

Capturing the Transient Microstructure of a Physically Assembled Gel Subjected to Temperature and Large Deformation

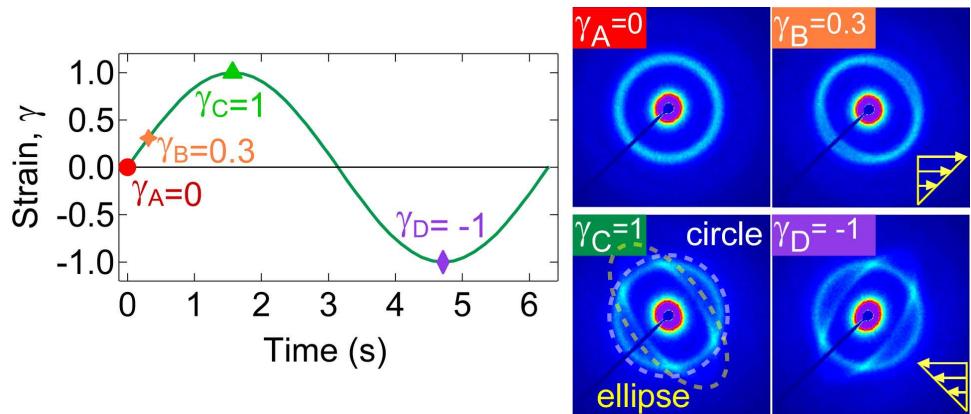
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Abstract

The microstructure of physically assembled gels depends on mechanical loading and environmental stimuli such as temperature. Here, we report the real-time change in the structure of physically assembled triblock copolymer gels that consist of 10 wt% and 20 wt% of poly(styrene)-poly(isoprene)-poly(styrene) [PS-PI-PS] triblock copolymer in mineral oil (i) during the gelation process with decreasing temperature, (ii) subjected to large oscillatory deformation, and (iii) during the stress-relaxation process after the application of a step-strain. The presence of loosely bounded PS-aggregates at temperatures higher than the rheologically determined gelation temperature (T_{gel}) captures the progressive gelation process spanning over a broad temperature range. However, the microstructure fully develops at temperatures sufficiently lower than T_{gel} . The microstructure orients in the stretching direction with the applied strain. In an oscillation strain cycle, such oriented structure has been observed at low-strain. But, at large-strain, because of strain-localization the oriented structure splits, and only a fraction of midblock participates in load-bearing. Both microstructure recovery and time-dependent moduli during the stress-relaxation process after the application of a step-strain have been captured using a stretched-exponential model. However, the microstructure recovery time has been found to be two orders of magnitude slower than the stress-relaxation time at room temperature, indicating a complex nature of stress-relaxation and microstructure recovery processes involving midblock relaxation, end-block pullout and reassociation. Due to their viscoelastic nature, these gels' mechanical responses are sensitive to strain, temperature, and rate of deformation. Therefore, insights into the microstructural information as a function of these parameters will assist these gels' real-life applications and design new gels with improved properties.

Introduction

ABA triblock copolymer gels in B-selective solvents are a class of gels that have garnered significant research interests over the last few decades.¹⁻⁸ These gels have been investigated for

their potential applications in various areas ranging from biomedical fields as wound dressing,⁹ protein carriers,¹⁰ and drug delivery,^{11,12} to ballistics,¹³ microfluidic devices,¹⁴ and soft robotics.^{15,16} These gels are significantly different than chemically crosslinked gels,^{16,17} and the underlying principle of gelation in these gels is the strong temperature-dependent solubility of the A-blocks (endblock) in the chosen solvent, in comparison to the very little change of solubility of the B-blocks (midblock) with temperature. Specifically, at higher temperatures, both A- and B-blocks are soluble in the solvent, however, the A-block's solubility becomes poor with the decrease of temperature. This causes the aggregation of a few A-blocks at low temperatures, forming physically associated crosslinks (aggregates) bridged by B-blocks. The B-blocks remain soluble in the solvent and act as load-bearing chains. This process leads to the formation of a physically assembled triblock copolymer gel. As captured using simulation studies, the gel microstructure at a particular temperature result from the free energy balance and is influenced by the factors such as the block lengths, solvent compatibility to endblocks, polymer volume fraction, corona crowdedness.¹⁸⁻²¹ The gels investigated in this study consist of poly(styrene)-poly(isoprene)-poly(styrene) [PS-PI-PS] in mineral oil. Here, the PS-blocks (A-blocks) form the aggregates, and these are connected by load-bearing bridges of PI-blocks (B-blocks).^{1,2,4,6,7} Due to the temperature-dependent solubility of A- and B-blocks, these gels are thermoreversible, and become a polymer solution (*sol*) at higher temperatures and gel again at lower temperatures.

Previously, there has been a significant effort to understand the effect of polymer volume fraction (ϕ),^{4,7,22} temperature,^{4,22} block lengths,^{7,13,19-21} endblock homopolymer addition,⁵ and solvent²³ on the physical properties of triblock copolymer gels, such as gelation behavior, critical gelation concentration, stress-relaxation, moduli, and rate-dependent responses. However, most of these properties were realized through macroscopic experimental observations, and the relationships between their mechanical properties and the microstructure are not well established.

Small-angle neutron/X-ray (SANS/SAXS) scattering has been used to understand the

change in ABA gel microstructure while varying the ϕ ,^{1,4} endblock and midblock lengths,^{4,7} and temperature,^{4,22} but mostly at the static condition. In those studies, structural information obtained from the scattering data at the static condition has been used to explain the gel responses subjected to mechanical deformation, leaving a gap between the theoretical understanding, prediction, and the experimental observations. For example, the characteristic time-scale for stress-relaxation in these gels determined from rheological experiments has been linked to the endblocks pullout from the aggregates and their reassociation with other aggregates.^{2,4,6,7,22,24-26} However, no information is available regarding the time scale associated with complete microstructure recovery. Therefore, real-time observation of the change in gel microstructure subjected to a mechanical deformation can provide further understanding regarding the microstructure-dependent mechanical properties of these gels, including structural reorganization during the relaxation process.

Such investigation requires real-time data collection using SAXS/SANS techniques while the gel is subjected to the mechanical loading. However, these experiments possess two main challenges. The first challenge is the requirement of a fast data collection necessary to capture the microstructure at any particular stress or strain value. This can be overcome by using a high flux beam typical to synchrotron. The second challenge is the availability of an instrument that allows the data collection along the appropriate plane. There are many reports in the literature to elucidate the real-time microstructural change during processing, and subjected to flow, mechanical loading, and magnetic field on polymers,²⁷⁻³³ complex fluids,^{34,35} protein gels,³⁶ and wormlike micelles.^{37,38} In these studies, interesting microstructure development such as shear-rate dependent orientation development has been reported. However, similar investigations for ABA gels are limited, as the previous investigations on acrylic gels formed by poly(methyl methacrylate)–poly(n-butyl acrylate)–poly(methyl methacrylate) [PMMA–PnBA–PMMA] in 2-ethyl-1-hexanol and n-butanol capture the microstructure only at the static condition.^{7,23,39}

For high modulus polymers and elastomers, it is possible to capture the real-time mi-

crostructural change as a function of uniaxial strain typically achieved in tensile testing.^{30,40} However, there are significant challenges to capture the real-time microstructure data during the tensile test of physically assembled gels. Particularly, because of their lower modulus, it is difficult to hold these samples in a tensile testing instrument. Also, the samples can undergo creep during the tests.^{6,7} Alternatively, the change in the gel microstructure subjected to mechanical deformation can be investigated in a shear-stage, where the scattering data collection is in the x-y plane while the beam is in the z-direction. Here "x" represents the flow/stretch direction (v), "y" denotes velocity gradient (∇v), and "z" denotes the vorticity direction ($v \times \nabla v$). Using this setup, microstructural information in the stretch, or flow direction, and orthogonal to that, i.e., in the gradient direction can be collected. Our experimental setup is similar to that has been recently utilized to investigate the structural change in associative protein gels subjected to thermal load, oscillatory deformation, and during stress-relaxation.³⁶

The present work focuses on real-time investigation of microstructural change in physically assembled PS-PI-Ps gels in mineral oil as a function of temperature, oscillatory strain, and during stress-relaxation. We have explored such transient microstructure in gels consisting of 10 wt% and 20 wt% of PS-PI-PS triblock copolymer, referred to as 10%-Gel and 20%-Gel, respectively. The PI-block molecular weight is higher than its entanglement molecular weight (≈ 6.4 kg/mol), leading to a slight entanglement of PI-blocks in 20%-Gel. We have used both the RheoSAXS and shear-rheometry techniques in parallel to relate the microstructural change with the applied load since our RheoSAXS setup cannot measure the stress.^{31,36} The RheoSAXS data was collected in the x-y plane, which provided a unique insight regarding the gel microstructure, particularly during large amplitude oscillatory strain (LAOS), where the structure changes reversibly in a strain-cycle.

Experimental Methods

Materials. Kraton D1164 is a poly(styrene)-poly(isoprene)-poly(styrene) [PS-PI-PS] tri-block copolymer, kindly provided by Kraton Inc. Klearol white mineral oil (kindly provided by Sonneborn Inc.) was the solvent used for the gel preparation.⁶⁻⁸ The number-average (M_n) and weight-average (M_w) molecular weight of D1164 polymer are ≈ 112 kg/mol and ≈ 125 kg/mol, respectively, estimated based on the polystyrene standard.⁶⁻⁸ The polymer has 29 wt% of PS and 71 wt% of PI, as indicated by the manufacturer. The estimated M_n of the PS-block is ≈ 16.2 kg/mol, and that of the PI-block is ≈ 79.4 kg/mol.

Sample preparation. The samples were prepared by adding the desired amount of D1164 polymer in white mineral oil and mixing at 120 °C by using a magnetic stirrer at 320 rpm. The polymer solutions were placed in a convective oven at 120 °C for 6 hrs, allowing the bubbles to escape, leading to clear solutions. Gels were obtained by cooling these solutions. We have considered two gels with 10 wt% and 20 wt% concentrations of D1164 polymer, corresponding to the polymer volume fractions (ϕ) of 0.089 and 0.181,^{6,7} respectively. These gels are referred to as 10%-Gel and 20%-Gel throughout this article. Table S1 summarizes the polymer weight and volume fractions and the PS and PI weight fractions in each gel.

Shear-rheometry. For the shear-rheometry, polymer solution was poured in a rectangular mold of 2 mm thickness and was allowed to cool for ≈ 30 min through natural cooling, obtaining gel sheets. Square-shaped specimens (30 mm \times 30 mm) were cut from the gel sheets for individual rheological experiments. A TA Instruments Discovery HR-2 hybrid rheometer equipped with a Peltier plate was used. The experiments were conducted using a 25 mm parallel plate geometry with a gap of 1 mm. 240 grit adhesive-backed silicon carbide sandpaper (Allied High Tech Products Inc.) was attached to the top and bottom plates to avoid possible slippage of samples on the rheometer plates. These experiments are referred to as shear-rheometry in the present article to distinguish them from the RheoSAXS experiments, which were performed in the synchrotron beamline as described below.

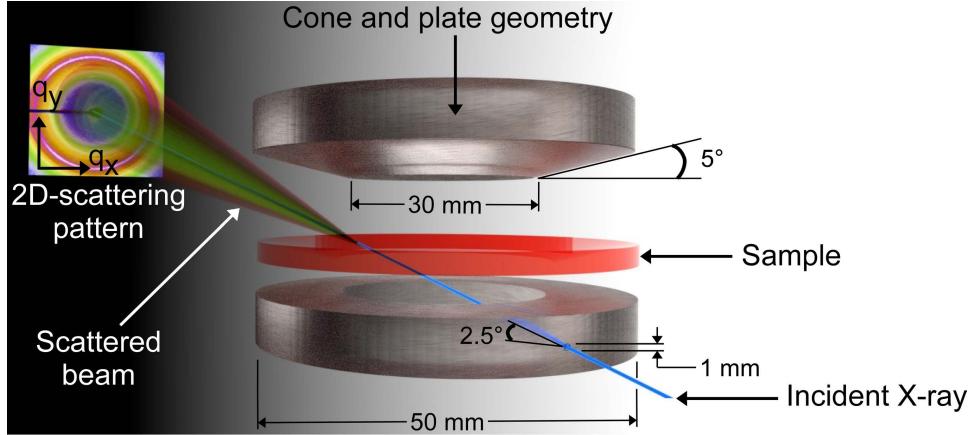


Figure 1: Schematic of the RheoSAXS setup with relevant details. The beam-path leading to data collection in the x-y plane is also presented.

