

¹ Multiplexing of Electrospray Ionization Sources Using Orthogonal ² Injection into an Electrodynamic Ion Funnel

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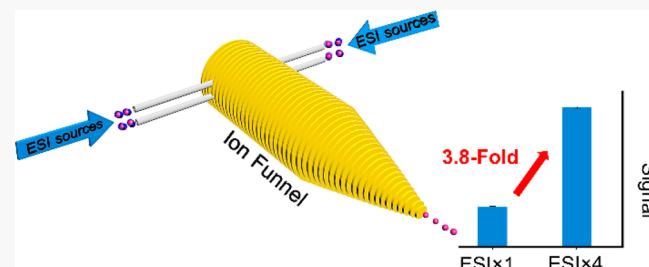
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ABSTRACT: In this contribution, we report an efficient approach to multiplex electrospray ionization (ESI) sources for applications in analytical and preparative mass spectrometry. This is achieved using up to four orthogonal injection inlets implemented on the opposite sides of an electrodynamic ion funnel interface. We demonstrate that both the total ion current transmitted through the mass spectrometer and the signal-to-noise ratio increased by 3.8-fold using four inlets compared to one inlet. The performance of the new multiplexing approach was examined using different classes of analytes covering a broad range of mass and ionic charge.

A deposition rate of $>10 \mu\text{g}$ of mass-selected ions per day may be achieved by using the multiplexed sources coupled to preparative mass spectrometry. The almost proportional increase in the ion current with the number of ESI inlets observed experimentally is confirmed using gas flow and ion trajectory simulations. The simulations demonstrate a pronounced effect of gas dynamics on the ion trajectories in the ion funnel, indicating that the efficiency of multiplexing strongly depends on gas velocity field. The study presented herein opens up exciting opportunities for the development of bright ion sources, which will advance both analytical and preparative mass spectrometry applications.



²¹ ■ INTRODUCTION

²² Electrospray ionization (ESI) is a widely used atmospheric ²³ pressure ionization technique in mass spectrometry (MS).^{1,2} In ²⁴ ESI, an electric field applied to the liquid meniscus formed at ²⁵ the tip of a capillary produces a Taylor cone, from which ²⁶ charged microdroplets are generated containing analyte ²⁷ molecules.³ Subsequent desolvation of the microdroplets ²⁸ produces bare or partially solvated ions that are analyzed by ²⁹ a mass spectrometer.^{4,5} Soft ionization with minimal ³⁰ fragmentation,⁶ compatibility with liquid-phase separation ³¹ techniques,^{7,8} access to a wide range of molecular ions,^{9,10} ³² along with simplicity and ease of operation make ESI ³³ particularly attractive for both analytical and preparative MS ³⁴ applications.^{11–14}

³⁵ Since the initial demonstration of ESI-MS, the scientific ³⁶ community has been on the quest for improving the efficiency ³⁷ by maximizing the ion flux provided by this powerful ionization ³⁸ technique. The dramatic improvements in the sensitivity of ³⁹ ESI-MS achieved through these efforts have opened up a wide ⁴⁰ range of applications in biological research,¹⁵ forensics,¹⁶ ⁴¹ environmental sciences,¹⁷ drug discovery,¹⁸ and clinical ⁴² studies.^{19,20} Moreover, preparative MS applications of interest ⁴³ to materials science,^{21,22} energy production and storage,^{23,24} ⁴⁴ catalysis,^{25,26} and molecular electronics²⁷ have been trans- ⁴⁵ formed by the development of brighter ESI sources. Many ⁴⁶ studies have focused on the efficient transfer of ESI-generated

ions into the vacuum system of a mass spectrometer.^{28–30} The ⁴⁷ inner diameter and length of the heated inlet have been ⁴⁸ optimized, and specially shaped heated capillary inlets have ⁴⁹ been developed to increase ion transmission in the ⁵⁰ atmosphere–vacuum interface.^{31–34} Alternatively, a sub-⁵¹ ambient-pressure ESI source interfaced with an electrodynamic ⁵² ion funnel may be used to generate ions inside the vacuum ⁵³ system, thereby preventing ion loss in the capillary inlet.³⁵ ⁵⁴ Ambient-pressure ion funnel systems have also been developed ⁵⁵ to enhance the transmission of ions.^{36,37}

Nonetheless, further improvement in the ion current from a ⁵⁷ single emitter is limited by the smallest droplet size that can be ⁵⁸ generated at a given flow rate and the maximum amount of ⁵⁹ charge carried by the ESI droplets, which is known as the ⁶⁰ Rayleigh limit.^{38–40} Multiplexing of the ESI emitters is a ⁶¹ promising strategy that has been employed to overcome this ⁶² limitation.^{41–45} One multiplexing strategy involves the ⁶³ development of ESI emitter arrays, which have been used ⁶⁴ both in analytical MS^{46,47} and ESI-based propulsion.^{48,49} In ⁶⁵

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66 analytical MS, a circular 22-emitter array has been used to
67 achieve more than a 2-fold improvement in the MS
68 sensitivity.⁵⁰ Ambient ion beam merging and focusing using
69 specially shaped 3D-printed devices and counter-propagating
70 beams provides an opportunity to manipulate and combine
71 multiple ion beams before they enter the vacuum system.^{51,52}

72 Despite the significant progress in this field, multiplexing of ion
73 beams still results in a substantial ion loss, which motivates the
74 development of new multiplexing strategies.

75 An electrodynamic ion funnel is commonly used in both
76 commercial and custom-designed mass spectrometers to
77 facilitate ion transmission in the ESI interface.⁵³ An ion funnel
78 is composed of a stack of ring electrodes operated using radio
79 frequency and direct current voltages to efficiently focus and
80 transmit ions at subambient pressures (0.5–30 Torr).⁵⁴ Ion
81 funnels are commonly used in conjunction with ESI and
82 heated capillary inlets. An ESI-generated ion beam is typically
83 injected along the axis of the ion funnel. Orthogonal injection
84 of ions from a heated inlet through a cutout section on one
85 side of the ion funnel has also been demonstrated.⁵⁵ This
86 configuration provided a 2–3-fold increase in ion transmission
87 in comparison with axial injection.³⁴ Furthermore, a substantial
88 improvement in the ion current was obtained by increasing the
89 inner diameter of the heated inlet from 0.76 to 1.17 mm.
90 However, further increase in the inner diameter of the heated
91 inlet did not improve the observed mass-selected ion current.
92 Another advantage of orthogonal injection is that it efficiently
93 eliminates neutral contaminants and noninertial droplets
94 entrained with the gas flow into the vacuum system, which
95 has been shown to improve the analytical performance of a
96 mass spectrometer.⁵⁵

97 Herein, we present an approach for efficient multiplexing of
98 independent ESI sources using multiple orthogonal injections
99 into an ion funnel. We demonstrate that multiplexing of four
100 orthogonal inlets results in an almost proportional increase in
101 the total ion current and signal-to-noise ratio as compared to a
102 single orthogonal inlet. In our approach, two pairs of heated
103 inlets are mounted on the opposite sides of the ion funnel, and
104 each inlet is equipped with an independently operated ESI
105 emitter. Gas flow and ion trajectory simulations provide
106 insights into factors affecting the efficient merging of ion beams
107 using orthogonal injection of multiple ion beams into an ion
108 funnel. The simulations demonstrate that the velocity and
109 direction of the gas flows generated by the individual inlets are
110 critical factors determining the ion extraction efficiency from
111 the gas stream into the ion funnel. In addition, simulations at
112 different gas pressures were used to identify the optimal
113 pressure for merging four inlets of 1 mm inner diameter. The
114 optimal pressure of ~7 Torr obtained in simulations is in good
115 agreement with the experimental data.

