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The scale-up of electrochemically mediated atom transfer radical polymerization without deoxygenation

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ARTICLE INFO

Keywords: Scale-up Electrochemistry ATRP Polymers Oxygen Pyruvate

ABSTRACT

The scale-up of Atom Transfer Radical Polymerization (ATRP) from 15 mL to 15 L (scale-up factor 1000) by galvanostatic simplified electrochemically mediated ATRP (seATRP) is disclosed. An electrochemical O₂ scavenging cycle was embedded in the ATRP equilibrium to allow self-degassing of the mixture and avoid impractical deoxygenation procedures. Low volume seATRP of acrylamide in water was optimized by studying various reaction parameters, including the concentrations of scavenger, supporting electrolyte, type of initiator and ligand, and catalyst loading. The target reaction was scaled up from 0.015 L to 15 L. At all volumes and up to 15 L, polymerizations were relatively fast and produced well-defined polyacrylamide with narrow molecular weight (MW) distributions. All reactions were powered by renewable electricity, obtained from a photovoltaic plant. Several water-soluble monomers, including (meth)acrylic acid and methacrylamide, were polymerized at pH ranging from 1.0 to 7.4, without compromising the self-degassing mechanism. These results show a feasible scale-up of seATRP and could foster its adoption by polymer industries promoting a more widespread use of controlled radical polymerizations.

1. Introduction

The goal of chemists in scaling-up reactions is to unequivocally demonstrate that large batches of a desired product are obtained without compromising product quality and yield [1]. To scale-up a process from a laboratory reactor to an industrial one, chemists have several options: continuous lab-scale operation, numbering-up, and scale-up. The last is usually chosen because it is most likely to yield an acceptable result, when throughput and capital costs are considered [1]. In electrochemical engineering and large electrochemical production plants, numbering-up (parallel mode) is also often employed [2]. In addition, design and full understanding of the reaction are important to identify problems and solutions along the scale-up development, not just for fundamental understanding. Polymerizations, like any other chemical process, obey these guidelines.

Atom Transfer Radical Polymerization (ATRP) is a widely used Reversible Deactivation Radical Polymerization (RDRP) technique that provides scientists in various branches of chemistry, materials and life sciences the ability to design well-defined, and often complex polymeric structures. ATRP is a catalytic process mediated by Cu(I)/Cu(II) based complexes and is tolerant to a variety of functional groups and solvents. Very active copper catalysts with strongly negative reduction potentials enabled well-controlled polymerizations at catalyst loadings as low as 10–100 parts per million (ppm, relative to the monomer concentration), in H₂O and organic solvents [3,4]. $[Cu^{I}L]^{+}$ (L = ligand, typically Npolydentate amine) activates the dormant C-X (X = Br, Cl) polymer chain end, forming [X-Cu^{II}L]⁺ and a carbon-centered radical. The [X-Cu^{II}L]⁺ complex deactivates the radical after a few propagation events, regenerating a dormant species. Because ATRP is a radical polymerization, it is inhibited by O2 in the vessel and by continuous diffusion of the gas in the mixture if it is open to air. Indeed, O2 can react with the propagating radicals and terminate the polymerization. [5–10]. In addition, even trace amounts of O₂ can inhibit polymerization by rapid oxidation of the [Cu¹L]⁺ activator [11]. Therefore, if O₂ is not removed from the mixture, both radicals and Cu^I species can rapidly react with it to form peroxyl radicals and hydroperoxo complexes or other Cu^{II}

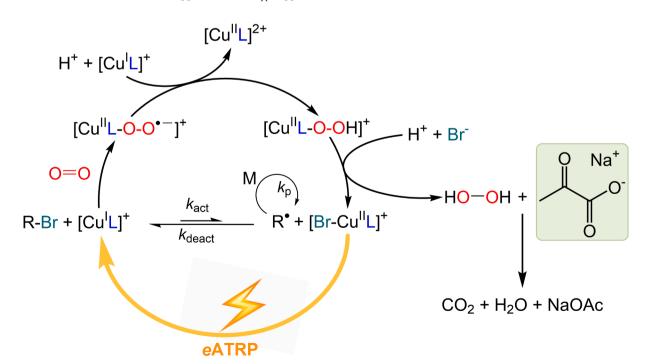
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complexes (Scheme 1) [12,13].

Reactions of alkyl radicals with O2 have rate constants close to the diffusion-controlled limit [14,15]. However, since the concentration of $[Cu^{I}L]^{+}$ is 10^{3} to $> 10^{6}$ times higher than that of the propagating radicals, the dominating reaction of O2 in solution is oxidation of the activator [Cu^IL]⁺ to [HOO-Cu^{II}L]⁺. If the hydroperoxo complex can be converted back to [Cu^IL]⁺ through a reductive pathway involving chemical or electrochemical reduction, O₂ can be chemically washed out of the mixture (Scheme 1). Because of its high sensitivity to O2, ATRP requires often special equipment and deoxygenation by injecting an inert gas prior to the polymerization, which can be cumbersome and costly, especially on a large scale reaction [16,17]. A few years after the introduction of ATRP, well-controlled ATRP in the presence of a limited amount of O₂ was obtained by using Cu⁰ as a reducing agent [18]. This concept was later extended to ATRP using copper wires [19-21] or plates [22-26] and other reducing agents, such as sodium dithionite [27], Fe⁰ [28–31], Zn⁰ [32], ascorbic acid [33,34], tin(II) 2-ethylhexanoate [35], and tertiary amines. [36] A few ATRP systems based on enzymatic degassing [29,37] were carried out in completely open reaction vessels with continuous O2 diffusion. [38] Achieving therefore oxygen tolerance is indeed of academic importance but even more for industrial-like large scale reactions [29,39-56]. In 2020, photoinduced initiators for continuous activator regeneration (PICAR) ATRP enabled regeneration of [Cu^IL]⁺ by excitation of [X-Cu^{II}L]⁺, followed by one electron donation from the excess amine ligand, with simultaneous removal of dissolved O2 in the presence of sodium pyruvate. PICAR ATRP was effective even under continuous diffusion of O2 from the atmosphere into the mixture and no stirring, in contrast to previous ATRPs carried out in sealed vessels with a limited amount of O2 in the reaction mixture or based on enzymatic degassing. It should be noted however that open vessels may not be the preferred type of industrial reactors and are not suitable for gaseous or volatile monomers, which besides often having an acrid odor, can be toxic or carcinogenic. Among all externally controlled ATRP methods, electrochemically mediated ATRP (eATRP), introduced in 2011 [57], is experiencing its heyday [57-63]. The concept behind eATRP is that the ratio of activator to deactivator is tightly controlled by an electrochemical redox process occurring at an electrode surface [46–48]. Factors such as applied current (I_{app}), applied

