

# Effects of laser processing parameters on properties of laser-induced graphene by irradiating CO<sub>2</sub> laser on polyimide

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The emerging technique of carbonization of polyimide (PI) by direct laser writing receives great attention for its flexibility, versatility, and ease-of-patterning capability in creating a variety of functional laser-induced graphene (LIG) sensors and devices. LIG prepared by CO<sub>2</sub> laser irradiating of the PI film is characterized by scanning electron microscopy (SEM), X-ray diffraction (XRD), transmission electron microscope (TEM), specific surface area analyzer, synchronous thermal analysis, and Raman spectroscopy with the focus on investigating the effects of laser parameters (e.g., power, scanning speed) on the microstructure, thickness, and sheet resistance of LIG. Both TEM and XRD indicate that LIG is composed of many graphene layers with a layer spacing of 0.34 nm. The specific surface area of LIG decreases with the increase of laser power. The ratio of the thickness of LIG over the depth of the carbonized PI film as the expansion ratio characterizes the expansibility of LIG. The influence of image resolution and off-focus value on the sheet resistance of LIG is explained by the superposition mechanism of laser scanning spots.

**CO<sub>2</sub> laser, laser parameters, laser-induced graphene, characterization, sheet resistance**

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## 1 Introduction

Graphene, which is a single-layer two-dimensional material with a honeycomb lattice of carbon atoms, has a wide application potential in material science [1–4] due to its unique lattice structure and excellent properties such as high surface area (2630 m<sup>2</sup> g<sup>−1</sup>) [5], large thermal conductivity (3000 W m<sup>−1</sup> K<sup>−1</sup>) [6], high light transmittance (visible and near-infrared absorption of 2.3%) [7], good chemical stability [8] and biocompatibility [9]. Three-dimensional porous graphene is of versatility in the field of flexible electronic

devices with its unique physical and chemical properties being capable of meeting the requirements of most flexible devices, and has become a research hotspot in recent decades [10–15]. Three-dimensional porous graphene has been mainly prepared by chemical vapor deposition (CVD) [16–18], but its scalability is limited [19] since the metal substrate has to be etched. In contrast, the treatment of functionalized graphene solution [20–22] is relatively more economical and scalable since porous graphene coatings can be prepared on various substrates. However, additional patterning steps are required to obtain patterned structures designed specifically to meet the requirements of flexible electronic devices [23]. Economically and environmentally friendly preparation

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processing of three-dimensional porous graphene is a challenge for the development of flexible electronic devices [24–29].

Laser technology, which is non-contact, non-toxic, and highly controllable, can achieve higher precision of thermal induction compared with conventional thermal methods, and has been widely used in material processing and manufacturing, medical treatment, and military instruments [30–33]. The basic working principle of laser technology is the photothermal effect and photochemical effect produced by the interaction between laser and material with its unique one-step laser scribing process being highly promising for a wide range of applications including micro-supercapacitors [34–41], sensors [26,42–45], photodetectors [46], water treatment interfaces [47], and electrocatalysts [48]. Laser-induced graphene (LIG), which is known as three-dimensional porous graphene and can be used as sensitive or electrode material in flexible electronic devices due to its high specific surface area ( $340 \text{ m}^2/\text{g}$ ), high thermal stability under high temperature ( $> 900^\circ\text{C}$ ) and excellent electrical conductivity ( $5\text{--}25 \text{ S/cm}$ ). Prepared by  $\text{CO}_2$  laser ablation of the precursor polyimide (PI) film in the atmosphere [33,34,49–51], the conductive, highly porous three-dimensional LIG with programmable patterns is easily functionalized to form LIG composites with metals, catalytic nanoparticles, aptamer or enzyme for biosensors, micro-supercapacitors, and radiofrequency devices [52–55]. Porous graphene can also be prepared on wood, which expands the material range of precursor, in Ar or  $\text{H}_2$  atmosphere by multiple scanning of variable laser focal lengths [48]. Nitrogen-doped graphene thin films were successfully prepared by laser irradiation of graphite oxide in the  $\text{NH}_3$  atmosphere [56]. A simple, controllable, and low-cost preparation method of LIG modified by manganese dioxide ( $\text{LIG/MnO}_2$ ) was proposed on the basis of laser direct printing technology with good performance of supercapacitor  $\text{LIG/MnO}_2$  [36]. Any material of high carbon can be transformed into porous graphene by laser processing in an inert atmosphere, provided that the energy density of laser processing reaches a critical threshold [48].

In this work, LIG was prepared by  $\text{CO}_2$  laser irradiating PI in the atmosphere with the focus on investigating the influence of laser processing parameters (e.g., laser power, scanning speed, off-focus value, scanning pass, and imported image resolution) on properties of LIG (e.g., thickness, morphology, microstructure, and sheet resistance). LIG was characterized by scanning electron microscopy (SEM), X-ray diffraction (XRD), transmission electron microscope (TEM), specific surface area analyzer, synchronous thermal analysis, and Raman spectroscopy. The influence of laser scanning speed and off-focus value on the sheet resistance of LIG was discussed by the superposition mechanism of laser scanning spots.

## 2 Material preparation and characterization

A laser engraving and cutting system (MUSE) equipped with a  $\text{CO}_2$  laser of wavelength  $\lambda = 10.6 \mu\text{m}$  was used for fabricating LIG under different conditions by varying laser power  $P$ , scanning speed  $v$ , repeated scanning pass  $n$ , image resolution, and off-focus value  $\Delta f$ . PI film of thickness  $125 \mu\text{m}$  was irradiated by a  $\text{CO}_2$  laser in a continuous mode. Large laser power can cause excessive carbonization of PI. Scanning speed,  $v$ , can be adjusted by the software RetinaEngrave 2.0, and the maximum value is  $400 \text{ mm/s}$ . The resolution of the imported scanning pattern needs to be converted, and only three resolutions are available in the RetinaEngrave 2.0, namely  $250 \times 250 \text{ dpi}$ ,  $500 \times 500 \text{ dpi}$ , and  $1000 \times 1000 \text{ dpi}$ . The distance of adjacent laser scanning lines is controlled by image resolution. Both image resolution of pre-designed patterns imported and laser scanning pass,  $n$ , affect sheet resistance of LIG. The rastering image used in the experiment is a rectangular solid area with an aspect ratio of 3:1 drawn by AutoCAD. The off-focus value,  $\Delta f$ , ranging from  $-3$  to  $3 \text{ mm}$  was used to study the influence of spot diameter on the sheet resistance of LIG considering the Gaussian characteristics of the  $\text{CO}_2$  laser beam.

