# Chance-Constrained Controller State and Reference Governor \*

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#### Abstract

The controller state and reference governor (CSRG) is an add-on scheme for nominal closed-loop systems with dynamic controllers which supervises the controller internal state and the reference input to the closed-loop system to enforce pointwisein-time constraints. By admitting both controller state and reference modifications, the CSRG can achieve an enlarged constrained domain of attraction compared to conventional reference governor schemes where only reference modification is permitted. This paper studies the CSRG for systems subject to stochastic disturbances and chance constraints. We describe the CSRG algorithm in such a stochastic setting and analyze its theoretical properties, including chance-constraint enforcement, finite-time reference convergence, and closed-loop stability. We also present examples illustrating the application of CSRG to constrained aircraft flight control.

Key words: Constrained systems, Stochastic systems, Predictive control, Reference governors

### 1 Introduction

Reference governors (RGs) are add-on control schemes used to protect pre-stabilized, closed-loop systems against violations of pointwise-in-time constraints (Garone et al., 2017). They do so by monitoring, and modifying when necessary, the reference input to the closed-loop system. Instead of (re-)designing a controller that simultaneously achieves stabilization and constraint enforcement (as well as other performance requirements) as in the model predictive control framework (Mayne et al., 2000), the RG setting preserves the existing/legacy architecture of the closed-loop system, while augmenting the nominal system with the ability to handle constraints.

An extension of the RG, called the *controller state and* reference governor (CSRG), was proposed for closedloop systems with dynamic controllers in McDonough and Kolmanovsky (2015a). The CSRG monitors and modifies not only the reference input to the closed-loop system but also the internal state of the dynamic controller (see Fig. 1). By allowing both controller state and reference modifications, the constrained domain of attraction, i.e., the set of initial states which can be recovered without constraint violation, is enlarged. It is worth noting that the approach of modifying/resetting controller state has also been exploited in classical nonlinear control, mainly for improving control performance. For instance, Bupp et al. (2000) proposed a control strategy called the resetting virtual absorber, where the controller state is periodically reset to dissipate energy from a vibrating system. In contrast, the CSRG modifies the controller state for enforcing constraints, which has not been broadly investigated before.



Fig. 1. Schematic of the controller state and reference governor (CSRG).

We note that the CSRG is also different from the extended command governor (ECG) (Gilbert and Ong, 2011). The ECG uses an auxiliary linear system to predict and plan the future evolution of the reference signal. As it does not restrict the reference signal modification over the planning horizon to a constant, as in conventional RGs, it can also lead to an enlarged constrained domain of attraction (Gilbert and Ong, 2011). However, the ECG still only modifies the reference input to the closed-loop system. In contrast, the CSRG also modifies the internal state of the controller, which is as an existing part of the closed-loop system. On the one hand, the extra degree of freedom created by controller state modification can translate into opportunities to further

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improve performance. On the other hand, due to controller state modification, the theoretical and computational properties of the CSRG are different from the ECG. Their analyses also require new techniques, which are addressed in this paper. The extension of ECG to the stochastic setting and schemes that combine CSRG and ECG in deterministic and stochastic settings are worth investigating. These developments are left to future research.

Conventional RG schemes, including the CSRG studied in McDonough and Kolmanovsky (2015a), are able to enforce constraints for deterministic systems (Bemporad et al., 1997; Bemporad, 1998; Borrelli et al., 2009), or robustly enforce constraints for systems subject to disturbance inputs that take values in compact sets (Gilbert and Kolmanovsky, 1999; Casavola et al., 2000; Gilbert and Kolmanovsky, 2002; Gilbert and Ong, 2011; Li et al., 2020). However, in many application scenarios, the system is acted on by disturbances which are represented by stochastic models. For instance, the effect of wind gusts on an aircraft can be modeled by stochastic von Kármán and Dryden's models (Hoblit, 1988). Electrical loads in power grids, computational loads in data centers, and product demand in supply chain management are also frequently modeled stochastically (Zhang and Li, 2011; Guo et al., 2013; Li et al., 2021). In this setting, a typical approach is to impose constraints as *chance constraints*, i.e., seek probabilistic guarantees on constraint satisfaction (Birge and Louveaux, 2011).

In recent years, there has been a growing interest in developing control techniques for systems subject to stochastic disturbances and chance constraints, mainly within the stochastic model predictive control framework (see Mesbah (2016); Mesbah et al. (2019) and references therein). A RG for chance-constrained systems was developed in Kalabić et al. (2017, 2019), which exhibited theoretical properties that were analogous to the ones for conventional RGs, including chance-constraint enforcement and reference convergence guarantees. Another stochastic approach to RG design was proposed in Osorio and Ossareh (2018), which, differently from Kalabić et al. (2017, 2019), treated disturbances that had compact support but exploited their probabilistic information to alleviate the conservativeness of conventional robust RG designs.

In this paper, we study the CSRG in a stochastic setting. The contributions of this paper are as follows:

- (1) We develop a CSRG scheme for discrete-time linear systems subject to stochastic disturbances and chance constraints. This CSRG scheme operates based on a finitely-determined approximation to a chance-constrained maximal output admissible set and online optimization. In particular, two online algorithms with distinct features are presented.
- (2) We analyze theoretical properties of the proposed CSRG scheme, including finite-determinability of the used output admissible set, closed-loop chanceconstraint satisfaction, almost-sure finite-time convergence of the modified reference to constant,

steady-state constraint-admissible commands, and mean-square stability of the commanded state set-point. These theoretical properties distinguish our CSRG scheme versus several other control techniques for systems subject to stochastic disturbances and chance constraints. For instance, in stochastic model predictive control, guarantees on closed-loop chance-constraint satisfaction and closed-loop stability are typically not easy to establish (Mesbah, 2016), especially in the presence of disturbances with unbounded supports (such as the Gaussian disturbance treated in this paper).

- (3) We extend the proposed CSRG scheme from its nominal formulation for the case of individual chance constraints to the one that can address joint chance constraints. We describe two approaches to this extension and compare their relative conservativeness, resulting in guidelines for when one approach is preferable over the other.
- (4) We illustrate the proposed chance-constrained CSRG scheme through examples representing its application to constrained aircraft flight control. With these examples, we also verify that applying the proposed chance-constrained CSRG can lead to a considerably larger constrained domain of attraction than a stochastic RG with only reference modification.

The paper is organized as follows. In Section 2, we define the system and the constraints to be treated. In Section 3, we present the chance-constrained CSRG scheme, including offline construction of the maximal output admissible set and two online CSRG algorithms. In Section 4, we analyze theoretical properties of the proposed CSRG scheme. In Section 5, we extend the scheme from treating individual chance constraints to treating joint chance constraints. In Section 6, we present examples illustrating application of CSRG to constrained aircraft flight control. Finally, Section 7 concludes the paper.

# 2 Problem Statement

In this paper, we consider systems which can be represented by discrete-time linear models of the form,

$$x_p(t+1) = Ax_p(t) + B_u u(t) + B_w w(t),$$
(1a)

$$y(t) = Cx_p(t) + D_u u(t) + D_w w(t),$$
 (1b)

where  $x_p(t) \in \mathbb{R}^{n_{x_p}}$  represents the plant state at the discrete-time instant  $t \in \mathbb{Z}_{\geq 0}$ ,  $u(t) \in \mathbb{R}^{n_u}$  denotes the control input,  $w(t) \in \mathbb{R}^{n_w}$  denotes an unmeasured disturbance input, and  $y(t) \in \mathbb{R}^{n_y}$  represents the system output. We assume that the following dynamic controller has been designed to stabilize the system (1),

$$u(t) = K_p x_p(t) + K_u x_u(t) + B_v v(t),$$
 (2a)

$$x_u(t+1) = A_p x_p(t) + A_u x_u(t) + D_v v(t),$$
 (2b)

where  $x_u(t) \in \mathbb{R}^{n_{xu}}$  denotes the controller state, and  $v(t) \in \mathbb{R}^{n_v}$  is a reference input determining the set-point

of the system. The closed-loop system combining (1) and (2) can be written in the following compact form,

$$\bar{x}(t+1) = \bar{A}\bar{x}(t) + \bar{B}_v v(t) + \bar{B}_w w(t), \qquad (3a)$$

$$y(t) = \bar{C}\bar{x}(t) + \bar{D}_v v(t) + \bar{D}_w w(t), \qquad (3b)$$

where  $\bar{x}(t) = [x_p^{\top}(t), x_u^{\top}(t)]^{\top}$ , and

$$\bar{A} = \begin{bmatrix} A + B_u K_p & B_u K_u \\ A_p & A_u \end{bmatrix}, \ \bar{B}_v = \begin{bmatrix} B_u B_v \\ D_v \end{bmatrix}, \ \bar{B}_w = \begin{bmatrix} B_w \\ 0 \\ (4) \end{bmatrix},$$
$$\bar{C} = \begin{bmatrix} C + D_u K_p & D_u K_u \end{bmatrix}, \ \bar{D}_v = D_u B_v, \ \bar{D}_w = D_w.$$

We make the following assumptions:

Assumption 1: The matrix  $\overline{A}$  is Schur, i.e., all eigenvalues of  $\overline{A}$  are strictly inside the unit disc.

Since  $\overline{A}$  corresponds to the closed-loop system consisting of the plant (1) and the stabilizing controller (2), Assumption 1 is reasonable. With Assumption 1, under any constant reference input  $v(t) \equiv r$ , the associated steady-state values of  $\overline{x}(t)$  and y(t), denoted as

$$\bar{x}^*(r) = \begin{bmatrix} x_p^*(r) \\ x_u^*(r) \end{bmatrix} = (I - \bar{A})^{-1} \bar{B}_v r, \qquad (5a)$$

$$y^*(r) = \left(\bar{C}(I - \bar{A})^{-1}\bar{B}_v + \bar{D}_v\right)r,$$
 (5b)

are exponentially stable in the disturbance-free case (i.e., with  $w(t) \equiv 0$ ).

Assumption 2: The disturbance inputs  $\{w(t)\}_{t\in\mathbb{Z}_{\geq 0}}$  are independent and identically distributed (i.i.d) Gaussian random variables with zero mean and covariance matrix W. They are also independent of  $\bar{x}(0)$  and  $\{v(t)\}_{t\in\mathbb{Z}_{\geq 0}}$ . We denote such disturbance inputs as

$$\{w(t)\}_{t\in\mathbb{Z}_{>0}}\sim\mathcal{N}(0,W).$$
(6)

The system is assumed to be subject to the following set of linear inequality constraints for all  $t \in \mathbb{Z}_{\geq 0}$ ,

$$G_i^{+} y(t) \le g_i, \quad i = 1, ..., n_g,$$
 (7)

where  $G_i \in \mathbb{R}^{n_y}$  and  $g_i \in \mathbb{R}$ . Because the Gaussian disturbance inputs  $\{w(t)\}_{t \in \mathbb{Z}_{\geq 0}} \sim \mathcal{N}(0, W)$  are not compactly supported, it is generally not possible to enforce constraints (7) deterministically. Instead, we are interested in enforcing them with high probabilities – we consider the following set of chance constraints,

$$\mathbb{P}\left\{G_i^{\top} y(t) \le g_i\right\} \ge \beta_i, \quad i = 1, ..., n_g, \tag{8}$$

with  $\beta_i \in (0.5, 1)$  being specified confidence levels of constraint satisfaction.

In what follows, we introduce a controller state and reference governor (CSRG) scheme to enforce (8).

#### 3 Controller State and Reference Governor

The CSRG is an add-on scheme for the closed-loop system (3) that supervises the controller state  $x_u(t)$  and the reference input v(t) to enforce the constraints (8). As an extension of both the deterministic CSRG in Mc-Donough and Kolmanovsky (2015a) and the stochastic RG in Kalabić et al. (2019), our stochastic CSRG utilizes the following maximal output admissible set,

$$\mathcal{O}_{\infty} = \bigcap_{i=1}^{n_g} \mathcal{O}_{\infty}^i, \tag{9}$$

where  $\mathcal{O}^i_{\infty}$  is defined as

$$\mathcal{O}_{\infty}^{i} = \left\{ (x_{p}, x_{u}, v) \in \mathbb{R}^{n_{xp}} \times \mathbb{R}^{n_{xu}} \times \mathbb{R}^{n_{v}} : \text{ if } x_{p}(0) = x_{p}, \\ x_{u}(0) = x_{u}, v(t) \equiv v, \text{ and } \{w(t)\}_{t \in \mathbb{Z}_{\geq 0}} \sim \mathcal{N}(0, W), \\ \text{ then } \mathbb{P}\left\{ G_{i}^{\top} y(t) \leq g_{i} \right\} \geq \beta_{i} \text{ for all } t \in \mathbb{Z}_{\geq 0} \right\}.$$
(10)

With  $\mathcal{O}_{\infty}$ , the CSRG determines the values of  $x_u(t)$  and v(t) based on the following optimization problem,

$$\min_{x_u,v} \quad J\left(x_u, v, x_p(t), r(t)\right), \tag{11a}$$

subject to 
$$(x_p(t), x_u, v) \in \mathcal{O}_{\infty},$$
 (11b)

with the cost function defined as

$$J(x_{u}, v, x_{p}(t), r(t)) = \left\| \begin{bmatrix} x_{p}(t) \\ x_{u} \end{bmatrix} - \begin{bmatrix} x_{p}^{*}(v) \\ x_{u}^{*}(v) \end{bmatrix} \right\|_{P}^{2} + \|v - r(t)\|_{R}^{2}$$
$$= \left\| \begin{bmatrix} x_{p}(t) \\ x_{u} \end{bmatrix} - (I - \bar{A})^{-1} \bar{B}_{v} v \right\|_{P}^{2} + \|v - r(t)\|_{R}^{2}, \quad (12)$$

where  $x_p(t)$  is the current plant state value, r(t) denotes the commanded/nominal value of the reference input, typically provided by a human operator or a higher-level planning algorithm, and  $\|\cdot\|_P = \sqrt{(\cdot)^\top P(\cdot)}, \|\cdot\|_R = \sqrt{(\cdot)^\top R(\cdot)}$  with P, R being positive-definite matrices. In particular, the matrix P is selected as the positivedefinite solution to the Lyapunov equation,

$$\bar{A}^{+}P\bar{A} - P + Q = 0,$$
 (13)

with Q being a positive-definite matrix. Such a choice of P facilitates the establishment of stability guarantee of the closed-loop system (see Proposition 4). Note that the cost function (12) is convex quadratic in the decision variables  $(x_u, v)$ .