RheoSAXS experiments. The rheometry experiments in conjunction with the small-angle X-ray scattering (RheoSAXS) experiments were conducted for the 10%- and 20%-Gels on the DND-CAT beamline of the Advanced Photon Source at Argonne National Lab (ANL, Chicago, IL). The X-ray have a wavelength of 0.7293 Å (energy=17 keV). A custom-built shear-stage equipped with an annular cone and plate geometry was used (Figure 1).^{31,36} The top geometry (cone) had a cone angle of 5°. The annular bottom plate had an inner diameter of 30 mm and an outer diameter of 50 mm. A 1 mm diameter pinhole (beam path) drilled through the bottom plate of the shear-stage at an angle of 2.5°, allowed the X-ray beam to pass through the sample (Figure 1). This bottom plate was equipped with a thermocouple. The samples were loaded in the *sol* state at \approx 80 °C and 100 °C for the 10%- and 20%-Gel, respectively. For the experiments at room temperature, the samples were cooled down to room temperature (\approx 27 °C) by blowing air on the samples for \approx 30 minutes to ensure their thermal equilibrium. The shear-stage was then tilted by 2.5° from its horizontal axis to align the beam-path for capturing the scattering data at the flow-vorticity plane.^{31,36,41} For the experiments where the scattering data were collected as a function of temperature, the samples were loaded in liquid state and the stage was tilted before cooling the sample. In these cases, the sample was allowed to cool naturally without blowing air onto the sample.

However, for the experiments performed at higher temperatures than room temperature, like the stress-relaxation experiments at 40 °C, the samples were brought down to experimental temperature by blowing air. A minimum waiting time of 15 min was allowed at the experimental temperature to attain thermal and structural equilibrium. Unless there was a macroscopic fracture, the same sample was used for multiple rheological experiments. However, after each experiment, the samples were heated to the sol state to erase the strain history. If the sample fractured during the test, a fresh sample was loaded using the same procedure discussed above.

The scattering data were collected for 10%- and 20%-Gels in three sets of experiments *viz.* (1) temperature sweep without any applied strain as the gelation of sample taking place, (2) oscillatory shear experiments with strain amplitudes (γ_{amp}) of 0.1 and 1, using a frequency (ω) of 1 rad/s at different temperatures, and (3) stress-relaxation experiments at different temperatures after the application of a step shear strain (γ_{step}) of 0.3. The two-dimensional (2D) scattering patterns were collected using a CCD detector. Igor Pro Nika package was used for data reduction from the 2D-scattering profiles to 1D intensity ($I(q)$) versus scattering vector (q) plots.^{42,43} A custom-built NCNR macro was used to fit the data with a polydispersed core hard-sphere model and its modified form.⁴⁴ Custom-built programs in MATLAB were also implemented to generate the azimuthal scans over a particular q -range and to estimate anisotropy.^{31,36}

Results and Discussion

Effect of Temperature on the Gel Microstructure

The gelation temperature (T_{gel}) and moduli of the gels were captured by using shear-rheometry performed with an oscillation frequency (ω) of 1 rad/s and strain amplitude (γ_{amp}) of 0.01 over the temperature (T) range of 80-20 °C and of 100-20 °C for the 10%- and the 20%-Gels, respectively. Correspondingly, to capture the evolution of the gel microstructure

with decreasing temperature, RheoSAXS experiments were performed over \approx 80 to 27 °C for the 10%-Gel, and from \approx 120 to 27 °C for the 20%-Gel. Note that the RheoSAXS setup cannot measure the stress, therefore, the change in microstructure observed in the RheoSAXS experiments has been related to the data obtained from the shear-rheometry.

Figure 2A displays the evolution of storage (G') and loss (G'') moduli for 10%- and 20%-Gels as a function of temperature. At high temperature, both gels behave like a viscous liquid (*sol*-state) as G'' is higher than G' . An increase in G' and G'' with the decrease of temperature indicates the formation of a network structure in these samples. At further lower temperature, a crossover of G' and G'' is observed, which can be identified as the gelation temperature (T_{gel}) corresponding to $\omega=1$ rad/s. The T_{gel} has been found to be \approx 63 °C for 10%-Gel and \approx 85 °C for 20%-Gel, respectively. For $T \leq 45$ °C, G' reaches a plateau with the values of 2.9 and 11.1 kPa for 10%- and 20%-Gels, respectively.

As discussed above, both PS- and PI-blocks' good solubility at high temperatures leads to a viscous solution. At low temperatures, the polymer network is formed because of physically associated PS-blocks connected by PI-blocks.^{1,2,6-8} A higher number of load-bearing chains in 20%-Gel as a result of higher polymer concentration leads to a higher G' value than that for 10%-Gel. Also, the higher number of chains facilitates the network formation at relatively higher temperature, therefore the 20%-Gel has higher T_{gel} .

T_{gel} determined by shear-rheometry generally varies with the applied frequency (ω), therefore, Winter-Chambon criterion is commonly implemented to identify the true gelation temperature.⁴⁵⁻⁴⁷ We have shown earlier that this gel does not follow Winter-Chambon criterion, similar to a few other physically assembled gels.^{8,48,49} It has been shown that for 10%-Gel, the G' and G'' crossover shifts by \approx 20 °C as ω increases from 0.1 to 100 rad/s.⁸ Therefore, the T_{gel} indicated here can be considered as the apparent gelation temperature, which is expected to change with applied ω . Note that the T_{gels} are sufficiently higher than the room temperature, therefore, the microstructure formation at room temperature is expected to be complete.

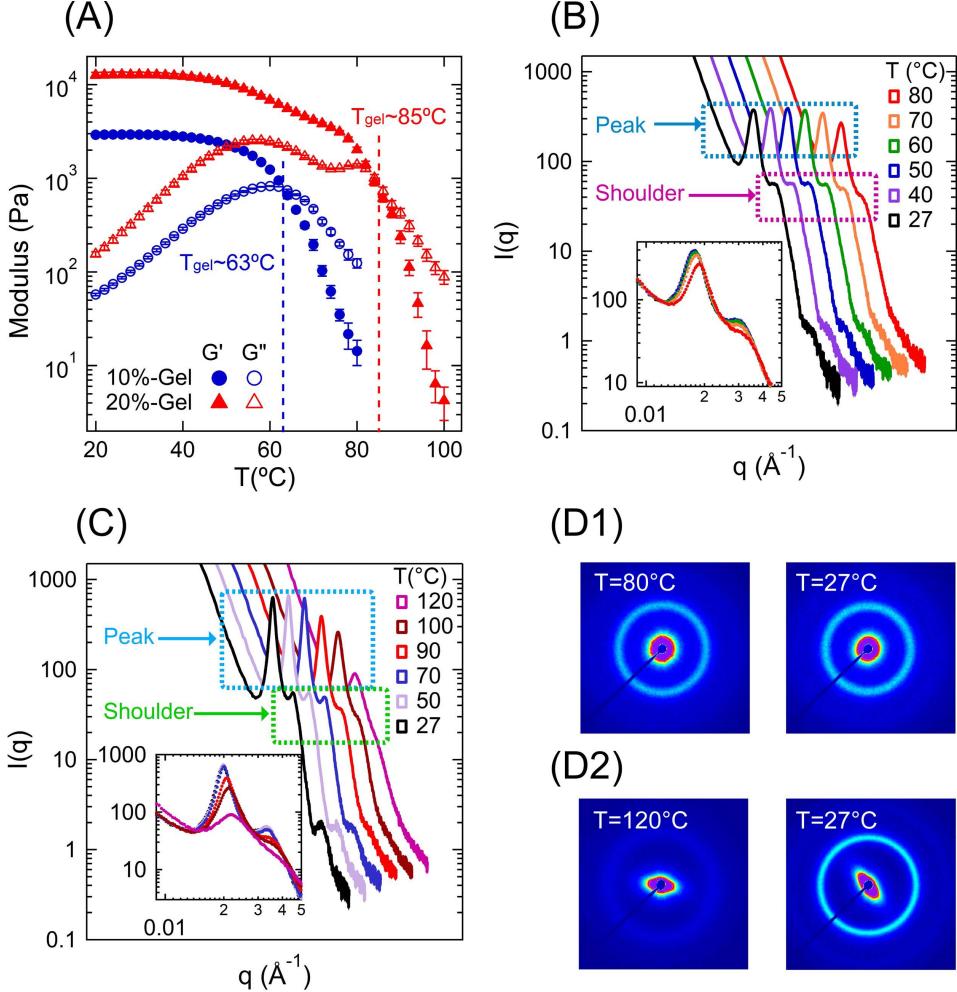


Figure 2: Temperature dependent gelation process. (A) Storage modulus (G') and loss modulus (G'') as a function of temperature (T) for 10%- and 20%-Gels captured using shear-rheometry with an oscillatory amplitude (γ_{amp}) of 0.01 and frequency (ω) of 1 rad/s. A cooling rate of 2 °C/min with a soak time of 300 s was applied. Intensity ($I(q)$) as a function of scattering angle (q) for (B) 10%-Gel at 27, 40, 50, 60, 70, and 80 °C, and for (C) 20%-Gel at 27, 50, 70, 90, 100, and 120 °C. The curves are shifted along the q -axis for clarity. The insets in B and C represent the $I(q)$ vs. q without shifting. The 2D-scattering patterns above T_{gel} and at room temperature are shown for (D1) 10%-Gel and (D2) 20%-Gel.

For capturing the change in gel microstructure using RheoSAXS, the samples were heated sufficiently above their T_{gel} and allowed to cool to 27 °C by natural convection (≈ 20 min). Particularly, the 10%-Gel sample was heated to 80 °C and the 20%-Gel to 120 °C, and was thermally equilibrated for ≈ 3 min at those temperatures. During cooling, the scattering data were collected at every 5 °C of temperature drop with an exposure time of 0.03 s. As

the sample was cooling continuously, there was a possibility of a small temperature gradient within the sample during the data collection. Figure 2B and C represent the circular averaged intensity $I(q)$ as a function of scattering vector (q) for the 10%- and 20%-Gels at different temperature. The 2D-scattering patterns presented in Figure 2D display a circular pattern indicating the isotropic gel microstructure as now was applied (i.e., static condition). Note that the elongated circle near the beam center captures the low- q region ($<0.0002 \text{ \AA}^{-1}$) and is mostly an experimental artifact that has not been considered for the analysis.

For both gels, a decrease in T causes the evolution of the microstructure, which is manifested by increased intensity and narrowing of the peak at $q \approx 0.02 \text{ \AA}^{-1}$. Development of a weak shoulder at $q \approx 0.03 \text{ \AA}^{-1}$ is also observed. This shoulder corresponds to a low-intensity circle in the 2D-scattering profiles (Figure 2D1-D2). The peak at $q \approx 0.02 \text{ \AA}^{-1}$ is related to the structure factor (Bragg peak) capturing inter-aggregate scattering, and the shoulder at $q \approx 0.03 \text{ \AA}^{-1}$ is primarily contributed by the form factor of PS-aggregates.^{6,7} As displayed in Figure S1 for 10%-Gel, $I(q) \propto q^{-3 \text{ to } -3.2}$ over the q -range of $0.0003 \leq q \leq 0.01 \text{ \AA}^{-1}$ for the temperatures considered here signifies a rough surface fractal similar to that observed for acrylic gels.²³ This fractal structure is a consequence of the local clustering of aggregates resulting in inhomogeneity in the gel structure. Further, $I(q) \propto q^{-4}$ for $0.04 \leq q \leq 0.06 \text{ \AA}^{-1}$ indicates the presence of spherical aggregates.

At $T < 45 \text{ }^{\circ}\text{C}$, the scattering profiles overlap and those do not change significantly with a further reduction in T (Figure 2B-C insets) indicating a developed microstructure, which is also evident from the plateau in G' (Figure 2A). The peaks beyond $q \approx 0.05 \text{ \AA}^{-1}$ are secondary reflections of the form factor.⁵⁰ Interestingly, the Bragg peak at $q \approx 0.02 \text{ \AA}^{-1}$ and a weak shoulder at $q \approx 0.03 \text{ \AA}^{-1}$ are also observed at $T \geq T_{gel}$ for both gels, although at a lower intensity than that observed below T_{gel} (see Figure 2B). The initiation of the aggregate formation above the T_{gel} supports the argument that the shear-rheometry capture an apparent gelation temperature. Also, gelation does not occur at a single temperature but takes place over a temperature range. A similar evolution of the structure and form factors

with temperature had also been captured for acrylic gels.^{4,23}

To capture the network characteristics, a polydispersed core hard-sphere model with Percus-Yevick closure has been used to fit the scattering data for the q -range of $0.01 \leq q \leq 0.050 \text{ \AA}^{-1}$.^{4,6,7,23} Mathematically, this model is expressed as, $I(q) \propto P(q)S_1(q)$, where $P(q)$ represents the spherical form factor and $S_1(q)$ the structure factor. As shown schematically in Figure S2, the PS aggregates are represented by cores with mean radius r_c and polydispersity σ/r_c , where σ is the standard deviation of r_c .^{4,6-8,23} These aggregates are surrounded by a fictitious hard sphere with an average thickness s_1 and a volume fraction ψ_1 . Considering that every hard-sphere is contained in a fictitious cube with a dimension D_1 (see Figure S2), the center-to-center inter-aggregate distance can be estimated as, $D_1 = (4\pi(r_c + s_1)^3/(3\psi_1))^{1/3}$.^{4,51} After subtracting the background, the features for $q > 0.050 \text{ \AA}^{-1}$ and $q < 0.01 \text{ \AA}^{-1}$ are not very discernible and have not been considered here for further analysis.

