

1 **Resin Based 3D Printing for Fabricating Reactive Porous Media**

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6 **Key Words: Digital Light Projection 3D printing, Reactive porous media, Accessible**
7 **surface area**

8 **Abstract**

9 Resin based three-dimensional (3D) printing is popular for many applications including
10 replicating geologic porous media samples. This study is the first to explore resin-based 3D
11 printing of reactive porous media. Here, digital light projection (DLP) 3D printing of sandstone
12 replicates was performed using photosensitive resin mixed with calcite of varying amounts.
13 Printed samples were imaged in 3D using X-ray micro computed tomography (μ CT). Printed
14 sample porosities are consistent and close to the original mesh porosity. Calcite volume fractions
15 are generally in agreement with the calcite content in the resin mixture. Calcite accessible
16 surface areas are similar to published values for real sandstones and calcite dissolution was
17 observed in acidic batch experiments, evidence of its surface reactivity. DLP printing is thereby
18 promising for fabricating reactive porous media samples.
19

20 **1 Introduction**

21 3D printing of porous media has shown utility for replicating pore networks in undisturbed soil
22 and rock samples [1-4], exploring hydraulic properties [5] and studying rock mechanics [6,7].
23 However, exploration of 3D printing for understanding reactive mineral systems in porous media
24 remains limited.
25

26 Geochemical reaction rates are poorly understood due to inherent sample heterogeneity [8]. Even
27 samples collected from the same formation have varying pore network structures and mineralogy
28 [9]. 3D printing of reactive porous media would enable controlled investigation of geochemical
29 reactions for varying conditions.
30

31 3D printing microparticles in resin has been studied for various applications [10,11], but not for
32 fabrication of reactive porous media. Printing reactive porous media was first explored using
33 calcite containing filaments using Fused Filament Fabrication (FFF) [12]. Accessible calcite
34 surface area agreed well with real sandstones but challenges with printing resolution and defects
35 resulted in internal voids and printing failure [12].
36

37 Here, DLP 3D printing, which has numerous advantages over FFF (including print resolution
38 [13,14]), is explored for fabricating reactive porous media containing calcite. Photosensitive
39 resin is mixed with varying calcite volume percentages and pore structures of a real sandstone
40 sample printed. The resulting printed samples analyzed using μ CT imaging.
41

42 **2 Methodology**

43 Commercial ANYCUBIC resin (density 1.1g/cm^3) was used. Iceland spar calcite crystals were
44 crushed manually and sieved through a $90\mu\text{m}$ mesh, captured on a $63\mu\text{m}$ mesh. This particle size
45 range is detectable by μ CT while not interfering with the printing process. Calcite powder and
46 resin were combined and thoroughly mixed in a beaker at varied calcite volume fractions of 3, 5,
47 and 7v%. Calcite content was determined gravimetrically based on the density of calcite
48 (2.71g/cm^3)[15].
49

50 A 3D Bentheimer sandstone μ CT image was downloaded from Digital Rock Portal [16]. The
51 image was cropped, denoised using a median filter, segmented to grains and pores, and the

52 selected region of interest (grain) converted into a 3D mesh in Dragonfly. The mesh was
53 enlarged 20x to match the 3D printer resolution and exported as a (.stl) file.

54
55 An ANYCUBIC Photon 3D DLP printer was used. The 3D model was sliced into 25 μ m layers
56 using Photon Workshop V2.1.26 and printed at 45° with supports (~6 hr print time). The 7v%
57 calcite mixture was also printed at 50 μ m layer thickness (~3 hr print time). After printing,
58 supports were removed, and the object washed using 70v% isopropyl alcohol and deionized
59 water to remove excess resin followed by a 10 minute UV chamber post-cure.