#### 3.1 Maximal output admissible set

The CSRG enforces the chance constraints (8) using the maximal output admissible set  $\mathcal{O}_{\infty}$  defined by (9) and (10). In this section, we address the explicit expression and algorithmic determination of  $\mathcal{O}_{\infty}$ .

Given  $\bar{x}(0) = [x_p^{\top}(0), x_u^{\top}(0)]^{\top}, v(t) \equiv v$  and  $\{w(t)\}_{t \in \mathbb{Z}_{\geq 0}} \sim \mathcal{N}(0, W)$ , the outputs of (3) are normally distributed according to

$$y(t) \sim \mathcal{N}\left(\bar{y}(t), \Sigma_y(t)\right),$$
 (14)

where the mean  $\bar{y}(t)$  is determined as

$$\bar{y}(t) = \bar{C}\bar{A}^t\bar{x}(0) + \left(\bar{C}\sum_{k=0}^{t-1}\bar{A}^k\bar{B}_v + \bar{D}_v\right)v, \qquad (15)$$

and the covariance  $\Sigma_y(t)$  satisfies

$$\Sigma_x(t+1) = \bar{A}\Sigma_x(t)\bar{A}^\top + \bar{B}_w W \bar{B}_w^\top, \qquad (16a)$$
$$\Sigma_y(t) = \bar{C}\Sigma_x(t)\bar{C}^\top + \bar{D}_w W \bar{D}_w^\top, \qquad (16b)$$

with  $\Sigma_x(0) = 0$ . From (16) and  $\Sigma_x(0) = 0$ , one can also derive the following explicit expression for  $\Sigma_y(t)$ ,

$$\Sigma_y(t) = \bar{C} \left( \sum_{k=0}^{t-1} \bar{A}^k \bar{B}_w W \bar{B}_w^\top (\bar{A}^\top)^k \right) \bar{C}^\top + \bar{D}_w W \bar{D}_w^\top.$$
(17)

Based on (14),  $G_i^{\top} y(t) \in \mathbb{R}$  is normally distributed according to

$$G_i^{\top} y(t) \sim \mathcal{N} \left( G_i^{\top} \bar{y}(t), G_i^{\top} \Sigma_y(t) G_i \right).$$
(18)

Then, the probability  $\mathbb{P}\left\{G_i^\top y(t) \leq g_i\right\}$  is computed as

$$\mathbb{P}\left\{G_{i}^{\top}y(t) \leq g_{i}\right\} = \Phi\left(\frac{g_{i} - G_{i}^{\top}\bar{y}(t)}{\sqrt{G_{i}^{\top}\Sigma_{y}(t)G_{i}}}\right)$$

$$= \frac{1}{2}\left[1 + \operatorname{erf}\left(\frac{g_{i} - G_{i}^{\top}\bar{y}(t)}{\sqrt{2G_{i}^{\top}\Sigma_{y}(t)G_{i}}}\right)\right],$$
(19)

where  $\Phi(\cdot)$  denotes the cumulative distribution function of the standard normal distribution and  $\operatorname{erf}(\cdot)$  denotes the error function

$$\operatorname{erf}(z) = \frac{2}{\sqrt{\pi}} \int_0^z e^{-t^2} dt.$$
 (20)

Note that  $\Phi(\cdot)$  and  $\operatorname{erf}(\cdot)$  are related according to  $\Phi(z) = \frac{1}{2} \left[ 1 + \operatorname{erf}\left(\frac{z}{\sqrt{2}}\right) \right].$ 

Then, the chance constraint (8) becomes

$$\frac{1}{2} \left[ 1 + \operatorname{erf}\left(\frac{g_i - G_i^{\top} \bar{y}(t)}{\sqrt{2G_i^{\top} \Sigma_y(t)G_i}}\right) \right] \ge \beta_i, \qquad (21)$$

which can be equivalently written as

$$G_i^{\top} \bar{y}(t) = G_i^{\top} \bar{C} \bar{A}^t \begin{bmatrix} x_p(0) \\ x_u(0) \end{bmatrix} + G_i^{\top} \left( \bar{C} \sum_{k=0}^{t-1} \bar{A}^k \bar{B}_v + \bar{D}_v \right) v$$
$$\leq g_i - \sqrt{2G_i^{\top} \Sigma_y(t)} G_i \operatorname{erf}^{-1} \left( 2\beta_i - 1 \right), \qquad (22)$$

where  $\operatorname{erf}^{-1}(\cdot)$  denotes the inverse of the error function  $\operatorname{erf}(\cdot)$ . Note that the  $\Sigma_y(t)$  in (22), computed from (16), is independent of  $(x_p(0), x_u(0), v)$ , and accordingly, (22) is a linear inequality condition on the triple  $(x_p(0), x_u(0), v)$ .

With (22), the set  $\mathcal{O}^i_\infty$  defined in (10) can be explicitly expressed as

$$\mathcal{O}_{\infty}^{i} = \left\{ (x_{p}, x_{u}, v) : G_{i}^{\top} \bar{C} \bar{A}^{t} \begin{bmatrix} x_{p} \\ x_{u} \end{bmatrix} + G_{i}^{\top} \left( \bar{C} \sum_{k=0}^{t-1} \bar{A}^{k} \bar{B}_{v} + \bar{D}_{v} \right) v \leq g_{i} - \sqrt{2G_{i}^{\top} \Sigma_{y}(t) G_{i}} \operatorname{erf}^{-1} (2\beta_{i} - 1), \forall t \in \mathbb{Z}_{\geq 0} \right\}.$$
(23)

The set  $\mathcal{O}_{\infty}^{i}$  in (23) is characterized by an infinite number of linear inequalities ( $\forall t \in \mathbb{Z}_{\geq 0}$ ) and cannot be finitely determined in general, and so is  $\mathcal{O}_{\infty} = \bigcap_{i=1}^{n_g} \mathcal{O}_{\infty}^{i}$ . Hence, we consider inner approximations of  $\mathcal{O}_{\infty}^{i}$  and  $\mathcal{O}_{\infty}$ , denoted by  $\tilde{\mathcal{O}}_{\infty}^{i}$  and  $\tilde{\mathcal{O}}_{\infty}$  respectively, which are defined as

$$\tilde{\mathcal{O}}_{\infty}^{i} = \mathcal{O}_{\infty}^{i} \cap \left( \mathbb{R}^{n_{xp}} \times \mathbb{R}^{n_{xu}} \times \tilde{\Omega}^{i} \right), \qquad (24a)$$

$$\tilde{\mathcal{O}}_{\infty} = \bigcap_{i=1}^{n_g} \tilde{\mathcal{O}}_{\infty}^i, \qquad (24b)$$

where  $\tilde{\Omega}^i$  is a compact and convex subset of  $int(\Omega^i)$  with nonempty interior. The set  $\Omega^i \subset \mathbb{R}^{n_v}$  is defined as

$$\Omega^{i} = \left\{ v \in \mathbb{R}^{n_{v}} : G_{i}^{\top} \left( \bar{C} (I - \bar{A})^{-1} \bar{B}_{v} + \bar{D}_{v} \right) v \\ \leq g_{i} - \sqrt{2G_{i}^{\top} \Sigma_{y}^{\infty} G_{i}} \operatorname{erf}^{-1} \left( 2\beta_{i} - 1 \right) \right\}, \quad (25)$$

if  $G_i^{\top} \left( \bar{C} (I - \bar{A})^{-1} \bar{B}_v + \bar{D}_v \right) \neq 0$ , and  $\Omega^i = \mathbb{R}^{n_v}$  otherwise. In (25),  $\Sigma_y^{\infty}$  denotes the steady-state covariance of y, computed from

$$\Sigma_y^{\infty} = \bar{C} \Sigma_x^{\infty} \bar{C}^{\top} + \bar{D}_w W \bar{D}_w^{\top}, \qquad (26)$$

where  $\Sigma_x^{\infty}$  denotes the steady-state covariance of  $\bar{x}$ , i.e.,  $\Sigma_x^{\infty} = \lim_{t \to \infty} \Sigma_x(t)$ , and is obtained as the solution to the following Lyapunov equation,

$$\Sigma_x^{\infty} = \bar{A} \Sigma_x^{\infty} \bar{A}^{\top} + \bar{B}_w W \bar{B}_w^{\top}.$$
 (27)

Note that  $\lim_{t\to\infty} \Sigma_x(t)$  exists and is equal to the solution of (27), which is guaranteed by  $\bar{A}$  being Schur (Assumption 1). For the latter case with  $G_i^{\top}(\bar{C}(I-\bar{A})^{-1}\bar{B}_v+\bar{D}_v) = 0$ , we assume  $g_i - \sqrt{2G_i^{\top}\Sigma_y^{\infty}G_i} \operatorname{erf}^{-1}(2\beta_i-1) > 0$ .

Algorithmically, the inner approximation  $\tilde{\mathcal{O}}_{\infty}$  of  $\mathcal{O}_{\infty}$  is constructed through the following iterative procedure,

$$\tilde{\mathcal{O}}_{t+1} = \tilde{\mathcal{O}}_t \cap \Xi_{t+1},\tag{28}$$

where  $\tilde{\mathcal{O}}_0 = \Xi_0 \cap \left( \mathbb{R}^{n_{xp}} \times \mathbb{R}^{n_{xu}} \times \bigcap_{i=1}^{n_g} \tilde{\Omega}^i \right)$ , and

$$\Xi_{t} = \left\{ (x_{p}, x_{u}, v) : G^{\top} \bar{C} \bar{A}^{t} \begin{bmatrix} x_{p} \\ x_{u} \end{bmatrix} + G^{\top} \left( \bar{C} \sum_{k=0}^{t-1} \bar{A}^{k} \bar{B}_{v} + \bar{D}_{v} \right) \\ \bar{D}_{v} \right\} v \leq g - \left[ \begin{array}{c} \sqrt{2G_{1}^{\top} \Sigma_{y}(t)G_{1}} \operatorname{erf}^{-1}(2\beta_{1} - 1) \\ \vdots \\ \sqrt{2G_{n_{g}}^{\top} \Sigma_{y}(t)G_{n_{g}}} \operatorname{erf}^{-1}(2\beta_{n_{g}} - 1) \end{bmatrix} \right\},$$

$$(29)$$

where  $G \in \mathbb{R}^{n_y \times n_g}$  is the matrix with  $G_i$ ,  $i = 1, ..., n_g$ , as its *i*th column, and  $g \in \mathbb{R}^{n_g}$  is the vector with  $g_i$  as its *i*th entry.

Firstly, note that  $\tilde{\mathcal{O}}_t$  generated by the iterative procedure (28) form a nonincreasing sequence of sets, i.e.,  $\tilde{\mathcal{O}}_{t+1} \subset \tilde{\mathcal{O}}_t$  for all  $t \in \mathbb{Z}_{\geq 0}$ . In this case, the set-theoretic limit  $\lim_{t\to\infty} \tilde{\mathcal{O}}_t$  exists and satisfies (Folland, 1999)

$$\lim_{t \to \infty} \tilde{\mathcal{O}}_t = \bigcap_{t=0}^{\infty} \tilde{\mathcal{O}}_t$$
$$= \bigcap_{t=0}^{\infty} \left( \left( \bigcap_{k=0}^t \Xi_k \right) \cap \left( \mathbb{R}^{n_{xp}} \times \mathbb{R}^{n_{xu}} \times \bigcap_{i=1}^{n_g} \tilde{\Omega}^i \right) \right)$$
$$= \left( \bigcap_{t=0}^{\infty} \Xi_t \right) \cap \left( \mathbb{R}^{n_{xp}} \times \mathbb{R}^{n_{xu}} \times \bigcap_{i=1}^{n_g} \tilde{\Omega}^i \right), \quad (30)$$

where we have expanded  $\tilde{\mathcal{O}}_t$  according to (28) in the second line. Then, from the expressions of  $\mathcal{O}^i_{\infty}$  in (23),  $\tilde{\mathcal{O}}^i_{\infty}$  in (24a),  $\tilde{\mathcal{O}}_{\infty}$  in (24b), and  $\Xi_t$  in (29), it follows that

$$\lim_{t \to \infty} \tilde{\mathcal{O}}_t = \tilde{\mathcal{O}}_\infty,\tag{31}$$

i.e., the sets  $\tilde{\mathcal{O}}_t$  generated by the iterative procedure (28) converge to  $\tilde{\mathcal{O}}_{\infty}$ .

To construct  $\tilde{\mathcal{O}}_{\infty}$ , the iterative procedure (28) chooses to consider all the constraints for  $i = 1, ..., n_g$  at each iteration t by defining  $\Xi_t$  according to (29), instead of obtaining each  $\tilde{\mathcal{O}}^i_{\infty}$  first and constructing  $\tilde{\mathcal{O}}_{\infty}$  then as the intersection of  $\tilde{\mathcal{O}}^i_{\infty}$  according to (24b). This strategy has been chosen due to its computational advantages: It enables us to deal with the constraints for  $i = 1, ..., n_g$ through vector/matrix operations in (29), which typically leads to higher computational efficiency than using for-loops (van de Geijn and Goto, 2011).

The set  $\tilde{\mathcal{O}}_{\infty}$  is finitely determined. This is formally presented as the following proposition:

**Proposition 1:** Suppose  $(\overline{C}, \overline{A})$  is observable and the set defined by the constraints in (7),  $\mathcal{Y} = \{y \in \mathbb{R}^{n_y} : G_i^\top y \leq g_i, i = 1, ..., n_g\}$ , is bounded. Then, (i) there exists  $t^* \in \mathbb{Z}_{\geq 0}$  such that  $\tilde{\mathcal{O}}_{\infty} = \tilde{\mathcal{O}}_{t^*}$ , and (ii)  $\tilde{\mathcal{O}}_{\infty}$  is compact and convex.

**Proof:** For any  $v \in \tilde{\Omega}^i \subset \operatorname{int}(\Omega^i)$ , there exists  $\varepsilon_i(v) > 0$  such that  $\mathcal{B}_{2\varepsilon_i(v)}(v) \subset \Omega^i$ , where  $\mathcal{B}_{2\varepsilon_i(v)}(v)$  denotes the open ball in  $\mathbb{R}^{n_v}$  centered at v with radius  $2\varepsilon_i(v)$ .

Since  $\tilde{\Omega}^i$  is compact and  $\{\mathcal{B}_{\varepsilon_i(v)}(v) : v \in \tilde{\Omega}^i\}$  is an open cover of  $\tilde{\Omega}^i$ , there is a finite subcover  $\{\mathcal{B}_{\varepsilon_i(v_j)}(v_j) : j = 1, ..., J_i\} \subset \{\mathcal{B}_{\varepsilon_i(v)}(v) : v \in \tilde{\Omega}^i\}$ . This means for any  $v \in \tilde{\Omega}^i$ , we have  $v \in \mathcal{B}_{\varepsilon_i(v_j)}(v_j)$  for some  $j = 1, ..., J_i$ .