Figure 3A compares the scattering profiles for the 10%- and 20%-Gels at $\approx 28 \text{ }^\circ\text{C}$. The solid lines represent the model fit, which capture the data reasonably well. Note that the structure factor peak for 10%-Gel is at slightly lower q than that for 20%-Gel, indicating a higher inter-aggregate distance. The fitted parameters at different temperatures for both gels are shown in Figure 3B and C for 10% and 20%-Gels, respectively.

These values are typical of the physically assembled gels in midblock-selective solvents.^{1,2,4,6-8,23} For both gels, r_c , s_1 , and ψ_1 evolve with decreasing T . For 10%-Gel, r_c remains almost constant ($\approx 8.6 \text{ nm}$), s_1 increases from 9.1 to 10.5 nm, and ψ_1 increases from 0.4 to 0.44 as T decreases from 80 to 27 $^\circ\text{C}$. Similarly, for 20% gel, r_c increases from 7.1 nm to 8.6 nm, s_1 increases from 6.8 to 9.2 nm, and ψ_1 increases from 0.29 to 0.50 while decreasing T from 120 to 27 $^\circ\text{C}$. Despite a lower number of polymer chains in 10%-Gel, the r_c is similar to that of 20%-Gel, indicating a lower number density of aggregates in the 10%-Gel. As a result, a higher hard-spheres thickness (s_1) and lower volume fraction (ψ_1) have been observed in 10%-Gel.

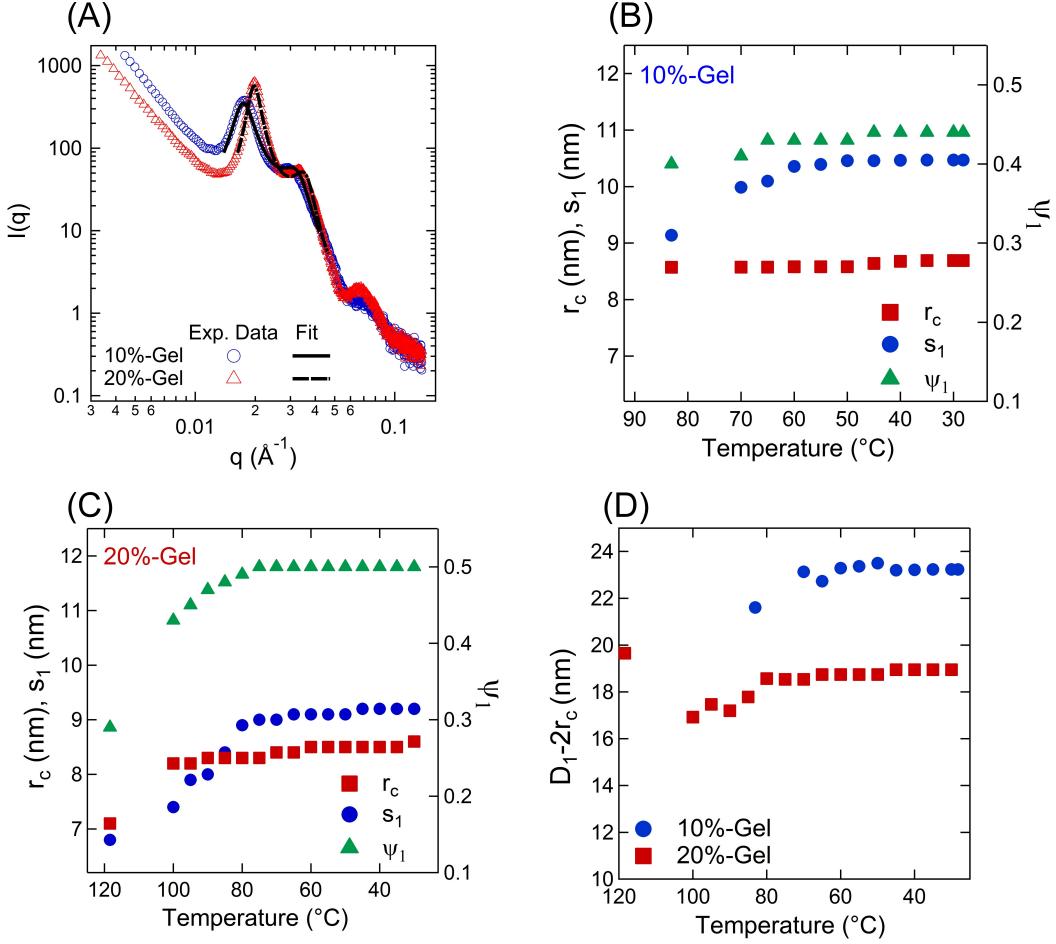


Figure 3: Evolution of gel microstructure as a function of temperature. (A) Comparison of $I(q)$ vs. q for 10%- and 20%-Gels at $T=27$ °C (markers), and fitting with a polydispersed core hard-sphere model (lines). Fitted parameters, *viz.* the core radius (r_c), hard-sphere thickness (s_1), and hard-sphere volume fraction (ψ_1) are presented as a function of temperature for the (B) 10%-Gel and (C) 20%-Gel. (D) PI block end-to-end distance ($D_1 - 2r_c$) in 10%-Gel and 20%-Gel.

The evolution of fitted microstructural parameters as a function temperature suggests that the microstructure of both gels first evolves with decreasing temperature. However, the microstructure almost remains unchanged below 50 °C for 10%-Gel and 75 °C for 20%-Gel. Although the evolution of microstructure for both gels follows the same trend, indicating gelation through a similar mechanism, the polymer chain density influences the network formation. For both gels, the temperatures at which the microstructure reaches the plateaus are approximately 10-13 °C lower than their respective T_{gel} . Interestingly, a comparison of

the evolution of G' (Figure 2A) and microstructural parameters (Figure 3B-C) indicates that microstructure has mostly developed at a relatively higher temperature. However, the PS-blocks can still be mobile. With a further decrease in temperature, the solvent quality for the PS-blocks becomes poorer, leading to low mobility of PS-blocks and frozen aggregates. Consequentially, G' attains a plateau.²³

With decreasing T , the PS-aggregates expel the solvent,^{3,4} and this process can lead to the decrease of the aggregates radii. However, our data suggest that r_c increases slightly, especially in 20%-Gel. It can be hypothesized that at higher T , the PS-blocks loosely associate to form smaller aggregates. Also, dangling PS-chains that are not connected to any aggregate also exist. This is also evident from not so well-developed form factor shoulders (weaker intensity) in Figure 2B-C. With the decrease in T , those non-connected PS-blocks merge in the existing bigger aggregates leading to an increase of r_c . The space between two aggregates also increases slightly to accommodate the PI chains, leading to an increase in s_1 .

The length of PI-block in the gels can be theoretically estimated by considering the mineral oil as a θ -solvent.^{2,6,7,52} The end-to-end distance of a PI-block in θ -solvent can be calculated as, $R_{e,PI} = b\sqrt{N} \approx 21.6$ nm, where b (≈ 0.84 nm) and N (≈ 662) are the length and number of Kuhn segments per PI-block, respectively.^{6,7,53} The estimated end-to-end distance of PI-block ($D_1 - 2r_c$) in 10%- and 20%-Gel are 23.2 and 18.9 nm at ≈ 28 °C. These values are close to that estimated using θ -solvent condition, therefore justifying our assumption.

Microstructural Change with Oscillatory Shear

The effect of shear deformation on the gel microstructure was explored using oscillatory shear experiments. Figure 4A displays G' and G'' for 10%- and 20%-Gels obtained from amplitude sweep experiments at 27 °C. The strain-amplitude (γ_{amp}) was varied over the range of 10^{-4} to 1 using ω of 1 rad/s. Over this range, the gel samples did not fail, and no noticeable change in G' and G'' was observed. The stress-controlled rheometer used in this study could

not correct the phase-angle accurately beyond $\gamma_{amp} > 1$, thus, those data have not been considered here. Note that we have also conducted the amplitude sweep experiments using cone and plate geometry, and parallel plate geometry without adhesive-backed sandpaper. We did not observe any significant differences in the moduli values (see Figure S3 in SI).

In RheoSAXS experiments, the 10%-Gel was subjected to oscillatory strain-amplitude of $\gamma_{amp}=0.1$ at 27 °C, and $\gamma_{amp}=1$ at 27 °C and 40 °C, respectively. Similarly, the 20%-Gel was subjected to $\gamma_{amp}=0.1$ and 1 at 27 °C. All these experiments were conducted using $\omega=1$ rad/s. For the experiments at 27 °C, three cycles with $\gamma_{amp}=0.1$ were applied, followed by three cycles with $\gamma_{amp}=1$. The scattering data were collected during three oscillatory cycles with an exposure time of 0.03 and 0.05 s for the 10%- and the 20%-Gel, respectively. With such a short exposure time, we estimate a maximum $\approx 5\%$ change in intracycle strain value while collecting the data. The time interval between two data points was 0.157 s, resulting in ≈ 40 data points over a strain cycle. Figure 4B represents a strain cycle for $\gamma_{amp}=1$ in which thirteen representative intracycle strain values ($\gamma_1 - \gamma_{13}$) are selected. The 2D-scattering patterns corresponding to these strain values for 10%- and 20%-Gels are displayed in Figure 4C and D. Two movies capturing the 2D-scattering pattern as a function of strain over three strain cycles for 10%- and 20%-Gels are shown in SI (10%Gel_27C_Strain1.avi, 20%Gel_27C_Strain1.avi). The inset in Figure 4B inset represents the stress vs. strain data for 20%-Gel in which a small hysteresis of the gel can be noted.

A particular strain-cycle can be divided into four quarters, for $\gamma = 0$ to $+1$, $+1$ to 0 , 0 to -1 , and -1 to 0 . For both gels, at $\gamma_1 (= 0)$, the scattering pattern is circular, indicating isotropic gel microstructure at the static condition (Figure 4C and D).^{4,6,7,23} For 10%-Gel, in the first quarter, as the strain increases, the circular pattern transforms to an elliptical pattern having clear major and minor axes (for example, $\gamma_2 = 0.31$). The elliptical pattern splits into two parts, elliptical and circular patterns, with increasing strain, as presented for $\gamma_3 = 0.71$. The circular pattern displays $I(q) - q$ profile similar to that observed at $\gamma_1 = 0$, however, with structure factor slightly shifted from $q=0.0160$ Å⁻¹ to 0.0165 Å⁻¹. With