Scanning electron microscopy (SEM) was performed by Quanta 250 to examine the microstructure of LIG processed under different conditions of laser irradiation. Raman spectroscopy was carried out by Invia Reflex Raman microscope with the excitation laser source emitting 10% of full power at a wavelength of  $532 \text{ nm}$ . X-ray diffraction (XRD) was conducted on LIG, which was carefully scraped off from PI to avoid the influence of PI, by a polycrystalline diffractometer DY5261/Xpert3 with  $\text{Cu } K_\alpha$  radiation ( $\lambda = 1.54 \text{ \AA}$ ). Transmission electron microscopy (TEM) and high-resolution TEM (HRTEM) images were obtained using a TECNAI G2 F20 field emission gun transmission electron microscope. TEM samples were prepared by scratching LIG from PI substrate, followed by sonication in alcohol, and dropping the slurry onto a lacey carbon copper grid. The surface area of LIG was measured with a specific surface area and porosity analyzer ASAP2460, and the powder samples were degassed at a temperature of  $300^\circ\text{C}$  for 6 h before the test. Synchronous thermal analysis was carried out by TG Instruments STA449C analyzer ( $10^\circ\text{C min}^{-1}$  from 29 to  $1000^\circ\text{C}$  in nitrogen) in order to characterize carbonization degradation temperature of PI and thermal stability of LIG. Three-dimensional morphologies of LIG and the intact region of PI film after the removal of LIG were characterized by the laser confocal microscope (OLYMPUS FV3000). Due to the dependence of sheet resistance  $R$  of LIG on the size of graphene, the laser scanning area was fixed to be  $18 \text{ mm} \times 6 \text{ mm}$ . Resistance  $R_m$ , from which sheet resistance  $R$  can be calculated ( $R = R_m W/L$ ,  $W$  and  $L$  are the width and length of LIG film, and  $W = 6 \text{ mm}$ ,  $L = 18 \text{ mm}$  in the current

study), was measured by voltammetry (Keithley 2450 digital source meter) with copper tapes and copper wires leading out electrodes. The influence of the contact resistance on the measurement of resistance is ignored, since the contact resistance between the metal wires and LIG is far less (about 1%) than the internal resistance of LIG [57].

### 3 Results and discussion

Figure 1(a)–(d) show scanning electron microscopy (SEM) of LIG obtained at four different powers (i.e., 7.2, 9, 10.8, and 12.6 W). Under a small power of 7.2 W in Figure 1(a), the surface morphology of LIG is uniform and smooth with grooves caused by the linear scanning of the laser. LIG is of a porous structure like foam, whose porosities are created by the gas that is generated by the recombination of heteroatoms [34,35]. When the laser power reaches 9 W, fibrous clusters appear at the overlapping domains of the adjacent scanning lines (Figure 1(b)), leading to the secondary carbonization and structure change of LIG. Most of the region is still porous under 9 W, and the pores under 9 W are larger than those under 7.2 W, indicating that the microstructure can be controlled by laser power. When the laser power reaches 10.8 W in Figure 1(c), the fibrous cluster material extends to the whole surface. The thickness of LIG further increases with the increasing laser power, as observed in the cross-sectional images in Figure 1(e)–(h). With the increase of laser power to  $P = 12.6$  W in Figure 1(d), fiber bundles are formed and entangled with one another to form a network structure with the whole surface being covered by fiber bundles in the absence of porous graphene. The diameters of laser-induced fiber bundles under 12.6 W are larger than those under 10.8 W. The structure of LIG can change from porous foam to fibrous structure bundles with the increase in laser power, which is consistent with the previous literature report [35].

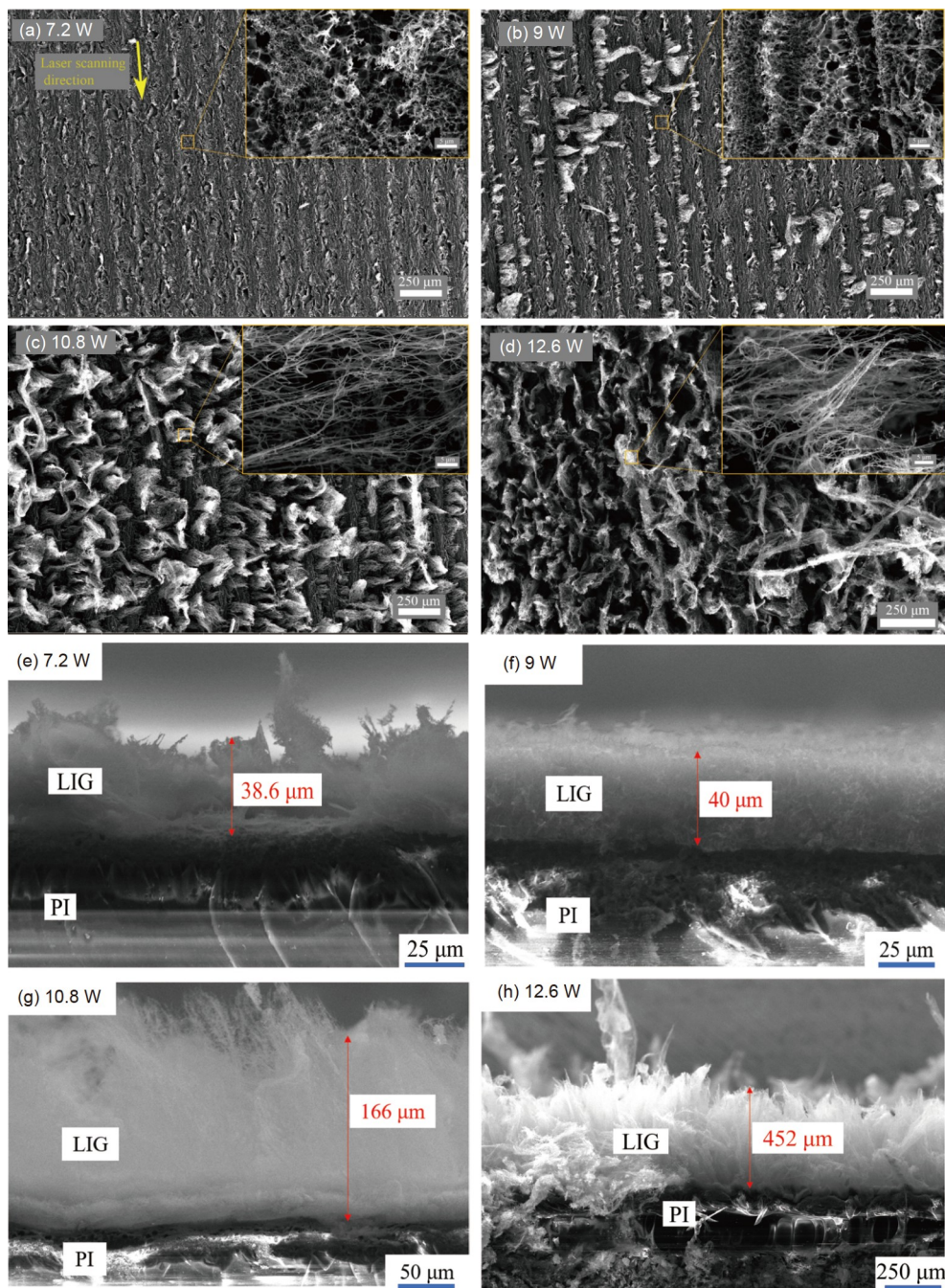
Figure 2(a) shows Raman spectra of precursor PI and LIG prepared at different powers (5.4, 7.2, 9, 10.8, and 12.6 W). PI has no characteristic peak in the Raman spectra, but LIG has three characteristic peaks: (1) D peak at about  $1350\text{ cm}^{-1}$  is the disordered vibration peak of graphene [58] to characterize defect of graphene; (2) G peak near  $1580\text{ cm}^{-1}$  comes from  $E_{2g}$  mode of double degenerate center [59] to characterize the symmetry and order of graphene; and (3) 2D peak at about  $2695\text{ cm}^{-1}$  as in the single-layer graphene [60] is the second-order Raman peak of double phonon resonance to reflect the stacking mode of carbon atom layers [61]. With the increase of laser power, the intensity and half-width of the characteristic peaks vary, but the Raman shift remains unchanged, demonstrating that LIG is successfully generated under the power range used in this study. The intensity ratios  $I_D/I_G$  and  $I_{2D}/I_G$  of LIG prepared at different powers indicate

