

# Unravelling the Mechanism of Viscoelasticity in Polymers with Phase-Separated Dynamic Bonds

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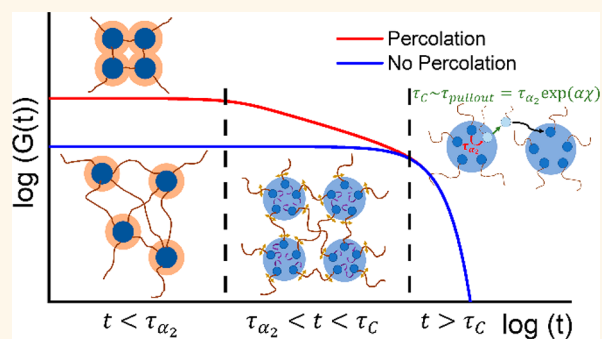
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**ABSTRACT:** Incorporation of dynamic (reversible) bonds within polymer structure enables properties such as self-healing, shape transformation, and recyclability. These dynamic bonds, sometimes refer as stickers, can form clusters by phase-segregation from the polymer matrix. These systems can exhibit interesting viscoelastic properties with an unusually high and extremely long rubbery plateau. Understanding how viscoelastic properties of these materials are controlled by the hierarchical structure is crucial for engineering of recyclable materials for various future applications. Here we studied such systems made from short telechelic polydimethylsiloxane chains by employing a broad range of experimental techniques. We demonstrate that formation of a percolated network of interfacial layers surrounding clusters enhances mechanical modulus in these phase-separated systems, whereas single chain hopping between the clusters results in macroscopic flow. On the basis of the results, we formulated a general scenario describing viscoelastic properties of phase-separated dynamic polymers, which will foster development of recyclable materials with tunable rheological properties.

**KEYWORDS:** associating polymers, network rearrangement, phase separation, interfacial layer, mechanical reinforcement, dynamic bonds



## INTRODUCTION

Polymers with dynamic bonds constitute an increasingly promising class of functional materials, where polymer chains are bonded together by reversible covalent<sup>1–3</sup> (e.g., vitrimers) or noncovalent (e.g., hydrogen and ionic bonds) interactions.<sup>4–8</sup> Because of the reversible nature of these transient interactions, it helps not only for developing functional materials such as self-healing ability and extreme stretchability,<sup>9,10</sup> shape memory,<sup>11,12</sup> and controlled stress relaxation but also makes them easy-to-process/recyclable.<sup>13,14</sup> The common interaction type is binary in nature, where two complementary groups form reversible bonds. The important parameter regarding this bond is the binding/dissociation energy along with the lifetime of the transient bonds,<sup>15</sup> which can be tuned based on the chemistry of the functional groups. At shorter time scale, material with these sticky bonds behaves as a network, whereas at time scale longer than that of the bond dissociation, the restriction to material flow is removed. However, this simple picture gets increasingly complicated in the presence of hierarchical structures within the material. Spider silk is one such example from the natural world, where H-bonds between adjacent  $\beta$ -strands of repetitive alanine/alanine-glycine moieties form nanocrystalline domains.<sup>16</sup>

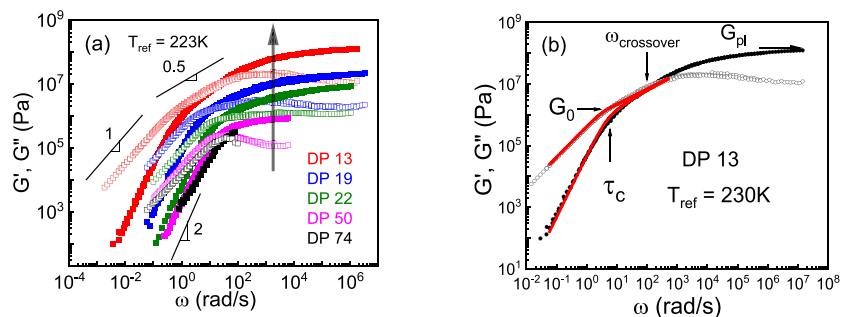
These  $\beta$ -sheet nanocrystals act as load-bearing cross-linking clusters within the glycine-rich amorphous matrix, endowing them with high elasticity and exceptional toughness/strength surpassing man-made fibers like Kevlar.<sup>17</sup>

Similar strategies have been employed in designing tough high-performance elastomers.<sup>18–20</sup> This type of nanophase separation can be achieved synthetically when the functional groups are immiscible with polymer matrix and phase-segregate in clusters, as observed in ionomers,<sup>21</sup> associating polymers,<sup>22–24</sup> and recently in vitrimers.<sup>25</sup> Clusters having higher glass transition or melting temperature compared to that of polymer matrix result in a prolonged rubbery plateau.<sup>24</sup> Moreover, recent studies<sup>26</sup> suggest that structural relaxation in these clusters controls viscosity and terminal relaxation of the polymers with phase separated associating groups. However, a

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**Figure 1.** (a) Shear modulus master curves for the telechelic PDMS-COOH measured at temperatures higher than second  $T_g$ . The arrow indicates the increased rubbery plateau value for shorter chains. Slope of 0.5 indicates Rouse-like regime, whereas regime with  $G' \approx \omega$  and  $G'' \approx \omega^2$  at lower frequencies indicate terminal flow behavior of these polymers. (b) Master curve of the shear modulus for DP 13 sample based on the reference temperature of 230 K. Solid and open symbols refer to  $G'$  and  $G''$  spectra, respectively. Fits based on the Rouse model are shown as red lines.  $\tau_c$  refers to terminal relaxation of the material. The values of the rubbery plateau modulus ( $G_{Pl}$ ) and shear modulus at terminal relaxation ( $G_0$ ) are indicated with arrows. The crossover of  $G'$  and  $G''$  is labeled as well, demonstrating that the estimation of the terminal relaxation time from the crossover is not accurate.

