



The Universal Program of Nonlinear Hyperelasticity

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Dedicated to Professor Roger L. Fosdick on the occasion of his 85th birthday

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Abstract

For a given class of materials, universal deformations are those that can be maintained in the absence of body forces by applying only boundary tractions. Universal deformations play a crucial role in nonlinear elasticity. To date, their classification has been accomplished for homogeneous isotropic solids following Ericksen's seminal work, and homogeneous anisotropic solids and inhomogeneous isotropic solids in our recent works. In this paper we study universal deformations for inhomogeneous anisotropic solids defined as materials whose energy function depends on position. We consider both compressible and incompressible transversely isotropic, orthotropic, and monoclinic solids. We show that the *universality constraints*—the constraints that are dictated by the equilibrium equations and the arbitrariness of the energy function—for inhomogeneous anisotropic solids include those of inhomogeneous isotropic and homogeneous anisotropic solids. For compressible solids, universal deformations are homogeneous and the material preferred directions are uniform. For each of the three classes of anisotropic solids we find the corresponding *universal inhomogeneities*—those inhomogeneities that are consistent with the universality constraints. For incompressible anisotropic solids we find the universal inhomogeneities for each of the six known families of universal deformations. This work provides a systematic approach to study analytically functionally-graded fiber-reinforced elastic solids.

Keywords Universal deformations · Nonlinear elasticity · Anisotropic elasticity · Inhomogeneity · Functionally-graded materials

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1 Introduction

In elasticity, for a given class of materials, universal deformations are those deformations that can be maintained in the absence of body forces by applying only boundary tractions for an arbitrary energy function in that class.¹ They are particularly important in nonlinear elasticity since they exist independently of a particular choice of energy function. Therefore, they can be used experimentally to study material properties and analytically as a basis for more complicated deformations or to gain insight into basic properties of materials. The history of a theory of universal deformations goes back to the seminal work of Ericksen who showed that for homogeneous compressible isotropic solids, universal deformations are homogeneous [9]. From that original seed, grew a large body of work addressing the same problems for materials that have constraints such as incompressibility, may be anisotropic, may be inhomogeneous, may be anelastic, or linear as shown in Fig. 1. The problem of finding universal deformations in the presence of internal constraints is more difficult [32]. For homogeneous incompressible isotropic solids, in a second seminal paper that was motivated by the earlier works of Rivlin [29–31], Ericksen [8] found four families of universal deformations. He conjectured that a deformation with constant principal invariants has to be homogeneous. This conjecture turned out to be incorrect [11], and motivated the discovery of a fifth family of universal deformations [20, 34]. The six known families of universal deformations are:

- Family 0: Homogeneous deformations
- Family 1: Bending, stretching, and shearing of a rectangular block
- Family 2: Straightening, stretching, and shearing of a sector of a cylindrical shell
- Family 3: Inflation, bending, torsion, extension, and shearing of a sector of an annular wedge
- Family 4: Inflation/inversion of a sector of a spherical shell
- Family 5: Inflation, bending, extension, and azimuthal shearing of an annular wedge

We should emphasize that for incompressible isotropic solids Ericksen's problem has not been solved completely to this day; the case of deformations with constant principal invariants is still an open problem. However, the conjecture is that there are no other possible families of universal deformations. In related works, there have been several studies of universal deformations and universal steady-state temperature fields in nonlinear thermoelasticity (see [6, 7, 26, 33], and references therein).

Based on Ericksen's seminal work, we embarked a few years ago into what we now refer to as the *universal program*: to generalize Ericksen's results to anisotropic and inhomogeneous materials for all hyperelastic materials, anelastic materials, and linear materials (see Fig. 1). Indeed, the analogue of universal deformations in linear elasticity are universal displacements [18, 38, 45]. In [45], it was shown that universal displacements explicitly depend on the symmetry class of the material; the larger the symmetry group is the larger the corresponding space of universal displacements is. More recently, we studied universal inhomogeneities in anisotropic linear elasticity [43]. There have been recent extensions of Ericksen's analysis to anelasticity. Yavari and Goriely [41] proved that in compressible anelasticity universal deformations must be covariantly homogeneous. In the case of incompressible anelasticity, Goodbrake et al. [15] observed that a key feature of the analysis is that the extra fields entering the analysis should follow the same symmetry as the universal deformations. They also showed that the six known families of

¹See Pucci et al. [27] for definitions of controllable, general, universal, and partial solutions in nonlinear elasticity.

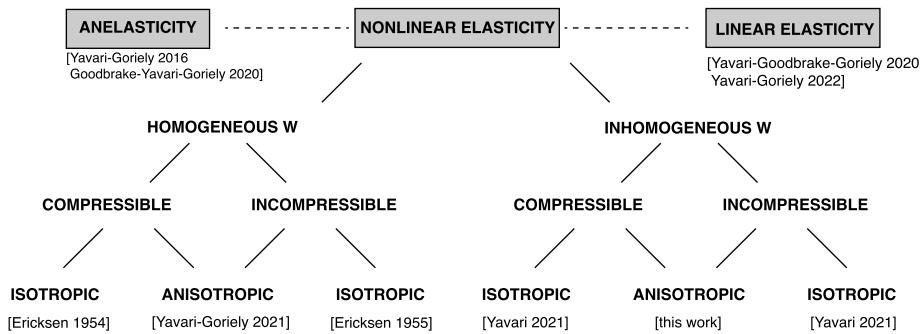


Fig. 1 The universal program: Finding all the universal deformations and displacements, together with the associated universal material preferred directions, and universal inhomogeneities, for both compressible and incompressible solids. These are the different cases considered so far with partial or complete solutions. Here, nonlinear elasticity refers to hyperelasticity and the existence of a strain-energy density W is assumed that can either be homogeneous or non-homogenous, isotropic or anisotropic

universal deformations are invariant under certain Lie subgroups of the special Euclidean group.

Until recently, there was no systematic study of universal deformations in anisotropic solids. There were early studies restricted to a subset of Family 1 deformations for two cases of homogeneous anisotropy, and Family 3 deformations for an example of homogeneous anisotropy [10] (see also [1, 2]). However, many examples of universal deformations for anisotropic fiber-reinforced systems were known and widely used [3, 4, 16, 17, 19, 23, 28, 36]. Recently, we studied universal deformations and universal material preferred directions in homogeneous compressible and incompressible anisotropic solids [42]. More specifically, we considered compressible and incompressible transversely isotropic, orthotropic, and monoclinic solids. We assumed that the material preferred directions can vary from point to point. In the case of compressible solids we showed that universal deformations are homogeneous and universal material preferred directions for the three classes of anisotropic solids must be uniform. In the case of homogeneous incompressible transversely isotropic, orthotropic, and monoclinic solids, we showed that in addition to the nine universality constraints for isotropic solids [8], there are extra 25, 74, and 152, respectively, extra universality constraints that must be satisfied. For each known family of universal deformations we obtained the universal material preferred directions assuming that they have the symmetry of the corresponding universal deformations (that are encoded in the symmetries of the right Cauchy-Green strain).²

Motivated by a result in [14], Yavari [40] extended the analysis of universal deformations to inhomogeneous isotropic solids (with position-dependent strain-energy density), and showed that in addition to those of homogeneous isotropic solids there are some extra universality constraints. It was shown that inhomogeneous compressible isotropic solids do not admit universal deformations. In the case of inhomogeneous incompressible solids the following results were obtained for each of the six known families of universal deformations.

²Unfortunately, there was a small mistake in calculating the universal material preferred directions for Family 5 deformations. The correct universal material preferred directions are given in (4.83), (5.17), and (6.31), for transversely isotropic, orthotropic, and monoclinic solids, respectively.