Let  $\varepsilon_i = \min \{ \varepsilon_i(v_j) : j = 1, ..., J_i \}$ . Then, for any  $v \in \tilde{\Omega}^i$ , we have  $v \oplus \mathcal{B}_{\varepsilon_i}(0) \subset \mathcal{B}_{\varepsilon_i(v_j)}(v_j) \oplus \mathcal{B}_{\varepsilon_i(v_j)}(0) = \mathcal{B}_{2\varepsilon_i(v_j)}(v_j) \subset \Omega^i$ . According to the definition of  $\Omega^i$  in (25), v satisfies

$$G_i^{\top} \left( \bar{C} (I - \bar{A})^{-1} \bar{B}_v + \bar{D}_v \right) v + \bar{\varepsilon}_i$$
  
$$\leq g_i - \sqrt{2 G_i^{\top} \Sigma_y^{\infty} G_i} \operatorname{erf}^{-1} \left( 2\beta_i - 1 \right), \qquad (32)$$

where

$$\bar{\varepsilon}_i = \sup_{v \in \mathcal{B}_{\varepsilon_i}(0)} G_i^\top \left( \bar{C} (I - \bar{A})^{-1} \bar{B}_v + \bar{D}_v \right) v > 0 \quad (33)$$

if  $G_i^{\top}(\bar{C}(I - \bar{A})^{-1}\bar{B}_v + \bar{D}_v) \neq 0$  and  $\bar{\varepsilon}_i = g_i - \sqrt{2G_i^{\top}\Sigma_y^{\infty}G_i} \operatorname{erf}^{-1}(2\beta_i - 1) > 0$  otherwise.

Because  $(\bar{C}, \bar{A})$  is observable and  $\mathcal{Y}$  and  $\bigcap_{i=1}^{n_g} \tilde{\Omega}^i$  are both bounded, there exists  $t_0 \in \mathbb{Z}_{\geq 0}$  such that  $\tilde{\mathcal{O}}_{t_0}$  constructed according to (28) is bounded.

Then, because  $\overline{A}$  is Schur, there exists  $t_1 \in \mathbb{Z}_{\geq t_0}$  such

that for any  $(x_p, x_u, v) \in \tilde{\mathcal{O}}_{t_0}$ , we have

$$G_i^{\top} \bar{C} \bar{A}^t \begin{bmatrix} x_p \\ x_u \end{bmatrix} \le \frac{\bar{\varepsilon}_i}{3}, \tag{34a}$$

$$G_{i}^{\top}\left(\bar{C}\sum_{k=0}^{t-1}\bar{A}^{k}\bar{B}_{v}+\bar{D}_{v}\right)v-G_{i}^{\top}\left(\bar{C}(I-\bar{A})^{-1}\bar{B}_{v}+\bar{D}_{v}\right)v$$

$$= -G_i^{\top} \bar{C} \bar{A}^t (I - \bar{A})^{-1} \bar{B}_v v \le \frac{\bar{\varepsilon}_i}{3},$$
(34b)

$$\left(\sqrt{2G_i^{\top}\Sigma_y(t)G_i} - \sqrt{2G_i^{\top}\Sigma_y^{\infty}G_i}\right)\operatorname{erf}^{-1}(2\beta_i - 1) \leq \frac{\bar{\varepsilon}_i}{3},$$
(34c)

for  $i = 1, ..., n_g$  and all  $t \in \mathbb{Z}_{\geq t_1}$ .

Combining (32) and (34), we obtain

$$G_{i}^{\top}\bar{C}\bar{A}^{t}\begin{bmatrix}x_{p}\\x_{u}\end{bmatrix}+G_{i}^{\top}\left(\bar{C}\sum_{k=0}^{t-1}\bar{A}^{k}\bar{B}_{v}+\bar{D}_{v}\right)v$$

$$\leq G_{i}^{\top}\left(\bar{C}(I-\bar{A})^{-1}\bar{B}_{v}+\bar{D}_{v}\right)v+\frac{2\bar{\varepsilon}_{i}}{3}$$

$$\leq g_{i}-\sqrt{2G_{i}^{\top}\Sigma_{y}^{\infty}G_{i}}\operatorname{erf}^{-1}(2\beta_{i}-1)-\frac{\bar{\varepsilon}_{i}}{3}$$

$$\leq g_{i}-\sqrt{2G_{i}^{\top}\Sigma_{y}(t)G_{i}}\operatorname{erf}^{-1}(2\beta_{i}-1), \qquad (35)$$

for  $i = 1, ..., n_g$  and all  $t \in \mathbb{Z}_{\geq t_1}$ . This means for any  $(x_p, x_u, v) \in \tilde{\mathcal{O}}_{t_0}$ , we have  $(x_p, x_u, v) \in \Xi_t$  for all  $t \in \mathbb{Z}_{\geq t_1}$ , i.e.,  $\tilde{\mathcal{O}}_{t_0} \subset \Xi_t$  for all  $t \in \mathbb{Z}_{\geq t_1}$ . Therefore, we have

$$\tilde{\mathcal{O}}_{\infty} = \tilde{\mathcal{O}}_{t_0} \cap \bigcap_{t=t_0}^{t_1-1} \Xi_t \cap \bigcap_{t=t_1}^{\infty} \Xi_t \supset \tilde{\mathcal{O}}_{t_0} \cap \bigcap_{t=t_0}^{t_1-1} \Xi_t \cap \tilde{\mathcal{O}}_{t_0} \\
= \tilde{\mathcal{O}}_{t_0} \cap \bigcap_{t=t_0}^{t_1-1} \Xi_t = \tilde{\mathcal{O}}_{t_1-1}.$$
(36)

Meanwhile, we also have  $\tilde{\mathcal{O}}_{\infty} = \tilde{\mathcal{O}}_{t_1-1} \cap \bigcap_{t=t_1}^{\infty} \Xi_t \subset \tilde{\mathcal{O}}_{t_1-1}$ , which yields  $\tilde{\mathcal{O}}_{\infty} = \tilde{\mathcal{O}}_{t^*}$  with  $t^* = t_1 - 1 \in \mathbb{Z}_{\geq 0}$ . This proves (i).

For (ii), because  $\tilde{\mathcal{O}}_{\infty} = \tilde{\mathcal{O}}_{t_0} \cap \bigcap_{t=t_0}^{\infty} \Xi_t$  and  $\tilde{\mathcal{O}}_{t_0}$ is bounded,  $\tilde{\mathcal{O}}_{\infty}$  is also bounded. Because  $\tilde{\mathcal{O}}_{\infty} = (\bigcap_{t=0}^{\infty} \Xi_t) \cap (\mathbb{R}^{n_{x_p}} \times \mathbb{R}^{n_{x_u}} \times \bigcap_{i=1}^{n_g} \tilde{\Omega}^i)$  where  $\Xi_t, t \in \mathbb{Z}_{\geq 0}$ , and  $\mathbb{R}^{n_{x_p}} \times \mathbb{R}^{n_{x_u}} \times \bigcap_{i=1}^{n_g} \tilde{\Omega}^i$  are closed and convex,  $\tilde{\mathcal{O}}_{\infty}$ is also closed and convex. This proves the compactness and convexity of  $\tilde{\mathcal{O}}_{\infty}$ .

# 3.2 CSRG algorithms

In this section, we present two CSRG algorithms. The algorithms are based on the constrained optimization problem (11) and augmented with additional features to achieve improved performance.

Algorithm 1: At each discrete-time instant  $t \in \mathbb{Z}_{\geq 0}$ ,

$$(x_u(t), v(t)) =$$

$$\begin{cases}
(\hat{x}_u(t), \hat{v}(t)), & \text{if } (x_p(t), \bar{x}_u(t), v(t-1)) \in \tilde{\mathcal{O}}_{\infty} \\
& \text{and } (38) \text{ is feasible,} \\
(\bar{x}_u(t), v(t-1)), & \text{otherwise,} 
\end{cases}$$
(37)

where  $\bar{x}_u(t) = A_p x_p(t-1) + A_u x_u(t-1) + D_v v(t-1)$ , and the pair  $(\hat{x}_u(t), \hat{v}(t))$  is determined as

$$(\hat{x}_u(t), \hat{v}(t)) = \underset{x_u, v}{\operatorname{arg\,min}} \quad J(x_u, v, x_p(t), r(t)), \qquad (38a)$$

ubject to 
$$(x_p(t), x_u, v) \in \tilde{\mathcal{O}}_{\infty},$$
 (38b)

$$\|v - r(t)\|_{R}^{2} \le (\max\{\|v(t-1) - r(t)\|_{R} - \delta, 0\})^{2},$$
(38c)

with  $\delta > 0$  being a sufficiently small constant.

 $\mathbf{S}$ 

We remark that unlike in the deterministic case (Mc-Donough and Kolmanovsky, 2015a,b), recursive feasibility of the constrained optimization problem (38)cannot be guaranteed in our considered stochastic setting. Specifically, because the Gaussian disturbance variables  $\{w(t)\}_{t\in\mathbb{Z}_{\geq 0}} \sim \mathcal{N}(0, W)$  are not compactly supported, there is always a non-zero probability for the plant state  $x_p(t)$  to get outside of  $\operatorname{proj}_{x_n}(\mathcal{O}_{\infty})$ , which denotes the projection of the compact set  $\tilde{\mathcal{O}}_{\infty} \in \mathbb{R}^{n_{xp}} \times \mathbb{R}^{n_{xu}} \times \mathbb{R}^{n_v}$  onto the  $x_p$ -space. Therefore, we introduce an infeasibility-handling mechanism in (37). In particular, when  $(x_p(t), \bar{x}_u(t), v(t-1)) \notin \mathcal{O}_{\infty}$ or (38) is infeasible, the controller state and reference pair  $(x_u(t), v(t))$  is set to  $(\bar{x}_u(t), v(t-1))$ , which was previously determined to be chance-constraint admissible. Moreover, it has been observed in Kalabić et al. (2019) that if the direction of reference modification is not restricted, a chance-constrained RG may move v(t)away from r(t), even cause sudden large changes in v(t), to enforce constraints. This can impede the convergence of v(t) to r(t) and degrade system performance. Therefore,  $\|v - r(t)\|_R^2 \le (\max \{\|v(t-1) - r(t)\|_R - \delta, 0\})^2$  is added to the optimization problem (38) as an extra constraint, (38c), to enforce  $\hat{v}(t)$  to be closer to r(t) than the previous reference value v(t-1). In particular, (38c) is a convex quadratic constraint on the decision variable v.

In some circumstances, the convergence of the modified reference v(t) to the commanded value r(t) is prioritized so that the system can potentially have faster response to human operator intention or planning algorithm schedule. For this, the following Algorithm 2 can be used.

Algorithm 2: At each discrete-time instant  $t \in \mathbb{Z}_{\geq 0}$ ,

where  $\hat{x}'_u(t)$  is determined as

$$\hat{x}'_{u}(t) = \operatorname*{arg\,min}_{x_{u}} J(x_{u}, r(t), x_{p}(t), r(t)),$$
 (40a)

subject to 
$$(x_p(t), x_u, r(t)) \in \mathcal{O}_{\infty}.$$
 (40b)

In what follows, we characterize theoretical properties of our CSRG algorithms, and also extend the CSRG scheme to treat joint chance constraints.

# 4 Theoretical Properties

In this section, we analyze theoretical properties of our CSRG algorithms. Three important properties of the CSRG scheme are: 1) constraint enforcement, 2) convergence of the modified reference v(t) to constant, steadystate constraint-admissible commanded value r, and 3) stability of the commanded set-point  $\bar{x}^*(r)$ . The first two are also important properties of conventional RGs (Garone et al., 2017; Kalabić et al., 2019). Unlike the conventional RG scheme where stability of  $\bar{x}^*(r)$  is inherited from stability of the nominal closed-loop system, for the CSRG scheme stability needs to be separately verified, because the CSRG scheme also modifies the control input signal u(t) through modifying the controller state  $x_u(t)$ . Due to the presence of stochastic disturbances, the techniques for establishing the above three properties of the chance-constrained CSRG scheme are significantly different from the techniques used in McDonough and Kolmanovsky (2015a) for the deterministic case. For instance, in the deterministic case these properties are established based on the positive invariance of the maximal output admissible set  $\mathcal{O}_{\infty}$ . In contrast, in our considered stochastic setting the set  $\tilde{\mathcal{O}}_{\infty}$  is not positively invariant, as has been discussed above, and consequently, new techniques for establishing these properties need to be developed.

Firstly, the following proposition establishes the chanceconstraint enforcement property of our CSRG algorithms. The significance is that with the infeasibilityhandling mechanism that we have introduced, the desired probabilistic constraint enforcement guarantee is maintained in *closed-loop operation* of the system. Note that while chance constraints are incorporated in the definition of the maximal output admissible set  $\tilde{\mathcal{O}}_{\infty}$ , during the closed-loop operation, the state may exit this set due to a disturbance realization, in which case our infeasibility-handling mechanism will be applied. Therefore, it is not a priori clear if chance constraints will be satisfied during closed-loop operation. We answer this conundrum affirmatively.

**Proposition 2:** Suppose  $(x_p(0), x_u(0), v(0)) \in \mathcal{O}_{\infty}$ . Then, the closed-loop response of the overall system (consisting of the plant (1), the nominal controller (2), and the CSRG algorithm 1 or 2) satisfies the chance constraints (8) for all  $t \in \mathbb{Z}_{\geq 0}$ .