116 ■ EXPERIMENTAL SECTION

117 Tris(2,2'-bipyridyl)dichlororuthenium(II) hexahydrate (118
118 (bpy)₃·6H₂O, CAS: 50525–27–4), sodium phosphotungstate
119 tribasic hydrate (Na₃[PW₁₂O₄₀]·xH₂O, CAS: 12026–98–1),
120 substance P acetate salt hydrate (CAS: 137348–11–9,
121 anhydrous), and ubiquitin from bovine erythrocytes (≥98%
122 purity, CAS: 79856–22–4) were purchased from Sigma-
123 Aldrich (St. Louis, MO) and used as received. Tetrabutyl-
124 ammonium-chlorinated dodecaborate ((TBA)₂B₁₂Cl₁₂) salt
125 was kindly provided by Drs. Jonas Warneke and Carsten Jenne.
126 Na[V₆O₇(OCH₃)₁₂] and [Co₆S₈(PEt₃)₆]Cl were synthesized
127 according to reported procedures.^{56,57} Substance P was

128 dissolved in a 9:1 (v/v) methanol/H₂O solution to a 129
concentration of 100 μM. Ubiquitin ions were dissolved in 129
CH₃OH/H₂O/CH₃COOH = 49.5/49.5/1% solution to a 130
concentration of 20 μM. Unless specified otherwise, other 131
analytes were dissolved in methanol at a concentration of 150 132
μM.

133 The multiplexed electrospray ionization (ESI) interface is 134
implemented on a custom-designed dual-polarity ion soft 135
landing instrument described in detail elsewhere.⁵⁸ Briefly, the 136
instrument is equipped with a high-transmission ESI interface 137
(Spectroglyph, LLC) composed of a tandem electrodynamic 138
ion funnel system and a bent flatapole ion guide (Figure S1).⁵⁸ 139
A high-pressure ion funnel (HPF) is housed in a vacuum 140
chamber differentially pumped to 7 Torr by a dry screw 141
vacuum pump (VARODRY VD200, 118 cubic feet per minute 142
(cfm), Leybold GmbH, Cologne, Germany). The pumping 143
port is located downstream from the inlets close to the next 144
vacuum chamber. Typical pressures in the chambers that house 145
the low-pressure ion funnel (LPF) and the bent flatapole ion 146
guide are 0.8 Torr and 10–20 mTorr, respectively. The fourth 147
vacuum stage, in which ion current detection and ion beam 148
characterization are performed, is differentially pumped to 3–6 149
× 10⁻⁵ Torr.

150 The high-transmission ESI interface described in our 151
previous publication is equipped with two orthogonal injection 152
ESI sources.⁵⁸ Ions are introduced into vacuum through 153
stainless-steel heated inlet tubes from the opposite sides of the 154
HPF. Each inlet tube is mounted on a stainless-steel cartridge 155
(Figure 1a, top left corner). The temperature of each heated 156 fl
inlet is maintained by a cartridge heater and a thermocouple. A 157
detailed drawing of the cartridge is shown in Figure 1a. In 158
particular, two inlets (1/16" OD, 0.04" ID, 7 cm length, VICI 159
Valco Instruments, Houston, TX) are inserted through two 160
channels drilled through the cartridge that are spaced by 6 mm. 161
We selected 0.04" ID inlets for multiplexing. This ID is close 162
to the optimum value reported in our previous study³⁴ and was 163
selected by considering the available pumping power. Two 2¹⁶⁴
V, 60W cartridge heaters (1/8" dia., 1–1/4" long, Gord¹⁶⁵
Sales, Layton, UT) are connected in series and inserted into 166
the side channels of the cartridge to provide sufficient heating 167
power for efficient desolvation of the ESI droplets. A 168
thermocouple wire is inserted into another channel between 169
the heaters. The temperature of the cartridges is maintained at 170
180 °C.

171 The HPF shown in Figure 1a,b and described in our 172
previous publication⁵⁸ is composed of a repeller section and a 173
funnel-shaped section. The heated inlets are inserted into the 174
HPF through two cutouts (10 × 10 mm) on the opposite sides 175
of the repeller section. Introducing the ion beams through the 176
funnel section, which was not explored in this work, may 177
require a different radio frequency (RF) potential well. The 178
cutouts are staggered along the HPF axis and separated by 5 179
mm. The heated inlets protrude into the cutouts of the HPF by 180
~1 mm, which is the optimized position for ion transmission.
181 A front view of the ion funnel when the four orthogonal inlets 182
are inserted into the funnel is shown on the right side of Figure 183
1b. Same direct current (DC) voltages are applied to the all the 184
inlets.

185 Ions are generated using direct infusion ESI at a typical flow 186
rate of 60 μL/h. Charged microdroplets are produced by 187
applying a ±3 kV voltage to the stainless-steel syringe needle.
188 The microdroplets are transferred into the ion funnel through 189
a heated inlet, where desolvation takes place to generate ions.
190

