

1 **Dynamics of hydrogels with a variable ratio of permanent**
2 **and transient crosslinks: constitutive model and its**
3 **molecular interpretation**

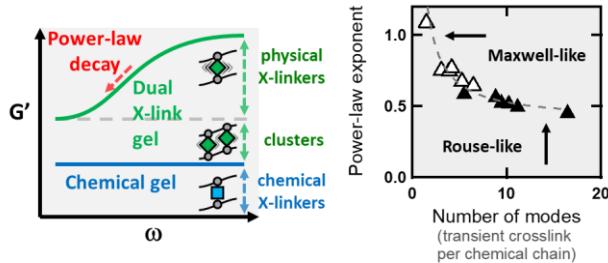
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Abstract

2 Mechanical reinforcement of hydrogels is important to gel science. “Dual crosslink” hydrogels
3 with chemical and transient crosslinks can exhibit improved mechanical properties compared
4 to the corresponding chemically crosslinked gels. Here we use model dual poly(vinyl alcohol)
5 crosslink gels with a variable ratio of chemical and transient crosslinks to study how this ratio
6 affects chain dynamics. Torsion and tensile test results are well described by a constitutive
7 model with only four parameters. The characteristic time of network relaxation (corresponding
8 to the peak of the loss modulus) increases with decreasing transient crosslinker concentration.
9 The characteristic time distribution gradually changes from Maxwell-like to Rouse-like
10 relaxation. These results imply that the Rouse mode of the chains between crosslinks controls
11 transient network dynamics. Our work provides a molecular interpretation of network dynamics
12 and guide optimization of the crosslinking ratios in dual crosslink gels.

13

1. Introduction

2 To overcome the brittleness of conventional chemical hydrogels for applications requiring
3 mechanical toughness, various strategies of mechanical reinforcement have been reported since
4 2001.¹⁻⁴ Among them, the concept of sacrificial bonds to dissipate strain energy and prevent
5 stress concentration to the crack tip was found promising. After the pioneering works of Gong
6 and her coworkers on “double network” hydrogels using irreversible covalent bond breaking in
7 the interpenetrated networks,^{3,5} use of reversible breaking of noncovalent bonds which can
8 break and reform has become popular and various examples of such dissipative hydrogels
9 having different noncovalent interactions as reversible crosslinks have been reported in the last
10 decades.⁶⁻¹⁰ Reversible dissociation/reassociation of the crosslinks can provide self-recovering
11 properties to the networks, attracting the attention of material scientists.¹¹⁻¹³

12 Though their specific time-dependent mechanical properties are of interest from a rheological
13 point of view, quantitative studies have been less reported. The two main parameters
14 investigated in our study are the concentration of elastically active crosslinks, which determines
15 the modulus, and the lifetime of the transient crosslinks, which controls the network relaxation
16 time. While it is feasible to tailor transient crosslinks at the molecular scale by choosing their
17 concentration and their lifetime by picking various types of interactions, it is more difficult to
18 quantitatively correlate molecular parameters to macromolecular properties such as the
19 distribution of chain relaxation times. In addition, it is a challenge to design and synthesize a
20 simple model dissipative gel system and to develop constitutive models able to quantitatively
21 describe the mechanical behaviors under small and large deformations with different loading
22 histories by taking into account the transient bond dynamics, with as few parameters as possible.
23 Narita, Creton and their coworkers have developed a simple model dynamic hydrogel based on
24 poly(vinyl alcohol), PVA, having simultaneously chemical and physical crosslinks.¹⁴⁻¹⁷

1 Starting from a PVA chemical gel crosslinked by glutaraldehyde, a “dual crosslink” PVA
2 hydrogel is prepared by immersing the chemical gel into a solution of borax to incorporate
3 borate ions acting as physical crosslinkers. When the stretch rate is sufficiently small compared
4 to the characteristic relaxation time of the transient crosslinks, it was demonstrated that
5 incorporation of the transient crosslinks to the chemical network improves the fracture
6 resistance of the gel compared to the corresponding chemical gel. The dynamics of the PVA
7 dual crosslink gel has a well-defined main relaxation time determined from the peak of the loss
8 modulus, stemming from the physical bond dissociation. Using the PVA dual crosslink
9 hydrogel, some rheological features such as additivity of the physical crosslinks and chemical
10 crosslinks (equivalent to the corresponding chemical gel) in terms of the moduli, as well as
11 separability of the strain rate-dependent stress into a time-dependent term and a strain-
12 dependent term (expressed as a neo-Hookean model), have been experimentally demonstrated
13 (for certain loading histories).^{14,15}

14 Hui and Long proposed a 3D finite strain constitutive model for the PVA dual crosslink gel.¹⁸⁻
15 ²⁰ A simplified description of the dynamics of the transient physical crosslinks with breaking
16 and healing times, taking into account the steady-state behavior of the transient physical
17 crosslinks, can fit both uniaxial tensile tests and torsion tests in shear rheometry. Using only
18 four physically grounded parameters, the model can fit and predict very well various
19 loading/unloading behaviors at different stretch rates. The model was successfully used to
20 model the propagation of a crack in the PVA dual crosslink gel.^{17,21}

21 In these previous works, the mechanical properties of the PVA dual crosslink gel were
22 intensively studied at one preparation condition at a fixed chemical and physical crosslinkers
23 concentrations, optimized for high toughness. The constitutive model has been applied to the
24 same optimized gel. It is however interesting to investigate the effects of the two main
25 parameters controlling transient crosslinks, their concentration and the relaxation time. The

1 effect of the relaxation time was investigated as a function of the temperature for the optimized
2 gel.²² The validity of the model and the applicability of time-temperature superposition were
3 confirmed. Here we report the influence of the relative ratio of chemical and physical crosslinks
4 on the rheological properties. We investigate a series of PVA dual crosslink gels with different
5 ratios of permanent and transient crosslinks. All gels are characterized by uniaxial tensile tests
6 and torsion tests and the validity of the constitutive model is tested by fitting both tensile and
7 torsion results with the same set of two parameters for the moduli and another two for the
8 characteristic time. More importantly, analyzing the crosslinker concentration dependence of
9 the parameters also helps us to understand their physical significance. A goal of this paper is
10 to provide molecular interpretations of the model parameters.

1 2. Experimental Section

2 2.1. Sample preparation

3 PVA dual crosslink gel samples at different chemical and physical crosslinking ratios were
4 prepared by using the procedure described previously.^{15,16} Briefly, PVA chemical gels were
5 first prepared by cross-linking PVA (molecular weight: 89,000–98,000, degree of
6 hydrolyzation: 99 %) in aqueous solutions with the chemical crosslinker glutaraldehyde, GA,
7 at pH =1.9. The PVA concentration was kept constant at 12 wt% for all the gels tested. We
8 used two GA concentrations in the feed, 5.5 and 16.5 mM, corresponding to crosslinking ratio
9 in the feed, $C_{GA} = 0.2$ and 0.6 mol% (molar ratio to the monomer units of PVA). After the
10 overnight crosslinking reaction, the obtained PVA chemical gels were used for measurements
11 as prepared. PVA dual crosslink gels were then prepared by incorporating borate ions, physical
12 crosslinkers, to the chemical gels. In this process the chemical gels were washed with a large
13 amount of water to a neutral pH. The swollen chemical gels were then immersed in aqueous
14 solutions of sodium tetraborate decahydrate (borax) for 3 days. The borax concentration in the
15 solution, C_{borax} , varied from 1 to 50 mM. The volume of the borax solution was 20 times that
16 of the chemical gels. By dissolution of tetraborate, borate ions are formed, which are able to
17 form complexes with diols on the PVA chains. To quantitatively study the effects of the
18 physical crosslinking ratio, it is crucial to compare gels with different crosslinking ratios at the
19 same PVA concentration. It should be noted that the complexation of borate ions induces both
20 deswelling (due to crosslinking) and swelling (due to the introduction of charges to the neutral
21 gel). The swelling ratio was controlled by addition of NaCl to the system: the electrostatic
22 interactions are screened and the gels deswell to the same PVA concentration as that of the
23 corresponding chemical gel. For each GA and borax concentration, the optimal NaCl
24 concentration was determined and varied from 90 to 460 mM.¹⁶

1 **2.2. Mechanical tests**

2 *2.2.1. Tensile tests*

3 Stress relaxation in uniaxial tensile tests was performed on an Instron 5565 tensile tester with a
4 10 N load cell. Samples of dual crosslink gels as well as chemical gels in a rectangular shape
5 with 5 mm width, 1.5 mm thickness, and 20 mm gauge length (length between clamps) were
6 stretched to $\lambda_0 = 1.1$ at a constant stretch rate of 0.1 s^{-1} , then stress relaxation was recorded. We
7 kept the samples in paraffin oil during all the tests to prevent them from drying.

8 *2.2.2. Torsion tests*

9 To characterize the linear viscoelastic properties of the dual crosslink gels and the chemical
10 gels, small strain oscillatory shear measurements were performed on a parallel plate geometry
11 having roughened surfaces (25 mm in diameter) with an ARES LS1 rheometer (TA
12 instruments). The sample thickness was 1.5 mm. Frequency sweep tests with a dynamic range
13 varying from 0.1 to 100 rad/s were carried out at 25°C within the linear viscoelasticity regime
14 (0.8 – 1 % strain).

15

1 **3. Continuum theory**

2 **3.1. Model description**

3 Here we briefly describe the latest version of the rate-dependent finite three-dimensional
4 continuum theory validated in the Gaussian chain regime for stretch lower than about 2, with a
5 PVA dual crosslink gel having a chemical crosslinking ratio of 0.2 mol% prepared with C_{borax}
6 of 1 mM.^{20,22} This model was developed with the following key assumptions. (1) The chemical
7 crosslinks are assumed to be unbreakable (fracture is not considered) while the physical
8 crosslinks are assumed to undergo a time-dependent breaking and reforming (healing) process.
9 The dual crosslink gel network consists of permanent chains attached to chemical crosslinks
10 and transient chains attached to physical crosslinks. The strain energy of the network is thus
11 the sum of that of the permanent and transient chains. (2) The physical bonds' breaking and
12 reforming process reaches a dynamic equilibrium soon after the gel is synthesized. In other
13 word, there is a thermodynamic equilibrium between "closed" transient crosslinks (elastically
14 active) and "open" crosslinks. Thus, the molar fraction of breaking crosslinks and healed
15 crosslinks per unit time are equal and independent of time (steady state assumption). This
16 breaking (healing) rate is denoted by $\bar{\gamma}_\infty$ (s^{-1}). (3) The stress sustained by a transient chain is
17 instantaneously relaxed when it breaks; after a temporary chain is reattached, it is in the relaxed
18 state immediately and carries no strain energy. The reattached temporary chain experiences the
19 deformation history from its birth at time τ (s) to the current time t (s). (4) Macroscopically the
20 gel is incompressible and isotropic. For both permanent and transient chains, the Neo-Hookean
21 model (Gaussian chains) is used to specify the strain energy of a chain under deformation. (5)
22 We assume that the rates of chain breaking and healing are independent of the imposed strain
23 history as observed by experiments.¹⁵

1 Assuming that before loading ($t < 0$), the physical crosslinks have reached a state of dynamic
 2 equilibrium in which the healing rate is equal to the breaking rate, i.e., $\bar{\gamma}_\infty$, the nominal stress σ
 3 (Pa) in a uniaxial tension test with stretch ratio $\lambda(t)$ is:

$$\sigma = \mu\rho \left(\lambda(t) - \frac{1}{\lambda^2(t)} \right) + \mu n(t) \left(\lambda(t) - \frac{1}{\lambda^2(t)} \right) + \mu \bar{\gamma}_\infty \int_0^t \phi_B \left(\frac{t-\tau}{t_B} \right) \left(\frac{\lambda(t)}{\lambda^2(\tau)} - \frac{\lambda(\tau)}{\lambda^2(t)} \right) d\tau. \quad (\text{eq.1})$$

4 Equation (1) means that the stress is the sum of three terms: (i) the stress carried by the
 5 permanent network (the first term of the right side), (ii) the stress carried by the transient chains
 6 existing from $t = 0$ (the second term) and survives to the current time, (iii) and the stress carried
 7 by healed transient chains (the third term with the integral).