- For inhomogeneous incompressible isotropic solids it was incorrectly concluded that Family 0 deformations are not universal. This is discussed in §4.1, and the corrected statement is given in Footnote 4.
- Family 1 deformations are universal for any energy function of the form $W = W(X, I_1, I_2)$, where (X, Y, Z) is a Cartesian coordinate system with coordinate lines normal to the faces of an undeformed rectangular block. Note that with respect to cylindrical coordinates (r, θ, z) in the deformed configuration, Family 1 deformations have the form: $(r, \theta, z) = (\sqrt{C_1(2X + C_4)}, C_2(Y + C_5), \frac{Z}{C_1 C_2} - C_2 C_3 Y + C_6)$, where C_1, \dots, C_6 are constants.
- Families 2, 3, and 4 deformations are universal for any energy function of the form $W = W(R, I_1, I_2)$, where R is the radial coordinate in the undeformed configuration of a cylindrical shell, an annular wedge, and a spherical shell, for Families 2, 3, and 4, respectively.
- For inhomogeneous incompressible isotropic solids, Family 5 deformations are not universal.

The remaining problem to be solved to complete Ericksen's program is to study elastic materials that are inhomogenous, and anisotropic. Therefore, we study universal deformations for inhomogeneous anisotropic solids and generalize the results of [40, 42]. We consider both compressible and incompressible transversely isotropic, orthotropic, and monoclinic solids. It is shown that the *universality constraints*—the constraints that are dictated by the equilibrium equations and the arbitrariness of the energy function—for inhomogeneous anisotropic solids include those of inhomogeneous isotropic and homogeneous anisotropic solids as special cases. For compressible solids, universal deformations are homogeneous and the material preferred directions are uniform. For each of the three classes of anisotropic solids we find the corresponding *universal inhomogeneities*—those inhomogeneities (position dependence of the energy function) that are compatible with the universality constraints. For incompressible anisotropic solids we find the universal inhomogeneities for each of the six known families of universal deformations.

This paper is organized as follows. In §2 we tersely review nonlinear anisotropic elasticity. In §3, we consider inhomogeneous compressible transversely isotropic, orthotropic, and monoclinic solids. The universal deformations, universal material preferred directions, and universal inhomogeneities of inhomogeneous incompressible transversely isotropic solids are analyzed for each of the six known families in §4. Similar analyses for inhomogeneous incompressible orthotropic and inhomogeneous incompressible monoclinic solids are given in §5 and §6, respectively. Conclusions are given in §7.

2 Nonlinear Anisotropic Elasticity

Kinematics Consider an elastic body \mathcal{B} . In nonlinear anelasticity the body is identified with a Riemannian manifold $(\mathcal{B}, \mathbf{G})$ whose metric \mathbf{G} is used in calculating the natural distances between material points in the body. In nonlinear elasticity $(\mathcal{B}, \mathbf{G})$ is flat, and is a submanifold of the Euclidean 3-space. A deformation of the body is a map $\varphi : \mathcal{B} \rightarrow \mathcal{S}$, where \mathcal{S} is the Euclidean ambient space, and \mathbf{g} is the Euclidean metric. The material velocity is defined as

$$\mathbf{V}_t : \mathcal{B} \rightarrow T_{\varphi_t(\mathbf{X})} \mathcal{S}, \quad \mathbf{V}_t(\mathbf{X}) = \mathbf{V}(\mathbf{X}, t) = \frac{\partial \varphi(\mathbf{X}, t)}{\partial t}. \quad (2.1)$$

The spatial velocity is defined as $\mathbf{v} = \mathbf{V} \circ \varphi_t^{-1}$. The deformation gradient—the tangent map (or derivative) of φ —is denoted by $\mathbf{F} = T\varphi$. With respect to local coordinate charts $\{x^a\}$ and $\{X^A\}$ on S and \mathcal{B} , respectively, deformation gradient is defined as

$$\mathbf{F}(\mathbf{X}) : T_{\mathbf{X}}\mathcal{B} \rightarrow T_{\varphi(\mathbf{X})}S, \quad F^a{}_A(\mathbf{X}) = \frac{\partial \varphi^a}{\partial X^A}(\mathbf{X}). \quad (2.2)$$

The deformation gradient is a linear map that maps vectors in the tangent space at a material point in the reference configuration to vectors in the tangent space of the same material point in the current configuration. The transpose of deformation gradient is defined as

$$\mathbf{F}^T : T_{\mathbf{x}}S \rightarrow T_{\mathbf{X}}\mathcal{B}, \quad \langle\langle \mathbf{F}\mathbf{V}, \mathbf{v} \rangle\rangle_{\mathbf{g}} = \langle\langle \mathbf{V}, \mathbf{F}^T \mathbf{v} \rangle\rangle_{\mathbf{G}}, \quad \forall \mathbf{V} \in T_{\mathbf{X}}\mathcal{B}, \quad \mathbf{v} \in T_{\mathbf{x}}S, \quad (2.3)$$

where $\langle\langle \cdot, \cdot \rangle\rangle_{\mathbf{G}}$ and $\langle\langle \cdot, \cdot \rangle\rangle_{\mathbf{g}}$ are the inner products induced by the material and ambient space metrics, respectively. \mathbf{F}^T has the following components

$$(F^T(\mathbf{X}))^A{}_a = g_{ab}(\mathbf{x}) F^b{}_B(\mathbf{X}) G^{AB}(\mathbf{X}). \quad (2.4)$$

The right Cauchy-Green deformation tensor is defined as

$$\mathbf{C}(X) = \mathbf{F}(\mathbf{X})^T \mathbf{F}(\mathbf{X}) : T_{\mathbf{X}}\mathcal{B} \rightarrow T_{\mathbf{X}}\mathcal{B}, \quad C^A{}_B = (F^T)^A{}_a F^a{}_B. \quad (2.5)$$

The pulled-back metric is denoted by $\mathbf{C}^{\flat} = \varphi^* \mathbf{g}$, and is defined as

$$\langle\langle \mathbf{U}, \mathbf{W} \rangle\rangle_{\varphi^* \mathbf{g}} = \langle\langle \mathbf{F}\mathbf{U}, \mathbf{F}\mathbf{W} \rangle\rangle_{\mathbf{g}}, \quad \forall \mathbf{U}, \mathbf{W} \in T_{\mathbf{X}}\mathcal{B}, \quad (2.6)$$

where \flat is the flat operator induced by the metric \mathbf{g} . \mathbf{C}^{\flat} has components $C_{AB} = (g_{ab} \circ \varphi) F^a{}_A F^b{}_B$. The left Cauchy-Green deformation tensor is defined as

$$\mathbf{B}^{\sharp} = \varphi^*(\mathbf{g}^{\sharp}), \quad B^{AB} = (F^{-1})^A{}_a (F^{-1})^B{}_b g^{ab}. \quad (2.7)$$

The spatial analogues of \mathbf{C}^{\flat} and \mathbf{B}^{\sharp} are denoted by \mathbf{c}^{\flat} and \mathbf{b}^{\sharp} (the Finger deformation tensor), respectively, and are defined as

$$\begin{aligned} \mathbf{c}^{\flat} &= \varphi_*(\mathbf{G}), & c_{ab} &= (F^{-1})^A{}_a (F^{-1})^B{}_b G_{AB}, \\ \mathbf{b}^{\sharp} &= \varphi_*(\mathbf{G}^{\sharp}), & b^{ab} &= F^a{}_A F^b{}_B G^{AB}. \end{aligned} \quad (2.8)$$

The second-order tensors \mathbf{C} and \mathbf{b} have the same principal invariants I_1 , I_2 , and I_3 that are defined as [25]

$$\begin{aligned} I_1 &= \text{tr } \mathbf{b} = b^a{}_a = b^{ab} g_{ab}, \\ I_2 &= \frac{1}{2} (I_1^2 - \text{tr } \mathbf{b}^2) = \frac{1}{2} (I_1^2 - b^a{}_b b^b{}_a) = \frac{1}{2} (I_1^2 - b^{ab} b^{cd} g_{ac} g_{bd}), \\ I_3 &= \det \mathbf{b}. \end{aligned} \quad (2.9)$$

