

1 Performance evaluations and applications of a  $\delta^{13}\text{C}$ -DIC analyzer in seawater and estuarine  
2 waters

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19 **Abstract:**

20 Dissolved inorganic carbon (DIC) and its stable isotope ( $\delta^{13}\text{C}$ -DIC) are important  
21 parameters for studying carbon cycling in aquatic environments. Traditional methods  
22 based on isotope-ratio mass spectrometers are labor-intensive and not easily deployable at  
23 field sites. Here we report the performance of a method that simultaneously measures DIC  
24 concentration and its stable isotope by using a  $\text{CO}_2$  extraction device and a Cavity Ring-  
25 Down Spectroscopy (CRDS) detector. A multi-port valve is used to increase sample  
26 throughput and improve precision. The instrument achieves average precisions of better  
27 than  $\pm 1.95 \mu\text{mol kg}^{-1}$  and  $\pm 0.06\text{\textperthousand}$ , respectively, for DIC and  $\delta^{13}\text{C}$ -DIC in seawater based  
28 on three injections for each sample. We also provide recommendations on how to precisely  
29 determine  $\delta^{13}\text{C}$ -DIC samples with a wide range of DIC content in different types of waters  
30 by examining injection volume and concentration effects. This technique was applied to  
31 study carbon cycling in the Delaware Estuary. It demonstrates that a combined  
32 determination of both DIC and  $\delta^{13}\text{C}$ -DIC is a powerful tool for constraining the processes  
33 controlling aquatic carbon cycling and  $\text{CO}_2$  fluxes. Both laboratory tests and field  
34 applications confirmed that this system can be used with high precision to study carbon  
35 cycling in various aquatic environments.

36 **Keywords:** Dissolved inorganic carbon; Stable carbon isotope  $\delta^{13}\text{C}$ -DIC; Cavity Ring-  
37 Down Spectroscopy; Continuous measurement; Delaware Estuary  
38 **Running head:** Laboratory and field assessments of a  $\delta^{13}\text{C}$ -DIC analyzer

39     **Synopsis:** This analyzer provides a precise, rapid, and onsite analysis of inorganic carbon  
40     concentration and its stable isotope ( $\delta^{13}\text{C}$ -DIC) in aquatic environments.

41     **Highlights**

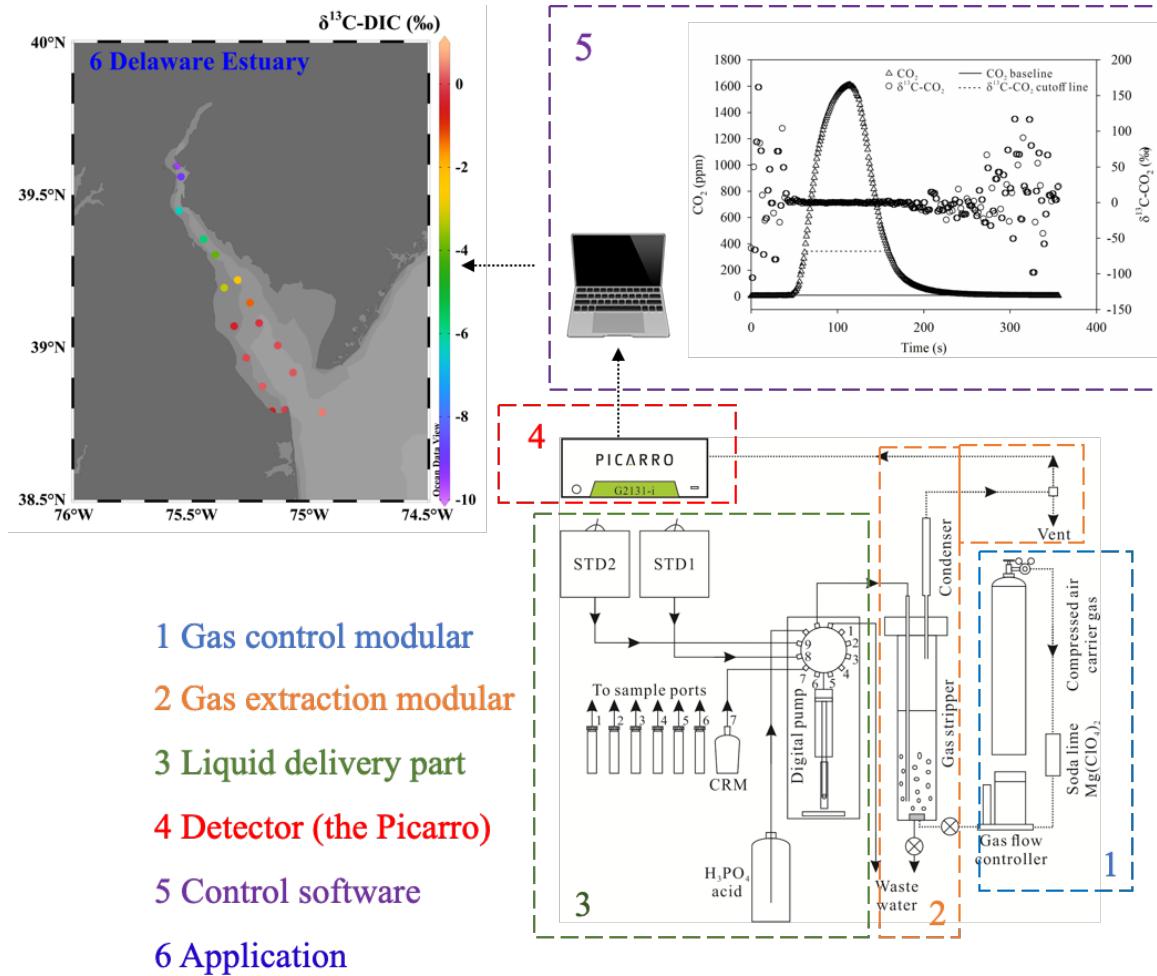
42     •     Instrument and technique to simultaneously and precisely measure DIC concentration  
43     and  $\delta^{13}\text{C}$ -DIC

44     •     Instrument is portable and can be deployed at field sites and onboard ships

45     •     Recommendations on how to precisely determine  $\delta^{13}\text{C}$ -DIC samples with different  
46     DIC contents

47     •     The system will enhance spatiotemporal near real-time analysis of DIC and  $\delta^{13}\text{C}$ -DIC

48 **Graphic Abstract**



51     **1 Introduction**

52         Dissolved inorganic carbon (DIC) is the primary carbon pool in natural waters and its  
53         quantification is essential for studying the global carbon cycle. The stable isotope of DIC  
54         ( $\delta^{13}\text{C}$ -DIC) is a powerful tool for determining the sources and sinks of DIC and in  
55         understanding carbon cycling and the associated biogeochemical processes in aquatic  
56         ecosystems<sup>1–8</sup>. In particular, the  $\delta^{13}\text{C}$ -DIC can be used to elucidate whether the source of  
57         DIC is allochthonous or autochthonous and can be used to separate the relative  
58         contributions among different pools of organic matter degradation, biological production,  
59         and physical processes that control DIC dynamics in the ocean and coastal waters<sup>1,3,9,10</sup>. In  
60         addition, the  $\delta^{13}\text{C}$ -DIC is a useful tracer in determining anthropogenic  $\text{CO}_2$  uptake rate by  
61         the ocean and can be used to identify whether an ocean region is a sink for anthropogenic  
62          $\text{CO}_2$ <sup>11,12</sup>.

63         In most oceanographic and hydrogeological studies, the  $\delta^{13}\text{C}$ -DIC is measured by gas  
64         source isotope-ratio mass spectrometry (IRMS). The high precision and accuracy have  
65         made IRMS the preferred conventional technique for determining  $\delta^{13}\text{C}$ -DIC over the last  
66         several decades<sup>13–17</sup>. However, the disadvantages of the IRMS-based conventional  
67         technique (e.g., the high level of required expertise for sample pretreatment and analysis,  
68         the complexity of equipment set-up, the expensive instrument maintenance, the inability to  
69         deploy in the field) limit the ability to conduct  $\delta^{13}\text{C}$ -DIC studies with high temporal and  
70         spatial resolutions<sup>18,19</sup>. In open ocean transect cruises, water samples were collected,

71 preserved and usually transported back to land-based laboratories for  $\delta^{13}\text{C}$ -DIC analysis by  
72 the IRMS technique. Thus, compared to the direct DIC concentration analysis onboard for  
73 every sampling station and depth, only <15% of samples have corresponding  $\delta^{13}\text{C}$ -DIC  
74 analysis<sup>20</sup>. Therefore, lower spatial and temporal  $\delta^{13}\text{C}$ -DIC coverages limit the full benefits  
75 of the  $\delta^{13}\text{C}$ -DIC as a more sensitive tracer than DIC for the study of anthropogenic  $\text{CO}_2$   
76 uptake and biogeochemical processes<sup>11,12</sup>. Finally, a lack of the flexibility of making  
77 immediate decisions on issues such as adding additional sampling stations and times based  
78 on feedbacks from onsite analysis is another obvious disadvantage of the use of the  
79 traditional IRMS method.