potential (E_{app}) , or even the total charge passed (Q) can be fixed a priori in eATRP, to constrain the redox equilibrium, and thus precisely control the polymerization. eATRP is also redox-switchable, as it can be stopped and (re)initiated (ON/OFF toggle) by modulating the electrochemical stimulus or even by switching off the cell, achieving temporal control over the process. eATRP provided very positive results in the synthesis of well-defined architectures, becoming increasingly attractive for scale-up in recent years. Although some limitations remain, particularly linked to its elaborate reaction setup, eATRP has become more user-friendly. Typically, eATRP is performed using a three-electrode system under potentiostatic conditions (fixed E_{app}). However, several modifications have improved and redesigned the setup, including: 1) the use of a sacrificial counter electrode (CE), which is introduced directly into the reaction mixture in the so-called simplified eATRP (seATRP);[64] 2) galvanostatic conditions, i.e. constant current electrolysis, without the need for a reference electrode; [62,65] and 3) the use of working electrodes made of materials less expensive than the usually employed Pt (e. g., SS304), with little or no effect on the polymerization outcome [66,67]. The most likely scenario for the scale-up of eATRP is a closed reactor [68–70] with O₂ diffusing from the confined headspace into the reaction mixture, if not removed physically or chemically. To promote the scale-up of eATRP and reduce the challenges associated to ATRP on an industrial scale, we have embedded an electrochemical O2 scrubbing cycle into the ATRP equilibrium, mediated by the ATRP catalyst itself. Inspired by PICAR ATRP [12], the process proposed herein avoids the need of enzymes, while employing electricity from renewable resources as a driving force. Non-enzymatic degassing is highly beneficial and significantly improves O2 removal from large mixtures, allowing for a fully functional, effective, and more user-friendly scale-up. With a scaleup factor of 1000, we successfully scaled up from 15 mL to 15 L the first self-degassing, large-volume, galvanostatic eATRP in H2O. High monomer conversions were reached in a relatively short time, demonstrating a true scale-up of eATRP. The polymerization at 15 L is likely one of the largest-volume ATRP ever reported, and the largest-volume eATRP reported in the literature.



Scheme 1. Proposed mechanism of eATRP with embedded O_2 scavenging cycle for self-degassing. M is the monomer, while k_{act} , k_{deact} and k_p are the activation, deactivation and propagation rate constants, respectively.

2. Results and discussion

2.1. Target reaction for scale-up.

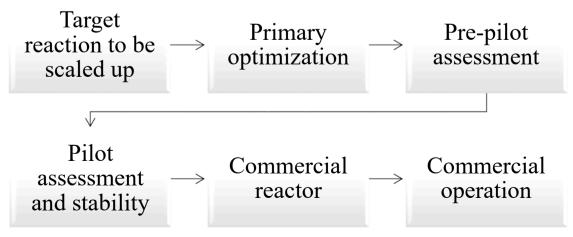
There are numerous aspects to consider for scaling up a polymerization: reaction mechanism, reactor configuration and operating conditions, heat removal, fluid dynamics, mass transfer, thermodynamics, boundary conditions, process dynamics and system stability [1,71]. In addition, an electrochemical scale-up presents other challenges, such as electrode and reactor fabrication, current/potential ratios, membrane/separator materials, charge transfer and electric field distribution [71]; typically predictions/modeling are extensively evaluated before the implementation [72]. These aspects are critical on a large scale, but it is essential that the target reaction is thoroughly investigated and understood prior to scale-up (Scheme 2).

An ATRP is influenced by several components, namely, solvent, monomer, ligand, catalyst type and structure, type of supporting electrolyte (only for eATRP), initiator, polymerization medium (homogeneous or heterogeneous), and type of driving force [58,73,74]. In such a multifaceted scenario, cost-efficiency becomes the fundamental aspect [75,76]. The scale-up requires to identify a polymerization that is economic not only at laboratory scale but also at large scale. Each component of the ATRP system was critically evaluated to find the most reasonable and cost-effective balance between cost and reaction outcome (see Supporting Information, Sections S3 and S5). The target reaction was selected to be an aqueous polymerization: H2O is a clean, universally available, inexpensive, and renewable solvent. Aqueous eATRP is very attractive from both economic and environmental points of view. In recent years, water-soluble poly(meth)acrylates and polyacrylamides have been successfully prepared using eATRP forming polymers with relatively narrow dispersity (D) and experimental molecular weight values (M_n) close to theoretical values [62,77,78]. However, aqueous eATRP presents some challenges. The Cu-X bond in the [X-Cu^{II}L]⁺ deactivator can easily dissociate in H₂O due to low halidophilicity of Cu^{II} (i.e. binding constants for X to $[Cu^{II}L]^{2+} < 10$ M⁻¹) [78]. Therefore, either high catalyst concentrations or the addition of halide salts are required [77,79]. The addition of excess X by introducing a salt that can also act as supporting electrolyte, promotes the formation of [X-Cu^{II}L]⁺ and significantly improves polymerization control. Moreover, temperature has an important effect on aqueous ATRP. The nucleophilic substitution (solvolysis) of alkyl halides in H₂O is suppressed at low temperatures. Therefore, aqueous eATRPs carried out at relatively low temperature (<70 $^{\circ}$ C) and Cu catalyst loading <500 ppm were most effective for some water-soluble monomers [80-82]. The ideal monomer for scale-up should be hydrophilic, should have a high propagation rate constant (k_p) , polymerize near room

temperature, be solid or liquid at the desired temperature; it must also be inexpensive and commercially available, preferably without inhibitor, industrially relevant, and made from inexpensive starting materials. Acrylamide (AAm) is a monomer that meets these requirements. Moreover, PAAm has a broad market, and very high monomer conversion is usually reached at the laboratory scale [81,83-90], which minimizes intensive post-processing of the mixture. ATRP of acrylamides is known and the literature provides proper starting conditions for further optimization [80-82]. The best catalyst for acrylamides is a Cu complex with tris(2-dimethylaminoethyl)amine (Me₆TREN) as ligand, while 2hydroxyethyl 2-bromoisobutyrate (HEBiB) is typically used as initiator in aqueous polymerizations. Although both Me₆TREN and HEBiB are commercially available, they can be easily prepared in high yields and their on-site synthesis is by far less expensive than the commercial purchase. In eATRP, a supporting electrolyte is necessary to make the solution electrically conductive, therefore inexpensive NaBr was chosen, which also acted as a halide source. Sodium pyruvate (SP), prepared from pyruvic acid and sodium hydroxide, [91] has been successfully used as reactive oxygen species (ROS) scrubber in PICAR ATRP of Nisopropylacrylamide (NIPAAm) and methyl acrylate (MA) [12]. SP was used also in this study. The chemistry of SP is well-understood in H₂O and even in the atmosphere [12,92–96], and it does not pose any threat to ATRP activation or deactivation. Regarding the cell setup, low-cost electrode materials should be used [64-67,97,98], therefore reactors made of stainless steel (SS) SS304, acting also as the cathode, were employed together with sacrificial aluminum anodes, thus working in a seATRP setup. Beside the electrodes, the power source becomes crucial for large-volume reactions. We used renewable electric energy obtained from sunlight by a photovoltaic system installed on the roof of the Chemical Engineering Department. This choice permits a cleaner eATRP; in addition, AAm can be provided as bio-acrylamide, as some chemical industries already reached a bio-synthesis of this monomer rather than relying on oil-based feedstocks [99]. Four reactors were used in the successive phases of the scale-up: a traditional five-neck glass cell, a 50 mL SS304 compact reactor for the primary optimization, followed by a 2 L, and 18 L SS304 electrochemical reactors (Fig. 1).