Balance laws The referential forms of the mass conservation and the balance of linear and angular momenta read

$$\frac{\partial \rho_0}{\partial t} = 0, \quad \text{Div } \mathbf{P} + \rho_0 \mathbf{B} = \rho_0 \mathbf{A}, \quad \mathbf{P} \mathbf{F}^T = \mathbf{F} \mathbf{P}^T, \quad (2.10)$$

where ρ_0 is the material mass density, \mathbf{B} is body force per unit referential volume, \mathbf{A} is the material acceleration, and \mathbf{P} is the first Piola-Kirchhoff stress. The spatial forms of conservation of mass and balance of linear and angular momenta read

$$\mathbf{L}_v \rho = 0, \quad \operatorname{div} \boldsymbol{\sigma} + \rho \mathbf{b} = \rho \mathbf{a}, \quad \boldsymbol{\sigma}^T = \boldsymbol{\sigma}, \quad (2.11)$$

where ρ is the spatial mass density, $\boldsymbol{\sigma}$ is the Cauchy stress, $\mathbf{b} = \mathbf{B} \circ \varphi_t^{-1}$, \mathbf{a} is the spatial acceleration, and $\mathbf{L}_v \rho$ is the Lie derivative of the spatial mass density with respect to the spatial velocity. \mathbf{P} and $\boldsymbol{\sigma}$ are related as $J \boldsymbol{\sigma}^{ab} = P^{aA} F^b{}_A$. The Jacobian of deformation $J = \sqrt{I_3}$ relates the material (dV) and spatial (dv) Riemannian volume forms as $dv = J dV$, and is given by

$$J = \sqrt{\frac{\det \mathbf{g}}{\det \mathbf{G}}} \det \mathbf{F}. \quad (2.12)$$

Constitutive equations For an inhomogeneous anisotropic hyperelastic solid the energy function (per unit undeformed volume) has the following functional form

$$W = \hat{W}(\mathbf{X}, \mathbf{C}^\flat, \mathbf{G}, \boldsymbol{\xi}_1, \dots, \boldsymbol{\xi}_n), \quad (2.13)$$

where W explicitly depends on \mathbf{X} (inhomogeneity), and the *structural tensors* $\boldsymbol{\xi}_i, i = 1, \dots, n$ characterize the material symmetry group of the solid. Using structural tensors the energy function becomes an isotropic function of its arguments. Instead of (2.13) one can write the energy as a function of an integrity basis for the set of tensors $\{\mathbf{C}^\flat, \mathbf{G}, \boldsymbol{\xi}_1, \dots, \boldsymbol{\xi}_n\}$. Denoting the integrity basis by $I_j, j = 1, \dots, m$, one can write $W = W(\mathbf{X}, I_1, \dots, I_m)$. The second Piola-Kirchhoff stress tensor has the following representation [5, 22, 44]

$$\mathbf{S} = 2 \frac{\partial \hat{W}}{\partial \mathbf{C}^\flat} = \sum_{j=1}^m 2 W_j \frac{\partial I_j}{\partial \mathbf{C}^\flat}, \quad W_j = W_j(\mathbf{X}, I_1, \dots, I_m) := \frac{\partial W}{\partial I_j}, \quad j = 1, \dots, m. \quad (2.14)$$

The relations between the second Piola-Kirchhoff stress, and the first Piola-Kirchhoff and Cauchy stresses are: $S^{AB} = (F^{-1})^A{}_a P^{aB} = J (F^{-1})^A{}_a (F^{-1})^B{}_b \sigma^{ab}$.

Isotropic solids For an inhomogeneous isotropic solid, $W = W(\mathbf{X}, I_1, I_2, I_3)$, where I_1, I_2 , and I_3 were defined in (2.9). From (2.14) one writes

$$\mathbf{S} = 2 W_1 \mathbf{G}^\sharp + 2 W_2 (I_2 \mathbf{C}^{-1} - I_3 \mathbf{C}^{-2}) + 2 W_3 I_3 \mathbf{C}^{-1}. \quad (2.15)$$

The Cauchy stress has the following representation

$$\sigma^{ab} = \frac{2}{\sqrt{I_3}} [W_1 b^{ab} + (I_2 W_2 + I_3 W_3) g^{ab} - I_3 W_2 c^{ab}], \quad (2.16)$$

where $c^{ab} = (F^{-1})^M{}_m (F^{-1})^N{}_n G_{MN} g^{am} g^{bn}$. For an incompressible isotropic solid $I_3 = 1$, and hence

$$\begin{aligned} \mathbf{S} &= -p \mathbf{C}^{-1} + 2 W_1 \mathbf{G}^\sharp - 2 W_2 \mathbf{C}^{-2}, \\ \boldsymbol{\sigma} &= -p \mathbf{g}^\sharp + 2 W_1 \mathbf{b}^\sharp - 2 W_2 \mathbf{c}^{-1}, \end{aligned} \quad (2.17)$$

where p is the Lagrange multiplier associated with the incompressibility constraint $J = \sqrt{I_3} = 1$. Equation (2.17)₂ in components reads $\sigma^{ab} = -p g^{ab} + 2 W_1 b^{ab} - 2 W_2 c^{ab}$.

Transversely isotropic solids In a transversely isotropic solid at every point there is a single material preferred direction, which is normal to the plane of isotropy at that point. We assume that a unit vector $\mathbf{N}(\mathbf{X})$ identifies the material preferred direction at $\mathbf{X} \in \mathcal{B}$. The energy function for an inhomogeneous transversely isotropic solid has the form $W = W(\mathbf{X}, \mathbf{G}, \mathbf{C}^\flat, \mathbf{A})$, where $\mathbf{A} = \mathbf{N} \otimes \mathbf{N}$ is a structural tensor [5, 21, 36]. The energy function W depends on five independent invariants that are defined as

$$\begin{aligned} I_1 &= \text{tr } \mathbf{C} = C^A{}_A, & I_2 &= \det \mathbf{C} \text{tr } \mathbf{C}^{-1} = \det(C^A{}_B)(C^{-1})^D{}_D, & I_3 &= \det \mathbf{C} = \det(C^A{}_B) \\ I_4 &= \mathbf{N} \cdot \mathbf{C} \cdot \mathbf{N} = N^A N^B C_{AB}, & I_5 &= \mathbf{N} \cdot \mathbf{C}^2 \cdot \mathbf{N} = N^A N^B C_{BM} C^M{}_A. \end{aligned} \quad (2.18)$$

The second Piola-Kirchhoff stress tensor has the following representation

$$\mathbf{S} = \sum_{j=1}^5 2W_j \frac{\partial I_j}{\partial \mathbf{C}^\flat}, \quad W_j = W_j(\mathbf{X}, I_1, \dots, I_5) := \frac{\partial W}{\partial I_j}, \quad j = 1, \dots, 5, \quad (2.19)$$

where

$$\begin{aligned} \frac{\partial I_1}{\partial \mathbf{C}^\flat} &= \mathbf{G}^\sharp, & \frac{\partial I_2}{\partial \mathbf{C}^\flat} &= I_2 \mathbf{C}^{-1} - I_3 \mathbf{C}^{-2}, & \frac{\partial I_3}{\partial \mathbf{C}^\flat} &= I_3 \mathbf{C}^{-1}, \\ \frac{\partial I_4}{\partial \mathbf{C}^\flat} &= \mathbf{N} \otimes \mathbf{N}, & \frac{\partial I_5}{\partial \mathbf{C}^\flat} &= \mathbf{N} \otimes (\mathbf{C} \cdot \mathbf{N}) + (\mathbf{C} \cdot \mathbf{N}) \otimes \mathbf{N}. \end{aligned} \quad (2.20)$$

Thus

$$\begin{aligned} \mathbf{S} &= 2W_1 \mathbf{G}^\sharp + 2W_2 (I_2 \mathbf{C}^{-1} - I_3 \mathbf{C}^{-2}) + 2W_3 I_3 \mathbf{C}^{-1} \\ &\quad + 2W_4 (\mathbf{N} \otimes \mathbf{N}) + 2W_5 [\mathbf{N} \otimes (\mathbf{C} \cdot \mathbf{N}) + (\mathbf{C} \cdot \mathbf{N}) \otimes \mathbf{N}]. \end{aligned} \quad (2.21)$$