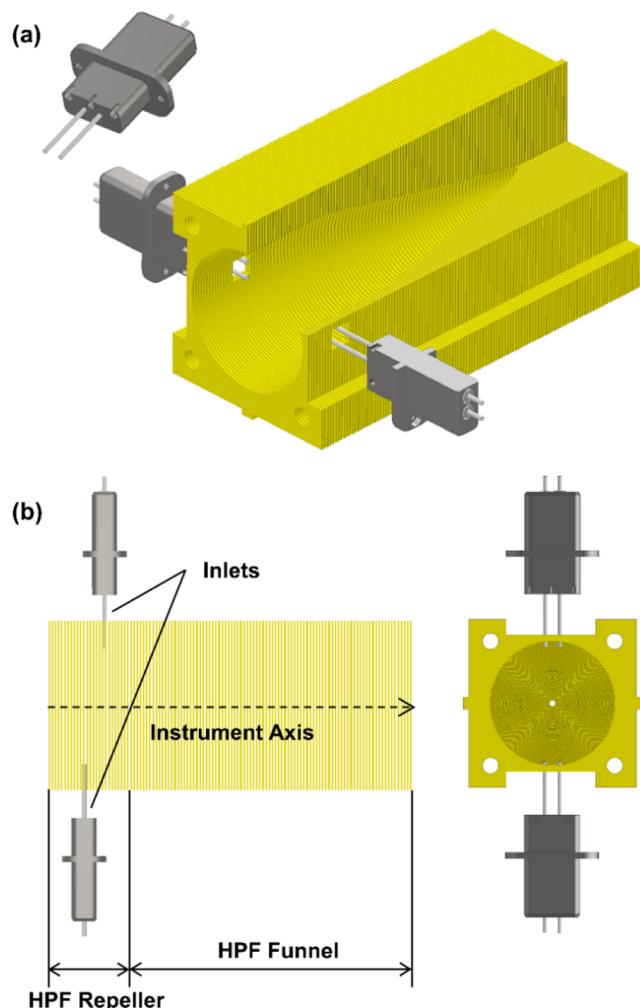


Figure 1. (a) Sectioned 3D drawing of the funnel with two two-inlet cartridges. A diagram of the two-inlet cartridge used for multiplexing experiments is shown on the top left corner. (b) Top (left) and front (right) view of the multiplexed ion funnel equipped with four heated inlets. The HPF repeller and funnel section are labeled in the schematic diagram on the left.

191 In the multiplexed mode where more than one ESI emitter is
 192 used to generate ions, each emitter is aligned with a specific
 193 heated inlet, and the same potential is applied to all the inlets.
 194 The ESI emitters that introduce ions from the same side of the
 195 HPF are mounted onto a 3D-printed bracket positioned in
 196 front of the heated inlets using a three-axis dovetail translation
 197 stage (DT12XYZ, Thorlabs Inc., Newton, NJ). Although the
 198 initial multiplexing experiments were performed using separate
 199 syringes interfaced with each ESI emitter, the complexity of the
 200 system may be reduced using T-unions for branching out the
 201 infusion lines from one syringe. In addition, quantity-limited
 202 samples for analytical applications may need to be diluted for
 203 injection into the multiplexed sources. However, this is not a
 204 concern for preparative mass spectrometry where sample is
 205 typically not quantity-limited.

206 In a typical experiment, an orthogonally injected ion beam is
 207 transferred through the HPF and LPF into the bent flatapole
 208 ion guide where collisional cooling takes place. Ions are
 209 subsequently transferred into a high-vacuum chamber and
 210 mass-selected using a quadrupole mass filter (Exrel CMS,
 211 Pittsburgh, PA), focused by an einzel lens, and directed onto a

212 current collector plate connected to a picoammeter (RBD 213 Instruments, Bend, OR) for ion current measurement. The 213 picoammeter is typically operated at a sampling rate of 300 ms, 214 and the current reported for a specific ion is averaged over a 215 time period of >30 s. 216

217 The analytical performance of the multiplexed source is 217 evaluated using a mass-dispersive rotating wall mass analyzer 218 (RWMA) described in detail elsewhere and in the *Supporting 219 Information*.^{59,60} The transmitted ion current of a particular 220 analyte is characterized by its peak intensity on an averaged ion 221 beam profile obtained using a position sensitive IonCCD 222 detector (OI Analytical, Pelham, AL). The signal intensity in 223 the averaged IonCCD profile is obtained using a Lorentzian 224 curve fitting, from which the peak height is extracted. The 225 noise level is analyzed using a section of the IonCCD profile in 226 the range of $x = (-5, 5 \text{ mm})$ where no distinct ion signal is 227 observed. The noise region of the IonCCD profile is first fitted 228 with a third-order polynomial using a Savitzky-Golay filter with 229 a 50-point window. The noise level is extracted by calculating 230 the standard deviation of the experimental profile from the 231 fitted profile. The SNR is obtained by taking the ratio of the 232 peak height to noise level. 233

234 Gas flow simulations inside the multiplexed HPF were 234 performed using the computational fluid dynamic (CFD) 235 package in Solidworks (version 2017 SP0, Waltham, MA). 236 Solidworks is a solid modeling computer-aided design (CAD) 237 software, which utilizes a parametric feature-based approach to 238 build up models and assemblies. Gas flow simulations utilized 239 Flow Simulation, a module in Solidworks that numerically 240 analyzes the flow inside the region considered to be the fluid 241 domain. The ion funnel model was recreated with as much 242 fidelity to the experimental version as possible. The model 243 included the inlet tubes, stack of ring electrodes, and the HPF 244 vacuum chamber with a pumping port. Solidworks employs 245 finite volume methods to run flow simulations due to their 246 ability to conserve flow properties (i.e., mass, momentum, and 247 energy). Once the geometric model is constructed, Solidworks 248 "meshes" the system by dividing the model into simple shapes, 249 in this case hexahedral. Although the first meshing is coarse 250 and performed automatically, it can be further refined. Refining 251 is important in places where abrupt flow changes may occur so 252 that the dynamics of the flow are accurately evaluated. As such, 253 the mesh was refined close to the capillaries and the surfaces of 254 the HPF. To predict turbulence, we used the Favre-averaged 255 Navier-Stokes equations, which incorporate time-averaged 256 effects of the turbulence perturbations. When these equations 257 are employed, extra stresses (known as Reynolds stresses) 258 appear in the equations, which are described using transport 259 equations for the turbulent kinetic energy and its dissipation 260 rate in what is known as the $k - \epsilon$ model. Solidworks has the 261 option to use a different set of interconvertible variables known 262 as turbulence intensity (Tu) and turbulence length scale (Tu_L). 263 The typical values of Tu and Tu_L are 3% and 0.001 m, 264 respectively. For the boundary conditions, the experimentally 265 measured pressures at the entrance (atmospheric pressure) and 266 exit (3–11 Torr) of the inlet tubes as well as at the HPF exit 267 (0.1–3 Torr) were applied. A temperature of 305 K was 268 applied on the inlet tubes in the simulation and to the outside 269 walls of the system. Once the simulation converged (around 270 300~400 iterations) and a steady state was reached, the 271 velocity data as a function of position was recorded. 272

273 Simulations of ion trajectories in the presence of the electric 273 field and gas flow were performed using SIMION software 274

