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Analysis of machining induced residual stresses of milled aluminum work-pieces, their repeatability and their resulting distortion

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Abstract

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13 Machining induced residual stresses (MIRS) are a main driver for distortion of thin walled monolithic aluminum work-
14 pieces. Before one can develop compensation techniques to minimize distortion, the effect of machining on the MIRS
15 has to be fully understood. This means that not only an investigation of the effect of different process parameters on the
16 MIRS is important. In addition, the repeatability of the MIRS resulting from the same machining condition has to be
17 considered. In past research statistical confidence of MIRS of machined samples was not focused on. In this paper the
18 repeatability of the MIRS for different machining modes, consisting of a variation in feed per tooth and cutting speed,
19 are investigated. Multiple hole-drilling measurements within one sample and on different samples, machined with the
20 same parameter set, were part of the investigations. Besides, the effect of two different clamping strategies on the MIRS
21 were investigated. The results show that an overall repeatability for MIRS is given for stable machining (between 16 %
22 and 34 % repeatability standard deviation of maximum normal MIRS), whereas instable machining, detected by vibra-
23 tions in the force signal, has worse repeatability (54 %) independent of the used clamping strategy. Further experiments,
24 where a 1 mm thick wafer was removed at the milled surface, show the connection between MIRS and their distortion.
25 A numerical stress analysis reveals that the measured stress data is consistent with machining induced distortion across
26 and within different machining modes. It was found that more and/or deeper MIRS cause more distortion.

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Keywords: Machining induced residual stresses, distortion, milling aluminum, finite element method

1. Introduction

38 The surface integrity is an important domain of part quality, especially the part quality of milled monolithic thin walled
39 aluminum components in the aerospace industries [1]. There is a constant need for improved surface integrity and en-
40 hanced functional performance of machined components [2]. Residual stresses (RS) are one attribute of the surface
41 integrity and have a major influence on in-service failures such as corrosion and fatigue life of parts [3]. RS are defined
42 as the internal stresses locked in a body, where force and torque equilibrium prevail and no thermal gradients appear
43 [4]. It is known that RS in thin walled monolithic aluminum parts, where up to 90 % of the initial material is removed,
44 cause distortions. These distortions lead to high costs due to remanufacturing and part rejection [4]. In this context one
45 must distinguish between two sorts of RS [5]. One sort are the initial bulk residual stresses (IBRS), which exist previous
46 to machining in the blank material. They are caused by processes like heat treatments (e.g. quenching) and appear
47 throughout the entire part-thickness [5]. The second sort are the machining induced residual stresses (MIRS), which are
48 driven into the material during the machining process. In terms of surface integrity, the MIRS are from greater interest,
49 because their penetration depth is limited to a shallow layer just under the part surface. A typical MIRS profile in a
50 milled aluminum material looks square root shaped ($-\sqrt{-}$) with compressive RS near the surface [5].

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It is known that different machining parameters and different tool geometries cause different MIRS [5]. Especially the
high mechanical loads which occur during machining induce a non-uniform plastic deformation on the surface layers of
the materials [6]. Typically, those deformations lead to a square rooted shaped compressive residual stress profile, which
varies in the maximum residual stress (MaxRS), the depth of it (t_m), and the penetration depth (t_p) depending on the

machining parameters. The penetration depth is hereby defined as the thickness of the layer containing MIRS. Research investigating the effect of the feed per tooth, cutting speed, width of cut, depth of cut, and tool geometry was conducted in the past. It was found that an increase of the feed per tooth leads to higher MaxRS at greater depths (t_m) when milling Al7449-T7651 samples with end mills and cutters with indexable inserts parallel to feed direction [7, 8]. The depth t_m increased from 0 μm to a maximum of approx. 45 μm , while the MaxRS increased from approx. -325 MPa to -400 MPa for milling with a cemented carbide helical cutter ($d=20\text{ mm}$) for an increased feed per tooth f_z from 0.05 mm to 0.30 mm ($a_p=4\text{ mm}$, $a_e=20\text{ mm}$) [7]. The same trend of an increased MaxRS was investigated for milling Al7050-T6 with inserts in cutting direction [9] and Al7050-T7451 with end mills in feed and cutting direction [10]. In contrast, the investigations of Tang et al. showed no systematic trend of MaxRS and t_m parallel or perpendicular to the feed direction when milling Al7050-T7451 with end mills [11]. The depth t_m e.g. lays between 15 and 20 μm and the MaxRS in feed direction does not change significantly (approx. -80 MPa) for an increased feed per tooth from 0.1 mm to 0.2 mm when milling with a three fluted cemented carbide end mill ($d=20\text{ mm}$, $R=3\text{ mm}$, $a_p=2\text{ mm}$, $a_e=10\text{ mm}$, $n=16000\text{ rpm}$) [11].

Past research showed that for the variation of cutting speed there is no common effect on the MIRS. Denkena et al. [8] and Perez et al. [3] e.g. observed that increased cutting speeds for milling Al7449-T7651, Al7050-T7451 respectively, with indexable inserts, lead to an increase in maximum compressive stresses. But in other studies by Denkena et al., the use of helical cutters for different cutting speeds did not influence MaxRS and t_m at all [7]. MaxRS of approx. -300 MPa was measured at a depth between 30 to 45 μm for different v_c between 250 and 1500 m/min [7]. Furthermore, decreased compressive RS for an increase of the cutting speed were observed by Tang et al. [11] and Rao et al. [9]. The MaxRS in feed direction was measured to -120 MPa ($n=4000\text{ rpm}$) and -90 MPa ($n=16000\text{ rpm}$) [11].

Different researchers found that the MaxRS increased with increasing depth of cut [7, 12]. In contrary for the variation of the width of cut the highest MaxRS were found for the lowest width of cut [7]. In terms of tool geometry, Denkena et al. showed that an increase of the cutting edge radius [7] and a decrease of the corner radius [8], lead to higher MaxRS.

Above mentioned research has in common that residual stress measurements per machining state were carried out only on one sample with limited or even no statistical confidence. No repeated measurements on different samples, sharing the same machining condition, were carried out. Furthermore, no shear RS were investigated, although they are an important factor of the distortion caused by the MIRS, hereafter called machining induced distortion [13]. The present research focuses on the repeatability of MIRS for multiple milled aluminum workpieces, machined with the same machining parameter. Our previous research studied the repeatability of RS measurement techniques (hole-drilling, slotting, $\sin^2(\psi)$ XRD, $\cos(\alpha)$ XRD) themselves [13, 14]. It was found that data from hole-drilling (HD) are most consistent with machining induced distortion for AA7050-T7451 parts and multiple measurements are necessary to describe the MIRS with good statistical confidence. Therefore, the HD technique and three measurements per sample were set as the standard for present research. In this context one measurement is defined as the measurement of the entire MIRS depth profile down to a depth of 500 μm . To identify the repeatability of MIRS resulting from machining under the same condition, three samples were machined for each machining set. Four different machining sets, consisting of a variation in feed per tooth and cutting speed, were investigated to analyze the effect of different machining parameters on the MIRS. Furthermore, the effect of two different clamping strategies, a vise and side clamps, on the MIRS was analyzed. Forces and temperatures were measured during machining. In total 17 samples were machined and 51 HD depth profiles were conducted. Moreover, distortion experiments, where a 1 mm thick wafer was removed at the milled surface, were carried out to show the machining induced distortion. In this context a numerical stress analysis was computed to analyze if the measured hole-drilling data are consistent with the measured distortion. The objectives of the present research are summarized as follows:

- Investigation of the repeatability of MIRS for machining multiple samples
- Investigation of the influence of machining parameters on MIRS and their repeatability
- Investigation of the influence of the clamping strategy on the MIRS
- Investigation of machining induced distortion

2. Methods

2.1 Machining induced residual stress experiments

Down milling was carried out on a 5-axis DMG Mori¹ DMU 70 CNC machine. Cemented carbide end mills of the type Kennametal¹ F3AA1200AWL were used, because it represents a typical tool for machining of aerospace aluminum alloys. The tool properties can be found in Table 1. Aluminum blocks AA7050-T7451 with the dimensions 206x102x28.5 mm³ were face milled on the 206x102 mm² face. In order to reduce the IBRS, the AA7050-T74 samples come in a stress relieved condition (T7451) [15], where the IBRS are decreased to magnitudes lower than 20 MPa [16]. The samples were cut from a large slab of stress relieved aluminum measuring 1250x1250x102 mm³, where six blocks of material (660x206x102 mm³) were saw cut. These blocks were cut again into 15 individual samples (206x102x28.5 mm³).

Table 1 Tool properties

tool properties	Kennametal ¹ F3AA1200AWL
type	regular end mill
diameter	12 mm
tool holder	HSK-A 63
material	cemented carbide 10 % Co, 0.6 % Cr, 89.4 % WC max. grain size 3 µm
number of flutes z	3
helix angle	45°
cutting edge radius	-
length	76 mm
coating	-

The feed (x-) direction corresponded to the 206 mm dimension and the orthogonal feed (y-) direction to the 102 mm dimension. The tool movement was along the negative x-direction with respect to the sample coordinate system (see Fig. 1). The feed per tooth f_z and the cutting speed v_c were varied. Three different feed per tooth and two different cutting speeds were investigated, which resulted in four parameter modes (see Table 2). They were selected by prior experiments because they represent different load cases and showed less vibrations and no interference with the eigenfrequency of the set up. The width of cut a_e and depth of cut a_p were kept constant at 4 mm and 3 mm respectively, and dry cutting was carried out to only investigate the effect of the cutting parameters on the MIRS without having superpositions due to the cooling.

Table 2 Machining parameters cutting speed v_c , feed per tooth f_z and resulting feed rate v_f , material removal rate Q_w and average chip thickness h_m [14,17]

Mode	cutting speed v_c (m/min)	feed per tooth f_z (mm)	feed rate v_f (mm/min)	material removal rate Q_w (mm ³ /min)	average chip thick- ness h_m (mm)
Mode 1	200	0.04	637	7600	0.023
Mode 2	200	0.1	1592	19100	0.058
Mode 3	200	0.2	3183	38200	0.115
Mode 4	450	0.04	1432	17200	0.023

Two different clamping devices were investigated to show the influence of the clamping strategy on the MIRS. A conventional vise and side clamps were used. The jaws of the vise were 125 mm long and the workpiece was clamped in a way that 5.5 mm protruded (in z-height) prior to cutting (see Figure 1a). The clamping force was 15 kN. Six side clamps of the type Lenzke¹ NU10a14 with a maximal nominal clamping force of 7 kN in the xy-plane and 3.5 kN in z-direction were used. The height of clamping was 5 mm in z-direction (see Figure 1b).

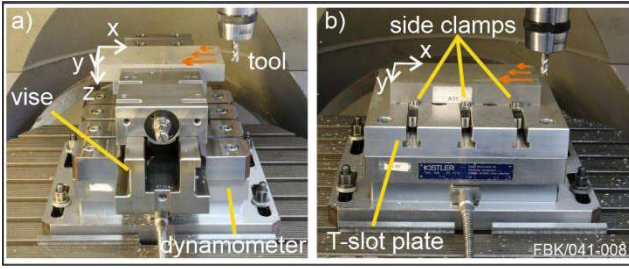


Fig. 1 Experimental setup with vise (a) and side clamps (b)

To investigate the repeatability of MIRS for multiple samples and the influence of different machining modes, twelve machining experiments (three for each mode) were carried out using the vise as a clamping device (see Table 3). In order to investigate the influence of the clamping strategy on the MIRS five more machining experiments were conducted. One sample each for machining Mode 1, 2 and 3 and two samples for Mode 4 were machined with the clamping strategy side clamps (see Table 3, where **MX** stands for machining mode; **A, B, C** are repetitions machined in vise and **D, E** samples machined in side clamps).

Table 3 Sample overview including machining modes and clamping strategies

	Mode 1	Mode 2	Mode 3	Mode 4
vise	M1A	M2A	M3A	M4A
	M1B	M2B	M3B	M4B
	M1C	M2C	M3C	M4C
side clamps	M1D	M2D	M2D	M4D
				M4E

The order of machining the samples was randomly chosen to minimize the influence of tool wear. Furthermore, the tool wear was monitored after machining each sample by a macroscope, so that worn tools were exchanged if wear in the form of corner break outs was qualitatively detected (see Figure 2).

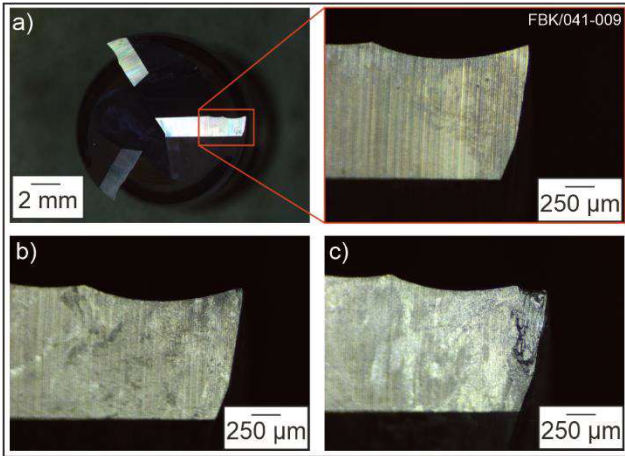


Fig. 2 Macroscopic picture of the end face of a new tool (a), used tool for second use allowed (b) and worn tool, not to be re-used (c)

Plastic deformation, thermal gradients, phase transformation and their combined effect are the physics which cause MIRS [5]. Therefore, monitoring the thermal and mechanical load during machining is essential for understanding the effect of different machining parameters on the MIRS. The process was monitored by recording forces using a piezoelectric dynamometer (Kistler¹ Type 9255) with a sampling rate of 15 kHz. One surface layer was removed, which resulted in 25 passes with a constant width of cut of 4 mm. The last 2 mm were removed in an additional pass. The three orthogonal forces (F_x , F_y , F_z), where F_x is the force in negative feed direction, F_y in orthogonal feed direction and F_z is the passive force (see Fig. 1), were analyzed. The forces in every fourth machining pass, beginning with the second, were measured. To compare the forces for the different samples and the different machining modes, the root mean square (RMS) of the force signal of each measured pass was calculated. Run in and run out effects were excluded from

the analysis by analyzing 80 % of the force signal. The arithmetic mean and standard deviation over all measured passes per sample, per mode respectively, was computed to compare the force of different samples for each mode, between the different machining modes respectively.

