

Vertical β -Ga₂O₃ Schottky Rectifiers with 750 V Reverse Breakdown Voltage at 600K

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Abstract

Field-plated vertical Ga₂O₃ rectifiers were operated up to 600K with reverse breakdown voltage (V_B) of 750 V, 950 V at 500K and 1460 V at 400K. The barrier height was 1.3 eV at 300K and reduced to 0.7 eV at 600K, with ideality factors of 1.05 ± 0.05 and 2 ± 0.1 , respectively at these temperatures. On-state resistance, R_{ON} , was $13 \text{ m}\Omega \cdot \text{cm}^2$ at 300K and $41 \text{ m}\Omega \cdot \text{cm}^2$ at 600K, leading to respective Baliga figures of merit of $151 \text{ MW} \cdot \text{cm}^{-2}$ (300K) and $13.9 \text{ MW} \cdot \text{cm}^{-2}$ (600K). The on-off ratio was $>10^4$ for all temperatures measured. The leakage current showed a good fit to the thermionic field emission model when the reverse voltage was less than 80 V, and it was dominated by the tunneling effect at higher voltage. The transition voltage from thermionic emission to tunneling effect decreased as the temperature increased. At high reverse voltage, a large number of electrons are injected into the drift region, and the current shows an $I \propto V^n$ relationship with voltage, indicating a trap-assisted space-charge-limited conduction (SCLC) mechanism. We observed this SCLC relation when the reverse voltage was larger than

400 V for 500 K and 600 K. The associated trap energies for these two regions were extracted as 0.2 and 0.4 eV, consistent with levels in the gap.

Introduction

The development of power electronics technology based on wide bandgap semiconductors is attracting much interest because of the potential for significantly higher switching efficiency and ability to operate at higher powers and temperatures. Within the next decade, about 80% of all US electricity is expected to flow through power electronics. These include power distribution systems, electric vehicle fast chargers, data center power supplies, ship power systems, and renewable wind/solar energy integration. Both SiC and GaN power electronics are now commercialized and provide more efficient performance than conventional Si-based devices [1-3]. The combination of high breakdown voltage, low on-state resistance and lower switching losses is improved in the ultra-wide bandgap semiconductors [4-10] [such as Ga_2O_3 , diamond, and AlN]. This leads to their high Baliga's figure of merit (BFOM), defined as $\epsilon \mu E_c^3$, where ϵ , μ , and E_c are the dielectric constant, carrier mobility, and critical breakdown field strength, respectively.

Among these ultra-wide bandgap semiconductors, monoclinic gallium oxide ($\beta\text{-Ga}_2\text{O}_3$) has recently attracted increasing attention due to the availability of high quality, large diameter single crystals from mature melt growth methods and its attractive material properties of wide E_G of 4.6–4.9 eV, good electron mobility ($>200 \text{ cm}^2/\text{Vs}$) and estimated critical breakdown field, E_c , of $\sim 8 \text{ MV/cm}$, yielding a relatively high BFOM (>3000) with respect to silicon [11-23]. Compared to other ultra-wide bandgap materials, the inexpensive substrates lower the manufacturing cost for $\beta\text{-Ga}_2\text{O}_3$ power devices for applications requiring high operation voltage and high energy conversion efficiency.

A large literature on demonstration of power devices in this materials system now exists, including vertical and lateral MOSFETs and rectifiers [6-43]. The absence of practical p-type

doping may be alleviated by use of other p-type oxide semiconductors to form a pn heterojunction with Ga_2O_3 , such as NiO, Cu_2O , CuI and Ir_2O_3 [27-34]. Some notable recent advancements in device performance for Ga_2O_3 diodes includes a 5A/700V junction Schottky barrier diode implemented with p-type NiO layer [35], 1.86kV p-n junction diode with NiO heterojunction [36], as well as demonstrations of >100A of absolute forward current using conventional field-plated Schottky diodes [37].

Wide energy bandgap materials are suitable for high temperature as well as high breakdown voltage applications. The ability to operate at high temperature enables wide bandgap devices to be attractive in terms of reduced package size and minimal requirement for cooling. Hindered by its low thermal conductivity, demonstrations of operation at high temperature for $\beta\text{-Ga}_2\text{O}_3$ are fairly limited. Wang et al.[38] reported operation up to 600K of rectifiers with beveled edge termination and spin-on glass passivation, achieving breakdown voltage of ~500V at this temperature. One way to increase the breakdown voltage is to grow thicker layers, but to date, the maximum drift layer thickness has been 30 μm , thinned to 20 μm after the chemical mechanical planarization (CMP) step needed to achieve a flat surface morphology [15].