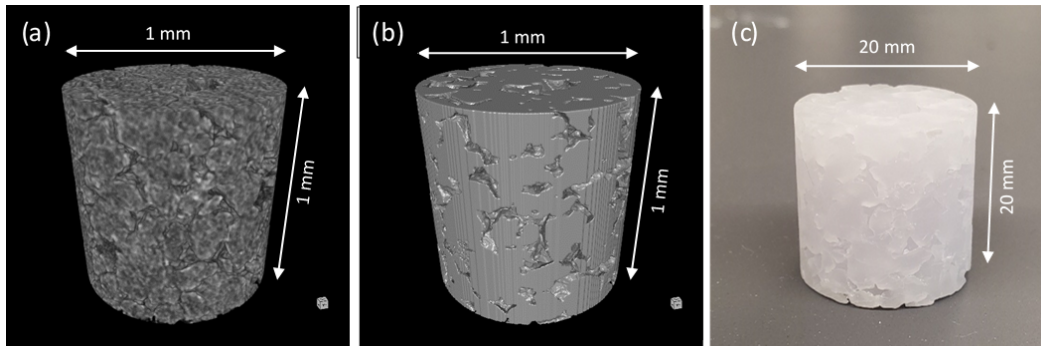
60
61 Printed samples were imaged with μ CT using a Zeiss Xradia 620 Versa 3D microscope at a
62 resolution of 12.5 μ m. Images were processed and analyzed to determine porosity, calcite volume
63 fraction, total and calcite accessible surface area, and normalized calcite surface area (details in
64 supplementary information).

65
66 Printed sample reactivity was examined in batch experiments. A sample without calcite and the
67 5v% calcite sample were immersed in pH 3.5 HCl solutions at room temperature (18°C) and pH
68 monitored. Calcium concentration was measured in the final solution using ICP-OES.

69 70 **3 Results**

71 3D μ CT images of the Bentheimer sandstone, resulting mesh, and 20x magnified 3D printed
72 sample with 5v% calcite are shown in Figure 1. The mesh porosity is 21.83% while the reported
73 porosity from the original μ CT image is 22.64% [16].