2.2 Temperature experiments

The thermal load was determined by temperature measurements. Those were carried out in separate experiments on smaller AA7050-T7451 samples with the dimension 30x20x9 mm³ (see Figure 3). The sample dimensions had to be decreased in comparison to the previous experiments in order to manufacture the thermocouple hole with an accurate depth. The orientation was the same compared to prior experiments. The feed (x-) direction was along the 30 mm dimension. The samples were clamped in the vise with 4 mm protruding prior to cutting. Thermocouples type K with a diameter of 1 mm (1KI10TDT-40-4000MS) were inserted from the bottom side in the middle of the sample. The nominal distance from their end face to the cutting face was 100 µm. Three samples per mode were machined in random order to exclude tool wear effects. The sampling rate of the temperature measurements was set to 2 kHz. The value of the maximum temperature is calculated by the arithmetic mean of 200 temperature values around the total temperature maximum of each sample (range ± 0.05 s).

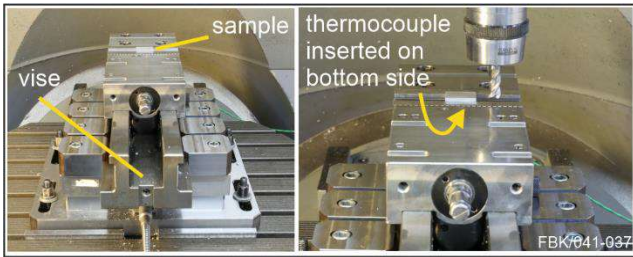


Fig. 3 Experimental set up for temperature measurements

Also, the true distance of the thermocouple face to the newly generated surface was measured after milling via cross-sections (see Fig. 4).

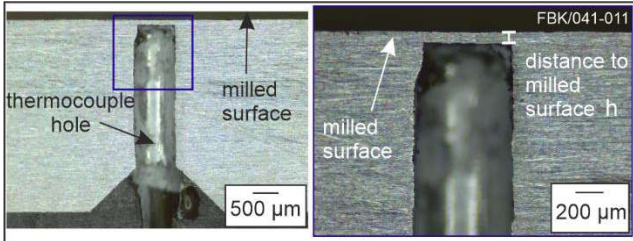


Fig. 4 Macroscopic picture of cross-section of thermocouple hole after milling

2.3 MIRS hole-drilling measurements

The hole-drilling measurements follow ASTM E837-13a [23], implementing fine incremental hole-drilling [24]. A rosette type A strain gage with a circle diameter of 5.13 mm is bonded directly to the machined surface at the measurement position (see Fig. 5). A hole with an approximate diameter of 2 mm is cut in an orbital path with a 1.59 mm diameter end mill on an electric spindle [14]. At each incremental cut the strain gage measures three components of strain. Following the depth increments in Table 4, a profile of strain versus depth data is produced which is used to compute stress versus depth profiles. Three HD measurements were carried out per sample at the positions I (b), II (b) and III (b) (see Fig. 5).

and then shifting the dataset by the z-height of the middle of the wafer, where the minimum was expected (average of z values in the middle of the sample, including all measured data within 0.5 mm in each (x-, y-) direction).

A numerical stress analysis was carried out to check to what extent the MIRS correlate with the wafer distortion. A static, linear elastic finite element model, based on the approach used in [19-21], was set up in ABAQUS¹. The measured MIRS were implemented as an input and the distortion was calculated, after equilibrium had been set. The geometry was, according to the wafers, a 25x25x1 mm³ thin plate (see Fig. 6), where the z-direction corresponds to the depth of the MIRS. The MIRS were linearly interpolated over depth at the element centroids and applied as an initial condition (initial condition type = stress, see [27]). For depth smaller than the first measured point the first measured MIRS was used. For depth greater than the last measured depth, the MIRS were set to 0 MPa (see Fig. 6). The respective information of the depth (z-position) of each element was read in from the ABAQUS¹ input file via a developed Matlab¹ script, which also assigned each element the information of the residual stress according to its depth. The mesh consisted of eight-node brick elements (C3D8) with 77,500 elements in total. The in-plane (xy) size of the elements was set to 500 μm. There were 31 elements in z-direction with the smallest size of 5 μm at the machined surface and bigger elements at the bottom face (100 μm) (see Fig. 6), in order to precisely resolve the residual stresses near the surface and still reduce the total number of elements for calculation time reasons. The body was constrained by the 3-2-1 constraint principle, which avoided rigid body motion, but enabled a free distortion of the body [22]. Linear elastic material behavior with a Young's modulus E of 71,700 MPa and a Poisson ratio ν of 0.33 was given. After equilibrium was calculated the displacement at the bottom was analyzed by levelling and shifting (by z-value in the middle of the wafer) the data and then compared to the wafer distortion measured in the experiment.

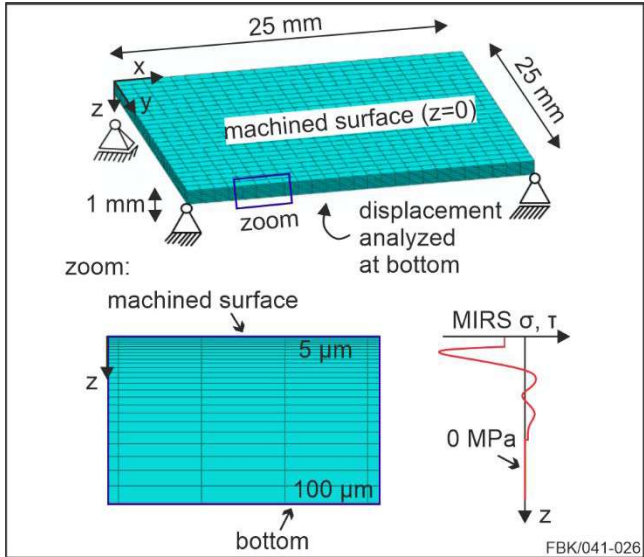


Fig. 6 Finite element model to predict distortion due to MIRS

Two wafers for each mode were investigated to show the distortion within and across different machining modes (see Table 5). In addition, FEM simulations were carried out for all wafers to show the connection between measured MIRS and their distortion.

Table 5 Wafer sample overview

	Mode 1	Mode 2	Mode 3	Mode 4
vise	M1A	M2A	M3B	M4A
	M1B	M2C	M3C	M4B

3. Results and Discussion

3.1 Force analysis

The comparison of the forces of samples machined in the vise show that for all modes, forces in y-direction are the highest (see Fig. 7), because this is the main cutting direction. Forces F_x and F_z are much lower than F_y . The one-way ANOVA was applied for statistically testing the differences in the means of all samples machined in the vise (for each mode and force component). The null hypothesis states that the means are the same. The p-value of each ANOVA test is displayed in Fig. 7 in the respective upper left corner (p_A). The ANOVA analysis found that the observations support a difference in the mean of all RMS vise forces except M2 F_z ($p_A > 0.05$ significance level), which highlights that the std of the mean RMS force of each sample is low, while the different mean values differ slightly. Nevertheless, from a physical point of view the forces within each mode are on a similar level with a maximum variation ($1 - \text{mean}_{\min}/\text{mean}_{\max}$) by only 20 %. Forces F_x of Mode 4 are an exception as they scatter more with a maximum variation of 60 % for vise samples. An independent t-test was applied for statistically testing the differences in the mean RMS forces for all samples machined in the vise compared to the ones of samples machined in the side clamps for each mode and force component respectively. The null hypothesis states that the means are the same. The p-value of each t-test is displayed in Fig. 7 in the respective upper right corner (p_t). The observations support a statistically significant difference except for M3 F_y , M4 F_x and M4 F_y ($p > 0.05$). But in general, the forces for samples machined in the side clamps are on a same level compared to the forces of samples machined in the vise (see Fig. 7): $|1 - \text{mean}_{\text{sc(DE)}}/\text{mean}_{\text{vise(ABC)}}| < 22\%$ for each case. Special trends will be discussed together with the MIRS (see section 3.3).

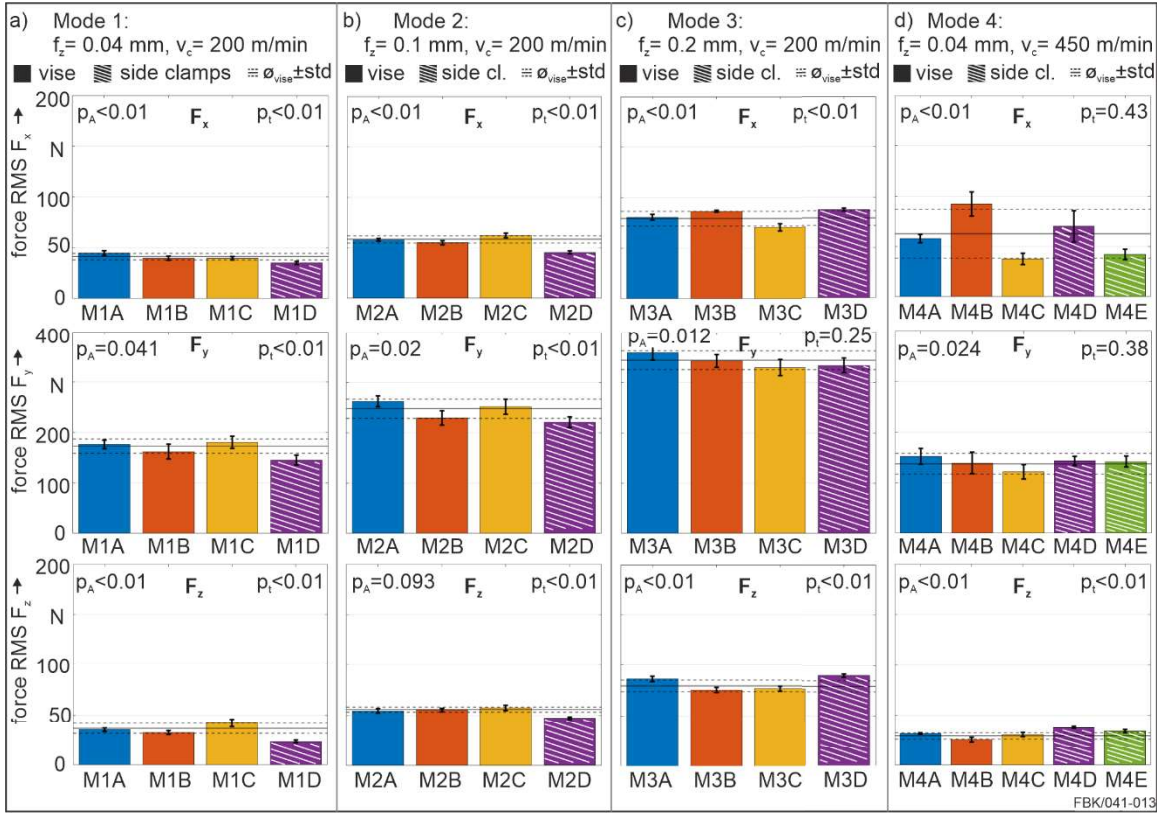


Fig. 7 Mean of RMS forces each sample in x-, y- and z-direction, error bars represent standard deviation, p_A is the p-value of the ANOVA for samples machined in vise for each mode and force component and p_t is the p-value of the independent t-test (group I samples machined in vise, group II samples machined in side clamps) for each mode and force component; mind different scales

The one-way ANOVA was applied for statistically showing that the difference of the mean of the forces of different modes is statistically significant. The null hypothesis states that the means are the same. The p-value of each ANOVA test is displayed in Fig. 8 in the respective upper left corner (p_A). A statistically significant difference is shown by $p_A < 0.05$ for all force components. The comparison of the forces of different machining modes show that increasing feed per tooth increases the cutting forces (see Fig. 8). This is due to the greater undeformed chip thickness and material

removal rate with increased feed per tooth (see Table 1), which results in a higher energy demand for the plastic deformation of the material and the overcoming of the higher friction [25]. An increase in the cutting speed leads to decreased forces F_y and F_z , and increased F_x due to the higher feed rate (compare Mode 1 to Mode 4 in Fig. 8).