that defect density and carbon atom stacking mode of graphene vary with laser power (Figure 2(b)). The characteristic peak intensity “ $I$ ” is calculated by integrating the peak area, and the subscript indicates the specific peak (D, 2D, or G). The intensity ratio,  $I_D/I_G$ , reflects the defect density: a larger  $I_D/I_G$  corresponds to a larger defect density of LIG. With the increase of laser power,  $I_D/I_G$  decreases first and then increases, consisting with the previously reported result [34]. When the laser power is 9 W,  $I_D/I_G$  is the minimum (about 0.6), indicating that the graphene defects are the fewest. With the increase in laser power, PI is further carbonized with more generation of LIG and more pores caused by the gas channeling, and LIG can be transformed from porous structure to fibrous bundles. The carbonized degree of PI and creation of pores are two competing mechanisms influencing the defect density of LIG: a higher extent of carbonization improves the stability of LIG, resulting in reduction of defects; while excessive power makes more pores, and LIG can transform from porous structure to fibrous bundles, resulting in the increase of defects, which is demonstrated by the increase in  $I_D/I_G$ . The number of graphene layers can be quantitatively characterized by  $I_{2D}/I_G$ : a larger  $I_{2D}/I_G$  indicates fewer graphene layers. With the increase of laser power, the peak intensity ratio  $I_{2D}/I_G$  decreases gradually, from 1.16 at 5.4 W to 0.86 at 12.6 W, which is caused by the recombination of some suspended bonds, dopants, and defect atoms in graphene due to thermal effect, making LIG with more fibrous bundles become more symmetrical and ordered with more layers [62].

The XRD patterns of LIG prepared under two different powers (5.4 W and 10.8 W) exhibit the prominent peak  $2\theta = 25.9^\circ$  (Figure 3(a)) that corresponds to (002) plane of LIG [35]. The layer spacing  $l$  of LIG can be obtained as  $l = 3.42\text{ \AA}$  by Bragg formula  $n\lambda = 2l\sin\theta$  ( $\lambda = 1.54\text{ \AA}$  is the wavelength of X-ray,  $\theta = 12.95^\circ$  is the incident contact angle,  $n = 1$  for the first-order diffraction), indicating that LIG has a high degree of graphitization. The peak at  $2\theta = 47^\circ$  is indexed to (100) reflections that are associated with in-plane structure [34,63], and is not obvious and only slightly seen.

LIG prepared at 5.4 W has good thermal stability and high graphitization degree (Figure 3(b)), since the weight of LIG decreases slightly below  $1000^\circ\text{C}$  with the small change due to the evaporation of water and the pyrolysis of internal impurities in LIG. Under low temperature ( $< 550^\circ\text{C}$ ), the weight of the precursor material PI decreases slightly with the subtle decrease being caused by dehydration, indicating good heat stability of PI. Under temperatures larger than  $550^\circ\text{C}$ , the pyrolysis becomes prominent, and PI can be carbonized as in the previous results [63]. Successful preparation of LIG requires a sufficiently large temperature, which is controlled by laser power. PI cannot be carbonized under small power, under which the required temperature cannot be met.



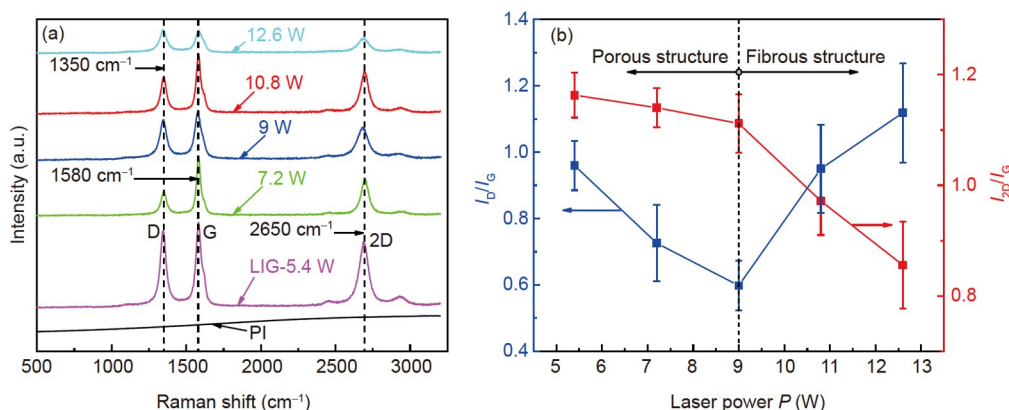


**Figure 1** (Color online) Scanning electron microscope (SEM) images of LIG at different powers (scanning speed  $v = 160$  mm/s, image resolution  $1000 \times 1000$  dpi, off-focus value  $\Delta f = 0$ , scanning pass  $n = 1$ ). (a) 7.2; (b) 9; (c) 10.8; (d) 12.6 W; (e)–(h) are cross-sectional images of LIG prepared at 7.2, 9, 10.8 and 12.6 W, respectively.