In this work, we report operation of field plated Schottky barrier diodes up to 750 V at 600K, with reasonable leakage current density. This was achieved by growing a 40 μm thick drift layer, thinned to 30 μm after CMP, as well as lower carrier concentration. The devices exhibit a negative temperature coefficient of breakdown and reverse leakage dominated by thermionic field emission when the reverse voltage was less than 80 V, and by tunneling conduction at higher voltage.

Experimental

The drift region of the material consisted of a 30 μm thick, lightly Si doped epitaxial layer grown by halide vapor phase epitaxy (HVPE) with minimum carrier concentration of $1.6 \times 10^{16} \text{ cm}^{-3}$ (the maximum was $\sim 3 \times 10^{16} \text{ cm}^{-3}$), and this epitaxial layer was grown on a (001) surface orientation Sn-doped $\beta\text{-Ga}_2\text{O}_3$ single crystal (Novel Crystal Technology, Japan). The HVPE layer is actually grown initially to a thickness of $\sim 40 \mu\text{m}$, but then chemically mechanically polished to planarize the surface by removing $\sim 10 \mu\text{m}$ of material. As seen in the Nomarski images of Figure 1, this produces a much smoother surface relative to the as-grown morphology, but there is still some surface roughness after the CMP step. It is important to note that this is a unique growth, the thickest ever attempted at NCT and the process is not optimized.

A full area Ti/Au backside Ohmic contact was formed by e-beam evaporation and was annealed at 550°C for 30s under N_2 ambient. 40 nm of Al_2O_3 and 400 nm of SiN_x were deposited as field plate dielectric using Cambridge-Nano-Fiji ALD and PlasmaTherm PECVD tools. Dielectric windows of $40 \mu\text{m} \times 40 \mu\text{m}$ was opened using dilute buffered oxide etchant (BOE), and a 200nm Ni/Au Schottky contact was deposited with E-beam after lithography pattern followed by standard acetone lift-off. Figure 2 shows a photograph and device geometry of fabricated diodes, respectively. Of the 121 devices on this chip, approximately 46 have very smooth morphology, but this was not the only parameter that correlated with achieving high breakdown voltage. We had a yield of $\sim 15\%$ (~ 20 devices out of 121) with breakdown in the range 745-754V. The carrier concentration of these highest breakdown voltages was typically $< 2 \times 10^{16} \text{ cm}^{-3}$ with no visible surface defects within the active area of the device. The remaining surface defects are due to the incomplete smoothing of the surface of the HVPE-grown layer.

The current-voltage (I-V) characteristics were recorded at 1MHz with a Tektronix 370-A curve tracer was used for forward and reverse current measurements over the temperature

range 300-600K on a temperature-controlled stage. No hysteresis was observed in any of the rectifier characteristics. The forward direction was dominated by the thermionic emission (TE) current, while in the reverse direction, the thermionic field emission (TFE) and tunneling currents played an important role at high reverse bias. To extract the barrier height (Φ_b) and ideality factor (n), we used the relationship for current density in TE theory, given by [1,3,38]

$$J = J_0 \exp (eV_A/nkT) [1-\exp (-eV_A/ kT)]$$

where $J_0 = A^* m_{eff}/m_0 T^2 \exp(\Phi_B /kT)$, e is electronic charge and A^* is the Richardson constant and V_A is the bias voltage applied. The magnitude of the series resistance can also be obtained from plots of $d(V_A)/d(\ln J)$ versus J , while the barrier height is obtained from $(kT/e) \ln(A^* T^2/J_0)$ [44,45]. The built-in voltage can be obtained from the C-V characteristics [45]. The fact that thermionic field emission was the dominant current transport mechanism over most of the conditions investigated can be established by the fact that the tunneling parameter E_{00}/kT was ~ 1 [42], where E_{00} is given by $(eh/4\pi)[N_D/m^* \epsilon_r]^{0.5}$ and h is Planck's constant and ϵ_r is the relative dielectric constant. If this parameter is much less than unity, then thermionic emission is significant and field emission is dominant if this parameter is $\gg 1$.

Capacitance-Voltage (C-V) characteristics were recorded with an Agilent 4284A Precision LCR Meter. The diode on/off ratio is another figure-of-merit was measured when switching from 2V forward to reverse biases up to 100V. The reverse breakdown voltage was defined as the bias for a reverse current of 1mA.