60 detailed microscopic understanding of how the network  
61 rearrangement occurs in the presence of phase separated  
62 clusters is still lacking. Simulations studies<sup>27</sup> suggested that  
63 structural rearrangements in this type of systems should go  
64 through fusion and dissociation of the clusters. This idea,  
65 however, was questioned in the recent experimental studies.  
66<sup>28,29</sup> Moreover, a clear separation between the time scale of  
67 cluster's structural relaxation time and rheological terminal  
68 mode was observed and remains unexplained.<sup>24,29</sup>

69 Experiments<sup>30–32</sup> also indicated the presence of a thin  
70 interfacial polymer layer with restricted mobility around these  
71 clusters, which also results in the elevated rubbery plateau  
72 modulus explained by the mechanical interfacial layer model  
73 (ILM). However, the interfacial layers might overlap forming a  
74 percolated network.<sup>33,34</sup> Since the mechanical ILM assumes  
75 independent fillers with interfacial layer,<sup>35</sup> the previous  
76 interpretation from mechanical ILM is questionable. For the  
77 polymer nanocomposites systems, the mechanical percolation  
78 model has already been utilized to describe the mechanical  
79 reinforcement in the presence of percolated network of the  
80 overlapping interfacial layers.<sup>36–38</sup> It has, however, never been  
81 used to study the analogous system like the phase separated  
82 associating polymers. Thus, the mechanism of network  
83 rearrangements and its effect on viscoelastic behavior in  
84 systems with clusters of the dynamic bonds remains a puzzle.  
85 Developing a microscopic understanding of viscoelasticity in  
86 polymers with clusters of dynamic bonds will help with rational  
87 design of materials with multifunctional properties and  
88 relatively easy recyclability.

89 To address this challenge, we provide a detailed analysis of  
90 the earlier studied model telechelic polymers with phase-  
91 separated functional end groups.<sup>24,39</sup> We demonstrate that the  
92 mechanical percolation model indeed explains well the  
93 unusually high rubbery plateau modulus in these materials.  
94 Most importantly, based on the analogy to block copolymers,  
95 we propose a mechanism of the network rearrangements via  
96 single chain hopping between clusters controlled by a  
97 thermodynamic energy barrier related to the immiscibility of  
98 the dynamic end groups and the polymer matrix. On the basis  
99 of these results, we propose a general scenario of viscoelasticity  
100 of polymers with clusters of dynamic bonds. The presented in-  
101 depth understanding provides design rules for developing  
102 functional materials with tunable viscoelastic properties.

## RESULTS AND DISCUSSION

103

The telechelic PDMS-COOH used in this work consists of a  
104 backbone with polydimethylsiloxane (PDMS) terminated with  
105 4-(propylamino)-4-oxobutanoic acid (COOH) (Figure S1).  
106 The telechelic PDMS-COOH has different degrees of  
107 polymerization (DP) of 13, 19, 22, 50, and 74.  
108

**Differential Scanning Calorimeters (DSC).** Each of the  
109 investigated PDMS-COOH samples shows two glass transition  
110 steps in their heat flow spectra. The one at lower temperature  
111 ( $\sim 150$  K) refers to the glass transition of the segmental  
112 motions of PDMS chains, while the one at higher temperature  
113 ( $\sim 200$  K) originates from the end-group motions within the  
114 clusters (Figure S3).<sup>24</sup>  
115

**X-ray Scattering.** Phase separation in PDMS-COOH has  
116 been verified through X-ray scattering in our previous  
117 publication.<sup>32</sup> The low- $q$  weak result at around  $0.1 \text{ \AA}^{-1}$   
118 indicates the phase separation. The similar X-ray scattering  
119 result was observed in DP 19 PDMS-COOH, which has not  
120 been studied before (Figure S4). The detailed analysis of X-ray  
121 scattering spectra<sup>32</sup> provides information on average center-to-  
122 center cluster distance ( $d$ ) and radius of the cluster ( $R_{cluster}$ )  
123 (Table S1). The nearest cluster surface-to-surface distance can  
124 be calculated through  $d_{IPS} = d - 2R_{cluster}$  (Table S1). With  
125  $R_{cluster}$ , the grafting density ( $n_e$ ) of PDMS chains on surface of  
126 the clusters can be calculated as  
127

$$n_e = \frac{V_{cluster}}{S_{cluster} V_{end}} = \frac{R\rho N_A}{3M_{end}} \quad (1) \quad 128$$

where  $M_{end}$  and  $\rho$  are the molecular weight and density of the  
129 associating chain end, respectively.  $N_A$  is the Avogadro's  
130 number. The grafting density was found to be  $\sim 1.7\text{--}1.9 \text{ nm}^{-2}$   
131 for all associating polymers (Table S1).  
132

**Rheology.** Small amplitude oscillatory shear was employed  
133 to measure linear viscoelastic behavior of the associating  
134 polymers. Shear modulus master curves were constructed  
135 (Figure 1a) by using time-temperature superposition (TTS)  
136 of the measured rheological spectra at different temperatures.  
137 The shift factor at various temperature used for TTS is shown  
138 in Figure S5. As was shown in our earlier studies,<sup>32,39</sup> the  
139 rubbery plateau modulus ( $G_{Pl}$ ) increases as the chain length of  
140 the polymer backbone decreases, reaching an unusually high  
141 level of  $G_{Pl} \approx 100 \text{ MPa}$  in the shortest chains with DP = 13  
142 (Figure 1a).  
143

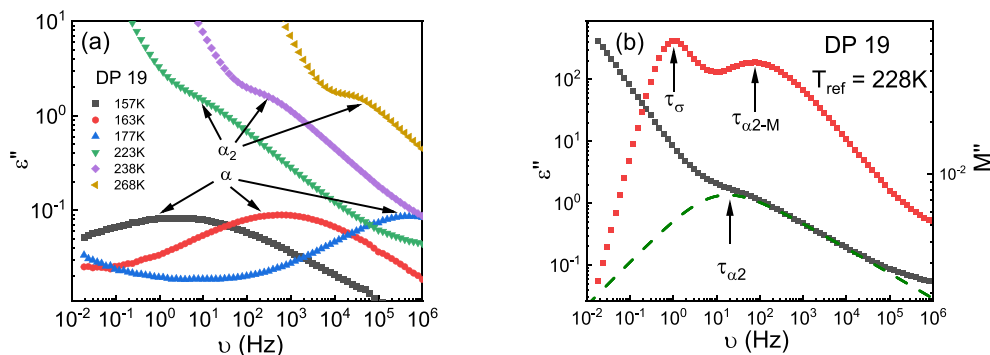


Figure 2. (a) Dielectric loss spectra for PDMS-COOH (DP 19) in the range of  $10^{-2}$  to  $10^6$  Hz. Loss peaks at low temperatures correspond to PDMS segmental motion ( $\alpha$ -relaxation), while at higher temperatures, sticker motion within the cluster is visible as a separate process, termed as  $\alpha_2$  process. (b) Comparison of  $\epsilon''$  spectra and  $M''$  spectra for telehelical PDMS-COOH with DP of 19 in which  $\tau_{\alpha_2}$ ,  $\tau_{\alpha_2-M}$ , and  $\tau_{\sigma}$  are labeled.