80 In recent years, extensive efforts have been made to overcome the limitations of the  
81 IRMS-based conventional technique, especially automation of sample preparation and  
82 deployability to conduct near-real-time  $\delta^{13}\text{C}$ -DIC analysis. Among these, the laser-based  
83 optical spectroscopy has gained increasing recognition and is a suitable alternative  
84 approach to simultaneously measure DIC concentrations and  $\delta^{13}\text{C}$ -DIC values because of  
85 its high detection sensitivity, relatively straightforward experimental set-up, and field-  
86 portability<sup>6,21–25</sup>. For example, Bass et al.<sup>21</sup> utilized a continuous, automated DIC analyzer  
87 to monitor DIC concentrations and its  $\delta^{13}\text{C}$ -DIC signals in water samples. However, their  
88 method required large sample volumes (350 mL) and their precision of  $\pm 10 \mu\text{mol kg}^{-1}$  for  
89 DIC and  $\pm 0.2\%$  for  $\delta^{13}\text{C}$ -DIC is inadequate for studying DIC processes with small  
90 variations or slow rates. Call et al.<sup>22</sup> coupled a commercially available non-dispersive

91 infrared (NDIR)  $\text{CO}_2$  detector based DIC analyzer to a Cavity Ring-Down Spectroscopy  
92 (CRDS) isotope analyzer to determine DIC concentrations and  $\delta^{13}\text{C}$ -DIC values,  
93 respectively, with high precisions of  $\pm 1.5\text{--}2.0 \mu\text{mol kg}^{-1}$  for DIC and  $\pm 0.14\text{\textperthousand}$  for the  
94  $\delta^{13}\text{C}$ -DIC, when DIC concentrations ranged from 1000 to 3600  $\mu\text{mol kg}^{-1}$ . In the approach,  
95 the NDIR detector was used to measure DIC with one injection of the sample while the  
96 CRDS detector was used to measure  $\delta^{13}\text{C}$ -DIC with different injection, and the two  
97 injections had different analytical conditions (i.e., the gas flow rate was 300  $\text{mL min}^{-1}$  in  
98 the former and 70  $\text{mL min}^{-1}$  in the latter). The fact that this approach requires two detectors  
99 and two different analytical procedures for DIC and  $\delta^{13}\text{C}$ -DIC probably has limited its  
100 application.

101 As an improvement, Su et al.<sup>6</sup> used one CRDS detector and a single procedure to  
102 simultaneously quantify both DIC and  $\delta^{13}\text{C}$ -DIC. In this approach, 3–4 mL samples were  
103 acidified to transfer DIC to  $\text{CO}_2$  and then both DIC concentration and its carbon isotope  
104 ratio were determined by the Picarro G2131-i CRDS analyzer to achieve precisions of  $\pm$   
105  $1.5 \mu\text{mol kg}^{-1}$  for DIC and  $\pm 0.09\text{\textperthousand}$  for  $\delta^{13}\text{C}$ -DIC. However, in both Call et al.<sup>22</sup> and Su et  
106 al.<sup>6</sup> methods, once a sample analysis is completed, an operator needs to manually load  
107 another sample, which is still labor-intensive and limits the sample throughput rate. The  
108 approaches may also limit the analytical precision due to less consistency between analyses  
109 (e.g., time interval between samples varies). Therefore, though initial results were

110 published in Su et al.<sup>6</sup>, further automation, improvements, and extensive evaluations of the  
111 performance of the analytical techniques and system are highly needed.

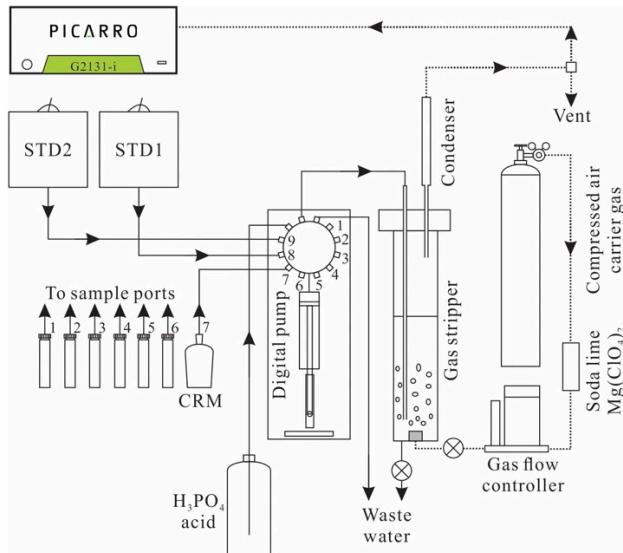
112 In the present study, we improved the instrument's sampling procedure from a single  
113 sample valve in Su et al.<sup>6</sup> to a multi-port valve to achieve automated multi-sample analysis  
114 with less labor-intensive monitoring and operation. The use of the multi-port valve is also  
115 expected to provide a better consistency among different samples and thus to improve the  
116 overall analytical precision. We have carried out both extensive laboratory tests and field  
117 sample analysis to evaluate the performance of the upgraded method and system. First, we  
118 examined the repeatability of the multi-port valve to ensure that all sample channels are  
119 identical in sample delivery and work consistently. Because we drew samples from the  
120 same stock of seawater, this experiment provided a rigorous evaluation of the analytical  
121 precision and the analytical system stability. Furthermore, the sample injection volume and  
122 DIC concentration experiments were conducted to determine the injection volume range  
123 for  $\delta^{13}\text{C}$ -DIC samples with different DIC concentrations in different types of aquatic  
124 environments. Finally, we demonstrated the applicability and advantages of this new  
125 CRDS-based method via a comprehensive field study of the carbonate system in the  
126 Delaware Estuary.

127 **2 Materials and Methods**

128 **2.1 Instrument structure and principle**

129 A whole-water CO<sub>2</sub> extraction device with a 12-port sample valve (AS-D1, Apollo  
130 Scitech, Newark, DE, USA; [www.apolloscitech.com](http://www.apolloscitech.com)) and a CRDS isotopic detector  
131 (G2131-i, Picarro, Santa Clara, CA, USA [www.picarro.com](http://www.picarro.com)), were coupled and automated  
132 with a single software to simultaneously measure DIC concentrations and  $\delta^{13}\text{C}$ -DIC signals  
133 via quantifying the CO<sub>2</sub> extracted from acidified samples (Fig. 1). The principle of a  
134 previous version of this system was described in Su et al.<sup>6</sup> and the AS-D1 device specifics  
135 and procedures of sample analysis have been introduced in Cheng et al.<sup>26</sup>. Briefly, an  
136 aliquot of sample is acidified with 5% H<sub>3</sub>PO<sub>4</sub> in the gas stripping reactor and the liberated  
137 CO<sub>2</sub> is brought by the carrier gas (CO<sub>2</sub>-free compressed air) to the CRDS analyzer, where  
138 DIC concentration and  $\delta^{13}\text{C}$ -DIC signal are determined simultaneously. The CO<sub>2</sub> stripper  
139 is composed of a porous bubbler, which is fixed at the bottom of the reactor. The carrier  
140 gas bubbles through the sample from the bottom to the top, and carries the liberated CO<sub>2</sub>  
141 through a condenser, which condenses the water vapor and minimizes the water vapor  
142 correction of the Picarro detector. The outlet pressure of the carrier gas is set to 15 psi, and  
143 a gas flow controller is used to precisely control the carrier gas flow rate at 60 mL min<sup>-1</sup>,  
144 which is higher than the input flow rate of the Picarro analyzer (~ 30 mL min<sup>-1</sup>), to ensure  
145 that all the measured CO<sub>2</sub> is CO<sub>2</sub> stripped out from the sample. Thus, about half of the gas  
146 stream is released to the room and no pressure is built up at the Picarro inlet side.

147 We improved the method described by Su et al.<sup>6</sup> by including a 12-port sample valve:  
148 one port for acid, another for the injection of sample and acid into the reactor, and a third  
149 port for waste, then nine other ports can be used for sample and standard analysis (Fig. 1).  
150 One of the sample ports is designated for the DIC standard, such as using a Certified  
151 Reference Material (CRM) or another secondary house standard to create a working  
152 standard curve for DIC calibration. We also prepared two home-made isotope standards.  
153 STD1 (-2.70‰) and STD2 (-19.57‰) were made by dissolving NaHCO<sub>3</sub> solids in  
154 deionized water, and along with CRM are used to calibrate the δ<sup>13</sup>C-DIC data. The δ<sup>13</sup>C-  
155 DIC values of the home-made isotope standards and CRM solution were verified by the  
156 IRMS technique in the stable isotope facility, University of California, Davis. In an  
157 environment with narrow ranges of DIC concentration and δ<sup>13</sup>C-DIC such as that in  
158 seawater (1800—2300 μmol kg<sup>-1</sup> in DIC and -3 to 2‰ in δ<sup>13</sup>C-DIC), a single pre-calibrated  
159 standard may be enough to serve as both concentration and isotope standard. However, in  
160 other environments such as in an estuary, two or even three standards for δ<sup>13</sup>C-DIC may  
161 be desirable.



162

163 **Fig. 1** A schematic layout of the  $\text{CO}_2$  extraction device (AS-D1) and CRDS isotope  
 164 detector (G2131-i) to measure DIC concentrations and  $\delta^{13}\text{C}$ -DIC signals autonomously and  
 165 simultaneously. A 5-mL syringe is used in this work (note that the syringe volume can be  
 166 changed to 10 mL for need). For the 12 ports valve, one connects to the acid, one delivers  
 167 the syringe's liquid to the gas stripper, one discharges to waste, the ports of #1 to #6 are  
 168 connected to the sample lines and the rest of three ports (#7, #8 and #9) are connected to  
 169 three standards (CRM, STD1 and STD2), respectively. Port #7 can be run in one single  
 170 volume or three different volumes of CRM standard for DIC calibration.