Results and Discussion

The barrier height was 1.23 eV at 300K and reduced to 0.7 eV at 600K, with ideality factors of 1.05 ± 0.5 and 2 ± 0.1 , respectively at these temperatures, extracted from the I-V-T characteristics in Figure 3 and those parameters plotted in Figure 4. It is commonly observed that

the barrier height decreases with increasing temperature, as it is easier for electrons to pass over the barrier since with pure thermionic emission there would be a reduced barrier at elevated temperatures. This will lead to contributions from other transport mechanisms and the commonly observed higher ideality factors at elevated temperatures. [42]. There may also be contributions from spatial inhomogeneity of the Schottky barrier [42].

The temperature coefficient was $-(2.1 \pm 0.6) \times 10^{-3}$ eV/K, which is the same order of magnitude as the temperature dependence of the band gap, namely (-4.5×10^{-3}) eV/K [40]. In Si, the temperature coefficient of the barrier height also depends on the chemical nature of the metal, in contradiction with models suggesting Fermi-level pinning at the center of the semiconductor's band gap [41]. In Ga₂O₃, the situation is more complex, with the dependence of barrier height on metal work function being a function of the orientation of the Ga₂O₃ surface. It is generally the case that a number of factors also have an influence on barrier height and its temperature dependence. For Ga₂O₃, these factors include the interface crystallography, contact inhomogeneities, the recombination velocities on different surface planes of Ga₂O₃ or for different polytypes. For example, Lyle et al [42] found a strong positive correlation between the calculated Schottky barrier heights and the work function of metal contacts on (100) β -Ga₂O₃, in contrast to (201) β -Ga₂O₃. Similarly, there were mixed results for (010) β -Ga₂O₃ [42]. The temperature dependence of barrier height and ideality factor in our devices is consistent with previous reports [38, 43]. We did not observe any significant change in carrier concentration as a result of the temperature cycling, as judged from the C-V measurements.

The on-state resistance of the rectifiers, R_{ON} , was 13 m Ω .cm² at 300K and 41 m Ω .cm² at 600K, leading to respective Baliga figures of merit of 150 MW.cm⁻² (300K) and 14 MW.cm⁻² (600K). The highest previous result was 4 MW. cm⁻² at 600K [38]. The series resistance of the

highest breakdown voltage rectifiers was typically between 200-300 Ω . The on-off ratio is another figure of merit in that having high on-current and low leakage current in reverse bias is desirable [46-49]. This was $>10^4$ for all temperatures measured, as shown in Figure 5.

As shown in Figure 6, at lower voltages, reverse bias leakage current is dominated by thermionic field emission (TFE) [38, 39], which is dependent on ambient temperature. However, with increasing voltage and hence electric field, the carrier tunneling and other conduction processes becomes predominant, and the leakage currents become more sensitive to temperature changes [50]. The leakage current shows a good fit to the TFE model when the reverse voltage is less than 80 V in Figure 6, and it is affected by the tunneling effect when voltage is higher than 80 V. However, the transition voltage from thermionic emission to tunneling effect did not follow the universal monotonic temperature [38,39]. The transition voltage actually decreased as the temperature increased, as illustrated in Figure 7, showing that impact ionization is not the breakdown mechanism, since that should exhibit positive temperature coefficient [46]. The variation of V_B with temperature can be represented by a relation of the form [47] :

$$V_B = V_{B0} [1 + \beta(T - T_0)]$$

where $\beta = -3.4 \pm 1.4 \text{ V. K}^{-1}$. We have previously found that current increases in vertical geometry Ga_2O_3 rectifiers during electron beam induced current measurements are dominated by impact ionization of deep acceptors in the depletion region. At room temperature, mobile hole diffusion in the quasi-neutral region of Schottky diodes contributes significantly to the charge collection efficiency [48]. Electron beam induced current measurements indicated a strong amplification of photocurrent in rectifiers, attributed to the Schottky barrier lowering by holes trapped on acceptors near the surface [49].

The breakdown fields calculated from the observed breakdown voltages at different temperatures were 5.0×10^5 V/cm at 600K, 6.3×10^5 V/cm at 500K and 9.8×10^5 V/cm at 400K. These were obtained from the non-punch through relation $E_{bd} = [(2eN_d V_{bd})/\epsilon]^{0.5}$ [50]. Currently, all Ga₂O₃ rectifiers show performance limited by the presence of defects and by breakdown initiated in the depletion region near the electrode corners.