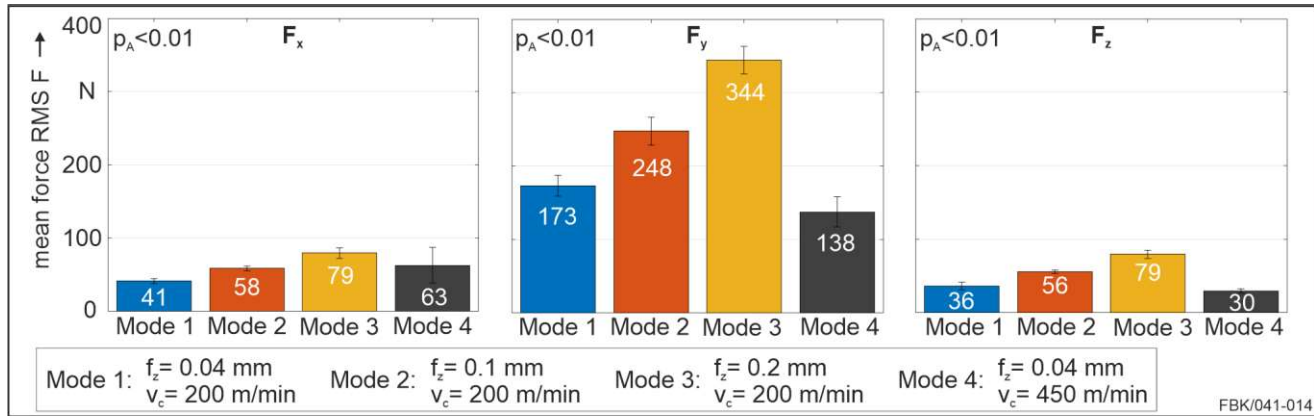


Fig. 8 Inter mode comparison of mean of RMS forces in x-, y- and z-direction for clamping with a vise, error bars represent standard deviation, p_A is the p-value of the ANOVA

Figure 9 presents a detailed look on the force signals in the z direction. The entire force signal F_z of pass number 14 is shown for one sample of each mode (M1A, M2A, M3A, M4A) machined in the vise. The samples and their force signals are representative for all samples and passes machined in the vise for the respective mode. Furthermore, a zoomed view, where one rotation of the tool can be traced, and the Fast-Fourier-Transformation (FFT) of the force signal, to highlight dominating frequencies during cutting, are shown. It can be seen that due to the given width of cut ($a_c = 4$ mm) and the tool diameter ($d = 12$ mm) only one flute per time is engaged with the material (tool has 3 flutes). Due to the tool geometry the tool is primarily pulling the material in negative z-direction (see Fig. 1). The cutting edge frequency f_c is here defined as the frequency of the initial contact of each flute with the material ($f_c = 1/t_r \cdot z$, where z represents the number of flutes and t_r the time per rotation). The time per rotation t_r and the cutting edge frequency f_c for each mode are shown in Table 6. The FFT in Figure 9 shows that for Mode 1, 2 and 3 the dominating frequency is the cutting edge frequency (265 Hz). The FFT of the Mode 4 force signal reveals that here the dominating frequency is the double of f_c of Mode 4 (1194 Hz). This indicates that Mode 4 shows the most vibrations and could be described as unstable machining.

Table 6 Spindle speed, time per rotation and cutting edge frequency for all modes

	Mode 1	Mode 2	Mode 3	Mode 4
spindle speed n (rot/min)	5305	5305	5305	11937
duration per rotation t_r (sec)	0.0113	0.0113	0.0113	0.005
cutting edge frequency f_c (Hz) $f_c = 1/t_r \cdot 3$	265	265	265	597

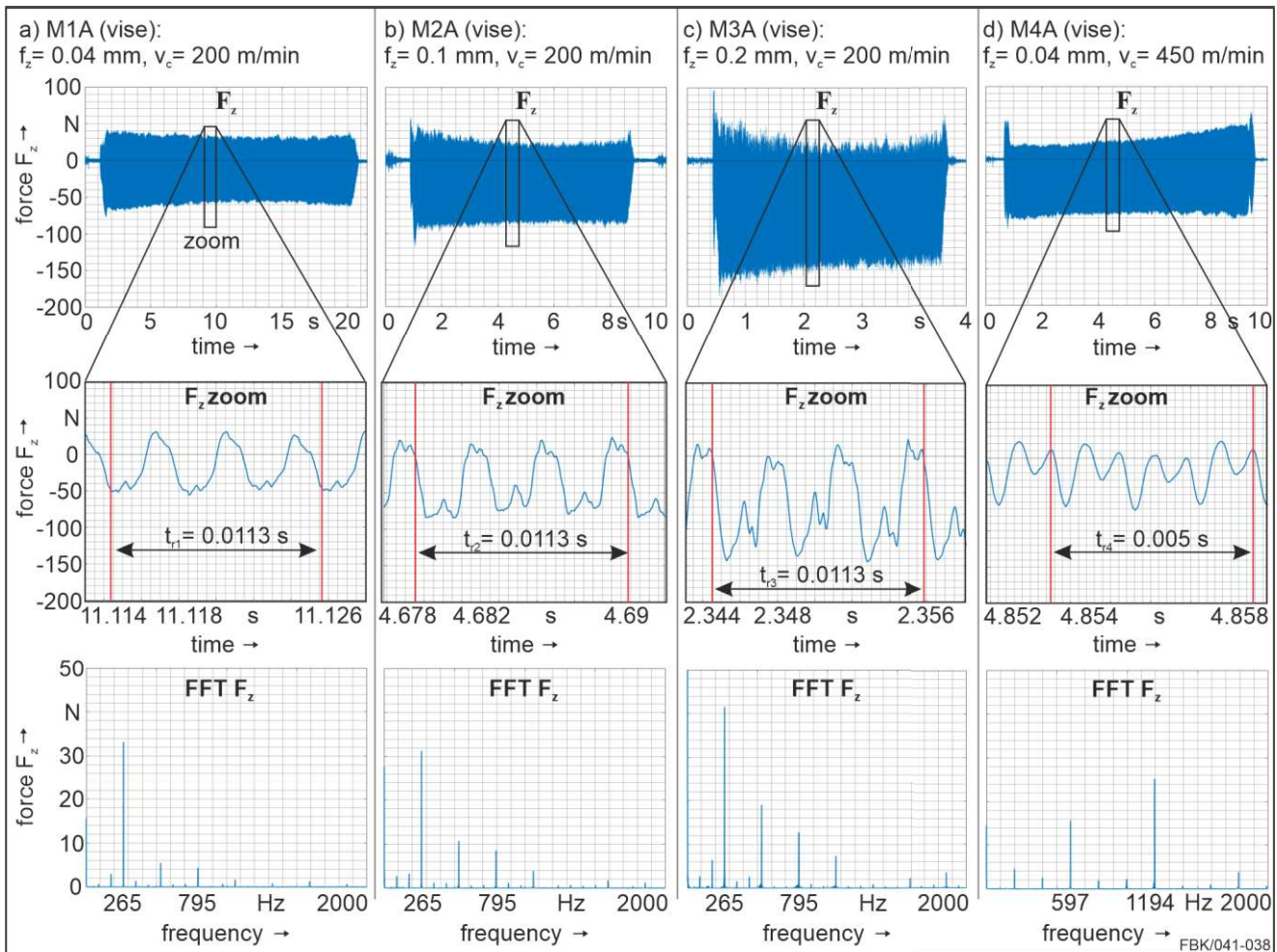


Fig. 9 Force signals F_z and FFT for pass 14 of one vise sample per mode

Figure 10 shows the forces F_z and their FFT for the samples machined in the side clamps M1D, M2D, M3D and M4D. In general, the force signal looks the same as previously discussed for the samples machined in the vise. But all forces contain more scatter (more higher frequencies of small magnitude) compared to the samples machined in the vise. The amplitudes of the forces for the cutting edge frequency are lower compared to the samples machined in the vise. But for Mode 4 the same trend as previously discussed occurs. Only Mode 4 has its highest force amplitude at the double cutting edge frequency (1194 Hz). Modes 1, 2 and 3 have their highest amplitude at their cutting edge frequency (265 Hz). This indicates that vibrations for Mode 4 are independent of the investigated clamping strategy.

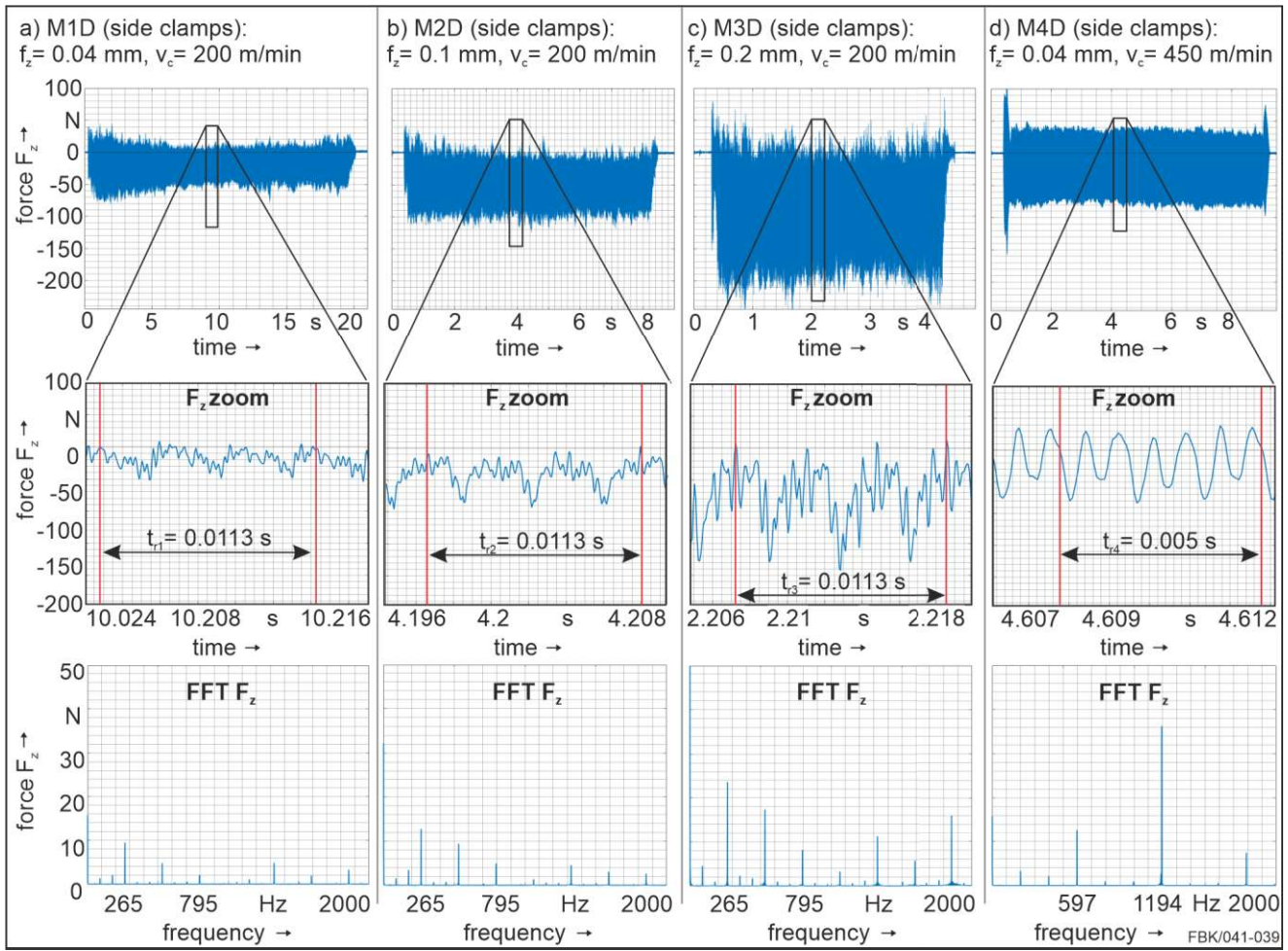


Fig. 10 Force signals F_z and FFT for pass 14 of side clamp sample for each mode

3.2 Temperature analysis

The maximum temperature is reached shortly after the tool was moved over the thermocouple. Figure 11a shows the average maximum temperature for each mode (3 measurements per mode). All temperatures at a depth of approximately 100 μm are on a low level and lie in a range between 30 and 55 $^{\circ}\text{C}$ (see Fig. 11). The actual distance of the thermocouple face to the surface varies and lays in the range of 75 to 125 μm , but has almost no effect on the measured temperatures (see Fig. 11b). The highest temperatures were recorded for Mode 1, with lowest feed. An increase in feed per tooth (Mode 1 < Mode 2 < Mode 3) leads to a decrease in temperatures that occur at a depth of 80 to 120 μm underneath the cutting surface. Higher cutting speeds (with constant feed per tooth) result in a slight decrease in temperatures at a depth of around 100 μm , compare Mode 1 and Mode 4. The reason for this effect is that for the given machining parameter Mode 1, the tool moves slower and the sample heats up for a longer time period. Therefore, Mode 1 with the lowest feed rate results in the highest temperatures. A comparison of Mode 2 and Mode 4 (which have similar feed rate – see Table 2) show that Mode 4 (higher cutting speed) results in higher temperatures, which can be explained by the higher amount of friction and shearing events per second for the higher cutting speed.

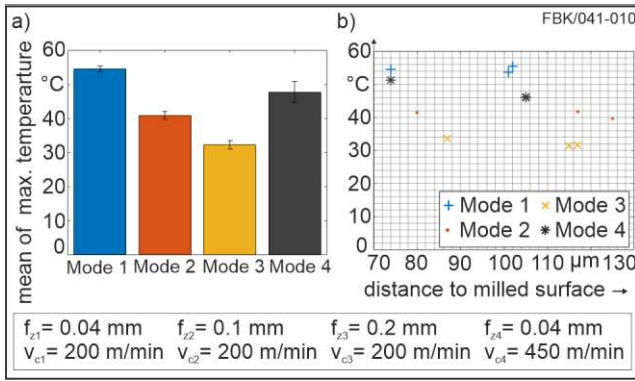


Fig. 11 Mean of maximum temperature per mode (a) and temperature over distance to milled surface distribution (b)

3.3 Machining induced residual stress analysis

Investigations on the MIRS are divided in following sections

- MIRS repeatability within one sample – leads to increased understanding of measurement process and variability of MIRS within a single sample
- MIRS repeatability of multiple samples sharing same machining condition – leads to increased understanding of MIRS consistency among different samples
- Comparison of MIRS from different machining modes – leads to increased understanding of influence of machining parameters on MIRS
- Comparison of MIRS from different clamping strategies – leads to increased understanding of influence of clamping on MIRS

3.3.1 Machining induced residual stress repeatability within one sample

The following discussion is based on measurements on M2B (Mode 2), which exhibits a representative RS introduced by milling found across all four modes. Figure 12 shows three RS measurements on M2B, measured at position I, II and III. Overall the three measurements agree well. They show similar stress profiles with compressive residual stresses near the surface and similar penetration depth t_p . A high precision is given for two out of three measurements (pos. II and III) for depths deeper than ~ 20 μm. Position I shows slightly deeper stresses than positions II and III. In general, the first measured points at a depth smaller than 20 μm show a difference in the magnitude of normal and shear residual stress. This is a result of the uncertainty of the measurement technique hole-drilling itself, which is indicated by the error bars in Fig. 12. The hole-drilling technique has the highest uncertainty at the first measured shallow depth (for more information see [13]).

