

Experimental observation of the geostrophic turbulence regime of rapidly rotating convection

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The competition between turbulent convection and global rotation in planetary and stellar interiors governs the transport of heat and tracers, as well as magnetic field generation. These objects operate in dynamical regimes ranging from weakly rotating convection to the “geostrophic turbulence” regime of rapidly rotating convection. However, the latter regime has remained elusive in the laboratory, despite a worldwide effort to design ever-taller rotating convection cells over the last decade. Building on a recent experimental approach where convection is driven radiatively, we report heat transport measurements in quantitative agreement with this scaling regime, the experimental scaling law being validated against direct numerical simulations (DNS) of the idealized setup. The scaling exponent from both experiments and DNS agrees well with the geostrophic turbulence prediction. The prefactor of the scaling law is greater than the one diagnosed in previous idealized numerical studies, pointing to an unexpected sensitivity of the heat transport efficiency to the precise distribution of heat sources and sinks, which greatly varies from planets to stars.

turbulent convection | geophysical and astrophysical fluid dynamics | rotating flows

The strong buoyancy gradients inside planets and stars drive turbulent convective flows that are responsible for the efficient transport of heat and tracers, as well as for the generation of the magnetic fields of these objects through the dynamo effect. This thermal and/or compositional driving competes with the global rotation of the astrophysical object: While moderate global rotation only affects the largest flow structures (1–3), rapid global rotation greatly impedes radial motion through the action of the Coriolis force, thereby restricting the convective heat transfer (4, 5). Because astrophysical and geophysical flows operate at extreme parameter values, beyond what will ever be achieved in laboratory experiments and numerical simulations, the characterization of these highly complex flows proceeds through the experimental or numerical determination of the constitutive equation, or scaling law, that relates the turbulent heat flux to the internal temperature gradients. Extrapolating this scaling law to the extreme parameter values of astrophysical objects sets the effective transport coefficients, the turbulent energy dissipation rate, the mixing efficiency, and the power available to induce magnetic field (4, 6–11).

Within the Boussinesq approximation (12) and adopting a local Cartesian geometry, the scaling laws are cast in terms of the dimensionless parameters that govern the system: the flux-based Rayleigh number $Ra_P = \alpha g P H^4 / \rho C \kappa^2 \nu$ quantifies the strength of the heat flux P , where H denotes the height of the fluid domain, α is the coefficient of thermal expansion, g is the acceleration of gravity, κ is the thermal diffusivity, ν is the kinematic viscosity, ρ is the mean density, and C is the specific heat capacity. The Nusselt number $Nu = PH / \rho C \kappa \Delta T$ measures the heat transport efficiency of the turbulent flow, as compared to that of a steady motionless fluid, in terms of the typical vertical temperature drop ΔT . Finally, the magnitude of the Coriolis force can be quantified through the Ekman number

$E = \nu / 2\Omega H^2$, a low value of E corresponding to a rapid global rotation rate Ω .

At the theoretical level, several arguments have been put forward to predict the scaling law for the heat transport efficiency of rotationally constrained turbulent convection, as measured by the Nusselt number Nu . Central to these theories is the assumption that the scaling relation between the turbulent heat flux and the internal temperature gradient should not involve the tiny molecular diffusivities κ and ν . In the physics community, this assumption is sometimes referred to as the existence of an “ultimate regime” (13), while, in the astrophysical community, it is often referred to as the “mixing-length” regime, because the latter theory neglects molecular diffusivities at the outset (6, 14).

The second assumption is that the heat transport efficiency of the flow depends only on the supercriticality of the system, that is, on the ratio of the Rayleigh number to the threshold Rayleigh number for the emergence of thermal convection. This idea is put on firm analytical footing through careful asymptotic expansions of the equations of thermal convection in the rapidly rotating limit (5, 15–17). When combined, these two assumptions lead to the following scaling law for turbulent heat transport by rapidly rotating thermal convection (see ref. 4 for the initial derivation):

$$Nu = C \times Ra_P^{3/5} E^{4/5} Pr^{-1/5}, \quad [1]$$

where $Pr = \nu / \kappa$ is the Prandtl number and C is a dimensionless prefactor. Eq. 1 is referred to as the “geostrophic

Significance

Turbulent convection is the main process through which nature moves fluids around, be it in deep planetary and stellar interiors or in the external fluid layers of planets and their satellites. Laboratory studies aim at reproducing the resulting fully turbulent flows, with the goal of determining the effective transport coefficients to be input into coarse geophysical or astrophysical models. Crucial to these applications is planetary or stellar rotation, which competes with convective processes to set the emergent transport properties. Building on a recent experimental approach that bypasses the limitations of boundary-forced convective flows, we report laboratory measurements in quantitative agreement with the fully turbulent regime of rotating convection.