**Proof:** Let  $t \in \mathbb{Z}_{\geq 0}$  be arbitrary and define  $\tau = \max \{t' \in \mathbb{Z}_{[0,t]} : (x_p(t'), x_u(t'), v(t')) \in \tilde{\mathcal{O}}_{\infty}\}$ . Since

it is assumed that  $(x_p(0), x_u(0), v(0)) \in \tilde{\mathcal{O}}_{\infty}$ , the set  $\{t' \in \mathbb{Z}_{[0,t]} : (x_p(t'), x_u(t'), v(t')) \in \tilde{\mathcal{O}}_{\infty}\}$  is necessarily non-empty and the variable  $\tau$  is therefore well-defined. Note that  $\tau$  is a random variable with the finite support  $\mathbb{Z}_{[0,t]}$ . In particular, we have

$$\sum_{k=0}^{t} \mathbb{P}\{\tau = k\} = \mathbb{P}\{\tau \in \mathbb{Z}_{[0,t]}\} = 1.$$
(41)

If  $\tau = k$ , then according to our CSRG algorithms, the trajectory of controller state and reference pair must satisfy  $(x_u(t'), v(t')) = (\bar{x}_u(t'), v(k))$  for all  $t' \in \mathbb{Z}_{[k+1,t]}$ . In this case, the plant and controller states  $\bar{x}(t') = [x_p^{\top}(t'), x_u^{\top}(t')]^{\top}$  evolve according to (3a) with  $v(t') \equiv v(k)$  over  $t' \in \mathbb{Z}_{[k,t]}$ . Since  $(x_p(k), x_u(k), v(k)) \in \tilde{\mathcal{O}}_{\infty} \subset \mathcal{O}_{\infty}^i$  and the dynamics of  $\bar{x}(t') = [x_p^{\top}(t'), x_u^{\top}(t')]^{\top}$  follow (3a) with  $v(t') \equiv v(k)$  for  $t' \in \mathbb{Z}_{[k,t]}$ , using the definition of  $\mathcal{O}_{\infty}^i$  in (10), we have

$$\mathbb{P}\left\{G_i^\top y(t) \le g_i \middle| \tau = k\right\} \ge \beta_i.$$
(42)

Note that this holds for all k = 0, ..., t and all  $i = 1, ..., n_g$ .

Combining (41) and (42), we obtain

$$\mathbb{P}\left\{G_{i}^{\top}y(t) \leq g_{i}\right\} = \sum_{k=0}^{t} \mathbb{P}\left\{G_{i}^{\top}y(t) \leq g_{i} \middle| \tau = k\right\} \mathbb{P}\left\{\tau = k\right\}$$
$$\geq \beta_{i} \sum_{k=0}^{t} \mathbb{P}\left\{\tau = k\right\} = \beta_{i}, \tag{43}$$

for  $i = 1, ..., n_g$ . As  $t \in \mathbb{Z}_{\geq 0}$  is arbitrary, the result follows.

We next discuss the convergence property of the modified reference v(t) to commanded value r(t). To begin with, we introduce the following lemma, which will be used to prove the main convergence result Proposition 3.

**Lemma 1:** Given  $\tilde{\mathcal{O}}_{\infty}$ , there exists  $\varepsilon > 0$  such that  $\mathcal{B}_{\varepsilon}(\bar{x}^*(v)) \times \{v\} \subset \tilde{\mathcal{O}}_{\infty}$  for any  $v \in \bigcap_{i=1}^{n_g} \tilde{\Omega}^i$ , where  $\mathcal{B}_{\varepsilon}(\bar{x}^*(v))$  denotes the open ball in  $\mathbb{R}^{n_{xp}+n_{xu}}$  centered at  $\bar{x}^*(v)$  with radius  $\varepsilon$ .

**Proof:** Firstly, it is easily seen from (17) that for any  $t \in \mathbb{Z}_{\geq 0}$ ,  $\Sigma_y(t+1) - \Sigma_y(t) = (\bar{C}\bar{A}^t\bar{B}_w)W(\bar{C}\bar{A}^t\bar{B}_w)^\top$  is positive semi-definite, denoted as  $\Sigma_y(t+1) \succeq \Sigma_y(t)$ . As a result, it holds that  $\Sigma_y^{\infty} \succeq \Sigma_y(t)$  for all  $t \in \mathbb{Z}_{\geq 0}$ , where  $\Sigma_y^{\infty}$  denotes the steady-state covariance of y, computed from (26). In turn,  $\sqrt{2G_i^\top \Sigma_y^{\infty} G_i} \ge \sqrt{2G_i^\top \Sigma_y(t)G_i}$  for all  $t \in \mathbb{Z}_{\geq 0}$  and  $i = 1, ..., n_g$ .

Then, referring to (32) in the proof of Proposition 1, for each  $i = 1, ..., n_q$ , there exists  $\bar{\varepsilon}_i > 0$  such that for any  $v \in \tilde{\Omega}^i$ , we have

$$G_{i}^{\top} \left( \bar{C} (I - \bar{A})^{-1} \bar{B}_{v} + \bar{D}_{v} \right) v + \bar{\varepsilon}_{i}$$

$$\leq g_{i} - \sqrt{2G_{i}^{\top} \Sigma_{y}^{\infty} G_{i}} \operatorname{erf}^{-1} \left( 2\beta_{i} - 1 \right)$$

$$\leq g_{i} - \sqrt{2G_{i}^{\top} \Sigma_{y} (t) G_{i}} \operatorname{erf}^{-1} \left( 2\beta_{i} - 1 \right), \qquad (44)$$

for all  $t \in \mathbb{Z}_{\geq 0}$ .

Now let

$$\varepsilon = \min\left\{\frac{\bar{\varepsilon}_i}{\sup_{t\geq 0} \|G_i^\top \bar{C}\bar{A}^t\|} : i = 1, ..., n_g\right\}.$$
 (45)

Because  $\bar{A}$  is Schur (Assumption 1),  $\sup_{t\geq 0} \|G_i^{\top} \bar{C} \bar{A}^t\| > 0$  is finite, and in turn,  $\varepsilon$  defined above satisfies  $\varepsilon > 0$ .

Combining (44) and (45), we obtain that for any  $v \in \bigcap_{i=1}^{n_g} \tilde{\Omega}^i$  and  $\bar{x} \in \mathcal{B}_{\varepsilon}(\bar{x}^*(v))$ ,

$$G_i^{\top} \bar{C} \bar{A}^t \bar{x} + G_i^{\top} \left( \bar{C} \sum_{k=0}^{t-1} \bar{A}^k \bar{B}_v + \bar{D}_v \right) v$$
  
$$= G_i^{\top} \bar{C} \bar{A}^t \bar{x}^* (v) + G_i^{\top} \left( \bar{C} \sum_{k=0}^{t-1} \bar{A}^k \bar{B}_v + \bar{D}_v \right) v$$
  
$$+ G_i^{\top} \bar{C} \bar{A}^t \left( \bar{x} - \bar{x}^* (v) \right)$$
  
$$\leq C_i^{\top} \left( \bar{C} \left( I - \bar{A} \right)^{-1} \bar{D} + \bar{D} \right) v + \| C_i^{\top} \bar{C} \bar{A}^t \| \| \bar{u} = \bar{u}^*$$

$$\leq G_{i}^{\top} \left( \bar{C} (I - \bar{A})^{-1} \bar{B}_{v} + \bar{D}_{v} \right) v + \|G_{i}^{\top} \bar{C} \bar{A}^{t}\| \|\bar{x} - \bar{x}^{*}(v)\| \\
\leq G_{i}^{\top} \left( \bar{C} (I - \bar{A})^{-1} \bar{B}_{v} + \bar{D}_{v} \right) v + \bar{\varepsilon}_{i} \\
\leq g_{i} - \sqrt{2G_{i}^{\top} \Sigma_{y}(t) G_{i}} \operatorname{erf}^{-1} (2\beta_{i} - 1),$$
(46)

holds for all  $t \in \mathbb{Z}_{\geq 0}$  and  $i = 1, ..., n_g$ . According to the definition of  $\tilde{\mathcal{O}}_{\infty}$  in (23) and (24), the above (46) implies  $\mathcal{B}_{\varepsilon}(\bar{x}^*(v)) \times \{v\} \subset \tilde{\mathcal{O}}_{\infty}$  for any  $v \in \bigcap_{i=1}^{n_g} \tilde{\Omega}^i$ . This completes the proof.

We now show the almost-sure finite-time convergence property of the modified reference v(t) to constant, steady-state constraint-admissible commands in the following proposition. We remark that this almost-sure finite-time convergence result is a stronger convergence result than the convergence in probability result established in Theorem 7 of Kalabić et al. (2019) for the stochastic RG. The reason our result here is stronger is because almost-sure convergence implies convergence in probability, but not vice versa (Folland, 1999).

**Proposition 3:** Suppose (i)  $(x_p(0), x_u(0), v(0)) \in \tilde{\mathcal{O}}_{\infty}$ , (ii)  $\Sigma_x^{\infty}$  is nonsingular, and (iii) there exists  $t_s \in \mathbb{Z}_{\geq 0}$  such that  $r(t) = r_s \in \bigcap_{i=1}^{n_g} \tilde{\Omega}^i$  for all  $t \in \mathbb{Z}_{\geq t_s}$ . Then, the modified reference v(t) almost surely (a.s.) converges to  $r_s$  in finite time, i.e.,

$$\mathbb{P}\Big\{\exists t_f \in \mathbb{Z}_{\geq t_s} \text{ such that } v(t) = r_s, \forall t \in \mathbb{Z}_{\geq t_f}\Big\} = 1.$$
(47)

**Proof:** Firstly, the constraint (38c) ensures that any realization of the sequence  $\{\|v(t) - r_s\|_R\}_{t=t_s}^{\infty}$  generated by the CSRG must be nonincreasing. Since  $\|v(t) - r_s\|_R$  is also bounded from below by 0, any realization of  $\{\|v(t) - r_s\|_R\}_{t=t_s}^{\infty}$  must converge to some  $\eta^* \in \mathbb{R}_{\geq 0}$ . More specifically, with (38c), whenever v(t) differs from its previous value v(t-1), it must hold that either  $\|v(t) - r_s\|_R \leq \|v(t-1) - r_s\|_R - \delta$ , with  $\delta$  being a positive constant, or  $\|v(t) - r_s\|_R = 0$ . This ensures that any realization of  $\{\|v(t) - r_s\|_R = 0$ . This ensures that any realization of  $\{\|v(t) - r_s\|_R = 0, \text{ with } \delta \text{ being a positive constant, or } \|v(t) - r_s\|_R + \delta, \text{ with } \delta \text{ being a positive constant, or } \|v(t) - r_s\|_R = 0$ . This ensures that any realization of  $\{\|v(t) - r_s\|_R\}_{t=t_s}^{\infty}$  must converge to its corresponding  $\eta^*$  through at most a finite/bounded number of jumps and the sequence  $\{v(t)\}_{t=t_s}^{\infty}$  converges to some  $v^* \in \mathbb{R}^{n_v}$  after these jumps. Note that due to the stochastic nature of the system (3), the  $\eta^*$  and  $v^*$  are random variables. In what follows we show that with probability 1,  $\eta^* = 0$  and  $v^* = r_s$ .

Assume the opposite, i.e.,  $\{v(t)\}_{t=t_s}^{\infty}$  converges to some  $v^* \neq r_s$ . In the above we have shown that  $\{v(t)\}_{t=t_s}^{\infty}$  must reach  $v^*$  after a finite number of jumps, which also implies that  $\{v(t)\}_{t=t_s}^{\infty}$  reaches  $v^*$  in finite time. Denote the time instant when  $\{v(t)\}_{t=t_s}^{\infty}$  reaches  $v^*$  as  $t^* \in \mathbb{Z}_{\geq t_s}$ . In particular,  $v(t) = v^* \neq r_s$  for all  $t \in \mathbb{Z}_{\geq t^*}$ .

In this case, the constraint (38c) would never be satisfied over  $t \in \mathbb{Z}_{\geq t^*}$ , and according to the CSRG algorithm (37),  $x_u(\bar{t}) = \bar{x}_u(t) = A_p x_p(t-1) + A_u x_u(t-1) + D_v v(t-1)$  for all  $t \in \mathbb{Z}_{\geq t^*}$ . This implies that the sequence  $\{\bar{x}(t)\}_{t=t^*}^{\infty} = \{[x_p^\top(t), x_u^\top(t)]^\top\}_{t=t^*}^{\infty}$  would be a Gaussian Markov process generated by the recursion (3a) with  $v(t) \equiv v^*$ . Then, because  $\Sigma_x^{\infty}$  is assumed to be nonsingular, the Strong Law of Large Numbers for Markov chains (Meyn and Caines, 1991) says that the following,

$$\lim_{N \to \infty} \frac{1}{N} \sum_{t=t^*}^{t^*+N-1} f(\bar{x}(t)) \stackrel{\text{a.s.}}{=} \int_{\mathbb{R}^{n_{xp}+n_{xu}}} f \,\mathrm{d}\mu^*, \quad (48)$$

would hold for any positive Borel function f on  $\mathbb{R}^{n_{xp}+n_{xu}}$ and almost every initial condition  $\bar{x}(t^*) \in \mathbb{R}^{n_{xp}+n_{xu}}$ , where  $\mu^*$  is the Gaussian measure with mean  $\bar{x}^*(v^*)$  and covariance  $\Sigma_x^{\infty}$  (Bogachev, 1998).

Because  $v^*$  is generated by the CSRG, it must hold that  $v^* \in \operatorname{proj}_v(\tilde{\mathcal{O}}_\infty) \subset \bigcap_{i=1}^{n_g} \tilde{\Omega}^i$ . Now consider  $f = \mathbb{I}_{\mathcal{B}_{\varepsilon/2}(\bar{x}^*(v^*))}$ , i.e., the indicator function of the open ball  $\mathcal{B}_{\varepsilon/2}(\bar{x}^*(v^*)) \subset \mathbb{R}^{n_{xp}+n_{xu}}$ , where  $\varepsilon > 0$  is defined according to (45). In this case, (48) yields

$$\lim_{N \to \infty} \frac{1}{N} \sum_{t=t^*}^{t^*+N-1} \mathbb{I}_{\mathcal{B}_{\varepsilon/2}(\bar{x}^*(v^*))}(\bar{x}(t))$$
(49)  
$$\stackrel{\text{a.s.}}{=} \int_{\mathbb{R}^{n_{xp}+n_{xu}}} \mathbb{I}_{\mathcal{B}_{\varepsilon/2}(\bar{x}^*(v^*))} \, \mathrm{d}\mu^* = \mu^* \big( \mathcal{B}_{\varepsilon/2}(\bar{x}^*(v^*)) \big) > 0,$$

which implies the existence of  $N' \in \mathbb{Z}_{\geq 0}$  such that  $\sum_{t=t^*}^{t^*+N'-1} \mathbb{I}_{\mathcal{B}_{\varepsilon/2}(\bar{x}^*(v^*))}(\bar{x}(t)) > 0$ . And this in turn im-

plies the existence of  $t' \in \mathbb{Z}_{[t^*,t^*+N'-1]} \subset \mathbb{Z}_{\geq t^*}$  such that  $\bar{x}(t') = [x_p^\top(t'), \bar{x}_u^\top(t')]^\top \in \mathcal{B}_{\varepsilon/2}(\bar{x}^*(v^*))$ . Then, according to Lemma 1, we have  $(x_p(t'), \bar{x}_u(t'), v^*) \in \mathcal{B}_{\varepsilon/2}(\bar{x}^*(v^*)) \times \{v^*\} \subset \tilde{\mathcal{O}}_{\infty}$ .