275 package (version 8.1.1.32, Scientific Instrument Services, 276 Ringoes, NJ). The electric field was generated through a 277 combination of DC and RF voltages applied to the electrodes, 278 mimicking the voltages from the experiment. SIMION allows 279 the user to incorporate a velocity field to the ion simulations, 280 which was obtained from the CFD simulations. Since the grid 281 in the SIMION simulation is different from the grid employed 282 in Solidworks, MATLAB was used to interpolate the results 283 and transform the velocity field into a suitable grid. A program 284 was written in SIMION using the Lua programming language 285 to couple the effects of electric and flow fields. The hard sphere 286 HS1 collision model in SIMION typically employed in low- 287 pressure environments was used to simulate collisions of ions 288 with background gas. In this model, the ions are considered to 289 be spherical, and the ion–neutral interaction potential is 290 represented by a step function. Simulations were performed 291 using ions of $m/z = 608$ corresponding to triply charged 292 $\text{PMo}_{12}\text{O}_{40}^{3-}$ species. To sample the ion trajectories, 40 ions 293 (10 for each inlet) were initially positioned randomly at the 294 end of the inlet tubes within a circle of 3 mm in diameter to 295 account for diffusion. The number of ions involved in the 296 simulation was selected based off the computational power 297 available. Their initial velocity was equal to the inlet flow 298 velocity (~ 400 m/s), and its direction was randomly selected 299 from within a cone of a half angle of 15° pointing away from 300 the inlet tube. The time-step size of $0.05\ \mu\text{s}$ used in the 301 simulations is a small fraction of the RF period, which was 302 selected to properly account for the RF effects on ion 303 trajectories. Decreasing the time-step beyond this value would 304 greatly increase the computational time. Space charge was not 305 considered in these initial simulations.

306 ■ RESULTS AND DISCUSSION

307 In this study, we demonstrate that orthogonal injection into an 308 ion funnel is an efficient approach to the multiplexing of 309 electrospray ionization (ESI) sources. Specifically, we modified 310 the dual-ion funnel interface in our laboratory to combine four 311 ion beams in the high-pressure funnel (HPF, Figure 1). 312 Because the cutouts in the HPF are offset relative to each 313 other, we could only explore a “staggered” configuration of the 314 multiplexed inlets experimentally. The number of inlets was 315 selected based on the size of the cutouts in the HPF and the 316 maximum pumping speed available in the lab. We use an 317 $\text{ESI}\times n$ ($n = 1\text{--}4$) notation to represent the number of inlets 318 used to introduce ion beams generated from individual ESI 319 emitters in different instrument configurations examined in this 320 study. Specifically, $\text{ESI}\times 1$ corresponds to one ESI emitter 321 interfaced with one of the four inlets, $\text{ESI}\times 2$ corresponds to 322 two emitters interfaced with two inlets, and so on. To evaluate 323 the applicability of the multiplexing approach to different types 324 of analytes, we selected several model systems representing 325 different classes of compounds of interest to both analytical 326 and preparative mass spectrometry (MS) applications.

327 We first characterized the analytical performance of the 328 multiplexed interface by systematically introducing ion beams 329 of a single-component solution through a different number of 330 inlets while keeping the same gas flow into the HPF vacuum 331 chamber. The ion beam was analyzed using a mass-dispersive 332 device, rotating wall mass analyzer (RWMA), and an IonCCD 333 detector. The RWMA separates ions onto spatially distinct 334 rings based on their m/z . Each ring generates a pair of signals 335 symmetrically located around the center of the one-dimensional 336 IonCCD profile. The resulting spatial distribution of

ions visualized using IonCCD is a mass spectrum composed of 337 two distributions that are mirror images of one another. 338

Typical IonCCD profiles obtained at a frequency of 50 kHz 339 for $\text{Ru}(\text{bpy})_3^{2+}$ and substance P in $\text{ESI}\times n$ ($n = 1\text{--}4$) modes are 340 shown in Figure 2a,b, respectively. In the profiles, the signal is 341 f2

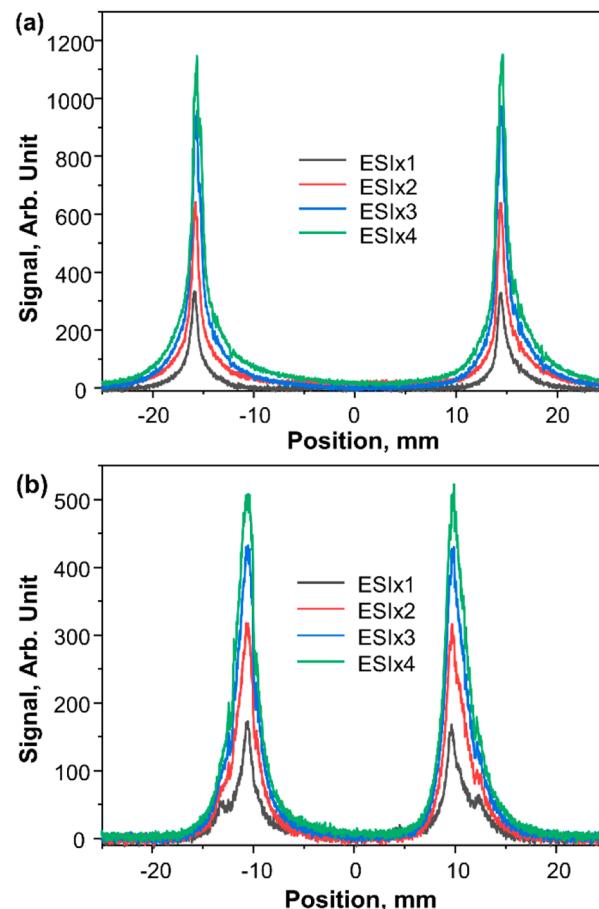


Figure 2. IonCCD profiles of $\text{Ru}(\text{bpy})_3^{2+}$ (a) and substance P (b) in $\text{ESI}\times n$ ($n = 1\text{--}4$) modes.

plotted as a function of the position on the IonCCD, which is 342 directly related to m/z . The pair of peaks in each profile in 343 Figure 2a is assigned to $\text{Ru}(\text{bpy})_3^{2+}$ at m/z 285. Meanwhile, 344 IonCCD profiles obtained for substance P (Figure 2b) contain 345 two pairs of peaks: the abundant signals at $\pm 10\text{ mm}$ and lower- 346 abundance signals at $\pm 12\text{ mm}$ assigned to $[\text{M} + 2\text{H}]^{2+}$ and $[\text{M} + 3\text{H}]^{3+}$ ions,⁶¹ respectively, using the calibration procedure 347 described in detail in our previous study.⁶⁰ The $[\text{M} + 3\text{H}]^{3+}$ 348 signal is clearly observed in the IonCCD profile obtained in the 349 $\text{ESI}\times 1$ mode (black trace) but is lower in abundance and 350 observed as a pair of shoulder peaks in IonCCD profiles 351 obtained in the $\text{ESI}\times n$ ($n = 2\text{--}4$) modes. 353