M2B position II picks up tensile stresses in x- and y- direction for depths greater than 80 μm. These are the left-over IBRS after the stress relief process in the middle of the bulk. Position I and position III show compressive stresses at those depths according to their position closer to the edges.

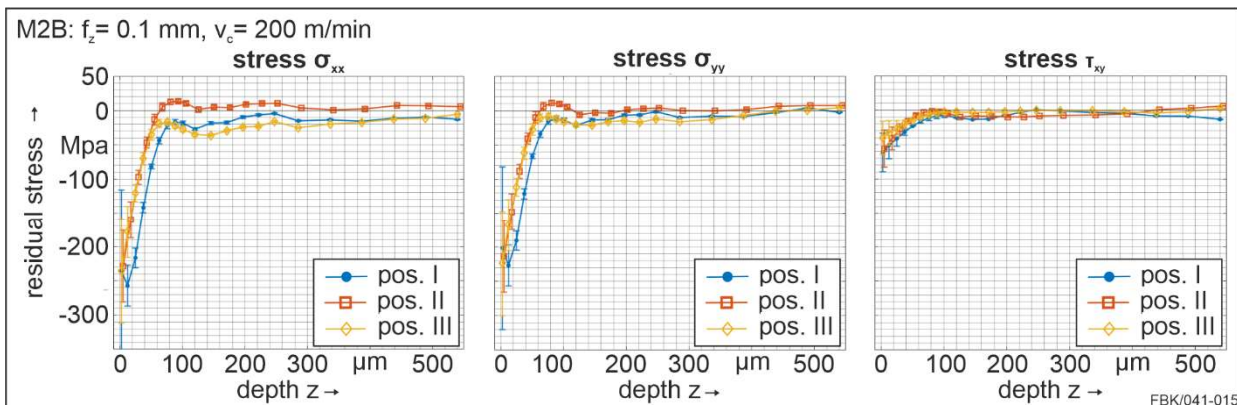


Fig. 12 MIRS measurements on M2B, error bars represent HD measurements uncertainty

3.3.2 Machining induced residual stress repeatability of multiple samples sharing the same machining condition

Model:

All three Mode 1 measurements (M1A, M1B, M1C) show a square root shaped profile for all three stress components σ_{xx} , σ_{yy} and τ_{xy} , except that the MaxRS exist at the shallowest depth, so that t_m is very small (see Fig. 13). The normal stresses σ_{xx} , σ_{yy} are similar in their magnitude. Shear stresses are smaller. M1A and M1C are highly repeatable. Almost all interpolated stresses are within the standard deviation of each other. The MaxRS is about -125 ± 34 MPa (M1A) and -146 ± 5 MPa (M1C) in x-direction, and -141 ± 35 MPa (M1A), -137 ± 19 MPa (M1C) in y-direction. Their penetration depth t_p is at about $60 \mu\text{m}$ for σ_{xx} and σ_{yy} . In shear direction their MaxRS_{xy} is -43 ± 7 MPa with a penetration depth of about $25 \mu\text{m}$. The stress profile of M1B is similar, but in general shallower with less MaxRS (-75 ± 32 MPa in x-direction and -95 ± 39 MPa in y-direction). The penetration depth is also lower compared to M1A and M1C at about $35 \mu\text{m}$ (normal stresses). The shear stress profile is lower than 20 MPa with the MaxRS_{xy} (-13 ± 8 MPa) at the first depth. A comparison of the forces shows the same trend for F_y and F_z (see Fig. 7). F_y and F_z of M1B are smaller than M1A and M1C. This trend does not show up for F_x .

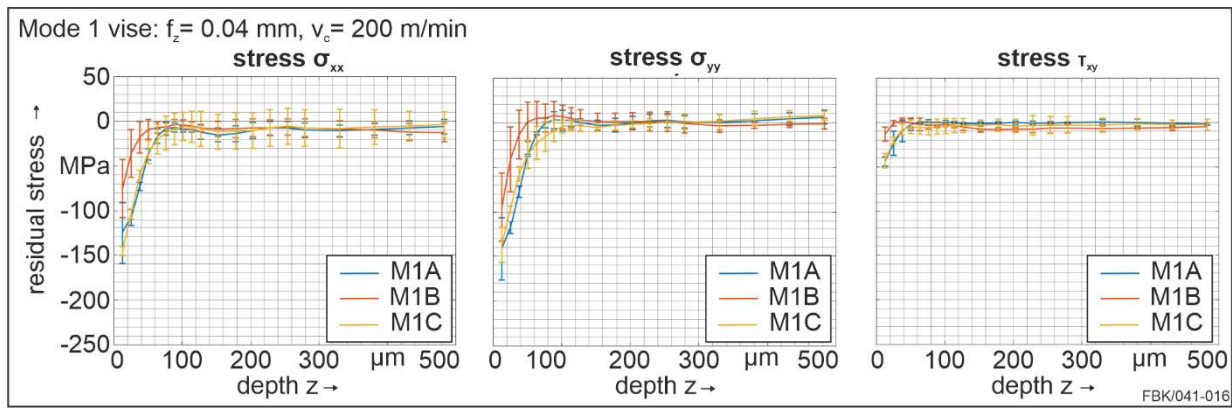


Fig. 13 MIRS Mode 1 vise (M1A, M1B, M1C), error bars represent RSTD

Mode 2:

Similar to Mode 1, M2A and M2B stress profiles show negative RS profiles for all three stress components σ_{xx} , σ_{yy} and τ_{xy} with the MaxRS at the first measured depth (see Fig. 14). M2C has their normal MaxRS at the second interpolated depth. Besides that, M2B and M2C are highly repeatable, almost all interpolated stresses are within each other's standard deviation. M2A has a similar stress profile with higher stresses at depths from 50 to $76 \mu\text{m}$. The normal MaxRS are about -162 ± 31 MPa (M2C), -189 ± 16 MPa (M2A) and -207 ± 43 MPa (M2B) in x-direction, and -164 ± 28 MPa (M2C), -195 ± 14 MPa (M2A) and -189 ± 33 MPa (M2B) in y-direction. The penetration depth t_p of the normal stresses is at about $65 \mu\text{m}$ (M2B, M2C) and $85 \mu\text{m}$ (M2A). The MaxRS_{xy} is -44 ± 10 MPa (M2B), -51 ± 20 MPa (M2C) and -61 ± 18 MPa (M2A) with t_p in shear direction at $40 \mu\text{m}$ (M2B, M2C) and $64 \mu\text{m}$ (M2A). A comparison of the forces shows that F_y is also the biggest for M2A. This trend does not follow for F_z and F_x .

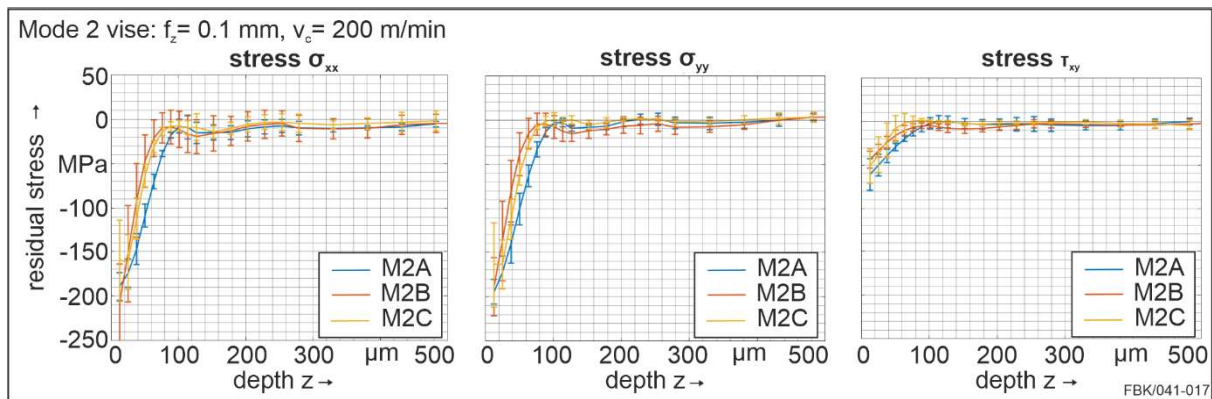


Fig. 14 MIRS Mode 2 vise (M2A, M2B, M2C), error bars represent RSTD

Mode 3:

The stress profiles of Mode 3 samples show a typical square root shape with a pronounced MaxRS for all three samples at greater depths (see Fig. 15). The normal MaxRS is about -103 ± 32 MPa (M3B), -148 ± 36 MPa (M3C) and -145 ± 33 MPa (M3A) in x-direction, and -124 ± 25 MPa (M3B), -165 ± 39 MPa (M3C) and -127 ± 26 MPa (M3A) in y-direction. M3A and M3B show also a pronounced square root shape profile of the shear stress. MaxRS_{xy} is -47 ± 12 MPa (M3B), -55 ± 12 MPa (M3C) and -46 ± 13 MPa (M3A). The depth of the normal MaxRS is about $64 \mu\text{m}$ (M3B), $51 \mu\text{m}$ (M3A, M3C x-direction) and $38 \mu\text{m}$ (M3C y-direction). The depth of the MaxRS_{xy} is at $38 \mu\text{m}$ (M3A, M3B) and $25 \mu\text{m}$ (M3C). The penetration depth is about the same for the normal stresses ($180 \mu\text{m}$) and in shear direction $90 \mu\text{m}$ (M3B, M3C), $140 \mu\text{m}$ (M3A) respectively. M3B shows the smallest force F_z . Aside from that, there is no trend or link to the stresses visible.

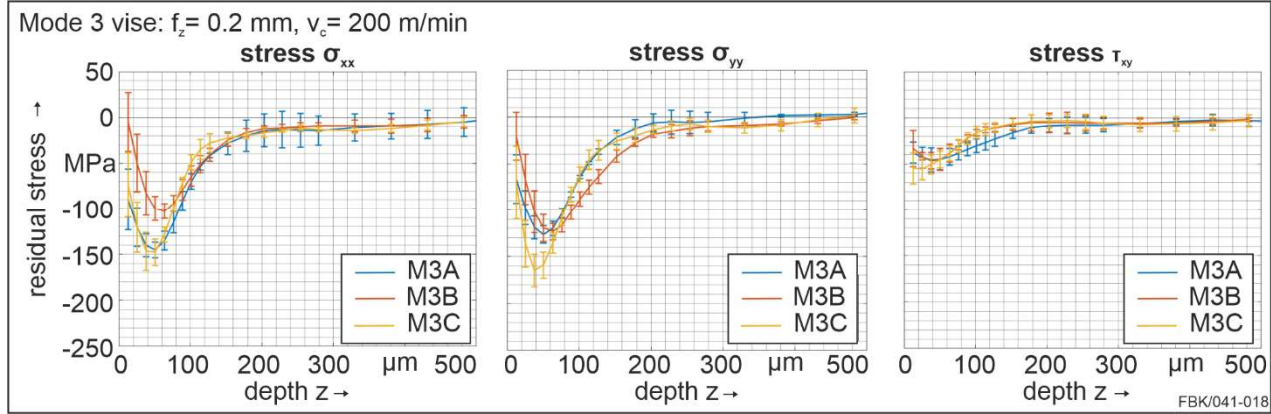


Fig. 15 MIRS Mode 3 vise (M3A, M3B, M3C), error bars represent RSTD

Mode 4:

The normal stress profiles of Mode 4 samples vary (see Fig. 16) more than for the other modes. RS of M4A and M4C have their MaxRS at the first interpolated depth. The MaxRS of M4B is at the second interpolated depth in x- and y-direction. But it should be considered that the standard deviation of the first interpolated depth is relatively high (35 and 50 MPa). The magnitude of MaxRS varies more than for the other modes: -224 ± 19 MPa (M4C), -162 ± 35 MPa (M4B), -63 ± 19 MPa (M4A) in x-direction and -217 ± 6 MPa (M4C), -134 ± 13 MPa (M4B), -61 ± 16 MPa (M4A) in y-direction. From greater depths ($30 \mu\text{m}$) on, M4B and M4C normal RS profiles are similar with a penetration depth of $75 \mu\text{m}$. M4A is shallower with a penetration depth of $40 \mu\text{m}$. The shear stresses of M4C and M4B are repeatable with MaxRS_{xy} -54 ± 15 MPa at the first measured depth and a penetration depth of $40 \mu\text{m}$. The shear stress profile of M4A is also shallower with smaller MaxRS_{xy} (-33 ± 3 MPa) and t_{pxy} $20 \mu\text{m}$. There can be no link or trend to the magnitude of measured forces drawn. As already mentioned in the force analysis section, a closer look at the force signals reveals that in z-direction an oscillating behavior is visible. The FFT shows its highest peak for the double cutting edge frequency (see Fig. 9). These vibrations may be the reason for the described differences in RS profiles.