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turbulence” scaling law of rapidly rotating convection.* In terms of the temperature-based Rayleigh number $Ra = Ra_P / Nu$, this scaling law becomes

$$Nu = C_{Ra} \times Ra^{3/2} E^2 Pr^{-1/2}, \quad [2]$$

where the dimensionless prefactor is $C_{Ra} = C^{5/2}$. Over the last decade, several state-of-the-art laboratory experiments have been developed to observe this extreme scaling regime and validate the geostrophic turbulence scaling law [1]: the Turbulent Rotating Convection to the Extreme (TROCONVEX) experiment in Eindhoven (18), the rotating U-boot experiment in Göttingen (19, 20), the Trieste experiment at International Centre for Theoretical Physics (21, 22), and the Romag and Nomag experiments at University of California, Los Angeles (23, 24). The goal is to produce a strongly turbulent convective flow in which rotational effects remain predominant (hence the ever-taller convective cells), while avoiding parasitic centrifugal effects (25). These experiments are all based on the Rayleigh-Bénard (RB) geometry, where a layer of fluid is contained between a hot bottom plate and a cold top one. A particularly challenging task then is to overcome the throttling effect of the boundary layers near these two plates: Fluid hardly moves there, and heat needs be diffused away from those regions (26). Even though asymptotic analysis indicates that heat transport should be controlled by the bulk turbulent flow in rapidly rotating RB convection, laboratory realizations indicate that the boundary processes keep limiting the heat transfer throughout the entire cell (27), bringing the molecular diffusivities back into play and preventing the observation of the scaling law [1] associated with the bulk rotating turbulent flow. Forty years after its initial derivation (4) and despite a worldwide effort to design ever-taller convection cells, the geostrophic regime of rapidly rotating convection still awaits experimental validation (28).

Recently, we introduced an innovative laboratory setup to overcome the above-mentioned limitations of RB convection as a model for bulk natural flows (29). Specifically, we used a combination of radiative internal heating and effective internal cooling to bypass the throttling boundary layers of traditional RB convection and achieve the fully turbulent—or “ultimate”—regime of nonrotating convection (29–31). These recent experimental developments suggest an alternative route to observe the geostrophic regime of rapidly rotating turbulent convection in the laboratory: Instead of trying to overcome the throttling effect of the RB boundary layers through intense thermal forcing, one can take advantage of the radiatively driven setup, where these boundary layers are readily bypassed, and subject the radiatively driven turbulent convective flow to rapid global rotation.

The resulting experimental setup, sketched in Fig. 1, is an evolution over the nonrotating setup described in a previous publication (29). The apparatus consists of a cylindrical tank of radius 10 cm with a transparent sapphire bottom boundary, filled with a light-absorbing mixture of water and carbon-black dye. A powerful spotlight located under a water-cooled infrared (IR) screening stage shines at the tank from below. Absorption of light by the dye results in an internal heat source that decreases exponentially with height z measured upward from the bottom of the tank, transferring to the fluid a total heat flux P over an e-folding absorption length ℓ . This source term causes the temperature at every location inside the tank to increase linearly with time. Superposed to this linear drift are internal temperature gradients that develop inside the tank and rapidly reach a statistically steady state. As recalled in *Materials and Methods*, the internal temperature difference between any two points inside the tank is then governed by a combination of the exponential

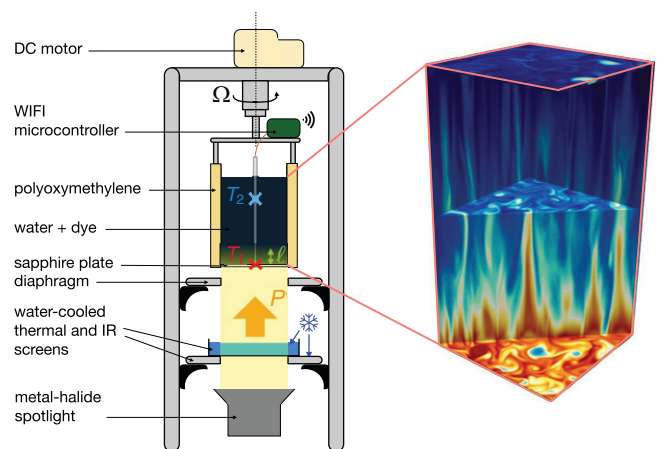


Fig. 1. Radiatively driven rotating convection. A powerful spotlight shines from below at a mixture of water and dye. The resulting internal heat source decreases exponentially with height over the absorption length ℓ , delivering a total heat flux P . The cylindrical tank is attached from above to a DC motor that imposes global rotation at a rate Ω (slight curvature of the top free surface not represented). Two thermocouples T_1 and T_2 measure the vertical temperature drop in the rotating frame, the data being communicated through WiFi to a remote Arduino microcontroller. On the right-hand side is a DNS snapshot of the temperature field in horizontally periodic geometry devoid of centrifugal and sidewall effects, highlighting the vertically elongated structures of rotating convection ($Ra_P = 10^{12}$, $E = 2 \times 10^{-6}$, $Pr = 7$, $\ell/H = 0.048$, arbitrary color scale ranging from blue for cool fluid to red for warm fluid).

radiative heat source together with an effective uniform heat sink.