2.2. Primary optimization.

The primary optimization of self-degassing seATRP involves numerous challenges: 1) embedding an O_2 washing pathway into the eATRP equilibrium; 2) raising the reaction temperature to values above the typical value (0 °C) used for ATRP of acrylamides, [81–83] without triggering parasitic reactions [83,100]; 3) minimizing reagent loadings, and thus energy requirements, without compromising the kinetics, 4) defining a robust electrochemical scale-up protocol for larger reactors,



Scheme 2. Proposed flowchart for eATRP scale-up, from targeting the reaction to scale to considering the requirements of a possible future commercial process.

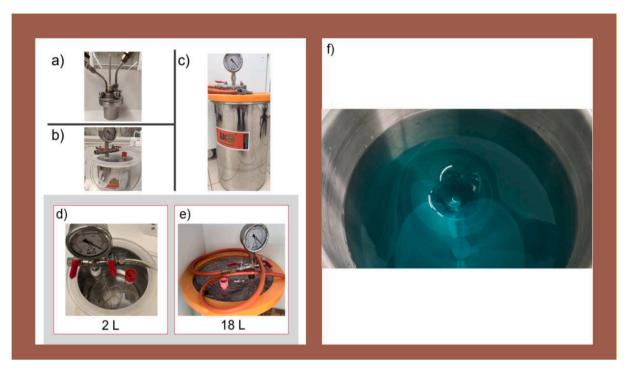


Fig. 1. Digital pictures of a) 50 mL, b) 2 L and c) 18 L reactors; heads of the (d) 2 L and (e) 18 L reactors; f) the 18 L reactor loaded with the polymerization mixture for the 15 L seATRP of AAm (see Table 3 entry 6).

5) dealing with magnetic stirring for reaction volumes beyond 5.0 L, without dramatic changes in mass transfer, and 6) dealing with limitations of the electrochemical equipment if high current outputs are required. First, we investigated the stability of the catalyst in the presence of sodium pyruvate, NaBr or NaCl, and the effect of the scavenger on the activation and deactivation rate constants, $k_{\rm act}$ and $k_{\rm deact}$ respectively, and the ATRP equilibrium constant, $K_{\rm ATRP}$. 2-Bromopropionamide (BrPAm) or 2-chloropropionamide (ClPAm) were used as model chain-ends for PAAm (**Section S4**). Cyclic voltammetry of [Cu^{II}Me₆TREN]²⁺ in H₂O/AAm (10 wt%) showed a quasi-reversible peak couple, which did not vary upon addition of excess X (**Figure S5**), indicating low halidophilicity of the Cu complex in aqueous media. Addition of a large excess of sodium pyruvate did not substantially change the voltammetric response, while remarkable catalytic

enhancement of the cathodic peak was observed when HEBiB was added (Figures S7-S8). The cathodic current enhancement is due to Cu(I)-catalysed activation of the initiator, which otherwise cannot generate radicals by direct reduction at the electrode at the chosen potential window. Electrode reduction of HEBiB requires potentials significantly more negative than the standard redox potential (E°) of the copper catalyst [101]. A rotating disk electrode (RDE) [102] was used to measure the values of $k_{\rm act}$ of BrPAm and ClPAm by [Cu^IMe₆TREN]⁺, yielding 1206 M⁻¹s⁻¹ and 8.4 M⁻¹s⁻¹, respectively. Thus, the activation of Br-capped PAAm chains was relatively fast, and over two orders of magnitude more rapid than for Cl-capped chains, in agreement with previous reports [78]. The addition of a large excess (100 equiv.) of NaBr or NaCl caused minimal variation in the activation kinetics, further suggesting that the catalyst has low halidophilicity. Further addition of

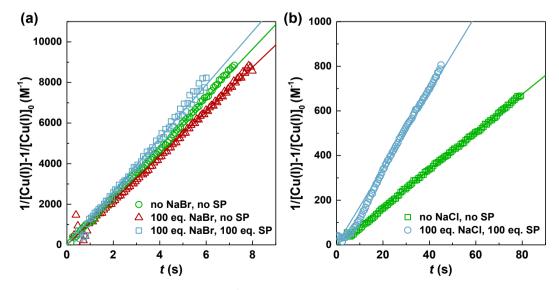


Fig. 2. Kinetic analysis of BrPAm (a) and ClPAm (b) activation by $[Cu^{1}Me_{6}TREN]^{+}$ in $H_{2}O/AAm$ (10 wt%) in the absence and presence of 100 equiv. NaX and/or sodium pyruvate (SP), measured using a rotating disk electrode (RDE), at $E_{app} = 0.15$ V vs SCE, and rotation speed = 4000 rpm.

sodium pyruvate in equimolar amount to the NaX salt increased the observed rate constants by a factor of 1.2 and 2 for BrPAm and ClPAm, respectively (Fig. 2). Pyruvate anion is capable of binding to Cu complexes, however it has only a small effect on the kinetics in the studied mixtures. The value of K_{ATRP} for the system composed of $\left[\text{Cu}^{\text{I}}\text{Me}_{6}\text{TREN}\right]^{+}$ and ClPAm was also measured by RDE [103], giving $K_{ATRP} = 5.1 \times 10^{-6}$. In the presence of excess of both sodium pyruvate and NaCl, the observed $K_{\rm ATRP}$ was ~ 3 times smaller (1.6 \times 10⁻⁶). As a result, k_{deact} (calculated as $k_{\text{act}}/K_{\text{ATRP}}$) increased by about 1 order of magnitude in the presence of sodium pyruvate, which can result in more effective deactivation of propagating radicals, and thus better control. The equilibrium constant for the BrPAm-based system was above the upper limit of the RDE method; however one can expect a K_{ATRP} value on the order of 10^{-5} , and thus $k_{\rm deact} \sim 10^8 \, {\rm M}^{-1} {\rm s}^{-1}$ [104]. Overall, the use of Br ions and C-Br chain end should result in faster and better controlled polymerization, compared to Cl and C-Cl chain end, as is typically observed in ATRP.