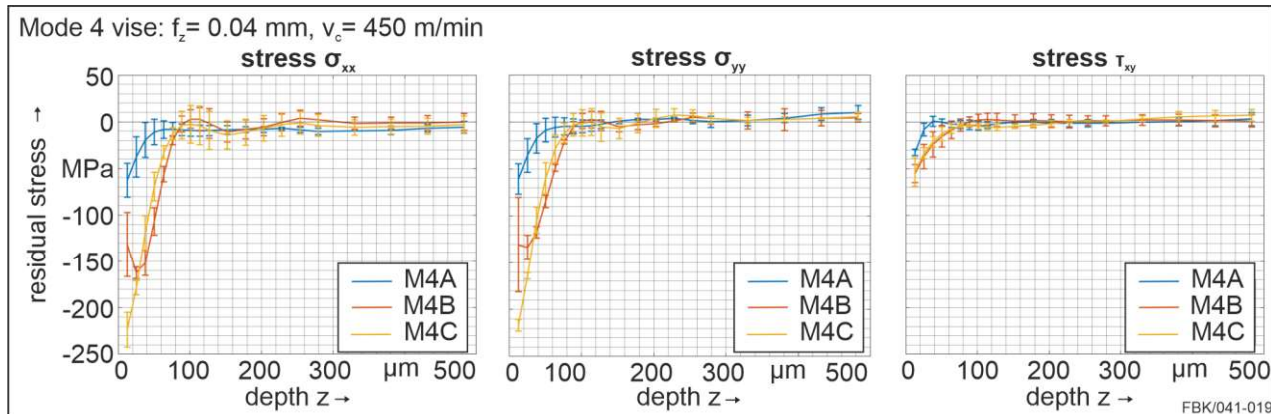


Fig. 16 MIRS Mode 4 vise (M4A, M4B, M4C), error bars represent RSTD

In summary the comparison of the different samples sharing the same machining mode shows that there is a repeatability to a certain amount present, where Mode 4 shows the highest variation. It has to be considered that two out of three profiles for Mode 1 and 2 are highly repeatable, but one profile differs slightly in form of a shallower, deeper respectively, stress profile. Variation within the different machining modes are quantified in the next section (3.3.3). Furthermore, wafer experiments will highlight if the mentioned differences in MIRS also result in different distortions (see section 3.4 Wafer analysis).

3.3.3 Comparison of machining induced residual stresses from different machining modes and their repeatability

Figure 17 highlights that higher feeds result in a higher penetration depths of RS profile and in higher depth of the MaxRS. Only Mode 3 shows a perfect square root shaped profile with pronounced MaxRS at greater depths and less compressive RS near the surface - whereas the MaxRS for lower feeds (Mode 1 and 2) are found closer to the surface, with Mode 2 having the highest MaxRS. An explanation for those effects is, that the increased load on the sample, due to greater uncut chip thickness and material removal rate (see Table 1), leads to larger plastically deformed areas and therefore deeper residual stresses and the shift of the maximum stresses deeper into the workpiece. Once the maximum of stress is at greater depth, the stresses near the surface are lower to remain in mechanical equilibrium (see Mode 3 stress Fig.17) [7]. Furthermore, the compressive residual stress distribution results from the combined effect of both competing processes, direct plastic surface deformation and plastic deformation of deeper layers due to Hertzian pressure [26]. It seems that for Mode 1 and Mode 2 much energy is consumed for direct plastic deformation of the surface, so that the effect of Hertzian pressure cannot be dominant. But here it should be also considered that the measurement technique HD has its highest uncertainty at the first measured depth. Besides, the temperatures do not seem to play a role, since they are on a similar low level (30 °C to 55 °C at a depth of 100 µm) for all three modes (see Fig. 11).

A comparison of the measured RS to the RS due to milling aluminum alloys found in the literature with similar tools shows that a similar RS depth profile with compressive RS in the subsurface and a maximum close to the surface is evident. The measured MaxRS are smaller compared to the ones found in [7] (see section 1. Introduction), because different cutting parameters (a_e and a_p) and tool diameter were used, which also lead to smaller forces compared to the ones shown in [7]. The increased depth of the MaxRS with an increased feed also agrees with findings in [7].

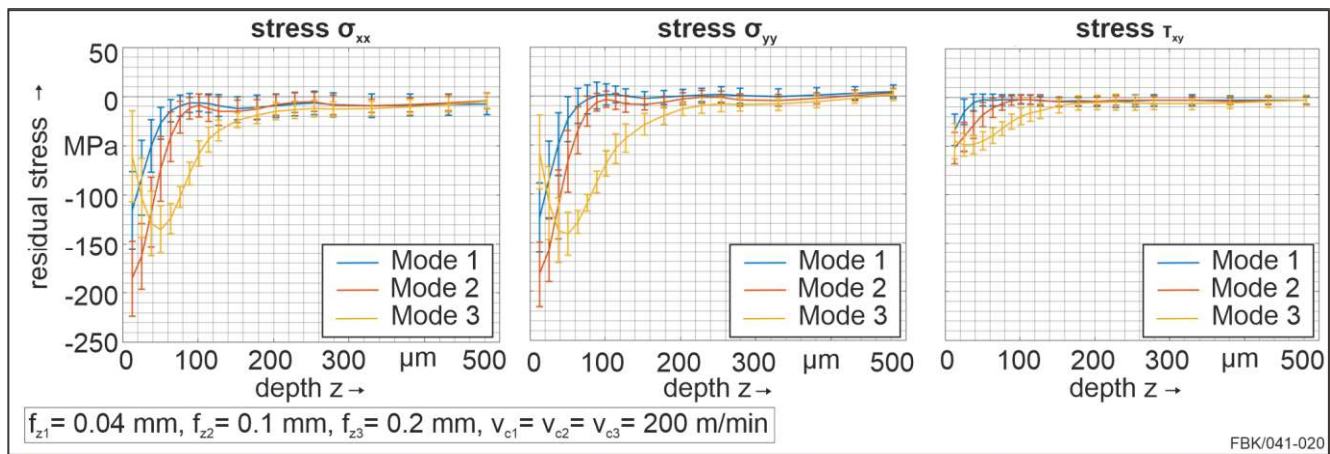


Fig. 17 MIRS inter mode comparison for variation of feed (Mode 1, Mode 2, Mode 3) vise, error bars represent RSTD

The variation of the cutting speed (see Fig 18) shows that the average MIRS profiles look similar, although Mode 4 shows the most variation, which is indicated by its high standard deviation. This can be explained by the forces, which are similar in their magnitude as well. Furthermore, the temperature experiments showed that there is no big temperature difference for both modes (see Fig. 11). This observation also agrees with similar trends found in the literature [7].

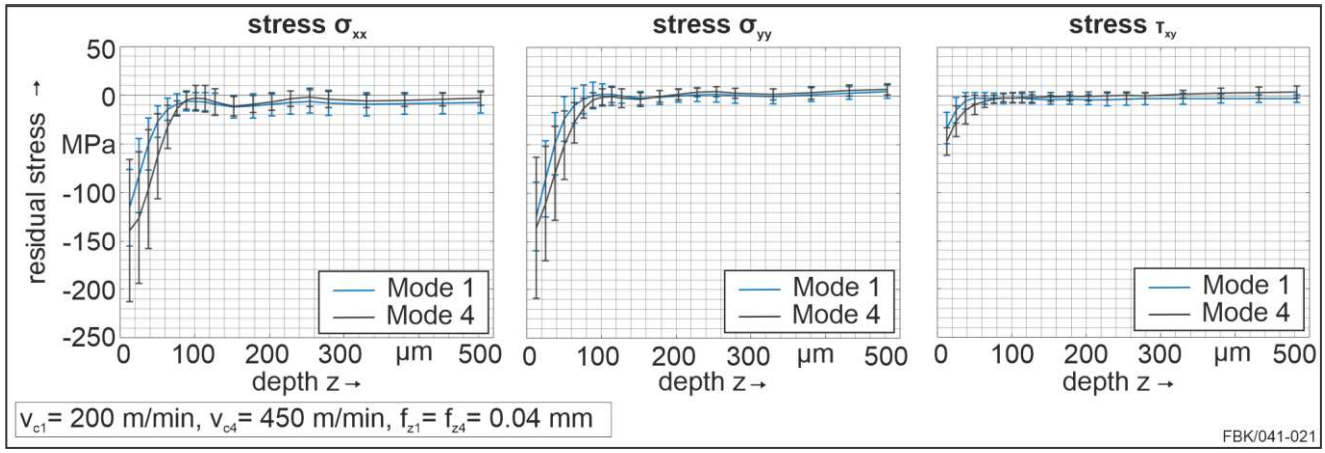


Fig. 18 MIRS inter mode comparison for variation of cutting speed (Mode 1, Mode 4) vise, error bars represent RSTD

To quantify the repeatability of the MIRS resulting from the four different modes the average of the MaxRS of each mode, its RSTD, the average of the penetration depth t_p and its RSTD were computed from all 9 MIRS measurements for each mode (see Table 7). As previously described Mode 4 normal stresses show the highest variation, where the RSTD reaches 54 % of the MaxRS. For the other modes the RSTD is lower (especially for Mode 2 and 3), where the highest RSTD goes down to 34 % (Mode 1), 29 % (Mode 2) and 25 % (Mode 3) of their MaxRS. In the shear direction Mode 1 machining causes the highest variation in MaxRS_{xy} (49 %). In general, it can be seen that the RSTD of the MaxRS increases for lower measured and shallower RS (see Table 7 Mode 1 and 4). The measurement technique HD might contribute to this fact, because the qualities to be observed here are close to the limits of the resolution of the observation technique itself [13]. A similar trend is found for the penetration depth t_p , where the highest variation shows up for the lowest shear residual stresses (Mode 1: 52 % and Mode 4: 41 %). The variation in the depth of the MaxRS t_m seems low for all modes, because for almost all of the MIRS measurements (except Mode 3) the MaxRS are found at the first measured depth. It can't be quantified, because the first measured depth varies (4 μm to 12 μm) and it is therefore not known at which depth exactly the MaxRS occur. However, this is not true for Mode 3, where the MaxRS are found at deeper depths. Here a variation of 50 ± 8 μm (x-direction), 52 ± 6 μm (y-direction) and 31 ± 22 μm (shear direction) was found.

Table 7 Repeatability standard deviation (RSTD) of MaxRS and penetration depth t_p for all modes

	Mode 1	Mode 2	Mode 3	Mode 4
MaxRS _x ± RSTD _x (MPa)	115 ± 39 (34 %)	185 ± 39 (21 %)	135 ± 24 (18 %)	139 ± 73 (53 %)
MaxRS _y ± RSTD _y (MPa)	125 ± 36 (29 %)	182 ± 32 (18 %)	141 ± 23 (16 %)	136 ± 73 (54 %)
MaxRS _{xy} ± RSTD _{xy} (MPa)	33 ± 16 (49 %)	52 ± 15 (29 %)	49 ± 12 (25 %)	47 ± 14 (30 %)
$t_{px} \pm t_p$ -RSTD _x (μm)	56 ± 22 (39 %)	74 ± 12 (16 %)	177 ± 62 (35 %)	62 ± 18 (29 %)
$t_{py} \pm t_p$ -RSTD _y (μm)	56 ± 19 (34 %)	70 ± 11 (16 %)	180 ± 22 (12 %)	62 ± 18 (29 %)
$t_{pxy} \pm t_p$ -RSTD _{xy} (μm)	21 ± 11 (52 %)	49 ± 14 (29 %)	105 ± 26 (25 %)	34 ± 14 (41 %)

3.3.4 Comparison of MIRS from different clamping strategies

The comparison of the MIRS profiles of samples machined in the vise and side clamps shows almost no significant differences for Mode 1 and Mode 2 (see Fig. 19 and Fig. 20). The differences of the MaxRS of the vise and side clamps are quantified by their relative change (MaxRS_{side clamps}/MaxRS_{vise} - 1). The change of MaxRS of Mode 1 is -15 % (x-direction), -11 % (y-direction) and -62 % (xy-direction). For Mode 2 the difference of MaxRS is quantified to -27 % (x-direction), -3 % (y-direction) and 5 % (xy-direction). So, the highest differences are found for the MaxRS_x for Mode 2 and the MaxRS_{xy} for Mode 1. But it has to be considered, that their error bars overlap and the MaxRS are at very shallow

depths, where the highest uncertainty of the HD technique takes place. In summary, it can be stated that the RS depth profiles for Mode 1 and Mode 2 are independent of the two investigated clamping strategies.

