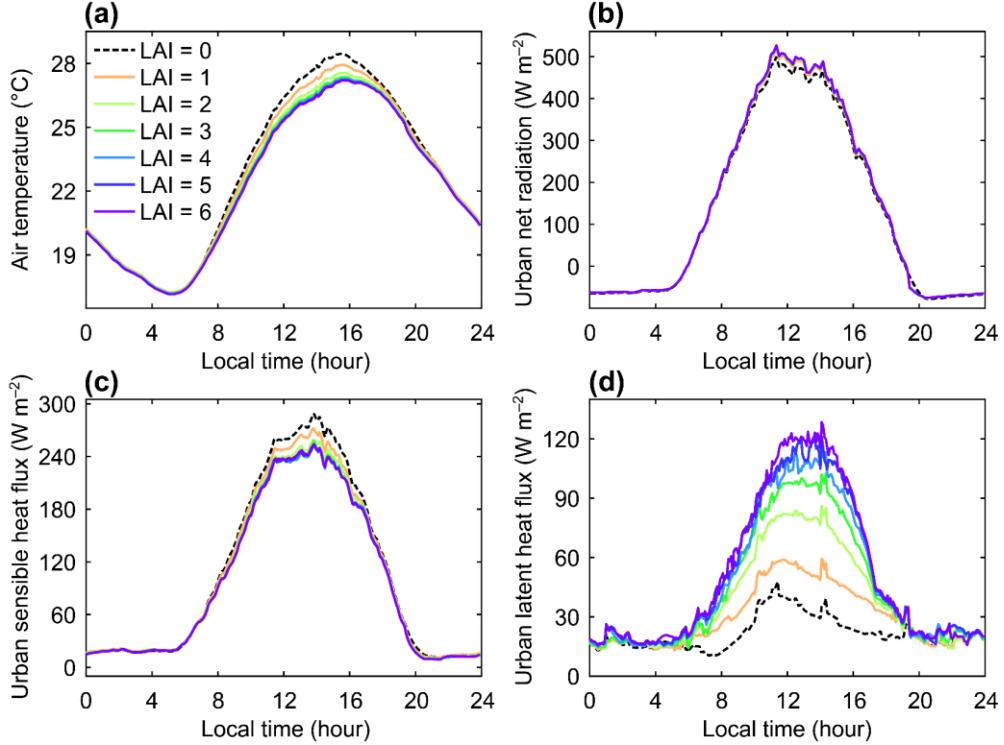
587

leaf area index of trees.

588

(Figure 11 is a 1.5-column fitting image)

589



590

591 **Figure 12.** Simulated (a) street canyon air temperature, (b) urban net radiation, (c) urban sensible  
 592 heat flux, and (d) urban latent heat flux with varying leaf area index of trees.  
 593 (Figure 12 is a 1.5-column fitting image)

594 As LAI of trees increases, the ground net radiation in general decreases during the  
 595 daytime except for a few hours after sunrise and before sunset (Fig. 11a), primarily due to the  
 596 strong shading effect of tree canopy [8,70]. Compared to the reference case (LAI = 0), urban  
 597 trees with LAI = 6 reduce the average daytime ground net radiation by  $42.58 \text{ W m}^{-2}$  and the peak  
 598 value by  $139.31 \text{ W m}^{-2}$  (maximum reduction is  $172.69 \text{ W m}^{-2}$ ). However, increasing ground net  
 599 radiation with LAI is observed at night, resulting from the radiative trapping effect of trees: the  
 600 upward longwave radiation emitted from ground is partially blocked by tree canopy [25,41]. The  
 601 average nighttime ground surface temperature in the case with LAI = 6 is even slightly warmer  
 602 than in the reference case ( $0.4 \text{ }^{\circ}\text{C}$  higher). Similar reductions of daytime net radiation are also  
 603 found for walls (Fig. 11b). On average, the daytime wall net radiation decreases by  $17.71 \text{ W m}^{-2}$

604 as LAI increases from 0 to 6. The radiative trapping effect of trees on nighttime wall net  
605 radiation is relatively weaker than its ground counterpart. Note that the abrupt changes and the  
606 peaks of net radiation in Fig. 11 are determined by the shadow cast by walls and/or trees. The  
607 impact of varying LAI on the net radiation of trees is very marginal (Fig. 11c), as the  
608 determinant of this variable (direct shortwave radiation) is independent of transmittance (see Eq.  
609 (20)). But the difference in tree net radiation influenced by LAI and transmittance becomes much  
610 clearer when averaged over the leaf plan area (see Eqs. (37) and (38)). The mean daytime net  
611 radiation of leaf with  $LAI = 6$  ( $\tau = 0.026$ ) decreases by  $83.71 \text{ W m}^{-2}$  when compared to the case  
612 with  $LAI = 1$  ( $\tau = 0.543$ ) (the reduction in peak value is  $213.87 \text{ W m}^{-2}$ ). The increasing LAI and  
613 diminishing transmittance jointly contribute to the observed changes in Fig. 11d. Note that the  
614 change in the impact of LAI gradually attenuates as it increases [18], resulting from the  
615 exponential nature of the  $LAI-\tau$  relationship in Eq. (17).