After the voltammetric study, the polymerization was investigated in detail in an undivided glass cell, with a Pt gauze as cathode and an Al wire as a sacrificial anode, at a total volume V=15 mL (**Tables 1 and S6**).

This allowed to fully understand the polymerization behavior and to identify the reagents that can be used in smaller amounts, in view of employing larger reactors. The polymerization was investigated in detail by changing the concentrations of SP and NaBr (or NaCl), degree of polymerization, catalyst load, and "type" of H₂O and electrolyte (NaBr or NaCl). Also, the effect of using a buffer was examined. Polymerizations with NaBr were more controlled than those with NaCl, in terms of optimal electrolyte amount, D of PAAm and charge consumption. In addition, raising the temperature to $T=10\,^{\circ}\mathrm{C}$ did not affect control and conversion. We also found that using 0.05 M SP + 0.05 M NaBr gave the same outcome as when 0.1 M concentration of both was used. The

catalyst concentration was diminished to 5×10^{-4} M. Electrogenerated $\rm H_2O_2$ should be<0.05 M but this is a very high amount. Typical dissolved $\rm O_2$ concentrations are below 0.2–0.3 mM if the solution is exposed to open-air, so the maximum amount of electrogenerated $\rm H_2O_2$ depends on the maximum amount of dissolved $\rm O_2$, which is low, considering that we operate in a closed system with purged headspace. Further results are shown in **Tables S6-S7**. This preliminary set of experiments suggested the selection of the optimal conditions reported in Table 2.

Once the best laboratory-scale mixture composition was identified, the polymerization was attempted by galvanostatic seATRP (Fig. 3) [65]. Galvanostatic electrolysis with one value of applied current or multistep currents is the usual choice for large scale electrosynthesis [105,106]. The choice of the applied current (I_{app}) and step length must consider various issues and parameters, including catalyst concentration, overall required charge, electrode surface area (S) and surface/ volume ratio (S/V). This is an unexplored area, lacking literature details, therefore we had to identify proper adjustment factors when needed (Table S8). Potentiostatic seATRP was employed to understand the effect of mixture composition, reactor, and electrodes parameters. After careful and extensive screening of polymerization conditions by potentiostatic seATRP (Table 1 and Table S6), a candidate polymerization was chosen for the scale-up (Table 1, entry 5 and Fig. 3). The reaction conditions summarized in Table 2 were used to compare a potentiostatic seATRP in a glass cell (solution volume = 15 mL) with a Pt working electrode (Fig. 3, black squares) with a galvanostatic seATRP in a compact 50 mL SS304 reactor (V = 40 mL, geometric surface area of the cathode exposed to the solution, $S = 53 \text{ cm}^2$) (Fig. 3, red circles). Both reactions were fast and very well-controlled, reaching ~ 90% conversion within 2 h (Fig. 3 a,b). Polymers with narrow monomodal molecular weight distributions were obtained, shifting toward higher molecular weight as conversion increased (Fig. 3 c,d). A short induction

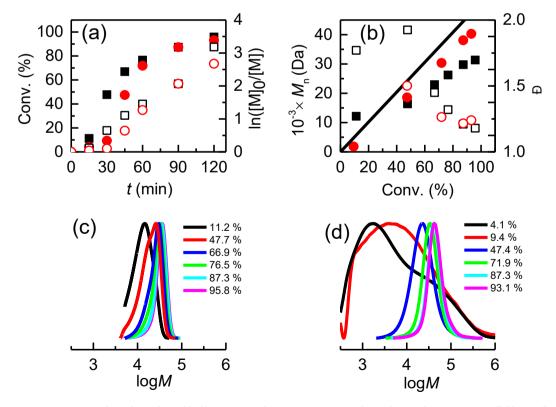


Fig. 3. 15 mL-potentiostatic seATRP with Pt electrode (\blacksquare black) vs 40 mL-galvanostatic seATRP with stainless steel 304 reactor scaffold (\blacksquare red) of AAm in H₂O at 10 °C: a) evolution of conversion (filled symbols) and $\ln([M]_0/[M])$ (empty symbols) vs time; b) evolution of M_n^{GPC} (filled symbols) and D (empty symbols) vs conversion; c, d) normalized evolution of molecular weight distribution of PAAm from potentiostatic (c) and galvanostatic (d) seATRPs. In galvanostatic seATRP (d), bimodality in the first two chromatograms at conv. = 4.1 and 9.4% is caused by normalization.

Table 1
Results of 15 mL seATRP of AAm (10 wt%) in the presence of NaBr and SP.^a.

Entry	NaBr (M)	CuBr ₂ (mM)	$E_{\rm app}$	SP (M)	t (h)	Conv. (%) ^b	$10^{-3} \times M_n^{c}$	$10^{-3} \times \textit{M}_{n}^{\text{th } d}$	Đ ^e		Observations
1	0.1	1	$E_{ m pc}$	0.1	3	-	-	-	-	3.77	Steady-state O ₂ diffusion, no observed polymerization
2	0.1	1	$E_{\rm pc}$	0.1	1.5	97	43.0	48.3	1.20	1.37	Blanketing at $t = 0$
3	0.1	1	$E_{\rm pc}$	0.1	1.5	94	41.1	43.3	1.21	1.08	No buffer
4	0.1	0.5	$E_{\rm pc}$	0.1	2	87	45.0	43.9	1.17	1.42	Buffer
5	0.05	0.5	$E_{\rm pc}$	0.05	1.5	93	40.4	46.9	1.18	1.46	Buffer, $T = 10$ °C
6	0.05	0.5	I_{app}	0.05	2.5	93	40.3	46.8	1.24	8.17	Buffer, $T = 10$ °C, $V = 40$ mL

^a 'Conditions: [AAm]/[HEBiB]/[CuBr₂]/[Me₆TREN] = 704/1/x/2, where x = 1 or 0.5, according to the third column, DP = 704. WE = Pt mesh approx. 6 cm², CE = aluminum wire directly immersed into the working solution. Stirring = 700 rpm. E_{pc} = cathodic peak potential. ^b Calculated from ¹H NMR in D₂O + 2 vol% DMF as internal standard. ^c Calculated from aqueous GPC with 6 narrow poly(sodium methacrylate) standards at T = 35 °C. ^d Calculated from ¹H NMR: M_n^{th} = Conv. × DP × MW_{AAm} + MW_{HEBiB}. ^e D = M_w/M_n . Additional comments: entries 1–4, 6: 0.012 M phosphate buffer and variable blanketing; entry 5: no buffer added and blanketing before electrolysis; entry 6: V_{TOT} = 40 mL in the compact 50 mL SS304 reactor with Al sacrificial anode.

 Table 2

 Chemical composition of the polymerization mixture of AAm.