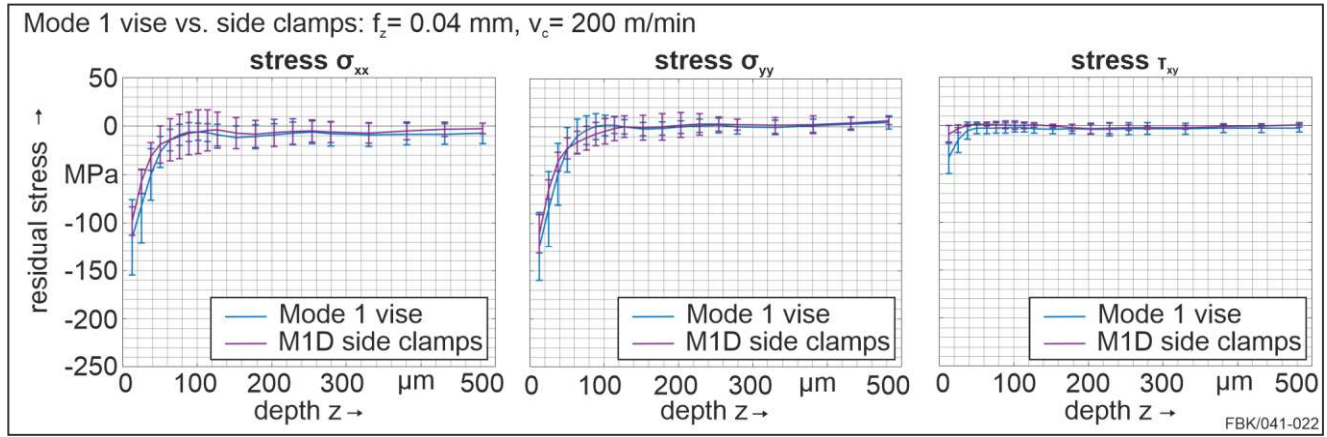


Fig. 19 MIRS Mode 1 comparison for vise and side clamps, error bars represent RSTD

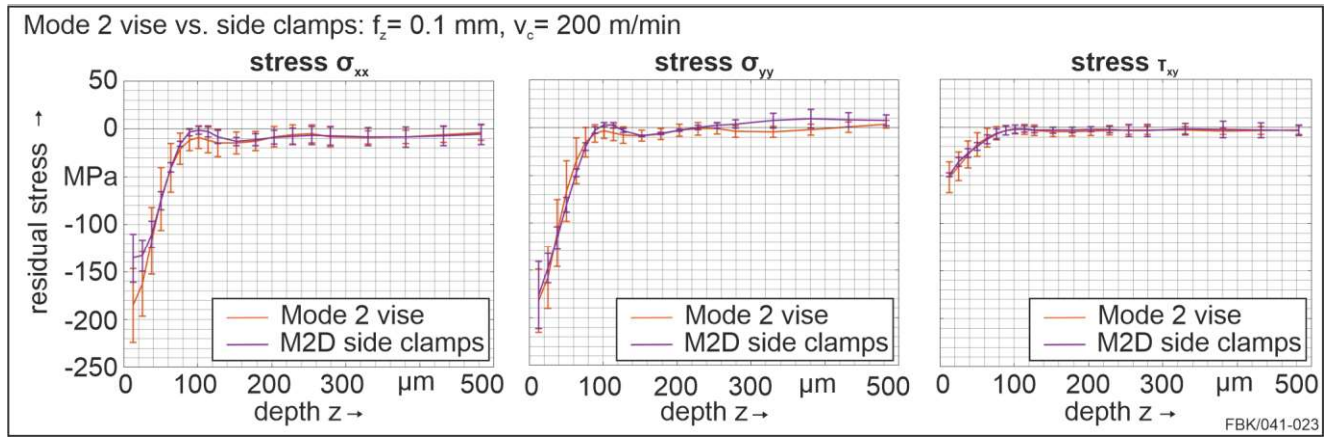


Fig. 20 MIRS Mode 2 comparison for vise and side clamps, error bars represent RSTD

Mode 3 stress profiles are also similar with a high repeatability of the penetration depth and the depth of MaxRS (see Fig. 21). The magnitude of compressive RS for the machined sample in side clamps (M3D) seems to be higher than for the samples machined in the vise. But for the normal stresses it has to be considered that their RSTD lays in each other's range, which means that the difference due to clamping is not statistically significant. The magnitude of shear stress with side clamps is higher than that with the vise and, in contrast, the difference is significant for depth smaller than 80 μm. The differences of the MaxRS are quantified to 21 % (x-direction), 27 % (y-direction) and 42 % (xy-direction).

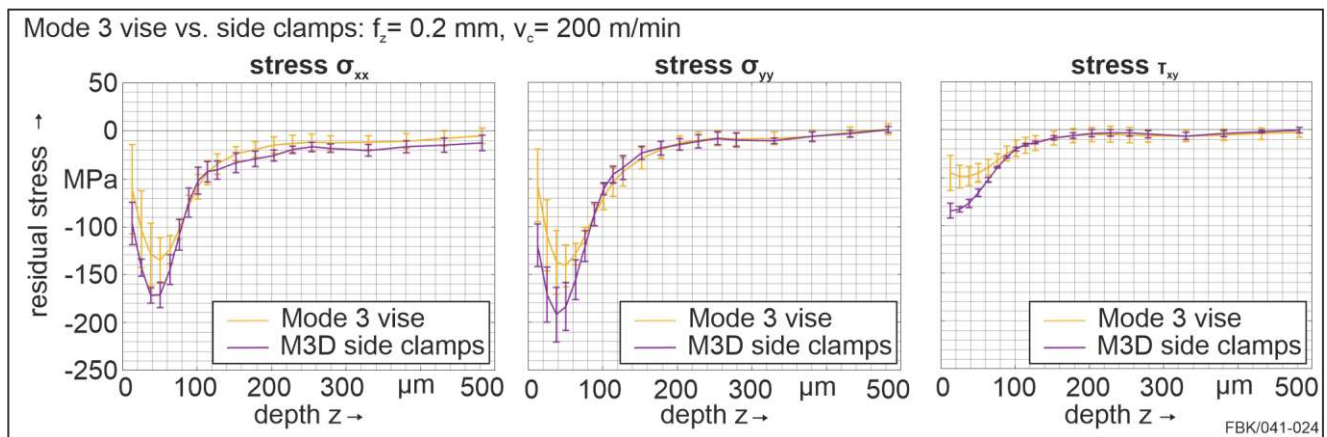


Fig. 21 MIRS Mode 3 comparison for vise and side clamps, error bars represent RSTD

A comparison between RS of Mode 4 samples which are machined in the vise and side clamps is difficult because, as was stated earlier, the RS resulting from machining of samples clamped in the vise have high variability. Therefore, two

instead of one sample was machined in the side clamps (M4D, M4E) to analyze if this condition depends on the clamping device or not. Fig. 22 highlights that the stress profile of M4E is shallower for all three stress components compared to M4D. The error bars of M4D and M4E do not touch each other for shallow depth smaller than 90 μm . A comparison to the stresses resulting from samples machined in the vise (Mode 4 vise), shows that the values of M4D are within the standard deviation from the average Mode 4 vise stresses. The differences of the MaxRS are quantified to -51 % (x-direction), -50 % (y-direction) and -64 % (xy-direction) by using the average of the MaxRS of the two samples clamped in side clamps and comparing it to the average MaxRS of the samples machined in the vise. A closer look at the force signals of M4D and M4E reveals that the vibrations have not improved (see Fig. 10). Mode 4 remains still as an unstable machining independent of the fixture.

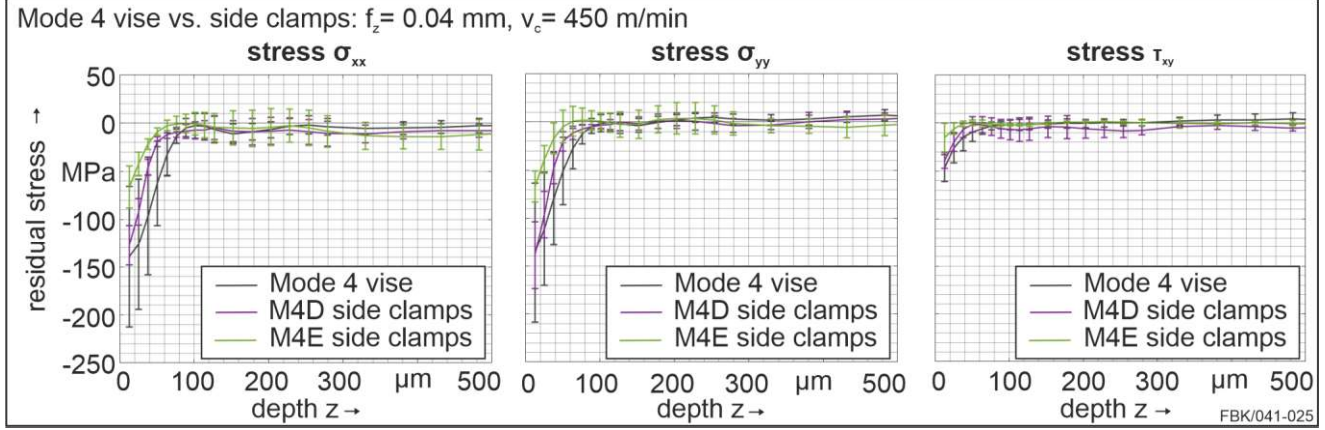


Fig. 22 MIRS Mode 4 comparison for vise and side clamps, error bars represent RSTD

In general, the stress profiles of the samples machined in the side clamps are similar to the ones machined in the vise. The clamping behavior in terms of clamping forces and stiffness of the system is similar and does not significantly influence the MIRS.

3.4 Wafer analysis

The wafer experiments are designed to show the distortion potential due to the MIRS. It is investigated whether those differences detected in the measured stress profiles cause different machining induced distortion. Furthermore, the distortion due to the different machining modes is compared. In addition, the numerical FEM simulations analyze whether those measured stresses are consistent with the measured distortion (see section 3.4.2 FEM wafer distortion analysis).

3.4.1 Comparison of experimental data

Figure 23 shows the measured wafer distortion M1A (Mode 1) as an example. Here, the distortion is defined as the out-of-plane (xy-plane) displacement of the wafer. The machined surface becomes convex ($\cap$ -shaped) due to the compressive MIRS at the top milled surface (see Fig. 23a). The color map in Fig. 23b mimics looking down at the milled surface with positive distortion in the z-direction (into the surface). Its maximum distortion is found at the top left (0 mm, 0 mm) and bottom right corner (25 mm, 25 mm), **because the shear stresses cause a torsional moment in addition to the bending moment induced by the normal RS** [13, 28]. **Therefore**, the shear stress is responsible for the diagonal orientation of the maximum distortion. In order to compare the distortion of different samples, the distortions along the diagonal lines, top left (0 mm, 0 mm) to bottom right corner (25 mm, 25 mm) (peak distortion diagonal (PDD)) and bottom left (0 mm, 25 mm) to top right (25 mm, 0 mm) (flat distortion diagonal (FDD)), are plotted (see Fig. 23c). A polynomial fit of the order 5 is applied to the data to smooth it.

Furthermore, the maxima for the PDD and the FDD of different wafers are compared. The distortion value at each corner is computed and averaged for the peak distortion corners (PDD_{max}) and the flat distortion corners (FDD_{max}) respectively (see Table 8). The ratio of PDD_{max} (or FDD_{max}) of two different wafers show how close their distortion is (e.g. PDD_{max} M1A / PDD_{max} M1B). Here 100 % means that their maximum magnitude of distortion at the specific corners is the same.

It should be noted that for samples M1B and M3B the analysis space of 23x23 mm² was trimmed due to measurement errors close to the edges of the wafers.

Table 8 Wafer experimental maximum distortion

Mode (<i>x</i> -position of measured edges)	Mode 1 (<i>x</i> ₁ =2.6 mm & <i>x</i> ₂ =22,4 mm)		Mode 2 (<i>x</i> ₁ =1 mm & <i>x</i> ₂ =24 mm)		Mode 3 (<i>x</i> ₁ =2.4 mm & <i>x</i> ₂ =22,6 mm)		Mode 4 (<i>x</i> ₁ =1 mm & <i>x</i> ₂ =24 mm)	
sample ID	M1A	M1B	M2A	M2C	M3C	M3B	M4B	M4A
PDD _{max} (mm)	0.062	0.045	0.14	0.116	0.152	0.116	0.123	0.047
FDD _{max} (mm)	0.024	0.02	0.056	0.032	0.032	0.025	0.028	0.014
ratio PDD _{max}	73 %		83 %		76 %		38 %	
ratio FDD _{max}	83 %		57 %		78 %		50 %	

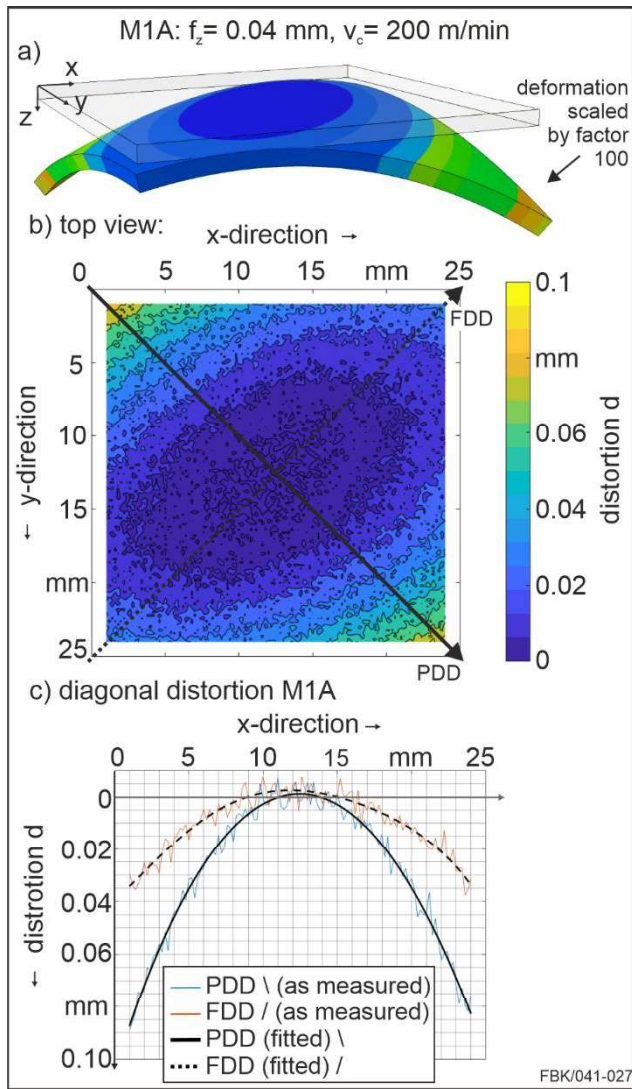


Fig. 23 Qualitative shape of wafer distortion (a), contour plot (b) and diagonal distortions of M1A (c)

The distortion of the Mode 1 wafers M1A and M1B are compared in Figure 24. It can be seen that the distortion shape of both wafers is the same convex shape as discussed previously. The distortion of M1B is smaller than M1A, which can be seen clearly from both diagonal line distortion plots (see Fig. 24). The average maximum distortion of the M1B PDD is 73 % of M1A and 83 % for the averaged maximum of the FDD (see Table 8). This behavior can be explained

by the differences detected in the MIRS profiles (see section 3 MIRS analysis). M1B has shallower MIRS with less MaxRS (in all directions) and penetration depth t_p compared to M1A (see Fig. 13).