For both model systems, we observe a gradual increase in 354 signal with an increase in the number of ESI emitters from one 355 ($\text{ESI}\times 1$ mode, black trace) to four ($\text{ESI}\times 4$ mode, green trace). 356 The absolute signals and signal-to-noise ratios (SNRs) 357 obtained for $\text{Ru}(\text{bpy})_3^{2+}$ and substance P $[\text{M} + 2\text{H}]^{2+}$ are 358 shown in Figure 3. We observe that the signal intensity 359 f3 increases almost proportionally to the number of inlets with a 360 slightly smaller increase from the $\text{ESI}\times 3$ to $\text{ESI}\times 4$ modes. 361 Meanwhile, the noise level in the IonCCD profiles is the same 362 in all the $\text{ESI}\times n$ ($n = 1\text{--}4$) modes. The resulting SNR values 363

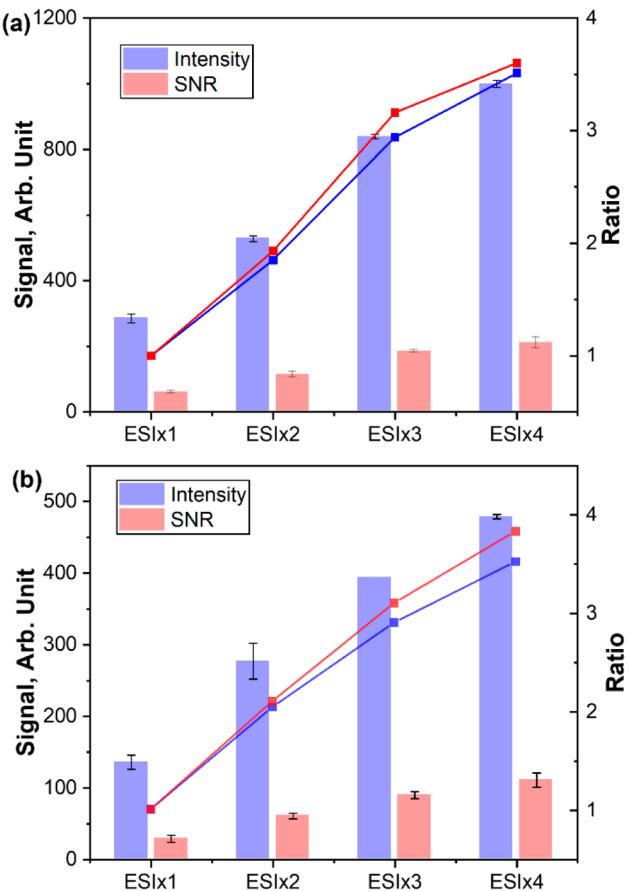


Figure 3. Peak intensities and SNRs extracted from the positive portion of the IonCCD profiles of $\text{Ru}(\text{bpy})_3^{2+}$ (a) and substance P $[\text{M} + 2\text{H}]^{2+}$ (b) shown in Figure 2 using the Lorentzian curve fitting. The blue and red bars/plots correspond to intensity and SNR of the signal in each panel.

364 follow the same trend as peak heights. This analysis indicates
 365 that multiplexing of four ESI sources results in a 3.6- and 3.8-
 366 fold increase in both the signal and SNR for $\text{Ru}(\text{bpy})_3^{2+}$ and
 367 substance P $[\text{M} + 2\text{H}]^{2+}$, respectively.

368 However, for substance P, the trend is more linear, resulting
 369 in a 3.8-fold increase in both the signal and SNR between the
 370 ESI×1 and ESI×4 modes. The observed difference between
 371 $\text{Ru}(\text{bpy})_3^{2+}$ and substance P data may be attributed to the
 372 higher overall ion current obtained for $\text{Ru}(\text{bpy})_3^{2+}$, which may
 373 result in the ion transmission loss for this system due to space-
 374 charge effects. The transmission loss may be reduced by
 375 optimizing the potential gradient between the bent flatapole
 376 offset and conductance limit, which was kept constant to
 377 ensure consistent instrument conditions in all the ESI× n ($n =$
 378 1–4) modes.

379 Figure 4a shows mass-selected ion currents obtained for
 380 several model analytes used in this study including the
 381 perchlorated *cis*-dodecaborate anion, $\text{B}_{12}\text{Cl}_{12}^{2-}$ ($m/z =$
 382 277), an anionic methoxy-oxovanadium cluster,
 383 $\text{V}_6\text{O}_7(\text{OCH}_3)_{12}^{-}$ ($m/z = 790$), a phosphotungstate anion,
 384 $\text{PW}_{12}\text{O}_{40}^{3-}$ ($m/z = 958$), and a cationic metal chalcogenide
 385 superatomic cluster, $\text{Co}_6\text{S}_8(\text{PEt}_3)_6^{+}$ ($m/z = 1317$), in the
 386 ESI×1 and ESI×4 modes. On average, we observe a 2.8-fold
 387 increase in the mass-selected ion current in the ESI×4 mode as
 388 compared to ion currents generated using a single ESI emitter.

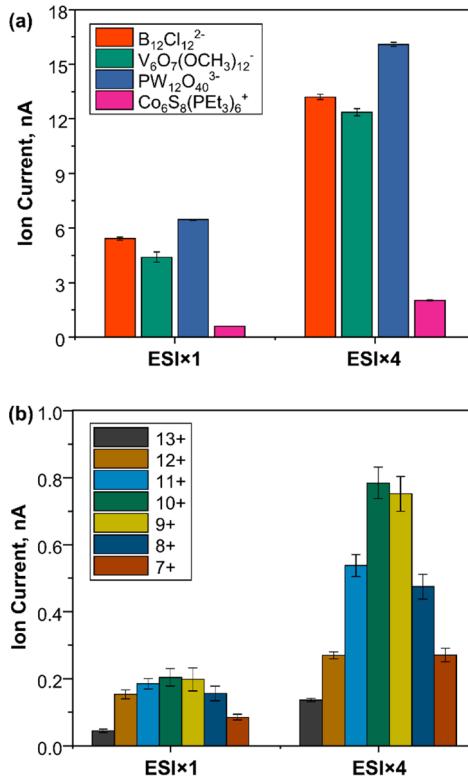


Figure 4. Mass-selected ion current obtained for (a) four model cluster ions, $\text{B}_{12}\text{Cl}_{12}^{2-}$, $\text{V}_6\text{O}_7(\text{OCH}_3)_{12}^{-}$, $\text{PW}_{12}\text{O}_{40}^{3-}$, $\text{Co}_6\text{S}_8(\text{PEt}_3)_6^{+}$, and (b) different charge states of ubiquitin (from 13+ to 7+) in the ESI×1 and ESI×4 modes.