171 As described in Su et al.<sup>6</sup>, the area under the curve of the mole fraction  $\text{CO}_2$  gas was  
 172 integrated over time to derive a net area for quantifying DIC concentrations (also included  
 173 in the upper right corner in the graphic abstract). In this work, three volumes of a CRM or  
 174 a home-made standard, e.g., 3.0, 3.5 and 4.0 mL, are used to create a working standard

175 curve between the net area and DIC mole amounts. The latter is calculated as the product  
176 of the CRM or home-made standard's volume and known concentration. The DIC  
177 concentration of a sample is then derived from the working standard curve and the known  
178 injection sample volume.

179 The  $\delta^{13}\text{C}$ -DIC is derived as the  $\text{CO}_2$  weighted mean of  $\delta^{13}\text{C}$ - $\text{CO}_2$  data. Similar to the  
180 practice in Su et al.<sup>6</sup> and Call et al.<sup>22</sup>, we set a cutoff value to exclude  $\delta^{13}\text{C}$ - $\text{CO}_2$  at low  $\text{CO}_2$   
181 concentrations. This is because the Picarro instrument internally determines  $\delta^{13}\text{C}$ - $\text{CO}_2$  by  
182 referencing the  $^{13}\text{C}$  signal to  $^{12}\text{C}$  signal, and thus, at a very low  $^{12}\text{C}$  signal, the  $\delta^{13}\text{C}$ - $\text{CO}_2$   
183 signal has high noise and should not be used. A  $\text{CO}_2$  range of 380–2000 ppm (or 1000–  
184 2000 ppm) is recommended by the manufacturer for a guaranteed isotope analysis  
185 precision of 0.1‰ (or 0.05‰) for the Picarro G2131-i. Noted that the cutoff value can be  
186 defined by users, for example, 350 ppm was set as the cutoff value in this study. As we  
187 adopted a weighted-mean method in our study, the final  $\delta^{13}\text{C}$ -DIC value is not particularly  
188 sensitive to the chosen cutoff value, because the noisy  $\delta^{13}\text{C}$ - $\text{CO}_2$  data at low  $\text{CO}_2$  only  
189 accounts for a small fraction of the entire dataset.

190 **2.2 Preparation of the stock seawater**

191 The stock seawater used in all laboratory experiments was collected from the Gulf of  
192 Mexico (GoM) and had been stored in a large tank designed for research supply in the  
193 Louisiana Universities Marine Consortium (LUMCON). The seawater was filtered through  
194 0.45  $\mu\text{m}$  cartridge filter and then transferred into a 4 L gastight bag (Cali-5-Bond,

195 Calibrated Instruments Inc.) and doped with 1 mL HgCl<sub>2</sub> to inhibit further biological  
196 activities, which is a standard operation protocol for preserving DIC samples<sup>27</sup>. Before  
197 preservation, biological respiration likely had increased DIC and decreased δ<sup>13</sup>C-DIC of  
198 this stock water compared to initial values from the GoM surface waters (0.5–1.0‰; Cai's  
199 laboratory unpublished data).

200 **2.3 Multi-port valve test, injection volume effect and concentration effect**  
201 **experiments**

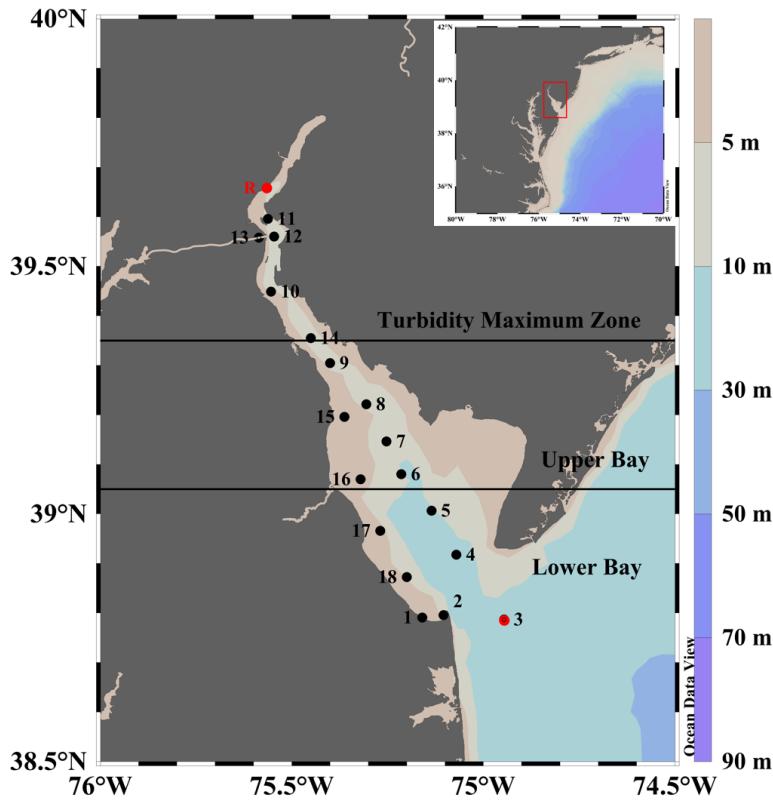
202 There is the possibility for cross-contamination caused by sample carryover between  
203 subsequent ports when using a multiport valve. Therefore, we assessed if the new multi-  
204 port system delivers identical DIC concentrations and δ<sup>13</sup>C-DIC values between ports. All  
205 sample and standard ports in the injection volume of 3.5 mL were connected to the same  
206 batch of stock seawater (preparation details in section 2.2) with three consecutive injections  
207 per port to assess the multi-port valve injection consistency.

208 Different aquatic samples from seawater to estuarine, river and lake waters may post  
209 different challenges in sample volumes and concentration ranges. To determine if different  
210 injection volumes with the same DIC concentration or different DIC concentrations with  
211 the same injection volume could affect the measurements of DIC concentrations and δ<sup>13</sup>C-  
212 DIC signals using the CRDS system, we conducted the following experiments. For the  
213 injection volume effect experiment, the stock seawater in the same bag was measured in  
214 different injection volumes in a sequence from 1.2–5.8 mL at 0.2 mL increment. For the

215 concentration effect experiment, stock seawater was diluted with CO<sub>2</sub>-free deionized water  
216 to make a series of solutions with 7 different DIC nominal concentrations, ranging from  
217 250 to 2300  $\mu\text{mol kg}^{-1}$ , then samples were run in the same injection volume (3.5 mL),  
218 simulating waters with a wide range of DIC concentration from natural environments.

219 **2.4 Field work in the Delaware Estuary**

220 We evaluated the analytical method and demonstrated its applicability in the Delaware  
221 Estuary, which is composed of 100 km long tidal Delaware River and Delaware Bay<sup>28</sup> and  
222 has a DIC range of  $\sim$ 1000  $\mu\text{mol kg}^{-1}$  at the river end and  $\sim$ 2000  $\mu\text{mol kg}^{-1}$  at the ocean end.  
223 A one-day cruise in the Delaware Estuary was conducted on April 3, 2019 (Fig. 2). The  
224  $\delta^{13}\text{C}$ -DIC and ancillary parameters of surface water were collected along the longitudinal  
225 axis in the main channel and the western shoal of the Delaware Estuary to demonstrate the  
226 applicability of our DIC and  $\delta^{13}\text{C}$ -DIC analysis method.



227

228 **Fig. 2** Sampling stations in the Delaware Estuary. The red filled dots represent the river  
 229 endmember (station R) and ocean endmember (station 3). Delaware Estuary is divided into  
 230 3 parts (turbidity maximum zone, upper bay and lower bay) by the solid horizontal lines  
 231 based on Sharp et al.<sup>29</sup>. The inserted regional map represents the location of the Delaware  
 232 Bay on the US east coast.

233 The DIC and  $\delta^{13}\text{C}$ -DIC samples were determined by the AS-D1  $\delta^{13}\text{C}$ -DIC analyzer as  
 234 described above. TA samples were measured by Gran titration with AS-ALK2 (Apollo  
 235 Scitech) with precision of 0.1%<sup>30</sup>, and pH with a Ross combination electrode calibrated  
 236 against three NBS buffers at  $25 \pm 0.1^\circ\text{C}$  with a precision of  $\pm 0.005$  pH. The partial pressure  
 237 of  $\text{CO}_2$  ( $p\text{CO}_2$ ) was monitored by an underway  $p\text{CO}_2$  analyzer (AS-P2, Apollo Scitech)

238 installed in the shipboard laboratory and calibrated against three standard gases<sup>31</sup>.  $\text{Ca}^{2+}$   
239 samples were measured using a modified technique of Kanamori and Ikegami<sup>32</sup> with a  
240 precision <0.1%. Aragonite saturation state ( $\Omega_{\text{Ar}}$ ) was derived by using the measured  $\text{Ca}^{2+}$ ,  
241 calculated  $\text{CO}_3^{2-}$  and aragonite solubility, according to Mucci<sup>33</sup>.