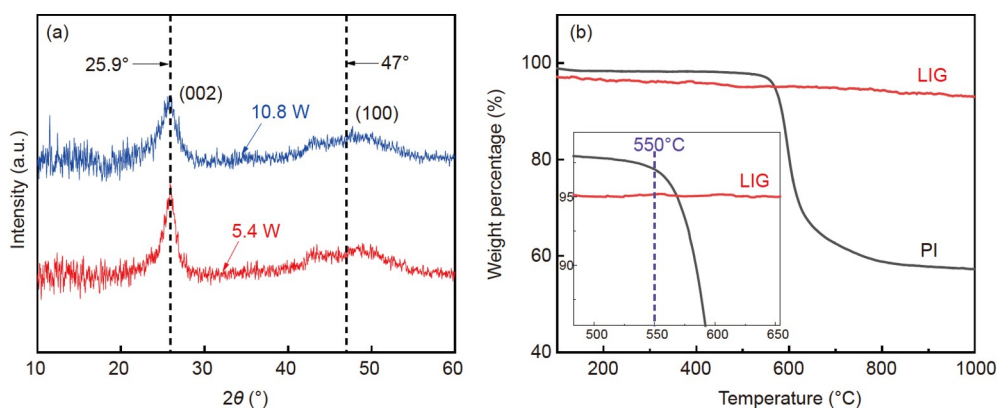
Transmission electron microscopy (TEM) images of LIG prepared by two different laser powers 7.2 and 10.8 W also confirm the observations from XRD and SEM (Figure 4). LIG prepared at 7.2 W is lamellar and similar to the thin silk towel with curl (Figure 4(a)). The high-resolution image of the edge shows that LIG is composed of many graphene layers with layer spacing of 0.34 nm, which is consistent with the layer spacing (i.e., 0.342 nm) obtained by the Bragg formula from the XRD pattern. The LIG obtained at  $P =$

10.8 W is fibrous (Figure 4(b)), which is also consistent with the observation of SEM. Under high laser power (e.g.,  $P = 10.8$  W) to induce high temperature, the lamellar LIG is further pyrolyzed, cracked, and curled into fibrous tubes. The high-resolution image of the edge of the fibrous LIG shows that it is still composed of many graphene layers with the same layer spacing of 0.342 nm, and the layer arrangement is more ordered.

The specific surface area of LIG can be obtained from



**Figure 2** (Color online) (a) Raman spectra of precursor PI and LIG prepared at different powers (scanning speed  $v = 160$  mm/s, image resolution  $1000 \times 1000$  dpi, off-focus value  $\Delta f = 0$ , scanning pass  $n = 1$ ); (b) analysis of D, 2D, and G peak intensities of Raman spectra of LIG.



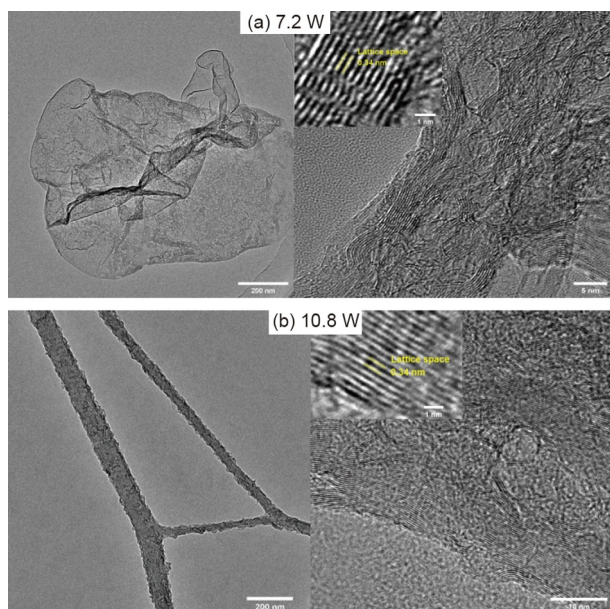
**Figure 3** (Color online) X-ray diffraction (XRD) analysis and thermogravimetric analysis (TGA) (scanning speed  $v = 160$  mm/s, image resolution  $1000 \times 1000$  dpi, off-focus value  $\Delta f = 0$ , scanning pass  $n = 1$ ). (a) XRD of LIG scraped from PI film at 5.4 and 10.8 W; (b) TGA of LIG prepared at 5.4 W and PI substrate under argon.

adsorption and desorption curves of LIGs (Figure 5(a) for 7.2 and 10.8 W) by Brunauer-Emmett-Teller (BET) method [64]. The adsorption and desorption curves of LIG do not coincide, and a hysteresis loop can be observed as in the previous study [65]. The specific surface area of LIG decreases with the increase of laser power, which makes the microstructure of LIG change from porous lamella to curly fibers. The specific surface area of LIG lies within the range from 70 [43] to 340  $\text{m}^2/\text{g}$  [34] reported for laser-induced three-dimensional porous graphene, and is much smaller than that of the monolayer graphene of a single flake (i.e., 2630  $\text{m}^2/\text{g}$ ) [5]. Since laser power has an important influence on the specific surface area of LIG, the values of the specific surface area obtained under large laser powers ( $\geq 7.2$  W) in the present study are reasonably smaller than that (i.e., 340  $\text{m}^2/\text{g}$ ) obtained under a small laser power of 3.6 W [34].

The dependence of sheet resistance  $R$  of LIG on laser power  $P$  is investigated by the experimental setup in Figure 6(a). After the measurement of resistance  $R_m$  from Keithley digital source meter, sheet resistance  $R$  can be obtained as  $R = R_m W/L$ , where  $W$  and  $L$  are the width and length

of LIG film ( $W = 6$  mm,  $L = 18$  mm in the current study). Since the transformation of PI film into porous graphene by laser processing requires that the energy density of laser processing reaches a critical threshold, LIG cannot be prepared under small laser power, which is indicated by the extremely large resistance ( $> 40$  M $\Omega$ ). The sheet resistance  $R$  decreases linearly with the increase of laser power  $P$  as in the previous study [34]. The basic principle of preparing porous graphene by laser direct writing is the photothermal effect of laser radiation on the surface of PI. The unit energy density increases with the increase of laser power, causing further carbonization of PI, which leads to the decrease of sheet resistance. LIG of fibrous microstructure also possesses more contact points or electrically conductive pathways to result in decreased sheet resistance compared to LIG of porous microstructure under the same image resolution. The ordered structure of LIG would be destroyed when  $P > 15$  W, under which sheet resistance would become larger, and macroscopically visible fibrous bundles can suspend and drift in the air. Figure 6(b) presents the dependence of normalized resistance change  $\Delta R/R_0$  ( $\Delta R = R_0 - R$ ,  $R_0$  and  $R$