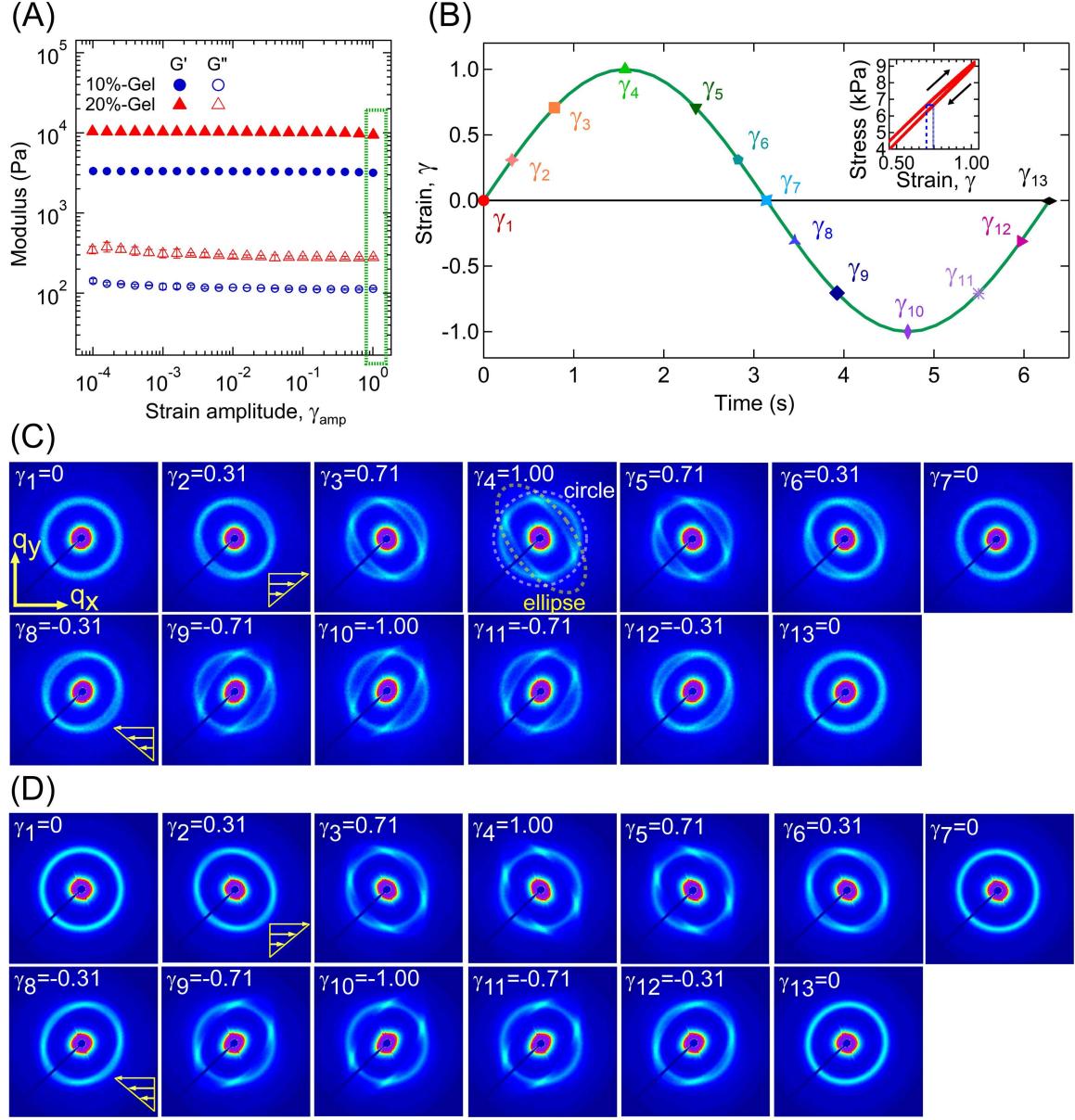


Figure 4: Shear-rheometry and RheoSAXS results for oscillatory shear experiments at 27 °C. (A) Storage modulus (G') and loss modulus (G'') as a function of strain amplitude (γ_{amp}) for 10%- and 20%-Gels using a frequency (ω) of 1 rad/s. The results for $\gamma_{amp}=1$ are highlighted. The error bars, smaller than the markers in some cases, represent one standard deviation. (B) Schematic of one oscillatory strain cycle as a function of time for $\gamma_{amp}=1$ at $\omega=1$ rad/s. The inset displays the stress vs. strain plot for 20%-Gel displaying a small hysteresis of the gel. The markers on the strain cycle correspond to the 2D-scattering patterns presented in (C) for 10%-Gel, and (D) for 20%-Gel. In C and D, q_x represents v or flow direction and q_y represents ∇v or velocity gradient direction.

increasing strain to $\gamma_4 = 1$, the split becomes more prominent. Interestingly, the q -value corresponding to the intersection of circular and elliptical profiles displays higher intensity relative to the other q -values. This intensity is similar to that observed for all q -values at γ_1 .

In the second quarter, as the strain values decrease to 0, the split pattern transforms to a purely elliptical pattern and then to a circular pattern at $\gamma_7 = 0$. In the 3rd quarter, the scattering pattern resembles that of the 1st quarter, however, the angle of orientation of the elliptical pattern changes because of the change in applied strain direction in an oscillatory cycle. Further, the data for 2nd and 4th quarters are similar. Note that scattering patterns for $\gamma = 0.31$ in the 1st and 2nd quarters, i.e., for γ_2 and γ_6 , are slightly different. We relate that to the slight hysteresis in the strain cycle (Figure 4B inset). Here, for the same stress values (≈ 6.7 kPa) there are two different γ values (≈ 0.71 and ≈ 0.75), which may have affected the symmetry of the 2D-scattering pattern with respect to γ . For 20%-Gel, the strain-dependent scattering profiles are very similar to those of 10%-Gel, except that the split elliptical pattern is more prominent in 10%-Gel (Figure 4D). 2D-scattering profiles are also represented for both gels for $\gamma_{amp}=0.1$ in Figure S4. For this low strain amplitude, no split in 2D-pattern was observed.

Figure 5A1-A3 displays the 2D-scattering patterns for 10%-Gel at the intracycle strain of $\gamma=0$, $+1$, and -1 . The corresponding $I(q)$ vs. q for different β values have been plotted by averaging $I(q)$ over $\beta \pm 5^\circ$ sector (Figure 5B-D). Here, β corresponds to the angle measured from the q_x -axis or flow direction (Figure 5A). As shown in Figure 5B, the scattering profiles at $\beta \approx 95^\circ$ and 155° for $\gamma=+1$, at $\beta \approx 30^\circ$ and 85° for $\gamma=-1$, and at $\beta \approx 0^\circ$ and 90° for $\gamma=0$ overlap. For $\gamma = \pm 1$, these β values represent the intersection between elliptical and circular patterns. Along the minor-axis of the elliptical pattern, i.e., the scattering profiles at $\beta \approx 35^\circ$ for $\gamma=+1$ (Figure 5A2) and at $\beta \approx 145^\circ$ for $\gamma=-1$ (Figure 5A3) overlap, as shown in Figure 5C. Similarly, as presented in Figure 5D, the scattering profiles along the major-axis of the elliptical pattern, i.e., at $\beta \approx 125^\circ$ for $\gamma=+1$ (Figure 5A2), and at $\beta \approx 55^\circ$ for $\gamma=-1$ (Figure 5A3) overlap.

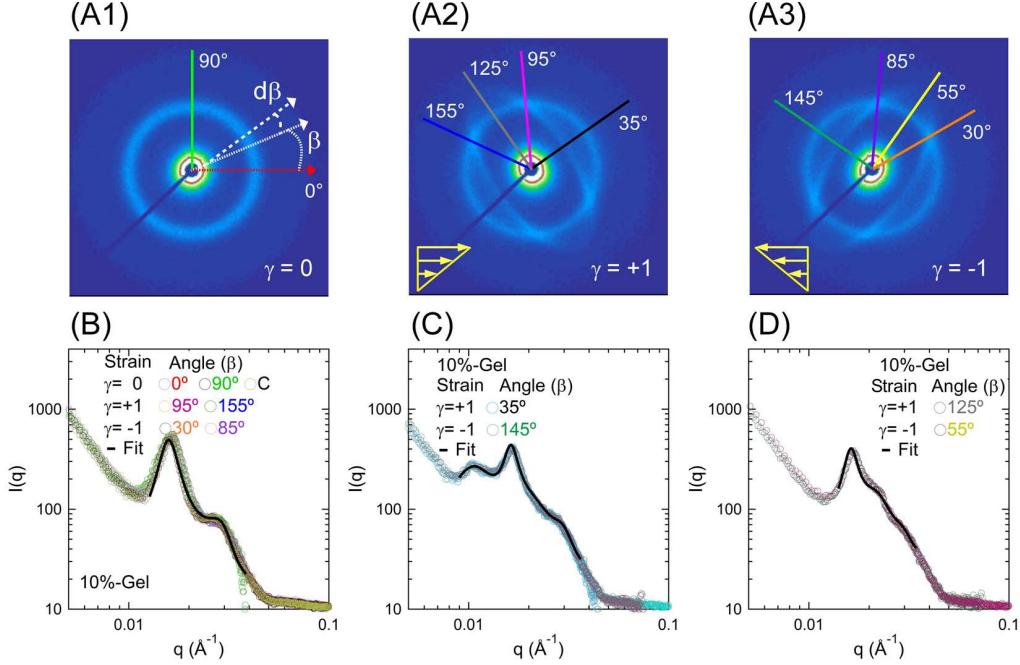


Figure 5: Scattering patterns and $I(q) - q$ plots for 10%-Gel at 27 °C for the strain amplitude of 1 and for the static condition. The azimuthal angle β is defined in (A1). The 2D-scattering patterns are shown for (A1) $\gamma=0$, (A2) $\gamma=+1$ (clockwise), and (A3) $\gamma=-1$ (anticlockwise). 1D-scattering patterns and model fit are shown for (B) circular pattern and intersection between circle and ellipse, (C) minor-axis of the ellipse, and (D) major-axis of the ellipse.

The $I(q) - q$ plots along the minor-axis of the ellipse for $\gamma = \pm 1$ display an additional peak at $q \approx 0.01 \text{ \AA}^{-1}$ (Figure 5C) compared to that for $\gamma=0$. Also, a slight decrease in the intensity of the peak at $q \approx 0.017 \text{ \AA}^{-1}$ can be noticed. A similar comparison between the $I(q) - q$ plots along the major-axis of the ellipse for $\gamma = \pm 1$, and that for $\gamma=0$ also indicates an additional peak at $q \approx 0.023 \text{ \AA}^{-1}$ (Figure 5D). However, this peak is in the vicinity of the form factor shoulder and is not clearly discernible. The decrease in the intensity of the structure factor peak is associated with the emergence of the additional peak signifying the change in inter-aggregate distance for some aggregates. In other words, the additional peak is also a structure factor peak with different inter-aggregate distance. As shown in Figure 5C-D, both elliptical and circular patterns are observed at $\gamma = \pm 1$. Further, the position and the intensity of the form factor shoulder remain similar for all γ values. The unchanged form factor peak signifies that the aggregates' shape and size have not changed

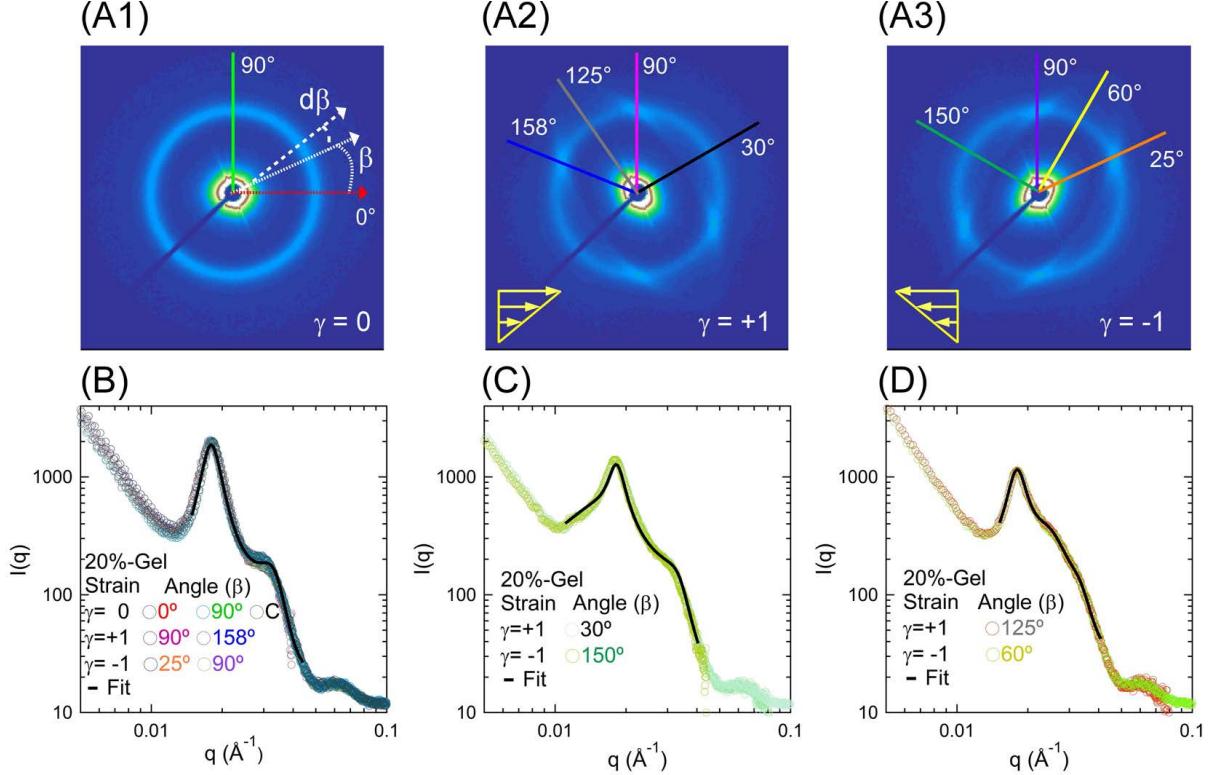


Figure 6: Scattering patterns and $I(q) - q$ plots for 20%-Gel at 27 °C for the strain amplitude of 1 and for the static condition. 2D-scattering patterns are shown for (A1) $\gamma=0$, (A2) $\gamma=+1$ (clockwise), and (A3) $\gamma=-1$ (anticlockwise). 1D-scattering patterns and model fit are shown for (B) circular pattern and intersection between circle and ellipse, (C) minor-axis of the ellipse, and (D) major-axis of the ellipse.

in the γ -range considered here. Similar behavior has also been observed for the 20%-Gel presented in Figure 6A-D. As shown in Figure 6B-D, at $\gamma = \pm 1$ and -1, additional peaks appear at $q \approx 0.013 \text{ \AA}^{-1}$ and $q \approx 0.025 \text{ \AA}^{-1}$, respectively. However, these additional peaks are not as prominent as for the case of 10%-Gel.