Terminal relaxation is observed at low frequencies where  $G'$  and  $G''$  increase with frequency as  $\omega^2$  and  $\omega^1$ , respectively. In addition, the samples with DP of 13, 19, and 22 exhibit an intermediate regime between the rubbery plateau and the terminal relaxation where both  $G'$  and  $G''$  follow power law behavior  $\sim \omega^\alpha$  with the exponent  $\alpha \approx 0.5$  (Figure 1a). In contrast, this regime is absent in spectra of samples with DP 50 and DP 74, where the terminal relaxation is reached right after the end of the rubbery plateau (Figure 1a). In our previous publication, the terminal relaxation time was determined from the crossover of  $G'$  and  $G''$ .<sup>24,39</sup> However, this method is only valid for the Maxwellian relaxation behavior. Because of the presence of the Rouse-like spectra in lower DP samples, the crossover is no longer able to provide the accurate estimation of the terminal relaxation time (Figure 1b). In such case, the longest Rouse time scale is more accurate. Thus, to acquire the accurate terminal relaxation time ( $\tau_c$ ) as well as its corresponding shear modulus level ( $G_0$ ), the Rouse model<sup>40</sup> is utilized to fit the shear modulus spectra:

$$G' = G_0 \sum_{j=1}^N \frac{\omega^2 \tau_j^2}{1 + \omega^2 \tau_j^2} \text{ and } G'' = G_0 \sum_{j=1}^N \frac{\omega \tau_j}{1 + \omega^2 \tau_j^2} \quad (2)$$

in which  $\tau_j = \frac{\tau_c}{j^2}$ . For PDMS-COOH with DP of 50 and 74,  $N$  is chosen to be 1, which corresponds to the Maxwell relaxation. However, for PDMS-COOH with DP of 13, 19, and 22,  $N$  is chosen to be an arbitrary number to fit the region of parallel decrease of the  $G'$  and  $G''$  with slope of 0.5. The proposed fit describes well the shear modulus spectra (see, e.g., Figure 1b for PDMS-COOH with DP of 13) and provides estimates of both the  $G_{pl}$  and  $G_0$  as well as  $\tau_c$ .

**Broadband Dielectric Spectroscopy (BDS).** To analyze dynamics in the studied systems, we employed dielectric spectroscopy that revealed two major dielectric processes.<sup>24,39</sup> As a representative example, dielectric loss spectra ( $\epsilon''$ ) for the sample with DP 19 at several temperatures are shown in Figure 2a. Dielectric loss spectra for the rest of the samples are presented in Figure S6a–d. The process at lower temperatures is PDMS segmental motion ( $\alpha$ -relaxation), while the process at higher temperatures is ascribed to motion of associating groups in the clusters, termed as  $\alpha_2$ -relaxation.<sup>24</sup>

To compare rheological and dielectric data, the latter should be converted to the dielectric modulus  $M^*(\omega)$ :<sup>41,42</sup>

$$M^*(\omega) = \frac{1}{\epsilon(\omega)} = M'(\omega) + iM''(\omega) \quad (3)$$

$M''$  spectra exhibit an additional dielectric process at lower frequencies (Figure 2b), which originate from conductivity relaxation ( $\tau_\sigma$ ).<sup>43,44</sup> We also noticed that the time scale of  $\alpha_2$  relaxation process from  $M''$  ( $\tau_{\alpha_2-M}$ ) is faster than that from  $\epsilon''$  spectra ( $\tau_{\alpha_2}$ ). This is expected, as the relationship between characteristic relaxation time from  $M''$  spectra ( $\tau_M$ ) and  $\epsilon''$  spectra ( $\tau_\epsilon$ ) can be expressed by<sup>45</sup>

$$\tau_M = \frac{\epsilon_{inf}}{\epsilon_s} \tau_\epsilon \quad (4)$$

in which  $\epsilon_s$  and  $\epsilon_{inf}$  indicate the dielectric constant in the limit of high and low frequencies. Thus,  $\tau_{\alpha_2-M}$  is shorter than  $\tau_{\alpha_2}$  as was already emphasized in the literature.<sup>15,32</sup>

To acquire the characteristic relaxation time from modulus spectra, the  $M''$  spectra were fit based on one Havriliak-Negami (HN) function plus one Debye-like process for conductivity relaxation:

$$M''(\omega) = \text{Im} \left\{ \frac{\Delta M_{\alpha_2}}{(1 + (2\pi\omega\tau_{HN-M})^{\beta_M})^{\gamma_M}} + \frac{\Delta M_\sigma}{1 + 2\pi i\omega\tau_\sigma} \right\} \quad (5)$$

in which  $\Delta M_{\alpha_2}$  and  $\Delta M_\sigma$  are the “modulus strength” of  $\alpha_2$  process and conductivity process.  $\tau_{HN-M}$  and  $\tau_\sigma$  are the HN relaxation time for  $\alpha_2$  process and the conductivity relaxation time from dielectric modulus.  $\beta_M$  and  $\gamma_M$  are the stretching parameters for the  $\alpha_2$  process. The relaxation time corresponding to the peak position of  $\alpha_2$  process in  $M''$  spectra is calculated using<sup>46</sup>

$$\tau_{\alpha_2-M} = \tau_{HN-M} \left[ \sin \left( \frac{\beta_M \pi}{2 + 2\gamma_M} \right) \right]^{-1/\beta_M} \left[ \sin \left( \frac{\beta_M \gamma_M \pi}{2 + 2\gamma_M} \right) \right]^{1/\beta_M} \quad (6)$$

**Mechanical Percolation Model.** Our previous studies revealed the existence of an interfacial polymer layer around the phase-separated clusters with a thickness  $l_{int} \approx 0.8\text{--}0.9$  nm regardless of PDMS backbone length.<sup>32</sup> This small thickness was explained by the small radius of the phase separated clusters,  $R_{cluster} \approx 1.4\text{--}1.6$  nm.<sup>32</sup> When the distance between clusters surfaces  $d_{IPS} < 2l_{int}$ , the interfacial layers overlap with

216 each other, forming a percolating network. According to Table  
 217 S1, the percolation of the interfacial regions can happen in  
 218 PDMS-COOH with DP of 13, 19, and 22, while the interfacial  
 219 layers are expected to be fairly separated in PDMS-COOH  
 220 with DP of 50 and 74 (Figure 3). The critical volume fraction  
 221 of the cluster,  $(f_e)_c$  for percolation is estimated as  $d_{IPS} \approx 2l_{int}$   
 222 and appears in the range  $\sim 13.5 \pm 1.2$  wt %.