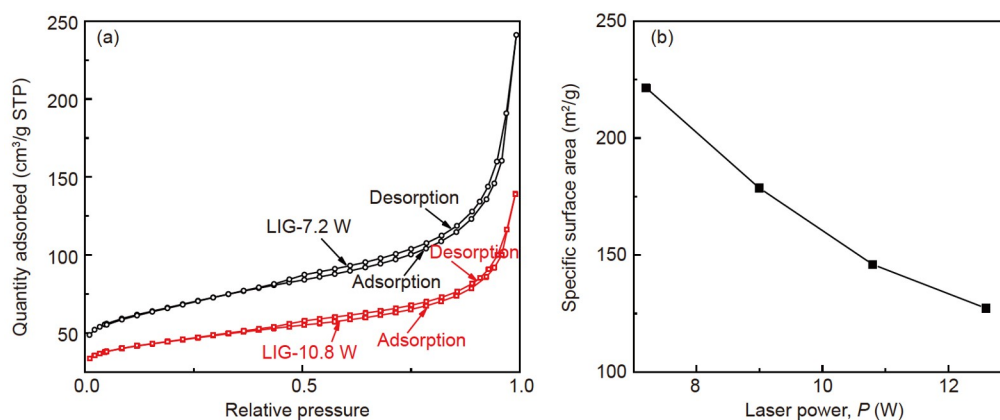
**Figure 4** (Color online) Transmission electron microscopy (TEM) and (HRTEM) images of LIG prepared under two different laser powers (scanning speed  $v = 160$  mm/s, image resolution  $1000 \times 1000$  dpi, off-focus value  $\Delta f = 0$ , scanning pass  $n = 1$ ). (a) 7.2 W; (b) 10.8 W.

represent sheet resistance before and after bending) of LIG on laser power  $P$  for different bending conditions ( $b = 12.5\%$ ,  $25\%$ ).  $\Delta R/R_0$  decreases with the increase of  $P$ , and a larger bending strain produces a greater change in  $\Delta R/R_0$ . However, the effect of bending on  $\Delta R/R_0$  becomes negligibly small under large  $P$ , which can be explained by the theory of contact units [66]. In brief, LIG/PI composite can be regarded as particulate-filled heterogeneous material in nature. The conductivity depends on the number of contact points or electrically conductive pathways of adjacent carbon units. Higher laser power can produce more robust and tight contact carbon units (like fibrous structures), weakening the sensibility of LIG to bending strain.

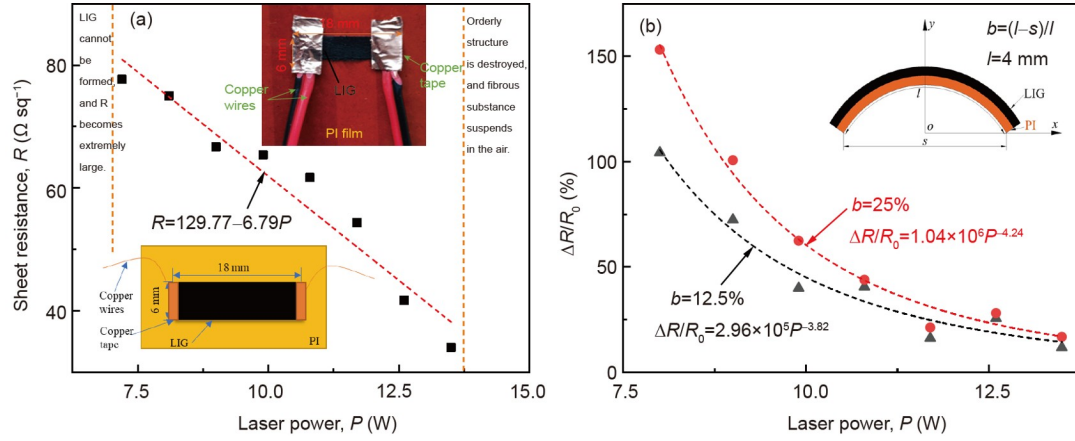
The total thickness  $h_t$  of the prepared LIG can be divided

into two parts with the upper part  $h_u$  above the original surface and the lower part  $h_l$  below the original surface, as shown in Figure 7(a). With the increase of laser power  $P$ , the total thickness  $h_t$  increases slowly in the power range of 6.3–9 W, and  $h_t$  increases sharply when the power becomes larger than 9.9 W. The two-stage variation of  $h_t$  with  $P$  can be explained by noting the microstructure change of LIG from porous structures to fibrous bundles. When the structure is porous under small  $P$ , the energy density absorbed by PI film increases with the increase of  $P$ , leading to the slow increase in  $h_l$ ; when fibrous bundles form under high  $P$ , LIG will expand to a greater extent, resulting in the rapid increase in  $h_t$  with  $P$ . The expansion of LIG is very pronounced, and  $h_t$  can be several times the thickness (i.e.,  $125 \mu\text{m}$ ) of the PI film, which is caused by thermal expansion and internal gas escape, especially under large laser power. A linear relationship between  $h_l$  and  $P$  can be approximated.

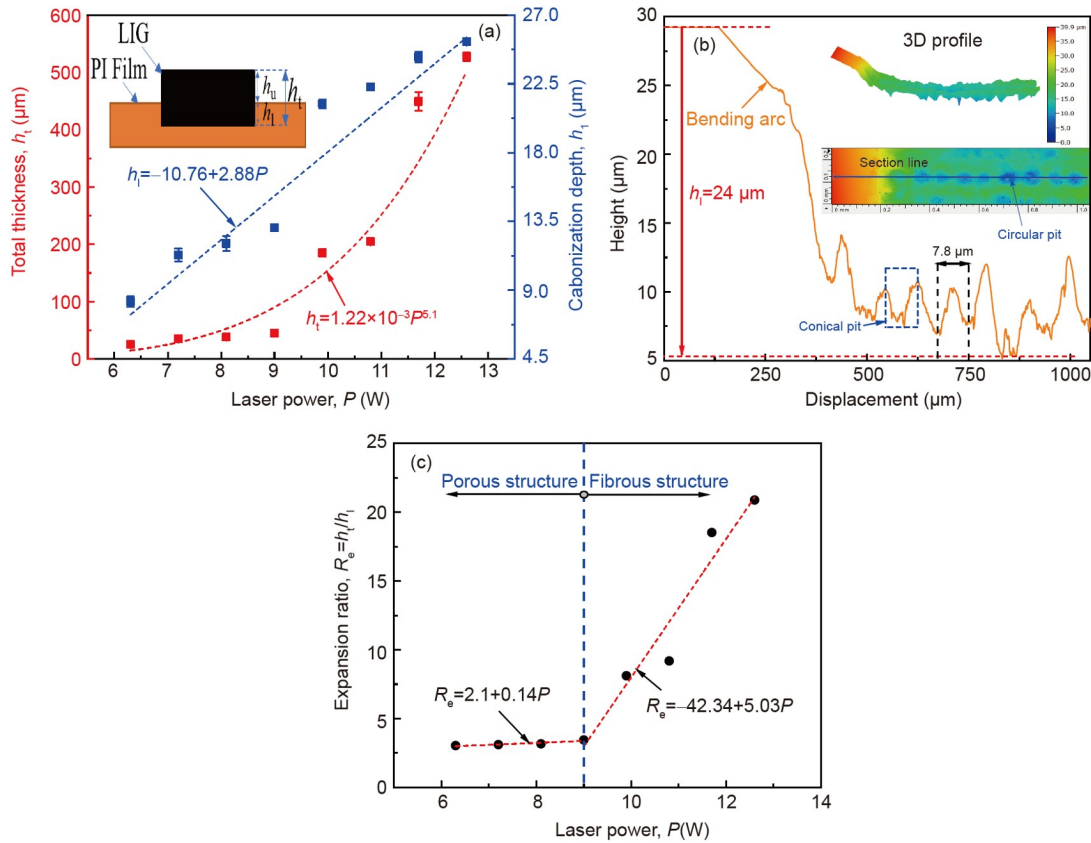
Figure 7(b) shows the height profile of the section line along scanning direction under laser power  $P = 11.7$  W with the inset showing the three-dimensional (3D) image of the intact region of PI after removing LIG. The equidistant conical pits that correspond to the circular regions on the contour plot of the intact region are caused by the Gaussian beam characteristics of the laser. The edges of LIG are not perpendicular to the surface with the bending caused by the thermal-stress-induced deflection of PI film. The diameter of circular pits and the distance between conical pits depend on laser power, scanning velocity, and image resolution (the diameter of circular pits and the distance between adjacent conical pits are both about  $80 \mu\text{m}$  at  $P = 11.7$  W). The carbonization depth of the LIG is determined as the vertical distance between the surface of PI and the bottom of the laser carbonization layer that is revealed by removing LIG. The carbonization depth of  $24 \mu\text{m}$  can be found for  $P = 11.7$  W (Figure 7(b)) based on the three-dimensional image of the residual carbonization region by laser confocal microscope (OLYMPUS FV3000).