242 **2.5 Two endmember mixing calculation**

243 The DIC concentrations and  $\delta^{13}\text{C}$ -DIC signatures in the Delaware Estuary vary due to  
244 several processes including mixing, gas exchange, carbonate precipitation/dissolution and  
245 biological processes. Thus, a two-endmember mixing model is used to separate physical  
246 mixing effect from other processes. The mixing fractions between two endmembers, river  
247 water and seawater, for each sample can be quantified using salinity as a conservative  
248 tracer<sup>34,35</sup>:

$$249 \quad f_r + f_{sw} = 1 \quad (1)$$

$$250 \quad S_r \times f_r + S_{sw} \times f_{sw} = S_{meas} \quad (2)$$

$$251 \quad \text{TA}_{mix} = \text{TA}_r \times f_r + \text{TA}_{sw} \times f_{sw} \quad (3)$$

$$252 \quad \text{DIC}_{mix} = \text{DIC}_r \times f_r + \text{DIC}_{sw} \times f_{sw} \quad (4)$$

$$253 \quad \text{DIC}_{mix} \times \delta^{13}\text{C}-\text{DIC}_{mix} = \delta^{13}\text{C}-\text{DIC}_r \times \text{DIC}_r \times f_r + \delta^{13}\text{C}-\text{DIC}_{sw} \times \text{DIC}_{sw} \times f_{sw} \quad (5)$$

254 where  $f$  is mixing fraction; the subscripts  $r$ ,  $sw$ ,  $mix$  and  $meas$  represent the river end-  
255 member, seawater end-member, conservative mixing value and the measured value of  
256 sample. Equations (3)–(5) are used to calculate the conservative TA, DIC and  $\delta^{13}\text{C}$ -DIC  
257 mixing lines in the two-endmember mixing model. The conservative pH mixing line (at

258 25°C) is calculated from the conservative DIC and TA with the CO2SYS program<sup>36</sup>. The  
259 station R (Fig. 2) in the Delaware River was chosen as the river endmember, since it has  
260 near-zero salinity, is minimally affected by tidal movement in spring, and is easily  
261 accessible from a pier; Station 3 is located outside the bay mouth and connected with the  
262 Atlantic Ocean, thus, is selected as the ocean end-member (Table 1).

263 **Table 1.** Summary information of the end-member stations in the two end-member model.

Endmembers	Latitude	Longitude	Salinity	DIC ( $\mu\text{mol kg}^{-1}$ )	TA ( $\mu\text{mol kg}^{-1}$ )	$\delta^{13}\text{C-DIC}$ (‰)
Riverine	39.5800°N	75.5869°W	0.16	970.6 ± 0.6	944.6 ± 0.0	-9.06 ± 0.07
Oceanic	38.7868°N	74.9459°W	30.54	1975.0 ± 0.6	2150.5 ± 1.9	0.37 ± 0.08

264 **3 Results and Discussion**

265 **3.1 Analytical precision and repeatability of the multi-port valve**

266 For the same seawater measurements in the nine ports, we obtained a total of 81 raw  
267 data in three rounds with three consecutive injections per port. Based on all 81 raw data  
268 without any drift correction, the precisions of DIC concentrations and  $\delta^{13}\text{C-DIC}$  values  
269 were  $1.95 \mu\text{mol kg}^{-1}$  and 0.06‰ (Fig. 3). These precisions may be viewed as the upper  
270 boundary of the method uncertainties, which are slightly better than or similar to the overall  
271 analytical precisions of DIC measurements from the traditional NDIR method (0.1%)<sup>30</sup> and  
272  $\delta^{13}\text{C-DIC}$  from the single-port version of this system (0.09‰)<sup>6</sup>. These results indicate that  
273 the DIC concentrations and  $\delta^{13}\text{C-DIC}$  values from all ports are not significantly different

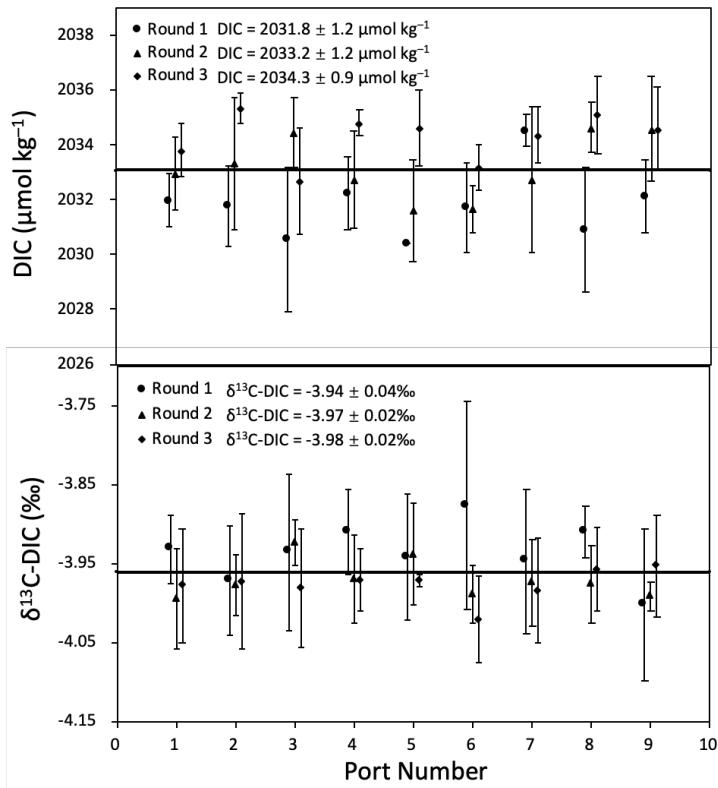
274 from each other, which is also verified by the statistics analysis (ANOVA test, DIC:  $p =$   
275 0.99,  $n = 81$ ;  $\delta^{13}\text{C}$ -DIC:  $p = 0.35$ ,  $n = 81$ ). However, if we first averaged the three  
276 consecutive injections on each port and then applied statistical analysis to each round (that  
277 is,  $n = 9$  for each round), the deviations were much reduced. The standard deviations of  
278 DIC and  $\delta^{13}\text{C}$ -DIC between multi-port valves were 0.9—1.2  $\mu\text{mol kg}^{-1}$  and 0.02—0.04‰,  
279 respectively (Table 2 and Fig. 3). Since during our analysis of standards and samples, we  
280 made three injections and then use the average of the three injections as the raw data for  
281 each standard or sample, the statistical analysis based on the 3-injection averaged data may  
282 reflect the true instrument performance better than those based on the individual 81 raw  
283 data. We argue that the average of 3-injection based statistics at least point to the potential  
284 precision and possibly accuracy this method can achieve if a suitable standardization  
285 method can be accomplished in the future. Since the ultimate performance of the  
286 instrument is also limited by the calibration and standards, for now, we are content with  
287 reporting the precision and accuracy as better than 1.95  $\mu\text{mol kg}^{-1}$  for DIC and 0.06‰ for  
288  $\delta^{13}\text{C}$ -DIC. Therefore, we conclude that our instrument setup and technique have achieved  
289 the goal of better than  $\pm 0.05\text{‰}$  for  $\delta^{13}\text{C}$ -DIC precision recommended by Global Ocean  
290 Observing System<sup>37</sup> and have the possibility to be a convenient tool to measure the  $\delta^{13}\text{C}$ -  
291 DIC samples both onboard and in the laboratory. However, as noted here, a suitable and  
292 long-term consistent standardization method is still to be evaluated. Currently, all our  $\delta^{13}\text{C}$ -

293 DIC values are based on  $\text{NaHCO}_3$  standards analyzed by the U.C. Davis Stable Isotope  
 294 Facility.

295 Table 2 The raw data of DIC and  $\delta^{13}\text{C}$ -DIC in the multi-port valve test.

Port	$\delta^{13}\text{C}$ -DIC (‰)			DIC ( $\mu\text{mol kg}^{-1}$ )		
	Round 1	Round 2	Round 3	Round 1	Round 2	Round 3
C	-3.93	-4.00	-3.98	2032.0	2033.0	2033.8
D	-3.97	-3.98	-3.97	2031.8	2033.3	2035.3
E	-3.94	-3.92	-3.98	2030.6	2034.4	2032.7
F	-3.91	-3.97	-3.97	2032.3	2032.7	2034.8
G	-3.94	-3.94	-3.97	2030.4	2031.6	2034.6
H	-3.88	-3.99	-4.02	2031.7	2031.7	2033.2
I	-3.95	-3.97	-3.98	2034.5	2032.7	2034.4
J	-3.91	-3.98	-3.96	2030.9	2034.7	2035.1
K	-4.00	-3.99	-3.95	2032.1	2034.6	2034.6
<i>Average</i>	<i>-3.94</i>	<i>-3.97</i>	<i>-3.98</i>	<i>2031.8</i>	<i>2033.2</i>	<i>2034.3</i>
<i>STD</i>	<i>0.04</i>	<i>0.02</i>	<i>0.02</i>	<i>1.2</i>	<i>1.2</i>	<i>0.9</i>
<i>Average</i> <i>(all 3 rounds)</i>		<i>-3.97</i>			<i>2033.1</i>	
<i>STD</i> <i>(all 3 rounds)</i>		<i>0.02</i>			<i>1.5</i>	

296



297 **Fig. 3** Measured DIC concentrations (upper panel) and  $\delta^{13}\text{C-DIC}$  values (lower panel) of  
 298 the stock seawater using the upgraded multi-port valve. The solid lines in the two panels  
 299 represent the averaged DIC concentration and  $\delta^{13}\text{C-DIC}$  value from CRDS. Three rounds  
 300 with three consecutive injections per port for nine ports were measured. The error bar is  
 301 the standard deviations of the three consecutive injections at each port. This analytical  
 302 procedure of three rounds lasted a total of about 20 hours.

