

# Tailoring Surface Hydrophobicity of Commercial Polyimide by Laser-Induced Nanocarbon Texturing

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*The growth of laser-induced nanocarbons, referred to here as laser-induced nanocarbon (LINC) for short, directly on polymeric surfaces is a promising route toward surface engineering of commercial polymers. This paper aims to demonstrate how this new approach can enable achieving varied surface properties based on tuning the nanostructured morphology of the formed graphitic material on commercial polyimide (Kapton) films. We elucidate the effects of tuning laser processing parameters on the achieved nanoscale morphology and the resulting surface hydrophobicity or hydrophilicity. Our results show that by varying lasing power, rastering speed, laser spot size, and line-to-line gap sizes, a wide range of water contact angles are possible, i.e., from below 20 deg to above 110 deg. Combining water contact angle measurements from an optical tensiometer with LINC surface characterization using optical microscopy, electron microscopy, and Raman spectroscopy enables building the process–structure–property relationship. Our findings reveal that both the value of contact angle and the anisotropic wetting behavior of LINC on polyimide are dependent on their hierarchical surface nanostructure which ranges from isotropic nanoporous morphology to fibrous morphology. Results also show that increasing gap sizes lead to an increase in contact angles and thus an increase in the hydrophobicity of the surface. Hence, our work highlight the potential of this approach for manufacturing flexible devices with tailored surfaces.*

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## 1 Introduction

Although the applications of commodity polymers are ubiquitous, controlling their surface properties in a scalable and affordable process is still challenging. This is particularly important for emerging applications of flexible device manufacturing. Recently, it has been shown that nanoscale graphitic structures can be synthesized by directly lasing of polyimide, a popular polymer, with commercially available low-cost infrared (IR) lasers [1]. The resulting material has been described in literature as: laser-induced porous graphene [1], laser induced graphene [2–4], laser-induced hierarchical carbon [5], or simply graphitic carbon [6]. Here, we use the term laser-induced nanocarbon (LINC) to describe the material, which is a more representative term for to the diversity of the generated nanoscale carbon material types formed by this process, which include fibers and sheets [7]. These LINC structures have been shown to exhibit excellent electrical and thermal conductivities as well as high surface area. In addition, different morphologies have been observed at the microscale for LINC materials, ranging from porous to fibrous [7]. Accordingly, wide-reaching potential applications of LINC such as anti-fouling [8], anti-icing [9], and antimicrobial [10] surfaces have been investigated.

Recent research has also shown that LINC surface properties depend on lasing parameters such as laser power and speed [4,11,12]. Lamberti et al. [11] has shown that by changing the laser speed and power, different morphologies of polyimide-based LINC lines can be achieved. The different line morphologies, described as sheets, needles, and porous had superhydrophobic contact angles. Tiliakos and coworkers [12] modulated laser power, scan rate, and step interval at a fixed laser spot size to

control the morphology of 1 cm<sup>2</sup> LINC areas. Their results have shown that LINC areas range from superhydrophobic to hydrophilic. They explain their results using topographical observations on the samples like hierarchical structures that combine macro-scale and microscale roughness leading to superhydrophobic results and porous structures leading to hydrophilic results. Nevertheless, no anisotropy of contact angle was observed in that study. Additionally, Li et al. [4] have shown that by changing the lasing environment using a gas-controlled chamber, the contact angle between water droplets and LINC areas can be switched between superhydrophobic (>150 deg) and superhydrophilic by tuning the oxygen content in different gas atmospheres.

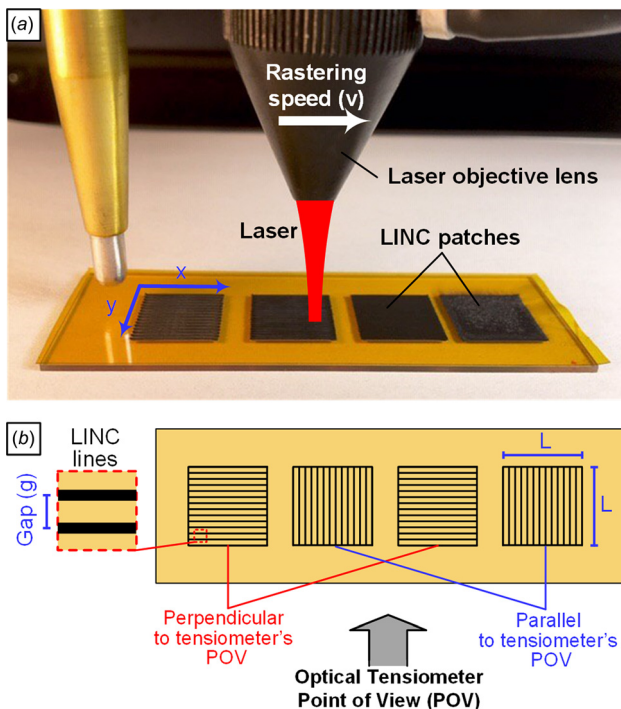
In this paper, we demonstrate the capability of tuning the anisotropic contact angles of LINC formed directly on the surfaces of the commercial polyimide films (Kapton) by lasing in air. We explore the effect of different laser processing parameters including laser power, speed, spot size, and rastering line-to-line gaps on water contact angle measured in two orthogonal directions. As a result, we are able to tune the surface properties in a large range of contact angles ranging from below 20 deg to above 110 deg. Importantly, this tunability can be achieved by only changing the lasing rastering parameters in atmospheric conditions (i.e., in air environment), which greatly simplifies the process since no special controlled-gas chamber is needed. Moreover, we propose a mechanism to explain the observed difference in contact angle measurements at different parameters by correlating contact angle with scanning electron microscopy (SEM) observations of the LINC areas.

## 2 Methods

**2.1 Sample Preparation.** The experiment was conducted by laser scribing on polyimide (PI) tape, also referred to as Kapton, (Grainger, Cat. No. 15C616, thickness: 3.5 mil), which was applied to a glass slide with a rubber roller to eliminate air bubbles. The glass slide maintains the flatness of the polyimide film

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**Fig. 1** (a) Photograph of the setup showing both the laser objective lens and the sample of polyimide tape on glass with four LINC patches on it and (b) schematic of each polyimide-covered glass slide with LINC patches at different orientations of rastering

during lasing. Prior to lasing, the polyimide surface is chemically cleaned by rinsing with acetone, followed by rinsing with isopropyl and quickly drying using a compressed air gun.