Now let  $\xi_i = \sup_{t\geq 0} \|G_i^{\top}(\bar{C}\sum_{k=0}^{t-1}\bar{A}^k\bar{B}_v + \bar{D}_v)\|$ , which is finite because  $\bar{A}$  is Schur, and consider  $\Delta v$  satisfying  $\|\Delta v\| \leq \min\{\bar{\varepsilon}_i/(2\xi_i) : i = 1, ..., n_g\}$ , where  $\bar{\varepsilon}_i > 0$ is defined as in (33). Referring to (46) in the proof of Lemma 1, we obtain that

$$\begin{aligned}
G_{i}^{\top}\bar{C}\bar{A}^{t}\bar{x}(t') + G_{i}^{\top}\left(\bar{C}\sum_{k=0}^{t-1}\bar{A}^{k}\bar{B}_{v} + \bar{D}_{v}\right)(v^{*} + \Delta v) \\
&= G_{i}^{\top}\bar{C}\bar{A}^{t}\bar{x}^{*}(v^{*}) + G_{i}^{\top}\left(\bar{C}\sum_{k=0}^{t-1}\bar{A}^{k}\bar{B}_{v} + \bar{D}_{v}\right)v^{*} \\
&+ G_{i}^{\top}\bar{C}\bar{A}^{t}\left(\bar{x}(t') - \bar{x}^{*}(v^{*})\right) + G_{i}^{\top}\left(\bar{C}\sum_{k=0}^{t-1}\bar{A}^{k}\bar{B}_{v} + \bar{D}_{v}\right)\Delta v \\
&\leq G_{i}^{\top}\left(\bar{C}(I - \bar{A})^{-1}\bar{B}_{v} + \bar{D}_{v}\right)v^{*} \\
&+ \|G_{i}^{\top}\bar{C}\bar{A}^{t}\|\|\bar{x}(t') - \bar{x}^{*}(v)\| + \xi_{i}\|\Delta v\|, \\
&\leq G_{i}^{\top}\left(\bar{C}(I - \bar{A})^{-1}\bar{B}_{v} + \bar{D}_{v}\right)v^{*} + \bar{\varepsilon}_{i} \\
&\leq g_{i} - \sqrt{2G_{i}^{\top}\Sigma_{y}(t)G_{i}}\operatorname{erf}^{-1}(2\beta_{i} - 1),
\end{aligned}$$
(50)

for all  $t \in \mathbb{Z}_{>0}$  and  $i = 1, ..., n_q$ .

Note that since  $v^*$  and  $r_s$  both belong to the convex set  $\bigcap_{i=1}^{n_g} \tilde{\Omega}^i$ , any  $v^* + \Delta v$  that lies on the line segment connecting  $v^*$  and  $r_s$  also belongs to  $\bigcap_{i=1}^{n_g} \tilde{\Omega}^i$ . This can be expressed as  $v^* + \Delta v \in \bigcap_{i=1}^{n_g} \tilde{\Omega}^i$  for any  $\Delta v$  that can be written as  $\Delta v = \lambda (r_s - v^*)$  for some  $\lambda \in [0, 1]$ . Then, this, together with (50) and according to the definition of  $\tilde{\mathcal{O}}_{\infty}$  in (23) and (24), leads to the following result: For any  $\Delta v = \lambda (r_s - v^*)$  with  $\lambda$  satisfying  $0 \leq \lambda \leq \bar{\lambda} =$ min  $\{\min \{\bar{\varepsilon}_i/(2\xi_i || r_s - v^*||) : i = 1, ..., n_g\}, 1\}$ , it holds that  $(x_p(t'), \bar{x}_u(t'), v^* + \Delta v) \in \tilde{\mathcal{O}}_{\infty}$ .

Recall that the  $\delta > 0$  in (38c) is a sufficiently small constant. Now consider  $\delta \leq \min \{\bar{\varepsilon}_i/(2\xi_i c) : i = 1, ..., n_g\}$ , where c > 0 is a constant such that  $\|\cdot\| \leq c \|\cdot\|_R$  (according to the equivalence of norms on  $\mathbb{R}^{n_v}$ ). Then, for  $\Delta v = \bar{\lambda}(r_s - v^*)$ , we have

$$\begin{aligned} \|v^{*} - r_{s}\|_{R} &- \|v^{*} + \Delta v - r_{s}\|_{R} \\ &= \|v^{*} - r_{s}\|_{R} - \|v^{*} + \bar{\lambda}(r_{s} - v^{*}) - r_{s}\|_{R} \\ &= \|v^{*} - r_{s}\|_{R} - (1 - \bar{\lambda})\|v^{*} - r_{s}\|_{R} = \bar{\lambda}\|v^{*} - r_{s}\|_{R} \\ &= \min\left\{\min\left\{\frac{\bar{\varepsilon}_{i}\|v^{*} - r_{s}\|_{R}}{2\xi_{i}\|v^{*} - r_{s}\|_{R}} : i = 1, ..., n_{g}\right\}, \|v^{*} - r_{s}\|_{R}\right\} \\ &\geq \min\left\{\min\left\{\frac{\bar{\varepsilon}_{i}}{2\xi_{i}c} : i = 1, ..., n_{g}\right\}, \|v^{*} - r_{s}\|_{R}\right\} \\ &\geq \min\left\{\delta, \|v^{*} - r_{s}\|_{R}\right\}, \end{aligned}$$
(51)

which can be equivalently written as  $||v^* + \Delta v - r_s||_R^2 \le (\max\{||v^* - r_s||_R - \delta, 0\})^2$ .

Therefore, we have shown that the pair  $(\bar{x}_u(t'), v^* + \Delta v) = (\bar{x}_u(t'), v^* + \bar{\lambda}(r_s - v^*))$  is a feasible solution to the optimization problem (38). Recall we have also shown above that  $(x_p(t'), \bar{x}_u(t'), v^*) \in \tilde{\mathcal{O}}_{\infty}$ . In this case, according to the CSRG algorithm (37), at  $t' \in \mathbb{Z}_{\geq t^*}$  we should have  $(x_u(t'), v(t')) = (\hat{x}_u(t'), \hat{v}(t'))$ , with  $(\hat{x}_u(t'), \hat{v}(t'))$  being the optimal solution to (38). In particular, the constraint (38c) ensures  $\hat{v}(t') \neq v^*$  (note that we have assumed  $v^* \neq r_s$ ).

This contradicts our assumption that  $\{v(t)\}_{t=t_s}^{\infty}$  converges to some  $v^* \neq r_s$ . Since at the beginning of the proof we have shown that any realization of the sequence  $\{v(t)\}_{t=t_s}^{\infty}$  must converge to some point, such a contradiction says that the converged point must be  $v^* = r_s$ .

To sum up, we have shown that the sequence  $\{v(t)\}_{t=t_s}^{\infty}$  generated by the CSRG almost surely converges to  $r_s$  after a finite/bounded number of jumps, which also implies the convergence occurs (i.e., the limit point  $r_s$  is reached) within a finite amount of time. Note that the "almost surely" comes from the almost sure equality in (48) and (49). This result can also be explicitly expressed as (47).

On the basis of the convergence result of the modified reference v(t) to constant, steady-state constraintadmissible commanded reference  $r_s$  in Proposition 3, we now discuss the stability property of the commanded set-point  $\bar{x}^*(r_s)$ . In our considered stochastic setting, the stability of  $\bar{x}^*(r_s)$  is characterized by the following Proposition 4 and Remark 1.

**Proposition 4:** Let  $t_f \in \mathbb{Z}_{\geq t_s}$  denote the time instant such that  $v(t) = r_s$  for all  $t \in \mathbb{Z}_{\geq t_f}$ . Then, for  $t \in \mathbb{Z}_{\geq t_f}$ , the difference between  $\bar{x}(t)$  and  $\bar{x}^*(r_s)$  is exponentially bounded in mean square (Tarn and Rasis, 1976). In particular, we have

$$\mathbb{E}\left\{ \|\bar{x}(t) - \bar{x}^{*}(r_{s})\|^{2} \left| \bar{x}(t_{f}) \right\} \leq \frac{\mu}{\alpha} + (1 - \alpha)^{t - t_{f}} \|\bar{x}(t_{f}) - \bar{x}^{*}(r_{s})\|^{2}, \quad (52)$$

for some constants  $\mu > 0$  and  $\alpha \in (0, 1]$ .

**Proof:** Let  $t \in \mathbb{Z}_{\geq t_f}$  be arbitrary. Define  $\zeta(t) = \bar{x}(t) - \bar{x}^*(r_s)$  and consider the function  $V(\zeta(t)) = \|\zeta(t)\|_P^2 = J(x_u(t), r_s, x_p(t), r_s)$ . If  $(x_p(t+1), \bar{x}_u(t+1), v(t) = r_s) \in \tilde{\mathcal{O}}_{\infty}$ , then (37) yields that  $(x_u(t+1), v(t+1)) = (\hat{x}_u(t+1), \hat{v}(t+1))$  with  $(\hat{x}_u(t+1), \hat{v}(t+1))$  determined by (38). In this case, both  $(\bar{x}_u(t+1), r_s)$  and  $(\hat{x}_u(t+1), \hat{v}(t+1))$  are feasible solutions to (38), with  $(\hat{x}_u(t+1), \hat{v}(t+1))$  being the optimal one. Indeed, the constraint (38c) also ensures  $\hat{v}(t+1) = r_s$ . As a result, we must have  $V(\zeta(t+1)) = J(\hat{x}_u(t+1), r_s, x_p(t+1), r_s) \leq J(\bar{x}_u(t+1), r_s, x_p(t+1), r_s)$ . If  $(x_p(t+1), \bar{x}_u(t+1), v(t) = r_s) \notin \tilde{\mathcal{O}}_{\infty}$ , then

(37) yields that  $(x_u(t+1), v(t+1)) = (\bar{x}_u(t+1), v(t) = r_s)$ , and the commanded set-point  $\bar{x}^*(r_s)$  being exponentially bounded in mean square as in (52) also yields that  $J(\bar{x}_u(t+1), r_s, x_p(t+1), r_s)$ .

For given  $\bar{x}(t) = [x_p^{\top}(t), x_u^{\top}(t)]^{\top}$ , we have

$$\mathbb{E}\left\{J\left(\bar{x}_{u}(t+1), r_{s}, x_{p}(t+1), r_{s}\right) \left|\bar{x}(t)\right\}\right\}$$

$$= \mathbb{E}\left\{\left\|\bar{A}\bar{x}(t) + \bar{B}_{v}r_{s} + \bar{B}_{w}w(t) - (I - \bar{A})^{-1}\bar{B}_{v}r_{s}\right\|_{P}^{2} \left|\bar{x}(t)\right\}\right\}$$

$$= \mathbb{E}\left\{\left\|\bar{A}\zeta(t) + \bar{B}_{w}w(t)\right\|_{P}^{2} \left|\zeta(t)\right\}\right\}$$

$$= \mathbb{E}\left\{\zeta(t)^{\top} \left(\bar{A}^{\top}P\bar{A}\right)\zeta(t) + 2w(t)^{\top} \left(\bar{B}_{w}^{\top}P\bar{A}\right)\zeta(t) + w(t)^{\top} \left(\bar{B}_{w}^{\top}P\bar{B}_{w}\right)w(t)\right|\zeta(t)\right\}$$

$$= \zeta(t)^{\top} \left(P - Q\right)\zeta(t) + \mathbb{E}\left\{w(t)^{\top} \left(\bar{B}_{w}^{\top}P\bar{B}_{w}\right)w(t)\right\}$$

$$= V\left(\zeta(t)\right) - \left\|\zeta(t)\right\|_{Q}^{2} + \operatorname{trace}\left(W\left(\bar{B}_{w}^{\top}P\bar{B}_{w}\right)\right). \quad (53)$$

Then, using the pointwise inequality  $V(\zeta(t+1)) \leq$  $J(\bar{x}_u(t+1), r_s, x_p(t+1), r_s)$  shown above and the equivalence of norms on  $\mathbb{R}^{n_{xp}+n_{xu}}$ , we obtain

$$\mathbb{E}\left\{V\left(\zeta(t+1)\right)\left|\zeta(t)\right\}\right. \leq \mathbb{E}\left\{J\left(\bar{x}_{u}(t+1), r_{s}, x_{p}(t+1), r_{s}\right)\left|\bar{x}(t)\right.\right\} \\ \leq \mu + (1-\alpha)V\left(\zeta(t)\right), \tag{54}$$

where  $\mu = \text{trace}\left(W\left(\bar{B}_w^\top P \bar{B}_w\right)\right)$  and  $\alpha \in (0, 1]$  is such that  $\sqrt{\alpha} \| \cdot \|_P \leq \| \cdot \|_Q$ .

Since the  $t \in \mathbb{Z}_{>t_f}$  is arbitrary, (54) also yields

$$\mathbb{E}\left\{V\left(\zeta(t+2)\right)\left|\zeta(t)\right\}\right\}$$

$$= \mathbb{E}\left\{\mathbb{E}\left\{V\left(\zeta(t+2)\right)\left|\zeta(t+1)\right\}\left|\zeta(t)\right\}\right\}$$

$$\leq \mathbb{E}\left\{\mu + (1-\alpha)V\left(\zeta(t+1)\right)\left|\zeta(t)\right\}\right\}$$

$$= \mu + (1-\alpha)\mathbb{E}\left\{V\left(\zeta(t+1)\right)\left|\zeta(t)\right\}$$

$$\leq \mu + (1-\alpha)\left(\mu + (1-\alpha)V(\zeta(t))\right)$$

$$= \left(\sum_{i=0}^{1}(1-\alpha)^{i}\right)\mu + (1-\alpha)^{2}V\left(\zeta(t)\right). \quad (55)$$

Continuing this way, we obtain

$$\mathbb{E}\left\{V\left(\zeta(t_f+n)\right)\left|\zeta(t_f)\right\}\right\}$$

$$=\left(\sum_{i=0}^{n-1}(1-\alpha)^i\right)\mu+(1-\alpha)^n V\left(\zeta(t_f)\right)$$

$$\leq \frac{\mu}{\alpha}+(1-\alpha)^n V\left(\zeta(t_f)\right).$$
(56)

Then, (52) follows from (56) and the equivalence of norms on  $\mathbb{R}^{n_{xp}+n_{xu}}$ .