The Cauchy stress has the representation [10, 12, 13]

$$\sigma^{ab} = \frac{2}{\sqrt{I_3}} [W_1 b^{ab} + (I_2 W_2 + I_3 W_3) g^{ab} - I_3 W_2 c^{ab} + W_4 n^a n^b + W_5 \ell^{ab}], \quad (2.22)$$

where $n^a = F^a{}_A N^A$, and

$$\ell^{ab} = n^a b^{bc} n_c + n^b b^{ac} n_c. \quad (2.23)$$

In the case of an incompressible transversely isotropic solid ($I_3 = 1$), $W = W(\mathbf{X}, I_1, I_2, I_4, I_5)$, and hence

$$\begin{aligned} \mathbf{S} &= -p \mathbf{C}^{-1} + 2W_1 \mathbf{G}^\sharp + 2W_2 (I_2 \mathbf{C}^{-1} - \mathbf{C}^{-2}) + 2W_4 (\mathbf{N} \otimes \mathbf{N}) \\ &\quad + 2W_5 [\mathbf{N} \otimes (\mathbf{C} \cdot \mathbf{N}) + (\mathbf{C} \cdot \mathbf{N}) \otimes \mathbf{N}]. \end{aligned} \quad (2.24)$$

Similarly, the Cauchy stress has the following representation [10, 12, 13, 37]

$$\sigma^{ab} = -p g^{ab} + 2W_1 b^{ab} - 2W_2 c^{ab} + 2W_4 n^a n^b + 2W_5 (n^a b^{bc} n^d g_{cd} + n^b b^{ac} n^d g_{cd}). \quad (2.25)$$

Orthotropic solids An orthotropic solid has reflection symmetry with respect to three mutually perpendicular planes at every point. Let three \mathbf{G} -orthonormal vectors $\mathbf{N}_1(\mathbf{X})$, $\mathbf{N}_2(\mathbf{X})$, and $\mathbf{N}_3(\mathbf{X})$ specify the orthotropic axes at a point \mathbf{X} in the reference configuration. The three tensors $\mathbf{A}_1 = \mathbf{N}_1 \otimes \mathbf{N}_1$, $\mathbf{A}_2 = \mathbf{N}_2 \otimes \mathbf{N}_2$, and $\mathbf{A}_3 = \mathbf{N}_3 \otimes \mathbf{N}_3$ are structural tensors. However, because $\mathbf{A}_1 + \mathbf{A}_2 + \mathbf{A}_3 = \mathbf{I}$, only two of them are independent. The energy function of an inhomogeneous orthotropic solid has the functional form $W = W(\mathbf{X}, \mathbf{G}, \mathbf{C}^\flat, \mathbf{A}_1, \mathbf{A}_2)$ [5, 21, 36]. It can be rewritten as a function of the following seven independent invariants:

$$\begin{aligned} I_1 &= \text{tr } \mathbf{C}, & I_2 &= \det \mathbf{C} \text{tr } \mathbf{C}^{-1}, & I_3 &= \det \mathbf{C}, \\ I_4 &= \mathbf{N}_1 \cdot \mathbf{C} \cdot \mathbf{N}_1, & I_5 &= \mathbf{N}_1 \cdot \mathbf{C}^2 \cdot \mathbf{N}_1, \\ I_6 &= \mathbf{N}_2 \cdot \mathbf{C} \cdot \mathbf{N}_2, & I_7 &= \mathbf{N}_2 \cdot \mathbf{C}^2 \cdot \mathbf{N}_2. \end{aligned} \quad (2.26)$$

Thus

$$\mathbf{S} = \sum_{j=1}^7 2W_j \frac{\partial I_j}{\partial \mathbf{C}^\flat}, \quad W_j = W_j(\mathbf{X}, I_1, \dots, I_7) := \frac{\partial W}{\partial I_j}, \quad j = 1, \dots, 7. \quad (2.27)$$

The second Piola-Kirchhoff stress tensor has the following representation

$$\begin{aligned} \mathbf{S} &= 2W_1 \mathbf{G}^\sharp + 2W_2 (I_2 \mathbf{C}^{-1} - I_3 \mathbf{C}^{-2}) + 2W_3 I_3 \mathbf{C}^{-1} \\ &\quad + 2W_4 (\mathbf{N}_1 \otimes \mathbf{N}_1) + 2W_5 [\mathbf{N}_1 \otimes (\mathbf{C} \cdot \mathbf{N}_1) + (\mathbf{C} \cdot \mathbf{N}_1) \otimes \mathbf{N}_1] \\ &\quad + 2W_6 (\mathbf{N}_2 \otimes \mathbf{N}_2) + 2W_7 [\mathbf{N}_2 \otimes (\mathbf{C} \cdot \mathbf{N}_2) + (\mathbf{C} \cdot \mathbf{N}_2) \otimes \mathbf{N}_2]. \end{aligned} \quad (2.28)$$

Similarly, the Cauchy stress is written as [12, 13, 35, 37]

$$\begin{aligned} \sigma^{ab} &= \frac{2}{\sqrt{I_3}} \left[W_1 b^{ab} + (I_2 W_2 + I_3 W_3) g^{ab} - I_3 W_2 c^{ab} \right. \\ &\quad + W_4 n_1^a n_1^b + W_5 (n_1^a b^{bc} n_1^d g_{cd} + n_1^b b^{ac} n_1^d g_{cd}) \\ &\quad \left. + W_6 n_2^a n_2^b + W_7 (n_2^a b^{bc} n_2^d g_{cd} + n_2^b b^{ac} n_2^d g_{cd}) \right], \end{aligned} \quad (2.29)$$

where $n_1^a = F^a{}_A N_1^A$, and $n_2^a = F^a{}_A N_2^A$. In the case of an incompressible orthotropic solid ($I_3 = 1$), $W = W(\mathbf{X}, I_1, I_2, I_4, I_5, I_6, I_7)$. Thus, using (2.28), one has

$$\begin{aligned} \mathbf{S} &= -p \mathbf{C}^{-1} + 2W_1 \mathbf{G}^\sharp + 2W_2 (I_2 \mathbf{C}^{-1} - \mathbf{C}^{-2}) \\ &\quad + 2W_4 (\mathbf{N}_1 \otimes \mathbf{N}_1) + 2W_5 [\mathbf{N}_1 \otimes (\mathbf{C} \cdot \mathbf{N}_1) + (\mathbf{C} \cdot \mathbf{N}_1) \otimes \mathbf{N}_1] \\ &\quad + 2W_6 (\mathbf{N}_2 \otimes \mathbf{N}_2) + 2W_7 [\mathbf{N}_2 \otimes (\mathbf{C} \cdot \mathbf{N}_2) + (\mathbf{C} \cdot \mathbf{N}_2) \otimes \mathbf{N}_2]. \end{aligned} \quad (2.30)$$

Similarly, the Cauchy stress tensor is written as

$$\sigma^{ab} = -p g^{ab} + 2W_1 b^{ab} - 2W_2 c^{ab} + 2W_4 n_1^a n_1^b + 2W_5 \ell_1^{ab} + 2W_6 n_2^a n_2^b + 2W_7 \ell_2^{ab}, \quad (2.31)$$

where $\ell_1^{ab} = n_1^a b^{bc} n_1^d g_{cd} + n_1^b b^{ac} n_1^d g_{cd}$, and $\ell_2^{ab} = n_2^a b^{bc} n_2^d g_{cd} + n_2^b b^{ac} n_2^d g_{cd}$.