Name	Empirical Formula	Role	Concentration
AAm	C ₃ H ₅ NO	Monomer	1.41 M
H_2O	H_2O	Solvent	~50 M
Copper(II) Bromide	CuBr ₂	Pre-catalyst	$5 \times 10^{-4} \text{ M}$
Tris(2- dimethylaminoethyl) amine	$C_{12}H_{30}N_4$	Ligand	$2 \times 10^{-3} \text{ M}$
Sodium Bromide	NaBr	Supporting electrolyte	$5.0 \times 10^{-2} \mathrm{M}$
Sodium Pyruvate	$C_3H_3O_3Na$	ROS scrubber	$5.0 \times 10^{-2} \text{ M}$
Sodium dihydrogenphosphate	NaH ₂ PO ₄	Buffer component	$1\times10^{2}\text{M}$
Potassium hydrogenphosphate	K ₂ HPO ₄	Buffer component	$1.8 \times 10^{-3} \text{ M}$
2-Hydroxyethyl 2- bromoisobutyrate	$C_6H_{11}BrO_3$	Alkyl halide Initiator	$2.0\times10^{\text{-}3}~\text{M}$
Dimethylformamide	C ₃ H ₇ NO	Internal standard	$2.6\times10^{\text{-4}}$ M (2 vol%)

period (15–30 min) was observed for galvanostatic seATRP (Fig. 3a). This is likely due to two separate processes. The first process is a self-cleaning of the stainless-steel surface, as some charge is used to modify the oxide layer that is present on the stainless-steel surface. The second process is the oxygen consumption which takes place once oxide-free electrode surface becomes available to reduce the catalyst from Cu (II)/L to Cu(I)/L. It is also possible that these two processes occur concurrently. Thus, the short induction period is attributed to the contributions of these two processes, which both result in charge consumption prior to the onset of the polymerization. After these encouraging results, the candidate mixture (Table 2) was adopted for the scale-up.

2.3. Large volume seATRP.

The combination of all above mentioned variables defines an applied current value that allows the polymerization to proceed at virtually any volume. Another requirement for successful large-scale electrolysis is efficient mass and charge transfer. As the solution is highly electrically conductive, we decided to rely on magnetic agitation for mass transfer. We employed a 7.5 cm diameter hub-shaped AlNiCo magnet, which provided sufficient stirring up to 15 L. The hub shape is preferred to a cylindrical one because it allows higher turbulence at lower torques, without stirrer uncoupling from the magnet. We found during the experimental design that seATRP of 10 L and 15 L required currents greater than the maximum output (± 0.8 A) of our potentiostat/galvanostat. In addition, a first attempt at 5 L showed some limitations of mass transfer that caused a runaway of the reaction at high current output ($I_{\rm app} = 0.545~{\rm mA}$) and led to passivation of the reactor surface. To

circumvent these limits, we decided to maintain $|I_{\rm app}|$ below 300 mA. Applying a lower $I_{\rm app}$ resulted in a slower $[{\rm Cu}^{\rm I}{\rm L}]^+$ regeneration, and thus a slower ${\rm O}_2$ consumption at the beginning of the reaction, which delayed the onset of polymerization (up to 3 h induction period was observed at V=15 L). The electrolysis programs are shown in **Table S9** and **Figure S13**. Using the reaction conditions reported in **Table 2**, scale-up of seATRP of AAm was evaluated at 0.5, 1.0, 5.0, 10.0 and 15.0 L (Table 3, entries 1–6).

First-order kinetic plots and molecular weight evolutions vs conversion are shown in Fig. 4.

The correct electrolysis programs afforded reactions that were relatively fast, controlled and reached high conversions without the undesired side-reactions known for acrylamides. Dispersity decreased with time because of the high number of activation/deactivation cycles, in line with conventional ATRP. Induction periods were observed, and their duration increased as volume increased from 0.04, 1, 5, 10 to 15 L (from about 15 min to 3 h). Nevertheless, these induction periods are the compromise between reaction time, rate of O2 consumption and instrumental limitations. Further optimizations should address this aspect, including improved mass transfer. The anodic dissolution of Al can be calculated from Faraday's laws of electrolysis. In H2O, electrogenerated Al^{3+} did not pose any threat to the polymerization (< 0.43 g of Al were dissolved during the 15 L seATRP). We also highlight the very low power consumption of these reactions: only at 15 L the peak power exceeded 1 W. The evolution of normalized molecular weight distributions is shown in Fig. 5.

Regardless of the reaction volume (0.04 L - 15 L), the chromatograms showed almost all monomodal, and almost symmetric molecular weight distributions, with no tailing, shifting to higher logM as conversion increased. Fig. 6 shows how surface area and S/V (a), conversion and molecular weight (b) and D (c) changed with the reaction volume. As V increased faster than S, the ratio S/V decreased. The best results in terms of conversion, polymer molecular weight and dispersity were obtained for higher S/V ratios ($>0.4~\rm cm^{-1}$). When S/V was decreased, conversion and M_n decreased, while D increased, all parameters stabilizing as S/V approached $0.2~\rm cm^{-1}$. Geometry plays a key role in every reactor design, and it is object of continuous extensive study and optimization [107-110]. Future design of bigger reactors for seATRP should critically evaluate geometry and how to increase the S/V ratio, perhaps treating the surface to make it porous or add an additional stainless steel electrode with an appropriate mesh size.

Based on energy data, monomer input, and conversion recorded at 15 L and energy cost (0.1548 €/KWh), the first euro of energy required by seATRP is spent after producing ~ 1912 kg of polyacrylamide. Most industries now already have a photovoltaic plant for energy self-production and, by using electricity from sunlight, seATRP could theoretically enable polymer production with clean energy and limited additional cost. In addition, other equipment (computers, reactor heating/cooling system, analytical instruments), serving this scale-up plant,

Table 3 Effect of volume increase (scale-up) of seATRP of AAm (10 wt%) at $T=10~^{\circ}$ C.