**Figure 5** (Color online) (a) Adsorption-desorption curves of LIGs under 7.2 and 10.8 W; (b) the dependence of specific surface area on laser power. Scanning speed  $v = 160$  mm/s, image resolution  $1000 \times 1000$  dpi, off-focus value  $\Delta f = 0$ , scanning pass  $n = 1$ .



**Figure 6** (Color online) Dependence of (a) sheet resistance  $R$  without bending and (b) normalized resistance change  $\Delta R/R_0$  of LIG with bending on laser power  $P$  (scanning speed  $v = 400 \text{ mm/s}$ , image resolution  $1000 \times 1000 \text{ dpi}$ , off-focus value  $\Delta f = 0$ , scanning pass  $n = 1$ ). The insets in (a) show the schematic illustration and the experimental setup for measuring resistance  $R_m$  of the LIG film. The inset in (b) shows the method of bending characterization.



**Figure 7** (Color online) Geometrical characterization of LIG (scanning speed  $v = 400 \text{ mm/s}$ , image resolution  $250 \times 250 \text{ dpi}$ , off-focus value  $\Delta f = 0$ , scanning pass  $n = 1$ ). (a) Dependence of the carbonization depth  $h_i$  of PI and total thicknesses  $h_t$  of LIG film on laser power  $P$ , the inset shows the schematic illustration of  $h_i$  and  $h_t$ ; (b) height profile of the section line on the intact region of PI after removing LIG under  $P = 11.7 \text{ W}$ , the section line is along the scanning direction, the insets show the 3D and surface morphology of the intact region of PI after removing LIG; (c) dependence of expansion ratio  $R_e = h_t/h_i$  on laser power  $P$ .

The expansion ratio  $R_e = h_t/h_i$  characterizes the expansion extent of LIG (Figure 7(c)). The increase in laser power makes LIG expand and also causes the transformation of its microstructure. With the increase in laser power, the expansion ratio increases in a piecewise linear way: the linear fitting slope is  $0.71 \text{ W}^{-1}$  for porous structures (laser power

range of  $6.3\text{--}9 \text{ W}$ ) and  $4.28 \text{ W}^{-1}$  for fibrous bundles (laser power range of  $9\text{--}12.6 \text{ W}$ ). Carbon material of high expansion ratio (e.g., conventional thermal reduction graphene oxide and laser reduced graphene oxide [65]) contains a porous structure for improved sensitivity and ion transport efficiency, which are suitable for sensing and storage of

electrolyte material as high capacitance supercapacitors. Since the expansion ratio ( $R_e > 20$  at  $P = 12.6$  W) of LIG prepared by laser carbonization of PI is much higher than that (about 3 [65]) of thermally reduced graphene oxide, LIG is more suitable for micro-supercapacitors and sensing.

A larger image resolution corresponds to a smaller distance between adjacent pixels, leading to a larger overlap area of adjacent laser spots that are assumed to be circular (inset, Figure 8). The overlap area  $A$  can be calculated as

$$A = 8 \int_{q/2}^{d_0/2} \left( \sqrt{\frac{d_0^2}{4} - x^2} \right) dx$$

$$= \frac{d_0^2}{2} \left( \pi - 2 \arcsin \frac{q}{d_0} - \frac{2q}{d_0} \sqrt{d_0^2 - q^2} \right), \quad (1)$$

where  $d_0$  is the laser spot diameter on the focal plane,  $q$  is the distance between the two adjacent laser beams, and  $x$  is along the scanning direction. The total energy  $E$  in a single circular area can be expressed as

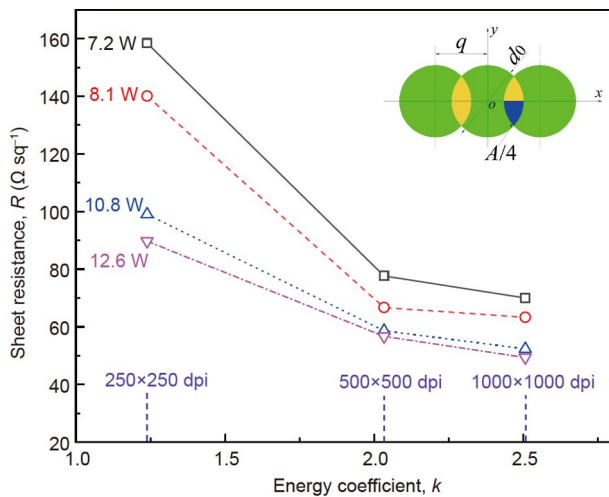
$$E = E_0 + \frac{A}{\pi(d_0/2)^2} E_0$$

$$= \left( 1 + \frac{4A}{\pi d_0^2} \right) E_0 = k E_0, \quad (2)$$

where  $E_0$  is the energy emitted by a single laser beam;  $4A/(\pi d_0^2)$  denotes the energy absorbed by the superimposed region, and  $k$  represents energy coefficient as

$$k = 1 + \frac{2}{\pi} \left( \pi - 2 \arcsin \frac{q}{d_0} - \frac{2q}{d_0} \sqrt{d_0^2 - q^2} \right). \quad (3)$$

With the increase of image resolution, the distance  $q$  between adjacent laser spots decreases from  $q = 78 \mu\text{m}$  for  $250 \times 250$  dpi to  $q = 39 \mu\text{m}$  for  $500 \times 500$  dpi and then to  $q = 19.5 \mu\text{m}$  for  $1000 \times 1000$  dpi. With known laser spot diameter  $d_0 = 100 \mu\text{m}$  under  $\Delta f = 0$ ,  $k$  calculated by eq. (3)