The experimental tank is attached from above to a DC motor that drives global rotation at a constant rate $\Omega \in [0; 85]$ rpm around the vertical axis of the cylinder. Rotation results in a slight curvature of the free surface: The relative variations in fluid height between center and periphery reach $\pm 20\%$ and $\pm 13\%$ for the two most rapidly rotating and shallowest data points, but are below $\pm 10\%$ (and often much below) for the remaining ~ 60 data points. Onboard temperature measurements are performed using two thermocouples, one in contact with the bottom sapphire plate and one at $z = 3H/4$, where H denotes the height of the free surface on the axis of the cylindrical cell, where the probes are located. The temperature signals are transmitted through WiFi to a remote Arduino microcontroller to ensure live monitoring of the experimental runs.

We show, in Fig. 2, the Nusselt number based on the time-averaged temperature difference ΔT between the two probes, for experimental runs spanning 1.5 decades in Ra_P and 2.5 decades in E , and two values of the dimensionless absorption length ℓ/H . The dataset is provided in *SI Appendix, Tables 1–2*, together with estimates of the error bars. In a similar fashion to the more standard RB system, for an approximately constant Ra_P , an increase in the global rotation rate leads to a dramatic drop in the heat transport efficiency as measured by the Nusselt number Nu .†

With the goal of establishing the turbulent nature of the flow and assessing the independence of its transport properties with respect to the molecular diffusivities, we form the ν - and κ -independent reduced Nusselt number $\mathcal{N} = Nu E / Pr$, together with the composite control parameter $\mathcal{R} = Ra_P E^3 / Pr^2$. The latter combination is the only dimensionless control parameter if

† As shown in *SI Appendix, Tables 1–2*, the temperature range varies between different data points, the consequence being that Ra_P and Pr vary between different points of a constant- H curve in Fig. 2. The entire range of Pr spanned by the experimental data is $4.4 \leq Pr \leq 6.7$.

*Geostrophy refers to the large-scale balance between the Coriolis and pressure forces.

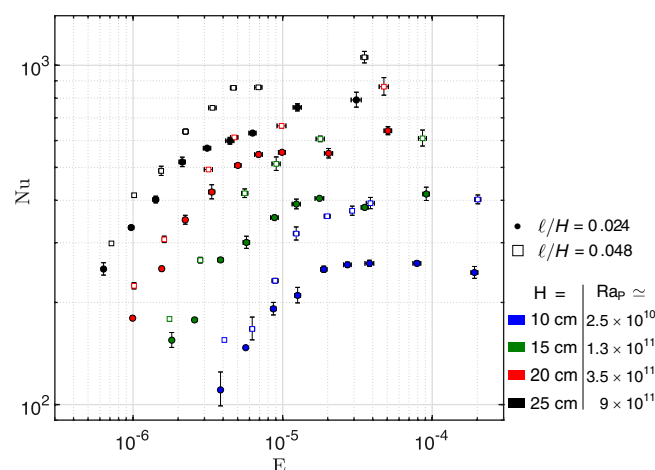


Fig. 2. Suppression of heat transport by global rotation. Heat transport efficiency Nu as a function of the Ekman number E , for various fluid heights: blue, $H = 10$ cm, $Ra_p \approx 2.5 \times 10^{10}$; green, $H = 15$ cm, $Ra_p \approx 1.3 \times 10^{11}$; red, $H = 20$ cm, $Ra_p \approx 3.5 \times 10^{11}$; black, $H = 25$ cm, $Ra_p \approx 9 \times 10^{11}$. The dimensionless absorption length is $\ell/H = 0.024$ (filled circles) or $\ell/H = 0.048$ (open squares). For fixed H and ℓ , the mixing efficiency dramatically decreases with increasing rotation rate (decreasing E). Error bars are estimated from the values obtained for the first and second halves of the measurement interval; see *Materials and Methods* and *SI Appendix*.