Entry	Scale-up factor ^b	V (L)	Electrolyis program	t (h)	Conv. ^c (%)	$10^{-3} \times M_{\rm n}^{\rm GPC\ d}$	$10^{-3} \times M_{\rm n}^{\rm th~e}$	Ð ^f	Q (C)	Peak power ^g (W)	Al dissolution (mg) ^h
1	2.6	0.04	I	2.5	93	40.3	46.8	1.24	8.17	< 0.01	0.76
2	33.3	0.5	II	2.5	97	42.9	48.6	1.16	78.74	0.04	7.39
3	66.6	1	II	3.5	97	46.5	48.6	1.17	245.60	0.27	22.91
4	333.3	5	IV	4.5	88	34.7	44.3	1.27	1527.60	0.43	142.43
5	666.6	10	V	6.0	79	40.7	40.0	1.27	3523.60	0.65	328.68
6	1000	15	VI	6.5	79	41.0	40.0	1.25	4596.70	1.01	428.77

^{a-}Conditions: [AAm]/[HEBiB]/[CuBr₂]/[Me₆TREN] = 703/1/0.5/2, where DP = 703 for AAm; $C_{\text{Cu(II)}} = 5 \times 10^{-4} \text{ M}$; $T = 10 \,^{\circ}\text{C}$. WE = SS304 body of the reactor; CE = 750 cm aluminum coil directly immersed into the working solution. Stirring = 700 rpm. ^{b-}Scale-up factor = Target volume/0.015 L. ^{c-}Calculated from ¹H NMR in D₂O + 2 vol% DMF as internal standard. ^{d-}Calculated from aqueous GPC with 6 narrow poly(sodium methacrylate) standards at $T = 35 \,^{\circ}\text{C}$. ^{e-}Calculated from ¹H NMR: $M_n^{\text{th}} = \text{Conv.} \times \text{DP} \times \text{MW}_{\text{AAm}} + \text{MW}_{\text{HEBiB}}$. ^{f-}D = M_w/M_n . ^{g-}The peak power is measured by the galvanostat during all the reaction time and the highest value recorded is reported. ^{h-}Al anodic dissolution is calculated as $m_{\text{Al}} = Q/3F \times \text{MW}_{\text{Al}}$.

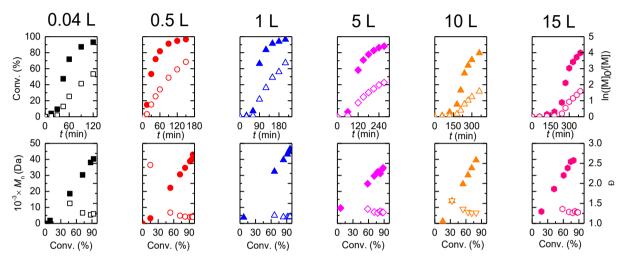


Fig. 4. Galvanostatic seATRP of AAm from 0.04 to 15 L. First row: evolution of conversion (filled symbols) and $\ln([M]_0/[M])$ (empty symbols) vs time; second row: evolution of M_n^{GPC} (filled symbols) and D (empty symbols) vs conversion.

may also be powered by renewable energy.

2.4. Exploratory self-degassing seATRP of other monomers.

After the scaling-up, we also examined the self-degassing seATRP of a selection of functional hydrophilic monomers such as oligo(ethylene oxide) methyl ether methacrylate (OEOMA500), methacrylic acid (MAA), acrylic acid (AA), N-isopropylacrylamide (NIPAAm), Nhydroxyethylacrylamide (HEAAm) and methacrylamide (MAAm) in the 15 mL electrochemical cell (Table 4 and Figures S14-S19). These polymers are commonly used in various fields: OEOMA for bioconjugates/biocompatibility [16,111], acrylic and methacrylic acids for polyelectrolytes and pH-responsive (co)polymers [112,113], NIPAAm for thermoresponsive (co)polymers [111,114], and HEAAm for antibacterial and antifouling coatings [115]. The uncommon and undervalued MAAm could be used in thermoresponsive (co)polymers as well [116]. MAA and AA were polymerized by eATRP at pH 1.0 and 2.0, respectively, as seATRP does not strictly require a buffer [117]. This is advantageous in contrast to PICAR ATRP, which requires a very tight pH control due to photochemical side-reactions [12].

NIPAAm and HEAAm reached 99% conversion in ≤ 1 h producing well-controlled polymers, whereas OEOMA $_{500}$ reached moderate conversion with [Cu^{II}TPMA] $^{2+}$ (TPMA = tris(2-pyridylmethyl)amine), the usual catalyst for ATRP in H $_2$ O [78,101]. Methacrylamide (MAAm) is one of the most challenging monomers for ATRP, to the best of our knowledge. While only few derivates of MAAm (such as hydroxypropyl methacrylamide and N-methyl methacrylamide) have been polymerized by ATRP or reversible addition-fragmentation chain-transfer (RAFT)

polymerization, [118-120] controlled ATRP of unsubstituted MAAm has not been reported. MAAm has k_p of the same order as methacrylates [116,121], but k_{act} of the dormant P_n -X should be higher than that of acrylamide because of the tertiary nature of the terminal C-X. Moreover, PMAAm shows upper critical solution temperature (UCST) near 40 °C in H₂O [116]. ATRP of MAAm in H₂O must balance two conflicting requirements: 1) ensuring polymer solubility, and 2) suppressing intramolecular cyclization side-reactions. Both requirements are temperature-dependent: PMAAm is only soluble above 40 °C, but at this temperature cyclization is much more rapid than at 0-10 °C, consuming chain-ends during conversion [83,85,87,100]. We therefore attempted the seATRP of MAAm just above its UCST to ensure full solubility, using 0.3 M NaCl to minimize intramolecular cyclization and $E_{\rm app} = E_{1/2} + 0.06 \text{ V}$ to avoid excessive radical formation. The initiator was the polychlorinated hexafunctional hexachloro-2-propanone (HCA), which was also used for AAm (see Section S5). This is the first time that HCA is used as initiator in ATRP to the best of our knowledge. PMAAm-Cl was obtained with 47 % conversion and D = 1.46, but side reactions were only partially prevented, as judged by the incomplete conversion. For (M)AA, these are the first seATRPs with a sacrificial aluminum anode. It is also worth noting that the reaction between electrogenerated H2O2 and pyruvic acid/pyruvic anion is strongly pHdependent and is significantly attenuated at low pH [95]. In addition, pyruvate is present in the non-ionized pyruvic acid form at low pH. In view of this, we added pure pyruvic acid to the mixture. At 0.3 M of pyruvic acid, ROS scrubbing still occurred, and polymerizations were carried out up to moderate conversions, showing that a suitable concentration of pyruvic acid is effective at low pH. P(M)AA-Cl was

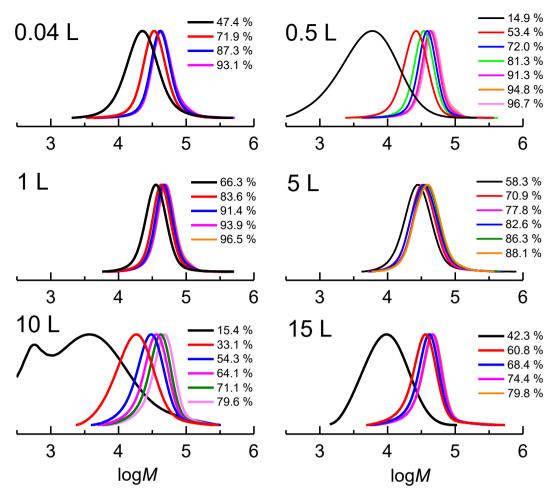


Fig. 5. Normalized evolution of molecular weight distribution of PAAm produced by galvanostatic *se*ATRP from 0.04 to 15 L. At 10 L, bimodality in the first chromatogram at conv. = 15.4% appeared because the signal of the polymer partially overlapped with the signal that corresponds to the eluent at the limit of the retention regime of our columns.