Monoclinic solids A monoclinic solid has three material preferred directions that are specified by three unit vectors $\{\mathbf{N}_1, \mathbf{N}_2, \mathbf{N}_3\}$ such that $\mathbf{N}_1 \cdot \mathbf{N}_2 \neq 0$ and \mathbf{N}_3 is normal to the plane of \mathbf{N}_1 and \mathbf{N}_2 [24]. The energy function of a monoclinic solid depends on nine invariants [37], seven of which are identical to those of orthotropic solids (2.26). The two extra invariants are

$$I_8 = g \mathbf{N}_1 \cdot \mathbf{C} \cdot \mathbf{N}_2, \quad I_9 = g^2, \quad (2.32)$$

where $g = \mathbf{N}_1 \cdot \mathbf{N}_2$. Note that

$$\frac{\partial I_8}{\partial \mathbf{C}^b} = \frac{g}{2} (\mathbf{N}_1 \otimes \mathbf{N}_2 + \mathbf{N}_2 \otimes \mathbf{N}_1), \quad \frac{\partial I_9}{\partial \mathbf{C}^b} = \mathbf{0}. \quad (2.33)$$

For orthotropic solids the second Piola-Kirchhoff stress has the following representation

$$\begin{aligned} \mathbf{S} = & 2W_1 \mathbf{G}^\sharp + 2W_2 (I_2 \mathbf{C}^{-1} - I_3 \mathbf{C}^{-2}) + 2W_3 I_3 \mathbf{C}^{-1} \\ & + 2W_4 (\mathbf{N}_1 \otimes \mathbf{N}_1) + 2W_5 [\mathbf{N}_1 \otimes (\mathbf{C} \cdot \mathbf{N}_1) + (\mathbf{C} \cdot \mathbf{N}_1) \otimes \mathbf{N}_1] \\ & + 2W_6 (\mathbf{N}_2 \otimes \mathbf{N}_2) + 2W_7 [\mathbf{N}_2 \otimes (\mathbf{C} \cdot \mathbf{N}_2) + (\mathbf{C} \cdot \mathbf{N}_2) \otimes \mathbf{N}_2] \\ & + gW_8 (\mathbf{N}_1 \otimes \mathbf{N}_2 + \mathbf{N}_2 \otimes \mathbf{N}_1), \end{aligned} \quad (2.34)$$

where $W_i = W_i(\mathbf{X}, I_1, \dots, I_9)$, $i = 1, \dots, 8$. Similarly, the Cauchy stress can be written as

$$\begin{aligned} \sigma^{ab} = & \frac{2}{\sqrt{I_3}} \left[W_1 b^{ab} + (I_2 W_2 + I_3 W_3) g^{ab} - I_3 W_2 c^{ab} \right. \\ & + W_4 n_1^a n_1^b + W_5 (n_1^a b^{bc} n_1^d g_{cd} + n_1^b b^{ac} n_1^d g_{cd}) \\ & + W_6 n_2^a n_2^b + W_7 (n_2^a b^{bc} n_2^d g_{cd} + n_2^b b^{ac} n_2^d g_{cd}) \\ & \left. + gW_8 (n_1^a n_2^b + n_1^b n_2^a) \right]. \end{aligned} \quad (2.35)$$

In the case of incompressible monoclinic solids ($I_3 = 1$), $W = W(\mathbf{X}, I_1, I_2, I_4, I_5, I_6, I_7, I_8, I_9)$. Thus

$$\begin{aligned} \mathbf{S} = & -p \mathbf{C}^{-1} + 2W_1 \mathbf{G}^\sharp + 2W_2 (I_2 \mathbf{C}^{-1} - \mathbf{C}^{-2}) \\ & + 2W_4 (\mathbf{N}_1 \otimes \mathbf{N}_1) + 2W_5 [\mathbf{N}_1 \otimes (\mathbf{C} \cdot \mathbf{N}_1) + (\mathbf{C} \cdot \mathbf{N}_1) \otimes \mathbf{N}_1] \\ & + 2W_6 (\mathbf{N}_2 \otimes \mathbf{N}_2) + 2W_7 [\mathbf{N}_2 \otimes (\mathbf{C} \cdot \mathbf{N}_2) + (\mathbf{C} \cdot \mathbf{N}_2) \otimes \mathbf{N}_2] \\ & + gW_8 (\mathbf{N}_1 \otimes \mathbf{N}_2 + \mathbf{N}_2 \otimes \mathbf{N}_1). \end{aligned} \quad (2.36)$$

Similarly, the Cauchy stress tensor is written as

$$\sigma^{ab} = -p g^{ab} + 2W_1 b^{ab} - 2I_3 W_2 c^{ab} + 2W_4 n_1^a n_1^b + 2W_5 \ell_1^{ab} + 2W_6 n_2^a n_2^b + 2W_7 \ell_2^{ab} + W_8 \ell_3^{ab}, \quad (2.37)$$

where $\ell_3^{ab} = g (n_1^a n_2^b + n_1^b n_2^a)$.

3 Compressible Inhomogeneous Anisotropic Solids

3.1 Transversely Isotropic Solids

We first consider an inhomogeneous body made of compressible transversely isotropic solids. We do not specify the material preferred direction $\mathbf{N}(\mathbf{X})$ a priori. In the absence of body forces, the equilibrium equations in Cartesian coordinates read $\sigma^{ab}_{,b} = 0$. Substituting (2.22) into the equilibrium equations one obtains [42]

$$\begin{aligned} & -I_3^{-\frac{3}{2}} I_{3,b} [W_1 b^{ab} + (I_2 W_2 + I_3 W_3) \delta^{ab} - I_3 W_2 c^{ab} + W_4 n^a n^b + W_5 \ell^{ab}] \\ & + 2I_3^{-\frac{1}{2}} [(I_{2,b} W_2 + I_2 W_{2,b} + I_{3,b} W_3 + I_3 W_{3,b}) \delta^{ab} + W_1 b^{ab}_{,b} + W_{1,b} b^{ab} \\ & - I_{3,b} W_2 c^{ab} - I_3 W_{2,b} c^{ab} - I_3 W_2 c^{ab}_{,b} \\ & + W_{4,b} n^a n^b + W_4 n^a_{,b} n^b + W_4 n^a n^b_{,b} + W_{5,b} \ell^{ab} + W_5 \ell^{ab}_{,b}] = 0. \end{aligned} \quad (3.1)$$

For universal deformations the equilibrium equations hold for an arbitrary energy function W . Knowing that W is an arbitrary function of its arguments, the coefficient of W_1 , W_2 , W_3 , W_4 , and W_5 must vanish separately. Thus [42]

$$\begin{aligned} W_1 : \quad & b^{ab}_{,b} = 0, \\ W_2 : \quad & I_{2,b} \delta^{ab} - I_3 c^{ab}_{,b} = 0, \\ W_3 : \quad & I_{3,b} = 0, \\ W_4 : \quad & (n^a n^b)_{,b} = 0, \\ W_5 : \quad & \ell^{ab}_{,b} = 0. \end{aligned} \quad (3.2)$$

The above constraints simplify (3.1) to read

$$b^{ab} W_{1,b} + (I_2 \delta^{ab} - I_3 c^{ab}) W_{2,b} + I_3 \delta^{ab} W_{3,b} + n^a n^b W_{4,b} + \ell^{ab} W_{5,b} = 0. \quad (3.3)$$

Note that $I_{3,b} = 0$ from (3.2)₃ and

$$\begin{aligned} W_{1,b} &= (F^{-1})^A_b W_{1,A} + W_{11} I_{1,b} + W_{12} I_{2,b} + W_{14} I_{4,b} + W_{15} I_{5,b}, \\ W_{2,b} &= (F^{-1})^A_b W_{2,A} + W_{12} I_{1,b} + W_{22} I_{2,b} + W_{24} I_{4,b} + W_{25} I_{5,b}, \\ W_{3,b} &= (F^{-1})^A_b W_{3,A} + W_{13} I_{1,b} + W_{23} I_{2,b} + W_{34} I_{4,b} + W_{35} I_{5,b}, \\ W_{4,b} &= (F^{-1})^A_b W_{4,A} + W_{14} I_{1,b} + W_{24} I_{2,b} + W_{44} I_{4,b} + W_{45} I_{5,b}, \\ W_{5,b} &= (F^{-1})^A_b W_{5,A} + W_{15} I_{1,b} + W_{25} I_{2,b} + W_{45} I_{4,b} + W_{55} I_{5,b}, \end{aligned} \quad (3.4)$$

where

$$W_{i,A} = \frac{\partial W_i}{\partial X^A}, \quad W_{ij} = \frac{\partial^2 W}{\partial I_i \partial I_j}, \quad i \leq j. \quad (3.5)$$