The overlapping data for $\gamma = \pm 1$ shown above indicate that the microstructure change during a strain cycle is independent of γ direction and solely depends on its magnitude ($|\gamma|$). Fitting a model to the extra peak of the $I(q) - q$ data along the minor and major axes of the elliptical pattern can provide additional insights regarding the change in gel microstructure with γ . As the aggregates remain the same, the scattering data in Figure 5B and 6B can be fitted with the same polydispersed core hard-sphere model described above for the static samples. A modified form of the polydispersed core hard-sphere model, mathematically

expressed as $I(q) \sim P(q)(S_1(q) + S_2(q))$ has been used. Here, $S_1(q)$ represents the structure factor corresponding to the circular pattern (or intersection). $S_2(q)$ represents the secondary structure factor corresponding to the elliptical pattern capturing the new peak. Note that the form factor ($P(q)$) is the same for $S_1(q)$ and $S_2(q)$, capturing that the features of the PS-aggregates do not change upon deformation. Note that this model results in two hard-sphere volume fractions, ψ_1 and ψ_2 , because of change in the inter-aggregate distance.

The model fittings are shown in Figure 5B-D and 6B-D for 10%- and 20%-Gels, respectively, and the fitted parameters are presented in Table 1. The r_c values for 10%- and 20%-Gels in Figure 5B and 6B are slightly higher than those observed in temperature sweep experiments presented in Figure 3B at 27 °C. This is possibly due to the different cooling cycled allowed in both experiments. Here, the samples were cooled by blowing air for ≈ 30 min while the data related to Figure 3 was collected during natural cooling of the gels (≈ 20 min). However, the difference in the r_c values is not very significant, as the change is within the limit of polydispersity ($\sigma/r_c \approx 0.2$).

Table 1: Parameters obtained from fitting scattering data to polydispersed core hard-sphere model with Percus-Yevick closure for three different sectors at $\gamma=0$, $+1$ and -1 .

Sample	Sector	r_c (nm)	σ/r_0	s_1 (nm)	ψ_1	s_2 (nm)	ψ_2
10%-Gel	intersection	10.2	0.01	11.0	0.43	–	–
	minor-axis	10.2	0.17	11.0	0.48	18.8	0.27
	major-axis	10.2	0.30	11.0	0.48	4.0	0.33
20%-Gel	intersection	9.3	0.19	9.6	0.46	–	–
	minor-axis	9.3	0.10	9.6	0.48	9.8	0.19
	major-axis	9.3	0.28	9.6	0.47	2.9	0.30

For the 10%-Gel, the inter-aggregate distance (D_1) at the static condition ($\gamma=0$) is estimated as ≈ 45.3 nm. For $|\gamma|=1$, two additional inter-aggregate distances (D_2) can be estimated corresponding to the major- and minor-axes. D_2 along the minor- and major-axes is expected to capture the inter-aggregate distance for the displaced aggregates because of applied strain (see Figure S5). Similar to D_1 , D_2 can be estimated as $(4\pi(r_c + s_2)^3/(3\psi_2))^{1/3}$ using the fitted parameters s_2 and ψ_2 . We obtain $D_1 \approx 43.6$ nm from the circular profiles

which is observed in addition to the elliptical profiles for $|\gamma|=1$, resembling the isotropic case of $\gamma=0$. The D_2 values corresponding to the major- and minor-axis are ≈ 33.1 nm and 72.3 nm, respectively. Similarly, for 20%-Gel, D_1 is ≈ 39.2 nm, and D_2 values are ≈ 53.6 nm and ≈ 29.4 nm for the minor- and major-axes, respectively. The smaller and higher D_2 values represent the decrease and increase in the inter-aggregate distance, respectively.

With the applied γ , the inter-aggregate distance (or hard-sphere thickness) increases in the stretch direction. As a result, the inter-aggregate distance in the orthogonal direction decreases, signifying a compression of hard-spheres. The corresponding stretch or compression ratios can be estimated as D_2/D_1 , the ratio of center-to-center distance of aggregates with and without stretching. We estimate the stretch and compression ratios as ≈ 1.65 and 0.75 for the 10%-Gel, and ≈ 1.37 and 0.75 for 20%-Gel respectively. The scattering data implies that the compression ratios are similar for these gels, whereas the stretch ratios are slightly different. These ratios can be related to the applied macroscopic deformation. For affine deformation of polymer chains, γ can be theoretically related to the uniaxial stretch/compression ratio (λ) as $\gamma = \lambda - \lambda^{-1}$.⁵⁴ For $\gamma=1$, this relationship provides $\lambda=1.62$ and -0.62, where the positive and negative signs indicate stretching and compression, respectively. The theoretical stretch ratio is similar to that obtained from the scattering data for 10%-Gel, but it is slightly higher than that for 20%-Gel. The compression ratios for gels are similar, however, are slightly lower than that estimated theoretically. Due to finite sizes of aggregates, which do not change significantly during shear, the stretch or compression ratios experienced by PI-blocks are slightly different than that estimated using D_2/D_1 . Those can be estimated as $(D_2 - 2r_c)/(D_1 - 2r_c)$. We estimate the stretch and compression ratios for the PI-blocks are ≈ 2.23 and ≈ 0.55 for 10%-Gel, and ≈ 1.72 and ≈ 0.52 for 20%-Gel, respectively.

For the case of 20%-Gel, a deviation in the stretch ratio than that obtained theoretically can be attributed to the relatively higher inhomogeneity in the microstructure, likely aided by the slightly entangled PI-blocks.^{6,7} In addition, thermal quenching protocol used here can also cause higher inhomogeneity in the gel microstructure. These local variations in the

microstructure can be viewed as defects, which can cause strain localization, as reported for the acrylic gels.^{55,56} In summary, the oscillatory shear-rheometry results indicate that the PI chains are stretched in the flow direction and are compressed in the orthogonal direction. The stretch and compression ratios are similar to those predicted theoretically. An oriented microstructure results in an elliptical 2D-scattering pattern. However, the presence of both elliptical and circular patterns at larger intracycle strain indicates that some of the aggregates have retracted to their unperturbed/non-stretched condition. We hypothesize that the strain-localization is present in these samples,^{55,56} where the local strain values can be different than the macroscopic strain value applied on the sample. We further postulate that some of the chains are being stretched, and those follow the applied strain over multiple cycles leading to the elliptical pattern, whereas, other chains do not follow the applied strain beyond a certain strain-value and relax to the nonstretched condition within a strain cycle.

It can also be argued that such strain-localization weakens the non-linear behavior of these gels, for example, strain-stiffening responses, which are prominent in the acrylic gels.^{25,57} For acrylic gels, these strain-stiffening responses were related to the maximum extensibility of midblocks before being pulled out from the aggregates. We have not observed any clear sign of non-linearity from the rheological responses of the gels investigated here, i.e., the e_3 and ν_3 values are almost zero.⁵⁷⁻⁶¹ It may be possible that because of local inhomogeneity individual PI-block may have reached the maximum stretchability, but collectively not displaying strain-stiffening response. Also, weaker association of PS blocks in comparison to that of PMMA block in the acrlyic gels cannot be ruled out. Further investigations will be necessary to identify the underlying principle precisely.

Stress-Relaxation Behavior

The viscoelastic nature of these gels causes stress dissipation when subjected to load. This dissipation process can be quantified through stress-relaxation experiments. In these experiments, a step shear strain (γ_{step}) was applied on the gels, and the samples were then allowed

to relax. The time-dependent stress decay ($\sigma(t)$) was recorded during the relaxation process and the corresponding time-dependent shear modulus ($G(t)$) can be estimated as $\sigma(t)/\gamma_{step}$. The corresponding change in microstructure was investigated from RheoSAXS experiments. Figure 7A1 represents the stress-relaxation behavior of a 10%-Gel at 40 °C over 600 s for $\gamma_{step}=0.3$. The relaxation behavior for $0.1 \leq t \leq 1800$ is shown in Figure S6. However, data only up to 600 s is presented here to compare with the RheoSAXS data. Similarly, for 20%-Gel, $G(t)$ was obtained at 50 and 70 °C (Figure 7B1-C1). Note that for 70 °C, the relaxation process is quite fast, resulting in a steeper decrease of $G(t)$. The experiments were also conducted for both gels at 27 °C where a smooth decay of $G(t)$ is observed (see Figure S8). For each case, $G(t)$ reaches a plateau after the relaxation process, indicating an equilibrium modulus. At higher T and lower polymer concentration, a relatively steeper decrease of $G(t)$ has been noticed.

RheoSAXS experiments were conducted at the same temperatures indicated above and $\gamma_{step}=0.3$ was applied. The scattering data were collected for 600 s with an X-ray exposure time of 0.03 s at an interval of 3 s. 2D-scattering profiles at different time points during the relaxation process are displayed in Figure 7A2-C2. Here, t_1 displays the circular pattern at the static condition. At t_2 , an elliptical pattern is observed representing a stretched or oriented structure as a result of applied γ_{step} . Figure S7 represents the $I(q)-q$ data before and after the application of strain for 20%-Gel at 50 °C. Here, we have compared the data along major- and minor-axes with that of the static condition. The shifting of structure factor peak to lower- q along the elliptical pattern's minor axis represents the sample stretch. Similarly, the data along the major-axis signifies the compression of those in the orthogonal direction. The form-factor peak display a slight change in intensity, however, the q -position does not change appreciably. Similar to that presented in the previous section, fitting the scattering data with polydispersed core hard-sphere model estimates stretching and compression ratios of 20%-Gel at 50 °C along the minor- and major-axes (D_2/D_1) as 1.15 and 0.95, respectively. These values are comparable to the theoretical prediction of 1.16 and 0.86, respectively. For