When a higher reverse voltage is applied, a large number of electrons are injected into the drift region, and the current shows an $I \propto V^n$ relationship with the voltage, indicating a trap-assisted space-charge-limited conduction (SCLC) mechanism [51, 52]. Under this mechanism, a current hump should be observed before the trap-filled limited voltage, and with electrons continue to be injected into the drift region, it will lead to a breakdown. This is commonly reported in GaN, ie. the logarithmic I-V curve shows that the current I is proportional to V^n until a hump (sharp transition in I-V curve) at some threshold voltage. Such behavior can be modeled by a space-charge-limited current (SCLC) conduction mechanism with traps [53,54]. Under reverse bias and below this threshold, electrons injected into the drift layer partly contribute to conduction current and are partly captured by acceptor traps known to be present. The hump threshold voltage represents the trap-filled-limited voltage of the acceptor traps, suggesting the applied voltage overcomes the negative potential formed by the un-neutralized electrons in traps and the ionized donors in the n-Ga₂O₃. [53,54]. This shows an SCLC relation when the reverse voltage is larger than 400 V for 500 K and 600 K in Figure 7.

The reverse current characteristics at different temperatures are shown in more detail in Figure 8 (top), with all showing $I \propto V^n$ relationship. A fit to the data for the 600K reverse current characteristic is shown at the bottom of Figure 8. The data fits well to a relationship $I \propto V^n$, where n is 5.2 and the constant of proportionality is 7.6×10^{-23} . The associated trap energies for

these two regions were extracted as 0.2 and 0.4 eV from an Arrhenius plot, as shown in Figure 9. Levels with these activation energies have been reported previously in epitaxial Ga₂O₃, but were ascribed to unknown impurities and native point defects, respectively, with no specific information on their microstructure [55].

The record high reverse breakdown at high temperature in this work is a significant advance for high temperature switching applications for β -Ga₂O₃, as shown in the reverse breakdown performance when compared with previous reported works at elevated temperature in Figure 10.

Summary and Conclusions

Ultrawide bandgap semiconductors offer higher switching frequencies, higher operating temperatures and lower losses that improve power conversion efficiency. The remaining challenges and new opportunities for Ga₂O₃ in high power applications ranging from electric vehicles, medium voltage motor drives, renewable energy interfaces, microgrids, to emerging applications such as electric propulsion for aircraft include more thermally stable contacts, development of stable MOS gates, optimized edge termination and continued improvements in epi and bulk growth. For EV motor drives, the improved efficiency of ultra wide bandgap semiconductor devices would enable either extended range for the vehicle for a given battery charge, or a reduction in the battery pack required to go a certain distance. The required power modules would need large area MOSFETs delivering current in the range of 80-120 Amps per chip at 650 V to 1200 V. The promising results from vertical Ga₂O₃ rectifiers reported previously in terms of breakdown voltages and now high temperature operation suggest that thermal management issues become more important to address.

Data Availability Statement

All data that support the findings of this study are included within the article (and any supplementary files)

Acknowledgments

The work at UF was performed as part of Interaction of Ionizing Radiation with Matter University Research Alliance (IIRM-URA), sponsored by the Department of the Defense, Defense Threat Reduction Agency under award HDTRA1-20-2-0002. The content of the information does not necessarily reflect the position or the policy of the federal government, and no official endorsement should be inferred. The work at UF was also supported by NSF DMR 1856662 (James Edgar). The work at NRL was supported by the Office of Naval Research.

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Figure Captions

Figure 1. Nomarski microscope images of the HVPE layers before (top, left and right) and after subsequent polishing to planarize the surface (bottom, left and right).

Figure 2. Schematic of vertical rectifier structure (top) and photograph of fabricated β -Ga₂O₃ Schottky diode array with 40 μ m \times 40 μ m squares (bottom).

Figure 3. Forward I-V characteristic for rectifiers as a function of temperature.

Figure 4. Schottky barrier height and ideality factor retrieved from diode forward I-V as a function of temperature.

Figure 5. On/off ratio when switching from 2 V forward bias to the reverse biases shown on the x-axes at various temperatures.

Figure 6. Reverse current density of the vertical β -Ga₂O₃ Schottky diode at various temperatures fitted to the TFE model for reverse biases of 5-100 V.

Figure 7. Reverse I-V-T characteristics at 400-600 K for rectifiers at various temperatures.

Figure 8. Experimental data for reverse current characteristics at 400-600K and fit to an $I \propto V^n$ relationship (top) and more detailed view of 600K reverse current characteristic and fit to an $I \propto V^n$ relationship with $n=5.2$ (bottom).

Figure 9. Arrhenius plot $\Delta I/\Delta V$ versus $1/T$. The I - V slope of the voltages ranges from 200-400 V, and ranges over 400 V for rectifiers measured as a function of temperature.

Figure 10. Comparison of operation temperature versus maximum reverse bias for reported vertical Ga₂O₃ rectifiers. Previous data comes from Virginia Tech [38], University of Canterbury [56], University of Florida [57] and NIICT [58].



