Notice that the first term on the right-hand side of each equation in (3.4) vanishes for homogeneous solids [42]. Substituting the above relations into (3.3) the coefficients of W_{13} and

W_{23} read

$$\begin{aligned} W_{13} : \quad & I_3 I_{1,b} \delta^{ab} = 0, \\ W_{23} : \quad & I_3 I_{2,b} \delta^{ab} = 0. \end{aligned} \quad (3.6)$$

Thus, $I_{1,b} = I_{2,b} = 0$. Substituting these into (3.4) and using (3.3) the coefficients of W_{34} and W_{35} read

$$\begin{aligned} W_{34} : \quad & I_3 I_{4,b} \delta^{ab} = 0, \\ W_{35} : \quad & I_3 I_{5,b} \delta^{ab} = 0. \end{aligned} \quad (3.7)$$

Hence, $I_{4,b} = I_{5,b} = 0$. Therefore, we have the following universality constraints

$$I_1, I_2, \text{ and } I_3 \text{ are constant,} \quad (3.8)$$

$$b^{ab}_{,b} = c^{ab}_{,b} = 0, \quad (3.9)$$

$$I_4, \text{ and } I_5 \text{ are constant,} \quad (3.10)$$

$$(n^a n^b)_{,b} = \ell^{ab}_{,b} = 0. \quad (3.11)$$

Note that (3.8) and (3.9) are the universality constraints for isotropic solids [9, 41] and imply that $F^a_{A|B} = 0$, i.e., universal deformations are homogeneous. In addition, since $I_{4,b} = I_{4,A} (F^{-1})^A_b = 0$, we have $I_{4,A} = 0$. Similarly, $I_{5,A} = 0$. The constraints (3.10) and (3.11) imply that \mathbf{N} is a constant unit vector [42].

For inhomogeneous solids one has the following extra five sets of universality constraints:

$$\begin{aligned} b^{ab} (F^{-1})^A_b W_{1,A} &= 0, \\ (I_2 \delta^{ab} - I_3 c^{ab}) (F^{-1})^A_b W_{2,A} &= 0, \\ I_3 \delta^{ab} (F^{-1})^A_b W_{3,A} &= 0, \\ n^a n^b (F^{-1})^A_b W_{4,A} &= 0, \\ \ell^{ab} (F^{-1})^A_b W_{5,A} &= 0. \end{aligned} \quad (3.12)$$

The first three constraints in (3.12) are identical to those of isotropic solids [40], and imply that

$$W_{1,A} = W_{2,A} = W_{3,A} = 0, \quad A = 1, 2, 3. \quad (3.13)$$

The constraint (3.12)₄ implies that $n^b (F^{-1})^A_b W_{4,A} = W_{4,A} N^A = 0$. As \mathbf{N} is a constant unit vector we can choose the Cartesian coordinates (X^1, X^2, X^3) in the reference configuration such that

$$\mathbf{N} = \frac{\partial}{\partial X^1}, \quad (3.14)$$

i.e., $N^A = \delta_1^A$. Here we have used the notation ∂_{X^i} to denote the unit (tangent) vector along the i th Cartesian direction as is customary in differential geometry. With this choice of coordinates the constraint $W_{4,A} N^A = 0$ reads

$$\frac{\partial W_4}{\partial X^1} = 0. \quad (3.15)$$

Note that $n^a = F^a{}_A N^A = F^a{}_A \delta_1^A = F^a{}_1$.

Equation (3.12)₅ is equivalent to

$$(F^{-1})^B{}_a \ell^{ab} (F^{-1})^A{}_b W_{5,A} = 0, \quad B = 1, 2, 3. \quad (3.16)$$

Using (2.23) the above constraints can be rewritten as

$$(N^A C^B{}_D N^D + N^B C^A{}_D N^D) W_{5,A} = 0, \quad B = 1, 2, 3. \quad (3.17)$$

Knowing that $N^A = \delta_1^A$, this last expression can be rewritten as

$$C^B{}_1 W_{5,1} + \delta_1^B C^A{}_1 W_{5,A} = 0, \quad B = 1, 2, 3. \quad (3.18)$$

For $B = 2$, it implies that $C^2{}_1 W_{5,1} = 0$, which must hold for arbitrary homogeneous deformations, i.e., for arbitrary constant $C^2{}_1$. Thus, $W_{5,1} = 0$. Now the constraint for $B = 3$ is trivially satisfied. For $B = 1$, $C^2{}_1 W_{5,2} + C^3{}_1 W_{5,3} = 0$, which must be satisfied for arbitrary constants $C^2{}_1$, and $C^3{}_1$. Therefore, $W_{5,2} = W_{5,3} = 0$. Thus, the constraint (3.12)₅ implies that $W_{5,A} = 0$. In summary, we have the following constraints

$$W_{1,A} = W_{2,A} = W_{3,A} = W_{5,A} = 0, \quad A = 1, 2, 3, \quad \& \quad W_{4,1} = 0. \quad (3.19)$$

This implies that

$$\frac{\partial W}{\partial X^1} = f_1(\mathbf{X}), \quad \frac{\partial W}{\partial X^2} = f_2(\mathbf{X}, I_4), \quad \frac{\partial W}{\partial X^3} = f_3(\mathbf{X}, I_4), \quad (3.20)$$

for some scalar functions f_A . Note that $\frac{\partial f_1}{\partial X^2} = \frac{\partial f_2}{\partial X^1}$. Since f_1 does not depend on I_4 , one has

$$f_2(\mathbf{X}, I_4) = \bar{f}_2(X^2, X^3, I_4) + \bar{\bar{f}}_2(\mathbf{X}). \quad (3.21)$$

Similarly, $\frac{\partial f_1}{\partial X^3} = \frac{\partial f_3}{\partial X^1}$ implies that

$$f_3(\mathbf{X}, I_4) = \bar{f}_3(X^2, X^3, I_4) + \bar{\bar{f}}_3(\mathbf{X}). \quad (3.22)$$

From (3.20)₁, one writes

$$W(\mathbf{X}, I_i) = \int_{X_0^1}^{X^1} f_1(X^1, X^2, X^3) dX^1 + h(X^2, X^3, I_i), \quad (3.23)$$

where X_0^1 is some fixed value of X^1 , h is some scalar function, and $W(\mathbf{X}, I_i)$ and $h(X^2, X^3, I_i)$ are short for $W(\mathbf{X}, I_1, I_2, I_3, I_4, I_5)$ and $h(X^2, X^3, I_1, I_2, I_3, I_4, I_5)$, respectively. Taking partial derivative with respect to X^2 of both sides one obtains

$$\begin{aligned} \frac{\partial W}{\partial X^2} &= \int_{X_0^1}^{X^1} \frac{\partial f_1(X^1, X^2, X^3)}{\partial X^2} dX^1 + \frac{\partial h(X^2, X^3, I_i)}{\partial X^2}, \\ &= \int_{X_0^1}^{X^1} \frac{\partial f_2(X^1, X^2, X^3, I_4)}{\partial X^1} dX^1 + \frac{\partial h(X^2, X^3, I_i)}{\partial X^2}, \\ &= f_2(X^1, X^2, X^3, I_4) - f_2(X_0^1, X^2, X^3, I_4) + \frac{\partial h(X^2, X^3, I_i)}{\partial X^2}. \end{aligned} \quad (3.24)$$

From (3.24) and (3.20)₂ one concludes that

$$\frac{\partial h(X^2, X^3, I_i)}{\partial X^2} = f_2(X_0^1, X^2, X^3, I_4). \quad (3.25)$$