303 This system is compact, both lab- and field-deployable, and analyzes DIC and  $\delta^{13}\text{C-}$   
 304 DIC values without any sample pretreatment. In contrast, for offline IRMS  $\delta^{13}\text{C-DIC}$   
 305 analysis, samples need to be acidified to liberate  $\text{CO}_2$ , which then goes through a vacuum  
 306 line to be purified and concentrated into small vials before IRMS analysis<sup>14</sup>. However, our

307 method and system only need an operator to replace the samples once the previous batch  
308 analysis is completed. This automation avoids labor-intensive monitoring and operation,  
309 which allows for continuous measurements around the clock. Moreover, because  
310 instrument drift is low (DIC only drifted 0.059% and  $\delta^{13}\text{C}$ -DIC drifted 0.047‰ within 3  
311 weeks), the 3 standards are run only once a day or once every two days, after which all the  
312 time is dedicated to samples analysis in all nine sample channels. Note that, the standards  
313 and samples are run in a sequence each with three injections and a complete run average  
314 about 6 h. This results in a theoretical maximum throughput capacity of 37 samples with  
315 three injections (or 3 replicate measurements) each day (e.g., total 126 runs = (5 standards  
316 + 37 samples)  $\times$  3, and each run needs about 11 minutes).

317 However, our system normally analyzed less samples during routine sample analysis  
318 due to instrument down time over night and due to the intention of evaluating the system  
319 performance via analyzing multiple standards during the method development and  
320 evaluation stage. For example, during our recent analysis of 1200 samples from the  
321 California Current System (samples were taken during June—July and analysis was  
322 conducted during August—early November, 2021), 24 samples and two standards were  
323 analyzed each day with three shifts starting at ~8 am, ~3 pm and ~9 pm, respectively.  
324 During the overnight shift, the standards and some samples were analyzed twice. In  
325 addition to the home laboratory analysis, about 800 samples had been analyzed at sea  
326 onboard the research vessel Ron Brown during a 40-days cruise by two operators (on 12-

327 hour shifts). Compared with the analytical efficiency and application limitation of the  
328 IRMS instrument, our system greatly improves the spatial resolution of the  $\delta^{13}\text{C}$ -DIC  
329 samples.

330 One potential issue that could affect the sample repeatability is the sample temperature.  
331 Although the Picarro G2131-i detector has a built-in temperature control mode to ensure  
332 the detector operates under stable thermal conditions to minimize the temperature effect on  
333  $\text{CO}_2$  and isotope detection, environmental temperature variations will still influence the  
334 density of the water sample and result in the uncertainty of carbon content in a fixed  
335 injection sample volume. In our study, all measurements were conducted in a temperature-  
336 controlled room ( $T = 22 \pm 1^\circ\text{C}$ ), where the  $1^\circ\text{C}$  temperature fluctuation will only cause a  
337 density change of 0.03% and an uncertainty of  $\pm 0.5 \mu\text{mol kg}^{-1}$  in DIC concentration. It is  
338 smaller than the acceptable DIC precision of  $2\text{--}4 \mu\text{mol kg}^{-1}$ , thus this temperature effect  
339 can be ignored. However, a water bath may be used onboard a ship or at a field laboratory  
340 to keep the sample temperature more stable.

341 **3.2 Injection volume effect and concentration effect experiments**

342 For the CRDS detector, the signals of  $\text{CO}_2$  and  $^{13}\text{CO}_2$  are determined by the carbon  
343 content liberated from water sample, rather than solely by the DIC concentration or  
344 injection volume. A smaller injection volume with a fixed DIC concentration or a lower  
345 DIC concentration with a fixed injection volume would result in a smaller integrated net  
346 area and a lower  $\text{CO}_2$  peak and less distributed points of  $^{13}\text{CO}_2$  above the cutoff value,

347 thereby potentially reducing the precision of  $\delta^{13}\text{C}$ -DIC. For example, with a fixed DIC  
348 concentration, the uncertainty of  $\delta^{13}\text{C}$ -DIC will increase as the injection volume decreases,  
349 which is known as injection volume effect. With a fixed injection volume,  $\delta^{13}\text{C}$ -DIC  
350 uncertainty is less than  $\pm 0.2\text{\textperthousand}$  when DIC concentration is above  $360 \mu\text{mol kg}^{-1}$ , whereas  
351 it rapidly increases to  $>0.5\text{\textperthousand}$  when DIC concentration is  $<130 \mu\text{mol kg}^{-1}$  in the study by  
352 Bass et al.<sup>21</sup>, which is known as the concentration effect. The same is true in our analysis.  
353 As an extreme case in our analysis, if the entire  $\text{CO}_2$  curve is less than the cutoff  $\text{CO}_2$  value,  
354 there will be no valid  $\delta^{13}\text{C}$ -DIC. If there is only a small fraction of the  $\text{CO}_2$  curve near the  
355 peak above the cutoff line, then, one would expect a higher uncertainty in the derived  $\delta^{13}\text{C}$ -  
356 DIC.

357 To examine the potential volume effect on the performance of the analyzer, we  
358 analyzed the same seawater with 24 different sample volumes (again each volume had three  
359 consecutive injections). The pooled averaged DIC concentration was  $2355.8 \pm 2.8 \mu\text{mol}$   
360  $\text{kg}^{-1}$  as determined by reference to CRM #185 (Fig. 4b), which is close to the value (2353.1  
361  $\pm 0.4 \mu\text{mol kg}^{-1}$ ) measured by the traditional NDIR method<sup>30</sup>. Except for a few points near  
362 the low injection volume, all the DIC data fall within the precision range of  $\pm 0.2\text{\textperthousand}$ , which  
363 is only slightly higher than that of the traditional NDIR method<sup>30</sup>. The averaged  $\delta^{13}\text{C}$ -DIC  
364 was  $-5.56 \pm 0.06\text{\textperthousand}$  (Fig. 4a), again with high precision same as that in the multi-port  
365 evaluation. To be specific, 77.8% of the  $\delta^{13}\text{C}$ -DIC data located in the averaged  $\pm 1\sigma$  ranges  
366 if following our system precision (0.06%) while 91.7% of  $\delta^{13}\text{C}$ -DIC data fall in the

367 averaged  $\pm 1\sigma$  ranges according to the precision (0.09%) of Su et al.<sup>6</sup>. We suggests that our  
368 measurement system is still stable even if the injection volume varies greatly. As  
369 mentioned above, the CO<sub>2</sub> and <sup>13</sup>CO<sub>2</sub> signal are measured based on the carbon content of  
370 a sample. In the injection volume and concentration effect experiments, DIC and its  $\delta^{13}\text{C}$ -  
371 DIC data are basically stable in a wide range of injection volume, which could be attributed  
372 to the fact that the stock seawater used in this experiment represents the typical open ocean  
373 water and has a high carbon content (DIC = 2355.8  $\mu\text{mol kg}^{-1}$ ). However, if estuarine water  
374 (such as DIC =  $\sim$ 1000  $\mu\text{mol kg}^{-1}$  or less) is used for this experiment, the stability of  $\delta^{13}\text{C}$ -  
375 DIC will be poor due to its low carbon content and few data points above the cutoff line.  
376 Therefore, the injection volume has a significant influence on the estuarine and riverine  
377 water with low DIC concentrations and a large injection volume will be needed to analyze  
378  $\delta^{13}\text{C}$ -DIC with high precision and accuracy.

379 For the concentration effect experiment, the  $\delta^{13}\text{C}$ -DIC value exhibited a decreasing  
380 trend with a decreased DIC concentration, and the  $\delta^{13}\text{C}$ -DIC became slightly depleted  
381 when DIC concentration decreased to 247  $\mu\text{mol kg}^{-1}$  (Fig. 4c). The standard deviation of  
382 all  $\delta^{13}\text{C}$ -DIC values was 0.20‰, which is not negligible given that the measurement  
383 precision of our measurement system is better than 0.06‰. However, besides the lowest  
384 concentration of 247  $\mu\text{mol kg}^{-1}$ , the isotope precision variation was small and better than  
385 0.10‰ when DIC concentration ranged from 536 to 2283  $\mu\text{mol kg}^{-1}$  (Fig. 4d), which is  
386 similar to the precision of Su et al.<sup>6</sup> and also closer to our system precision. The lower  $\delta^{13}\text{C}$ -

387 DIC in lower DIC concentration could likely be attributed to the invasion of atmospheric  
388 CO<sub>2</sub> with lighter isotope during the pre-treatment process of the stock seawater dilution,  
389 which thus has a significant concentration effect on lower DIC concentration samples,  
390 compared with higher DIC concentration samples as Call et al.<sup>22</sup> suggested before.