8 The use of neo-Hookean model means that the stress in the permanent network is
 9 $\mu\rho \left(\lambda(t) - \frac{1}{\lambda^2(t)} \right)$, where μ (Pa) is the small stain shear modulus, ρ is the molar fraction of the
 10 permanent chains relative to the total number of chains. Since both the transient and permanent
 11 networks obey Gaussian chain statistics (i.e., neo-Hookean model) the stress carried by the
 12 transient chains has the same dependence on the stretch ratio except in this case ρ is replaced
 13 by the molar fraction of the transient crosslinks, which are attached at $t = 0$ and survive to the
 14 current time $t > 0$, $n(t)$. $n(t)$ is^{19,20}

$$n(t) = \bar{\gamma}_\infty \int_{-\infty}^0 \phi_B \left(\frac{t-\tau}{t_B} \right) d\tau = \bar{\gamma}_\infty \frac{t_B}{2 - \alpha_B} \left[1 + (\alpha_B - 1) \frac{t}{t_B} \right]^{\frac{2-\alpha_B}{1-\alpha_B}}, \quad (\text{eq.2})$$

15 where $\bar{\gamma}_\infty$ (s^{-1}) and ϕ_B are given by

$$\bar{\gamma}_\infty = \frac{1 - \rho}{t_H + \frac{t_B}{2 - \alpha_B}}, \quad (\text{eq.3})$$

$$\phi_B\left(\frac{t-\tau}{t_B}\right) = \left[1 + (\alpha_B - 1)\frac{t-\tau}{t_B}\right]^{\frac{1}{1-\alpha_B}}. \quad (\text{eq.4})$$

1 $\bar{\gamma}_\infty$ (s^{-1}) is a function of the characteristic transient bond breaking time t_B (s) and the
 2 characteristic transient bond healing time t_H (s). Its physical signification can be better
 3 explained by shear modulus expression shown later in this section. $\phi_B(t - \tau)$ is called the
 4 survivability function which denotes the fraction of chains that are born at τ and survive till the
 5 current time $t > \tau$. Eg.4 can be obtained by solving a simple breaking model, $d\phi_B/dt =$
 6 $-\phi_B^{\alpha_B}/t_B$, where $1 < \alpha_B < 2$ is a dimensionless material constant that specifies the average
 7 survival time of a physical bond, to statistically describe the spectrum of the relaxation time
 8 related to the transient physical bond breaking. This second term represent the stress relaxation
 9 due to the breaking of the physical bonds attached at $t = 0$.

10 The third term expresses the recovery of stress by healing of the broken bonds. We assume that
 11 the transient chain healed at $t = \tau$ does not carry stress, starts to obey the same survivability
 12 function ϕ_B , and has a different reference configuration from the original chain. This results in
 13 a different stretch dependent term $\lambda(t) \cdot \lambda^{-2}(\tau) - \lambda(\tau) \cdot \lambda^{-2}(t)$.

14 The theory also predicts the dynamic shear modulus in linear viscoelastic regime with the same
 15 set of parameters.^{19,22} The complex modulus $G^*(\omega)$ is written as:

$$G^*(\omega) = \mu \left\{ \rho + \bar{\gamma}_\infty \frac{t_B}{2 - \alpha_B} \left[1 - \frac{2 - \alpha_B}{\alpha_B - 1} \cdot I(\omega) \right] \right\} \quad (\text{eq.5})$$

16 with

$$I(\omega) = \int_0^\infty \exp\left(-i \frac{\omega t_B}{\alpha_B - 1} u\right) (1 + u)^{-\frac{1}{\alpha_B - 1}} \cdot du \quad (\text{eq.6})$$

17 The integral $I(\omega)$ which is a function of the angular frequency ω , is numerically evaluated. And
 18 the expressions for $G'(\omega)$ and $G''(\omega)$ are given as:

$$G'(\omega) = Re[G^*(\omega)]$$

$$= \mu\rho + \mu\bar{\gamma}_\infty \frac{t_B}{2 - \alpha_B} \left[1 - \frac{2 - \alpha_B}{\alpha_B - 1} \int_0^\infty \cos\left(\frac{\omega t_B}{\alpha_B - 1} u\right) (1 + u)^{\frac{-1}{\alpha_B - 1}} du \right] \quad (\text{eq.7})$$

$$G''(\omega) = Im[G^*(\omega)]$$

$$= \mu\bar{\gamma}_\infty \frac{t_B}{2 - \alpha_B} \left[\frac{2 - \alpha_B}{\alpha_B - 1} \int_0^\infty \sin\left(\frac{\omega t_B}{\alpha_B - 1} u\right) (1 + u)^{\frac{-1}{\alpha_B - 1}} du \right] \quad (\text{eq.8})$$

1 From **eq.7** the low frequency limit is:

$$\begin{aligned} G'(\omega \rightarrow 0) \\ = G_0 = \mu\rho + \left[\frac{\mu(1 - \rho)t_B}{(2 - \alpha_B)t_H + t_B} \Gamma\left(\frac{2\alpha_B - 3}{\alpha_B - 1}\right) \cos\left(\frac{2 - \alpha_B}{2(\alpha_B - 1)}\pi\right) \right] \left(\frac{t_B\omega}{\alpha_B - 1}\right)^{\frac{2 - \alpha_B}{\alpha_B - 1}} \\ \sim \mu\rho \end{aligned} \quad (\text{eq.9})$$

2 In the low frequency limit, the transient chains fully relax, and the modulus corresponds to that of the permanent chains.
4 In the high frequency limit, we have:

$$\begin{aligned} G'(\omega \rightarrow \infty) \\ = \mu\rho + \frac{\mu(1 - \rho)t_B}{(2 - \alpha_B)t_H + t_B} \left[1 - \frac{2 - \alpha_B}{bt_B^2} \frac{1}{\omega^2} \right] \\ = \mu\rho + \mu(1 - \rho) \frac{\frac{t_B}{2 - \alpha_B}}{t_H + \frac{t_B}{2 - \alpha_B}} \\ = \mu\rho + \mu\bar{\gamma}_\infty \frac{t_B}{2 - \alpha_B} \end{aligned} \quad (\text{eq.10})$$

5 In the high frequency limit, both permanent crosslinks and closed transient crosslinks additively contribute to the elasticity, thus the modulus corresponding to the closed transient crosslinks is written as $G'_{\text{closed}} = \mu\bar{\gamma}_\infty \frac{t_B}{2 - \alpha_B}$. The fraction of closed transient crosslinks to the total

1 crosslinks is written as $\rho_{closed} = \bar{\gamma}_\infty \frac{t_B}{2-\alpha_B}$, since $G'_{closed} = \mu \rho_{closed}$. It should be noted that

2 the fraction of the (total) transient crosslinks is $1 - \rho$, which is equal to $\bar{\gamma}_\infty \left(t_H + \frac{t_B}{2-\alpha_B} \right) =$

3 $\bar{\gamma}_\infty t_H + \rho_{closed}$ by **eq.3**. Thus, the fraction of the open transient crosslinks, ρ_{open} , is $\rho_{open} =$

4 $\bar{\gamma}_\infty t_H$.

5 **Eq.8** shows that $G''(\omega)$ is concave downward, thus the value of time, $\tau_X = 1/\omega_X$ corresponding

6 to the maximum, which traditionally used in the interpretation of linear rheological experiments

7 to define the relaxation time, is a reasonable characteristic time of the dissipation of the system.

8 Its value can be analytically calculated as a function of the model parameters (the derivation is

9 given in Supporting Information):

$$\tau_X = \frac{t_B}{(\alpha_B - 1) \cdot f \left(\frac{2 - \alpha_B}{\alpha_B - 1} \right)} \quad (\text{eq.11})$$

10 where f is a dimensionless function of $\frac{2 - \alpha_B}{\alpha_B - 1}$. Therefore, τ_X is proportional to t_B , with a

11 coefficient which is a function of only α_B . For $0.1 \leq \frac{2 - \alpha_B}{\alpha_B - 1} \leq 0.9$, $f \left(\frac{2 - \alpha_B}{\alpha_B - 1} \right)$ can be well

12 approximated by a linear function, $f \left(\frac{2 - \alpha_B}{\alpha_B - 1} \right) = -0.053 + 0.802 \frac{2 - \alpha_B}{\alpha_B - 1}$.

13 The five material parameters, μ (Pa), ρ , t_B (s), t_H (s) and α_B , can be reduced to the following

14 four parameters, which have plausible rheological significance: $\mu\rho$ (Pa), $\mu\bar{\gamma}_\infty$ (Pa s⁻¹), t_B (s) and

15 α_B . $\mu\rho$ and $\mu\bar{\gamma}_\infty$ represent the modulus (in the form of $\mu\bar{\gamma}_\infty \frac{t_B}{2-\alpha_B}$) for the chemical and the

16 transient networks respectively, and their crosslinker concentration dependence will be

17 discussed in section 4.2. t_B and α_B control the characteristic relaxation time of the network.

18 Their dependences on the crosslinker concentrations and physical interpretation are discussed

19 in section 4.3.