the diffusivities are to play no roles (9, 10, 32). $\mathcal{R}$ is also the cube of the so-called flux-based convective Rossby number, identified as the main control parameter of open ocean convection (17, 33). We plot $\mathcal{N}$ as a function of $\mathcal{R}$ in Fig. 3 (data points and estimates of the error are provided in *SI Appendix*). In this representation, the dataset for a given value of ℓ/H collapses onto a single master curve, which validates the fact that the molecular diffusivities are irrelevant: We conclude that the present experimental setup achieves a “fully turbulent” scaling regime, according to the definition given at the outset. The collapse is particularly good for rapid global rotation and slow global rotation—low and large $\mathcal{R}$, respectively—with a bit more scatter for intermediate values. For slow global rotation (large $\mathcal{R}$), the master curve gradually approaches the scaling law of radiatively driven nonrotating convection, reported in previous publications (29–31). This regime is associated with a large- $\mathcal{R}$ asymptote of the form $\mathcal{N} \approx \mathcal{R}^{1/3}$, represented in Fig. 3: After crossing out E from both sides of the scaling relation $\mathcal{N} \approx \mathcal{R}^{1/3}$, one recovers the ultimate scaling law of nonrotating convection, where Nu is proportional to the square root of Ra (29–31). The approach to that asymptotic behavior is clearly visible for $\ell/H = 0.024$ at large $\mathcal{R}$, with a bit more scatter for $\ell/H = 0.048$.[‡] More interestingly, the focus of the present study is on the rapidly rotating regime that arises for $\mathcal{R} \lesssim 3 \times 10^{-7}$. In this parameter range, the master curve follows a power-law behavior $\mathcal{N} \approx \mathcal{R}^\beta$ over one and a half decades. The best-fit exponents β are given in Table 1. Over the last decade in $\mathcal{R}$, we measure $\beta = 0.57 \pm 0.03$ and $\beta = 0.62 \pm 0.01$, respectively, for $\ell/H = 0.024$ and $\ell/H = 0.048$. These values are within 5% of the theoretical exponent $\beta = 3/5$ associated with the geostrophic turbulence scaling-law [1].

While the flux-based parameter $\mathcal{R}$ is the natural control parameter of the present experiment, the reader accustomed to the standard RB setup may be interested in characterizing the data in terms of the Rayleigh number Ra based on the emergent temperature gradient. In *SI Appendix*, we thus plot $\mathcal{N}$ as a function of the

[‡]One would probably need to reach larger $\mathcal{R}$ to avoid any signature of the intermediate- $\mathcal{R}$ scatter.

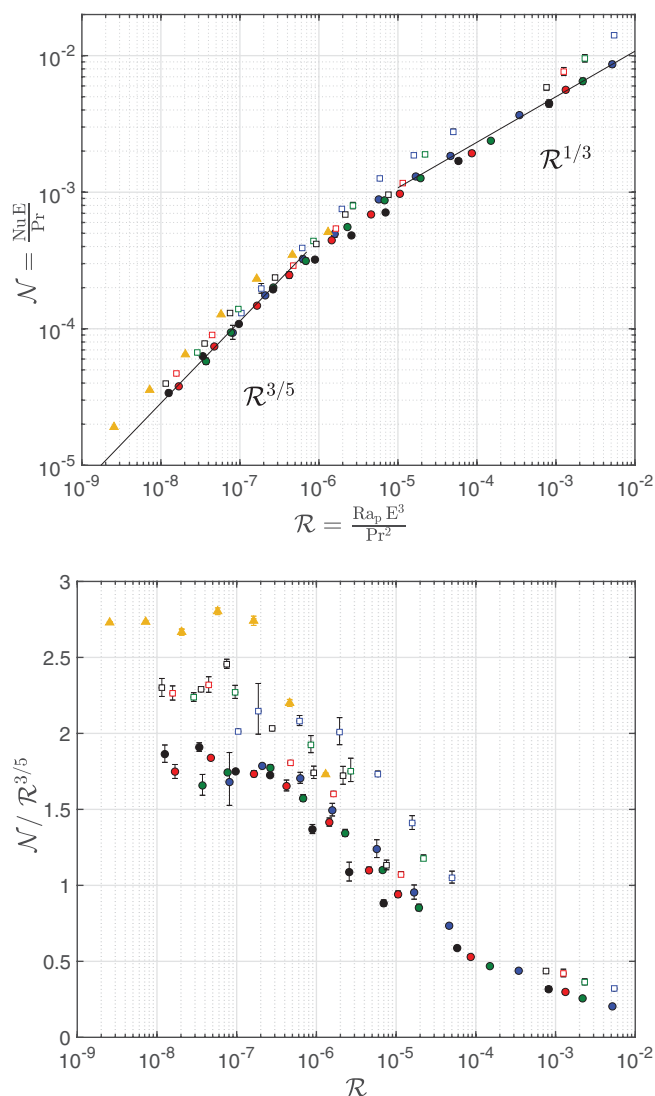


Fig. 3. Observation of the geostrophic turbulence regime. (Top) In terms of the diffusivity-independent parameters $\mathcal{N}$ and $\mathcal{R}$, the data gathered for a given value of ℓ/H collapse onto a master curve, which validates the “fully turbulent” assumption. In the rapidly rotating regime $\mathcal{R} \lesssim 3 \times 10^{-7}$, the master curve displays a power-law behavior over one and a half decades in $\mathcal{R}$, in excellent agreement with the prediction $\mathcal{N} \approx \mathcal{R}^{3/5}$ associated with the geostrophic turbulence scaling regime of rapidly rotating convection (shown as an eye guide; see Table 1 for best-fit exponents). Same symbols as in Fig. 2 for the experimental data. The triangles are DNS data for $Ra_p = 10^{12}$, $Pr = 7$, and $\ell/H = 0.048$. Experimental and numerical error bars are visible when larger than the symbol size. (Bottom) Same data compensated by the geostrophic turbulence scaling prediction. An approximate plateau is observed for $\mathcal{R} \lesssim 3 \times 10^{-7}$.