**2.2 Laser-Induced Nanocarbon Processing.** A commercial CO<sub>2</sub> laser system (Full Spectrum Laser Pro-Series 20 × 12, 1.5 in. focus lens) with 10.6  $\mu\text{m}$  wavelength and 45 W laser power, was used for all lasing experiments. The system allows tuning the power by controlling the laser current. The knife edge method [13] was used to estimate the beam spot size at different points along its z-axis, utilizing a CO<sub>2</sub> laser power meter (HLP-200, Changchun Laser Optoelectronics Technology Co., Ltd.). The beam waist diameter ( $2w_{0x}$ ) based on  $(1/e^2)$  was measured to be 220  $\mu\text{m}$ . The beam radius was changed by adjusting the distance between the sample surface and beam waist. The laser objective lens is mounted on an XYZ stage with a maximum rastering speed of 500 mm/s.

**2.3 Experiment Design.** As shown in Fig. 1(a), each slide has four square patches (1.27 cm × 1.27 cm) that are lased at different conditions. A single LINC patch is formed by laser rastering that proceeds as following: lasing in the positive x-direction a distance ( $L$ ) at speed  $v$ , then shifting by an increment ( $g$ ) in the y-direction, followed by lasing in the negative x-direction by the same distance ( $L$ ) (Fig. 1(b)). This sequence is repeated until the square is completed. The laser machine input design file is generated by programming a MATLAB script with lines and a certain number of pixels gap between lines representing a single patch.

Experiments in this study were carried out by varying laser powers ( $P$ ) between 12 W and 28 W, speed ( $v$ ) between 350 mm/s and 500 mm/s, and the line-to-line gap ( $g$ ) between 0 pixels, and 7 pixels (with increments of 3), where one pixel represents a shift of 50.8  $\mu\text{m}$  (Fig. 1). Finally, the patches were rotated 90 deg for a total of two orientations in order to investigate contact angle anisotropy (Fig. 1(b)). The complete lasing and measurements parameters used in this study are presented in Table 1.

**Table 1** Laser parameters used in this study

Parameter	Values
Speed ( $v$ ) (mm/s)	500, 310
Power (W)	12, 28
Gap ( $g$ ) ( $\mu\text{m}$ )	50.8, 203.2, 304.8, 406.4
Spot size radius ( $w_0$ ) ( $\mu\text{m}$ )	100, 300
Orientation of optical tensiometer measurements relative to rastering direction	Perpendicular, Parallel

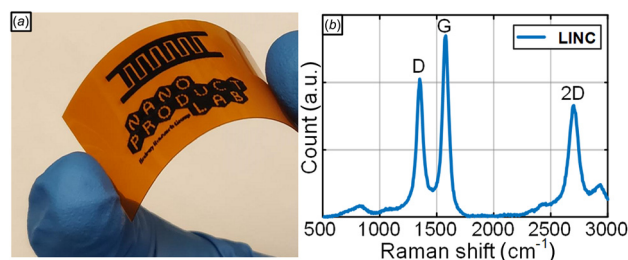
**2.4 Contact Angle Measurements.** Quantitative results were obtained by measuring the Young-Laplace's contact angle using a Biolin Scientific Optical Tensiometer. The process included ejecting four 5  $\mu\text{l}$  water droplets on each sample and recording the results at  $\approx 7$  frames per second for 20 s. Afterward, the software OneAttention was used to analyze each droplet by fitting the contact angle (CA) of the droplet for each of the 140 frames. The average of the 140 contact angles was then recorded as the contact angle for each measured droplet. Four drops are used for each condition on the same patch and the average and standard deviation of the contact angle are recorded.

**2.5 Morphology Characterization.** To characterize the morphology of the LINC patches, SEM images were taken with a Zeiss SIGMA VP Scanning Electron Microscope. Moreover, carbon structure was also characterized by Raman spectroscopy measurements (Xplora, Horiba Scientific, Kyoto, Japan) using the 638 nm excitation wavelength.