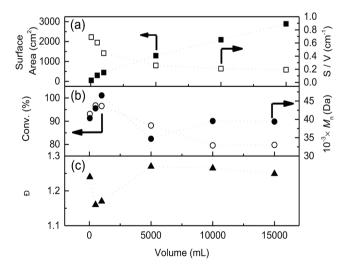


Fig. 6. Evolution of a) geometric surface area (\blacksquare) and surface/volume ratio (\square), b) conversion (\bullet) and apparent molecular weight (\circ), and c) D (\blacktriangle) recorded at the end of seATRP of AAm at 0.04, 0.5, 1, 5, 10 and 15 L.

obtained with low dispersity (D < 1.3). Evolution of normalized molecular weight distributions of water-soluble polymers produced by self-degassing potentiostatic *se*ATRP is shown in Fig. 7:

2.5. Chain extension of PAAm.

To prove the livingness of PAAm-Br, a chain extension was attempted. A short PAAm-Br macroinitiator was prepared by electrolyzing for 15 min a polymerization mixture prepared as of Table 1, entry 5. NMR and GPC analysis of this solution showed 11.4% AAm conv. (DP = 80), yielding PAAm-Br with $M_n = 5900$. 1 mL of this mixture containing PAAm-Br as macroinitiator was withdrawn. Then, the chain extension was continued by injecting this 1 mL of PAAm-Br mixture in a new mixture prepared as of Table 4, entry 2, with HEAAm as the second monomer. Electrolysis was triggered at $E_{app} = E_{pc}$. Considering the low AAm amount injected, competition between AAm and HEAAm during the synthesis of the second block was minimal. In addition, the reactivity ratio of AAm/HEAAm is close to 1 ($r_{\rm AAm} \sim$ 1, $r_{\rm HEAAm} \sim$ 1, and $r_{\rm AAm} \times$ $r_{\rm HEAAm} \sim 1$) so that the majority of the second block should contain HEAAm and very few units of AAm statistically distributed along the chain [122]. The block copolymer, PAAm₈₈-b-PHEAAm₂₅₆-Br, had a $M_{\rm n}^{\rm SEC} = 36.3 \times 10^3$, $M_{\rm n}^{\rm th} = 35.4 \times 10^3$, D = 1.30 and conv._{HEAAm} = 53 %. MW distribution traces indicated extension and the peak shifted almost entirely towards higher MW (Fig. 8).

3. Conclusions

Controlled radical polymerizations by seATRP in large volume reactors of up to 15 L were achieved by embedding an O_2 scavenging system in the eATRP equilibrium. All reactions were powered by renewable energy taken from a photovoltaic system. The headspace was

Table 4Potentiostatic self-degassing *se*ATRP of hydrophilic monomers (NIPAAm, and MAAm 10 wt% and HEAAm, OEOMA₅₀₀, MAA and AA 10 vol%) at a Pt cathode and a sacrificial Al anode, with pyruvic acid/pyruvate anion as ROS scrubber ^a.

Entry	SE ^b (M)	Catalyst	$E_{\rm app}$	Pyruvate (M)	t (h)	Conv. ^c (%)	$10^{\text{-3}} \times \textit{M}_{n}^{\text{GPC}}$	$10^{\text{-3}} \times \textit{M}_{n}^{\text{th } d}$	Đ		pН	T (°C)
NIPAAm	0.1 NaBr	[Cu ^{II} Me ₆ TREN] ²⁺	$E_{\rm pc}$	0.05	1	99	53.1 ^e	49.5	1.05	1.07	7.4	0
HEAAm	0.1 NaBr	[Cu ^{II} Me ₆ TREN] ²⁺	$E_{\rm pc}$	0.05	0.75	99	61.8 ^f	61.4	1.30	2.28	7.4	0
MAAm	0.3 NaCl	[Cu ^{II} Me ₆ TREN] ²⁺	$E_{1/2} + 0.06$	0.05	2	47	33.3 ^g	23.6	1.46	4.13	7.4	42
OEOMA ₅₀₀	0.1 NaCl	[Cu ^{II} TPMA] ²⁺	$E_{1/2} + 0.06$	0.05	4	61	67.6 ^h	36.2	1.13	3.36	7.4	25
MAA	0.3 NaCl	[Cu ^{II} TPMA] ²⁺	$E_{ m pc}$	0.3^{i}	3	71	45.7 ^f	36.1	1.23	2.03	1.0	25
AA	0.006 NaCl	[Cu ^{II} TPMA] ²⁺	$E_{ m pc}$	0.3^{i}	6	52	38.4 ^f	27.3	1.25	3.23	2.0	25

a·Conditions: [NIPAAm]/[HEBiB]/[CuBr₂]/[Me₆TREN] = 884/2/0.5/2, DP = 442; [HEAAm]/[HEBiB]/[CuBr₂]/[Me₆TREN] = 965/2/0.5/2, DP = 482; [MAAm]/[HCA]/[CuCl₂]/[Me₆TREN] = 118/0.2/0.05/0.2, DP = 588, HCA = hexachloroacetone; [OEOMA₅₀₀]/[HEBiB]/[CuBr₂]/[TPMA] = 216/2/1/2, DP = 108; [MAA]/[DCPA]/[CuCl₂]/[TPMA] = 118/0.2/0.1/0.4, DP = 590, DCPA = 2.2-dichloropropionic acid; [AA]/[TCAA]/[CuCl₂]/[TPMA] = 146/0.2/0.1/0.4, DP = 729, TCAA = trichloroacetic acid. ^h Supporting electrolyte. ^c Calculated from ¹H NMR in D₂O + 2 vol% DMF as internal standard. ^d Calculated from ¹H NMR; M_n^{th} = Conv. × DP × MW_{monomer} + MW_{RX}. ^e Calculated from DMF GPC with 6 narrow poly(methyl methacrylate) standards at T = 60 °C. ^f Calculated from aqueous GPC with 6 narrow poly(sodium methacrylate) standards at T = 35 °C. ^g Calculated from THF GPC with 6 narrow poly(styrene) standards at T = 30 °C. ^h Calculated from aqueous GPC with 6 narrow poly(sodium methacrylate) standards at T = 30 °C. ^h Calculated from aqueous GPC with 6 narrow poly(sodium methacrylate) standards at T = 30 °C. ^h Calculated from aqueous GPC with 6 narrow poly(sodium methacrylate) standards at T = 30 °C. ^h Calculated from aqueous GPC with 6 narrow poly(sodium methacrylate) standards at T = 30 °C. ^h Calculated from aqueous GPC with 6 narrow poly(sodium methacrylate) standards at T = 30 °C. ^h Calculated from aqueous GPC with 6 narrow poly(sodium methacrylate) standards at T = 30 °C. ^h Calculated from aqueous GPC with 6 narrow poly(sodium methacrylate) standards at T = 30 °C. ^h Calculated from aqueous GPC with 6 narrow poly(sodium methacrylate) standards at T = 30 °C. ^h Calculated from aqueous GPC with 6 narrow poly(sodium methacrylate) standards at T = 30 °C. ^h Calculated from aqueous GPC with 6 narrow poly(sodium methacrylate) standards at T = 30 °C. ^h Calculated from aqueous GPC with 6 narrow poly(sodium methacrylate) standards at T = 30 °C. ^h Calculate