616 The presence of street trees effectively lowers the daytime canyon air temperature.  
617 Compared to the reference case, the case with the densest tree canopy ( $LAI = 6$ ) reduced the  
618 maximum daytime air temperature by  $\sim 1.3 \text{ }^{\circ}\text{C}$  (Fig. 12a). Owing to the reduced net radiation and  
619 surface temperature of canyon facets (ground and walls), the peak urban sensible heat flux of the  
620 same case is  $34.91 \text{ W m}^{-2}$  lower than in the case without trees (Fig. 12c), and the peak daytime  
621 ground and wall temperatures are reduced by  $4.69 \text{ }^{\circ}\text{C}$  and  $3.81 \text{ }^{\circ}\text{C}$ , respectively. Meanwhile, the  
622 average urban latent heat flux is enhanced by  $43.75 \text{ W m}^{-2}$  (maximum increase is  $92.79 \text{ W m}^{-2}$ ;  
623 Fig. 12d). The reductions in air temperature and sensible heat flux, as well as the increases in  
624 latent heat flux, are nonlinearly dependent on LAI. In contrast, the changes in urban net radiation  
625 are relatively marginal (Fig. 12b). These changes clearly suggest that the synergistic interplay of  
626 radiative shading and evapotranspiration is the underlying mechanism of the observed cooling

627 effect [2,6]. The results in Figs. 11 and 12 have strong implications for the mitigation of urban  
628 heat stress during hot seasons. For example, the reduced air temperature, surface temperature,  
629 and net radiation of ground are beneficial to thermal comfort, especially at the pedestrian level.  
630 The decreased wall net radiation and surface temperature also suggest a reduction in the  
631 conductive heat flux into buildings, which plays a vital role in building energy saving [8].

632

### 633 *5.2 Radiation exchange and turbulent heat fluxes influenced by tree crown radius*

634 We further examine the impacts of varying tree crown radius on urban radiation  
635 exchange and turbulent heat fluxes. Similarly, we use input parameters identical to those in Table  
636 3 except for the tree crown size. Here the radius ranges from 0 m (without trees; reference case)  
637 to 6 m. Results are shown in Figs. 13 and 14.

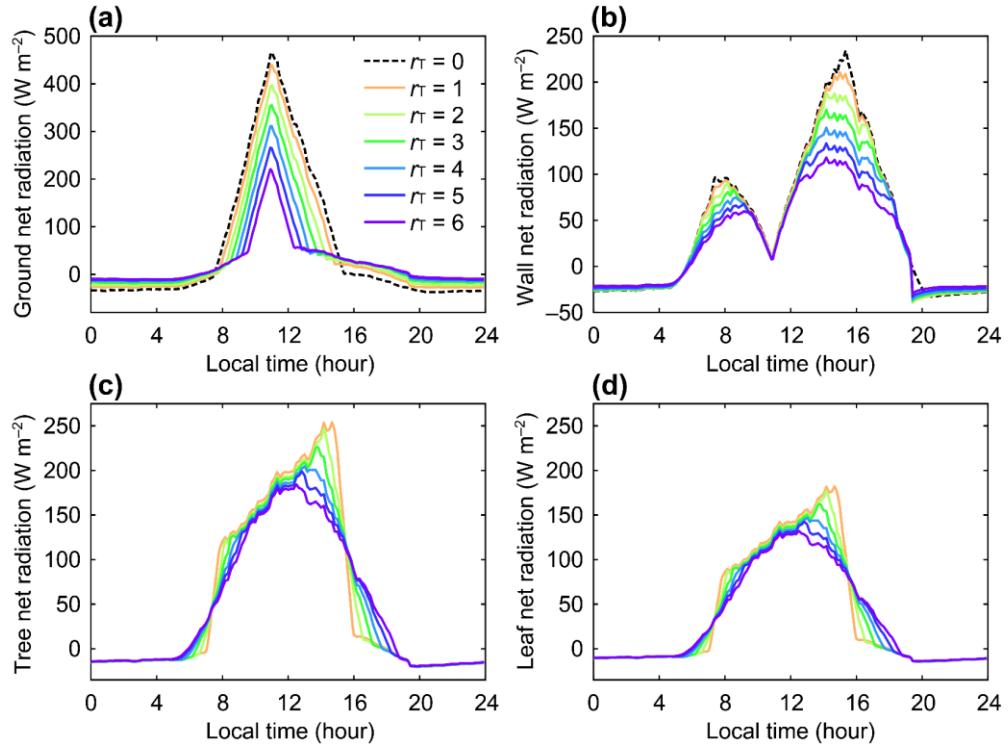
638 Compared to the results in Section 5.1, increasing the tree crown size can more  
639 effectively reduce the net radiation of ground and wall via shading. The largest tree crowns ( $r_T =$   
640 6 m) on average reduce the daytime net radiation of ground and wall by  $64.80 \text{ W m}^{-2}$  and  $32.25$   
641  $\text{W m}^{-2}$ , respectively (compared to the reference case; Fig. 13a and b). The reduction of peak  
642 values with increasing tree crown size is nearly linear; for example, the reduction of peak net  
643 radiation for ground is  $\sim 41.8 \text{ W m}^{-2}$  per meter of increase in tree crown radius ( $R^2 = 0.996$ ).