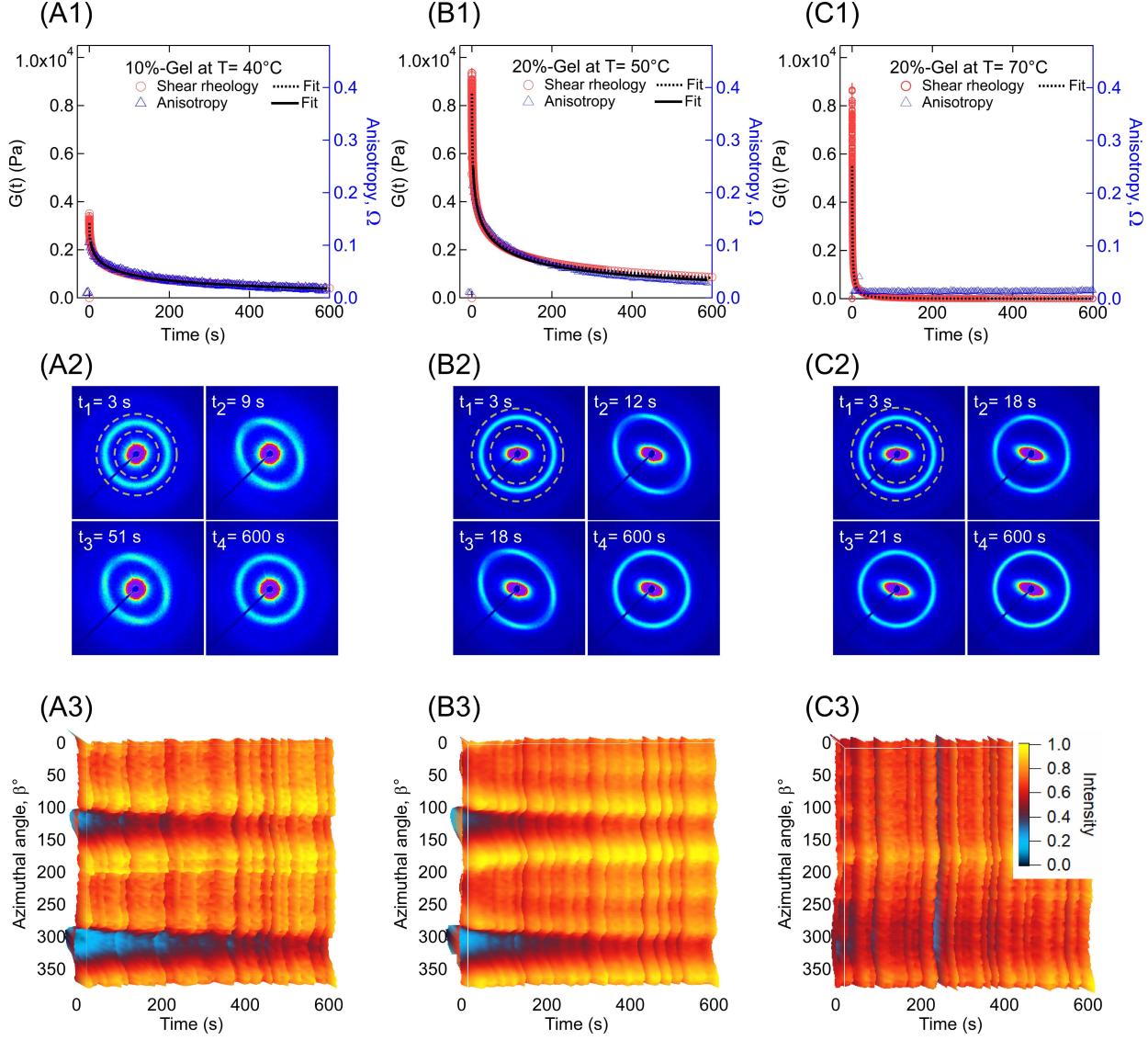


Figure 7: Stress-relaxation behavior obtained from shear-rheometry and RheoSAXS experiments. Data for the applied step strain of 0.3 for the (A) 10%-Gel at 40 °C, and 20%-Gel at (B) 50 °C and (C) 70 °C. (A1, B1, C1) Time-dependent modulus ($G(t)$), obtained from shear-rheometry experiments, and anisotropy factor (Ω) estimated from RheoSAXS experiments. Lines represent stretched exponential model fitted to $G(t)$ and Ω data. (A2, B2, C2) 2D-scattering patterns before the application of strain (t_1), after the application of strain (t_2), after $t = \tau_{SR}$ determined from stress-relaxation data (t_3), and at 600s (t_4). The q -range considered for the calculation of anisotropy factor is indicated by two dashed-circles in each t_1 -image. For model fitting, the time-scale was shifted appropriately. (A3, B3, C3) Azimuthal plots as a function of time for different β values are shown.

the 20%-Gel at 70 °C (Figure 7C2-C3), the relaxation process was very fast and the elliptical scattering pattern was captured for only one frame.

An azimuthal plot can be created by plotting average intensity over a specified q -range, i.e., $I(\beta)$, for β values from 0 to 359° at any particular time point. As defined above, β is measured from the flow/stretch direction (Figures 5A and 6A). The average intensity values are estimated by taking an average over the q -ranges of $\approx 0.015\text{--}0.018 \text{ \AA}^{-1}$ for 10%-Gel at 40°C , and $\approx 0.017\text{--}0.021 \text{ \AA}^{-1}$ for 20%-Gel at 50 and 70°C . Since the form factor peak position and intensity almost remain the same during the relaxation process, the q -ranges are chosen to capture the change in structure-factor peak position. Figure 7A3-C3 displays the time-lapsed azimuthal plots over 600 s. The azimuthal plot captures the peaks corresponding to the oriented elliptical pattern having uneven intensity distribution. These peaks start to fade with time, indicating a restoration of its isotropic microstructure. No significant change in azimuthal plots and 2D-scattering patterns are observed at 27°C (Figure S8) over 600 s indicating a slower microstructural relaxation process.

The degree of microstructure orientation can be quantified by estimating the anisotropic factor (Ω). The Ω values are displayed in the right axis of Figure 7A1-C1. A point in the 2D-scattering plot can be represented in the form of a unit vector, $\vec{u} = u_x i + u_y j$, where u_x and u_y represent the components of $I(\beta)$ parallel and perpendicular to the flow direction. The Ω can be mathematically expressed as:^{31,36,62,63}

$$\Omega = [(\langle u_x^2 \rangle - \langle u_y^2 \rangle)^2 + 4\langle u_x u_y \rangle^2]^{1/2} \quad (1)$$

where $\langle \dots \rangle$ represents $I(\beta)$ weighted average quantity as,

$$\langle u_x^2 \rangle = \frac{\int_0^{2\pi} I(\beta) \cos^2 \beta d\beta}{\int_0^{2\pi} I(\beta) d\beta}, \quad \langle u_y^2 \rangle = \frac{\int_0^{2\pi} I(\beta) \sin^2 \beta d\beta}{\int_0^{2\pi} I(\beta) d\beta}, \quad \text{and} \quad \langle u_x u_y \rangle = \frac{\int_0^{2\pi} I(\beta) \cos \beta \sin \beta d\beta}{\int_0^{2\pi} I(\beta) d\beta} \quad (2)$$

Before the application of strain, Ω is as low as ≈ 0.020 for all the cases. The Ω increases with the application of step strain as the oriented elliptical pattern emerges. At higher T , the increase of Ω is relatively higher (see Figure S8A-B). For example, for the 10%-Gel at 40°C , Ω jumps from ≈ 0.01 to 0.1. Such behavior is due to the higher mobility of chains at

elevated T facilitating the orientation development. As shown in Figure 7A1-C1, with time Ω decreases for all cases, a trend similar to $G(t)$. Due to the faster relaxation of 20%-Gel at 70 °C, the Ω value jumps from 0.041 to 0.010 rapidly.

Table 2: Parameters obtained by fitting the stretched exponential function to the stress-relaxation and anisotropy factor data for 10%- and 20%-Gels at different temperatures. Here T represents experimental temperature, α stretch parameter, G_0 zero-time shear modulus, τ_{SR} stress-relaxation time, Ω_0 anisotropy at $t \approx 0$, i.e., after the application of strain, and τ_Ω microstructure recovery time.

Sample	T (°C)	α	Shear-rheometry		RheoSAXS	
			G_0 (Pa)	τ_{SR} (s)	Ω_0	τ_Ω (s)
10%-Gel	27	0.30	3398±5	955.3±5.2	0.14	99928±5320
	40	0.30	3668±4	40.2±0.2	0.17	38.2±1
20%-Gel	27	0.26	9714±15	3432.5±26.1	0.27	2.23e6±1.33e5
	50	0.22	12454±17	6.1±0.1	0.61	4.6±0.2
	70	0.28	12780±23	0.18	—	—

The relaxation modulus, $G(t)$ can be reasonably captured by a stretched exponential function, mathematically represented as $G(t) = G_0 \exp(-(t/\tau_{SR})^\alpha)$.^{4,6,7,22,64} Here, G_0 is zero-time shear modulus, τ_{SR} is the characteristic relaxation time, and α represents the stretch in the relaxation time spectrum. Note that $\alpha \rightarrow 1$ represents the Maxwell-type fluid with a single relaxation time. Although two exponent models can be used,^{36,65} the stretch exponential function is widely used to capture the stress-relaxation behavior of self-assembled gels with a broad distribution of relaxation time originated from their inhomogeneous microstructure.^{4,6,7,22,64} Here, we fit this model to $G(t)$ over the time scale of 0.1 to 1800 s. G_0 , τ_{SR} , and α have been treated as floating parameters and the results are shown in Table 2. Note that fitting the data up to 600 s does not display a significant variation in the fitting parameters.

An increase in G_0 and τ_{SR} with polymer concentration can be attributed to the higher number of PI-blocks participating as the load-bearing chains.^{8,49} A decrease in τ_{SR} at higher T signifies increased chain mobility along with the increase in the solubility of PS-blocks in mineral oil.^{1,6} Both of these factors lead to a faster pullout of PS-blocks among the

aggregates. The α values of both gels vary from 0.2-0.3 indicating a distributed τ_{SR} due to the inhomogeneous microstructure of gels. For 20%-Gel, α is slightly lower than that of 10%-Gel suggesting a higher inhomogeneity of the microstructure.^{4,6,7,22}

Interestingly, the stress-relaxation and microstructure recovery follows a similar trend (Figure 7A1-C1), indicating the characteristic time scales associated with various steps during these processes follow a similar distribution. Note that, the microstructural recovery data have not been collected for a very long duration, i.e., until the microstructure recovers completely. So, the overall trend can be slightly different. However, such long-term data collection on a beamline could be difficult due to time-constraint and possible radiation damage of samples. Because of similar trend, the microstructure recovery time can also be represented in the form of stretched-exponential function as $\Omega(t) = \Omega_0 \exp(-(t/\tau_\Omega)^\alpha)$, where $\Omega(t)$ is the time-dependent anisotropic factor, Ω_0 signifies the anisotropy at $t \approx 0$, i.e., just after the application of strain, and τ_Ω represents the characteristic recovery time of the microstructure, which is referred here as the microstructural recovery time. As τ_{SR} and τ_Ω follow the same trend, we have fixed the α values to those obtained from the fitting of stress-relaxation data. The fitted model captures the data reasonably well (Figure 7A1-C1), and the fitted parameters are shown in Table 2.

For 10%-Gel at 40 °C and for 20%-Gel at 50 °C, τ_{SR} and τ_Ω are similar. For 70 °C, due to fast relaxation time, sufficient microstructure data could not be collected. It signifies that the microstructural relaxation time is less than the sampling time in RheoSAXS (3 s). At 27 °C, τ_Ω is approximately two orders of magnitude higher than the τ_{SR} , which warrants further discussion.

After the application of step-strain, several processes can take place in a sample, resulting in a multimode relaxation process. The applied strain facilitates the end-block (PS-block) pullout, and such a process results in stress relaxation. The relaxation of PI-blocks, particularly if those are entangled, also contributes to the stress-relaxation process.² It has been shown that for the same endblock length, the stress relaxation is slower for the gels with

longer and entangled midblock chains.^{2,7,8} The overall multimode relaxation process has the characteristic time scale of τ_{SR} . The pulled-out endblocks can further reassociate to an existing aggregate, or multiple of the endblocks associate to form new aggregates. Although not necessary for stress-relaxation, the reassociation of end blocks in addition to the chain pull-out is needed for complete recovery of microstructure, resulting in modulus and center-to-center distance of aggregates similar to that of the non-stretched samples. The reassociation step is also influenced by many processes such as endblock diffusion, the entropic penalty associated with midblock stretching/compression, and corona screening,^{26,68,69} therefore, the corresponding timescale is expected to be longer. The endblock diffusion process can be retarded by the crowded environment because of high chain density and entanglements of PI-blocks.

We can also compare our case with the healing of fractured acrylic gels, whereas, the reassociation of endblocks is necessary for healing.^{66,67} For those gels, the healing time has been reported to be 2-3 orders higher than the corresponding characteristic relaxation time, similar to the difference in τ_{SR} and τ_Ω presented here.^{66,67} Additional inferences can be drawn from time-temperature superposition data reported earlier for PS-PI-PS gels in mineral oil.⁶⁻⁸ Although not captured for 20%-Gel, the crossover frequency at 22 °C for 10%-Gel has been found to be $\approx 2 \times 10^{-5} \text{ s}^{-1}$, corresponds to a time-scale (τ_c) of $\approx 50,000 \text{ s}$. For 27 °C, τ_c is expected to be slightly lower, but τ_c is closer to τ_Ω in comparison to τ_{SR} . Most likely τ_c is more representative relaxation time that includes both chain pull-out and reassociation processes in contrast to τ_{SR} , which is dominated by the chain pullout process. But, further investigations will be necessary as in few cases we could not capture τ_c precisely.