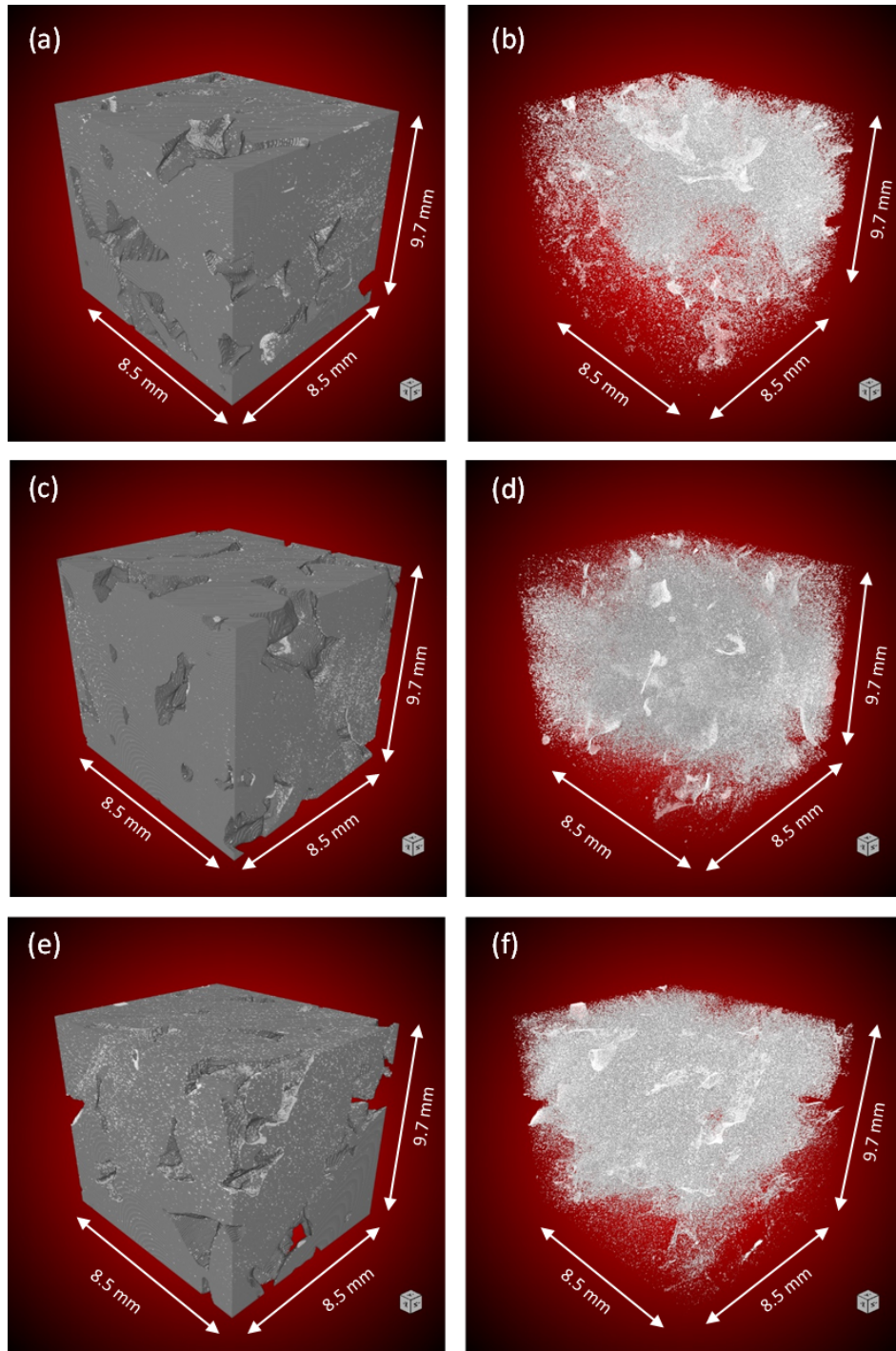
74



75
76 **Figure 1** (a) μ CT image of Bentheimer sample, (b) generated 3D mesh, and (c) 20x magnification printed sample
77 with 5v% calcite.

78

79 μ CT images of the printed samples are shown in Figure 2(a-f) and analyzed properties given in
80 Table 1. The printed sample porosities are very consistent; 18.9%, 18.5% and 18.2%,
81 respectively (standard deviation of 0.28%), indicating minimal variation. This is good agreement
82 with the generated model porosity (21.8 %), similar to the difference seen in other studies
83 [17,18] likely due to trapping of resin in the micropores [18].



84
 85 **Figure 2** Segmented μ CT images of calcite (white) and polymer (gray) for the (a) 3v%, (c) 5v%,
 86 and (e) 7v%. Segmented calcite particle distribution in (b) 3v%, (d) 5v%, and (f) 7v%.
 87

88 The 3 and 5v% samples contain 2.76v% and 4.52v% calcite, respectively; in good agreement
 89 with the resin calcite content. The 7v% calcite sample, however, only contains 2.52v% calcite,
 90 significantly less than in the resin mixture. This is attributed to particle agglomeration and
 91 settling, promoted by the large calcite content. To prevent this behavior, a sample was printed
 92 with 7v% calcite using a 50 μ m layer thickness (reduced printing time). This significantly

93 increased the calcite volume fraction (4.62v%) while maintaining the target porosity. However,
 94 further optimization is needed for printing samples with targeted higher calcite contents.

95
 96 From printed sample images, calcite is present throughout the sample (Figure 2(b,d,f)) with some
 97 surface clumps observed. Calcite accessibility, defined as calcite on the surface of the structure
 98 and accessible to reactive fluids, is quantified from the images (Table 1). Only a fraction of the
 99 calcite present is accessible, 5.39%, 10.22% and 6.28% for 3, 5, and 7v% samples.

100

101 **Table 1** Sample Properties Extracted from μ CT Images of 3-D Printed Samples

Sample Property	3v% calcite	5v% calcite	7v% calcite	7v% calcite
Calcite in resin mixture (v%)	3	5	7	7
Printing layer thickness(μ m)	25	25	25	50
Polymer in printed sample (v%)	97.24	95.48	97.48	95.42
Calcite in printed sample (v%)	2.76	4.52	2.52	4.57
Porosity of printed sample	18.9 %	18.5 %	18.2 %	18.2 %
Calcite accessibility (%)	5.39	10.22	6.28	8.85
Polymer accessibility (%)	94.61	89.78	93.72	91.15
Total surface area (m^2) ($\times 10^{-4}$)	5.12	6.00	5.36	5.76
Calcite accessible surface area (m^2) ($\times 10^{-5}$)	2.76	6.13	3.37	5.10
Calcite in printed sample (g)	0.038	0.062	0.034	0.062
Normalized accessible calcite surface area (m^2/g) ($\times 10^{-4}$)	7.35	9.96	9.82	8.20

102

103 Porous media reaction rates are largely controlled by reactive surface area. The total surface area,
 104 calcite accessible surface area, and normalized accessible calcite surface area extracted from
 105 printed sample images are in Table 1. Total accessible surface areas are similar, indicating good
 106 agreement between the 3D printed pore structures. Slightly larger variations are found for calcite
 107 accessible surface area, though within one order of magnitude, between samples.