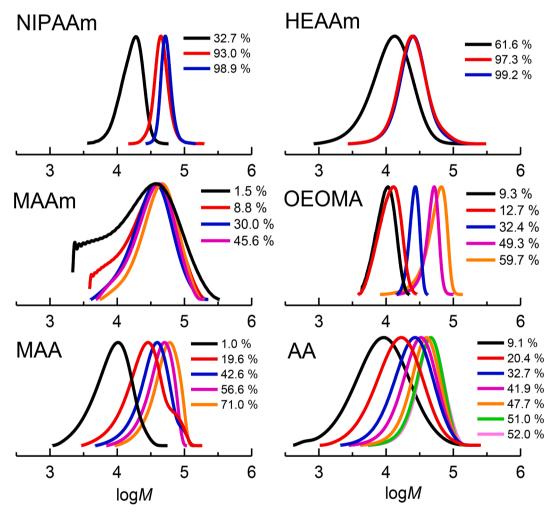


Fig. 7. Evolution of normalized molecular weight distributions of water-soluble polymers produced by self-degassing potentiostatic seATRP at 15 mL at pH 7.4 (NIPAAm, HEAAm, MAAm and OEOMA $_{500}$), 2.0 (AA) and 1.0 (MAA).

degassed with N₂, while the presence of sodium pyruvate in solution ensured a relatively rapid self-degassing of the mixture once the electrolysis started. Sodium pyruvate reacts with ROS, preventing poisoning of the polymerization. Mechanistically, the process has some steps in common with PICAR ATRP [12], but the electrochemical control circumvents the radical generation that occurs during PICAR ATRP, allowing for decreasing the concentration of sodium pyruvate to 0.05 M

to obtain an effective scrub. All AAm polymerizations from 15 mL to 15 L (scale-up factor 1000) were very well-controlled (D < 1.27) and achieved high monomer conversions (>79%) in a relatively short time (<6.5 h). Moreover, pH control in *seATRP* is not a strict requisite, in contrast to PICAR ATRP, because pH-changing side reactions occurring in the photochemical cycle do not occur in *seATRP*. Thanks to this, we polymerized several other water-soluble monomers, including (meth)

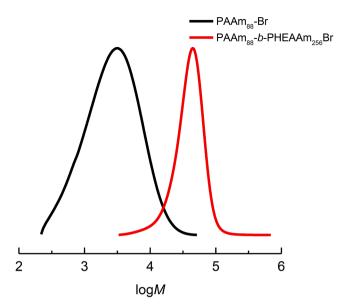


Fig. 8. Evolution of normalized molecular weight distributions of PAAm₈₀-Br and PAAm₈₀-b-PHEAAm₂₅₆-Br produced by self-degassing potentiostatic *se*ATRP in a 15 mL electrochemical cell.

acrylic acids (at pH \leq 2), in the presence of sodium pyruvate or pyruvic acid, using either [Cu^{II}Me₆TREN]²⁺ (for AAm, HEAAm, NIPAAm, MAAm) or [Cu^{II}TPMA]²⁺ (for OEOMA, MAA, AA) as catalyst. The applicability of this process to hydrophobic monomers is currently under investigation in our laboratory and it will be reported in near future. However, the scale-up for hydrophobic monomers is hard to be achieved by homogeneous polymerizations, due to the cost of solvent and organic electrolytes, even by employing relatively inexpensive solvents like ethanol. A final issue is that sodium pyruvate is not soluble in organic solvents. eATRP is currently a known and well-established technique for polymer synthesis, and its expansion to reactors with volumes ≥ 100 L is envisioned. Further challenges for seATRP on an industrial scale may include: i) an improved electrode configuration for homogeneous electric field distribution, ii) the implementation of mechanical stirring for improved mass transfer, minimization of deoxygenation time, and online sensing elements for real-time reaction monitoring, and iii) expansion to non-homogeneous polymerizations.

CRediT authorship contribution statement

Francesco De Bon: Conceptualization, Investigation, Formal analysis, Writing – original draft, Writing – review & editing, Funding acquisition, Validation, Supervision. Rita G. Fonseca: Writing – review & editing, Validation. Francesca Lorandi: Investigation, Formal analysis, Writing – original draft, Writing – review & editing, Validation. Arménio C. Serra: Writing – review & editing, Validation. Abdirisak A. Isse: Writing – review & editing, Validation. Krzysztof Matyjaszewski: Writing – review & editing, Funding acquisition, Validation. Jorge F.J. Coelho: Conceptualization, Writing – review & editing, Funding acquisition, Validation, Supervision.

Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

Acknowledgments

The authors acknowledge Diana C. M. Ribeiro for her technical support during the synthesis of Me₆TREN and HEBiB, Dr. Kurt Olson for

his comments during the manuscript preparation. F. De Bon thanks FCT for the project POCI-01-0145-FEDER-029742 (POLYCEL) and the project PTDC/EQU-EQU/2686/2020 (POLYELECTRON). Rita G. Fonseca thanks FCT for her PhD scholarship (SFRH/BD/133040/2017). Funding from MATIS (CENTRO-01-0145-FEDER-000014), co-financed by the European Regional Development Fund (FEDER) through "Programa Operacional Regional do Centro" (CENTRO2020) is also acknowledged. The NMR data were obtained at the Nuclear Magnetic Resonance Laboratory of the Coimbra Chemistry Centre (http://www.nmrccc.uc.pt), University of Coimbra, supported in part by Grant REEQ/481/QUI/ 2006 from FCT, POCI-2010, and FEDER, Portugal. This research was partially sponsored by FEDER funds through the program COMPETE -Programa Operacional Factores de Competitividade – and by national funds through FCT – Fundação para a Ciência e a Tecnologia, under the project UIDB/00285/2020. FL and KM acknowledge support from NSF (CHE 2000391).

Appendix A. Supplementary data

Supplementary data to this article can be found online at https://doi.org/10.1016/j.cej.2022.136690.

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