The same trend occurs for wafers M2A and M2C, both machined with Mode 2. The one cut out of the sample with shallower MIRS measured, shows less distortion (see Fig 25 and compare Fig. 14). The average maximum distortion of the PDD of M2C is 83 % of M2A and 57 % for the averaged maximum of the FDD (see Table 8).

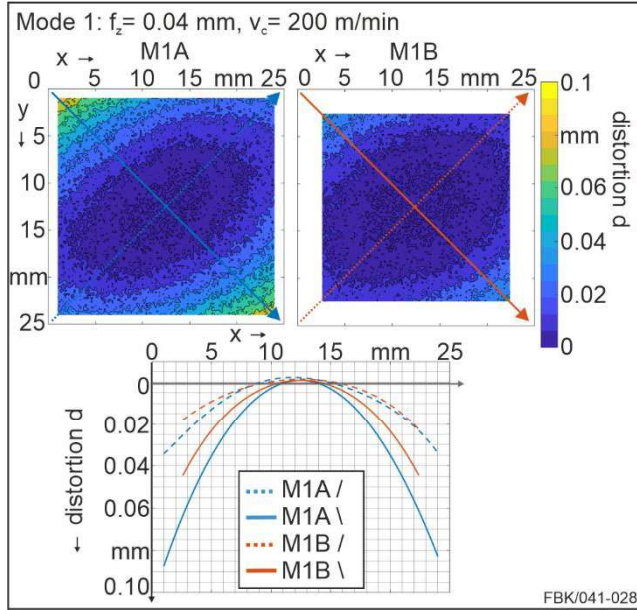


Fig. 24 Mode 1 wafer M1A and M1B distortion

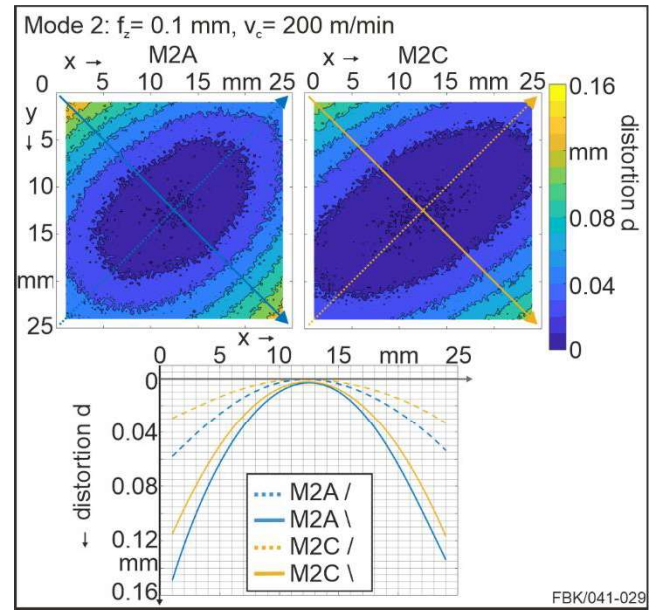


Fig. 25 Mode 2 wafer M2A and M2C distortion

The distortion shape of the Mode 3 wafers M3B and M3C is also convex (see Fig. 26). It can be seen that their distortion is consistent. The average maximum distortion of the PDD of M3B matches the one of M3C by 76 %. The averaged maximum of the FDD of M3B accounts for 78 % of M3C's FDD (see Table 8). M3B has less MaxRS (in all directions) than M3C (see Fig. 15), which also results in a lower distortion.

The distortions of the Mode 4 wafers M4A and M4B show the same convex shape with their maximum distortion at the corners (0,0) and (25, 25) (see Fig. 27). It can be seen that the distortion of M4A is significantly smaller than M4B. The average maximum distortion of the M4A PDD is 38 % of M4B and 50 % for the averaged maximum of the FDD (see Table 8). This is due to the differences in MIRS (see section 3 MIRS analysis). M4A has significant shallower MIRS with less MaxRS (in all directions) compared to M4B (see Fig 16).

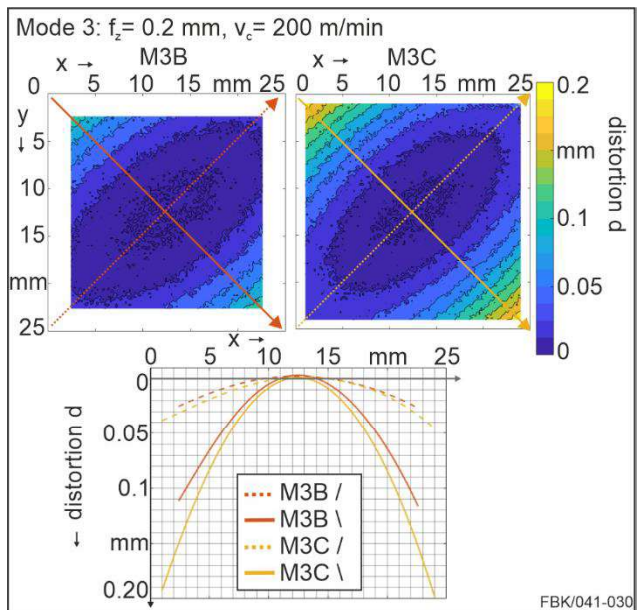


Fig. 26 Mode 3 wafer M3B and M3C distortion

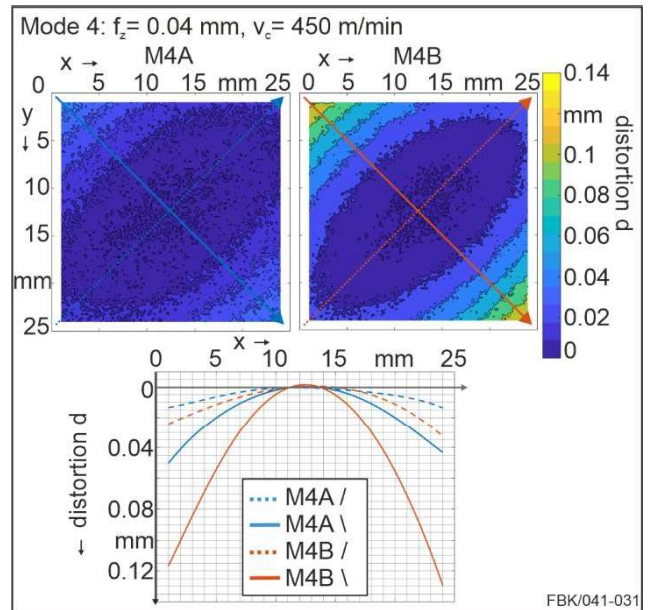


Fig. 27 Mode 4 wafer M4A and M4B distortion

In summary, small differences in MIRS for Mode 1, 2 and 3 result in small changes in their distortion. Big differences in Mode 4 MIRS also lead to big differences in distortion of Mode 4 wafers. Furthermore, Fig. 28a shows that with increasing feed the maximum distortion increases. The distortion of the opposite diagonal, the flat distortion, does not show this trend, because of the high normal stresses of Mode 2 compared to Mode 3 (compare Fig. 17). The comparison of the variation in cutting speed shows no clear trend, because Mode 4 has such big variations in MIRS and distortions (Fig. 28b). In general, it can be stated that the MIRS and the wafer distortion are related, with more and/or deeper compressive RS causing more distortion.

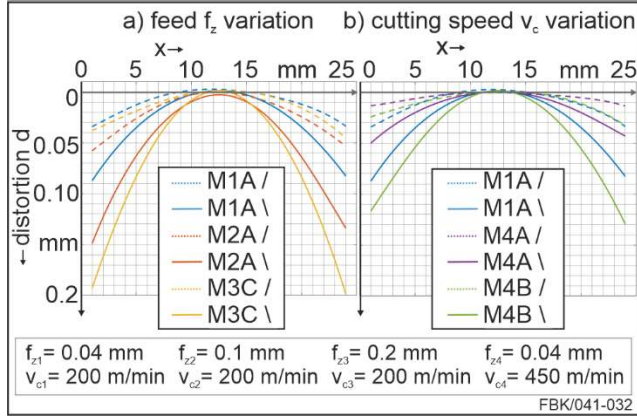


Fig. 28 Inter mode comparison of wafer distortion for feed variation (a) and cutting speed variation (b)

3.4.2 FEM wafer distortion analysis

Figure 29 shows the distortion of Mode 1 M1A and M1B wafer and the simulated distortions due to the measured MIRS from M1A (averaged three measurements), M1B respectively, as contour plots and their diagonal distortions. The distortion of simulation and experiment of M1A match. Both show the previously described convex shaped distortion on a similar level, but the experimental data is more twisted than the simulation. This indicates that shear stresses used for the simulation are not fully correct. The line plots show that the real distortion is bigger than the simulated one. Table 9 highlights that the experimental averaged maximum distortion of the PDD (FDD) of M1A is reached by the simulation up to 75 % (65 %). A similar behavior is visible for M1B. But here the simulated shape differs in a way that the FDD shows almost no bending. This indicates that the MIRS used for the simulation were not fully correct, which is also suggested by the higher RSTD of the M1B MIRS (see Fig. 13). However, the PDD reaches 76 % of the measured data.

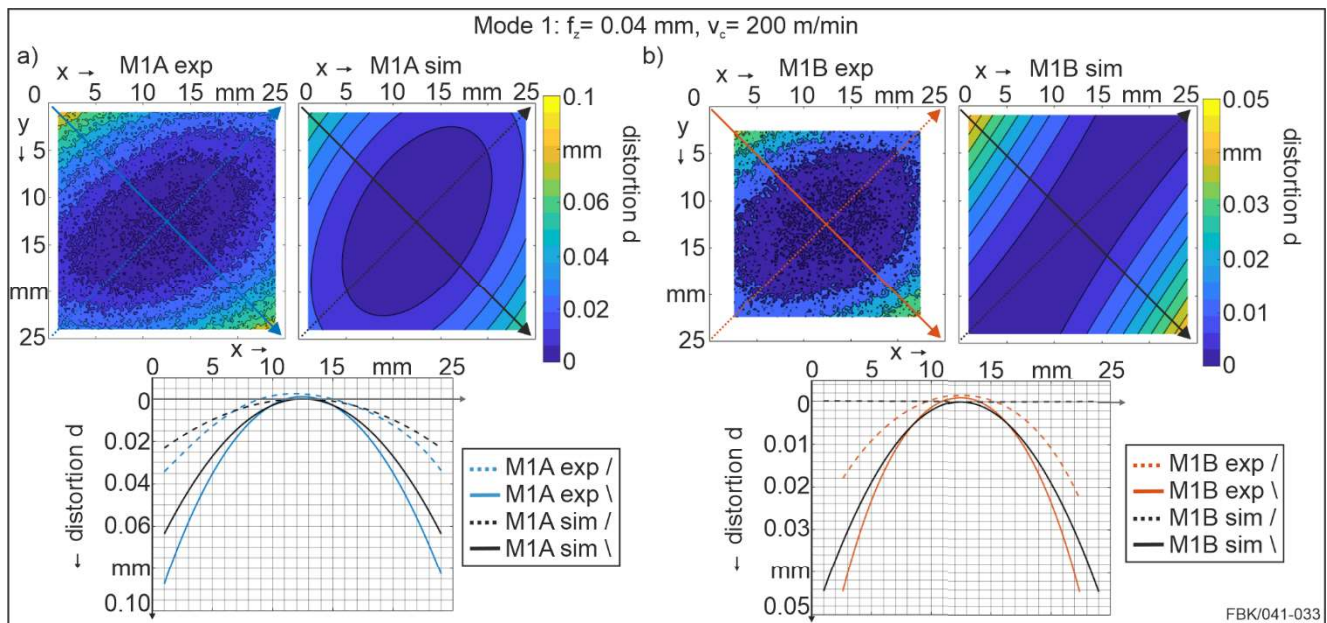


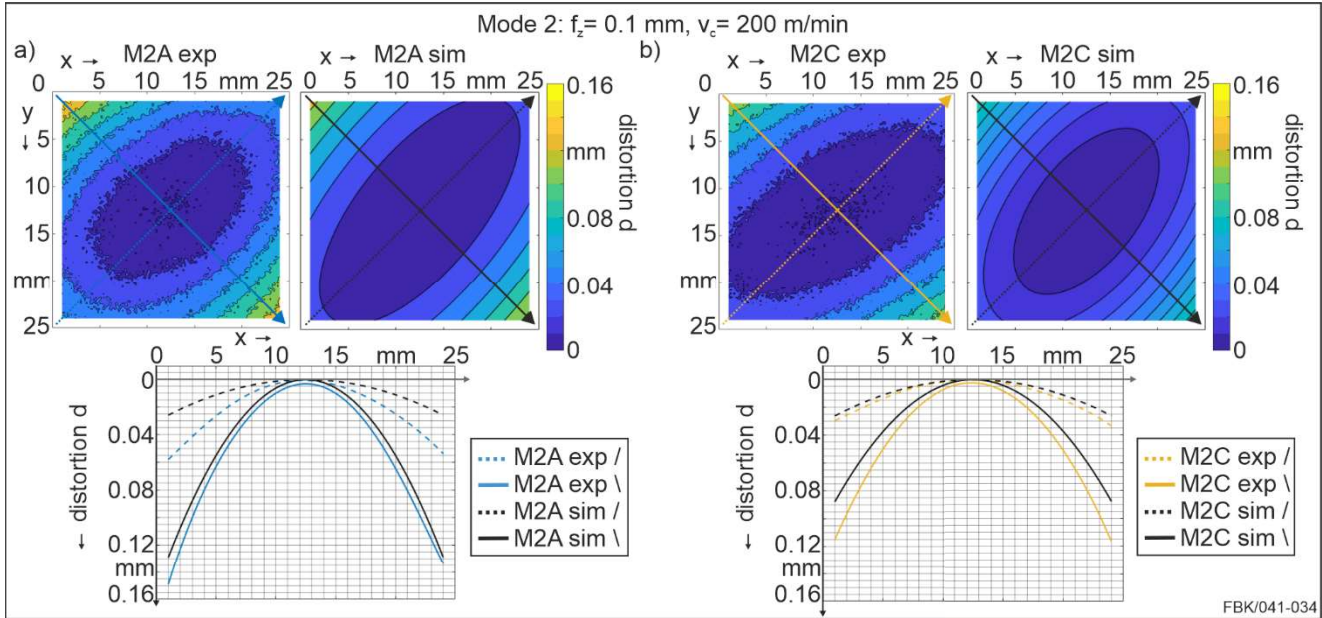
Fig. 29 Wafer Mode 1 measured and simulated distortion of M1A (a) and M1B (b); mind different scales