**Figure 8** (Color online) Dependence of sheet resistance  $R$  of LIG on energy coefficient  $k$  (scanning speed  $v = 400$  mm/s, off-focus value  $\Delta f = 0$ , scanning pass  $n = 1$ ) with the inset showing the schematic diagram of laser spot superposition.

increases with the increase of image resolution from 1.239 to 2.033 and then to 2.507 as image resolution increases from  $250 \times 250$  to  $500 \times 500$  and then to  $1000 \times 1000$  dpi. Larger  $k$  corresponds to larger laser energy contributing to more carbonization of the PI film. Therefore, sheet resistance  $R$  of LIG decreases with the increase in energy coefficient  $k$  (Figure 8), since more carbonization of PI can make LIG more electrically conductive. When  $k$  increases from 1.239 (image resolution of  $250 \times 250$  dpi) to 2.033 (image resolution of  $500 \times 500$  dpi), sheet resistance  $R$  decreases significantly, whereas  $R$  decreases slightly as  $k$  further increases from 2.033 to 2.507 (image resolution of  $1000 \times 1000$  dpi). The carbonization of PI tends to saturate under large power, which is manifested by the small difference of  $R$  between 10.8 and 12.6 W. A larger image resolution prepares LIG of a denser microstructure, resulting in more conductive pathways, and thus smaller sheet resistance. The capacitor fabricated by the combination of fibrous LIG prepared at small image resolution and porous LIG prepared at large image resolution was found to have larger capacitance than LIG capacitor of pure porous structure [43].

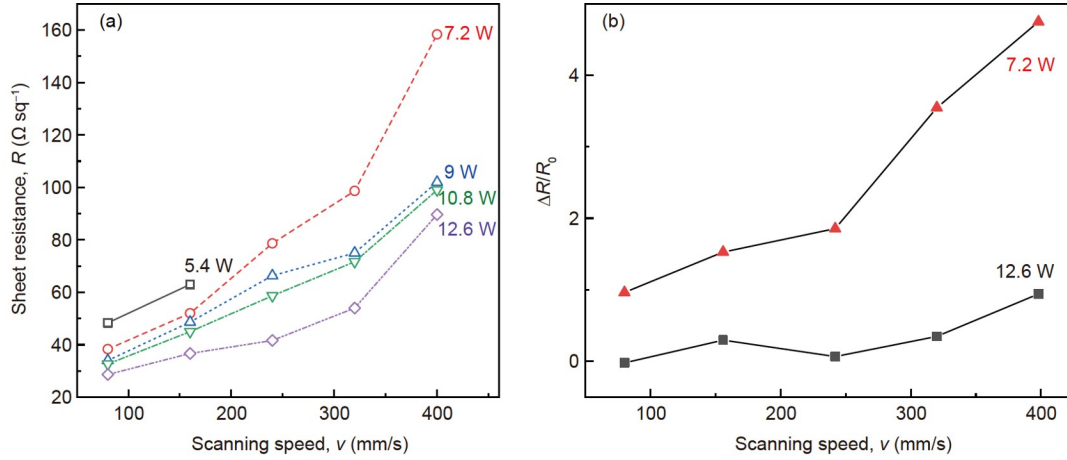
Sheet resistance  $R$  of LIG increases with the increase of scanning speed  $v$  (Figure 9(a)). The significant influence of scanning speed on sheet resistance of LIG can be explained by noting that the scanning speed can affect the unit energy applied to the unit scanned area, since the processing time of thermal effect in a single circular scanning area increases with the decrease of scanning speed. PI film cannot be carbonized into LIG under high scanning speed (e.g.,  $v > 160$  mm/s for  $P = 5.4$  W).  $R$  is more sensitive to  $v$  for small  $P$  ( $< 9$  W), since the extent of carbonization is low under small  $P$ , resulting in a prominent effect of processing time or  $v$  on  $R$ .

Figure 9(b) shows the normalized resistance change  $\Delta R/R_0$  of LIG as a function of laser scanning speed  $v$  for a bending strain of  $b = 12.5\%$ .  $\Delta R/R_0$  increases with the increase of  $v$ , and  $\Delta R/R_0$  from a lower laser power (e.g., 7.2 W) is larger than that from a higher laser power (e.g., 12.6 W) for the same scanning speed. With the increase of laser radiation energy, the microstructure of LIG changes from porous structures to tighter and fibrous bundles, which weakens the sensitivity of sheet resistance on scanning speed.

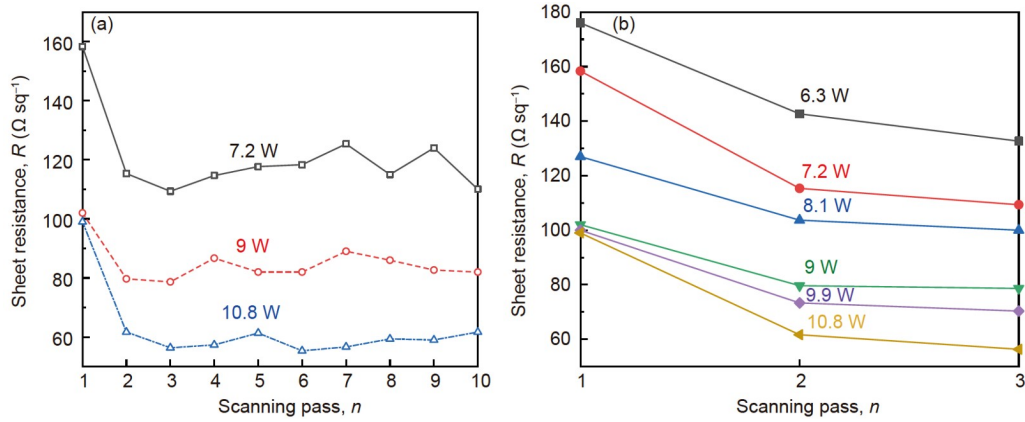
Under three different  $P$  for the laser scanning pass  $n \leq 10$ , sheet resistance  $R$  can be approximated to be constant when  $n \geq 3$  (Figure 10 (a)). The variation of  $R$  under different  $P$  for  $n \leq 3$  exhibits a prominent decrease in  $R$  at  $n = 2$  with a slight decrease at  $n = 3$  (Figure 10(b)). The decrease in  $R$  for  $n \leq 3$  can be explained by noting that more scanning passes can make LIG more homogeneous and uniform with more carbonization of PI, while the little change of  $R$  for  $n \geq 3$  is caused by the saturation of carbonization.