Thus

$$\int_{X_0^2}^{X^2} \frac{\partial h(X^2, X^3, I_i)}{\partial X^2} dX^2 = \int_{X_0^2}^{X^2} f_2(X_0^1, X^2, X^3, I_4) dX^2, \quad (3.26)$$

where X_0^2 is some fixed value of X^2 . Hence

$$h(X^2, X^3, I_i) = h(X_0^2, X^3, I_i) + \int_{X_0^2}^{X^2} f_2(X_0^1, X^2, X^3, I_4) dX^2. \quad (3.27)$$

Using the above relation in (3.23), one writes

$$W(\mathbf{X}, I_i) = h(X_0^2, X^3, I_i) + \int_{X_0^1}^{X^1} f_1(X^1, X^2, X^3) dX^1 + \int_{X_0^2}^{X^2} f_2(X_0^1, X^2, X^3, I_4) dX^2. \quad (3.28)$$

Taking partial derivative with respect to X^3 of the above relation one obtains

$$\begin{aligned} \frac{\partial W}{\partial X^3} &= \frac{\partial h(X_0^2, X^3, I_i)}{\partial X^3} + \int_{X_0^1}^{X^1} \frac{\partial f_1(X^1, X^2, X^3)}{\partial X^3} dX^1 + \int_{X_0^2}^{X^2} \frac{\partial f_2(X_0^1, X^2, X^3, I_4)}{\partial X^3} dX^2, \\ &= \frac{\partial h(X_0^2, X^3, I_i)}{\partial X^3} + \int_{X_0^1}^{X^1} \frac{\partial f_3(X^1, X^2, X^3, I_4)}{\partial X^1} dX^1 + \int_{X_0^2}^{X^2} \frac{\partial f_3(X_0^1, X^2, X^3, I_4)}{\partial X^2} dX^2, \\ &= \frac{\partial h(X_0^2, X^3, I_i)}{\partial X^3} + f_3(X^1, X^2, X^3, I_4) - f_3(X_0^1, X_0^2, X^3, I_4). \end{aligned} \quad (3.29)$$

Thus using (3.20)₃ one concludes that

$$\frac{\partial h(X_0^2, X^3, I_i)}{\partial X^3} = f_3(X_0^1, X_0^2, X^3, I_4). \quad (3.30)$$

Hence

$$\int_{X_0^3}^{X^3} \frac{\partial h(X_0^2, X^3, I_i)}{\partial X^3} dX^3 = \int_{X_0^3}^{X^3} f_3(X_0^1, X_0^2, X^3, I_4) dX^3, \quad (3.31)$$

where X_0^3 is some fixed value of X^3 . Thus

$$h(X_0^2, X^3, I_i) = h(X_0^2, X_0^3, I_i) + \int_{X_0^3}^{X^3} f_3(X_0^1, X_0^2, X^3, I_4) dX^3. \quad (3.32)$$

Substituting the above relation into (3.28) one obtains

$$W(\mathbf{X}, I_i) = h(X_0^2, X_0^3, I_i) + \int_{X_0^1}^{X^1} f_1(X^1, X^2, X^3) dX^1 + \int_{X_0^2}^{X^2} f_2(X_0^1, X^2, X^3, I_4) dX^2$$

$$+ \int_{X_0^3}^{X^3} f_3(X_0^1, X_0^2, X^3, I_4) dX^3. \quad (3.33)$$

Substituting (3.21) and (3.22) into the above relation one finds that $W(\mathbf{X}, I_i) = \hat{W}(\mathbf{X}) + \overline{W}(I_i) + \widetilde{W}(X^2, X^3, I_4)$. Note that the term $\hat{W}(\mathbf{X})$ is mechanically inconsequential, and hence we have proved that the only universal deformations are homogeneous and the only possible dependence on the position is through I_4 and in directions normal to a constant vector \mathbf{N} :

Proposition 3.1 *For compressible nonlinear transversely isotropic solids, universal deformations are homogeneous, the universal material preferred direction is at all points a constant unit vector \mathbf{N} , and the universal inhomogeneity has the following form*

$$W(\mathbf{X}, I_1, I_2, I_3, I_4, I_5) = \overline{W}(I_1, I_2, I_3, I_4, I_5) + \widetilde{W}(X^2, X^3, I_4), \quad (3.34)$$

where the Cartesian X^1 -coordinate line is parallel to \mathbf{N} .

3.2 Orthotropic Solids

For inhomogeneous compressible orthotropic solids there are two sets of universality constraints. The first set of constraints are identical to those of homogeneous compressible orthotropic solids and read [42]:

$$I_1, I_2, \text{ and } I_3 \text{ are constant,} \quad (3.35)$$

$$b^{ab}{}_{,b} = c^{ab}{}_{,b} = 0, \quad (3.36)$$

$$I_4, \text{ and } I_5 \text{ are constant,} \quad (3.37)$$

$$(n_1^a n_1^b)_{,b} = \ell_1^{ab}{}_{,b} = 0, \quad (3.38)$$

$$I_6, \text{ and } I_7 \text{ are constant,} \quad (3.39)$$

$$(n_2^a n_2^b)_{,b} = \ell_2^{ab}{}_{,b} = 0. \quad (3.40)$$

These constraints imply again that universal deformations are homogeneous and the material preferred directions are uniform. In the reference configuration we choose the Cartesian coordinates (X^1, X^2, X^3) such that

$$\mathbf{N}_1 = \frac{\partial}{\partial X^1}, \quad \mathbf{N}_2 = \frac{\partial}{\partial X^2}, \quad \mathbf{N}_3 = \frac{\partial}{\partial X^3}. \quad (3.41)$$

The second set of universality constraints are:

$$\begin{aligned} b^{ab} (F^{-1})^A{}_b W_{1,A} &= 0, \\ (I_2 \delta^{ab} - I_3 c^{ab}) (F^{-1})^A{}_b W_{2,A} &= 0, \\ I_3 \delta^{ab} (F^{-1})^A{}_b W_{3,A} &= 0, \\ n_1^a n_1^b (F^{-1})^A{}_b W_{4,A} &= 0, \\ \ell_1^{ab} (F^{-1})^A{}_b W_{5,A} &= 0, \\ n_2^a n_2^b (F^{-1})^A{}_b W_{6,A} &= 0, \\ \ell_2^{ab} (F^{-1})^A{}_b W_{7,A} &= 0. \end{aligned} \quad (3.42)$$

The first three constraints are identical to those of isotropic solids [40], and imply that $W_{1,A} = W_{2,A} = W_{3,A} = 0$. Similarly to the universality constraints of transversely isotropic solids, (3.42)₄ and (3.42)₆ imply that

$$\frac{\partial W_4}{\partial X^A} N_1^A = \frac{\partial W_4}{\partial X^1} = 0, \quad \frac{\partial W_6}{\partial X^A} N_2^A = \frac{\partial W_6}{\partial X^2} = 0. \quad (3.43)$$

The universality constraints (3.42)₅ and (3.42)₇ imply that

$$W_{5,A} = W_{7,A} = 0, \quad A = 1, 2, 3. \quad (3.44)$$

This means that

$$\frac{\partial W}{\partial X^1} = f_1(\mathbf{X}, I_6), \quad \frac{\partial W}{\partial X^2} = f_2(\mathbf{X}, I_4), \quad \frac{\partial W}{\partial X^3} = f_3(\mathbf{X}, I_4, I_6). \quad (3.45)$$

Note that

$$\frac{\partial f_1(\mathbf{X}, I_6)}{\partial X^2} = \frac{\partial f_2(\mathbf{X}, I_4)}{\partial X^1}, \quad \frac{\partial f_1(\mathbf{X}, I_6)}{\partial X^3} = \frac{\partial f_3(\mathbf{X}, I_4, I_6)}{\partial X^1}, \quad \frac{\partial f_2(\mathbf{X}, I_4)}{\partial X^3} = \frac{\partial f_3(\mathbf{X}, I_4, I_6)}{\partial X^2}. \quad (3.46)$$