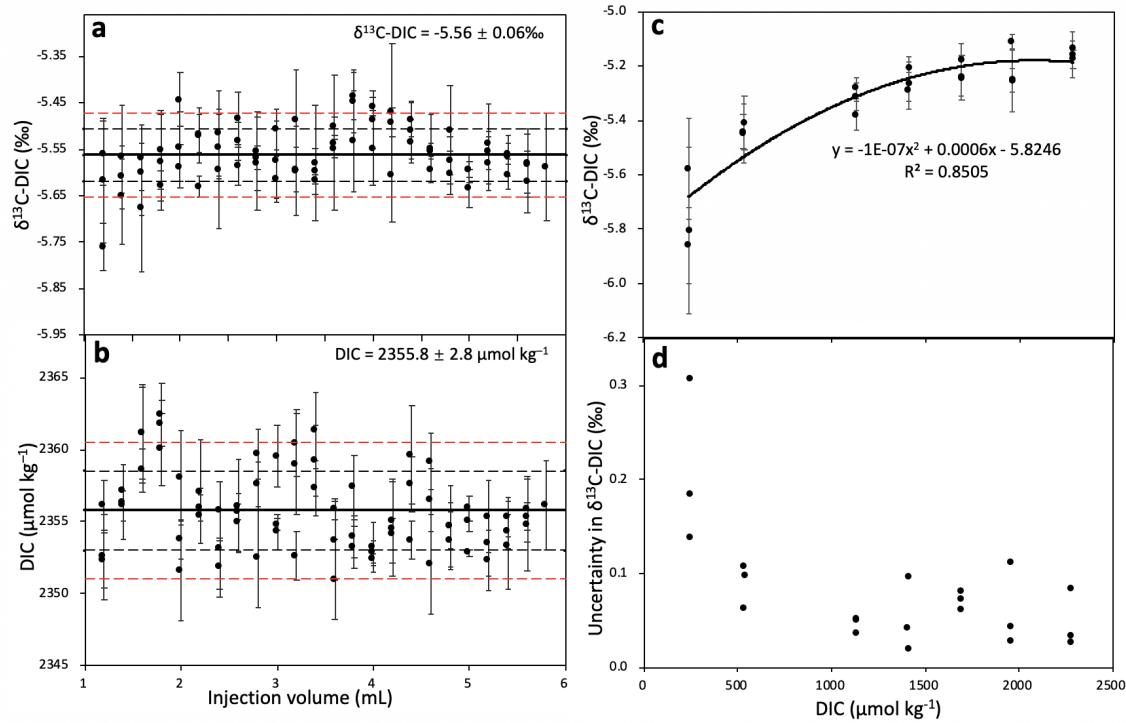
391 Similarly, an obviously negative correlation between  $\delta^{13}\text{C}$ -DIC values and DIC  
392 concentrations in the concentration effect for  $\delta^{13}\text{C}$ -DIC experiment in Cheng et al.<sup>26</sup> also  
393 verified the invasion of atmospheric CO<sub>2</sub> in the preparation of a set of NaHCO<sub>3</sub> standard  
394 solution, since atmospheric CO<sub>2</sub> has a heavier isotope compared with -21.04‰ NaHCO<sub>3</sub><sup>26</sup>.

395 Here we offer an alternative explanation. As the carbon amount becomes lower either  
396 because of low sample volume or low DIC concentration, the weight of  $\delta^{13}\text{CO}_2$  with higher  
397 instrument noise at lower  $^{12}\text{CO}_2$  concentration (near 350 ppm) becomes more significant.

398 We have noticed that such noise at low CO<sub>2</sub> level of a Picarro instrument is not necessarily  
399 random and may be instrument specific (for the two G2131-i units in our laboratory, one  
400 goes to more positive and another goes to more negative). Thus, we recommend  
401 maximizing the sample volume when DIC concentration of the sample is low.

402 While not fully and purposely evaluated, results from the volume and concentration  
403 experiments also indicate that there is no visible isotope fractionation effect in our  
404 instrument and method. Since we have selected a fixed criteria for ending sample analysis  
405 (when baseline after the peak is < 5 ppm CO<sub>2</sub> above the baseline before the peak) and the  
406 cutoff CO<sub>2</sub> reading for averaging the  $\delta^{13}\text{CO}_2$  value is fixed at 350 ppm (though both are

407 user definable), the higher the DIC amount in the sample (either larger volume or higher  
 408 concentration or both), the less  $\delta^{13}\text{CO}_2$  signal is lost in counting towards the final  $\delta^{13}\text{C}$ -  
 409 DIC value. The fact that no statistically significant difference is observed beyond  $\pm 0.06\text{\textperthousand}$   
 410 when seawater sample volume is  $> 2 \text{ mL}$  (when DIC about  $2000 \text{ }\mu\text{mol kg}^{-1}$ ) suggests that  
 411 no significant isotope fractionation occurs in our method. It also appears that the same  
 412 conclusion can be drawn for estuarine and freshwater analysis when the DIC concentration  
 413 is above  $500 \text{ }\mu\text{mol kg}^{-1}$  (injection volume is  $3.5 \text{ mL}$ ) and a slightly larger uncertainty of  $\pm$   
 414  $0.1\text{\textperthousand}$  uncertainty is permitted. For analysis of freshwater samples with lower DIC, we  
 415 recommend using a larger sample injection volume of  $5.0 \text{ mL}$  or greater.



416  
 417 **Fig. 4**  $\delta^{13}\text{C-DIC}$  values and its precision (a) as well as measured DIC concentrations (b) of  
 418 the aged seawater in the injection volume effect experiment; concentration effect on  $\delta^{13}\text{C}$ -

419 DIC values (c) and  $\delta^{13}\text{C}$ -DIC uncertainty vs. DIC concentration (d) in the concentration  
420 effect experiment. In Fig (a) and (b), the black solid-lines indicate the averaged values of  
421  $\delta^{13}\text{C}$ -DIC values and DIC concentrations; For all data, the black dashed-lines represent 1  
422  $\sigma$  standard deviation interval; the red dashed-lines indicate 0.09‰ range for  $\delta^{13}\text{C}$ -DIC and  
423 2  $\sigma$  standard deviation interval for DIC. In Fig (c), the black curve represents the  
424 relationship between the  $\delta^{13}\text{C}$ -DIC values and DIC concentrations. Note that these two  
425 experiments were two separate sets that ran on different days and were merged here  
426 together. Each injection volume and concentration have three repeat samples, and error bar  
427 means the standard deviations of the three injections for each sample. Specifically, the  
428 injection volume effect experiment lasted about 64 hours and the concentration effect  
429 experiment lasted about 35 hours, the instrument always ran well during the intervals of  
430 these days (7 days).

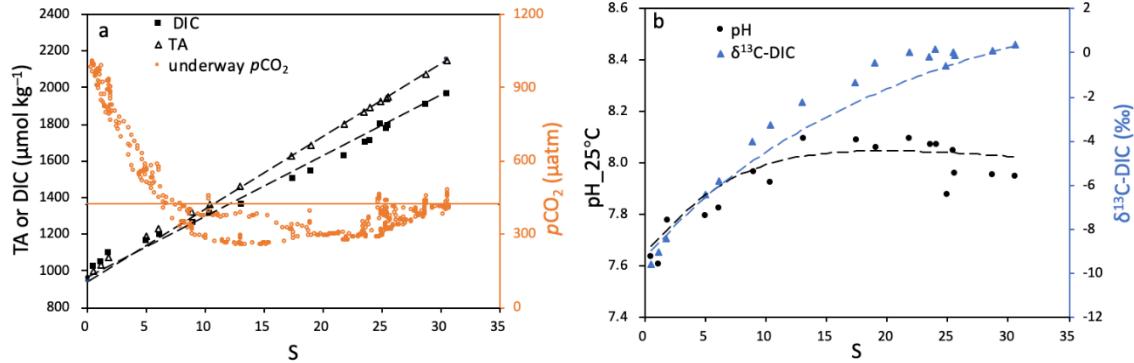
431 **3.3 Carbonate system in the Delaware Estuary**

432 Compared with other systems like the Chesapeake Bay, the physical circulation and  
433 hydrology in the Delaware Estuary are relatively simple, because the major inflow is a  
434 single river and water is generally vertically well-mixed<sup>38</sup>. Thus, the Delaware Estuary is  
435 an ideal site for method development and evaluation, and has served this purpose well as a  
436 backyard laboratory for researchers at the University of Delaware for decades<sup>28,29,38-41</sup>.

437 The measured DIC and TA, pH<sub>25°C</sub> and δ<sup>13</sup>C-DIC increased while underway *p*CO<sub>2</sub>  
438 decreased with the increasing salinity from the upper tidal river to the low bay (Fig. 5).  
439 Specifically, from the river end to the ocean end, DIC increased from 970.6 to 1975.0 μmol  
440 kg<sup>-1</sup>, TA increased from 944.6 to 2150.5 μmol kg<sup>-1</sup>, and δ<sup>13</sup>C-DIC increased from -9.57 to  
441 0.37‰. DIC and TA had slightly higher values than the conservative mixing lines in the  
442 turbidity maximum zone. However, DIC concentrations were slightly lower than the  
443 conservative mixing line and TA values followed the conservative mixing line in the mid-  
444 salinity upper bay (Fig. 5a).