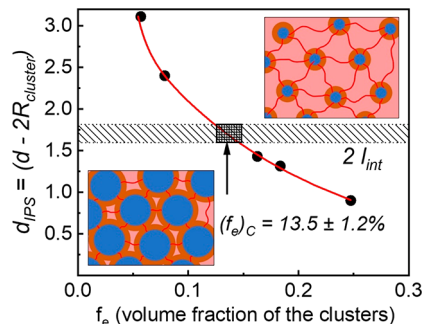


Figure 3.  $d_{IPS}$  as a function of  $f_e$ . Range of  $2l_{int}$  value shown as a gray area. The box area indicates the estimated range of percolation threshold,  $(f_e)_c$ , when  $d_{IPS} \approx 2l_{int}$ . Above the percolation threshold, interfacial layers overlap to form a percolated network, whereas below the threshold, they are well separated. Blue circles represent the clusters of functional groups, which are surrounded by interfacial layers (orange) and linked by PDMS chains (red).

223 This analysis reveals that indeed interfacial layers form a  
 224 percolating structure in systems with low DP, and the  
 225 mechanical percolation model needs to be used to describe  
 226 the elevated mechanical modulus observed in these samples.  
 227 According to this model,<sup>47</sup> a composite modulus is expressed  
 228 as

$$G_c = \frac{(1 - 2\psi + \psi X_r)G_s G_r + (1 - X_r)\psi G_r^2}{(1 - X_r)G_r + (X_r - \psi)G_s} \quad (7)$$

230 in which  $G_r$  is the shear modulus of the rigid phase.  $G_s$  is the  
 231 shear modulus of the matrix (in this case PDMS matrix, which  
 232 can be estimated from the classical rubber elasticity theory).  $X_r$   
 233 is the volume fraction of the overall rigid phase.  $\psi$  is the  
 234 volume fraction of the spanning rigid phase formed in the  
 235 percolated network through the overlapping of the interfacial  
 236 layer and defined as

$$\psi = \begin{cases} 0, & X_r < X_c \\ X_r \left( \frac{X_r - X_c}{1 - X_c} \right)^b, & X_r \geq X_c \end{cases} \quad (8)$$

238 Here  $X_c$  is the volume fraction of the rigid phase at the  
 239 percolation threshold;  $b$  is the percolation exponent character-  
 240 izing the rate of the percolation structure formation with  $X_c$ .

241 We assume for simplicity that the clusters and their  
 242 interfacial layers form a single rigid phase with volume fraction  
 243  $X_r = \varphi_{cluster} + \varphi_{int}$ . The mechanical percolation model (eqs 7  
 244 and 8) successfully describes the mechanical reinforcements in  
 245 studied polymers (Figure 4). The value of  $X_r$  at the percolation  
 246 threshold is found to be 56.5%, which corresponds to the  
 247 critical volume fraction of the cluster,  $(f_e)_c \approx 14.8\%$ . The  
 248 obtained value is in good agreement with the value estimated  
 249 assuming an ordered cubic arrangement of the clusters (Figure

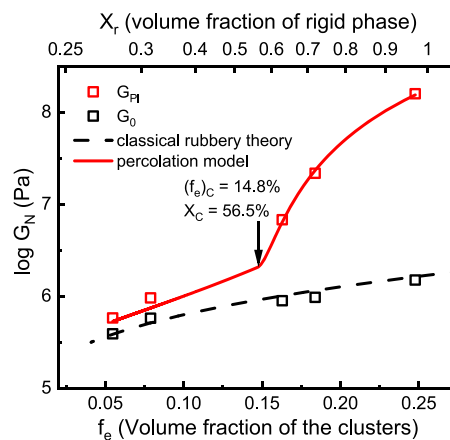


Figure 4. Variation of  $G_{PL}$  (red squares) and  $G_0$  (black squares) as a function of  $f_e$  and  $X_r$ . Red line shows the fitting based on the mechanical percolation model (eqs 7 and 8). Black dashed line indicates the prediction from classical rubber elasticity theory. The arrow indicates the estimated from the fit percolation threshold.

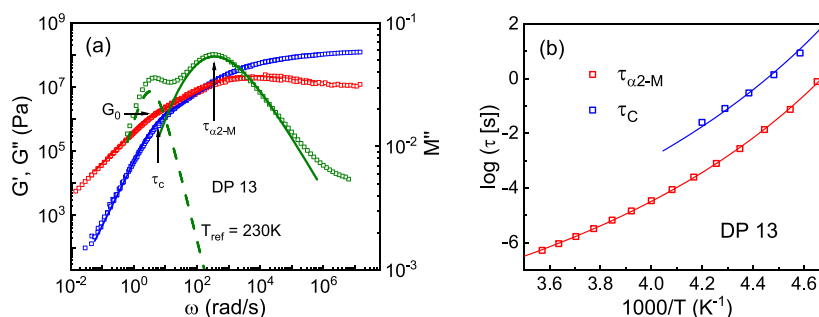
4). The critical exponent  $b$  obtained from the fit is  $\sim 1.7$ , which  
 also agrees with the prediction from scalar elastic model in 3  
 dimensions developed by de Gennes.<sup>48</sup> Experimental inves-  
 tations of percolation in various systems including organic  
 polymer blends, polymer gels, and nanocomposite indicate the  
 exponent  $b$  ranges from 1.6 to 2.2.<sup>49–54</sup> The model also  
 provides the estimates of the shear modulus of the rigid phase,  
 $G_r \approx 177$  MPa.