20 **3.2. Parameter determination by fitting**

1 The experiments reported in this work are performed in the linear regime where the strains are
 2 small. This is the regime of focus in this paper. The four parameters were determined by fitting
 3 the experimental data of both the tensile and torsion tests using the equations governing each
 4 test. A set of parameters fitting both tests was found. Determination of the parameters was
 5 done by fitting the data of a tensile stress relaxation test, and the parameters were fine-tuned to
 6 match the rheology data. Details of the fitting procedure can be found in the reference.²⁰ Briefly,
 7 from a single tensile stress relaxation test, consisting of a rapid stretching to $\lambda = \lambda_0$ and
 8 relaxation, $\mu\rho$ and α_B were determined from the relaxation part. Since the healed transient
 9 chains do not carry stress during relaxation, **eq.1** is simplified to:

$$\sigma(t) = \mu\rho(\lambda_0 - \lambda_0^{-2}) + \mu n(t)(\lambda_0 - \lambda_0^{-2}) \quad (\text{eq.12})$$

$$= \sigma_\infty + (\lambda_0 - \lambda_0^{-2}) \cdot \mu\bar{\gamma}_\infty \frac{t_B}{2 - \alpha_B} \left[1 + (\alpha_B - 1) \frac{t}{t_B} \right]^{-\frac{2 - \alpha_B}{\alpha_B - 1}}$$

10 where σ_∞ is the stress at long times, from which the value of $\mu\rho$ is determined as $\mu\rho =$
 11 $\sigma_\infty/(\lambda_0 - \lambda_0^{-2})$. For $t \gg t_B$, one finds from **eq.12** $\sigma(t) - \sigma_\infty \sim t^{-\frac{2 - \alpha_B}{\alpha_B - 1}}$. This allows us to
 12 determine α_B from the slope of the logarithmic plot of stress versus time. t_B and $\mu\bar{\gamma}_\infty$ were
 13 determined by fitting the rapid stretching part of the stress-strain curve with **eq.1**. Next, we
 14 fitted the torsion data. $G'(\omega)$ and $G''(\omega)$ were fitted using **eq.7** and **eq.8** to fine-tune the
 15 parameters. The value of t_B was accurately determined by this fine-tuning, thanks to the peak
 16 position in G'' which is sensitive to the value of t_B (**eq.11**).

17 As noted in our previous work,¹⁶ the moduli from the torsion tests are lower than those predicted
 18 from the parameters by the tensile tests by a factor of about 2. This discrepancy is believed to
 19 arise from the fact that the torsion test is performed in a parallel plate geometry (not in the cone
 20 plate geometry) where pre-compression is applied, and this is not accounted for in our equations
 21 (**eq.7** and **eq.8**).¹⁹

1 **4. Results and Discussion**

2 **4.1. Fitted material parameters**

3 A set of the fitting parameters for both the tensile and torsion tests was determined and
4 summarized in **Table I**. Comparison between fitting curves calculated with these parameters
5 and the experimental results of the tensile stress relaxation and the torsion frequency sweep
6 tests are shown in **Figures 1** for four dual crosslink gels as example. In Supporting Information
7 one can find comparisons for all the dual crosslink gels tested in this work for both tests, up to
8 100 s in stress relaxation tests (**Figures S2 – S5**). The model agrees well with the experimental
9 results for all samples tested, and one set of the parameters for each dual crosslink gel can
10 reasonably fit both tensile and torsion tests. This result indicates the validity of the model for
11 a wide range of crosslinking ratios.

12 **Table I.** Four reduced fitting parameters and the shift factor for moduli.

C_{GA} (mol%)	C_{borax} (mM)	$\mu\bar{\gamma}_\infty$ (kPa s ⁻¹)	$\mu\rho$ (kPa)	t_B (s)	α_B	Shift factor
0.2	1	20.9	2.41	0.367	1.64	0.90
	3	77.7	3.24	0.213	1.69	0.34
	5	125	6.73	0.174	1.66	0.47
	10	263	7.82	0.110	1.67	0.48
	20	452	9.55	0.0734	1.66	0.29
	50	1240	34.9	0.0572	1.63	0.20
0.6	1	33.7	17.2	0.393	1.48	0.48
	3	106	19.1	0.238	1.57	0.54
	5	155	19.7	0.213	1.57	0.37
	10	340	20.9	0.130	1.60	0.41
	20	578	21.0	0.0916	1.61	0.43
	50	1020	38.4	0.0683	1.57	0.39

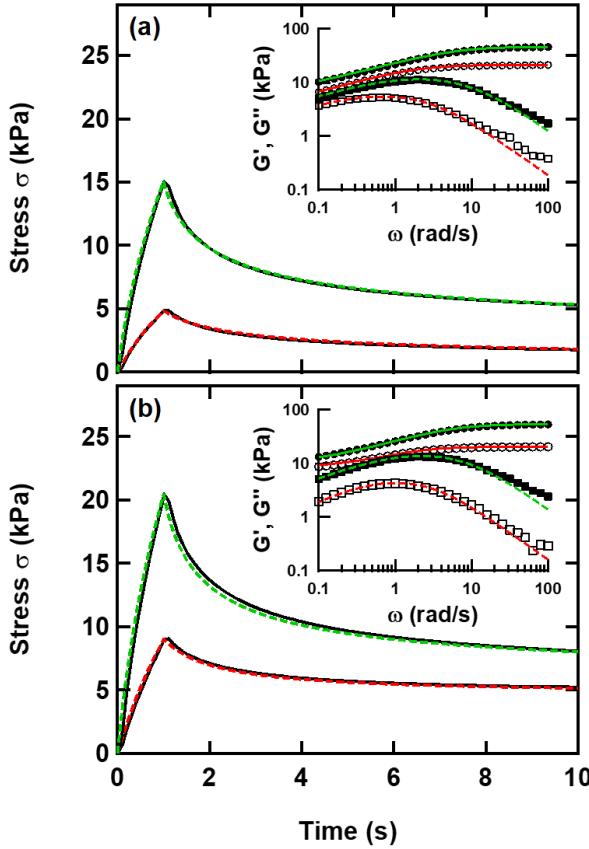


Figure 1. Comparison of the model prediction with the experimental results for the tensile relaxation tests. Uniaxial tensile stress as a function of time for dual crosslink gels with a chemical crosslinker concentration of (a) 0.2 and (b) 0.6 mol%. Results for two borax concentrations are shown, 1 mM (red) and 10 mM (green). Solid curves: experiments. Dashed curves: model prediction. Inset: Comparison of the model prediction with the experimental results for the small amplitude shear torsion tests. Viscoelastic moduli as a function of angular frequency for dual crosslink gels with a chemical crosslinker concentration of (a) 0.2 and (b) 0.6 mol%. Results for two borax concentrations are shown, 1 mM (red lines, open symbols) and 10 mM (green lines, filled symbols). Solid curves and circles: G' . Dashed curves and squares: G'' .

We emphasize that by fitting both tensile and torsion data, we were able to obtain reasonably accurate material parameters, for the following reasons. By fitting the tensile tests, from the stress relaxation part, the values of μ_p and α_B can be accurately determined, while those of t_B and $\mu\bar{\gamma}_\infty$, are less accurately found (the product of them is accurately found). This is due to the relatively low amount of broken and healed transient bonds during the rapid loading phase of the relaxation test where λ is high but the final stretch ratio λ_0 is low. By fitting the torsion

1 tests, the values of t_B can be accurately determined from the peak of G'' . However, the values
2 of $\mu\rho$ and $\mu\bar{\gamma}_\infty$ are less accurately measured due to the precompression applied in the parallel
3 plate geometry. The values of the shift factor used to adjust the discrepancy in the absolute
4 values of the moduli in the tensile tests and rheology tests are also shown in **Table I**. The
5 values of $\mu\rho$ and $\mu\bar{\gamma}_\infty$, which fitted well the tensile tests data, were multiplied by this factor to
6 fit the torsion test data. The average value of these shift factors is 0.45. The dispersion of the
7 shift factor is large since for each gel the measurement is different, and the normal force
8 relaxation of the pre-compressed sample is difficult to control.

9 **4.2. Modulus ($\mu\rho$ and $\mu\bar{\gamma}_\infty$)**

10 **4.2.1. Elastically active crosslinker populations**

11 In this section we study the relation between the crosslinker concentrations and the two
12 parameters, $\mu\rho$ and $\mu\bar{\gamma}_\infty$. We use the glutaraldehyde concentration in the feed, C_{GA} in mol%,
13 and the borax concentration in the feed in the preparation solution, C_{borax} in mM, as
14 experimental parameters of the chemical and physical crosslinkers concentrations, respectively.
15 First we investigate $\mu\bar{\gamma}_\infty$. The contribution of the closed transient crosslinks to the elastic
16 modulus is given by $G'_{closed} = \mu\bar{\gamma}_\infty \cdot \frac{t_B}{2-\alpha_B}$, which is a measurable rheological quantity of the
17 system(recall G'_{closed} is the contribution of the phydical crosslinks to the elastic modulus at high
18 frequency $\omega \rightarrow \infty$, see **eq.10**). Here we evaluate this reduced parameter $\mu\bar{\gamma}_\infty \cdot \frac{t_B}{2-\alpha_B}$ without
19 discussing separately the four parameters of which it is composed (μ , $\bar{\gamma}_\infty$, t_B and α_B). The
20 dependence of G'_{closed} on the borax concentration C_{borax} are plotted in **Figure 2a**. They increase
21 with borax concentration, and practically no chemical crosslinker concentration dependence is
22 found. A power-law fitting curve is shown in the figure: the exponent is found to be about 0.5,
23 i.e., $G'_{closed} \propto C_{borax}^{0.5}$.