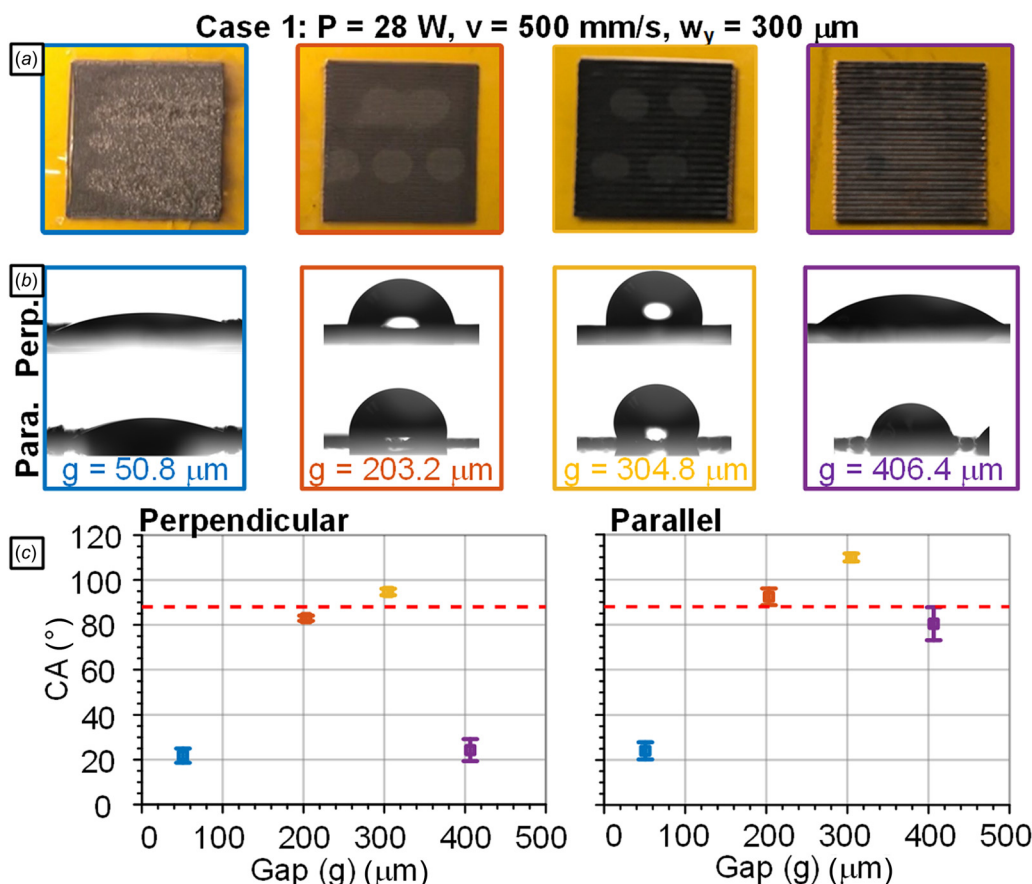
### 3 Results

Before lasing of the polyimide samples, the CA of water on the native surface was measured, in order to be used as a control measurement for this study. Water CA on polyimide was measured to have an average of 88 deg. The experimental study is divided into eight cases, each with different parameters as listed in Table 1. First, we demonstrate the capability of our approach to generate patterns of LINC on flexible polyimide films, as depicted in Fig. 2(a). Figure 2(b) shows the Raman spectrum collected from one of the laser patches, exhibiting the characteristic G, D and 2D peaks associated with  $\text{sp}^2$  carbon, which confirms the formation of high quality graphitic carbon.

**3.1 Case 1 ( $P = 28\text{ W}$ ,  $v = 500\text{ mm/s}$ ,  $w_0 = 300\text{ }\mu\text{m}$ ).** Figure 3 illustrates the results at lasing power of 28 W, rastering speed of 500 mm/s, and laser spot size of 300  $\mu\text{m}$ . The  $g = 50.8\text{ }\mu\text{m}$  case exhibits a gray color with no visible periodicity in the patch, the color of the patch gets darker with increasing gap up to  $g = 304.8\text{ }\mu\text{m}$ . At  $g = 406.4\text{ }\mu\text{m}$ , the line patterns are visible but the color is not as dark. At  $g = 50.8\text{ }\mu\text{m}$ , the contact angle measured in the perpendicular and parallel directions are very low at around 20 deg. With increasing gap, the angle increases to be higher than the control value, with the value in the parallel direction being higher than the perpendicular direction until it drops



**Fig. 2** (a) Image illustrating direct writing of LINC on flexible substrates and (b) Raman spectra of LINC sample



**Fig. 3** (a) Top view image of each patch for case 1 (lasing parameters  $P = 28 \text{ W}$ ,  $v = 500 \text{ mm/s}$ ,  $w_y = 300 \mu\text{m}$ ), (b) optical tensiometer images of water droplets, and (c) plots of contact (CA) at different gap values. Horizontal dashed line represents control CA. Error bars represent  $\pm$  standard deviation.

for both directions at  $g = 406.4 \mu\text{m}$ . At that point, the average perpendicular contact angle drop to around 20 deg, while the parallel contact angle drops slightly lower than the control. Hence, the patch with  $406.4 \mu\text{m}$  gap exhibits the most CA anisotropy.

**3.2 Case 2 ( $P = 28 \text{ W}$ ,  $v = 350 \text{ mm/s}$ ,  $w_y = 300 \mu\text{m}$ ).** Figure 4 illustrates the results at lasing power of 28 W, rastering speed of 350 mm/s, and laser spot size of  $300 \mu\text{m}$ . These are the same parameters of case 1, except at a lower speed indicating higher fluence delivered to the polyimide during lasing. The  $g = 50.8 \mu\text{m}$  also exhibits a gray color with no visible periodicity in the patch, the color of the patch gets darker up to a maximum at  $g = 304.8 \mu\text{m}$ . At  $g = 304.8 \mu\text{m}$  and  $g = 406.4 \mu\text{m}$ , the line patterns are visible but the patch color are not very dark. At  $g = 50.8 \mu\text{m}$ , the contact angle is maximum at around 100 deg. The contact angle displays a decreasing pattern similar the largest gap in case 1 with the lowest contact angle in the perpendicular direction at around 50 deg. Again at  $g = 406.4 \mu\text{m}$ , the drop anisotropy is highest.

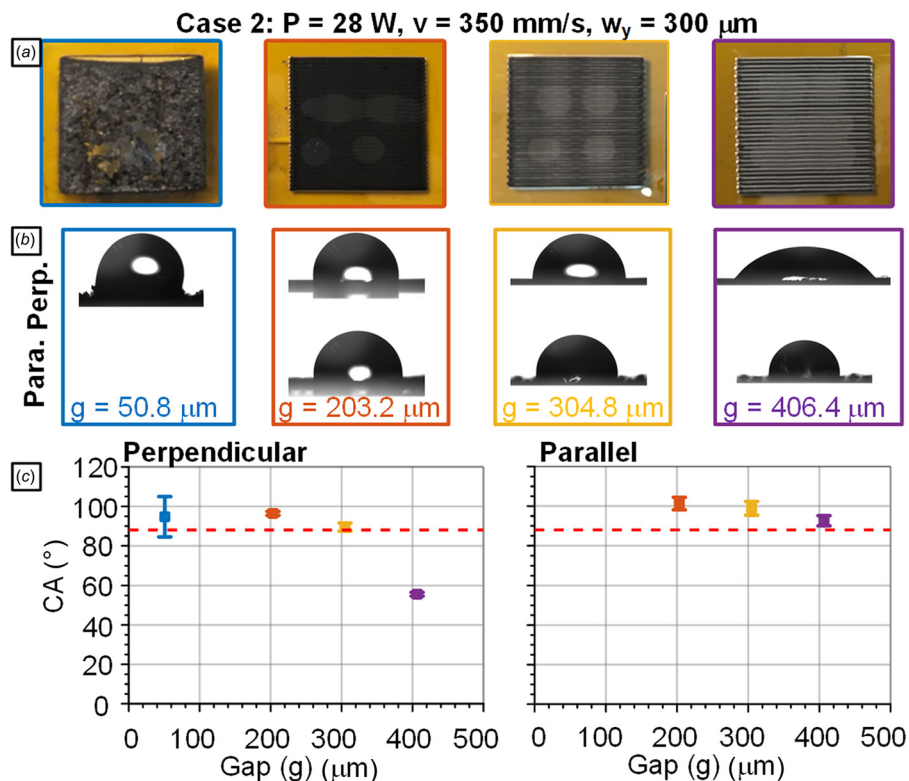
**3.3 Case 3 ( $P = 12 \text{ W}$ ,  $v = 500 \text{ mm/s}$ ,  $w_y = 300 \mu\text{m}$ ).** Figure 5 illustrates the results at lasing power of 12 W, rastering speed of 500 mm/s and laser spot size of  $300 \mu\text{m}$ . These are the same parameters of case 1, except at a lower power indicating lower fluence delivered to the polyimide surface during lasing. From the image, none of the patches exhibit any change in color indicating very limited, if any, carbonization of polyimide. The contact angles show little change from the control value of bare polyimide. However, with increasing gap, drop anisotropy is noted to increase, illustrating the effect of surface patterning of anisotropy, even for low fluence cases.