The obtained  $G_r$  value agrees well with the estimates of the  
 shear modulus of the rigid phase using the two-phase model  
 (TPM) (Table 1). The two phases are clusters and the

Table 1. DP, Volume Fraction of Clusters  $\varphi_{cluster}$ , Volume Fraction of the Interfacial Layer  $\varphi_{int}$ , Volume Fraction of Clusters in Rigid Phase  $\varphi_{cluster,TPM}$ , Volume Fraction of Interfacial Regions in Rigid Phase  $\varphi_{int,TPM}$  and Overall Shear Modulus of Rigid Phase Estimated Using TPM for PDMS-COOH Associating Polymers

material	DP	$\varphi_{cluster}$ (%)	$\varphi_{int}$ (%)	$\varphi_{cluster,TPM}$ (%)	$\varphi_{int,TPM}$ (%)	$G_r$ (TPM) (MPa)
PDMS-COOH	13	24.7	71.8	25.6	74.4	171
	19	18.4	59.1	23.7	76.3	164
	22	16.3	40.8	28.5	71.5	183
	50	7.9	26.6	22.9	77.1	161
	74	5.7	19.7	22.4	77.6	159

interfacial layer. The necessary parameters to estimate the  
 shear modulus using TPM are shear modulus, volume fraction,  
 and Poisson ratio of both clusters and the interfacial layer. The  
 modulus of the interfacial layer was estimated to be  $\sim 100$   
 MPa.<sup>32</sup> The Poisson's ratio of the interfacial layer (which  
 consists of PDMS segments) is taken from literature<sup>55</sup> based  
 on the PDMS values. For clusters, the modulus and the  
 Poisson's ratio are assumed to be 3 GPa and 0.33, respectively,  
 which are typical values for glassy hydrogen-bonded systems  
 such as glycerol.<sup>56</sup> The volume fraction of cluster and  
 interfacial layer in the rigid phase were estimated as  
 $\varphi_{cluster,TPM} = \frac{\varphi_{cluster}}{\varphi_{cluster} + \varphi_{int}}$  and  $\varphi_{int,TPM} = \frac{\varphi_{int}}{\varphi_{cluster} + \varphi_{int}}$ , respectively,  
 where values of  $\varphi_{cluster}$  and  $\varphi_{int}$  for PDMS-COOH with DP of  
 13, 22, 50, and 74 were taken from previously published



**Figure 5.** (a) Comparison between the shear modulus (red and blue symbols) and the dielectric loss modulus spectra (green symbols) for PDMS-COOH with DP of 13 sample at 230 K. Terminal relaxation time scale ( $\tau_c$ ) and  $\alpha_2$ -relaxation time scale ( $\tau_{\alpha_2-M}$ ) (arrows) are separated by more than one order of magnitude. The low-frequency process (dashed line) in the dielectric modulus spectrum corresponds to conductivity relaxation process with a Debye-like shape. (b) Temperature dependence of the two time scales (symbols) and their fit based on eq 12 and eq 11 (lines).

work,<sup>32</sup> and  $\varphi_{int}$  of DP 19 PDMS-COOH was estimated through

$$\varphi_{int} = \varphi_{cluster} \left[ \left( \frac{l_{int}}{R_{cluster}} + 1 \right)^3 - 1 \right] \quad (9)$$

by using  $l_{int} = 0.85$  nm, the value estimated in our previous studies.<sup>32</sup> The results are in good agreement with the value from mechanical percolation model ( $\sim 177$  MPa), validating that the percolation model explains well the mechanical reinforcement in the studied samples.

**Viscoelastic Behavior near Terminal Relaxation.** It is interesting that in systems with no percolation (i.e., with DP of 50 and 74), the terminal relaxation demonstrates Maxwellian behavior, that is, the rubbery plateau stops at the terminal relaxation. In contrast, the rubbery plateau in systems with percolating rigid regions (i.e., with DP of 13, 19, and 22) first decreases with a power law before reaching the terminal relaxation (Figure 1a). Consequently, the moduli  $G_{pl}$  and  $G_0$  (eq 2) appear to be comparable for nonpercolated systems, while  $G_{pl}$  is much higher than  $G_0$  in percolating systems, and the difference increases with decreases in samples DP (Figure 4). Analysis of these data revealed that  $G_0$  obtained from the fit for all the sample follows the classical rubber elasticity<sup>57</sup> predictions for a given length of the PDMS chains (Figure 4), demonstrating that the mechanical reinforcement actually vanishes at terminal relaxation.

To study the viscoelastic properties in phase separated associating polymers, we compared shear modulus spectra and dielectric  $M''$  spectra (Figure 5a). It is evident that  $\tau_c$  is significantly slower than  $\tau_{\alpha_2-M}$ , indicating that motion of stickers inside the clusters is not sufficient for terminal relaxation. Interestingly, the shear modulus in percolating systems starts to decrease from the rubbery plateau level at the time scale comparable to  $\tau_{\alpha_2-M}$  (Figure 5a), suggesting that the stickers motions within the clusters lead to the softening of the modulus down to the level predicted from classical rubber elasticity. Indeed, when chain ends in clusters are unable to move, the whole system is similar to nanoparticles with extremely high grafting density  $\sim 1.7$ – $1.9$  chains/nm<sup>2</sup> (Table S1). This grafting density is  $\sim 3$ -times higher than in usual polymer grafted nanoparticles, leading to strong crowding and stretching of the chains in the interfacial layer. Stretching of the chain is supported by larger population of the gauche states found from wide-angle X-ray scattering results.<sup>32</sup> All these

factors strongly hinder bending of the PDMS segments in the interfacial layer and lead to high modulus. However, when chain ends start to move inside the clusters, the PDMS segments in the interfacial layer can be easily rearranged and change their conformations under external force, and the macroscopic deformation is easier to reach. This results in a gradual softening of the polymer interfacial layer, which is demonstrated through the parallel decrease of the  $G'$  and  $G''$  with decrease in frequency. This softening reaches the modulus level expected from the rubber elasticity at the time of the terminal relaxation. Moreover, similar temperature dependences of both  $\tau_{\alpha_2-M}$  and  $\tau_c$  (Figures 5b and S7) suggest that dynamics in the clusters might act as a precursor for the macroscopic rearrangement of the network.

**Mechanism of Network Rearrangement.** The mechanism of network rearrangement in phase separated associating polymers remains a puzzle. It is obvious that the network rearrangement should involve exchange of the stickers between different clusters.<sup>27,58</sup> On the basis of computer simulations, Amin et al. suggested that exchange should go through a merge of different clusters.<sup>27</sup> This mechanism was questioned by Mordvinkin et al.,<sup>28,29</sup> where telechelic poly(isobutylene) (PIB) with functional end groups was studied. These systems, like the polymers studied here, have well-separated clusters, and merging of these clusters is not feasible due to the presence of multiple chains between the clusters. These systems, however, are similar to phase separating triblock copolymers. In phase separating triblock copolymers, network rearrangement process is dominated by a chain pullout process, which needs to overcome the free energy penalty from the immiscibility of different blocks.<sup>58–60</sup> In other words, the block in the phase separated cores needs to be pulled out and diffuse to another phase-separated core to complete the rearrangement process. According to refs 61–63, the pullout time scale is expressed as

$$\tau_{pullout} = \tau_{Rouse} \exp(\alpha\chi N_{core}) \quad (10)$$

in which  $\tau_{Rouse}$  is Rouse relaxation time of the block inside the phase separated cores.  $\chi$  is the Flory–Huggins parameter.  $N_{core}$  is the number of Kuhn segments of the block forming phase-separated cores.  $\alpha$  is a constant in the order of unity. We hypothesize that the similar mechanism controls bond rearrangements in the studied telechelic systems, and the free energy barrier to “chain end pullout” process determines the network rearrangement process.