389 **Figure 4b** shows ion currents obtained for different charge 389
 390 states of a model protein, ubiquitin ($M = 8.6$ kDa). Ubiquitin 390
 391 ions were generated from an acidic 49.5:49.5:1 methanol/ 391
 $\text{H}_2\text{O}/\text{CH}_3\text{COOH}$ (v/v/v) solution. An LTQ mass spectrum of 392
 393 5 μM ubiquitin in this solvent shown in Figure S2 displays a 394
 394 charge state distribution centered at 10+, which is consistent 394
 395 with the literature.⁶² A 20 μM ubiquitin solution was used to 395
 396 test multiplexing of ubiquitin ion beams in the ESI×4 mode. 396
 397 On average, we observe a 3.1-fold increase in the ion current 397
 398 for different charge states of ubiquitin ranging from 7+ to 13+. 398
 399 Collectively, these results demonstrate the applicability of the 399
 400 multiplexing approach to a broad range of molecular ions. 400

401 The results presented so far indicate that orthogonal 401
 402 injection of ion beams from both sides of the ion funnel 402
 403 provides an efficient way for multiplexing of independent ESI 403
 404 sources. The almost proportional increase in the ion current 404
 405 suggests that the individual inlets are effectively decoupled. To 405
 406 test this assertion, we used the ESI×2 mode to examine ion 406
 407 currents generated using different pairs of inlets. As shown in 407
 408 Figure S3, we observe similar ion currents, independent of 408
 409 which of the two inlets are used for ion beam multiplexing. 409
 410 This experiment demonstrates that independent orthogonally 410
 411 injected ion beams introduced at different locations of the ion 411
 412 funnel may be efficiently merged to generate a brighter ion 412
 413 beam.

414 The stability of the ion current over time is important to 414
 415 both analytical and preparative MS applications. Figure S4 415
 416 shows the stability of the mass-selected ion current of $\text{B}_{12}\text{Cl}_{12}^{2-}$ 416
 417 in the ESI×4 mode monitored for ~1 h. We observe a stable 417
 418 mass-selected ion current of ~13 nA (or 6.5 nA/charge), 418
 419 which is substantially higher than previously reported ESI ion 419

420 currents achieved in preparative MS applications.³⁴ This high
421 ion current may be used to achieve a deposition rate of $>10 \mu\text{g}$
422 of mass-selected ions per day, which substantially improves the
423 efficiency of ion soft landing experiments.

424 The transmission efficiency of ion funnels strongly depends
425 on the operating pressure and voltages applied to the funnel
426 plates. In particular, the radio frequency (RF) electric field is
427 critical to the radial confinement of the ion cloud. Meanwhile,
428 the direct current (DC) field drives the ions axially through the
429 ion funnel. We examined the effect of the RF and DC fields
430 along with the pressure in the ion funnel on the transmission
431 efficiency of high-intensity multiplexed ion beams of Ru-
432 (bpy)₃²⁺ generated in the ESI \times 4 mode. In these experiments,
433 the total ion current dominated by Ru(bpy)₃²⁺ was
434 measured on the rods of the bent flatapole ion guide to
435 quantify the transmission efficiency of the ion funnel interface.
436 Figure 5a shows the ion current transmitted at different RF

437 currents achieved in preparative MS applications.³⁴ This high
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447 along with the pressure in the ion funnel on the transmission
448 efficiency of high-intensity multiplexed ion beams of Ru-
449 (bpy)₃²⁺ generated in the ESI \times 4 mode. In these experiments,
450 the total ion current dominated by Ru(bpy)₃²⁺ was
451 measured on the rods of the bent flatapole ion guide to
452 quantify the transmission efficiency of the ion funnel interface.
453 Figure 5a shows the ion current transmitted at different RF

454 currents achieved in preparative MS applications.³⁴ This high
455 ion current may be used to achieve a deposition rate of $>10 \mu\text{g}$
456 of mass-selected ions per day, which substantially improves the
457 efficiency of ion soft landing experiments.

458 Figure 5a also shows the transmitted ion current at different DC
459 gradients averaged from three measurements. As described in our
460 previous study,⁵⁸ the HPF is composed of a repeller and funnel
461 section. The DC gradient in the repeller section does not have a
462 significant effect on ion transmission. In contrast, the ion current
463 increases with increase in the axial DC gradient in the funnel region.
464 The highest ion current was obtained at a DC gradient of 28 V/cm (320 V DC
465 voltage difference between the first and last electrodes). A further increase in the
466 DC gradient caused a failure of the power supply, which led to a substantially lower and
467 unstable ion current (Figure 5a, ~ 30 V/cm, DC voltage at 330 V). In the future, we will upgrade the
468 DC power supply to obtain the optimal DC gradient required for
469 multiplexing.

470 We also studied the effect of pressure in the HPF ion transmission
471 using the RF of 230 V_{p-p} and a DC of 28 V/cm. The operating pressures in the ion funnels were
472 adjusted by choking the valve on the VARODRY VD 200 mechanical
473 pump evacuating the HPF chamber. We observed a decrease in
474 the ion current with increase in the HPF pressure (Figure 5b), which is in
475 agreement with previous studies, according to which ion diffusion in ion funnels enhanced at higher
476 pressures makes it more difficult to focus the ions using RF and DC fields.⁶³ The highest ion transmission was observed at the
477 lowest achievable pressure of 7.25 Torr. We expect that ion transmission may be further improved using more powerful
478 vacuum pumps or by increasing the upper limit of the DC power supply to maintain ion transmission at higher HPF
479 pressures.

480 To obtain further insights into the ion transmission in the ESI \times 4 mode and rationalize the experimental results, we carried out a series of SIMION ion trajectory simulations combined with gas flow calculations. The simulations were also used to examine the performance of another geometry of the ESI \times 4 mode, which cannot be currently implemented in our experiments. In particular, we compared the results obtained using the staggered 2 + 2 inlet configuration (two inlets on the two sides of the HPF) implemented in the experiments and aligned 2 + 2 configuration, which will be examined experimentally in future studies.