**3.4 Case 4 ( $P = 12 \text{ W}$ ,  $v = 350 \text{ mm/s}$ ,  $w_y = 300 \mu\text{m}$ ).** Figure 6 illustrates the results at lasing power of 12 W, lasing speed of 350 mm/s and laser spot size of  $300 \mu\text{m}$ . These are the same parameters of case 2, except at a lower power indicating less fluence delivered when lasing. The  $g = 50.8 \mu\text{m}$  is the darkest patch, the color of the patch gets lighter till a minimum at  $g = 406.4 \mu\text{m}$ , indicating less carbonization at these gap values. The line pattern is noticed in all patches. Drop anisotropy is highest at  $g = 406.4 \mu\text{m}$ . The patches are noticeably hydrophilic at  $g = 203.2 \mu\text{m}$  with contact angles between 15 deg and 20 deg, in contrast with the other patches, which show values closer to the control.

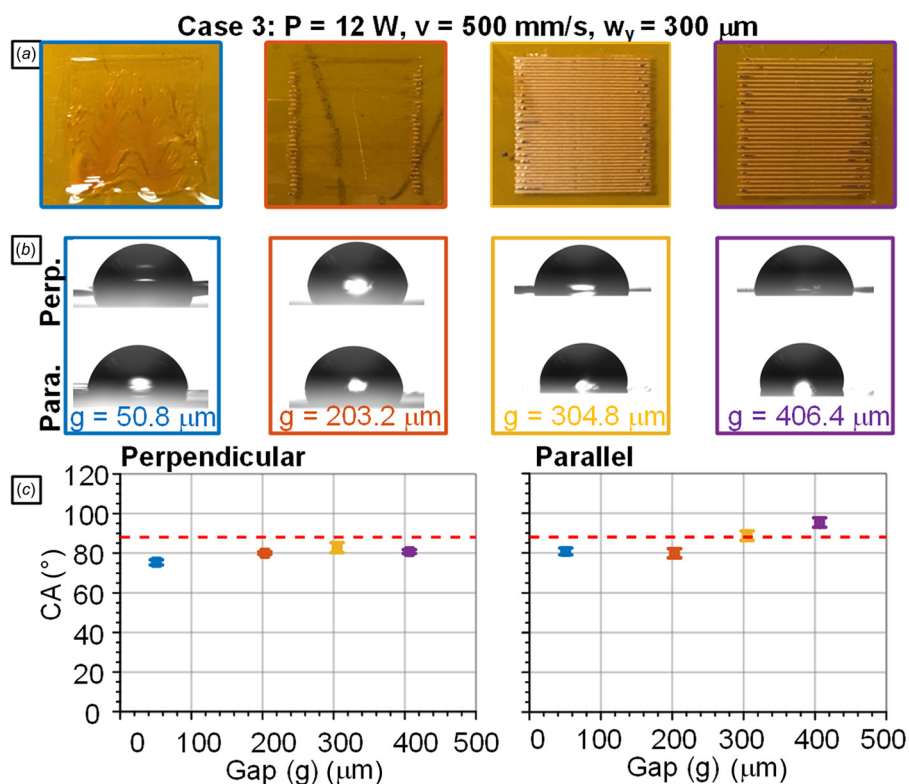
**3.5 Case 5 ( $P = 28 \text{ W}$ ,  $v = 500 \text{ mm/s}$ ,  $w_y = 100 \mu\text{m}$ ).** Figure 7 illustrates the results at lasing power of 28 W, rastering speed of 500 mm/s and laser spot size of  $100 \mu\text{m}$ . These parameters are the same as case 1, except that it has a smaller spot size. The  $g = 50.8 \mu\text{m}$  case exhibits a gray color, at  $g = 203.2 \mu\text{m}$ , the color is darker. At higher gaps, the line patterns are more visible, but the lines themselves are very dark. At  $g = 50.8 \mu\text{m}$ , the contact angle in the perpendicular and parallel direction are relatively low (in the range of 40–60 deg), with increasing gap, the angle increases to be around the control value. The perpendicular contact angle drops at  $g = 304.8 \mu\text{m}$  to increase again at  $g = 406.4 \mu\text{m}$ .

**3.6 Case 6 ( $P = 28 \text{ W}$ ,  $v = 350 \text{ mm/s}$ ,  $w_y = 100 \mu\text{m}$ ).** Figure 8 illustrates the results at lasing power of 28 W, rastering speed of 350 mm/s and laser spot size of  $100 \mu\text{m}$ . These are the same parameters of case 5, except at a lower speed indicating higher fluence delivered to the polyimide surface during lasing. All





**Fig. 4** (a) Top view image of each patch for case 2 (lasing parameters  $P = 28 \text{ W}$ ,  $v = 350 \text{ mm/s}$ ,  $w_y = 300 \text{ }\mu\text{m}$ ), (b) optical tensiometer images of water droplets, and (c) plots of contact (CA) at different gap values. Horizontal dashed line represents control CA. Error bars represent  $\pm$  standard deviation.