644 Larger tree crowns can enhance the nighttime radiative trapping effect, leading to greater  
645 increases in average net radiation of ground and wall (e.g., an increase of  $25.02 \text{ W m}^{-2}$  in the  
646 average ground net radiation for the case with  $r_T = 6 \text{ m}$  when compared to the reference case).  
647 Increasing tree crown radius in general reduces the tree net radiation during the daytime (Fig.  
648 13c). The peak reduction in the tree net radiation occurs in the afternoon, as small tree crowns

649 are strongly affected by the shadow cast by walls. With a constant transmittance, the change of  
650 leaf net radiation is proportional to that of tree net radiation (Fig. 13d; see Eqs. (37) and (38)).

651 The increasing cooling effect of trees with greater tree crown size is also nearly linear  
652 (Fig. 14a): a reduction of 0.36 °C in peak canyon air temperature per meter of increase in tree  
653 crown radius ( $R^2 = 0.997$ ). On average, the daytime canyon air temperature for the case with  $r_T =$   
654 6 m is 1.35 °C lower than that for the reference case. The reductions in peak daytime surface  
655 temperatures of ground and walls are even greater: 8.87 °C and 6.17 °C, respectively, which are  
656 attributable to the shading of trees. The change in nighttime temperatures depends on the tree  
657 crown size. For trees with a crown radius lower than 4 m, the radiative trapping effect leads to a  
658 higher minimum nighttime air temperature than that in the reference case. But for air temperature  
659 in street canyons with bigger tree crowns, the cooling effect dominates its entire diurnal cycle. In  
660 contrast, higher ground surface temperatures are found in all cases with trees as compared to the  
661 reference case, consistent with field observations in different cities [71,72]. The nighttime  
662 warming effect observed here is different from the results using the coupled WRF–ASLUM v3.0  
663 [24,25], primarily because of the simplified tree module (see Section 2) when coupled with the  
664 existing WRF-urban modeling system [52]. This highlights that more realistic repartitioning of  
665 sensible and latent heat fluxes is of key importance to improve the representation of trees in  
666 urban canopy models, as inaccurate repartitioning will likely lead to inaccurate estimates of the  
667 cooling effect, especially at night. Urban net radiation shows minor changes with different tree  
668 crown sizes (Fig. 14b). As a result of shading and evapotranspiration, the urban sensible heat  
669 flux and latent heat flux gradually decreases and increases, respectively, as tree crowns become  
670 larger. On the other hand, the increase in latent heat flux gradually plateaus when tree crown

671 radius is greater than 4 m, suggesting that the cooling effect of large trees is mainly attributed to  
672 radiative shading.