108

109 The utility of this approach for reflecting porous media reactivity was probed by comparing
 110 accessible calcite surface area with those quantified for actual sandstones, where good agreement
 111 is found in comparison with a Paluxy sandstone ($8.13 \times 10^{-4} m^2/g$) [19]. Normalized calcite
 112 surface areas are an order of magnitude higher than the $2.14 \times 10^{-5} m^2/g$ quantified for a 0.03v%
 113 calcite volcanogenic sandstone sample, though lower accessible surface area for that sample is
 114 possibly a result of clay coatings [20].

115

116 Batch acid dissolution experiments showed no pH change (Figure 3) or dissolved calcium for the
 117 sample without calcite, whereas the 5v% calcite sample showed both a pH increase over 4 days
 118 (Figure 3) and a calcium solution concentration of 5.15mg/L.

119

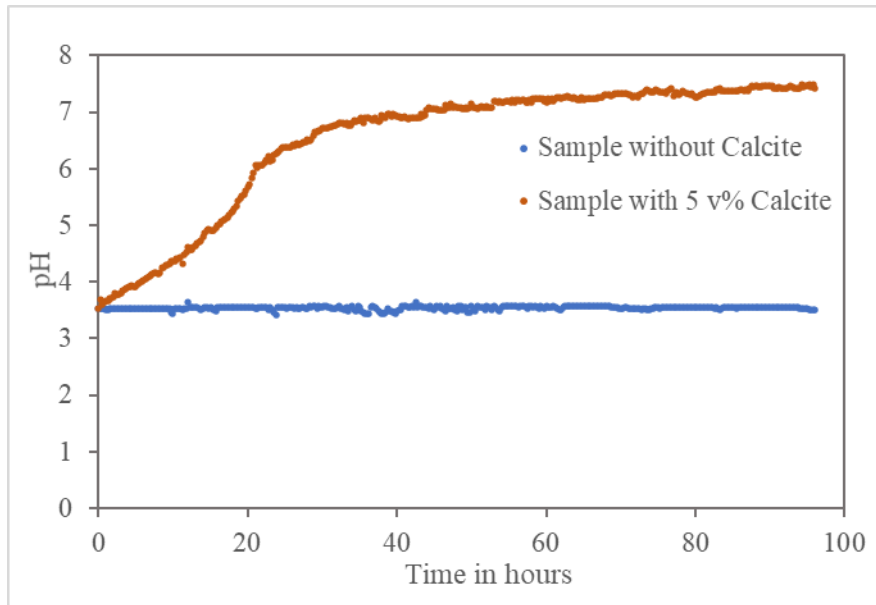


Figure 3 pH evolution for 3D printed samples.

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5 Conclusions

124 DLP 3D printing of reactive porous media was demonstrated where printed samples reflected the
125 reactive properties of real samples through inclusion of calcite within the resin at varied
126 amounts. 3D images of printed samples found calcite content to increase with the resin calcite
127 content, though for the highest volume fraction (7v%) particle settling reduced calcite content in
128 the printed specimen. Improvement (83%) in calcite content for the 7v% was achieved by
129 reducing printing time through a larger layer thickness (50 μ m). With regards to reproducibly
130 replicating porous media characteristics, the extracted porosity were reproducible (standard
131 deviation of 0.28%) and the normalized calcite accessible surface areas agree well with real
132 sandstone samples. Furthermore, calcite dissolution during the batch experiment validated the
133 reactivity of surface present calcite. Overall, DLP printing is a viable means to fabricate
134 replicable reactive porous media.

135

Declaration of Competing Interest

136 The authors declare that they have no known competing financial interests or personal
137 relationships that could have appeared to influence the work reported in this paper.

138

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139
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