**Fig. 5** (a) Top view image of each patch for case 3 (lasing parameters  $P = 12 \text{ W}$ ,  $v = 500 \text{ mm/s}$ ,  $w_y = 300 \text{ }\mu\text{m}$ ), (b) optical tensiometer images of water droplets, and (c) plots of contact (CA) at different gap values. Horizontal dashed line represents control CA. Error bars represent  $\pm$  standard deviation.

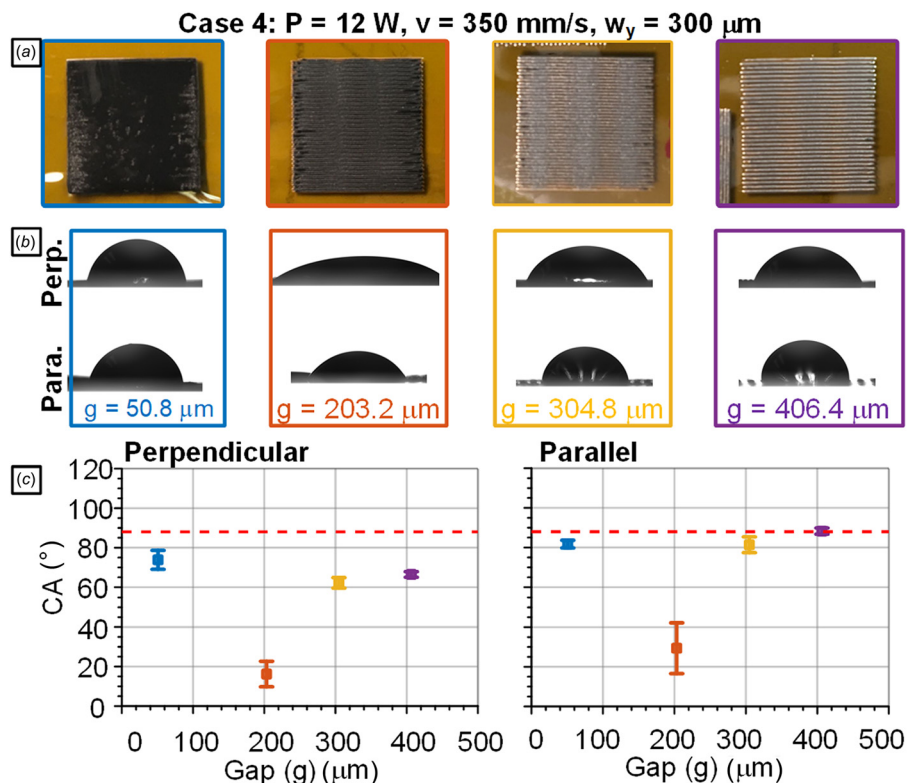


Fig. 6 (a) Top view image of each patch for case 4 (lasing parameters  $P=12\text{ W}$ ,  $v=350\text{ mm/s}$ ,  $w_y=300\text{ }\mu\text{m}$ ), (b) optical tensiometer images of water droplets, and (c) plots of contact (CA) at different gap values. Horizontal dashed line represents control CA. Error bars represent  $\pm$  standard deviation.

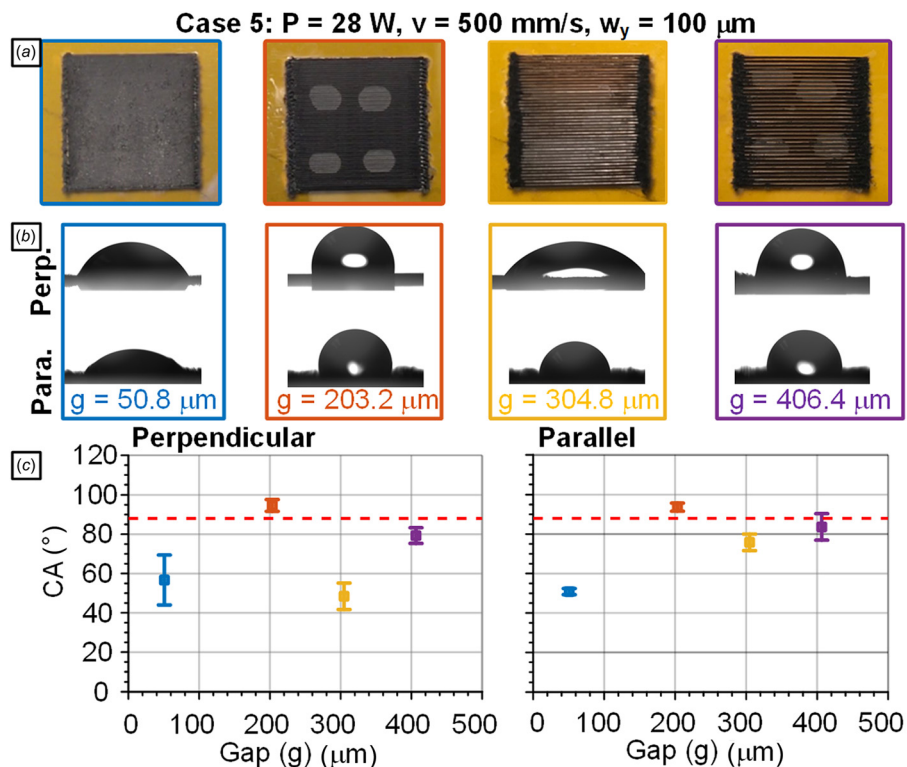


Fig. 7 (a) Top view image of each patch for case 5 (lasing parameters  $P=28\text{ W}$ ,  $v=500\text{ mm/s}$ ,  $w_y=100\text{ }\mu\text{m}$ ), (b) optical tensiometer images of water droplets, and (c) plots of contact (CA) at different gap values. Horizontal dashed line represents control CA. Error bars represent  $\pm$  standard deviation.