diffusivity-free Rayleigh number $Ra_* = Ra E^2 / Pr$ [also known as the square of the temperature-based convective Rossby number (17)]. This representation is equivalent to the one in Fig. 3, with an equally satisfactory collapse of the dataset. The power-law fits reported in Table 1 translate into power laws $\mathcal{N} \approx Ra_*^\gamma$, where the exponent γ is within 12% of the theoretical prediction $3/2$ ($\gamma = 1.33 \pm 0.14$ and $\gamma = 1.63 \pm 0.07$, respectively, for $\ell/H = 0.024$ and $\ell/H = 0.048$).

These values contrast with the scaling exponent γ in the constant- E scaling law $Nu \approx Ra^\gamma$ reported in laboratory studies of rotating RB convection (see ref. 34 for a recent review). According to the literature, the RB exponent measured experimentally achieves a value close to $1/3$ in the slowly rotating

Table 1. Best-fit exponent β for laboratory and DNS data, to be compared to the theoretical prediction $3/5$ associated with the geostrophic turbulence scaling regime

β	$\mathcal{R} \leq 3 \times 10^{-7}$	$\mathcal{R} \leq 10^{-7}$
Experiments $\ell/H = 0.024$	0.59 ± 0.01	0.57 ± 0.03
Experiments $\ell/H = 0.048$	0.57 ± 0.01	0.62 ± 0.01
DNS $\ell/H = 0.048$	0.601 ± 0.002	0.601 ± 0.002

The error $\pm\sigma_\beta$ is estimated by propagating the error on $\log \mathcal{N}$ into an SD σ_β for the exponent.

regime, in line with the “classical theory” of nonrotating RB convection (26). For fast rotation and moderate supercriticality, laboratory experiments typically enter a transitional regime where the exponent γ increases sharply. An extension of the experimental data using direct numerical simulations (DNS) indicates that γ eventually reaches a value ranging between three and four (23), the lower value, three, being again associated with a “classical” regime controlled by marginally stable boundary layers (35), while the larger value, four, has been attributed to Ekman pumping (36) (see also ref. 37 for a theoretical demonstration of increasing heat transport exponents as a result of boundary layer pumping). By contrast, in the present experiment, radiative heating bypasses the boundary layers of standard rotating RB convection, thus circumventing the limitations of this traditional setup and providing experimental observations in excellent agreement with the geostrophic scaling regime of rapidly rotating turbulent convection.

As a side note, we stress the fact that the system operates far above the instability threshold. In the rapidly rotating limit, convection arises above a threshold value of the order of 15 for the reduced flux-based Rayleigh number $\text{Ra}_P E^{4/3}$. We report the values of $\text{Ra}_P E^{4/3}$ in *SI Appendix*: In the rapidly rotating regime, this parameter ranges between 1.5×10^3 and 2.5×10^4 , orders of magnitude above its threshold value. This large distance from threshold is confirmed by the large values of the Nusselt number in Fig. 2, which range between 10^2 and 10^3 . The collapse in Fig. 3 is thus not a mere consequence of near-onset behavior, a phenomenon reported in Cheng and Aurnou (38) for synthetic near-onset data. We illustrate this point further in Fig. 3, *Bottom*, where we plot $\mathcal{N}$ compensated by the geostrophic turbulence scaling law $\mathcal{R}^{3/5}$, in semilogarithmic coordinates. This rather stringent representation confirms 1) the good collapse of the data and 2) the existence of a plateau at low $\mathcal{R}$, in agreement with the geostrophic turbulence scaling law. By contrast, the near-onset data discussed by Cheng and Aurnou would not display such a collapse onto a plateau in compensated form, as illustrated in *SI Appendix*, Fig. S2. We further emphasize this point in *SI Appendix* by plotting the Nusselt number multiplied by $\sqrt{\text{Pr}}$ to collapse the various Pr data points, according to the geostrophic turbulence scaling—as a function of the reduced temperature-based Rayleigh number $\text{Ra} E^{4/3}$. The resulting *SI Appendix*, Fig. S3 makes it clear that the present data do not correspond to the near-onset behavior discussed by Cheng and Aurnou in the RB context: They are associated with greater supercriticality—the latter being better estimated by the even greater reduced flux-based Rayleigh number $\text{Ra}_P E^{4/3}$ in the present context—and a scaling exponent compatible with the $\gamma = 3/2$ geostrophic turbulence value (see *SI Appendix* for details).