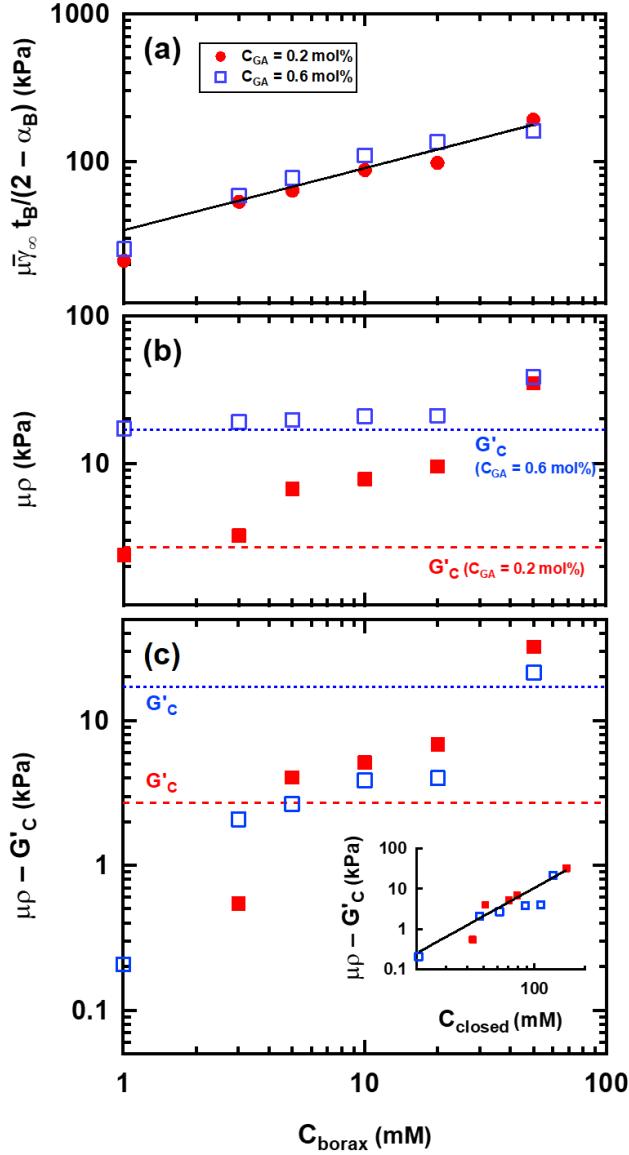


Figure 2. (a) Borax concentration dependence of $G'_{\text{closed}} = \mu \bar{\gamma}_\infty \frac{t_B}{2 - \alpha_B}$ (Modulus contribution from closed transient crosslinks). The solid line is a power-law fit with an exponent of 0.51. (b) The borax concentration dependence of $\mu \rho$. The dashed lines indicate the elastic modulus of the corresponding chemical gels. (c) The value of $G'_{\text{slow}} = \mu \rho - G'_c$ as a function of the borax concentration C_{borax} in feed. Inset: the elastically active closed physical crosslinker concentration C_{closed} . The solid line is a linear fit with an exponent of 2.3. The filled red circles represent the dual crosslink gel for $C_{\text{GA}} = 0.2 \text{ mol\%}$, open blue circles for $C_{\text{GA}} = 0.6 \text{ mol\%}$.

For a more quantitative discussion, we estimate *the molar concentration of the elastically active transient physical crosslinks, C_{closed}* , from the elastic modulus G'_{closed} . The elastic modulus is proportional to the molar concentration of elastically active chain and is written as $G'_{\text{closed}} =$

1 $\frac{1}{2} C_{\text{closed}} \cdot RT$, where R is the gas constant and T is the absolute temperature. The factor 1/2
2 indicates that each crosslinker is tetrafunctional and crosslinks two chains. In this relation
3 C_{closed} has mol/m³ as unit, and is recalculated in mM. We found values between 17 and 155
4 mM with the same C_{borax} dependence as G'_{closed} .²³

5 Next we study the dependence on the borax concentration of the time-independent reduced
6 parameter $\mu\rho$. Recall that $\mu\rho$ corresponds to the elastic modulus at zero frequency ($t \gg t_B$)
7 (**eq.10**). We performed tensile stress relaxation test up to 100 s for t_B lower than 1 s. The
8 physical model of the dual crosslink gel assumes that the transient crosslinks dissociate and the
9 chains fully relax at low frequency, thus the value of $\mu\rho$ is expected to be the same as the
10 modulus of the chemical gel used to prepare the dual crosslink gels, and therefore should be
11 independent of the borax concentration in the feed, C_{borax} .

12 **Figure 2b** shows the borax concentration dependence of $\mu\rho$. For both chemical crosslinking
13 ratios, the values of the elastic modulus G'_C for the corresponding chemical gels (measured
14 independently with the chemical gel samples) are indicated by the dashed lines. For the gels
15 with $C_{\text{GA}} = 0.2$ mol%, at low borax concentrations we find fitted values of $\mu\rho$ close to that of
16 the chemical gel (2.7 kPa), then they increase with increasing borax concentration. At $C_{\text{borax}} =$
17 50 mM, $\mu\rho$ reaches 25 kPa. For gels with $C_{\text{GA}} = 0.6$ mol%, at borax concentrations below 20
18 mM the values of $\mu\rho$ are comparable to that of the chemical gel (17 kPa), then they increase to
19 30 kPa for $C_{\text{borax}} = 50$ mM. These results indicate that at the lower frequency experimentally
20 investigated, the modulus of the dual crosslink gels matches with that of the chemical gels only
21 at sufficiently low borax concentration. *This result suggests that at high borax concentrations*
22 *the physical crosslinkers increase $\mu\rho$, forming a second population of elastically active physical*
23 *crosslinkers with a much longer lifetime than that corresponding to G'_{closed} .* This second

1 population is rheologically indistinguishable from the chemical crosslinks within the window
2 of observation times explored here.

3 The modulus due to the presence of this longer lived population of physical crosslinks can be
4 determined by subtracting *the elastic modulus of the corresponding chemical gel G'_C* from the
5 fitted value of $\mu\rho$ for each dual crosslink gels assuming that additivity holds for this population.
6 The result is shown in **Figure 2c**. Even though the eventual errors of this subtraction between
7 the data from two separate rheological measurements can be large, one can still see that the
8 values of $G'_{\text{slow}} = \mu\rho - G'_C$ increase with borax concentration C_{borax} , and no clear effect of the
9 degree of chemical crosslinking is found. This result suggests that the presence of the
10 permanent crosslinks does not influence the formation of this slower population at the studied
11 crosslinking ratios. The values of G'_{slow} (0.1 – 30 kPa) are comparable to (or lower than) those
12 of G'_C (3 or 17 kPa). Finally, these values of modulus due to slow physical crosslinks are also
13 lower than those of the closed physical crosslinks (21 – 190 kPa, as shown in **Figure 2a**).

14 To better characterize the origin of this long lived population of physical crosslinks, the values
15 of $G'_{\text{slow}} = \mu\rho - G'_C$ are plotted in the inset of **Figure 2c** as a function of the concentration of
16 elastically active chains due to physical crosslinkers which dissociate within the experimental
17 time scale, C_{closed} . The values of G'_{slow} increase with C_{closed} with a power-law exponent of about
18 2.3. This power-law exponent suggests that the origin of this slow population is due to
19 clustering of two (or more) physical crosslinkers.

20 In the case of binding of mobile crosslinkers which can diffuse in the network and bind on the
21 chains, the binding potential can entropically and enthalpically vary depending on the position
22 relative to the existing physical and chemical crosslinkers. Binding to a site very close to an
23 existing crosslinker is preferred, as the local polymer concentration is higher. This clustering
24 is also expected to bring an entropic gain for polymer chains.²⁴ The lifetime of a cluster made
25 of several physical bonds should be longer than that of a single bond, as it is necessary to break

1 all the bonds for the chain to relax. Clustering involving a chemical crosslink and physical
2 crosslinks might occur. However, it is difficult to rheologically detect such clusters, since they
3 are not distinguishable from a simple chemical crosslink in the linear regime. Furthermore, we
4 expect the concentration of clusters near a chemical crosslink to be very low since the
5 concentration of the chemical crosslinks itself, C_C , estimated from the value of G'_C , is also very
6 low compared to C_{closed} . The values of C_C are estimated to be 2 and 14 mM for C_{GA} of 0.2 and
7 0.6 mol%.

8 The slower population can be an important factor in determining gel failure under large
9 deformation. Previously it was shown that the stretch at break of the dual crosslink gels is very
10 sensitive to the chemical and physical crosslinking ratios, and decreases with increasing
11 chemical and physical crosslinking ratio.¹⁶ This is presumably due to the increase in the amount
12 of the slower population which is expected to behave similarly to permanent crosslinks which
13 enhance the brittleness.

14 The concentrations of the three different elastically *active* components are summarized here.
15 The concentrations of permanent chemical crosslinks (C_C), and of the two populations of
16 transient physical crosslinks, the fast one (C_{closed}) and slow one (C_{slow}), were estimated from the
17 corresponding modulus and are plotted as a function of the borax concentration in the feed C_{borax}
18 in **Figure 3a**. At all borax concentrations C_{borax} tested here, the values of C_{closed} are higher than
19 those of C_{slow} and C_C , indicating that the time-dependent elasticity of the dual crosslink gels is
20 still governed by the transient crosslinks. At high C_{borax} , the difference between C_{closed} and C_{slow}
21 becomes smaller.

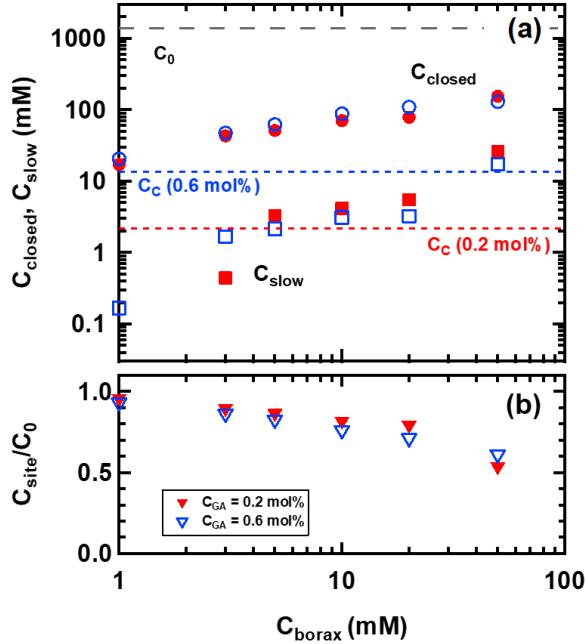


Figure 3. The borax concentrations dependence of the two populations of the transient physical crosslinks: the fast one C_{closed} (circles) and the slow one C_{slow} (squares). The red symbols are for $C_{\text{GA}} = 0.2 \text{ mol\%}$, blue ones for $C_{\text{GA}} = 0.6 \text{ mol\%}$. Dashed lines: red for C_c for $C_{\text{GA}} = 0.2 \text{ mol\%}$, blue for C_c for $C_{\text{GA}} = 0.6 \text{ mol\%}$, gray for the total concentration of the binding site, C_0 (see the text).

4.2.2. Elastically inactive crosslinker populations

In the previous subsection, we have shown that there are three populations of elastically active crosslinkers, and that their concentration can be estimated from the corresponding elastic modulus. The correspondence between the elastic modulus and the model parameters, $\mu\mu$ and $\mu\bar{\gamma}_\infty$, was also demonstrated. In our steady state model, we assume that there is a thermodynamic equilibrium between the elastically active closed crosslinks and the elastically *inactive* open crosslinks. This equilibrium depends on the physical chemistry of the dynamic bonds used as transient crosslinks. In this subsection, we discuss the open crosslinks and other elastically inactive populations of the transient crosslinks. As seen later in this subsection, the concentration of available binding sites is an important parameter influencing the dynamics of the breaking/healing of the transient crosslinks and we now attempt to approximately evaluate

1 it. This argument will be useful to better comprehend the discussion about the dynamics
2 developed in the next section 4.3.