We also need to compare the microstructural evolution in oscillation and stress-relaxation experiments. We have found that the scattering patterns for the intracycle strain value of ≈ 0.3 (see γ_2 in Figure 4C-D) and the step-strain value of 0.3 (see t_2 Figure S8A2 and B2) are slightly different, where step-strain leads to more anisotropic (elliptical) structure. This can be attributed to the rate of applied strain, which was rapid for the step-strain

case in comparison to a lower frequency of 1 rad/s in oscillatory shear experiments. In oscillatory shear experiments, with applied strain the scattering pattern changes from circular to split (a combination of elliptical and circular) and back to circular. The elliptical pattern indicates that a fraction of PI-chains follow the applied strain, without significant pull-out and reassociation events. However, the circular pattern at the maximum intracycle strain indicates that a fraction of the chains relax to their nonstretched condition. The origin of this is not completely understood as microstructural recovery through pullout and reassociation is unlikely. That is because the reassociation time-scale is significantly higher than strain-cycle time considered here. Further investigations will be necessary where the frequency of applied oscillation strain will be varied over a few decades, and the end- and mid-blocks will be tracked through contrast matching possible in SANS experiments.

Concluding Remarks

We have related the microstructure and rheometry results for 10 and 20 wt% of PS-PI-PS triblock copolymer gels in mineral oil during temperature-dependent gelation, subjected to large amplitude oscillatory strain, and during the stress-relaxation process. During gelation, loosely bounded aggregates are observed at higher temperatures than T_{gel} obtained from shear-rheometry. The microstructure evolved with decreasing temperature, and at room temperature, the microstructure evolution is complete. Correspondingly, G' reaches a plateau. With the application of strain, the gel microstructure orients in the stretching direction. This results in the transformation of the circular scattering pattern in the isotropic state to an oriented elliptical scattering pattern. However, in an oscillatory strain cycle with high strain amplitude, a split in scattering pattern has been observed with increasing intracycle strain, γ , displaying both ellipse and circle patterns. This has been attributed to the strain localization in the sample. A polydisperse core hard-sphere model can capture the scattering data both at the static and under loading conditions. The estimated results are

comparable to that estimated using affine deformation. In the stress-relaxation experiments, the microstructure relaxes faster at higher temperatures. The characteristic stress-relaxation time and microstructural recovery time, estimated using a stretched-exponential model, are similar at higher temperatures but deviate significantly at room temperature. This has been attributed to the complex multimode relaxation process including PI-block relaxation, PS-block pull-out and reassociation process. Further understanding of the stress relaxation and microstructure recovery behavior needs additional experimental investigations such as oscillation experiments using frequencies over multiple decades, dielectric measurement,⁷⁰ and SANS with appropriate contrast matching,²⁶ which can capture the A-block pullout and B-block relaxation process. Future experiments will also involve the investigation of microstructural relaxation process by varying the A- or B-block lengths.

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Associated Content

Supplementary Information

A table displaying gel nomenclature, polymer concentration, polymer volume fraction, and contents of PS and PI in the gels (wt%); Graph displaying $I(q) - q$ data for 10%-Gel; Schematic of polydispersed core hard-sphere model with characteristic parameters; Shear-

rheometry results from amplitude sweep and stress-relaxation experiments conducted using different geometries and protocols; 2D-scattering patterns for 10%- and 20%-Gel at 27 ° with applied strain of 0, 0.1, and -0.1; Proposed schematic of gel microstructure at static condition and after the application of a shear strain; Stress-relaxation results for 10%-Gel at 27 and 40 °C, and 20%-Gel at 27, 50, and 70 °C; $I(q) - q$ plot at t_2 at 50 °C; Stress-relaxation data at 27 °C, and corresponding azimuthal plots, and 2D-scattering patterns for 10%- and 20%-Gel.

Animated Videos

Movies capturing SAXS images as a function of applied strain at 27°C for 10%- and 20%-Gel.

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Supplementary Information[†]:

Capturing the Transient Microstructure of a Physically Assembled Gel Subjected to Temperature and Large Deformation

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Table S1: Gel nomenclature, polymer concentration in wt%, polymer volume fraction (ϕ), and PS and PI content in the gels (wt%).

Sample	wt%	ϕ (v/v)	PS (wt%)	PI (wt%)
10%-Gel	10	0.089	2.9	7.1
20%-Gel	20	0.181	5.8	14.2

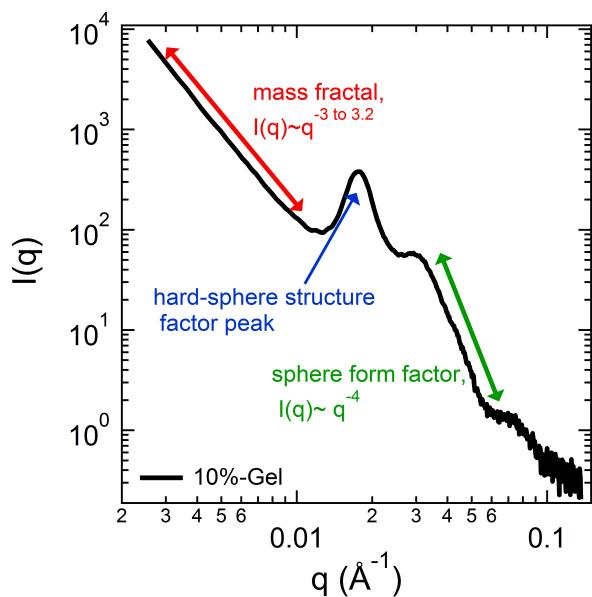


Figure S1: $I(q) - q$ data for 10%-Gel indicating the mass fractal at low q , peaks arising from structure factor at intermediate q , and the slope of -4 at higher q capturing sphere form factor.

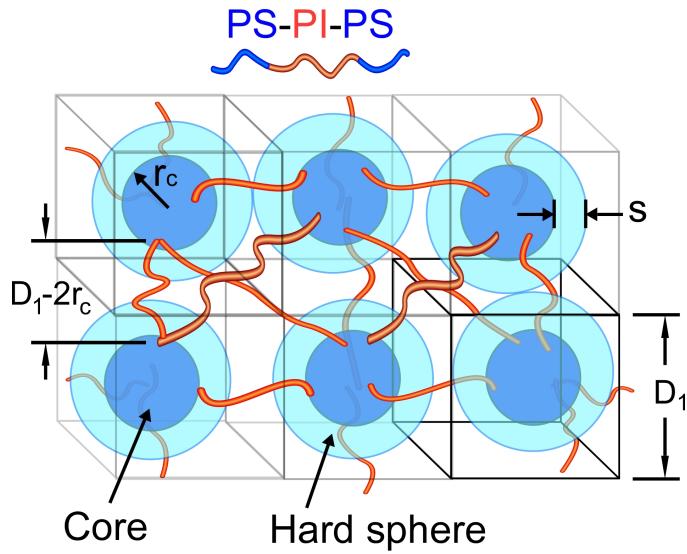


Figure S2: Schematic representing gel structure. 3D crosslinked network formed by poly(styrene)-poly(isoprene)-poly(styrene) [PS-PI-PS] triblock copolymer in mineral oil, where the PS-blocks form aggregates bridged by PI-blocks. The PS-aggregates of core radius r_c are surrounded by a fictitious hard sphere of thickness s contained in a cube with dimension of D_1 . Note that the hard-spheres does not necessarily touch each other.

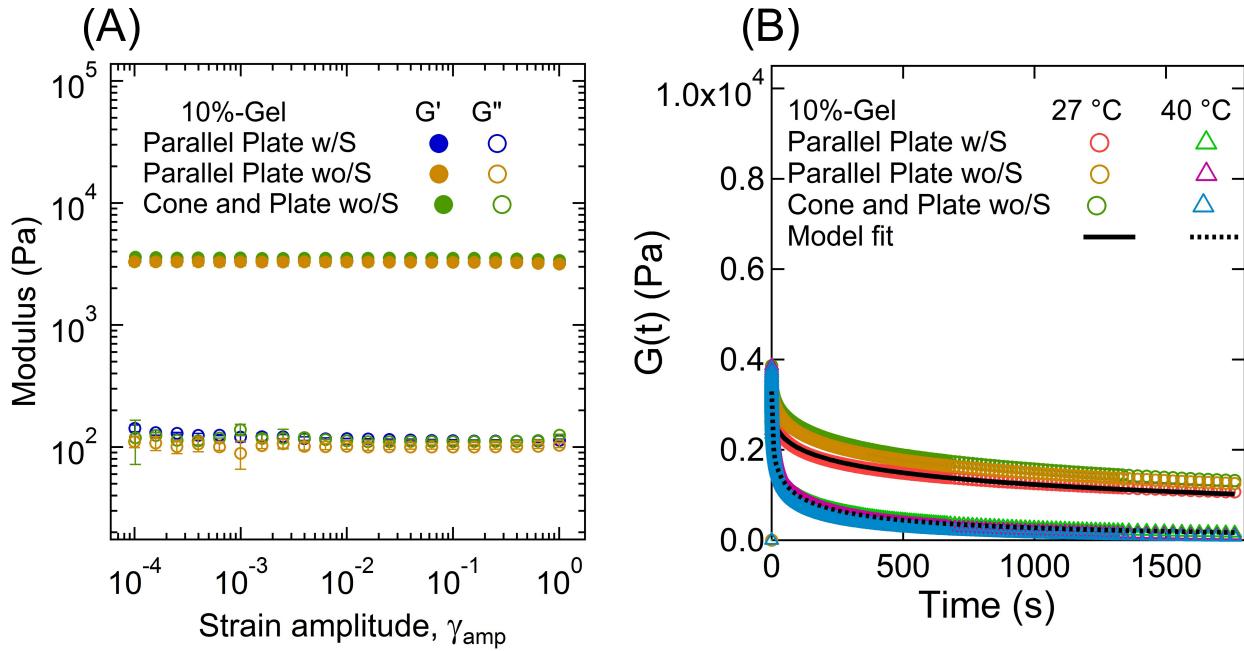


Figure S3: Shear-rheometry results for 10%-Gel performed using different geometries, viz., parallel plate with 240 grit sand paper (parallel plate w/S), parallel plate without sand paper (parallel plate wo/S), and cone and plate without sand paper (cone and plate wo/S). (A) Storage (G') and loss moduli (G'') as a function of strain amplitude (γ_{amp}) using oscillatory frequency (ω) of 1 rad/s. (B) Stress relaxation experiments performed at 27°C and 40°C using γ_{step} of 0.3.

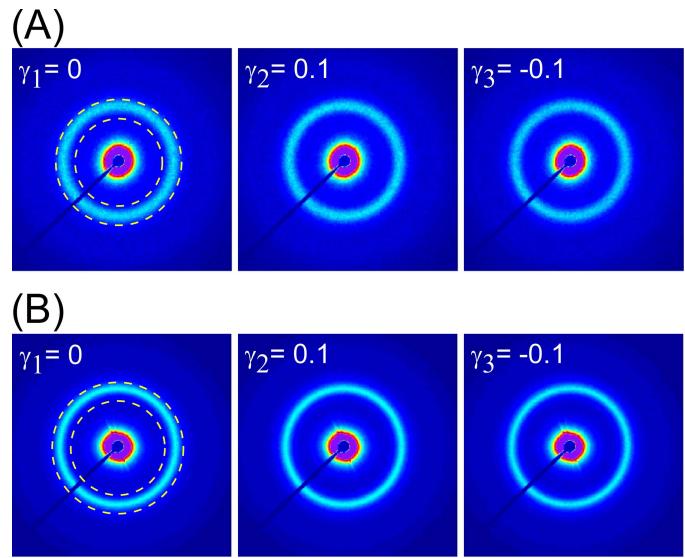


Figure S4: 2D-scattering patterns for gels at 27 °C during a strain cycle with γ_{amp} of 0.1. 2D-scattering patterns are shown for γ (intracycle strain) equal to 0, 0.1, and -0.1 for the (A) 10%-Gel and (B) 20%-Gel. The dashed lines in the γ_1 images indicate the analyzed q -range.