Table 9 Wafer experimental maximum distortion

	Mode 1				Mode 2			
Exp./Sim. Sample ID	Exp M1A	Sim M1A	Exp M1B	Sim M1B	Exp M2A	Sim M2A	Exp M2C	Sim M2C
x-coord. of edges (mm)	1, 24	1, 24	2.6, 22.4	2.6, 22.4	1, 24	1, 24	1, 24	1, 24
PDD _{max} (mm)	0.085	0.064	0.045	0.034	0.142	0.129	0.116	0.088
FDD _{max} (mm)	0.034	0.022	0.020	0	0.056	0.025	0.031	0.026
Ratio PDD _{max}	75 %		76 %		91 %		76 %	
Ratio FDD _{max}	65 %		-		45 %		83 %	

	Mode 3				Mode 4			
Exp./Sim. Sample ID	Exp M3B	Sim M3B	Exp M3C	Sim M3C	Exp M4A	Sim M4A	Exp M4B	Sim M4B
x-coord. of edges (mm)	2.4, 22.6	2.4, 22.6	1, 24	1, 24	1, 24	1, 24	1, 24	1, 24
PDD _{max} (mm)	0.114	0.104	0.196	0.161	0.047	0.036	0.123	0.082
FDD _{max} (mm)	0.026	0.008	0.042	0.018	0.014	0.004	0.028	0.027
Ratio PDD _{max}	91 %		82 %		77 %		67 %	
Ratio FDD _{max}	31 %		43 %		29 %		96 %	

The distortion of the Mode 2 wafers M2A and M2C are consistent to their simulated distortion, calculated with the average of the three measured MIRS profiles of M2A, M2C respectively (see Fig. 30). Its convex distorted shape is similar and the magnitude of distortion is at a similar level. The simulated averaged maximum distortion accounts for 91 % (M2A) and 76 % (M2C) of the experimental averaged maximum distortion PDD_{max} (see Table 9). The FDD_{max} shows 45 % (M2A) and 83 % (M2C) agreement between the simulation and measured averaged maximum flat distortion.

**Fig. 30** Wafer Mode 2 measured and simulated distortion of M2A (a) and M2C (b)

The measured distortion of the Mode 3 wafers M3B and M3C and their simulated distortion (input: average of three measurements on M3B, M3C respectively) are displayed in Fig 31. It can be seen, that the measured and simulated shapes of distortion agree well. The distortion of the PDD and the FDD show small differences in magnitude. The simulation gets as close as 91 % (M3B) and 82 % (M3C) of the experimental PDD_{max} data (see Table 9). Only 31 % (M3B) and 43 % (M3C) are reached for FDD_{max}.

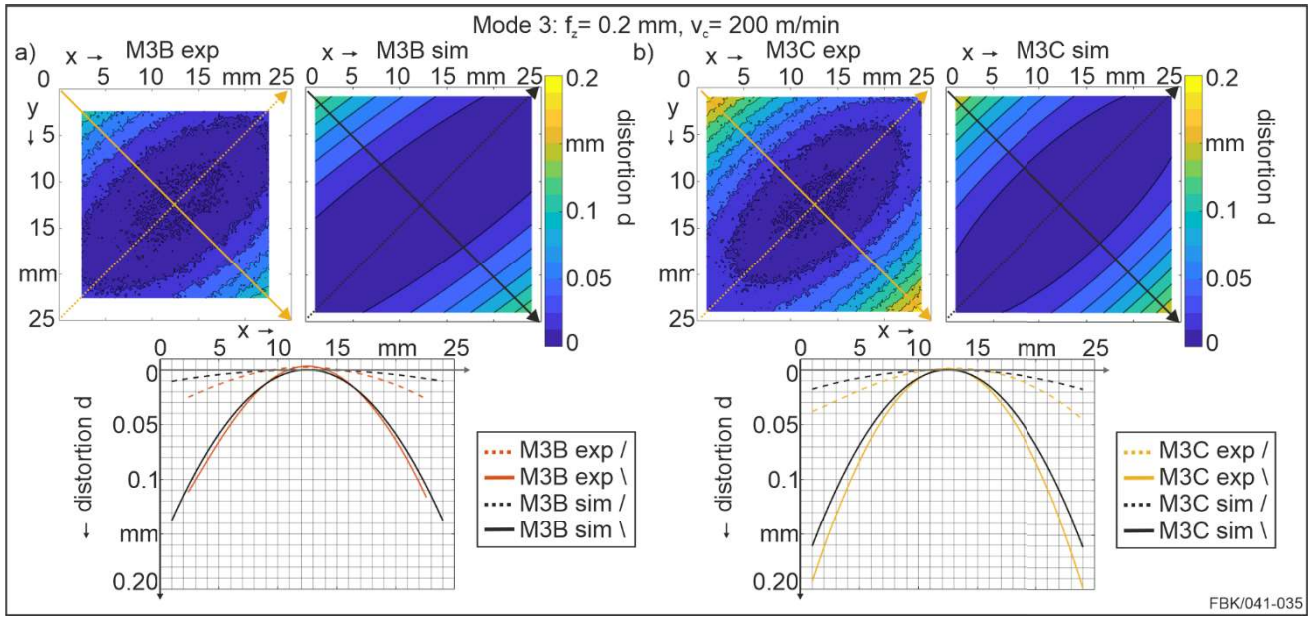


Fig. 31 Wafer Mode 3 measured and simulated distortion of M3B (a) and M3C (b)

The distortion of the Mode 4 wafer M4B is consistent to its simulated distortion due to the measured MIRS (average of three measurements on M4B) (see Fig. 32). The prediction of the wafer distortion shape M4A agrees to a certain point, whereas the bending in the FDD direction is not fully achieved similar to M1B distortion prediction. The reason is that the MIRS of the input are not fully correct, because MIRS are really low with higher variability. Furthermore, as discussed in the previous section the level of distortion of both samples (M4A and M4B, mind different scales in Fig.32) varies accordingly to their induced RS. The model is able to predict those different levels of distortion. The peak corner distortions PDD_{max} are reached by 77 % (M4A) and 67 % (M4B) by the simulation. 29% (M4A) and 96 % (M4B) of the FDD_{max} data are reached by the simulation (see Table 9).

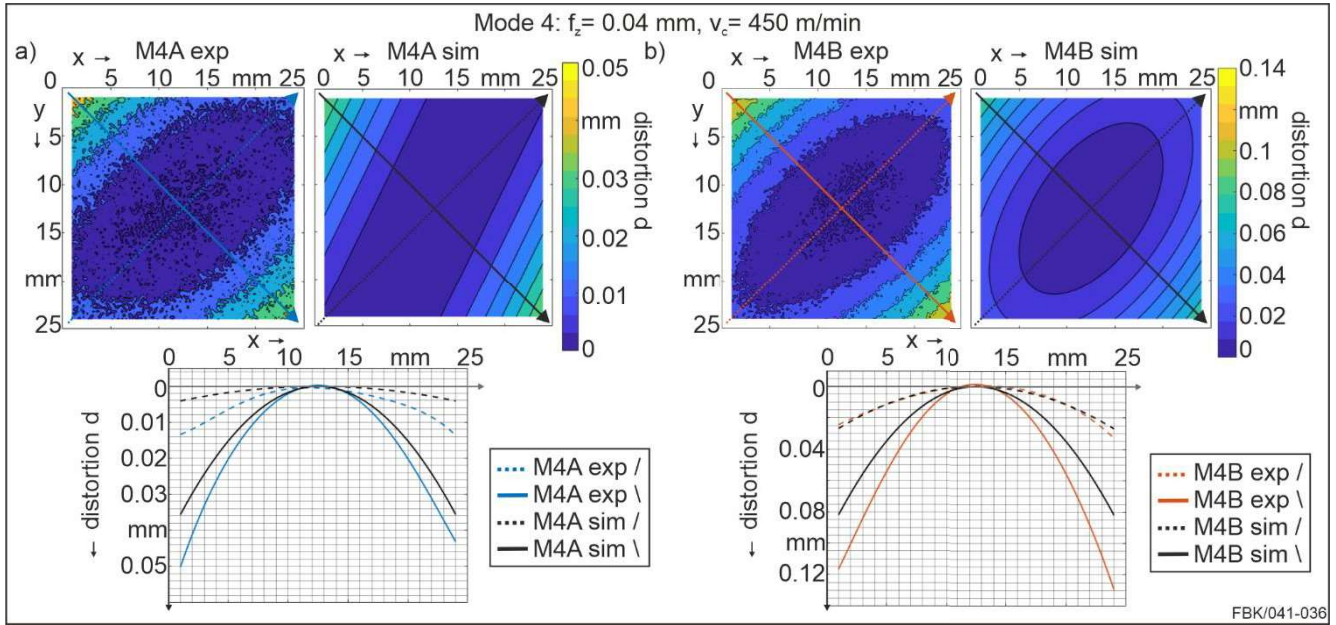


Fig. 32 Wafer Mode 4 measured and simulated distortion of M4A (a) and M4B (b); mind different scales

In general, the finite element simulations show that the measured MIRS are consistent with the measured distortion for different machining parameters, because the overall distorted shape of experiment and simulation match for each wafer. The magnitude of measured and simulated distortion of each wafer is on a same level, but e.g. the highest distortions found vary down to 67 % (peak line distortion). Especially for really low MIRS (see M1A, M1B and M4A) the biggest differences between model and wafer measurements are found, because those low MIRS showed the highest variability

themselves. For higher distortions due to higher MIRS an agreement up to 91 % of PDD_{max} (M2A, M3B) is found. Furthermore, the distortion in the peak diagonal direction is simulated to a higher accuracy than the opposite direction. One reason for the differences in the magnitude of distortion could be that the MIRS are only measured to a depth of approximately 500 μm . Although a stress relief process was carried out after heat treatment and before machining, there is still a small amount of IBRS up to 20 MPa left [16], which is neglected by the simulation. Moreover, the already mentioned uncertainties of the measuring technique itself, especially at shallow depths, contribute to the difference in distortion of simulation and experiment. Besides there could be RS induced by the EDM cutting, although the cutting parameters were chosen to minimize the stress induced during cutting.

However, it was found that variations of MIRS within one machining mode result in a variation of distortion in a way that is consistent as determined via the model.

4. Conclusions and Outlook

An overall repeatability of measured RS and forces for Mode 1, 2, 3 has been proven and the two investigated clamping strategies (vise and side clamps) have almost no impact for those modes on the MIRS. E.g. the difference of the MaxRS in normal direction were stated to a maximum of 15 % (M1) and 27 % (M2 & M3). The repeatability standard deviation for those modes machined in the vise lays in the normal directions between 16 % and 34 % of the maximum normal compressive residual stresses. Furthermore, it was found that the repeatability standard deviation of the maximum shear stress was the highest for the machining Mode 1 (49 %) inducing least shear residual stresses. A similar behavior was detected for the penetration depth of the MIRS, where the highest RSTD was reached by Mode 1 in shear direction (52 % of t_{pxy}). Those detected variations in the MIRS profiles within machining Modes 1, 2 and 3 also lead to small deviations in the wafer distortion.

Mode 4 showed more variability compared to other modes for the vise and side clamps, because machining for Mode 4 was not stable. The RSTD of the MaxRS was greater than for the other modes in normal directions (53 % of the $MaxRS_x$ and 54 % $MaxRS_y$). Vibrations were detected in the force signal of F_z . The big differences in MIRS also resulted in big (compared to other modes) differences in the machining induced distortion.

The variation of feed per tooth showed that higher feeds result in a higher penetration depths of RS profile and in higher depth of the maximum compressive RS due to the increased load on the sample, which leads to larger plastically deformed areas and therefore deeper residual stresses and the shift of the maximum stresses deeper into the workpiece. These stresses also lead to an increased machining induced distortion with increased feeds. The variation of the cutting speed showed in average, although Mode 4 had the highest variation itself, similar MIRS profiles due to similar forces and temperatures prevailing during machining. In order to see an effect of an increased cutting speed on the MIRS, higher cutting speeds are needed.

Furthermore, the numerical stress analysis showed that the measured distortion across all machining modes is a machining induced distortion. The MIRS and the distortion behave related in a way that more and/or deeper compressive RS cause more distortion. It was found that variations of MIRS within one machining mode result in a variation of distortion in a way that is consistent as determined via the model. Besides, the shear stresses are essential and responsible for a **torsional moment, which contributes highly to the shape and maximum of distortion.**

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¹Naming of specific manufacturers is done solely for the sake of completeness and does not necessarily imply an endorsement of the named companies nor that the products are necessarily the best for the purpose.

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Declaration

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Conflicts of interest/Competing interests (include appropriate disclosures)

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

Availability of data and material (data transparency)

Data and material are stored at TU Kaiserslautern and UC Davis.

Code availability (software application or custom code)

The commercial software ABAQUS was used to run the distortion simulations.

Authors' contributions

Not applicable

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