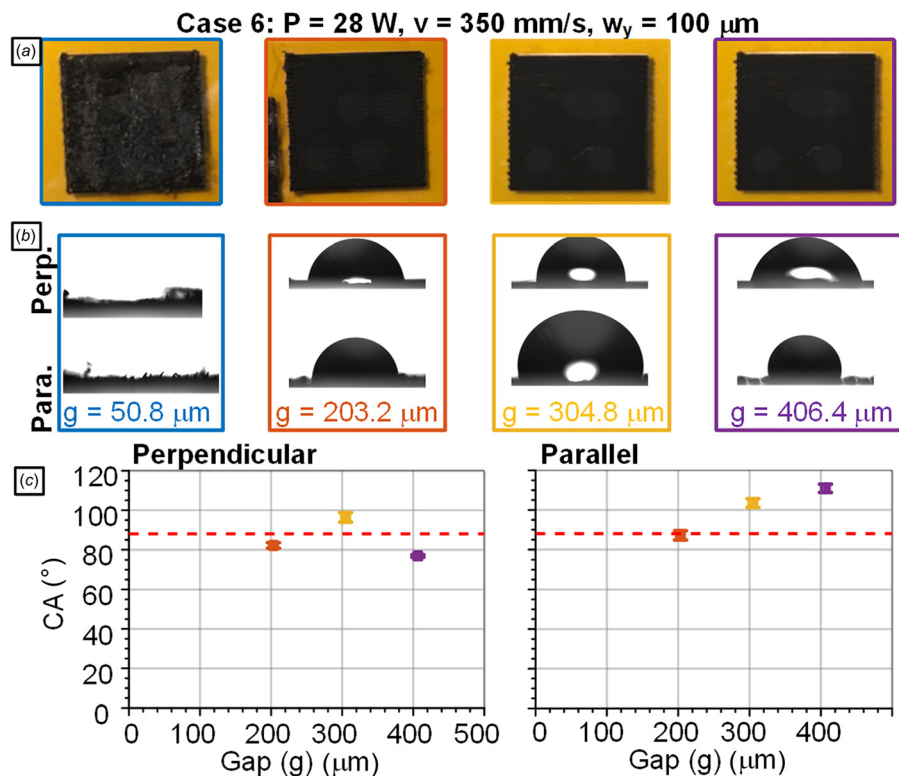


Fig. 8 (a) Top view image of each patch for case 6 (lasing parameters  $P=28\text{W}$ ,  $v=350 \text{ mm/s}$ ,  $w_y=100 \text{ }\mu\text{m}$ ), (b) optical tensiometer images of water droplets, and (c) plots of contact (CA) at different gap values. Horizontal dashed line represents control CA. Error bars represent  $\pm$  standard deviation.

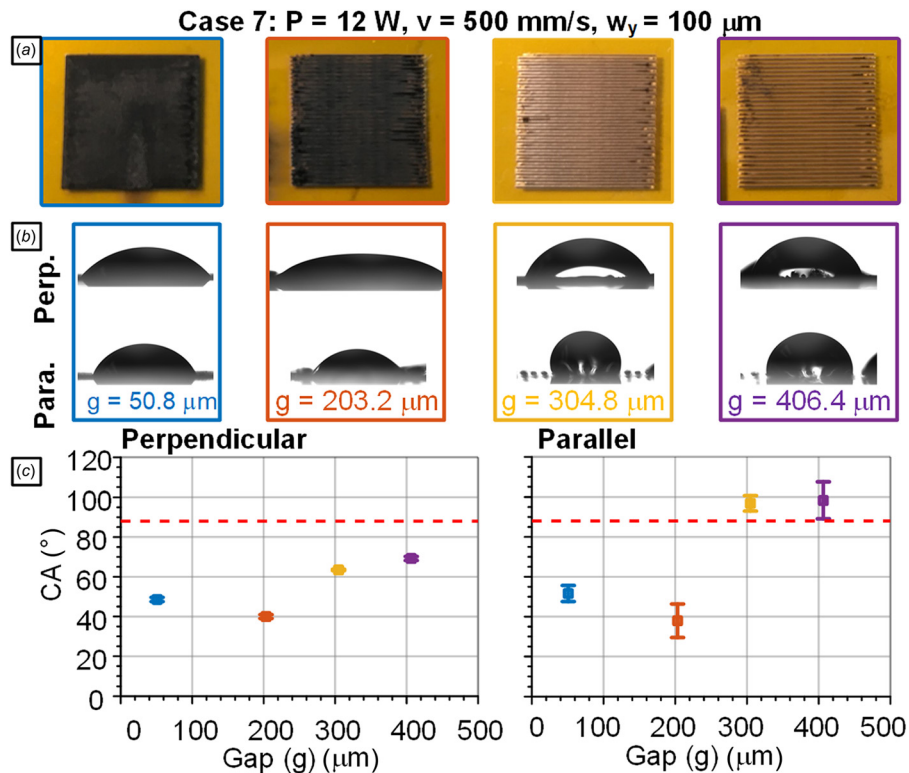
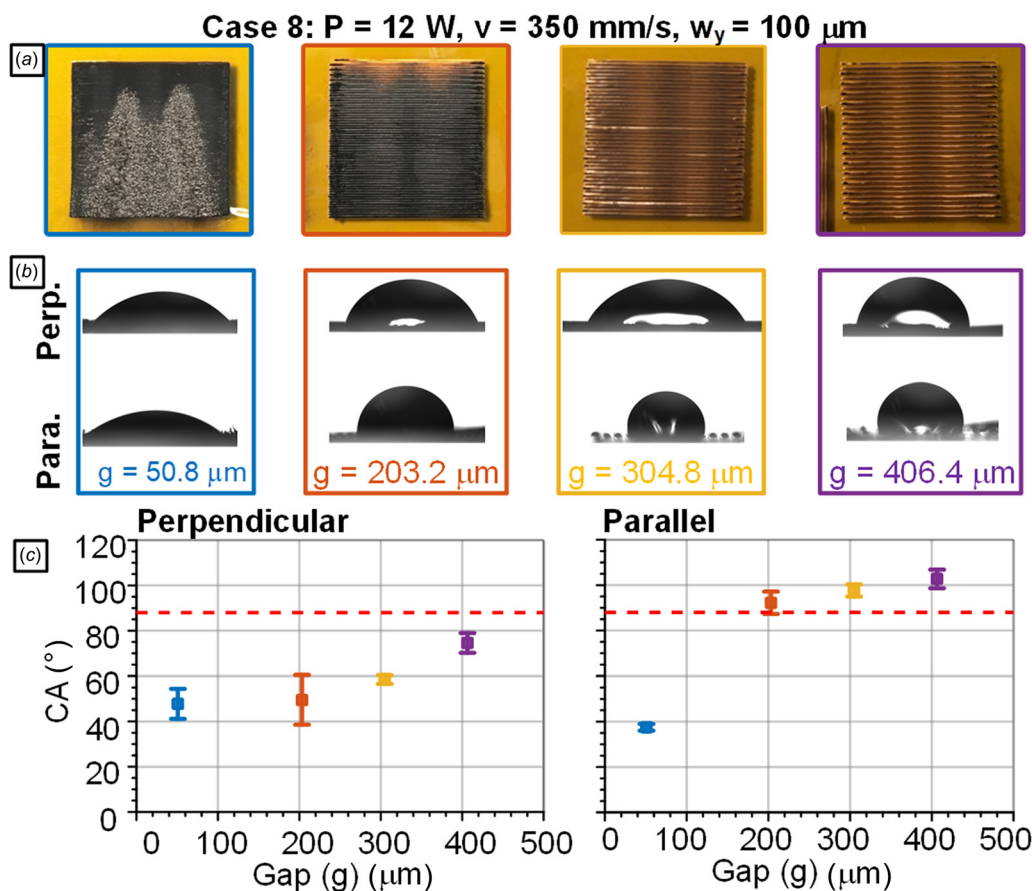