445 The δ<sup>13</sup>C-DIC values along the salinity gradient were depleted in the freshwater areas,  
446 while enriched in the mid-salinity zone of the estuary (Fig. 5b). The pH<sub>25°C</sub> and  
447 underway *p*CO<sub>2</sub> values were in the ranged from 7.61–8.10 and 1010–258 μatm,  
448 respectively, with marked salinity gradient changing from 0.16 to 30.54 (Figs. 5b and 5a).  
449 To be specific, pH increased from 7.61 in the Delaware River up to 8.10 in the upper bay,  
450 then decreased slightly to 7.95 in the marine part of the estuary. Compared to the  
451 atmospheric level (422 μatm), *p*CO<sub>2</sub> was obviously supersaturated (>500 μatm) in the  
452 turbidity maximum zone and then decreased to undersaturated in the mid and low bay.  
453 Consistent with pH distribution, *p*CO<sub>2</sub> value was lowest in the mid-salinity upper bay and  
454 slightly increased to near the atmospheric CO<sub>2</sub> level in the lower bay (Fig. 5a). Overall, the  
455 Delaware Estuary is characterized as a strong CO<sub>2</sub> source to the atmosphere in the river

456 end and at the turbidity maximum zone and a weak CO<sub>2</sub> sink in the mid and lower bays  
457 during springtime. This observation is consistent with the investigation of Joesoef et al.<sup>40</sup>.



458

459 **Fig. 5** Distributions of DIC and TA concentrations and underway  $p\text{CO}_2$  (a),  $\text{pH}_{25^\circ\text{C}}$  and  
460  $\delta^{13}\text{C-DIC}$  (b) against salinity. In Fig. 5a, the black dashed lines are the DIC and TA  
461 conservative mixing lines, the orange horizontal line represents the atmospheric  $p\text{CO}_2$  level;  
462 In Fig. 5b, the black and blue dashed curves are the pH and  $\delta^{13}\text{C-DIC}$  conservative mixing  
463 lines, respectively. The DIC, TA,  $\text{pH}_{25^\circ\text{C}}$  and  $\delta^{13}\text{C-DIC}$  conservative mixing lines are  
464 specified in section 2.5.

465 While it is clear that physical mixing plays the most important role in the Delaware  
466 Estuary, the deviations of carbonate parameters from the conservative mixing lines (Fig. 5)  
467 indicate that processes other than physical mixing also play an important role in regulating  
468 their distributions in the estuary. While DIC distribution and dynamics have been studied  
469 by Joesoef et al.<sup>39</sup>,  $\delta^{13}\text{C-DIC}$  has not been studied and could add an important constraint to  
470 identifying biogeochemical mechanisms important in controlling the carbon cycling and  
471 air-sea CO<sub>2</sub> flux. Therefore, in order to discuss the influencing mechanism of other

472 processes on the DIC and its isotope distributions in the Delaware Estuary, the deviations  
473 of DIC concentrations and  $\delta^{13}\text{C}$ -DIC signals from the above conservative mixing lines are  
474 used here for discussion, since the processes affecting DIC will have distinct  $\delta^{13}\text{C}$ -DIC  
475 source values and isotope fractionation. Following the method described in Alling et al.<sup>1</sup>,  
476 the deviations of DIC concentrations and  $\delta^{13}\text{C}$ -DIC signals from their conservative mixing  
477 lines (Equations 4 and 5) can be calculated by the equations:

478 
$$\Delta\text{DIC} = \frac{\text{DIC}_{\text{meas}} - \text{DIC}_{\text{mix}}}{\text{DIC}_{\text{mix}}} \quad (6)$$

479 
$$\Delta\delta^{13}\text{C-DIC} = \delta^{13}\text{C-DIC}_{\text{meas}} - \delta^{13}\text{C-DIC}_{\text{mix}} \quad (7)$$

480 Where  $\text{DIC}_{\text{mix}}$  and  $\delta^{13}\text{C-DIC}_{\text{mix}}$  are given in Equation 4 and 5, respectively. The main  
481 biogeochemical mechanisms affecting the distributions of  $\delta^{13}\text{C-DIC}$  and DIC could be  
482 inferred by the slopes of the relationship between  $\Delta\delta^{13}\text{C-DIC}$  and  $\Delta\text{DIC}$  (Fig. 6).

483 Stations near the Delaware River fall within quadrant IV, which is characterized by  
484 the strong DIC addition and  $\delta^{13}\text{C-DIC}$  depletion. It represents the influence of terrestrial  
485 organic matter degradation and is confirmed by the oversaturated  $p\text{CO}_2$  relative to  
486 atmospheric  $\text{CO}_2$  (Fig. 5a) and relatively low pH (Fig. 5b)<sup>42-44</sup>. Meanwhile, low aragonite  
487 saturation state ( $\Omega_{\text{arag.}} < 0.37$ , Fig. 7) near the freshwater area indicates that  $\text{CaCO}_3$   
488 dissolution might also occur, which added to both DIC and TA, and in the meantime,  
489 enriched the  $\delta^{13}\text{C-DIC}$  value by releasing the  $^{13}\text{C}$ -enriched carbonate and bicarbonate ions  
490 into the water column DIC pool<sup>3</sup>. Therefore, the points in quadrant IV slightly deviate from  
491 the theoretical vector of terrestrial organic matter decomposition from the river source and

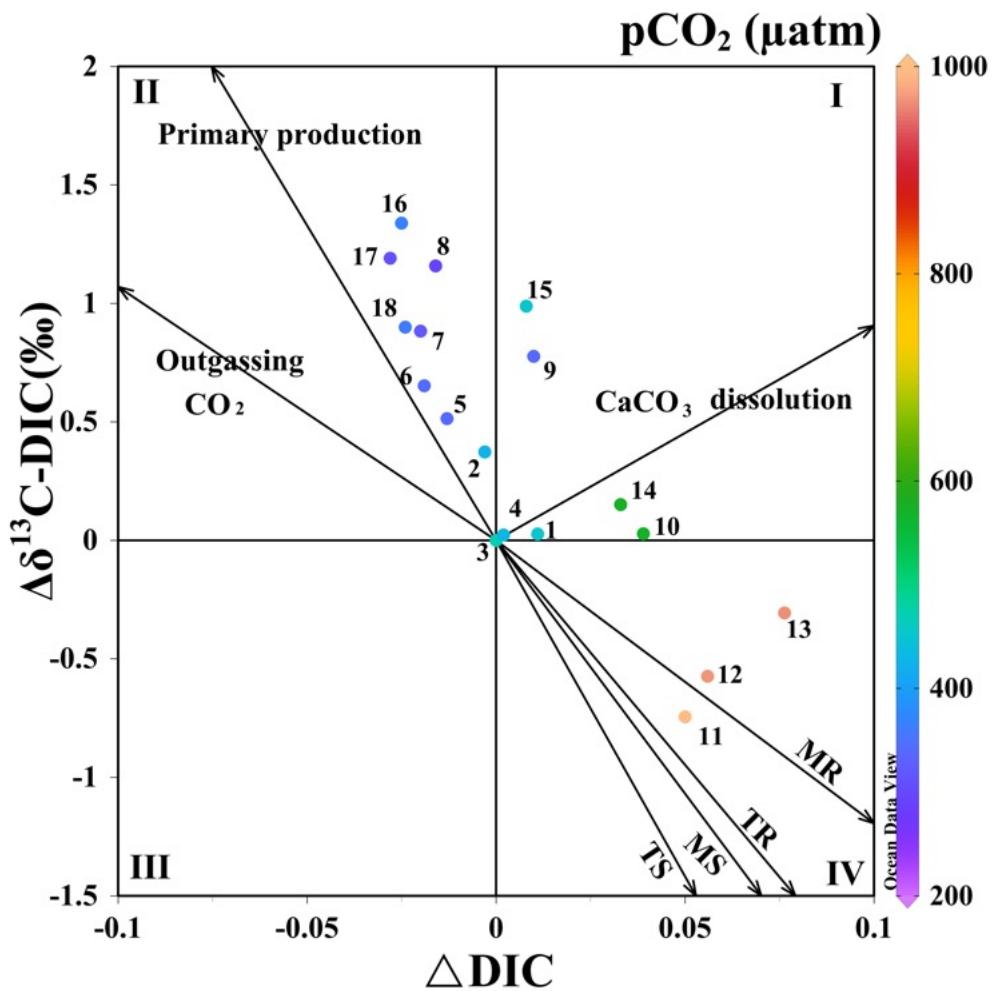
492 shifted upward to the direction of the vector of  $\text{CaCO}_3$  dissolution. Note that while the  
493 stoichiometric ratio of  $\Delta\text{TA}$  to  $\Delta\text{DIC}$  should be 2:1 during  $\text{CaCO}_3$  dissolution, if the  
494 dissolution is driven by metabolically produced  $\text{CO}_2$  input, then the ratio would be nearly  
495 or less than 1:1 (i.e., metabolic carbonate dissolution,  $\text{CaCO}_3 + \text{CH}_2\text{O} + \text{O}_2 + \text{H}_2\text{O} \rightarrow \text{Ca}^{2+}$   
496  $+ 2\text{HCO}_3^-$ )<sup>45</sup>, which occurs in the freshwater member with  $S < 3$  (Fig. 7).

497 The turbidity maximum zone stations are in the lower portion of quadrant I, mainly  
498 affected by  $\text{CaCO}_3$  dissolution of suspended particulate matter and organic matter  
499 degradation. Additional evidence supporting the  $\text{CaCO}_3$  dissolution mechanism is the  
500 substantial additions of DIC and TA in the low salinity region (Fig. 7). The excess TA  
501 ( $\Delta\text{TA} = \text{TA}_{\text{meas}} - \text{TA}_{\text{mixing}}$ ) in and near the turbidity maximum zone ( $5 < S < 10$ ) may mainly  
502 come from the  $\text{CaCO}_3$  dissolution. Here the  $\Delta\text{TA}$  to  $\Delta\text{DIC}$  ratio ranges 1.3-1.7 and is much  
503 higher than those at or near the river endmember ( $S < 2$ ) (Fig. 7). Therefore, the variations  
504 of DIC and  $\delta^{13}\text{C}$ -DIC in the turbidity maximum zone were mainly controlled by the  
505 combined effects of organic carbon degradation from rivers and  $\text{CaCO}_3$  dissolution.