3 The complexation of borate ions with diol binding sites (two neighboring hydroxyl groups) on
4 the PVA chains has two binding equilibria as borate ions can interact with one or two diol
5 binding sites as illustrated in **Figure 4**. At equilibrium, the borate ions can take three states. (1)
6 “Free” borate ions in the gel and in the solution which do not interact with PVA chains, their
7 concentration is defined as C_{free} (mol/L). (2) Borate ions which complex with one diol binding
8 site (monodiol complexation), do not crosslink chains. This state corresponds to “open”
9 crosslink (with the concentration of C_{open}), as it readily forms a closed crosslink with an
10 available diol binding site. (3) Borate ions complexing with two diol binding sites (didiol
11 complexation) can be further classified into three different states which are not
12 thermodynamically distinguishable. (3a) The borate ions in didiol complexes can be *intra-*
13 *chain* didiol complexes (C_{intra}), and these complexes are elastically *inactive*. (3b) They can be
14 also inter-chain didiol complexes which serve as “closed” crosslinks (C_{closed}), thus elastically
15 *active*. Finally, (3c) they can also form a cluster of the didiol complexes behaving as a slow
16 population of the crosslink (C_{slow}), considered as elastically *active*.

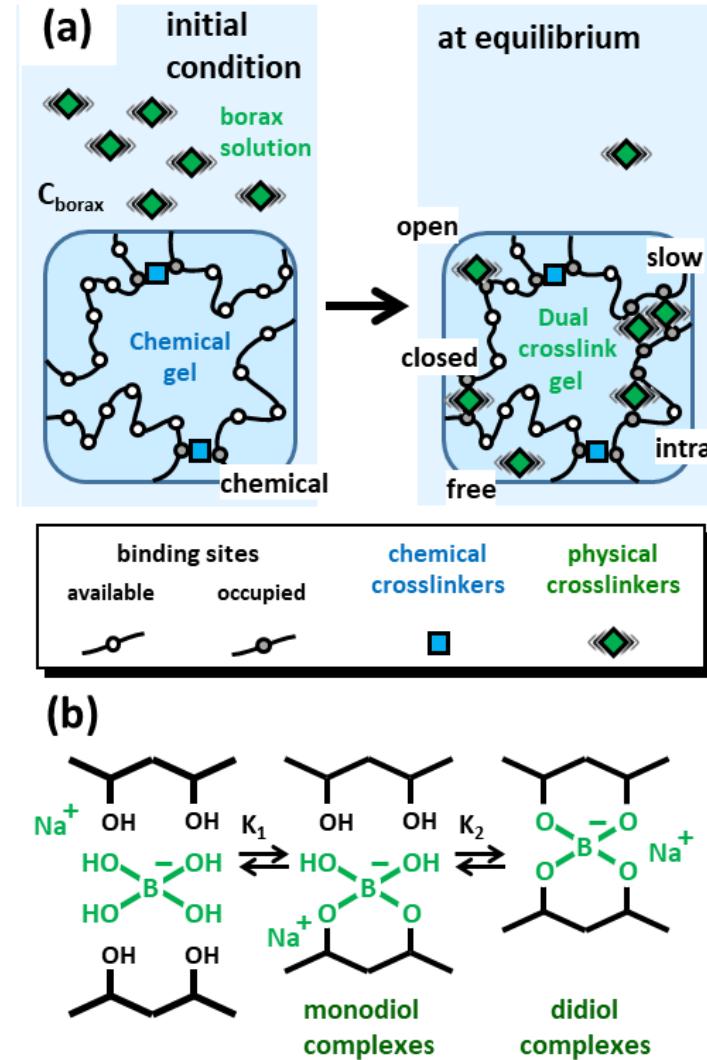
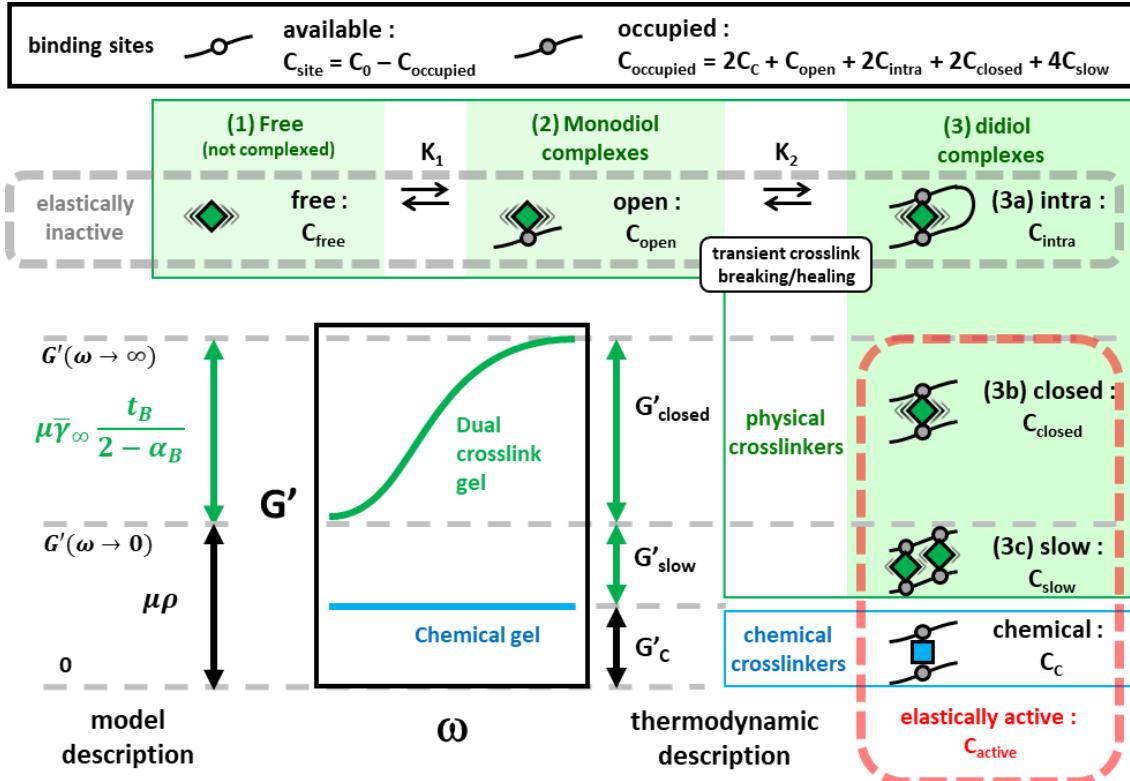


Figure 4. (a) Schematic illustrations of transient crosslinker incorporation into the chemical gel. (b) Binding equilibria of the borate ion and diols on PVA chains.

The two binding constants, K_1 and K_2 (L/mol), are written as $K_1 = \frac{C_{\text{open}}}{C_{\text{free}} \cdot C_{\text{site}}}$ and $K_2 = \frac{C_{\text{di}}}{C_{\text{open}} \cdot C_{\text{site}}}$, where C_{site} is the concentration of available binding sites on the PVA chains, and $C_{\text{di}} = C_{\text{intra}} + C_{\text{closed}} + C_{\text{slow}}$. In **Figure 5** we schematically illustrated in green these five different populations of physical crosslinkers (borate ions), as well as chemical crosslinks (in blue) and diol binding sites on the PVA chains. For the elastically active populations (3b, 3c and the chemical crosslinks), the correspondence with $G'(\omega)$ and the model parameters are also shown. The dynamics of the transient crosslink breaking/healing are described by the second equilibrium

1 (i.e., by the binding constant K_2), which depends on the three concentrations, C_{di} , C_{open} and C_{site} .

2 Here we attempt to estimate them as quantitatively as possible.



3

4 **Figure 5.** Classification of the different species involved in the binding equilibria of borate ion-diol

5 complexes, and their concentration. Correspondence between the model description and the

6 thermodynamic description of the elastic modulus.

7 *Didiol complex concentration.* Contrary to C_{closed} and C_{slow} , which are concentrations of the

8 elastically active populations, it is experimentally difficult to determine the concentration of the

9 rheologically undetectable intrachain crosslink, C_{intra} . In dilute solutions intrachain

10 crosslinking is favored, while in semi-dilute solutions and gels the amount of the interchain

11 crosslinks increases. Since intrachain crosslinking involves the formation of a loop on the

12 polymer chain, chain rigidity is a factor controlling the size of the loop. Pezron et al.²⁵⁻²⁷

13 estimated the ratio of interchain to intrachain crosslinks as a function of the polymer

14 concentration, by correlating the sizes of the blob and the loop formed by intrachain crosslink.

15 Applying their theory to our system with a fixed PVA concentration of 12 wt%, the ratio of

16 inter- to intra-chain crosslink is estimated to be about 1.7. In the following, we use this value,

1 thus $C_{\text{intra}} = (C_{\text{closed}} + C_{\text{slow}})/1.7$. It should be noted that for our systems the PVA chains are
2 integrated into the percolated chemical network, thus the chains between crosslinks might have
3 lower deformability to form a loop than the chains in solution, and C_{intra} could be lower than
4 this estimate.

5 *Monodiol complex (open crosslink) concentration.* For solutions with relatively low PVA
6 concentrations (without chemical crosslinks), ^{11}B NMR spectroscopy has been used to
7 determine the concentrations of different states of borate ions.^{28,29} The results indicate that
8 monodiol complexes, corresponding to open transient crosslinks have much weaker signals
9 than the didiol complexes (closed transient crosslinks), as the binding equilibrium is toward the
10 didiol complexes, or $C_{\text{closed}} \gg C_{\text{open}}$. We will further discuss C_{open} in the next section. We did
11 not perform NMR measurements of our chemically crosslinked systems with relatively higher
12 PVA concentration, due to difficulties in sample preparation.

13 *Available binding site concentration.* The total concentration of binding sites is estimated to
14 be $C_0 = 1.36 \text{ M}$,³⁰ which is shown as a black dashed line in **Figure 3a**. The concentration of
15 occupied binding sites can be determined from that of the chemical crosslinks and the bound
16 borate ions in monodiol and didiol complexes, thus C_{C} , C_{open} , C_{closed} , C_{intra} and C_{slow} .
17 Specifically, the concentration of the occupied sites can be written as $C_{\text{occupied}} = 2C_{\text{C}} + C_{\text{open}} +$
18 $2C_{\text{closed}} + 2C_{\text{intra}} + 4C_{\text{slow}}$, where the numerical factors 1, 2 or 4 in this equation indicate the
19 number of binding sites for the different binding mechanisms and assumes a cluster of 2 didiol
20 complexes. The concentration of available binding sites C_{site} is $C_{\text{site}} = C_0 - C_{\text{occupied}}$. The values
21 of C_{site} are estimated by inputting into this equation the values of these different concentrations
22 (rheologically determined: C_{C} , C_{closed} , C_{slow} ; estimated from C_{closed} and C_{slow} : C_{intra} ; C_{open} is
23 ignored since $C_{\text{open}} \ll C_{\text{closed}}$). In **Figure 3b** C_{site}/C_0 is plotted as a function of the borax
24 concentration C_{borax} . C_{site}/C_0 decreases with C_{borax} , and for the gel with the highest degree of
25 binding, C_{site}/C_0 is estimated to be about 0.54 (C_{site} is about 0.73 M). Therefore, although the

1 concentration of the elastically inactive populations may not be quantitatively very accurate we
2 can still conclude that the saturation of binding sites does not occur in the studied conditions:
3 there are plenty of available binding sites. Note that $K_2 \cdot C_{\text{site}} = \frac{C_{\text{di}}}{C_{\text{open}}}$, thus close to the binding
4 saturation, with decreasing C_{site} , C_{di} relatively decreases and the dynamics of the transient
5 crosslink breaking/healing can be very different.