481 Figure 6a shows the gas flow velocity in the plane defined by the center of the exit aperture of the HPF and the centers of both cutouts in the repeller region of the HPF. The inlets are located above and below this plane and are equidistant from it. The velocity maps provide insights into gas dynamics inside different regions of the inner space of the HPF. For both the staggered and aligned geometries, the highest gas flow velocity is observed in the HPF repeller region, which is consistent with the previously reported supersonic gas expansion on the vacuum side of capillary inlets. Meanwhile, the flow fields indicate significant differences between the aligned and staggered configurations. Specifically, in the staggered configuration, the different high-speed gas flows exiting the inlets pass each other and move directly to the opposite sides of the HPF with an average gas velocity in the repeller region of >10 m/s. In contrast, in the aligned configuration, the interaction between the high-speed gas flows results in a decrease in the

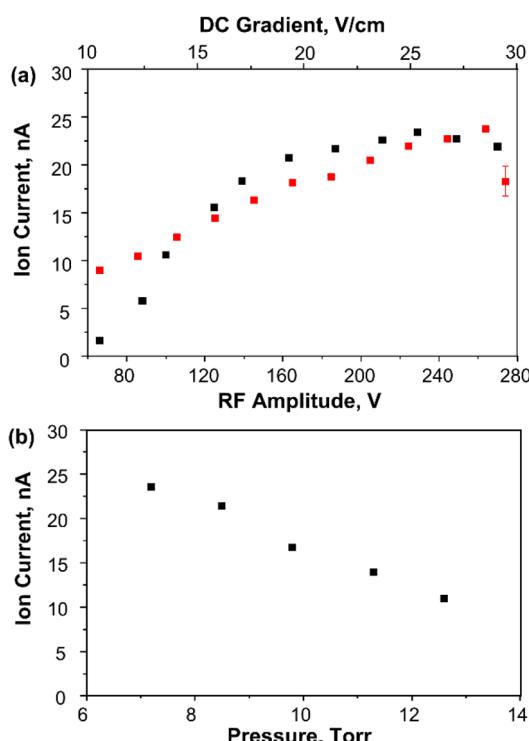


Figure 5. Ion current of Ru(bpy)₃²⁺ as a function of (a) RF amplitude (black), DC gradient (red), and (b) pressure in the HPF.

482 amplitudes applied to the HPF at a resonance frequency of 740
483 kHz. The transmission efficiency increases with increase in the
484 RF amplitude and reaches a plateau at 230 V_{p-p} (peak-to-peak
485 voltage). Further increase in the RF amplitude results in a
486 decrease in transmission. We attribute this decrease in signal to
487 an increase in the low-mass cutoff with an increase in the RF
488 amplitude, which discriminates against lower-*m/z* ions such as
489 Ru(bpy)₃²⁺. The optimal RF amplitude of 230 V_{p-p} found for
490 the ESI \times 4 mode is higher than the typical value of 150 V_{p-p}
491 used when only two orthogonal inlets are coupled into the ion
492 funnel operated at a similar pressure.⁵⁸ This may be attributed
493 to the space-charge-induced expansion of the brighter ion
494 beam produced in the ESI \times 4 mode, which requires a deeper
495 RF potential well to radially confine the beam. Space-charge
496 effects are determined by the magnitude of the ion current, ion
497 kinetic energy, and volume traversed by the ion beam and may

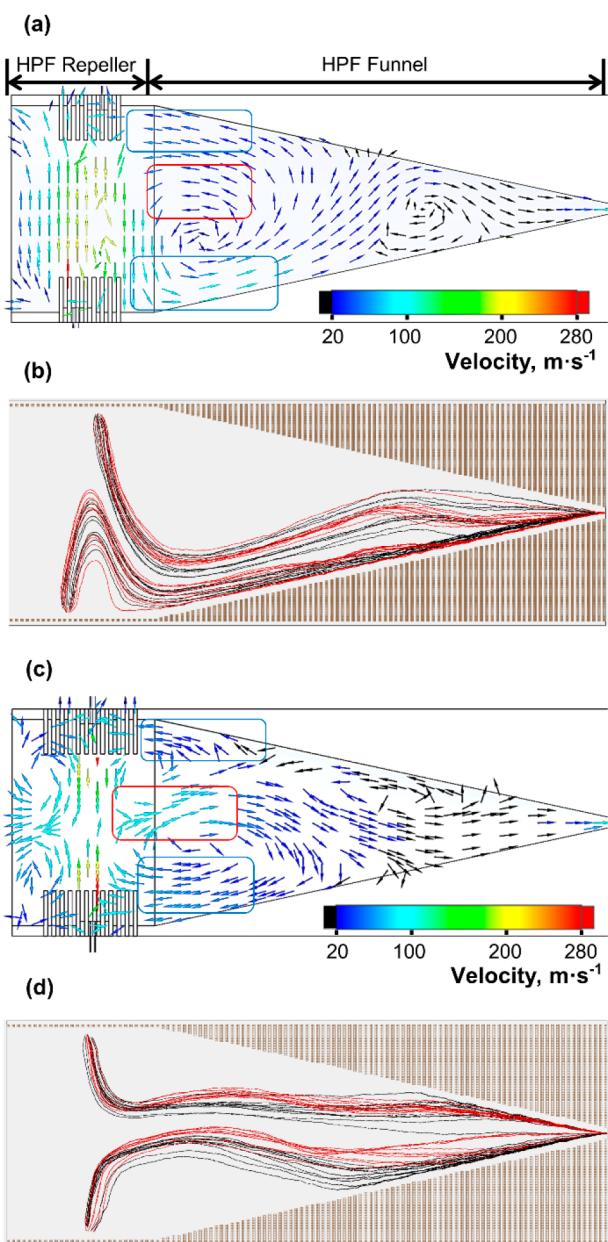


Figure 6. Gas flow velocity field of the HPF along the central plane for the staggered (a) and aligned (c) 2 + 2 inlet configurations. The direction and velocity of the gas flow at a specific location are depicted by the arrows colored according to the velocity scale. The color bar is shown in each panel with velocities below 20 m/s colored in black. The center and off-centered area of the wide opening of the HPF funnel region are marked with red and blue squircles in panels (a) and (c). SIMION simulations of ion trajectories obtained for $m/z = 608$ in the HPF in the presence of both the gas flow and RF and DC electric fields in the staggered (b) and aligned (d) 2 + 2 inlet configurations.

516 average gas velocity in the center of the repeller region to ~ 100
 517 m/s. In both configurations, gas flow velocities decrease to
 518 < 100 m/s in the funnel region where both gas streams merge
 519 and move toward the HPF exit along the instrument axis.
 520 The gas dynamics in the funnel region of the HPF shows
 521 substantial differences between the staggered and aligned 2 + 2
 522 configurations. In particular, in the center of the HPF funnel
 523 region highlighted by red squircles in Figure 6a,c, gas flow