Fig. 9 (a) Top view image of each patch for case 7 (lasing parameters  $P=12\text{W}$ ,  $v=500 \text{ mm/s}$ ,  $w_y=100 \text{ }\mu\text{m}$ ), (b) optical tensiometer images of water droplets, and (c) plots of contact (CA) at different gap values. Horizontal dashed line represents control CA. Error bars represent  $\pm$  standard deviation.



**Fig. 10** (a) Top view image of each patch for case 8 (lasing parameters  $P=12\text{ W}$ ,  $v=350\text{ mm/s}$ ,  $w_y=100\text{ }\mu\text{m}$ ), (b) optical tensiometer images of water droplets, (c) plots of contact (CA) at different gap values. Horizontal dashed line represents control CA. Error bars represent  $\pm$  standard deviation.

patches exhibit a very dark color, representing the darkest case of all eight cases. At  $g = 50.8\text{ }\mu\text{m}$ , the droplets immediately wick: they are drawn into the patches through capillary action. At higher gaps, the drops have an increasing contact angle that is maximum around 115 deg parallel with 75 deg perpendicular.

**3.7 Case 7 ( $P = 12\text{ W}$ ,  $v = 500\text{ mm/s}$ ,  $w_y = 100\text{ }\mu\text{m}$ ).** Figure 9 illustrates the results at lasing power of 28 W, rastering speed of 350 mm/s, and laser spot size of 100  $\mu\text{m}$ . These are the same parameters of case 5, except at a lower power indicating lower fluence delivered to the polyimide surface during lasing. The patches with the smallest two gaps have a darker color while the larger two gaps have a lighter color (closer to the original color of Kapton), indicating less carbonization. The patches are initially hydrophilic at  $g = 50.8\text{ }\mu\text{m}$  and  $g = 203.2\text{ }\mu\text{m}$ . At higher gaps, the contact angles measured from a parallel view to the lasing lines is hydrophobic at a maximum of 100 deg, with the perpendicular contact angle at 50 deg, exhibiting contact angle anisotropy.

**3.8 Case 8 ( $P = 28\text{ W}$ ,  $v = 350\text{ mm/s}$ ,  $w_y = 100\text{ }\mu\text{m}$ ).** Figure 10 illustrates the results at lasing power of 28 W, rastering speed of 350 mm/s and laser spot size of 100  $\mu\text{m}$ . These are the same parameters of case 6, except at a lower power indicating lower fluence delivered to the polyimide surface during lasing. Similar to case 7, The patches with the smaller two gaps have a darker color while the larger two gaps have a lighter color (closer to the original color of Kapton), indicating less carbonization. However, the patches at  $g = 304.8\text{ }\mu\text{m}$  and  $g = 406.4\text{ }\mu\text{m}$  exhibit alternating light and dark patterns along the lines, that repeat with each line. Like case 7, the contact angle changes from isotropic hydrophilic to hydrophobic at a maximum parallel contact angle

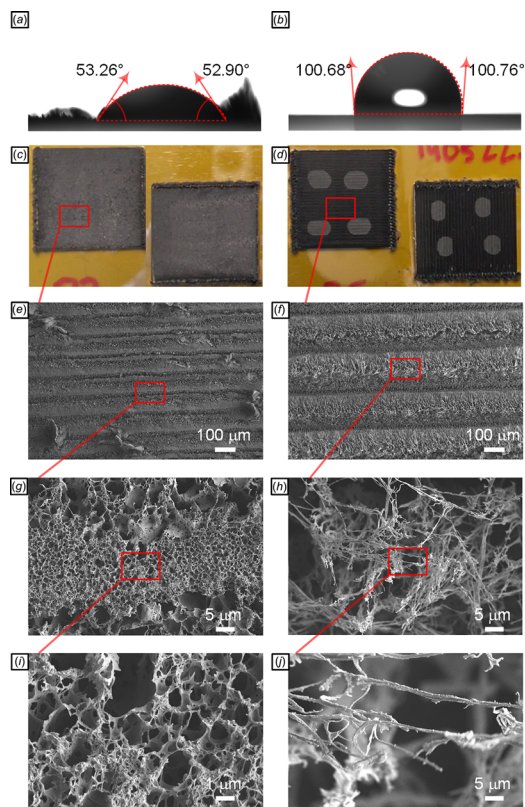
at around 105 deg with maximum anisotropy observed at  $g = 406.4\text{ }\mu\text{m}$ .

#### 4 Discussion

To explain the observed difference in contact angle measurements and their dependence on lasing conditions, we correlate the observed behavior with the morphology of the patches as seen in SEM images. We imaged LINC lines formed with lasing power of 28 W and rastering speed of 500 mm/s. We focused our measurements on two gaps:  $g = 50.8\text{ }\mu\text{m}$  and  $g = 203.2\text{ }\mu\text{m}$ , as shown in Fig. 11. It is evident from the differences between the two cases that gap size plays an important role in morphology.