6 **4.3. Characteristic time (t_B and α_B)**

7 In this section we investigate the effect of the crosslinking ratio on the characteristic relaxation
8 time of the dual crosslink gels, by focusing on the two parameters, t_B and α_B . t_B is the
9 characteristic transient bond breaking time and is proportional to the rheologically directly
10 measurable relaxation time τ_X of the peak position of G'' (section 3.1, **eq.11**) with a coefficient
11 depending only on α_B . In the inset of **Figure 6**, this proportionality is shown. The values of
12 the coefficient, $1/[(\alpha_B - 1) \cdot f(q)]$, vary between 2.5 and 4.7. The concentration dependence
13 of α_B will be discussed later in this section. As seen in the inset of **Figure 1** (and **Figure S2**),
14 the position of the peak depends on the chemical crosslinker concentration: gels with $C_{\text{borax}} =$
15 10 mM (filled symbol, green curves) show the peak at higher frequency than the gels with $C_{\text{borax}} =$
16 = 1 mM (open symbols, red curves). **Figure 6** shows that fitted values of t_B obtained from the
17 rheological curves decrease with increasing borax concentration C_{borax} , and do not show any
18 obvious chemical crosslinking ratio dependence. The value of t_B is found to approximately
19 scale as $t_B \sim C_{\text{borax}}^{-0.48}$. Thus, for this system, the bond breaking time decreases with increasing
20 physical crosslinker concentration.

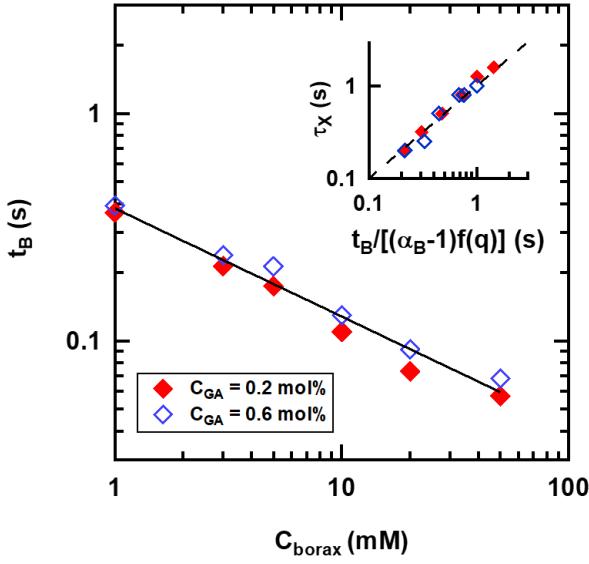


Figure 6. The values of t_B as a function of the borax concentration C_{borax} . Red diamonds: $C_{\text{GA}} = 0.2 \text{ mol\%}$; blue diamonds: $C_{\text{GA}} = 0.6 \text{ mol\%}$. The solid line is a power-law fit with an exponent of -0.48. Inset: the network relaxation time at the peak of G'' , τ_X , as a function of t_B (see eq.11).

4.3.1 Molecular interpretation: theoretical framework

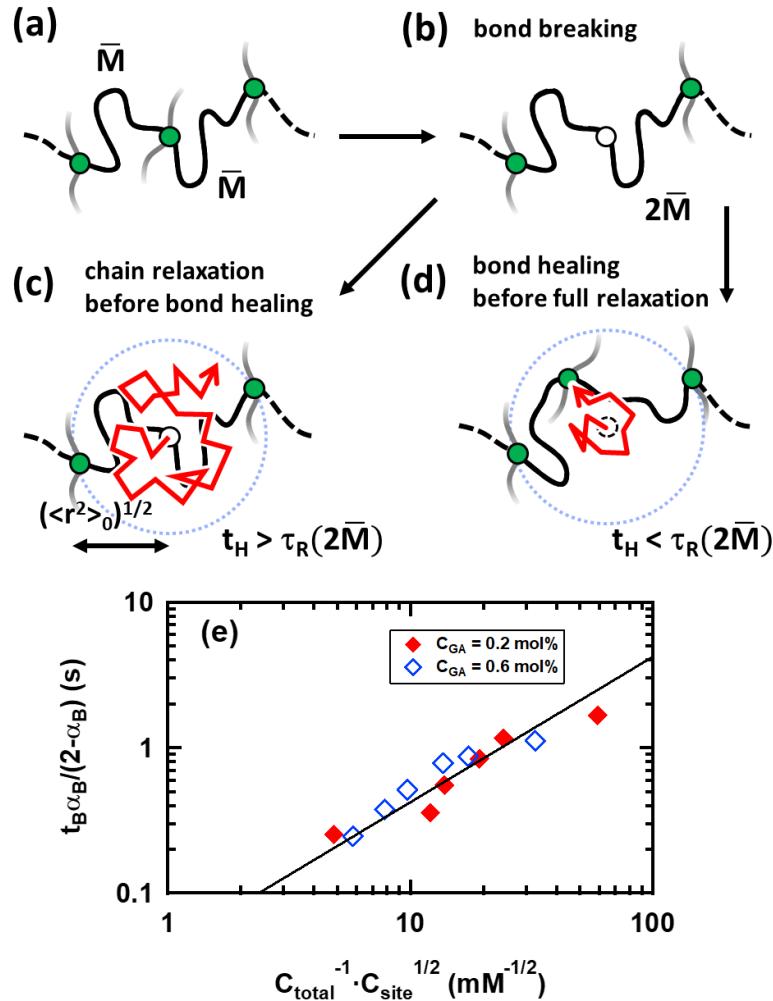
We now attempt to interpret this concentration (C_{borax}) dependence from a macromolecular point of view, by considering the chain relaxation dynamics as a function of transient bond breaking and healing times following the argument of Indei and Takimoto for associative polymers.³¹

In a dual crosslink network prepared from a percolated chemical network by incorporating additional transient crosslinks, each transient crosslink is located on a part of a chain between two other crosslinks which can be permanent or transient, and are elastically active during the bond breaking time scale considered here. In **Figure 7a** this chain is indicated in black and the average Kuhn segment number between two adjacent crosslinks is defined as \bar{M} . When the transient crosslink breaks with a characteristic breaking time t_b , a subchain having $2\bar{M}$ segments is released and starts to relax (**Figure 7b**). We will discuss the relation between this molecular parameter t_b and the model parameter t_B later in this section. The mean square displacement, MSD, of the open transient bond on this subchain (after its release) is approximately:³²

$$MSD \sim \langle \Delta r^2 \rangle_0 \left(\frac{t}{\tau_R} \right)^{\frac{1}{2}} \quad \text{for } t < \tau_R \quad (\text{eq.13i})$$

$$MSD \sim \langle \Delta r^2 \rangle_0 \quad \text{for } t > \tau_R \quad (\text{eq.13ii})$$

1 where $\langle \Delta r^2 \rangle_0$ is the mean square length of the subchain, and τ_R is the Rouse relaxation time of
 2 a subchain having the segment number of $2\bar{M}$.



3
 4 **Figure 7.** (a) – (d) Schematic illustrations of relaxation of a subchain after bond breaking in
 5 competition with bond healing. (e) τ_x as a function of $C_{\text{total}}^{-1} \cdot C_{\text{site}}^{1/2}$. Red diamonds: $C_{\text{GA}} = 0.2 \text{ mol\%}$;
 6 blue diamonds: $C_{\text{GA}} = 0.6 \text{ mol\%}$. The solid line is a linear fit.

7 Next we include bond healing in the argument: the open transient crosslink can reattach with
 8 an available binding site nearby, and its characteristic time is t_h . Since the transient crosslink

1 can move while it is open (starting at $t = 0$), the subchain can fully relax if $t < t_h$. Thus, we can
 2 rewrite **eq.13** by replacing t with t_h :

$$MSD \sim \langle \Delta r^2 \rangle_0 \left(\frac{t_h}{\tau_R} \right)^{\frac{1}{2}} \quad \text{for } t_h < \tau_R \quad (\text{eq.14i})$$

$$MSD \sim \langle \Delta r^2 \rangle_0 \quad \text{for } t_h > \tau_R \quad (\text{eq.14ii})$$

3 For the case of $t_h > \tau_R$, the subchain can fully relax before the transient crosslink reattaches
 4 (**Figure 7c**), thus the MSD of the open transient crosslink can reach its maximum value, $\langle \Delta r^2 \rangle_0$.
 5 On the contrary, for $t_h < \tau_R$, the transient crosslink reattaches before the chain fully relaxes
 6 (**Figure 7d**), thus the value of MSD is lower than that for $t_h > \tau_R$. Bond healing can occur in
 7 multiple steps (number of step: n_{step}) when $t_h < \tau_R$, until the subchain fully relaxes and its
 8 equilibrium is reached, thus $MSD \cdot n_{\text{step}} \sim \langle \Delta r^2 \rangle_0$.
 9 The network relaxation time τ_X can also be interpreted as the time required for the subchain to
 10 reach its equilibrium state during which the transient crosslink breaks in single or multiple steps,
 11 thus it is written as

$$\tau_X \sim n_{\text{step}} \cdot t_b \sim \frac{\langle \Delta r^2 \rangle_0}{MSD} \cdot t_b \quad (\text{eq.15})$$

12 In summary, our analysis shows that

$$\tau_X \sim \left(\frac{\tau_R}{t_h} \right)^{\frac{1}{2}} \cdot t_b \quad \text{for } t_h < \tau_R \quad (\text{eq.16i})$$

$$\tau_X \sim t_b \quad \text{for } t_h > \tau_R \quad (\text{eq.16ii})$$

13 4.3.2 Molecular interpretation: Experimental data

14 The physical crosslinker concentration dependences of t_h and τ_R are now studied. The Rouse
 15 relaxation time of the subchain having the Kuhn segment number of $2\bar{M}$ is written as $\tau_R = \tau_0 \cdot$
 16 $(2\bar{M})^2$, where τ_0 is the relaxation time of the Kuhn segment. Since \bar{M} is inversely proportional

1 to the crosslinking ratio, τ_R scales with the concentration of the total elastically active crosslinks,