361 Borrowing the idea of chain exchange kinetics in block  
 362 copolymer micelles,<sup>58–60,64</sup> relationship between  $\tau_c$  and  $\tau_{\alpha_2-M}$   
 363 can be expressed as

$$\tau_c(T) = \tau_{\alpha_2-M}(T) \exp\left(\frac{E_a}{RT}\right) = \tau_{\alpha_2-M}(T) \exp(\alpha\chi N_{core}) \quad (11)$$

364 in which the activation energy barrier,  $E_a$ , is related to the  
 365 thermodynamic penalty for the sticker to be placed in the  
 366 polymer matrix  $\sim\alpha\chi N_{core}$ . To estimate the activation barrier  
 367 from the experimental result,  $\tau_{\alpha_2-M}(T)$  was fit to the Vogel–  
 368 Fulcher–Tammann (VFT) eq (Figure 5b, red line):  
 369

$$\tau_{\alpha_2-M}(T) = \tau_0 \exp\left(\frac{B}{T - T_0}\right) \quad (12)$$

371 Here  $\tau_0$ ,  $B$ , and  $T_0$  are the VFT fit parameters. Then  $\tau_c(T)$  was  
 372 fitted using eq 11, in which  $\tau_{\alpha_2-M}$  was substituted by the VFT  
 373 equation, with the energy barrier  $E_a$  as the only free fit  
 374 parameter (Figure 5b). The fitting results revealed the average  
 375 activation energy to be  $\sim 6.6$  kJ/mol (Figure 6). Strong  
 376 deviation in the case of the sample with DP 74 might be caused  
 377 by crystallization that strongly limited the studied temperature  
 378 range.

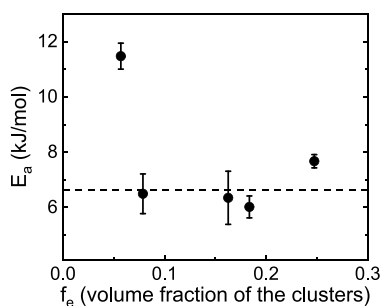


Figure 6. Estimated energy barrier for single sticker “pullout” into PDMS matrix. The solid dashed line indicates the average activation energy for this process. Value for the lowest  $f_c$  data is not reliable due to possible sample crystallization.

379 The obtained activation energy can be compared to the  
 380 expected  $\sim\alpha\chi N_{core}$ .  $N_{core}$  of the end group is 1, and the Flory–  
 381 Huggins parameter,  $\chi$ , can be estimated from the solubility  
 382 parameters ( $\delta$ ) and molar volume of the chain end instead of  
 383 the molar volume of a copolymer block:<sup>65</sup>

$$\chi = \frac{(\delta_{end} - \delta_{PDMS})^2 V_{end}}{RT} \quad (13)$$

The solubility parameter of the PDMS backbone  $\delta_{PDMS}$  is 7.3  
 cal<sup>1/2</sup> cm<sup>-3/2</sup>.<sup>66</sup> The solubility parameter of the chain end  
 (COOH),  $\delta_{end}$ , is estimated to be 11.86 cal<sup>1/2</sup> cm<sup>-3/2</sup> via  
 Hansen solubility parameter (HSP)<sup>67</sup> approach, which divides  
 the solubility parameter into three partial components:  
 dispersion, polarity, and hydrogen-bonding (detailed method  
 is mentioned in the Supporting Information). The molar  
 volume of chain ends  $V_{end}$  is calculated using  $V_{end} = \frac{M_{end}}{\rho_{end}}$ , where  
 the molecular weight of chain ends  $M_{end}$  is 158 g/mol, and the  
 density of chain ends is assumed to be the same as that of  
 glycerol,  $\rho_{end} = 1.26$  g/cm<sup>3</sup>. Thus,  $(\delta_{end} - \delta_{PDMS})^2 V_{end}$   
 is estimated to be  $\sim 11$  kJ/mol, in reasonable agreement with the  
 experimentally estimated  $E_a$  assuming  $\alpha$  value of  $\sim 0.6$ . The  
 value of  $\alpha$  close to 0.6 has been reported in several studies of  
 chain exchange kinetics in different block copolymer  
 micelles.<sup>60,68,69</sup> Thus, the single chain hopping mechanism  
 provides reasonable estimates of the energy barrier controlling  
 terminal relaxation in polymers with phase separated stickers.

On the basis of these results and analysis, we propose the  
 following mechanism of the terminal relaxation in polymers  
 with phase separated reversible bonds (stickers). Network  
 rearrangements require mobility of stickers in the clusters and  
 a sticker escape from the cluster requires to overcome an  
 energy barrier controlled by miscibility of stickers in a polymer  
 matrix. Once the sticker escaped from the cluster, it will diffuse  
 through the polymer matrix to another cluster with a time scale  
 of  $\tau_{diffusion}$ , which will be mainly governed by Rouse  
 subdiffusive motion, that is,  $\tau_{diffusion} \approx \tau_\alpha \left(\frac{d}{l_k}\right)^4$ , here  $d$  is the  
 distance between clusters ( $\sim 5$  nm, Tables S1) and  $l_k$  is the  
 Kuhn segment length of PDMS ( $\sim 1$  nm). This provides  
 estimates of  $\tau_{diffusion} \approx 10^3 \tau_\alpha$ . At the onset of second  $T_g$ , where  
 stickers can move inside the clusters,  $\tau_\alpha$  is  $\sim 10^{-9}$  s (Figure  
 S6e) and  $\tau_{diffusion}$  is  $\sim 10^{-6}$  s. This time is many orders faster  
 than terminal relaxation time at the same temperatures. Thus,  
 we can safely assume that sticker escape from the cluster is the  
 rate-determining step in the single chain hopping process. This  
 mechanism is similar to that describing the network rearrange-  
 ment of Butyl ionomer.<sup>70</sup> However, we introduce the  
 microscopic mechanism of these rearrangements and identify  
 the energy barrier controlling the sticker hopping process. This  
 mechanism also explains the difference between the time scale