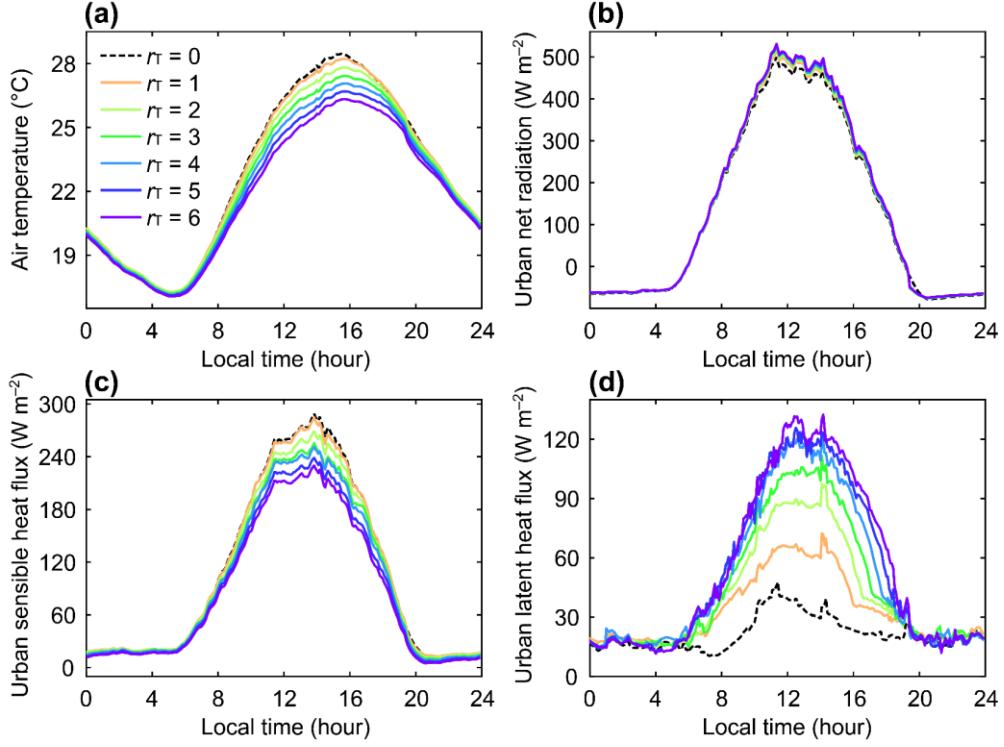


673

674 **Figure 13.** Same as Fig. 11 but with varying tree crown sizes (unit of  $r_T$ : m).

675 (Figure 13 is a 1.5-column fitting image)

676



677

678 **Figure 14.** Same as Fig. 12 but with varying tree crown sizes (unit of  $r_T$ : m).

679 (Figure 14 is a 1.5-column fitting image)

680

681 **6. Concluding remarks**

682 We develop a new Monte Carlo ray tracing method for radiative heat exchange in urban  
 683 street canyons with trees. The proposed method is able to simulate the impact of canopy  
 684 transmittance on radiative view factors. Results are evaluated against analytical solutions,  
 685 suggesting the robustness and accuracy of the proposed model. Sensitivity tests show that the  
 686 view factors between urban facets and trees are more sensitive to the tree crown size, canyon  
 687 geometry, and transmittance of foliage, but less sensitive to tree height. This new ray tracing  
 688 method is then incorporated into a new single-layer urban canopy model (ASLUM v3.1), which  
 689 enables the realistic numerical representation of radiative shading, evapotranspiration, and root  
 690 water uptake of urban trees. The performance of ASLUM v3.1 is evaluated against field

691 measurements. Compared to its previous version (ASLUM v2.0), the new urban canopy model  
692 exhibits clear improvements in accuracy (especially for latent heat flux). We also apply the  
693 model to investigate the effect of trees on radiation exchange, turbulent heat fluxes, and  
694 temperatures. Results show that trees with higher LAI and greater crown size can more  
695 effectively reduce net radiation of wall and ground, sensible heat flux, and canyon air  
696 temperature with enhanced latent heat flux via shading and evapotranspiration, but may exhibit  
697 slight warming effect at night due to radiative trapping.

698 It is noteworthy that for simplicity, the transmittance of urban trees in the proposed  
699 model is a lumped parameter based on an empirical equation, and ASLUM v3.1 described here  
700 simulates tree evapotranspiration with a few assumptions. The current design in ASLUM v3.1  
701 does not allow trees higher than the buildings. Street canyons with different aspect ratios  
702 (especially high aspect ratios) should be evaluated in future applications of the proposed model.  
703 The influence of trees on canyon wind and turbulent transport (e.g., [33,41]) is another important  
704 component that should be included in future versions of ASLUM. More complex physiological  
705 processes of urban trees (e.g., stomatal closure and biogenic carbon exchange [73]) should also  
706 be considered in future development for simulations under diverse climate conditions. However,  
707 the proposed ray tracing method is sufficiently generic with high accuracy and reliability, so that  
708 it can be readily modified to simulate radiation exchange of trees with vertical canopy profiles  
709 (e.g., [35,36]) and different shapes (e.g., elliptical or prismatic [74,75]), as well as the impact of  
710 airborne pollutants (as participating media [42]) in heavily polluted street canyons. In addition,  
711 the proposed ASLUM v3.1 remains simple in its geometry and computationally economic,  
712 leaving open the possibility of being incorporated into the WRF platform for online simulations  
713 of land–atmosphere interactions. In particular, if seasonal profiles of LAI and transmittance are

714 provided, the new ASLUM v3.1 will enable more realistic simulations of trees with phenological  
715 variations. Such simulations can provide critical information in terms of selecting tree species  
716 and locations in urban planning through systematic evaluation of how trees affect heat stress,  
717 seasonal pedestrian thermal comfort, and building energy consumptions.

718

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724

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