2 $C_{\text{active}} = C_{\text{closed}} + C_{\text{slow}} + C_C$, as

$$\tau_R \sim C_{\text{active}}^{-2} \quad (\text{eq.16iii})$$

3 C_{active} is estimated from the elastic moduli, and found to be between 19 and 183 mM, For
4 simplification, we have ignored the influence of loops made by the intrachain crosslinks on the
5 chain dynamics. Bond healing requires an available binding site on the polymer, thus the bond
6 reassociation time t_h is inversely proportional to its concentration, i.e.,

$$t_h \sim C_{\text{site}}^{-1} \quad (\text{eq.16iv})$$

7 where $C_{\text{site}} = C_0 - 2C_C - C_{\text{open}} - 2C_{\text{closed}} - 2C_{\text{intra}} - 4C_{\text{slow}}$, as shown in the subsection 4.2.2. As
8 discussed previously, we assume $C_{\text{open}} \ll C_{\text{closed}} < C_0$, thus we ignore C_{open} . C_{site} varies between
9 1.3 and 0.73 M. From **eq.16i,iii,iv**, τ_X is expected to scale as $\tau_X \sim C_{\text{active}}^{-1} \cdot C_{\text{site}}^{1/2}$. In **Figure 7e**,
10 the values of τ_X , are plotted as a function of $C_{\text{active}}^{-1} \cdot C_{\text{site}}^{1/2}$. The solid line corresponds to a
11 linear fit, suggesting that the scaling corresponding to **eq.16i** holds. Even at lower values of τ_X ,
12 we did not observe a regime corresponding to **eq.16ii**. The absence of this regime shows that
13 in the studied conditions, the relaxation time of the network equals $n_{\text{step}} \cdot t_b$, with $n_{\text{step}} > 1$ and $\tau_R >$
14 t_h .

15 Here we compare the constitutive model parameters (t_B and t_H) with the molecular parameters
16 (t_b and t_h). According to the definition, t_H is identical to t_h . From **eq.11** and **eq.15**, we have
17 $\tau_X \sim t_B \sim n_{\text{step}} \cdot t_b$. Thus we conclude that the decrease in t_B with increase in C_{borax} shown in
18 **Figure 6** is due to the decrease in n_{step} , as a consequence of the decrease in C_{site} and of the
19 increase in C_{active} . Since $n_{\text{step}} > 1$, it is necessary to slightly modify one of the assumptions of
20 the model described in section 3.1 to meet the argument above. The assumption (3) should be
21 rewritten as “(3’) the stress sustained by a transient chain is relaxed with a Rouse relaxation
22 time after single or multiple transient bond breaking steps, as a function of the healing time of

1 the crosslink. A fully relaxed temporary detached chain can be reattached without carrying
2 strain energy, and experiences the deformation history from its birth at time τ (s) to the current
3 time t (s)." The equations are identical and consistent with the argument.

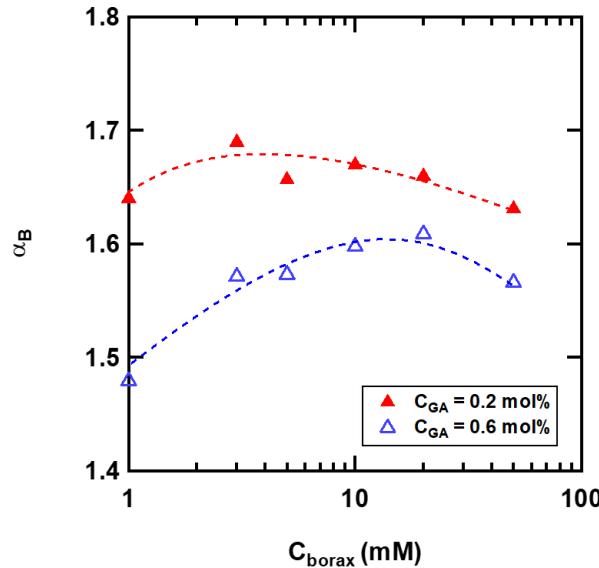
4 Let us roughly estimate the order of the three characteristic times, τ_R , t_b , and t_h . From the value
5 of the plateau modulus at high frequency $G' = k_B T / \xi^3$, the size of the Gaussian subchain, ξ , is
6 determined. Then the number of Kuhn segment \bar{M} is determined from $\xi = b_K \bar{M}^{1/2}$, with the
7 Kuhn segment size of b_K . The Rouse relaxation time τ_R is written as $\tau_R = \tau_0 \cdot (2\bar{M})^2$. We
8 used the viscosity of water, $\eta_s = 0.00089$ Pa s, $b_K = 0.62$ nm,³³ thus $\tau_0 = \eta_s b_K^3 / k_B T = 5.2 \times$
9 10^{-11} s. The values of τ_R for the dual crosslink gels studied here are estimated to be between
10 1×10^{-6} and 7×10^{-8} s.

11 The values of t_b and t_h cannot be determined from the analysis above. Still, from **eq.15** and
12 **eq.16i**, we can estimate the highest values of t_h and t_b , as well as the lowest value of n_{step} .
13 Specifically, since $t_h < \tau_R$, $t_b < \tau_X$, **eq.15** and **eq.16i**, imply $\tau_X/t_b \sim n_{\text{step}} = (\tau_R/t_h)^{1/2}$. Since $t_b < \tau_X$,
14 we assume the highest value of t_b is close to the lowest value of τ_X measured, about 0.2 s. With
15 $t_b = 0.2$ s, we find the values of n_{step} between 1 and 8 for the different crosslinking ratios. Since
16 $n_{\text{step}} = (\tau_R/t_h)^{1/2}$, we can approximately estimate t_h from the values of τ_R , and we find the values
17 of t_h is between 1×10^{-8} and 8×10^{-8} s. This very fast healing time might be due to the presence
18 of binding site in the vicinity of the closed crosslink. In fact, practically any part of the PVA
19 chain can be a binding site, and a dissociated crosslink can be immediately captured by a
20 neighboring binding site.

21 From the thermodynamic argument,³⁴ we have $\frac{t_b}{t_h} = \frac{C_{\text{di}}}{C_{\text{open}}}$. Thus the ratio of the two
22 characteristic time corresponds to the ratio of the closed and open crosslinks. For the largest
23 value of $t_b = 0.2$, the ratio t_b/t_h varies between 3×10^6 and 2×10^7 , indicating that $t_B \gg t_H$ and
24 $C_{\text{closed}} \approx C_{\text{di}} \gg C_{\text{open}}$. And when t_b is smaller, then this ratio becomes larger.

1 **4.3.3. Molecular interpretation of α_B**

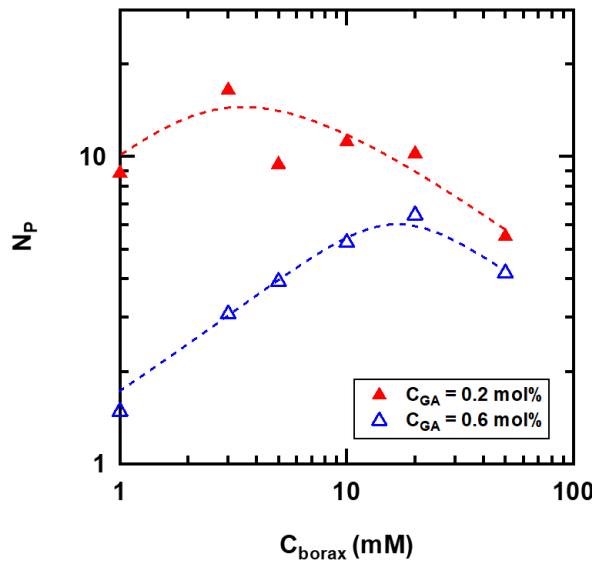
2 The values of α_B are plotted as a function of the borax concentration in **Figure 8**. For the gels
3 with the chemical crosslinking ratio of $C_{GA} = 0.6 \text{ mol\%}$, the values of α_B are found between
4 1.48 and 1.61, they first increase with C_{borax} then decrease. The maximum is at $C_{borax} \sim 20 \text{ mM}$.
5 For gels with $C_{GA} = 0.2 \text{ mol\%}$, the values of α_B are found between 1.63 and 1.69, higher than
6 those for the gel with $C_{GA} = 0.6 \text{ mol\%}$. Though the variation is small, they peak around C_{borax}
7 = 3 mM.



9 **Figure 8.** The values of α_B as a function of the borax concentration. Red triangles: $C_{GA} = 0.2 \text{ mol\%}$;
10 blue triangles: $C_{GA} = 0.6 \text{ mol\%}$. The dashed curves are guide for the eye.

11 The material parameter α_B describes the spectrum of relaxation times of the transient strands.
12 As shown in 4.3.1, the relaxation time τ_X depends on the subchain length, or on the crosslinking
13 ratio. Thus it is expected that the spectrum of the relaxation times can be expressed as a function
14 of the number of relaxation modes due to the distribution of the subchain length in the dual
15 crosslink network. First, we find the slowest relaxation modes (longest chain). It is reasonable
16 to take the Rouse mode of a primary chain between the two neighboring permanent crosslinks
17 as the slowest mode, since we first prepare a permanent chemical network then we add transient

1 crosslinks. When the transient crosslinks are added to the primary chain, the primary chain is
 2 divided into subchains, having shorter Rouse relaxation times. We define a parameter N_p , the
 3 number of the transient crosslinks per primary chain, as the ratio of $\rho_{closed} = \bar{\gamma}_\infty \cdot \frac{t_B}{2-\alpha_B}$ to ρ ,
 4 which signifies the ratio of the transient closed physical crosslinks to the permanent crosslink
 5 including the chemical crosslinks and the slow population of the physical crosslinks which do
 6 not break at the time scale of the measurement, thus behave similarly to the permanent
 7 crosslinks.

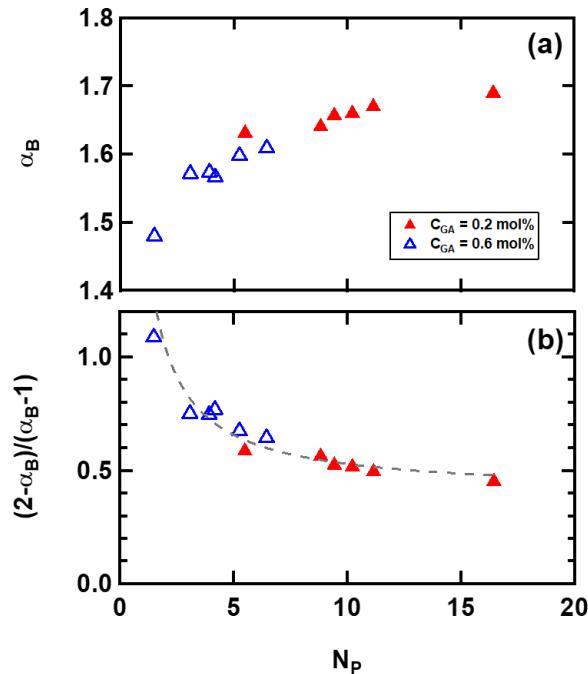


9 **Figure 9.** Number of the elastically active transient physical crosslinks per non transient crosslinks
 10 as a function of the borax concentration. Filled red triangles: $C_{\text{GA}} = 0.2 \text{ mol\%}$; open blue triangles:
 11 $C_{\text{GA}} = 0.6 \text{ mol\%}$. The dashed curves are guide for the eye.