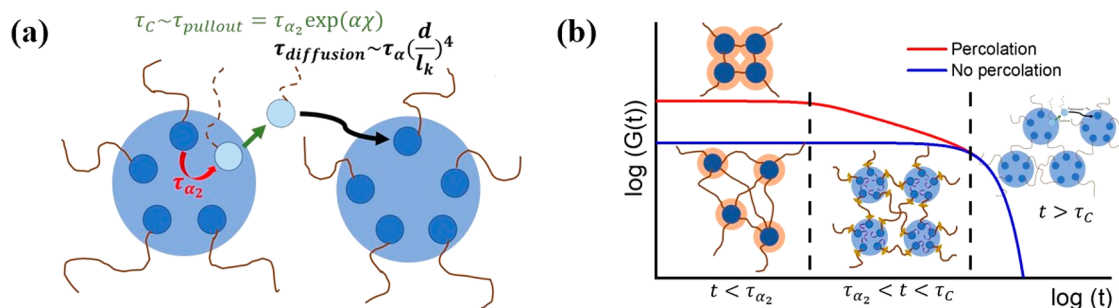


Figure 7. (a) Cartoon of a single chain exchange process between two clusters, which leads to a macroscopic rearrangement of the network. (b) Qualitative picture of the shear modulus variation with time for a phase-separated associated polymer network with percolated interfacial layers (red line) and with no percolation (blue line). Dashed lines mark two important time scales of the system:  $\tau_{\alpha_2}$ , relaxation in clusters of dynamic bonds; and  $\tau_c$ , terminal relaxation defined by the network rearrangement time.

426 of network rearrangement and the dynamic bonds motion  
427 inside the clusters. The proposed mechanism is consistent with  
428 the recent NMR studies<sup>28,29</sup> revealing that single chain  
429 relaxation is responsible for the terminal relaxation in the  
430 associating polymer with phase separation. These studies of  
431 telechelic PIBs with barbituric acid end groups and with  
432 thymine end groups also revealed that cluster relaxation  
433 process observed in dielectric spectra is faster than the terminal  
434 relaxation, and the ratio of these time scales depends on  
435 chemistry of the stickers<sup>29</sup> (Figure S9). Following the  
436 proposed mechanism, we estimated the energy barrier  
437 (through eq 11) to be  $E_a \approx 16\text{--}17$  kJ/mol for more polar  
438 barbituric acid end groups and  $\sim 9$  kJ/mol for less polar  
439 thymine end group (Table S2). Moreover, these values agree  
440 with estimates of  $(\delta_{end} - \delta_{PDMS})^2 V_{end}$  ( $\sim 26$  kJ/mol for  
441 barbituric acid end group and  $\sim 13$  kJ/mol for thymine end  
442 group) assuming  $\alpha \approx 0.6$  (see Supporting Information). Thus,  
443 the proposed mechanism also provides good understanding for  
444 the network rearrangement in other systems with phase-  
445 separated stickers.

446 **General Molecular Picture.** On the basis of analysis of the  
447 presented above results, we propose a general picture of  
448 viscoelasticity in polymers with phase separated dynamic  
449 bonds (Figure 7b). Functional end-group clusters possess a  
450 higher  $T_g$  value than the polymer matrix, and their dynamics is  
451 governed by a time scale of structural relaxation in these  
452 clusters,  $\tau_{\alpha_2}$ . At times  $t < \tau_{\alpha_2}$ , clusters are glassy and control the  
453 rubbery plateau level. In such case, not only chain ends are  
454 fixed but also the grafting density is extremely high, resulting in  
455 chains crowding and stretching in an interfacial layer around  
456 these clusters. These severely restrict segmental mobility and  
457 chain bending (similar to polymer grafted nanoparticles),  
458 leading to a much higher elastic modulus.<sup>32,39</sup> In the absence of  
459 percolation of the interfacial polymer regions, the mechanical  
460 reinforcement from the interfacial layer is small, and  
461 mechanical strength of the associating polymer is mostly  
462 defined by the rubber elasticity of network structure cross-  
463 linked by the clusters. However, in a case where interfacial  
464 regions overlap, significant mechanical reinforcement is  
465 observed, which can be ascribed to a percolation phenomenon  
466 (Figure 7b). On time scale  $\tau_{\alpha_2} < t < \tau_{\alpha_1}$  stickers become mobile  
467 within the clusters, and even if the grafting density is high, the  
468 segments in the vicinity of clusters can easily rearrange and  
469 change conformations. This leads to a subsequent decrease of  
470 the mechanical modulus in the interfacial layer down to the  
471 level expected in the rubber elasticity theory. As a result, the  
472 macroscopic modulus level drops down significantly in the case  
473 of percolated network as the effect of percolation fades away  
474 with the gradual decreasing of the modulus in the interfacial  
475 layer. When there is no percolation, the decrease in the shear  
476 modulus is negligible until topological reorganization of  
477 network occurs at the terminal relaxation time ( $\tau_c$ ). At  $t > \tau_c$ ,  
478 sticky ends start to move out of the cluster overcoming the free  
479 energy barrier due to their immiscibility with the polymer  
480 matrix and subsequently diffuse to another cluster. Through  
481 this single chain exchange process, macroscopic stress  
482 relaxation happens within the network.