It proves insightful to compare the present experimental results to existing numerical studies. DNS have been used as an extremely valuable tool both to address rotating convection inside full or partial spheres (39) and also to develop thought experiments in which one can alter the exact equations and/or boundary conditions to identify the mechanisms at play. This leads to idealized situations in which the geostrophic scaling regime emerges. Some studies have considered stress-free boundary conditions

instead of the no-slip boundaries of experimental tanks (40, 41), some have used tailored internal heat sources and sinks that conveniently vanish at the boundaries of the domain (42, 43), and some have focused on reduced sets of equations obtained through an asymptotic expansion of the rapidly rotating Boussinesq equations (15, 16, 44). DNS also offer an opportunity to eliminate the potential biases of laboratory experiments. One source of experimental bias is the centrifugal acceleration, which increases with global rotation rate and distance from the rotation axis. Horn and Aurnou (25) proposed the criterion $\Omega^2 H/g \lesssim 1$ for centrifugal effects to be negligible in standard rotating RB convection (see also refs. 45 and 46). The precise threshold value on the right-hand side of this inequality can probably be debated and requires further investigation; specifically, Cheng et al. (18) report experimental measurements unaffected by centrifugal effects even when $\Omega^2 H/g$ is as large as two. In *SI Appendix*, we provide the value of $\Omega^2 H/g$ for all the experimental data points: This ratio never exceeds two, with only three data points for which this ratio exceeds one (per value of ℓ/H). A second distinction between the idealized horizontally unbounded convective layer and the finite-size experimental tanks is the possible emergence of localized convective modes near the vertical walls of the latter (47–50). Wall modes have a lower onset than bulk modes and can dominate the dynamics near the instability threshold of the latter. However, they have also been shown to have a negligible impact on bulk heat transport in the turbulent regime (51). The collapse of the various data points in Fig. 3—which differ in terms of both centrifugal ratio $\Omega^2 H/g$ and aspect ratio—is a first indication that the present measurements are not impacted by the centrifugal acceleration nor the sidewalls.

With the goal of further validating the experimental results and the subdominance of centrifugal, sidewall, and non-Boussinesq effects, we have performed DNS of the present radiatively driven setup in the idealized horizontally periodic plane layer geometry. The combination of radiative heating and uniform internal cooling is implemented in a pseudospectral code that solves the rotating Boussinesq equations of thermal convection with a no-slip insulating bottom boundary and a stress-free insulating top one (see *Materials and Methods* for details). We provide a snapshot of the temperature field in statistically steady state in Fig. 1, for $\text{Ra}_P = 10^{12}$, $E = 2 \times 10^{-6}$, $\text{Pr} = 7$, and $\ell/H = 0.048$. This temperature field displays the typical vertically elongated structures that characterize rapidly rotating convection (28), with a predominance of thin warm plumes emanating from the heating region. The full numerical dataset consists in a sweep of the Ekman number E for $\text{Ra}_P = 10^{12}$, $\text{Pr} = 7$, and $\ell/H = 0.048$, the resulting data points being plotted in Fig. 3. The error bars on these data points, provided in *SI Appendix*, Table 3, are much smaller than the size of the symbols. The low- $\mathcal{R}$ numerical data again display a power-law behavior, with a best-fit exponent β within 0.5% of the theoretical exponent $3/5$ associated with the geostrophic turbulence scaling regime; see Table 1. The numerical data points lie very close to the experimental ones for the same value of ℓ/H , the reduced Nusselt number being slightly larger for the DNS data (by $\sim 20\%$), possibly as a consequence of the somewhat different geometries of the numerical and experimental setups. Overall, the quantitative agreement between experiments and DNS, together with the good collapse in Fig. 3 of data points obtained for various aspect ratios and centrifugal ratios, indicates that the aforementioned potential biases are subdominant in the present experiment. As far as the present heat transport measurements are concerned, the central region of the tank seems hardly affected by the centrifugal effects, by the sidewalls, by the slight curvature of the free surface, or by non-Boussinesq effects.