Remark 1: Note first that the existence of the finite time  $t_f \in \mathbb{Z}_{\geq t_s}$  in Proposition 4 is almost surely guaranteed (see Proposition 3). The difference between  $\bar{x}(t)$  large (Tarn and Rasis, 1976), since as  $t \to \infty$ ,

$$\mathbb{E}\left\{\lim_{t\to\infty}\left\|\bar{x}(t)-\bar{x}^*(r_s)\right\|^2\right\} \le \frac{\mu}{\alpha}.$$
(57)

Note that we have dropped the condition on  $\bar{x}(t_f)$  from the expectation since the right-hand side does not depend on  $\bar{x}(t_f)$  (Tarn and Rasis, 1976).

#### 5 **Extension to Joint Chance Constraints**

The CSRG formulation introduced in Section 3 uses the maximal output admissible set  $\mathcal{O}_{\infty}$  to treat the set of individual chance constraints in (8). However, one may sometimes be interested in treating chance constraints in the following form,

$$\mathbb{P}\left\{G_i^{\top} y(t) \le g_i, \, i = 1, ..., n_g\right\} \ge \beta,\tag{58}$$

with  $\beta \in (0.5, 1)$ , called a *joint chance constraint*. In this section, we extend the CSRG scheme to treat such joint chance constraints.

In principle, one could define a maximal output admissible set similar to the one defined in (9) and (10) but corresponding to the joint chance constraint (58) as follows.

$$\mathcal{O}_{\infty} = \left\{ (x_p, x_u, v) \in \mathbb{R}^{n_{xp}} \times \mathbb{R}^{n_{xu}} \times \mathbb{R}^{n_v} : \text{ if } x_p(0) = x_p, \\ x_u(0) = x_u, v(t) \equiv v, \text{ and } \{w(t)\}_{t \in \mathbb{Z}_{\geq 0}} \sim \mathcal{N}(0, W), \\ \text{then } \mathbb{P}\left\{ G_i^\top y(t) \le g_i, i = 1, ..., n_g \right\} \ge \beta \text{ for all } t \in \mathbb{Z}_{\geq 0} \right\}.$$
(59)

Then, with this new  $\mathcal{O}_{\infty}$  set, one could formulate the CSRG algorithms similarly as before. However, the exact construction of the above  $\mathcal{O}_{\infty}$  set requires evaluation of  $\mathbb{P}\{G_i^{\top}y(t) \leq g_i, i = 1, ..., n_g\}$ , which involves integra-tion of the density function of a multivariate normal distribution over a polyhedral set and is in general computationally challenging (Khachiyan, 1989). Furthermore, this  $\mathcal{O}_{\infty}$  set cannot be characterized by a collection of linear inequalities as in (23), which could also cause the online problems (38) and (40) to be difficult to solve.

Therefore, in what follows we pursue inner approximations of the above  $\mathcal{O}_{\infty}$  set that are easier to compute and will use such approximations to formulate our CSRG algorithms instead of directly using  $\mathcal{O}_{\infty}$ . In particular, we consider the following two approximation approaches:

#### 5.1 Risk allocation

Note the left-hand side of (58) can be lower bounded as

$$\mathbb{P}\left\{G_{i}^{\top}y(t) \leq g_{i}, i = 1, ..., n_{g}\right\} = \mathbb{P}\left\{\bigcap_{i=1}^{n_{g}}\left(G_{i}^{\top}y(t) \leq g_{i}\right)\right\}$$

$$= 1 - \mathbb{P}\left\{\bigcup_{i=1}^{n_{g}}\left(G_{i}^{\top}y(t) > g_{i}\right)\right\} \geq 1 - \sum_{i=1}^{n_{g}}\mathbb{P}\left\{G_{i}^{\top}y(t) > g_{i}\right\}$$

$$= 1 - \sum_{i=1}^{n_{g}}\left(1 - \mathbb{P}\left\{G_{i}^{\top}y(t) \leq g_{i}\right\}\right)$$

$$= \sum_{i=1}^{n_{g}}\mathbb{P}\left\{G_{i}^{\top}y(t) \leq g_{i}\right\} - (n_{g} - 1), \quad (60)$$

where we have used Boole's inequality in the second line. Then, it can be easily seen that one can enforce the joint chance constraint (58) through enforcing the set of individual chance constraints (8) with some  $\beta_i$ ,  $i = 1, ..., n_g$ , satisfying

$$\sum_{i=1}^{n_g} \beta_i \ge \beta + (n_g - 1). \tag{61}$$

The parameters  $\beta_i$ ,  $i = 1, ..., n_g$ , could be treated as optimization variables to reduce conservativeness in the approximation (Blackmore and Ono, 2009; Paulson et al., 2020). This way, the constraint functions in (23) characterizing the  $\mathcal{O}^i_{\infty}$  set would be nonlinear functions of the variables  $(x_p, x_u, v, \beta_i)$ . To render linear constraints so as to simplify both the offline construction of  $\mathcal{O}^i_{\infty}$  and the online problems (38) and (40), an alternative way is to pre-specify the values of  $\beta_i$ ,  $i = 1, ..., n_g$ , such that the condition (61) is satisfied. A typical choice as in Nemirovski and Shapiro (2007) is given by

$$\beta_i = \frac{\beta + (n_g - 1)}{n_g}, \quad i = 1, \cdots, n_g.$$
 (62)

To sum up, to treat the joint chance constraint (58), the CSRG algorithms are formulated as in Section 3, with the  $\beta_i$ ,  $i = 1, ..., n_g$ , determined according to (62). Following Blackmore and Ono (2009); Paulson et al. (2020), this approach to treating joint chance constraints is referred to as the *risk allocation* approach.

#### 5.2 $\beta$ -level confidence ellipsoid

Another approach to guaranteeing satisfaction of the joint chance constraint (58) is to enforce the  $\beta$ -level confidence ellipsoid of y(t) to be entirely contained in the constraint set. Specifically, the following set of conditions are enforced,

$$G_i^{\top} \mathcal{P}(t) \le g_i, \quad i = 1, \cdots, n_g, \tag{63}$$

in which  $\mathcal{P}(t) = \{y \in \mathbb{R}^{n_y} : (y - \bar{y}(t))^\top (\Sigma_y(t))^{-1} (y - \bar{y}(t)) \leq F^{-1}(\beta, n_y)\}$  is the  $\beta$ -level confidence ellipsoid of  $y(t) \sim \mathcal{N}(\bar{y}(t), \Sigma_y(t))$ , where  $F(\cdot, n_y)$  denotes the cumulative distribution function of the  $\chi^2$ -distribution with  $n_y$  degrees of freedom. Note that (63) guarantees

$$\mathbb{P}\left\{G_{i}^{\top}y(t) \leq g_{i}, i = 1, ..., n_{g}\right\} \\
\geq \mathbb{P}\left\{\left(G_{i}^{\top}y(t) \leq g_{i}, i = 1, ..., n_{g}\right) \cap \left(y(t) \in \mathcal{P}(t)\right)\right\} \\
= \mathbb{P}\left\{y(t) \in \mathcal{P}(t)\right\} = \beta,$$
(64)

where we have used (63) to derive the equality between the second and the third lines. Note also that the support function of the confidence ellipsoid  $\mathcal{P}(t)$  is  $h_{\mathcal{P}(t)}(y) = y^{\top} \bar{y}(t) + \sqrt{F^{-1}(\beta, n_y) y^{\top} \Sigma_y(t) y}$  (Kurzhanski and Varaiya, 2000). Then, according to Theorem 2.3 of Kolmanovsky and Gilbert (1998), the conditions in (63) can be equivalently expressed as

$$G_i^{\top} \bar{y}(t) = G_i^{\top} \bar{C} \bar{A}^t \begin{bmatrix} x_p(0) \\ x_u(0) \end{bmatrix} + G_i^{\top} \left( \bar{C} \sum_{k=0}^{t-1} \bar{A}^k \bar{B}_v + \bar{D}_v \right) v$$
$$\leq g_i - \sqrt{F^{-1}(\beta, n_y)} G_i^{\top} \Sigma_y(t) G_i \,. \tag{65}$$

Therefore, to treat the joint chance constraint (58), the CSRG algorithms are formulated similarly as in Section 3, but with the linear inequalities characterizing the  $\mathcal{O}_{\infty}^{i}$  set, (22), replaced with the above (65). This approach to treating joint chance constraints has been exploited in Van Hessem and Bosgra (2006); Kalabić et al. (2019), referred to as the *confidence ellipsoid* approach.

# 5.3 Comparison

The risk allocation approach and the confidence ellipsoid approach both can guarantee the satisfaction of the joint chance constraint (58), shown in (60) and (64), respectively. However, probability inequalities are exploited in (60) and (64) to achieve this guarantee, which typically cause the feasible set to shrink and result in conservativeness. We now compare the relative conservativeness of the two approaches.

Recall that in the risk allocation approach, (58) is converted into a set of constraints on the mean  $\bar{y}(t)$  as follows:

$$G_i^{\top} \bar{y}(t) \leq \tag{66}$$
$$g_i - \sqrt{2} \operatorname{erf}^{-1} \left( 2 \frac{\beta + (n_g - 1)}{n_g} - 1 \right) \sqrt{G_i^{\top} \Sigma_y(t) G_i},$$

for  $i = 1, ..., n_g$ ; while in the confidence ellipsoid approach, the following set of constraints on  $\bar{y}(t)$  are enforced:

$$G_i^{\top} \bar{y}(t) \le g_i - \sqrt{F^{-1}(\beta, n_y)} \sqrt{G_i^{\top} \Sigma_y(t) G_i}, \quad (67)$$

for  $i = 1, ..., n_q$ .

It can be seen that (66) and (67) are both linear inequalities on  $\bar{y}(t)$ , with the same left-hand side  $G_i^{\dagger} \bar{y}(t)$ and constant right-hand sides. Note that the right-hand sides are constants because the covariance  $\Sigma_y(t)$ , determined according to (17), is independent of the variables  $(x_p(0), x_u(0), v)$ . Based on such an observation, the relative conservativeness of the risk allocation approach and the confidence ellipsoid approach can be determined by comparing the right-hand sides of (66) and (67). Specifically, in the case where (66) has a greater right-hand side than (67), which implies that the feasible set characterized by (66) is a superset of that characterized by (67), the risk allocation approach is less conservative than the confidence ellipsoid approach; and vice versa. Furthermore, which one between the right-hand sides of (66) and (67) is greater can be determined by the sign of the following function,

$$\Gamma(n_y, n_g, \beta) = (68)$$
  
 $\sqrt{2} \operatorname{erf}^{-1} \left( 2 \frac{\beta + (n_g - 1)}{n_g} - 1 \right) - \sqrt{F^{-1}(\beta, n_y)},$ 

which depends only on the dimension of the output vector  $n_y$ , the number of constraints  $n_g$  and the required confidence level of constraint satisfaction  $\beta$ , but not on time t, specific system dynamics (3) or constraints  $(G_i, g_i)$ . In particular, the relationship between the sign of (68) and the relative conservativeness of the two approaches is characterized by the following proposition.

**Proposition 5:** If in (68),  $\Gamma(n_y, n_g, \beta) < 0$ , then the feasible set corresponding to the risk allocation approach is a strict superset of that corresponding to the confidence ellipsoid approach, i.e., the risk allocation approach is less conservative than the confidence ellipsoid approach; if  $\Gamma(n_y, n_g, \beta) = 0$ , then the two approaches are equally conservative; if  $\Gamma(n_y, n_g, \beta) > 0$ , then the risk allocation approach is more conservative than the confidence ellipsoid approach.

**Proof:** It can be easily seen that if  $\Gamma(n_y, n_g, \beta) < 0$ , then for any  $i = 1, ..., n_g$  and  $t \in \mathbb{Z}_{\geq 0}$ , (66) has a strictly greater right-hand side than (67), which implies that the feasible set characterized by (66) is a strict superset of that characterized by (67), i.e., the risk allocation approach is less conservative than the confidence ellipsoid approach. The other two cases can be shown in a similar way.

**Remark 2:** Although stated in the context of our chance-constrained CSRG, Proposition 5 represents a more general result on the relative conservativeness of the risk allocation approach with equal risks (62) and the confidence ellipsoid approach to treating the joint chance constraint (58). This result can also be used in other chance-constrained control techniques, such as in stochastic model predictive control (Mesbah, 2016).

For a specific joint chance constrained problem with given  $(n_y, n_g, \beta)$  values, one can refer to Proposition 5

to choose between the risk allocation approach and the confidence ellipsoid approach to achieve a less conservative CSRG design. Fig. 2 shows the graph of the function  $\Gamma(n_y, n_g, \beta)$  when  $\beta$  is fixed at 0.98. In Fig. 2, the data points marked by blue (yellow) correspond to the cases where the risk allocation approach (the confidence ellipsoid approach) is less conservative. It can be seen that for cases with small  $n_y$  and large  $n_g$ , the confidence ellipsoid approach is less conservative; the risk allocation approach is less conservative.



Fig. 2. Graph of  $\Gamma(n_y, n_g, \beta)$  for  $\beta = 0.98$ .

# 6 CSRG Application to Aircraft Flight Control

We now use numerical examples to illustrate the CSRG application to constrained control of aircraft. The aircraft models used in this section are taken from Mc-Donough and Kolmanovsky (2015a,b), which are generated using the NASA generic transport model (GTM) (Cunningham et al., 2008) at the trim condition of altitude  $h_0 = 800$  ft, airspeed  $U_0 = 118.15$  ft/s (70 knots), sideslip angle  $\beta_0 = 0$  rad, flight path angle  $\gamma_0 = 0$  rad, and yaw rate  $\dot{\psi}_0 = 0$  rad/s.

#### 6.1 Constrained longitudinal flight control

The aircraft longitudinal dynamics are represented by the following continuous-time linear model,

$$\begin{bmatrix} \Delta \dot{U} \\ \Delta \dot{\alpha} \\ \Delta \dot{q} \\ \Delta \dot{\theta} \end{bmatrix} = \begin{bmatrix} -0.0665 - 11.4608 & 0.1439 & -32.1740 \\ -0.0035 & -2.4714 & 0.9514 & 0 \\ -0.0090 & -43.9070 & -3.4738 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} \Delta \alpha \\ \Delta q \\ \Delta \theta \end{bmatrix} + \underbrace{\begin{bmatrix} -0.0435 & 0.1424 \\ -0.0043 & -0.0001 \\ -0.7662 & 0.0192 \\ 0 & 0 \end{bmatrix}}_{=B_{u}^{\text{lon}}} \begin{bmatrix} \Delta \delta_{e} \\ \Delta \delta_{T} \end{bmatrix} - \underbrace{\begin{bmatrix} -0.0665 & -11.4608 \\ -0.0035 & -2.4714 \\ -0.0090 & -43.9070 \\ 0 & 0 \end{bmatrix}}_{=B_{w}^{\text{lon}}} \begin{bmatrix} w_{x} \\ w_{z} \end{bmatrix}$$

$$(69)$$

where the states  $x_p^{\text{lon}} = [\Delta U, \Delta \alpha, \Delta q, \Delta \theta]^{\top}$  represent the deviations in longitudinal airspeed (ft/s), angle of attack (rad), pitch rate (rad/s) and pitch angle (rad), respectively, the control inputs  $u^{\text{lon}} = [\Delta \delta_e, \Delta \delta_T]^{\top}$  represent the deviations in elevator angle (rad) and thrust throttle percentage, and  $w^{\text{lon}} = [w_x, w_z]^{\top}$  represents effects of model mismatch, atmospheric disturbances/turbulence, etc. in the longitudinal and vertical directions. The treatment of more general, dynamic models for atmospheric disturbances is out of scope of this paper but will be addressed in future work. The continuous-time model (69) is converted to a discrete-time model using zero-order hold on the inputs with a sampling period of  $\Delta T = 0.1$  s for the nominal controller and our CSRG design.