At  $g = 50.8\text{ }\mu\text{m}$ , high overlap between lased lines (Figs. 11(c) and 11(e)) is observed, whereas  $g = 203.2\text{ }\mu\text{m}$  shows less overlap (Figs. 11(d) and 11(f)). Since the spacing between the laser paths at  $g = 50.8\text{ }\mu\text{m}$  is small compared to the spot size diameter of 200  $\mu\text{m}$ , where each point on the area along the lased line would have been lased for around four passes. When the  $g = 203.2\text{ }\mu\text{m}$ , the overlap is minimized since the line-to-line distance is almost equal to the spot size. From the SEM imaging, the high overlap in  $g = 50.8\text{ }\mu\text{m}$  resulted in a porous morphology, looking much like a sponge (Figs. 11(g) and 11(i)). This enhances water wicking through the internal porosity owing to the capillary effects. Hence, this nanoporous morphology leads to lower contact angles ( $\sim 53$  deg). On the other hand, the sample with  $g = 203.2\text{ }\mu\text{m}$  that has less overlap, exhibited a larger contact angle ( $\sim 100$  deg) and a more fibrous morphology (Figs. 11(h) and 11(j)). This suggests that the high overlap between the lased lines led to the destruction of formed fibers, hence the nanoporous morphology. The high contact angle noted with the fiber formations implies that fibrous LINC formations lead to hydrophobic drop behavior.





**Fig. 11** Contact angle measurements of power 28 W, speed 500 mm/s, at (a)  $g = 50.8 \mu\text{m}$ , (b)  $g = 203.2 \mu\text{m}$ . (b) and (c) Top view optical images of (a) and (b). (e), (g), (i) SEM images of (a) at 250 $\times$ , 5000 $\times$ , and 25,000 $\times$ , respectively. (f), (h), (j) SEM images of (b) at the same magnification.

We summarize the results of the different cases in Table 2. We also color code the results according to the hydrophobicity or hydrophilicity of the surface (according to the measured water contact angle). Taken together, our results show that a number of interacting factors contribute to the observed value and anisotropy of water contact angle on LINC patches.

Water contact angle on LINC depends on the extent of carbonization of the polyimide surface, the resulting topography of the surface, and the internal porous morphology. These surface properties in turn result from laser processing parameters: lasing power, rastering speed, spot size, and how much overlap there is between rastering lines. Understanding these complex process–structure–property relationships is key for achieving a high degree of tunability of both the values and anisotropy of water contact angle. As observed in Table 2, the parallel orientation generally has a higher contact angles as compared to its perpendicular counterparts due to the directional topographic effects that causes pinning of water droplets at LINC lines leading to anisotropic drop shapes. In general, it is observed that the contact angles shift to hydrophobic progressively with increasing gap size.

The SEM and optical imaging of two selected patches lased at identical power and lasing speed, but different gap sizes provides insight on the effect of line-to-line gap on morphology and contact angle. Optical images of the patch show that the patches have different colors and distinct macroscopic appearances that can be observed with the naked eye.

It was also observed that in some cases, a clear discoloration is observed where water droplets were located even after drying. For example the results shown in Fig. 11 demonstrate this observation for the case of wider gap sample (Fig. 11(d)), whereas in the small gap case (Fig. 11(c)), no discoloration is observed. This indicates that capillary forces involved in water droplet drying significantly change the fibrous LINC morphology obtained at  $g = 203.2 \mu\text{m}$ . On the other hand, the connected nanoporous morphology at  $g = 50.8 \mu\text{m}$  are not significantly affected by capillary forces. Moreover, the anisotropic shape of these impressions confirm the anisotropic nature of the droplet contact on LINC lines.

In sum, we observe that some of the resulting contact angles are very low due to wicking effect of porous LINC morphology,

**Table 2** Summary of results showing a color-coded classification of wetting behavior

Case	P(W)	v (mm/s)	w <sub>y</sub> (μm)	g = 50.8 μm		g = 203.2 μm		g = 304.8 μm		g = 406.4 μm	
				⊥		⊥		⊥		⊥	
1	28	500	300	22°	24°	83°	92°	95°	110°	24°	80°
2	28	350	300	95°	-	96°	101°	90°	99°	56°	93°
3	12	500	300	75°	81°	80°	80°	83°	89°	81°	95°
4	12	350	300	74°	82°	16°	29°	62°	81°	66°	88°
5	28	500	100	57°	51°	95°	94°	48°	76°	79°	84°
6	28	350	100	W	W	82°	87°	96°	104°	77°	111°
7	12	500	100	49°	52°	40°	38°	63°	97°	69°	98°
8	12	350	100	48°	38°	50°	92°	59°	98°	75°	103°
9	Untreated PI			88°							



Hydrophilic  
<85



Hydrophobic  
>95



=85-95°



while others exhibit decidedly hydrophobic contact angles due to the fibrous morphology. Also, some contact angles are highly anisotropic, owing to the effect of rastering gaps and water pinning on individual LINC lines. Hence, the approach shown in the paper provides a promising path to engineering anisotropic wetting behavior on commercial polymers. This capability has potential applications in the design of microfluidic devices, lab-on-a-chip sensors, microreactors, and self-cleaning surfaces [14]. This is a new approach to achieve anisotropic wetting surfaces [14]. Importantly, this approach is potentially more scalable and cost-effective compared to previously explored approaches. For example, anisotropic wetting was previously achieved using one-dimensional topographical patterns created using expensive lithographical patterning [15], embossing [16], etching [17], as well as by creating areas of alternating surface energies [18]. Thus, using a direct-write commercial CO<sub>2</sub> laser processing system is a significant advantage of our approach.

## 5 Conclusions

We demonstrate that varying laser power, rastering speed, line-to-line gap, and spot size in LINC formation directly on polyimide surfaces enables tuning the contact angle of water. Our results show that a wide range of contact angles can be achieved, ranging from hydrophilic approaching 0 deg to hydrophobic surfaces approaching 120 deg as well as anisotropic wetting behavior. Characterizing the morphologies using a combination of optical and electron microscopy also enabled correlating these properties to the structure of LINC. Our findings highlight the versatility of this technique, which is promising for tuning the surface properties of commercial polymers for various applications, such as self-cleaning, antifouling, and self-cleaning surfaces.

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