524 moves upstream in the staggered configuration and down-
 525 stream in the aligned configuration. In the off-centered 525
 526 locations of the funnel region highlighted with blue squircles, 526
 527 gas flow moves in the opposite directions on the two sides of 527
 528 the HPF when the inlets are in the staggered configuration. In 528
 529 contrast, in the aligned configuration, gas flow moves upstream 529
 530 toward the repeller region on both sides of the HPF. The 530
 531 observed differences in the gas flow dynamics in the staggered 531
 532 and aligned configurations have a pronounced effect on ion 532
 533 trajectories. Figure 6b,d shows ion trajectories in the presence 533
 534 of the same electric field for gas flow fields shown in Figure 534
 535 and 6c for the staggered and aligned 2 + 2 configurations, 535
 536 respectively. In the staggered configuration, ions produced in 536
 537 the upstream inlets shown on the bottom of the diagram 537
 538 initially follow the streams coming out of the inlets. However, 538
 539 they are deflected by the DC field into the incoming jets from 539
 540 the top of the diagram, which deflect the ions toward the 540
 541 electrodes (Figure 6b). Subsequently, the upstream ion 541
 542 "crawling" is due to the high-speed gas flow in the region 542
 543 between the repeller and funnel section shown in Figure 6a. In 543
 544 this area, gas dynamics dominate over the electric field, turning 544
 545 the ion beam back toward the HPF wall. Meanwhile, ions 546
 546 produced by the downstream inlets shown on the top of the 547
 547 diagram are not blocked by the streams of the other jets and 548
 548 start to make the turn toward the funnel region earlier. In the 549
 549 aligned configuration, in the same region between the repeller 550
 550 and the funnel region of the HPF, gas flow directs the ions to 551
 551 the center of the HPF where they make the turn toward the 552
 552 funnel region (Figure 6c). As a result, we observe close to 553
 553 symmetric ion trajectories from both sides of the HPF that are 554
 554 directed toward the center of the HPF where ions are extracted 555
 555 by the electric field and directed toward the HPF exit. In this 556
 556 configuration, the gas flow keeps the ions away from the 557
 557 electrodes and potentially eliminates ion transmission losses. 558
 558 Regardless of the shape of ion trajectories, SIMION 559
 559 simulations presented in Figure 6b support the experimentally 560
 560 observed additive ion transmission from the four inlets in the 561
 561 ESI $\times 4$ mode. Based on the simulation results, we conclude 562
 562 that ion transmission in the aligned 2 + 2 configuration may 563
 563 provide better results than that in the staggered configuration, 564
 564 which was examined experimentally in this study. In the future, 565
 565 we will redesign the HPF chamber to enable multiplexing using 566
 566 the aligned inlet configuration, which will allow us to evaluate 567
 567 the performance of the aligned configuration. 568

We also carried out simulations to understand the effect of 569
 pressure in the HPF on multiplexing. Figure S5 shows gas flow 570
 velocity fields and ion trajectories of the 2 + 2 aligned 571
 configuration at three different pressures of 11, 7, and 4 Torr. 572
 At higher pressures of 11 and 7 Torr (Figure S5a,b), gas flow 573
 573 between the repeller and the funnel region of the HPF is 574
 directed downstream along the HPF axis, which is favorable for 575
 575 ion transmission. At a lower pressure of 4 Torr, gas flow in the 576
 center of the HPF funnel region moves away from the central 577
 axis, which is detrimental to ion transmission. Consequently, 578
 the calculated ion trajectories start to diffuse away from the 579
 HPF central axis earlier at 4 Torr. This effect is not observed at 580
 higher pressures, which rationalizes the improved ion trans- 581
 mission at 7 and 11 Torr. We also observe that at 7 Torr, ion 582
 582 trajectories are kept farthest away from the electrodes. From 583
 the pressure-dependent study, we conclude that 7 Torr is the 584
 optimal HPF pressure for multiplexing of ESI sources using the 585
 2 + 2 aligned configuration. We note that although the 586

587 simulations were performed with a temperature of the inlet
588 tubes of 305 K, we anticipate qualitatively similar results at
589 higher temperatures of ~450 K used experimentally. Reiss et
590 al. have demonstrated that the maximum gas flow velocity
591 through a heated inlet increases by <10 m/s with a
592 temperature increase from 350 to 550 K.³⁰ Interestingly, the
593 maximum gas velocity is observed ~0.2 mm off the inlet axis at
594 550 K. The relatively small increase in gas velocity and small
595 offset off the inlet tube axis will not affect to a significant extent
596 the results of the gas flow and ion trajectory simulations
597 reported herein.

598 ■ CONCLUSIONS

599 In this study, we demonstrate that orthogonal injection of ions
600 into an electrodynamic ion funnel is a promising approach for
601 the multiplexing of independent ESI sources. In particular, we
602 used a total of four orthogonal inlets that were split into two
603 pairs and implemented on the opposite sides of the ion funnel.
604 For the different types of analytes used in our proof-of-concept
605 experiments, we observed an almost proportional increase in
606 both the ion current and SNR with increase in the number of
607 orthogonal inlets used for ion beam injection. Using the
608 optimized values of the instrument parameters including the
609 RF amplitude, axial DC gradient, and pressure in the HPF, we
610 have achieved a maximum mass-selected ion current of up to 7
611 nanoamperes per charge, which corresponds to the deposition
612 of >10 μg of mass-selected ions per day, substantially higher
613 than the typical deposition rate of ~1 μg with a single ESI
614 source. The bright ion source developed in this study provides
615 a direct path for materials synthesis and device fabrication
616 using beams of mass-selected ions. Furthermore, analytical MS
617 applications would benefit from this mode of multiplexing,
618 which increases the SNR in proportion to the number of inlets.
619 The experimental results were rationalized using the combined
620 gas flow and ion trajectory simulations. The simulations were
621 further employed to examine the aligned inlet configuration,
622 which could not be implemented experimentally. Based on the
623 simulation results, we conclude that it is possible to further
624 optimize the geometry of the multiplexing configuration. We
625 envision that multiplexing of more than four ESI sources is
626 possible using more powerful mechanical pumps to maintain
627 the pressure in the HPF at its optimal value. In addition to
628 preparative MS applications, multiplexed ESI sources may be
629 implemented on commercial analytical mass spectrometers,
630 which will improve their performance in analytical applications
631 including multiomics studies, single-cell analysis, and bio-
632 molecular imaging.

633 ■ ASSOCIATED CONTENT

634 ■ Supporting Information

635 The Supporting Information is available free of charge at
636 <https://pubs.acs.org/doi/10.1021/acs.analchem.1c02092>.

637 Description of RWMA; Figure S1: Schematic diagram of
638 the high-transmission ESI interface; Figure S2: ESI-MS
639 spectrum of ubiquitin; Figure S3. Mass-selected ion
640 current of $\text{B}_{12}\text{Cl}_{12}^{2-}$ in the ESI×2 mode; Figure S4.
641 Long-term stability of ion current of $\text{B}_{12}\text{Cl}_{12}^{2-}$; Figure
642 S5. Gas flow velocity fields and ion trajectories at
643 different pressures ([PDF](#))

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Notes

The authors declare no competing financial interest.

[¶]Undergraduate researcher. (A.J.S.)

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