We consider a state-feedback controller with integral action for tracking commanded flight path angles  $\Delta \gamma = -\Delta \alpha + \Delta \theta$ . The controller takes the form of (2), where

$$K_{p}^{\text{lon}} = \begin{bmatrix} -0.4735 & -37.7045 & 2.4948 & 46.3031 \\ -2.4179 & 38.5827 & 0.2705 & -33.6410 \end{bmatrix},$$
$$K_{u}^{\text{lon}} = \begin{bmatrix} 2.2715 \\ -6.1106 \end{bmatrix}, \qquad B_{v}^{\text{lon}} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}, \qquad (70)$$

with the integrator

$$x_{u}^{\text{lon}}(t+1) = \underbrace{\begin{bmatrix} 0 & -1 & 0 & 1 \end{bmatrix}}_{=A_{p}^{\text{lon}}} x_{p}^{\text{lon}} + x_{u}^{\text{lon}}(t) - \Delta \gamma_{\text{com}}(t).$$
(71)

We note that this controller design is motivated by the longitudinal flight controllers proposed in Mc-Donough and Kolmanovsky (2015a,b). In particular, the gains  $K^{\text{lon}} = [K_p^{\text{lon}}, K_u^{\text{lon}}]$  are obtained by solving a discrete-time Linear-Quadratic-Regulator (LQR) problem with  $\bar{A}_{\text{open}}^{\text{lon}} = \begin{bmatrix} A^{\text{lon}} & 0\\ A_p^{\text{lon}} & 1 \end{bmatrix}$ ,  $\bar{B}_u^{\text{lon}} = \begin{bmatrix} B_u^{\text{lon}}\\ 0 \end{bmatrix}$  and  $Q^{\text{lon}} = \text{diag}(10, 10, 10, 10, 100)$ ,  $R^{\text{lon}} = \text{diag}(10, 1)$ .

We assume that the aircraft operation is subject to the following set of constraints on the states and control inputs,

$$-20 \leq \Delta U(t) \leq 20, \quad -\frac{\pi}{32} \leq \Delta \alpha(t) \leq \frac{\pi}{24}, \\ -\frac{\pi}{12} \leq \Delta q(t) \leq \frac{\pi}{12}, \quad -\frac{\pi}{6} \leq \Delta \theta(t) \leq \frac{\pi}{6}, \quad (72) \\ -\frac{\pi}{6} \leq \Delta \delta_e(t) \leq \frac{\pi}{6}, \quad -25 \leq \Delta \delta_T(t) \leq 25.$$

The disturbance  $w^{\text{lon}} = [w_x, w_z]^{\top}$  is modeled as a Gaussian noise. In particular, we assume the inputs  $\{w^{\text{lon}}(t)\}_{t\in\mathbb{Z}_{\geq 0}}$  to satisfy Assumption 2 with

$$\{w^{\text{lon}}(t)\}_{t\in\mathbb{Z}_{\geq 0}} \sim \mathcal{N}\left(0, \text{diag}(10^{-2}, 10^{-4})\right).$$
 (73)

Firstly, we simulate the response of the nominal closedloop system (consisting of the plant (69) and the nominal controller (70)-(71)) starting from the initial condition  $x_p^{\text{lon}}(0) = [0, 0, 0, 0]^{\top}$  and  $x_u^{\text{lon}}(0) = 0$  to track the commanded flight path angle profile  $\Delta \gamma_{\text{com}}(t)$  shown by the red dotted curve in Fig. 3(a). The trajectories of the actual flight path angle  $\Delta \gamma(t) = -\Delta \alpha(t) + \Delta \theta(t)$  and the elevator angle  $\Delta \delta_e(t)$  are plotted in Fig. 3. It can be observed from Fig. 3(b) that the transient responses of  $\Delta \delta_e(t)$  to the step changes in  $\Delta \gamma_{\text{com}}(t)$  significantly violate the constraints  $-\frac{\pi}{6} \leq \Delta \delta_e(t) \leq \frac{\pi}{6}$ .



Fig. 3. Longitudinal flight control: Simulated trajectory of the nominal closed-loop system.

We now apply the proposed CSRG scheme to enforce the constraints (72). Due to the presence of the stochastic disturbances (73), we enforce the constraints (72) probabilistically. In this example, we enforce each of them as an individual chance constraint in the form of (8), with  $\beta_i = 0.99$  for all i = 1, ..., 12. For the CSRG online optimization problem, we choose P as the positive-definite solution to (13) with Q = diag(1, 1, 1, 1, 1) and  $R = 10^4$  in the cost function (12). We remark that a large R can increase the convergence speed of the modified reference v(t) to the commanded value r(t). Also, we choose  $\delta = 10^{-6}$  in the constraint (38c).



Fig. 4. Longitudinal flight control: Simulated trajectory of the closed-loop system augmented with CSRG Algorithm 1.

We consider both the applications of CSRG Algorithms 1 and 2 and compare them. The responses of the closedloop system starting from the same initial condition to track the same commanded flight path angle profile as before when augmented with CSRG Algorithms 1 and 2 are illustrated in Figs. 4 and 5, respectively. Recall that the CSRG replaces the original command  $\gamma_{\rm com}(t)$ in (71) with a modified reference v(t) to enforce constraints. The trajectory of v(t) is shown by the green



Fig. 5. Longitudinal flight control: Simulated trajectory of the closed-loop system augmented with CSRG Algorithm 2.

dashed-dotted curve in panel (a) of Figs. 4 and 5. It can be observed that, in both cases, v(t) deviates from the command  $\gamma_{\rm com}(t)$  when  $\gamma_{\rm com}(t)$  has step changes and converges to  $\gamma_{\rm com}(t)$  after a short-period transient response. From panel (b) of Figs. 4 and 5 we can observe that with CSRG, the significant violations of the constraints  $-\frac{\pi}{6} \leq \Delta \delta_e(t) \leq \frac{\pi}{6}$  in Fig. 3(b) have been avoided. Indeed, if we look at panel (b) of Figs. 4 and 5 more closely, we can find a few slight constraint violations over  $40 \sim 45$  s. Such slight violations are due to our probabilistic enforcement of the constraints. We also note that the other constraints of (72) are all strictly satisfied in both cases. Comparing panel (a) of Figs. 4 and 5 we can observe that, unlike the gradual convergence of v(t) to  $\gamma_{\rm com}(t)$  in Fig. 4(a), the modified reference v(t) converges to the command  $\gamma_{\rm com}(t)$  abruptly through a jump at about 2 s and through another jump at about 45 s in Fig. 5(a). This is a result of the fact that CSRG Algorithm 2 is designed for prioritizing the convergence of v(t). Meanwhile, it can also be observed that the state responses resulting from the two algorithms, shown by the blue solid curves, have similar speeds in this example. Interestingly, in Fig. 4(a) we can observe a few places where the state response is ahead of the reference response. This is partly attributed to the integrator state resets by CSRG, and is also related to effects of the stochastic disturbances (73).

To verify the closed-loop chance-constraint enforcement property of our CSRG algorithms, we run the simulations  $N_{\text{max}} = 1000$  times and consider the metric,

$$\rho_v \left( z \in \mathcal{Z} \right) = \max_{t=0,\dots,t_{\max}} \frac{N(z(t) \notin \mathcal{Z})}{N_{\max}}, \qquad (74)$$

where z denotes an output variable,  $z \in \mathcal{Z}$  denotes a constraint on the output variable, and  $N(z(t) \notin \mathcal{Z})$  denotes the observed times the constraint  $z \in \mathcal{Z}$  is violated at the time instant t among the  $N_{\max}$  simulation trials. In this case,  $\frac{N(z(t)\notin\mathcal{Z})}{N_{\max}}$  represents an estimate of the frequency of constraint violation at t. According to Proposition 2, our CSRG algorithms should guarantee that the probability of constraint satisfaction is higher than  $\beta$  at every time instant  $t = 0, ..., t_{\max}$ . This implies the value of  $\rho_v$  ( $z \in \mathcal{Z}$ ) should be upper bounded by  $1-\beta$  as  $N_{\max} \to \infty$ .

For the above longitudinal flight control example, we consider the variable  $\Delta \delta_e$  and the constraint  $\Delta \delta_e \leq \frac{\pi}{6}$ . We choose to consider this pair because it is observed in Figs. 4(b) and 5(b) that  $\Delta \delta_e$  rides the constraint boundary at  $\frac{\pi}{6}$  over 40 ~ 45 s, which implies higher chances of constraint violation. The applications of our CSRG Algorithms 1 and 2 lead to  $\rho_v \left(\Delta \delta_e \leq \frac{\pi}{6}\right) = 0.009$  and 0.008, respectively, both of which are less than and close to the theoretical bound  $1 - \beta = 1 - 0.99 = 0.01$ . This result verifies the chance-constraint enforcement guarantee of our CSRG algorithms.

#### 6.2 Constrained lateral flight control

The aircraft lateral dynamics are represented by the following continuous-time linear model,

$$\begin{bmatrix} \Delta \dot{\beta} \\ \Delta \dot{p} \\ \Delta \dot{r} \\ \Delta \dot{\phi} \end{bmatrix} = \begin{bmatrix} -0.5229 & 0.0861 & -0.9852 & 0.2374 \\ -90.5885 & -6.2736 & 2.0861 & 0 \\ 29.1873 & -0.4833 & -1.4043 & 0 \\ 0 & 1 & 0.0857 & 0 \end{bmatrix} \begin{bmatrix} \Delta \beta \\ \Delta p \\ \Delta r \\ \Delta \phi \end{bmatrix} \\ = A^{\text{lat}} \\ + \underbrace{\begin{bmatrix} -0.0002 & 0.0031 \\ -0.9174 & 0.2321 \\ -0.0523 & -0.4436 \\ 0 & 0 \end{bmatrix}}_{=B^{\text{lat}}_{w}} \begin{bmatrix} \Delta \delta_a \\ \Delta \delta_r \end{bmatrix} - \begin{bmatrix} -0.5229 \\ -90.5885 \\ 29.1873 \\ 0 \end{bmatrix} w_y, \quad (75)$$

where the states  $x_p^{\text{lat}} = [\Delta\beta, \Delta p, \Delta r, \Delta\phi]^{\top}$  represent the deviations in sideslip angle (rad), roll rate (rad/s), yaw rate (rad/s) and roll angle (rad), respectively, the control inputs  $u^{\text{lat}} = [\Delta\delta_a, \Delta\delta_r]^{\top}$  represent the deviations in aileron angle (rad) and rudder angle (rad), and the disturbance input  $w^{\text{lat}} = w_y$  represents effects of model mismatch, atmospheric disturbances/turbulence, etc. in the lateral direction. Firstly, as in the longitudinal case, the continuous-time model (75) is converted to a discrete-time model using zero-order hold on the inputs with a sampling period of  $\Delta T = 0.1$  s. Then, a nominal controller in the form of (2) with

$$K_p^{\text{lat}} = \begin{bmatrix} -1.4874 \ 0.3021 \ 0.8549 \ 2.1801 \\ -0.4431 \ 0.2363 \ 1.2214 \ 2.1289 \end{bmatrix},$$

$$K_u^{\text{lat}} = \begin{bmatrix} 0.0680 \\ 0.0684 \end{bmatrix}, \qquad B_v^{\text{lat}} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}, \qquad (76)$$

$$A_p^{\text{lat}} = \begin{bmatrix} 0 \ 0 \ 0 \ 1 \end{bmatrix}, \qquad A_u^{\text{lat}} = 1, \qquad D_v^{\text{lat}} = -1,$$

is used to track commanded roll angles  $r(t) = \Delta \phi_{\rm com}(t)$ (McDonough and Kolmanovsky, 2015b), where the gains  $K^{\rm lat} = [K_p^{\rm lat}, K_u^{\rm lat}]$  are obtained by solving a discrete-

time LQR problem with 
$$\bar{A}_{\text{open}}^{\text{lat}} = \begin{bmatrix} A^{\text{lat}} & 0\\ A_p^{\text{lat}} & A_u^{\text{lat}} \end{bmatrix}, \ \bar{B}_u^{\text{lat}} =$$

 $\begin{bmatrix} B_u^{\text{lat}} \\ 0 \end{bmatrix} \text{ and } Q^{\text{lat}} = \text{diag}(100, 100, 100, 100, 1), R^{\text{lat}} = \text{diag}(100, 100). \text{ We consider the following set of constraints.}$ 

$$-\frac{\pi}{12} \leq \Delta\beta \leq \frac{\pi}{12}, \qquad -\frac{\pi}{12} \leq \Delta p \leq \frac{\pi}{12}, \\ -\frac{\pi}{12} \leq \Delta r \leq \frac{\pi}{12}, \qquad -\frac{\pi}{3} \leq \Delta\phi \leq \frac{\pi}{3}, \qquad (77) \\ -\frac{\pi}{6} \leq \Delta\delta_a \leq \frac{\pi}{6}, \qquad -\frac{\pi}{6} \leq \Delta\delta_r \leq \frac{\pi}{6},$$

and we model the disturbance  $w^{\text{lat}} = w_y$  as a Gaussian noise satisfying Assumption 2 with

$$\{w^{\text{lat}}(t)\}_{t\in\mathbb{Z}_{\geq 0}} \sim \mathcal{N}(0, 10^{-5}).$$
 (78)

In this example, we enforce the constraints (77) jointly as a chance constraint in the form of (58), where the required confidence level  $\beta$  is chosen as 0.98. It can be determined from (77) that we have  $n_y = 6$  outputs and  $n_g = 12$  constraints. In this case, referring to Proposition 5 or Fig. 2, we know that the risk allocation approach has a lower degree of conservativeness than the confidence ellipsoid approach for treating the formulated joint chance constraint. Therefore, we choose to use the risk allocation approach to formulate our CSRG algorithm. In particular, according to (62), we set  $\beta_i = \frac{0.98+(12-1)}{12} = 0.9983$  for all i = 1, ..., 12. The parameters P, R and  $\delta$  for the CSRG online optimization problem are chosen to be the same as in the longitudinal case.