506 Almost all stations in the Delaware Bay, including the upper bay and the lower bay,  
507 are in quadrant II. The Delaware Estuary has an inverted funnel shape, and the upper bay  
508 is below the neck of funnel, where the bay becomes wider, water flow slows down, clarity  
509 improves and biological production increases<sup>28,39,40</sup>. In addition, small scale spring blooms  
510 with high primary production usually occur in the Delaware Bay in March and April,  
511 especially in the upper bay<sup>46</sup>. The high primary production, associated with DIC uptake,

512 preferentially removes lighter  $^{12}\text{C}$  and enriches the water with the heavier stable carbon  
513 isotope<sup>47</sup>. Considering high biomass and primary productivity lead to undersaturated or  
514 nearly equilibrated  $p\text{CO}_2$  relative to the atmospheric  $\text{CO}_2$ , there should be no impact from  
515  $\text{CO}_2$  outgassing. In addition, Stations 15 and 9 in the upper portion of the upper bay fall in  
516 the upper portion of quadrant I, which is dominated by the combined factors of primary  
517 production and  $\text{CaCO}_3$  dissolution ( $\Omega_{\text{arag}} = 0.6$  and 1.0, Fig. 7). Therefore, DIC loss and  
518 elevated  $\delta^{13}\text{C}$ -DIC in the upper Delaware Bay are mainly attributed to primary production  
519 and  $\text{CaCO}_3$  dissolution.

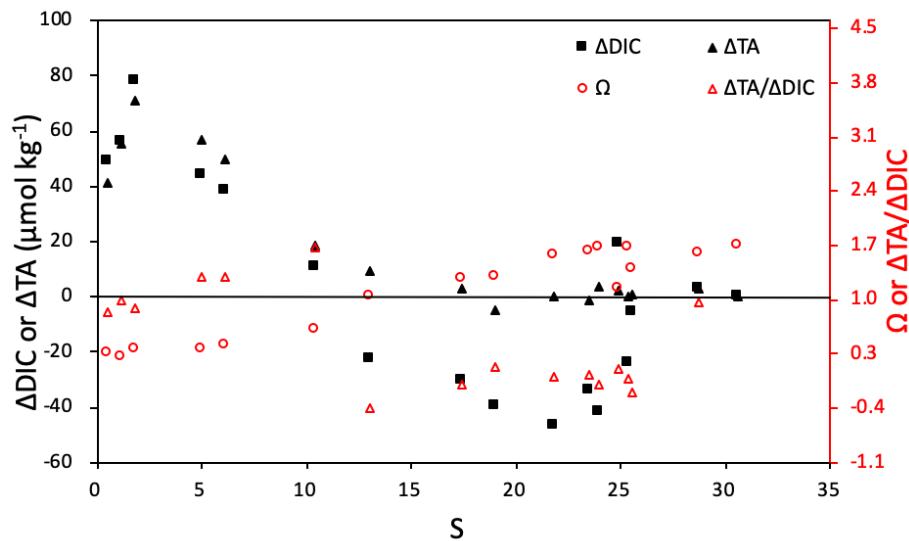
520 Although our calculations are associated with some uncertainties and limitations, the  
521 approach used in this study certainly provides a new insight into the sources and cycling  
522 of DIC in the Delaware Estuary and serves as a good example of using DIC concentrations  
523 and  $\delta^{13}\text{C}$ -DIC values to study biogeochemical processes in aquatic systems. The deviations  
524 of DIC and  $\delta^{13}\text{C}$ -DIC from conservative mixing lines can be regarded as fingerprints left  
525 by different biogeochemical processes. Overall, the variations of the carbonate system are  
526 primarily controlled by the physical mixing in the Delaware Estuary. Besides that, the  
527 control mechanisms in the Delaware River and turbidity maximum zone are the combined  
528 effects of the degradation of organic carbon and carbonate dissolution, but are dominated  
529 by primary production in the Delaware Bay. The relative importance of these processes  
530 changes over seasons, which will be the subject of a subsequent publication.



531

532 **Fig. 6** The absolute changes of  $\delta^{13}\text{C}$ -DIC ( $\Delta\delta^{13}\text{C}$ -DIC) and the relative changes of DIC  
 533 concentration ( $\Delta\text{DIC}$ ) relative to the conservative mixing lines in the Delaware Estuary in  
 534 April 2019. The origin represents the data only controlled by physical mixing. The figure  
 535 is divided into four quadrants, each indicating the position of samples whose DIC  
 536 concentration and  $\delta^{13}\text{C}$ -DIC were influenced by additional processes (non-physical mixing  
 537 process). Quadrant I represents carbonate dissolution when both DIC and  $\delta^{13}\text{C}$ -DIC  
 538 increase; quadrant II represents primary production or CO<sub>2</sub> outgassing when DIC decreases  
 539 while  $\delta^{13}\text{C}$ -DIC increases; quadrant III represents calcite precipitation when both DIC and

540  $\delta^{13}\text{C}$ -DIC decrease; quadrant IV represents degradation of organic carbon when DIC  
 541 increases but  $\delta^{13}\text{C}$ -DIC decreases. The vectors indicate the effects of most likely processes  
 542 affecting DIC. Four vectors in quadrant IV indicate four possible effects of organic matter  
 543 degradation, which depend on the sources of organic carbon (T: terrestrial source; M:  
 544 marine source) and the initial DIC and  $\delta^{13}\text{C}$ -DIC composition in the water (S: seawater; R:  
 545 river water). MR (or TR) stands for  $\text{CO}_2$  addition from the decomposition of marine (or  
 546 terrestrial) organic matter to river water and MS (or TS) stands for  $\text{CO}_2$  addition from the  
 547 decomposition of marine (or terrestrial) organic matter to seawater. Arabic numerals in the  
 548 figure represent the sampling stations. The calculations of all vectors are based on Samanta  
 549 et al.<sup>3</sup>.



550  
 551 **Fig. 7** The TA and DIC differences between measured and conservative mixing values  
 552 ( $\Delta\text{TA}$  and  $\Delta\text{DIC}$ , left axis), aragonite saturation ( $\Omega$ , right axis) and the ratio of  $\Delta\text{TA}$  and  
 553  $\Delta\text{DIC}$  ( $\Delta\text{TA}/\Delta\text{DIC}$ , right axis) against salinity. The black dashed horizontal line represents

554 both the 0-reference line of  $\Delta$ TA or  $\Delta$ DIC, and the 1.0 aragonite saturation line. Data (solid  
555 square and triangle symbol) above the line mean addition, while beneath the line indicate  
556 removal of DIC or TA. Also, data (open circle symbol) above the line indicate calcium  
557 carbonate precipitation but dissolution below the line.

558 **4 Conclusion**

559 Here we extensively evaluated the performance of a method where we coupled a CO<sub>2</sub>  
560 extraction device with a multi-port sample valve and a CRDS detector to simultaneously  
561 analyze DIC concentrations and  $\delta^{13}\text{C}$ -DIC values with high precision (better than  $\pm 1.95$   
562  $\mu\text{mol kg}^{-1}$  for DIC concentration and better than  $\pm 0.06\text{\textperthousand}$  for  $\delta^{13}\text{C}$ -DIC). The highlight of  
563 this instrument configuration is an upgraded multi-sample valve compared to a single-  
564 sample valve used in Su et al.<sup>6</sup>. The instrument setup can potentially analyze about 37  
565 samples per day with three replicate measurements and achieve continuous measurements  
566 around the clock, which is convenient and labor-saving during analysis. Moreover, the  
567 instrument can be used in a land-based laboratory, at sea or at a field station. For the coastal  
568 and open ocean waters with high DIC concentration, the choice of injection volume has  
569 little impact on the  $\delta^{13}\text{C}$ -DIC sample determination. However, we recommend using a large  
570 injection volume for samples with low DIC concentration to minimize the influence of low  
571 injection volume on the  $\delta^{13}\text{C}$ -DIC precision.

572        This technique was applied in the Delaware Estuary in Spring of 2019 to determine  
573        the spatial distributions of DIC concentration and  $\delta^{13}\text{C}$ -DIC and to understand the  
574        controlling mechanisms. The relationship between  $\Delta\text{DIC}$  and  $\Delta\delta^{13}\text{C}$ -DIC demonstrated  
575        that, in addition to estuarine mixing, they were primarily controlled by the degradation of  
576        organic carbon and carbonate dissolution in the Delaware River and turbidity maximum  
577        zone, but mainly by primary production in the Delaware Bay. This application provides a  
578        new insight for distinguishing the control mechanisms on DIC and  $\delta^{13}\text{C}$ -DIC in the  
579        Delaware Estuary. The application of this measuring system could rapidly expand the  
580        temporal and spatial coverages of the paired DIC concentration and  $\delta^{13}\text{C}$ -DIC in the  
581        fieldwork, thereby facilitating further the understanding of the underlying biogeochemical  
582        processes and controls on air-sea  $\text{CO}_2$  flux and acidification in different aquatic  
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