## 483 CONCLUSIONS

484 In this study, we investigated telechelic PDMS with functional  
485 groups phase-separating in clusters due to their immiscibility  
486 with the polymer backbone. We demonstrated that mechanical

percolation model describes well the strong mechanical  
487 reinforcement observed in these systems. Although the result  
488 is similar to what we achieved earlier using mechanical ILM,<sup>32</sup>  
489 the percolation model is more appropriate to explain the  
490 mechanical reinforcement since interfacial layers overlap in  
491 most of the studied samples. Moreover, our results and analysis  
492 question the proposed earlier mechanism<sup>27</sup> of network  
493 relaxation through a merger of phase-separated clusters.  
494 Instead, we propose a chain-hopping mechanism of network  
495 rearrangement borrowed from the field of block copolymer. It  
496 provides a reasonably good description of the presented data  
497 even on a quantitative level. This mechanism also describes  
498 earlier data on telechelic PIB.<sup>29</sup> Finally, we formulate a general  
499 molecular picture describing the viscoelastic behavior of  
500 associating polymers. When phase separated clusters are  
501 frozen, the system behaves as a permanent network, which  
502 show strong mechanical reinforcement depending on whether  
503 there is percolation. Then the softening of the interfacial layer  
504 occurs upon the motion of functional groups inside the phase  
505 separated clusters, followed by the network rearrangement  
506 controlled by additional energy barrier defined by immiscibility  
507 of stickers and polymer matrix.  
508

The presented analysis and the proposed mechanism  
509 provide a detailed understanding of the viscoelastic behavior  
510 of polymers with phase-separated reversible bonds. These  
511 mechanisms should work not only for telechelic associating  
512 polymers but also for any associating polymer having phase  
513 separating dynamic bonds. The developed understanding is of  
514 paramount importance for rational design of advanced  
515 materials with enhanced mechanical properties, and better  
516 recyclability.  
517

## 518 METHODS

**Synthesis of PDMS-COOH Polymers.** Synthesis of PDMS-  
519 COOH polymers was described in detail in our previous  
520 publication.<sup>24,39</sup> The synthesis route is shown in Scheme 1 in Xing  
521 et al.<sup>24</sup> DP 19 PDMS-COOH was synthesized in this work. Five  
522 grams of PDMS-NH<sub>2</sub> (5 mmol, Gelest Inc. DMS-A11) was added  
523 into a flame-dried 100 mL round-bottom flask, and then 2 g of  
524 succinic anhydride (20 mmol) was also added followed by the  
525 addition of 1.518 g of triethylamine (15 mmol), 0.611 g of 4-  
526 dimethylaminopyridine (5 mmol), and 30 mL tetrahydrofuran  
527 (THF). The reaction was conducted under an N<sub>2</sub> atmosphere at 40  
528 °C for 2 days. After the reaction was completed, THF was removed by  
529 rotary evaporation. Ten milliliters of 1 M hydrochloric acid was  
530 added, a total amount of 50 mL of dichloromethane (DCM) was  
531 utilized to extract the product from the aqueous solution three times.  
532 The organic layer was collected and was removed by rotary  
533 evaporation. The final product was obtained and dried in a vacuum  
534 oven to remove all residual solvents. <sup>1</sup>H NMR was utilized to confirm  
535 the final product with CDCl<sub>3</sub> as solvent. The chemical structure and  
536 the <sup>1</sup>H NMR spectra analysis is shown in Figure S2.  
537

**Differential Scanning Calorimetry (DSC) Measurements.** DSC  
538 was employed to probe the glass transition temperature ( $T_g$ ) of  
539 PDMS-COOH using a Q2500 DSC equipment from TA Instruments.  
540 The samples were dried in a vacuum oven at 333 K overnight before  
541 being placed into DSC pans. The samples were first equilibrated  
542 isothermally at 363 K for 10 min to remove the thermal history before  
543 being quenched to 113 K (to avoid crystallization). After equilibration  
544 for 10 min, the samples were heated up to 293 K with a rate of 10 K/  
545 min. This procedure was repeated twice for each sample to ensure  
546 repeatability.  
547

**X-ray Scattering.** X-ray scattering spectra for DP 13, 22, 50, and 74  
548 PDMS-COOH, as well as the reference sample PDMS-CH<sub>3</sub>, were  
549 measured previously. The procedure was described in detail in ref 32.  
550 The DP 19 PDMS-COOH was measured on XEUS 3.0 (Xenocs, 551

552 France) equipped with a Cu  $K\alpha$  microfocus source and a Pilatus 300k  
553 detector (Dectris, Switzerland). The scattering vector ( $q$ ) was  
554 calibrated by a silver behenate standard material. The distance  
555 between sample and detector was 0.9 m and 0.55 m for SAXS and  
556 WAXS, respectively. The sample was squeezed into a capillary tube  
557 made of quartz glass with diameter 1.5 mm and wall thickness 0.01  
558 mm. Then the capillary was placed perpendicularly to the X-ray beam.  
559 The measurement mentioned above was also done on the empty  
560 capillary to subtract the background. X-ray measurements were  
561 performed at room temperature.

562 **Broadband Dielectric Spectroscopy (BDS).** BDS in the frequency  
563 range from  $10^{-2}$  to  $10^6$  Hz was measured utilizing a Novocontrol  
564 system that includes an Alpha-A impedance analyzer and a Quatro  
565 Cryosystem temperature control unit. DP 13, 22, 50, and 74 PDMS-  
566 COOH were placed into a parallel-plate dielectric cell made of  
567 sapphire and invar steel with an electrode diameter of 12 mm, and  
568 capacitance 20 pF with an electrode separation of 50  $\mu\text{m}$ . DP 19  
569 PDMS-COOH was placed into a parallel plate dielectric cell made of  
570 sapphire and invar steel with an electrode diameter of 10 mm, and  
571 capacitance 3.3 pF with an electrode separation of 210  $\mu\text{m}$ . To  
572 prevent crystallization, all samples were quenched from room  
573 temperature to about 113 K and reheated to 10 K below the  $T_g$   
574 before the measurements. All the spectra were measured on heating.  
575 After each temperature increase, the samples were equilibrated for 10  
576 min to reach thermal stabilization within 0.1 K.

577 **Small-Amplitude Oscillatory Shear (SAOS) Measurement.** SAOS  
578 measurement was utilized to probe the viscoelastic properties of  
579 telechelic PDMS-COOH through a strain-controlled mode of the  
580 AR2000ex (TA Instruments) with an angular frequency range from  
581  $10^2$  to  $10^{-1}$  rad/s using parallel plate geometry with a disk diameter of  
582 4 mm at a variety of temperatures range from second  $T_g$  to  
583 temperatures that the sample can flow freely. The strain amplitude  
584 during the measurement was chosen to be in the range from 0.2% to  
585 5% depending on the modulus level at different temperatures.

## 586 ASSOCIATED CONTENT

### 587 **SI** Supporting Information

588 The Supporting Information is available free of charge at  
589 <https://pubs.acs.org/doi/10.1021/acsnano.2c00046>.

590 Chemical structure; DSC results; X-ray scattering  
591 spectrum; structural information; rheological shift  
592 factors; dielectric spectra; energy barrier estimation;  
593  $\delta_{end}$  estimation; activation energy estimation (PDF)

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## Notes

The authors declare no competing financial interest.

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