In some sense, our experiment follows a strategy similar to Barker et al. (42) while proposing a situation that can be realized in the laboratory. It thus comes as a surprise that the heat transport efficiency measured in the present experiment is significantly

greater than the one reported in the idealized numerical setups of Barker et al. (42), Stellmach et al. (40), and Julien et al. (16) in Cartesian geometry, and in Gastine et al. (39) in spherical geometry: The experimentally measured value of the prefactor $\mathcal{C}$ is approximately twice as large as the value extracted from Barker et al. (42), it is 6 times greater than the value reported in Julien et al. (16), and it is 3 times larger than the value reported in Gastine et al. (39) (the latter in spherical geometry). In terms of the prefactor appearing in the scaling law [2], this translates into an experimentally measured $\mathcal{C}_{\text{Ra}}$ that is approximately 6 times greater than the value extracted from Barker et al. (42), 60 times greater than the value reported in Julien et al. (16), and 20 times greater than the value reported in Gastine et al. (39). This points to an unexpected sensitivity of the heat transport efficiency of rapidly rotating turbulent convection to the precise spatial distribution of heat sources and sinks. We confirmed this conclusion experimentally by doubling the value of the absorption length ℓ/H , from $\ell/H = 0.024$ to $\ell/H = 0.048$: this change in the geometry of the heat source leads to an increase in the prefactor $\mathcal{C}$ by approximately 30%, and an approximate doubling of the prefactor $\mathcal{C}_{\text{Ra}}$. Beyond the observation of the geostrophic turbulence heat transport scaling law [1], our laboratory setup thus offers a unique experimental opportunity to determine the dependence of the prefactor on the distribution of heat sources and sinks, which greatly varies from planets to stars.

Materials and Methods

Radiative Heating and Effective Uniform Cooling. Within the framework of the Boussinesq approximation, and denoting the temperature and velocity fields as T and $\mathbf{u}$, respectively, the temperature equation for the radiatively heated fluid reads

$$\partial_t(\rho C T) + \mathbf{u} \cdot \nabla(\rho C T) = \rho C \kappa \nabla^2 T + \frac{P}{\ell} e^{-z/\ell}, \quad [3]$$

where the radiative heating term—the last term on the right-hand side—results from Beer–Lambert’s law. In this expression, z denotes the vertical coordinate measured upward from the bottom of the tank, and P is the total heat flux. The boundaries are thermally insulating: $\nabla T \cdot \mathbf{n} = 0$ at all boundaries, with $\mathbf{n}$ the unit vector normal to the boundary. Denoting as $\bar{T}(t)$ the spatial average of the temperature field inside the fluid domain, the spatial average of Eq. 3 yields

$$\frac{d\bar{T}(t)}{dt} = \frac{P}{\rho C H} (1 - e^{-H/\ell}). \quad [4]$$

The spatially averaged temperature increases linearly with time. Once the system reaches a quasi-stationary drifting state, the temperature everywhere inside the tank drifts at a mean rate given by the right-hand side of [4]. We can thus extract the power P from the drift of the time series.

Consider now the deviation from the spatial mean, $\theta(\mathbf{x}, t) = T(\mathbf{x}, t) - \bar{T}(t)$. We form the equation for θ by subtracting Eq. 4 from Eq. 3/ ρC ,

$$\partial_t \theta + \mathbf{u} \cdot \nabla \theta = \kappa \nabla^2 \theta + S(z), \quad [5]$$

where the source/sink term $S(z)$ is

$$S(z) = \frac{P}{\rho C} \left(\frac{1}{\ell} e^{-z/\ell} - \frac{1 - e^{-H/\ell}}{H} \right). \quad [6]$$

The second term inside the parentheses is an effective cooling term associated with the secular heating of the body of fluid. It balances the heating term, on average over the domain, but has a different spatial structure. Eq. 5 is coupled to the rotating Navier–Stokes equation,

$$\partial_t \mathbf{u} + (\mathbf{u} \cdot \nabla) \mathbf{u} + 2\Omega \mathbf{e}_z \times \mathbf{u} = -\nabla p + \alpha g \theta \mathbf{e}_z + \nu \nabla^2 \mathbf{u}, \quad [7]$$

where the generalized pressure term absorbs the contribution from the mean temperature $\bar{T}(t)$ and the centrifugal acceleration has been neglected.

The set of Eqs. 5–7 corresponds to the standard equations of rotating Boussinesq convection, with internal heating decreasing exponentially with height and uniform cooling at an equal and opposite rate. The solutions to this set of equations reach a statistically steady state, and the temperature difference $\Delta\theta$ realized by [5–7] is equal to the temperature difference ΔT of the initial setup.