12 The values of $N_p = \rho_{closed}/\rho$ are plotted as a function of C_{borax} in **Figure 9**. At low C_{borax} , N_p
 13 increases with C_{borax} as the increase in ρ_{closed} is dominant, while at high C_{borax} it decreases with
 14 C_{borax} since the increase in ρ is dominant due to the increase in the slow population of the
 15 physical crosslinks, giving a maximum. The position of the maximum is determined by the
 16 value of G'_C : for gels with the lower chemical crosslinking ratio ($C_{\text{GA}} = 0.2 \text{ mol\%}$) the peak is
 17 found at a lower C_{borax} (about 0.3 mM), while for the gels with $C_{\text{GA}} = 0.6 \text{ mol\%}$ the peak is at
 18 about 20 mM. The values of N_p range between 5.5 and 16 for $C_{\text{GA}} = 0.2 \text{ mol\%}$, and between

1 1.5 and 6.4 for $C_{GA} = 0.6$ mol%, indicating that it is experimentally difficult to increase the
 2 value by more than 20 in this system.

3 One can notice resemblance between the C_{borax} dependence of α_B and that of N_P shown in
 4 **Figure 8** and **Figure 9**, suggesting that α_B scales with N_P . **Figure 10a** shows α_B as a function
 5 of N_P for both chemical crosslinking ratios. We clearly see a consistent trend for the two
 6 chemical crosslinker concentrations: α_B increases with N_P . This result indicates that the
 7 physical meaning of the parameter α_B is related to the number of the relaxation modes of a
 8 chain.



9
 10 **Figure 10.** The values of (a) α_B and (b) $(2 - \alpha_B)/(\alpha_B - 1)$ as a function of N_P . Filled red triangles:
 11 $C_{GA} = 0.2$ mol%; open blue triangles: $C_{GA} = 0.6$ mol%. The dashed curve is an empirical relation
 12 $\frac{2 - \alpha_B}{\alpha_B - 1} = \frac{1.28}{N_P} + 0.40$ (see the text).

13 To further quantify the rheological significance of α_B , we estimate the dependence of $\frac{2 - \alpha_B}{\alpha_B - 1}$ on
 14 N_P . We consider the value of $\frac{2 - \alpha_B}{\alpha_B - 1}$ as a criterion to understand the rheological signification of
 15 α_B : in tensile relaxation tests, the power-law behavior $\sigma(t) - \sigma_\infty \sim t^{-\frac{2 - \alpha_B}{\alpha_B - 1}}$ is found from eq.12,

1 and in torsion tests, we find a power-law behavior $G' - \mu\rho \sim \omega^{\frac{2-\alpha_B}{\alpha_B-1}}$ from **eq.9**. The values of
 2 $\frac{2-\alpha_B}{\alpha_B-1}$ are plotted as a function of N_P in **Figure 10b**. They range between 1.09 and 0.45 and
 3 decreases with N_P . This result suggests that with increasing number of transient crosslinkers
 4 and hence relaxation modes, the dynamics of the system gradually move from a Maxwell-like
 5 behavior with $\frac{2-\alpha_B}{\alpha_B-1} = 1$ to a Rouse-like behavior with $\frac{2-\alpha_B}{\alpha_B-1} = 0.5$. It suggests also that the
 6 value of α_B can be determined from the rheologically measurable value of $N_P =$
 7 $(\mu\bar{\gamma}_\infty \cdot \frac{t_B}{2-\alpha_B})/\mu\rho = [G'(\omega \rightarrow \infty) - G'(\omega \rightarrow 0)]/G'(\omega \rightarrow 0)$. By fitting the data in **Figure**
 8 **10b**, we propose an empirical relation:

$$\frac{2-\alpha_B}{\alpha_B-1} = \frac{1.28}{N_P} + 0.40, \quad (\text{eq.17})$$

9 which is shown in the figure as a gray dashed curve. The value of $\frac{2-\alpha_B}{\alpha_B-1}$ goes to 0.4 at $N_P \gg 1$,
 10 this value is slightly lower than what is expected for the Rouse mode. The two factors (1.28
 11 and 0.40) should be intrinsic to this system. Universality of this relation needs to be further
 12 confirmed with different dual crosslink networks.

13 It should be noted that it is difficult to observe this Rouse-like mode in associative polymer
 14 solutions (physical gels) with small numbers of stickers (small N_P), due to the terminal flow.
 15 In fact, this Rouse-like mode should occur between the relaxation times due to the transient
 16 crosslink breaking τ_X and the terminal time τ_{terminal} , where τ_{terminal} scales as $\tau_{\text{terminal}} \sim \tau_X \cdot N_P^2$.³¹
 17 Thus, for small N_P , the terminal flow occurs immediately after the transient bond breaking and
 18 the Maxwell type rheological response is obtained. In the case of the dual crosslink systems,
 19 the terminal flow is suppressed by the permanent chemical crosslinks, thus the dynamics of the
 20 gels with a small number of transient crosslinks can be measured and studied.

1 5. Conclusions

2 In this paper, the dynamics of the PVA-borax dual crosslink hydrogels as a function of the
3 chemical and physical crosslinker concentrations were studied. The constitutive theory which
4 predicts the stress-strain behaviors in both tensile and torsion tests, was used to determine a set
5 of four reduced parameters fitting both tests. The validity of the theory for the PVA dual
6 crosslink gels at various crosslinking ratios was confirmed. To systematically describe the
7 network dynamics and to provide molecular interpretation of the model parameters, we
8 discussed the crosslinkers concentration dependences of the elastic modulus, the characteristic
9 relaxation time and its distribution.

10 Evidently the main contribution of the transient crosslinkers is the time-dependent elastic
11 population having the elastic modulus of $\mu\bar{\gamma}_\infty \frac{t_B}{2-\alpha_B}$, with a large dissipation. With increasing
12 crosslinker concentration, this modulus increases. Besides this transient population of the
13 elasticity which was expected, we found a second population of longer lived elastically active
14 chains, measured as part of the low frequency modulus, $\mu\rho$, but higher than the modulus of the
15 corresponding chemical gel. This additional long live population of crosslinks increases with
16 transient crosslinker concentration and had not been previously identified for the PVA dual
17 crosslink gel. We speculate that these long live crosslinks are due to clustering of mobile
18 transient crosslinkers which can bind to any part of the chain. This result suggests that the
19 dissipative properties of the dual crosslink gels do not proportionally increase with the
20 transient crosslinker concentrations, and formation of such slower population needs to be
21 considered.

22 It is noteworthy that the concentration of transient crosslinks can influence the relaxation time.
23 We found that the network relaxation time τ_X obtained from the peak of G'' increases with
24 decreasing borax concentration. This crosslinker concentration dependence was interpreted to

1 be a consequence of an imperfect relaxation of the subchain due to bond reassociation faster
2 than the chain relaxation: before full relaxation of a chain, multiple transient crosslink breaking
3 and healing occur, increasing the apparent relaxation time τ_x . The average length of the
4 subchain between two physical crosslinks is thus a parameter as it determines the Rouse
5 relaxation time.

6 The scaling analysis with eq.16i,iii,iv suggests that the network relaxation time is inversely
7 proportional to the concentration of the elastically active crosslinks and to the square root of
8 the concentration of available binding sites. The studied dual crosslink gels have plenty of
9 binding sites for the mobile transient crosslinkers on the chains, and at the studied conditions
10 where the binding is far below the saturation, the binding site concentration remains high. This
11 results in a fast bond healing time and very low open transient crosslinker concentration. Thus
12 the dynamics are governed by the change in the total active crosslinker concentration, or by the
13 Rouse relaxation time.

14 Networks with less binding sites in fixed positions along the chain can be developed, by
15 copolymerizing monomers with and without ligand, for example. Such networks have a lower
16 binding site concentration and saturation can be easily achieved. Close to the saturation the
17 available binding site concentration decreases and concentration of open crosslinks and the
18 bond healing time would increase, resulting in crosslinking ratio dependences of the network
19 dynamics different from the current system. Systematic comparative studies are necessary for
20 complete understanding.

21 The distribution of the apparent relaxation times, expressed in the theory as the exponent α_B ,
22 corresponds to the distribution of the Rouse relaxation time. We showed that the exponent α_B
23 is a function of the number of the relaxation modes on a permanent chain having transient
24 crosslinks, expressed as the ratio of the high frequency modulus and the low frequency modulus,

1 $N_P = \left(\mu \bar{\gamma}_\infty \cdot \frac{t_B}{2 - \alpha_B} \right) / \mu \rho = [G'(\omega \rightarrow \infty) - G'(\omega \rightarrow 0)] / G'(\omega \rightarrow 0)$. We believe that the simple
2 relation between α_B and N_P expressed by eq.17 also proves that the Rouse dynamics of the
3 subchains determine the network relaxation. This result suggests also that the number of the
4 fitting parameter of the constitutive model can be reduced to three, as α_B is a function of the
5 other three parameters.

6

7 **Supporting Information**

8 Derivation of Equation 11. Fitting curves for tensile and torsion tests for all the dual crosslink
9 gels tested in this work.

10

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15

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6 the borax concentration in the feed of the solution in which the chemical gel is immersed. The ratio
7 of the volume of the solution to that of the chemical gel is 20 and the gel volume was kept constant,
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18 by intrachain crosslink, interchain crosslinking should become favored. Thus the ratio of interchain
19 crosslinks to intrachain crosslinks, $R_{\text{inter/intra}}$, scales with the blob size ξ as $R_{\text{inter/intra}} \approx \xi_l/\xi$. Since ξ
20 varies with the polymer concentration C as $\xi \sim C^{-5/4}$, we have $R_{\text{inter/intra}} \approx (C/C_l)^{5/4}$. Pezron et al.
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12 healing rate constant. The binding constant K_2 (M^{-1}) is equivalent to the ratio of the healing rate
13 constant to the breaking rate constant, $K_2 = \frac{k_{\text{heal}}}{k_{\text{break}}}$. Since we can define the breaking time t_B as
14 $t_b = \frac{1}{k_B}$, and the healing time t_H as $t_H = \frac{1}{k_H \cdot C_{\text{site}}}$, we have $\frac{t_B}{t_H} = \frac{k_H \cdot C_{\text{site}}}{k_B} = K_2 \cdot C_{\text{site}} = \frac{C_{\text{di}}}{C_{\text{open}}}$.

15