In the schematic diagram of the working area of the laser beam (Figure 11(a)),  $f$  represents focal length,  $L$  denotes the

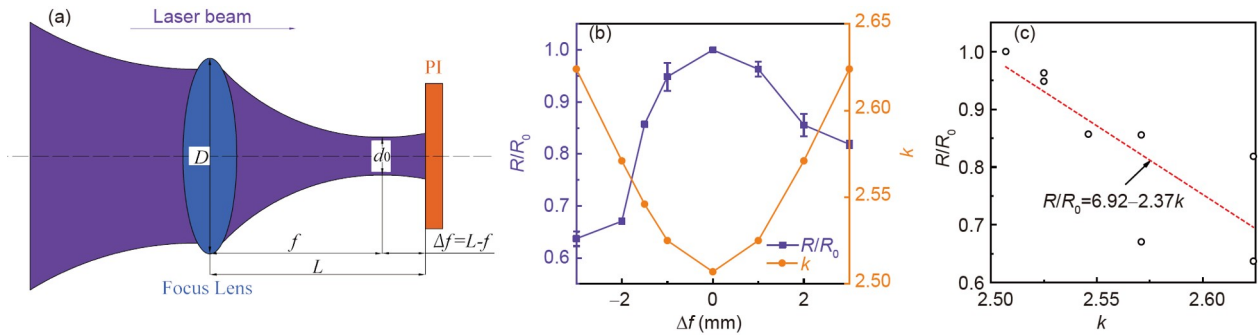




**Figure 9** (Color online) Dependence of (a) sheet resistance  $R$  without bending and (b) normalized resistance change  $\Delta R/R_0$  of LIG with bending ( $b = 12.5\%$ ) on laser speed scanning  $v$  (image resolution  $250 \times 250$  dpi, off-focus value  $\Delta f = 0$ , and scanning pass  $n = 1$ ).



**Figure 10** (Color online) Variation of sheet resistance  $R$  of LIG with scanning pass  $n$  (scanning speed  $v = 400$  mm/s, image resolution  $250 \times 250$  dpi, off-focus value off-focus value  $\Delta f = 0$ ). (a)  $n \leq 10$  under three different  $P$ ; (b)  $n \leq 3$  under different  $P$ .



**Figure 11** (Color online) Influence of off-focus value (laser power  $P = 9.9$  W, scanning speed  $v = 400$  mm/s, image resolution  $1000 \times 1000$  dpi, scanning pass  $n = 1$ ). (a) Schematic diagram of the working area of the laser beam; (b) dependence of normalized  $R$  (by  $R_0$  at  $\Delta f = 0$ ) and energy coefficient  $k$  by eq. (5) on off-focus value  $\Delta f$ ; (c) dependence of  $R/R_0$  on  $k$ .

distance between the focal lens and PI surface, and  $d_0$  is the diameter of the laser spot on the focal plane.  $\Delta f = L - f$  is off-focus value with positive defocus ( $\Delta f > 0$ ) corresponding to the case that the focal plane is above the sample surface and

negative defocus ( $\Delta f < 0$ ) corresponding to the case that the focal plane is below the sample surface. The diameter  $d$  of the laser spot on the PI surface can be calculated according to Gaussian beam characteristics:

$$d = d_0 \sqrt{1 + \left(\frac{\Delta f}{f}\right)^2}, \quad (4)$$

where  $d$  increases with the increase of  $\Delta f$ . If the off-focus value is considered,  $d_0$  should be changed to  $d$  in Eq. (3), so that the energy coefficient  $k$  can be expressed as

$$k = 1 + \frac{2}{\pi} \left[ \pi - 2 \arcsin \frac{q}{d_0 \sqrt{1 + \left(\frac{\Delta f}{f}\right)^2}} - \frac{2q}{d_0^2 \left[ 1 + \left(\frac{\Delta f}{f}\right)^2 \right] \sqrt{d_0^2 \left[ 1 + \left(\frac{\Delta f}{f}\right)^2 \right] - q^2}} \right], \quad (5)$$

where  $q = 19.5 \mu\text{m}$  for  $1000 \times 1000 \text{ dpi}$ ,  $f = 3.5 \text{ mm}$ , and  $d_0 = 100 \mu\text{m}$ .

Figure 11(b) shows the dependence of the relative resistance  $R/R_0$  ( $R$  is resistance considering off-focus value, and  $R_0$  is the resistance at  $\Delta f = 0$ ) and the energy coefficient  $k$  on off-focus value  $\Delta f$ .  $R/R_0$  decreases with the increase of the absolute value of  $\Delta f$ , and  $R$  reaches the minimum value at zero off-focus value. Since both energy coefficient  $k$  and spot diameter  $d$  increase with the increase in the absolute value of  $\Delta f$ , a larger  $|\Delta f|$  results in more carbonization of PI and more homogenous structure of LIG for a smaller sheet resistance. In the case of negative defocus ( $\Delta f < 0$ ), the maximum energy density surface (i.e., the focal plane) is located in the interior of the sample [67], making the carbonization process start from the interior of PI, which is the reason why the resistance decreases more sharply for  $\Delta f < 0$  than that for  $\Delta f > 0$ , under which condition the focal plane is above the PI surface. A linear relationship between  $R/R_0$  and  $k$  can be approximated as shown in Figure 11(c). The decrease in  $R/R_0$  with  $k$  can be explained from the perspective of energy, since a larger  $k$  corresponds to more energy for carbonization of PI, resulting in lower sheet resistance.

## 4 Conclusions

LIG was prepared by laser direct writing technology with the focus on characterizing the influence of laser parameters on the structure and sheet resistance of LIG. The microstructure of LIG changes from porous structure to fibrous bundles with the increase of laser power. Both thickness and expansion ratio increase with laser power. The expansion of LIG is very pronounced with the total thickness being several times the thickness of PI film. TEM observation shows that LIG is composed of many graphene layers with layer spacing of  $0.34 \text{ nm}$ , which is consistent with the layer spacing obtained

from the XRD pattern by the Bragg formula. The specific surface area of LIG decreases with the increase of laser power. Laser power was found to have a great influence on the morphology, thickness, and sheet resistance of LIG. Laser processing parameters such as laser power, scanning speed, image resolution, scanning pass, and off-focus value all have significant effects on the sheet resistance of LIG. The smaller sheet resistance of LIG can be achieved under a larger laser power, a smaller scanning speed, a smaller off-focus value (absolute value), and a higher image resolution due to the larger energy consumed by PI. In addition, with the increase of laser radiation energy, the microstructure of LIG changes from porous to tighter fibrous structure, weakening its bending strain sensitivity. A second laser scan can make sheet resistance decrease significantly with little effect after three scanning passes due to the saturation of carbonization of PI. The superposition mechanism of adjacent laser spots can be used to explain the influence of image resolution and off-focus value on the energy consumed by PI and thus on the sheet resistance of LIG. The understanding of the influence of laser processing parameters on microstructure and electrical conductivity paves the way for the rational design of LIG-based flexible electronic devices with improved sensing performance and reduced energy consumption.

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