Detailed Experimental Protocol. An experimental run consists of the following steps: The tank is filled with 7 °C water mixed with carbon-black dye to obtain a target value of ℓ . The tank is set into uniform rotation at a rate Ω . After an initial waiting period, for the fluid to achieve solid body rotation, the 2,500-W metal-halide spotlight is turned on. Two thermocouples horizontally centered inside the tank give access to the temperature at heights $z = 0$ and $z = 3H/4$. The corresponding temperature signals are measured by an Arduino microcontroller and transmitted through WIFI to a second Arduino microcontroller, which allows for live monitoring of the signals. An example of time series is provided in Fig. 4. After an initial transient phase, the system settles into a quasi-stationary state characterized by a linear drift of the two time series at an equal rate (visible for $t \gtrsim 1,500$ s in Fig. 4), together with a statistically steady temperature difference between the two probes. The fact that the two time series drift at a constant and equal rate is a first indication that thermal losses are negligible. We determine the input heat flux P from the drift rate of the two signals using relation [4]. The time average of the temperature difference between $z = 0$ and $z = 3H/4$ yields the temperature drop ΔT . This average is performed over the boxed time interval in Fig. 4. The dimensionless parameters are computed using the fluid properties evaluated for the mean bottom temperature over that interval. To quantify the error associated with the slow temporal drift of the various fluid properties (diffusivities, thermal expansion, etc.), we also compute the various quantities and dimensionless parameters using the first and second halves of the boxed region, denoted, respectively, as subregion I and subregion II in Fig. 4. For each of the two subregions, we average the temperature difference over the subinterval, and we compute the dimensionless parameters using the mean bottom temperature inside the subinterval. The corresponding values are reported in *SI Appendix* with a subscript I or II depending on the subinterval. Also reported are the initial and final bottom temperatures of the boxed measurement interval, denoted as T_{start} and T_{end} , respectively. The error bars in Figs. 2 and 3 correspond to the values obtained by restricting attention to a single subinterval. When estimating the best-fit exponent β , we first compute the rms error on $\log \mathcal{N}$ over the range of $\mathcal{R}$ of interest (of the order of 5%), before propagating this error into an SD σ_β for the best-fit exponent β .

DNS. We solve Eqs. 5–7 inside a horizontally periodic domain with the pseudospectral solver Coral (52), previously used for nonrotating convective flows (31) and validated against both analytical results (53) and solutions computed with the Dedalus software (54). The bottom boundary is insulating and no slip, while the top boundary is insulating and stress-free. Depending on the Ekman number, the horizontal extent $L_\perp$ of the domain is set to $0.4H$ or $0.5H$, to account for the variation in the characteristic horizontal scale of the rotating flow. The equations are discretized on a grid containing $(N_x, N_y, N_z) = (441, 441, 576)$ points, which corresponds to 296 alias-free Fourier modes in the horizontal directions and 384 Chebyshev

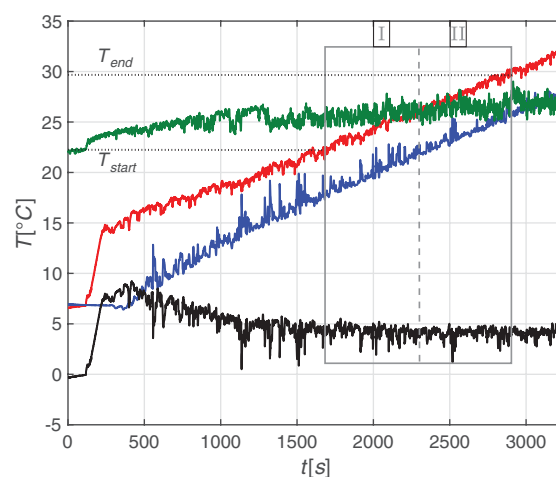


Fig. 4. Raw signals from thermocouples T_1 (red, $z = 0$) and T_2 (blue, $z = 3H/4$) as a function of time t for $H = 25$ cm, $\Omega = 30$ rpm, and $\ell/H = 0.048$. Also shown are the instantaneous temperature drop between the two probes (black), and room temperature (green). The solid box indicates the total measurement interval, separated by a dashed line into two subintervals, I and II.

polynomials along the vertical. The initial condition is chosen as either small-amplitude noise or a checkpoint from a previous simulation with smaller supercriticality. We restrict attention to the statistically steady state that arises after the initial transient. We denote as τ_{meas} the duration of integration in this statistically steady state, and we focus on the difference between the horizontally averaged temperatures at $z = 0$ (bottom boundary) and $z = 3H/4$. The time average of the resulting signal yields the temperature drop from which $\mathcal{N}$ is inferred. The SD σ of the signal and its correlation time τ_{corr} (time lag of the first zero of the autocovariance function) allow us to estimate the statistical error on $\mathcal{N}$. Following, for example, ref. 18, we compute the number of “effectively independent realizations” $N_{\text{eff}} = \tau_{\text{meas}}/\tau_{\text{corr}}$ before estimating the statistical error $\sigma_{\mathcal{N}}$ on the mean temperature drop as

$\sigma/\sqrt{N_{\text{eff}}}$. The resulting error bars are provided in *SI Appendix*, together with the values of $\mathcal{N}$ obtained by averaging over only the first or second half of the signal, denoted as $\mathcal{N}_I$ and $\mathcal{N}_{II}$, respectively.

Data Availability. All study data are included in the article and *SI Appendix*.

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