The state response of the nominal closed-loop system, i.e., without CSRG, and the reference and state responses of the closed-loop system augmented with CSRG Algorithm 1 starting from the initial condition  $x_p^{\text{lat}}(0) = [0, 0, 0, 0]^{\top}$  and  $x_u^{\text{lat}}(0) = 0$  to track the commanded roll angle profile  $\Delta \phi_{\text{com}}(t)$  shown by the red dotted curve in Fig. 6(a-1) are illustrated in Fig. 6(a) and (b), respectively. It can be observed from Fig. 6 that without CSRG, the constraints on  $\Delta p$  and on  $\Delta \delta_r$  are violated; with CSRG, these constraint violations are avoided. We note that the other constraints of (77) are also enforced when CSRG is used.

Similarly as in the previous example, we run the simulation  $N_{\text{max}} = 1000$  times and count the value of  $\rho_v (z \in \mathbb{Z})$ , where we now consider  $z = (x_p^{\text{lat}}, u^{\text{lat}})$  and  $\mathbb{Z}$  to be defined by all of the constraints in (77). We consider this pair because in this example our CSRG algorithm enforces (77) as a joint chance constraint. The application of CSRG Algorithm 1 with the risk allocation approach leads to  $\rho_v (z \in \mathbb{Z}) = 0.006$ , which is smaller than the required bound  $1 - \beta = 1 - 0.98 = 0.02$ . The difference between the observed  $\rho_v (z \in \mathbb{Z}) = 0.006$  and  $1 - \beta = 0.02$  reflects the conservative approximation nature of the risk allocation approach.



Fig. 6. Lateral flight control: Simulated trajectories of (a) the nominal closed-loop system and (b) the closed-loop system augmented with CSRG Algorithm 1.

#### 6.3 Comparisons

To compare the constrained domain of attraction with both controller state and reference modifications and that with only reference modification (i.e., without controller state modification), we consider the following set,

$$\tilde{\mathcal{O}}_{\infty}^{x_u(0)=0} = \tilde{\mathcal{O}}_{\infty} \cap \big\{ (x_p, x_u, v) : x_u = 0 \big\}.$$
(79)

This set represents the set of chance-constraint admissible pairs of initial plant state,  $x_p(0)$ , and constant reference input, v, when the initial controller state,  $x_u(0)$ , is zero and cannot be adjusted, which serves as an example of allowing only reference modification. Then, we consider the projections of  $\tilde{\mathcal{O}}_{\infty}$  and  $\tilde{\mathcal{O}}_{\infty}^{x_u(0)=0}$  onto the  $x_p$ -space, denoted as  $\operatorname{proj}_{x_p}(\tilde{\mathcal{O}}_{\infty})$  and  $\operatorname{proj}_{x_p}(\tilde{\mathcal{O}}_{\infty}^{x_u(0)=0})$ , respectively. According to the definition of  $\tilde{\mathcal{O}}_{\infty}$ ,  $\operatorname{proj}_{x_p}(\tilde{\mathcal{O}}_{\infty})$  represents the set of plant states at which there exist controller state and reference pairs that guarantee their corresponding future system trajectories satisfying the chance constraints. Referring

to Propositions 3 and 4, the reference v(t) and state  $\bar{x}(t)$  responses in closed-loop operation of the system augmented with CSRG starting from these plant states are guaranteed to converge to r in finite time almost surely and to  $\bar{x}^*(r)$  in mean square for constant, steady-state constraint-admissible command r. Therefore,  $\operatorname{proj}_{x_p}(\tilde{\mathcal{O}}_{\infty})$  is referred to as the constrained domain of attraction of CSRG. In contrast,  $\operatorname{proj}_{x_p}(\tilde{\mathcal{O}}_{\infty}^{x_u(0)=0})$  represents the set of plant states at which the chance constraints can be enforced by properly choosing the reference value if the current controller state is zero and cannot be adjusted.

The comparison between  $\operatorname{proj}_{x_p}(\tilde{\mathcal{O}}_{\infty})$  and  $\operatorname{proj}_{x_p}(\tilde{\mathcal{O}}_{\infty}^{x_u(0)=0})$  for the longitudinal flight control example is illustrated in Fig. 7, where the blue and red 3D polygons show, respectively, the projections of  $\tilde{\mathcal{O}}_{\infty}$  and  $\tilde{\mathcal{O}}_{\infty}^{x_u(0)=0}$  onto the  $(\Delta U, \Delta \alpha, \Delta \theta)$ -space. Similarly,  $\operatorname{proj}_{x_p}(\tilde{\mathcal{O}}_{\infty})$  and  $\operatorname{proj}_{x_p}(\tilde{\mathcal{O}}_{\infty}^{x_u(0)=0})$  for the lateral flight control example are illustrated by the blue solid and red dash-dotted 2D polygons in Fig. 8. It can be observed from Figs. 7 and 8 that  $\operatorname{proj}_{x_p}(\tilde{\mathcal{O}}_{\infty})$  is much larger than  $\operatorname{proj}_{x_p}(\tilde{\mathcal{O}}_{\infty}^{x_u(0)=0})$ in both cases. This demonstrates the fact that, by admitting both controller state and reference modifications. our proposed CSRG scheme can have a considerably larger constrained domain of attraction compared to admitting only reference modification as in conventional RG schemes. In Fig. 8, we also show the projection onto the  $(\Delta\beta, \Delta\phi)$ -plane of the  $\tilde{\mathcal{O}}_{\infty}$  set corresponding to the confidence ellipsoid approach to treating the formulated joint chance constraint in the lateral flight control example. It can be observed that the green dashed polygon, which corresponds to the confidence ellipsoid approach, is strictly contained in the blue solid polygon, which corresponds to the risk allocation approach. The conclusion that the risk allocation approach is less conservative than the confidence ellipsoid approach in this example is consistent with Proposition 5 and Fig. 2. Specifically, in this example we have  $(n_y, n_g, \beta) = (6, 12, 0.98)$  and  $\Gamma(n_y, n_g, \beta) = \Gamma(6, 12, 0.98) < 0.$ 

# 7 Concluding Remarks

In this paper, we introduced the chance-constrained controller state and reference governor (CSRG), as an add-on scheme for closed-loop systems with dynamic controllers that are subject to stochastic disturbances and pointwise-in-time constraints. We showed that this chance-constrained CSRG guarantees closed-loop chance-constraint satisfaction, almost-sure finite-time convergence of the modified reference to constant, steady-state constraint-admissible command, and meansquare stability of the commanded state set-point. We also extended CSRG formulation from treating individual chance constraints to treating joint chance constraints, and developed guidelines for when risk allocation is advantageous over the confidence ellipsoid approach in treating such joint constraints. Finally, we illustrated CSRG application using constrained aircraft



Fig. 7. Longitudinal flight control: Projections of  $\tilde{\mathcal{O}}_{\infty}$  versus  $\tilde{\mathcal{O}}_{\infty}^{x_u(0)=0}$  onto the  $(\Delta U, \Delta \alpha, \Delta \theta)$ -space.



Fig. 8. Lateral flight control: Projections of  $\tilde{\mathcal{O}}_{\infty}$ ,  $\tilde{\mathcal{O}}_{\infty}^{x_u(0)=0}$  with the risk allocation (RA) approach, and  $\tilde{\mathcal{O}}_{\infty}$  with the confidence ellipsoid (CE) approach onto the  $(\Delta\beta, \Delta\phi)$ -plane.

flight control examples. Extensions of the CSRG to nonlinear systems and non-Gaussian stochastic disturbances will be pursued in future work. As mentioned in the introduction, combining CSRG with the ECG to further improve performance is also worth investigating and is left as a topic for future research.

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#### References

- Bemporad, A., 1998. Reference governor for constrained nonlinear systems. IEEE Transactions on Automatic Control 43 (3), 415–419.
- Bemporad, A., Casavola, A., Mosca, E., 1997. Nonlinear control of constrained linear systems via predictive reference management. IEEE Transactions on Automatic Control 42 (3), 340–349.

Birge, J. R., Louveaux, F., 2011. Introduction to stochastic programming. Springer Science & Business Media.

- Blackmore, L., Ono, M., 2009. Convex chance constrained predictive control without sampling. In: AIAA Guidance, Navigation, and Control Conference. p. 5876.
- Bogachev, V. I., 1998. Gaussian measures. No. 62. American Mathematical Soc.
- Borrelli, F., Falcone, P., Pekar, J., Stewart, G., 2009. Reference governor for constrained piecewise affine systems. Journal of Process Control 19 (8), 1229–1237.
- Bupp, R. T., Bernstein, D. S., Chellaboina, V. S., Haddad, W. M., 2000. Resetting virtual absorbers for vibration control. Journal of Vibration and Control 6 (1), 61–83.
- Casavola, A., Mosca, E., Angeli, D., 2000. Robust command governors for constrained linear systems. IEEE Transactions on Automatic Control 45 (11), 2071– 2077.
- Cunningham, K., Foster, J., Murch, A., Morelli, E., 2008. Practical application of a subscale transport aircraft for flight research in control upset and failure conditions. In: AIAA Atmospheric Flight Mechanics Conference and Exhibit. p. 6200.
- Folland, G. B., 1999. Real analysis: Modern techniques and their applications. Vol. 40. John Wiley & Sons.
- Garone, E., Di Cairano, S., Kolmanovsky, I., 2017. Reference and command governors for systems with constraints: A survey on theory and applications. Automatica 75, 306–328.
- Gilbert, E., Kolmanovsky, I., 2002. Nonlinear tracking control in the presence of state and control constraints: A generalized reference governor. Automatica 38 (12), 2063–2073.
- Gilbert, E. G., Kolmanovsky, I., 1999. Fast reference governors for systems with state and control constraints and disturbance inputs. International Journal of Robust and Nonlinear Control: IFAC-Affiliated Journal 9 (15), 1117–1141.
- Gilbert, E. G., Ong, C.-J., 2011. Constrained linear systems with hard constraints and disturbances: An extended command governor with large domain of attraction. Automatica 47 (2), 334–340.
  Guo, Y., Gong, Y., Fang, Y., Khargonekar, P. P.,
- Guo, Y., Gong, Y., Fang, Y., Khargonekar, P. P., Geng, X., 2013. Energy and network aware workload management for sustainable data centers with thermal storage. IEEE Transactions on Parallel and Distributed Systems 25 (8), 2030–2042.
- Hoblit, F. M., 1988. Gust loads on aircraft: Concepts and applications. American Institute of Aeronautics and Astronautics.
- Kalabić, U., Vermillion, C., Kolmanovsky, I., 2017. Constraint enforcement for a lighter-than-air windenergy system: An application of reference governors with chance constraints. IFAC-PapersOnLine 50 (1), 13258–13263.
- Kalabić, U. V., Li, N. I., Vermillion, C., Kolmanovsky, I. V., 2019. Reference governors for chanceconstrained systems. Automatica 109, 108500.
- Khachiyan, L. G., 1989. The problem of calculating the volume of a polyhedron is enumerably hard. Russian Mathematical Surveys 44 (3), 199.

- Kolmanovsky, I., Gilbert, E. G., 1998. Theory and computation of disturbance invariant sets for discrete-time linear systems. Mathematical Problems in Engineering 4 (4), 317–367.
- Kurzhanski, A. B., Varaiya, P., 2000. Ellipsoidal techniques for reachability analysis: Internal approximation. Systems & Control Letters 41 (3), 201–211.
- Li, N., Kolmanovsky, I. V., Girard, A., 2020. A reference governor for nonlinear systems with disturbance inputs based on logarithmic norms and quadratic programming. IEEE Transactions on Automatic Control 65 (7), 3207–3214.
- Li, X., Li, N., Kolmanovsky, I., Epureanu, B. I., 2021. Stochastic model predictive control for remanufacturing system management. Journal of Manufacturing Systems 59, 355–366.
- Mayne, D. Q., Rawlings, J. B., Rao, C. V., Scokaert, P. O., 2000. Constrained model predictive control: Stability and optimality. Automatica 36 (6), 789–814.
- McDonough, K., Kolmanovsky, I., 2015a. Controller state and reference governors for discrete-time linear systems with pointwise-in-time state and control constraints. In: American Control Conference (ACC). IEEE, pp. 3607–3612.
- McDonough, K., Kolmanovsky, I., 2015b. Integrator resetting for enforcing constraints in aircraft flight control systems. In: AIAA Guidance, Navigation, and Control Conference. p. 1995.
- Mesbah, A., 2016. Stochastic model predictive control: An overview and perspectives for future research. IEEE Control Systems Magazine 36 (6), 30–44.
- Mesbah, A., Kolmanovsky, I. V., Di Cairano, S., 2019. Stochastic model predictive control. In: Handbook of Model Predictive Control. Springer, pp. 75–97.
- Meyn, S. P., Caines, P., 1991. Asymptotic behavior of stochastic systems possessing Markovian realizations. SIAM Journal on Control and Optimization 29 (3), 535–561.
- Nemirovski, A., Shapiro, A., 2007. Convex approximations of chance constrained programs. SIAM Journal on Optimization 17 (4), 969–996.
- Osorio, J., Ossareh, H. R., 2018. A stochastic approach to maximal output admissible sets and reference governors. In: 2018 IEEE Conference on Control Technology and Applications (CCTA). IEEE, pp. 704–709.
- Paulson, J. A., Buehler, E. A., Braatz, R. D., Mesbah, A., 2020. Stochastic model predictive control with joint chance constraints. International Journal of Control 93 (1), 126–139.
- Tarn, T.-J., Rasis, Y., 1976. Observers for nonlinear stochastic systems. IEEE Transactions on Automatic Control 21 (4), 441–448.
- van de Geijn, R., Goto, K., 2011. BLAS (Basic Linear Algebra Subprograms). In: Encyclopedia of Parallel Computing. Springer, Boston, MA, pp. 157–164.
- Van Hessem, D., Bosgra, O., 2006. Stochastic closedloop model predictive control of continuous nonlinear chemical processes. Journal of Process Control 16 (3), 225–241.
- Zhang, H., Li, P., 2011. Chance constrained programming for optimal power flow under uncertainty. IEEE Transactions on Power Systems 26 (4), 2417–2424.