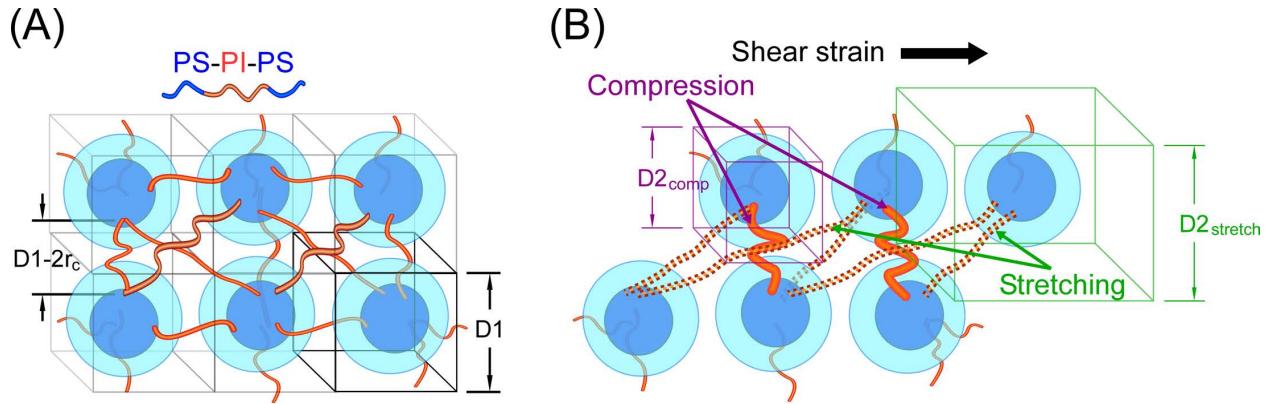


Figure S5: Gel structure at the static condition and after the application of a shear strain. (A) Gel structure formed by PS-aggregates surrounded by a fictitious hard sphere contained in a cube with dimension D_1 at the static condition. (B) The change of structure after a shear strain is applied, displaying compressed, and stretched chains. The corresponding cube has dimension of D_2

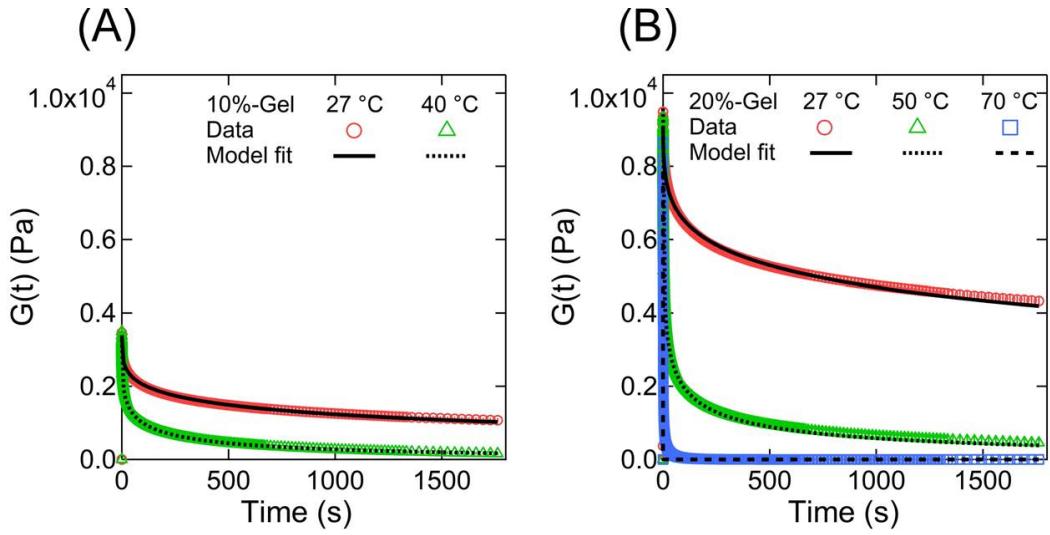


Figure S6: Stress relaxation for 10%- and 20%-Gels over 1800 s at different temperatures obtained from shear rheometry experiments. Time-dependent modulus ($G(t)$) over time with an applied step strain (γ_{step}) of 0.3, and fitted with a stretched exponential function for the (A) 10%-Gel at 27 and 40 °C, and the (B) 20%-Gel at 27, 50, and 70 °C.

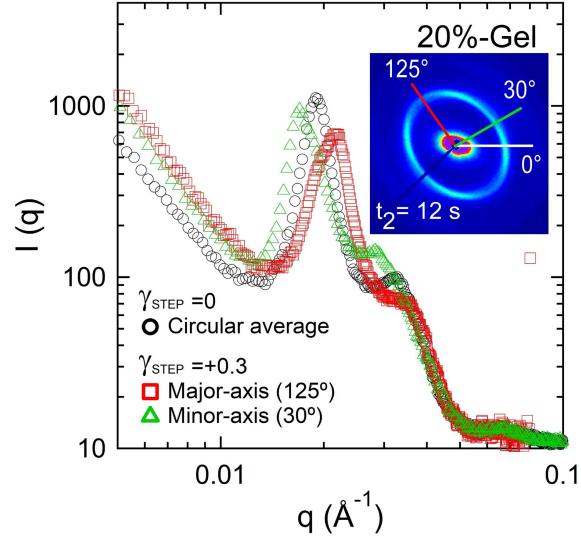


Figure S7: $I(q) - q$ data corresponding to t_2 obtained from RheoSAXS experiments for 20% Gel at 50 °C. A step strain $\gamma_{step}=0.3$ was applied and the gel was allowed to relax. Here, the sector averages along major- and minor-axis ($\beta=125^\circ$ and 30°) are compared with the circular average data at the static condition ($\gamma_{step}=0$). The inset represents the oriented 2D-scattering pattern along with the azimuthal angles (β) corresponding to the major- and minor-axes.

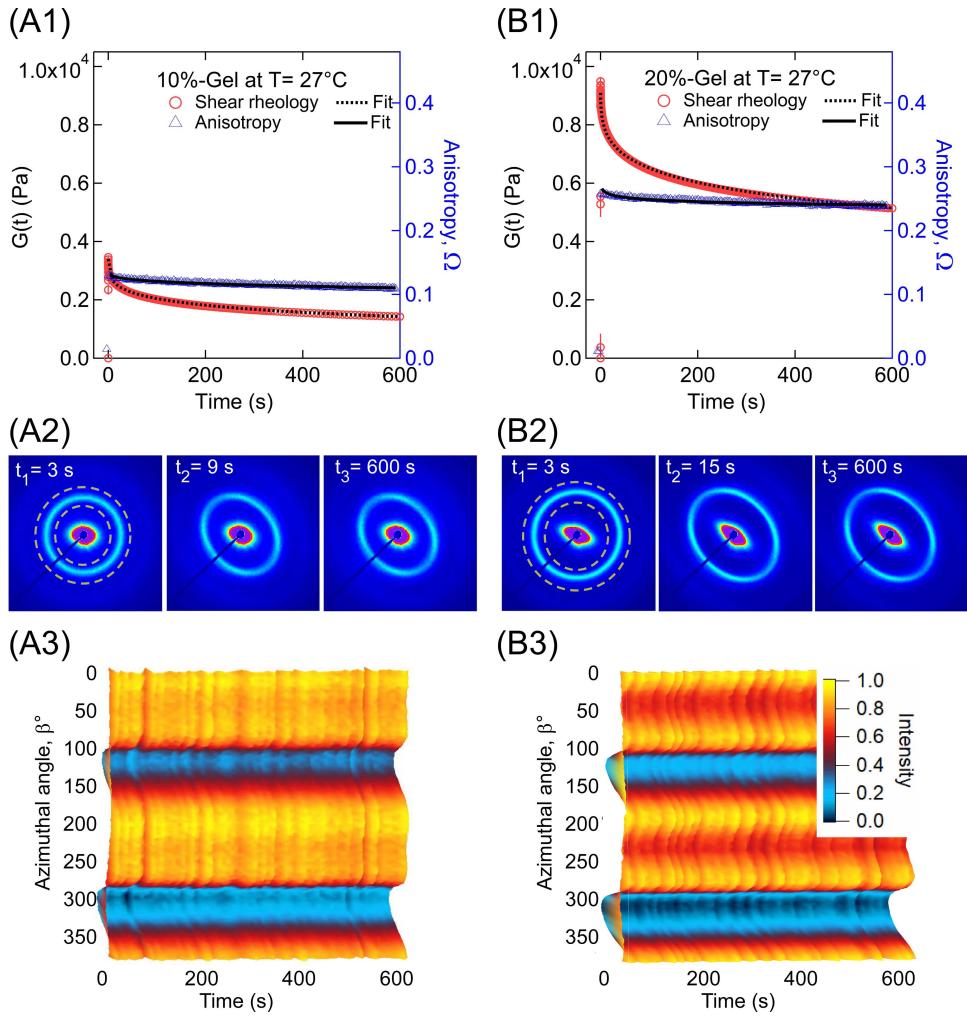


Figure S8: Results for the stress relaxation experiments at 27 °C, azimuthal plots, and 2D-scattering patterns for gels. Time-dependent modulus ($G(t)$) fitted with stretched exponential function, 2D-scattering patterns at different time points, and stacked azimuthal plots over time are shown for the (A) 10%-Gel and (B) 20%-Gel. Here, t_2 is just after the strain is applied. The dashed lines in the t_1 -images indicate the analyzed q -range for each case.

Model description

Model fit for the gels at static conditions: We have characterized the gel microstructure using a polydispersed core hard-sphere model for the gels at static conditions. According to this model, the PS-aggregates can be viewed as cores having a Gaussian distribution in radius. The cores have a mean radius r_c with polydispersity σ/r_c . The cores are surrounded by fictitious hard spheres, concentric to the cores, with thickness s_1 estimating the radius of hard spheres as $r_c + s_1$. The hard spheres occupy a volume fraction ϕ_1 in the gel. The model is a combination of a spherical form factor ($P(q)$) multiplied with hard-sphere structure factor ($S(q)$), mathematically represented as $I(q) \propto P(q) \times S_1(q)$. The inter-aggregate distance, approximately representing the end-to-end distance of a PI-block in the gel can also be calculated as $D_1 = (4\pi R^3/(3\psi_1))^{1/3}$,¹ where $R = r_c + s_1$ is the radius of the hard-sphere. The above model is also used for the cases in which the gel is under deformation but the 2D scattering pattern does not display a split.

Model fit for the gels at stretched conditions: For the gels at $\gamma = \pm 1$, a modified polydispersed core hard-sphere model was used for the fitting. The model is justified as follows. At these γ values, we observed a circular pattern and an elliptical pattern. The circular pattern resembling the scattering pattern at the static condition. The oriented microstructure displays an elliptical pattern. The $I(q) - q$ curve displays two length scales viz. (1) along the minor-axis, displaying the increase in the inter-aggregate distance as a result of applied γ , and (2) along the major-axis, signifying a decrease in the inter-aggregate distance or compression as a consequence of stretching in the orthogonal direction (minor-axis). The state of the hard spheres in case-1 and -2 can be referred to as stretched and compressed, respectively, when compared with those at static conditions. Therefore, at a particular γ , three inter-aggregate distances can be envisaged - unperturbed, increased, and decreased. Along with the minor-axis sector, the $I(q) - q$ data signifies two arrangements of hard spheres- unperturbed and stretched. Similarly, along the major-axis, the data represents unperturbed and compressed hard spheres. Note that our data indicates an intact form factor

peak, meaning that the aggregates do not change the size and shape during deformation. Since the value of the hard-sphere radius (R) signifies the inter-aggregate distance, the changed inter-aggregate distance can be conveniently represented by adding a hard-sphere in the model while keeping the form factor the same. We represent the modified polydispersed hard-sphere model as $I(q) \propto P(q) \times (S_1(q) + S_2(q))$, where $S_2(q)$ is the structure factor related to the new hard-sphere to capture the characteristics of displaced hard spheres.

Mathematical expression: Here, the structure factor is calculated based on Percus-Yevick closure as

$$S(q) = \frac{1}{1 + 25\psi G(A)/A} \quad (\text{S1})$$

where $A = 4\pi qR$, R is the radius of hard sphere, and ψ is the hard-sphere volume fraction.

$$G(A) = \alpha (\sin A - A \cos A) + \beta/A^3 (2A \sin A + (2 - A^2) \cos A - 2) + \gamma (-A^4 \cos A + 4((3A^2 - 6) \cos A + (A^3 - 6A) \sin A + 6)) / A^5 \quad (\text{S2})$$

and

$$\alpha = \frac{(1 + 2\psi)^2}{(1 - \psi)^4} \quad (\text{S3})$$

$$\beta = -6\psi \left(1 + \frac{\psi}{2}\right)^2 / (1 - \psi)^2 \quad (\text{S4})$$

$$\gamma = \frac{\psi\alpha}{2} \quad (\text{S5})$$

Form factor of sphere can be mathematically expressed as:

$$P_1(q, r) = \left(\frac{4\pi r_c^3}{3}\right)^2 \left(\left(\frac{3}{qr_c}\right)^3 (\sin(qr_c) - qr_c \cos(qr_c))\right)^2 \quad (\text{S6})$$

The polydispersity is σ/r_c , where σ is the variance of distribution in aggregate radius

r_c . And the average form factor is:

$$\langle P(q, r_c, \sigma) \rangle = \int_0^\infty \frac{1}{\sigma(2\pi)^{1/2}} \exp\left(-\frac{(r - r_c)^2}{2\sigma^2}\right) F(q, r) dr \quad (\text{S7})$$

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