Thus

$$\begin{aligned} f_1(\mathbf{X}, I_6) &= \bar{f}_1(X^1, X^3, I_6) + \bar{\bar{f}}_1(\mathbf{X}), \\ f_2(\mathbf{X}, I_4) &= \bar{f}_2(X^2, X^3, I_4) + \bar{\bar{f}}_2(\mathbf{X}). \end{aligned} \quad (3.47)$$

Using (3.45)₁, one writes

$$W(\mathbf{X}, I_i) = \int_{X_0^1}^{X^1} f_1(X^1, X^2, X^3, I_6) dX^1 + h(X^2, X^3, I_i), \quad (3.48)$$

where h is some scalar function, and X_0^1 is some fixed value of X^1 . Taking partial derivative with respect to X^2 of both sides one obtains

$$\begin{aligned} \frac{\partial W}{\partial X^2} &= \int_{X_0^1}^{X^1} \frac{\partial f_1(X^1, X^2, X^3, I_6)}{\partial X^2} dX^1 + \frac{\partial h(X^2, X^3, I_i)}{\partial X^2}, \\ &= \int_{X_0^1}^{X^1} \frac{\partial f_2(X^1, X^2, X^3, I_4)}{\partial X^1} dX^1 + \frac{\partial h(X^2, X^3, I_i)}{\partial X^2}, \\ &= f_2(X^1, X^2, X^3, I_4) - f_2(X_0^1, X^2, X^3, I_4) + \frac{\partial h(X^2, X^3, I_i)}{\partial X^2}. \end{aligned} \quad (3.49)$$

From (3.49) and (3.45)₂ one concludes that

$$\frac{\partial h(X^2, X^3, I_i)}{\partial X^2} = f_2(X_0^1, X^2, X^3, I_4). \quad (3.50)$$

Thus

$$\int_{X_0^2}^{X^2} \frac{\partial h(X^2, X^3, I_i)}{\partial X^2} dX^2 = \int_{X_0^2}^{X^2} f_2(X_0^1, X^2, X^3, I_4) dX^2, \quad (3.51)$$

where X_0^2 is some fixed value of X^2 . Hence

$$h(X^2, X^3, I_i) = h(X_0^2, X^3, I_i) + \int_{X_0^2}^{X^2} f_2(X_0^1, X^2, X^3, I_4) dX^2. \quad (3.52)$$

Using the above relation in (3.48), one has

$$W(\mathbf{X}, I_i) = h(X_0^2, X^3, I_i) + \int_{X_0^1}^{X^1} f_1(X^1, X^2, X^3, I_6) dX^1 + \int_{X_0^2}^{X^2} f_2(X_0^1, X^2, X^3, I_4) dX^2. \quad (3.53)$$

Taking partial derivative with respect to X^3 of the above relation one obtains

$$\begin{aligned} \frac{\partial W}{\partial X^3} &= \frac{\partial h(X_0^2, X^3, I_i)}{\partial X^3} + \int_{X_0^1}^{X^1} \frac{\partial f_1(X^1, X^2, X^3, I_6)}{\partial X^3} dX^1 + \int_{X_0^2}^{X^2} \frac{\partial f_2(X_0^1, X^2, X^3, I_4)}{\partial X^3} dX^2, \\ &= \frac{\partial h(X_0^2, X^3, I_i)}{\partial X^3} + \int_{X_0^1}^{X^1} \frac{\partial f_3(X^1, X^2, X^3, I_4, I_6)}{\partial X^1} dX^1 \\ &\quad + \int_{X_0^2}^{X^2} \frac{\partial f_3(X_0^1, X^2, X^3, I_4, I_6)}{\partial X^2} dX^2, \\ &= \frac{\partial h(X_0^2, X^3, I_i)}{\partial X^3} + f_3(X^1, X^2, X^3, I_4, I_6) - f_3(X_0^1, X_0^2, X^3, I_4, I_6). \end{aligned} \quad (3.54)$$

Thus using (3.45)₃ one concludes that

$$\frac{\partial h(X_0^2, X^3, I_i)}{\partial X^3} = f_3(X_0^1, X_0^2, X^3, I_4, I_6). \quad (3.55)$$

Hence

$$\int_{X_0^3}^{X^3} \frac{\partial h(X_0^2, X^3, I_i)}{\partial X^3} dX^3 = \int_{X_0^3}^{X^3} f_3(X_0^1, X_0^2, X^3, I_4, I_6) dX^3, \quad (3.56)$$

where X_0^3 is some fixed value of X^3 . Thus

$$h(X_0^2, X^3, I_i) = h(X_0^2, X_0^3, I_i) + \int_{X_0^3}^{X^3} f_3(X_0^1, X_0^2, X^3, I_4, I_6) dX^3. \quad (3.57)$$

Using the above relation in (3.53), one obtains

$$\begin{aligned} W(\mathbf{X}, I_i) &= h(X_0^2, X_0^3, I_i) + \int_{X_0^1}^{X^1} f_1(X^1, X^2, X^3, I_6) dX^1 + \int_{X_0^2}^{X^2} f_2(X_0^1, X^2, X^3, I_4) dX^2 \\ &\quad + \int_{X_0^3}^{X^3} f_3(X_0^1, X_0^2, X^3, I_4, I_6) dX^3. \end{aligned} \quad (3.58)$$

Substituting (3.47) into (3.58) one finds

$$W(\mathbf{X}, I_i) = \hat{W}(\mathbf{X}) + \overline{W}(I_i) + \int_{X_0^1}^{X^1} \bar{\tilde{f}}_1(X^1, X^3, I_6) dX^1 + \int_{X_0^2}^{X^2} \bar{\tilde{f}}_2(X^2, X^3, I_4) dX^2 \\ + \int_{X_0^3}^{X^3} f_3(X_0^1, X_0^2, X^3, I_4, I_6) dX^3. \quad (3.59)$$

Noting that the term $\hat{W}(\mathbf{X})$ is mechanically inconsequential, we have proved the following result.

Proposition 3.2 *For compressible nonlinear orthotropic solids universal deformations are homogeneous, the universal material preferred directions are everywhere the same three mutually orthogonal constant unit vectors $\mathbf{N}_1, \mathbf{N}_2$, and the universal inhomogeneity has the following form*

$$W(\mathbf{X}, I_1, I_2, I_3, I_4, I_5, I_6, I_7) = \overline{W}(I_1, I_2, I_3, I_4, I_5, I_6, I_7) \\ + \widetilde{W}(X^3, I_4, I_6) + \widehat{W}(X^2, X^3, I_4) + \widehat{W}(X^1, X^3, I_6), \quad (3.60)$$

where the Cartesian coordinate lines are the orthotropy directions.

While the form of this strain-energy density seems involved, it can be written explicitly in terms of the Cartesian components of \mathbf{C} as

$$W(\mathbf{X}, \mathbf{C}) = \overline{W}(\mathbf{C}) + \widetilde{W}(X^3, C_{11}, C_{22}) + \widehat{W}(X^2, X^3, C_{11}) + \widehat{W}(X^1, X^3, C_{22}). \quad (3.61)$$

3.3 Monoclinic Solids

Note that orthogonality of the material preferred directions was not assumed when deriving the constraints (3.35)-(3.40), i.e., these universality constraints hold for monoclinic solids as well. However, there are the following extra universality constraints [42]:

$$I_8, \text{ and } I_9 \text{ are constant,} \quad (3.62)$$

$$(n_3^a n_3^b)_{,b} = \ell_3^{ab} ,_{,b} = 0. \quad (3.63)$$

For compressible monoclinic solids the universality constraints (3.35)-(3.40) imply that universal deformations are homogeneous, and the three unit vectors $\mathbf{N}_1, \mathbf{N}_2$, and \mathbf{N}_3 are constant. This means that (3.62), (3.63) are trivially satisfied. Let us assume that the angle between \mathbf{N}_1 and \mathbf{N}_2 is θ ($0 < \theta < \frac{\pi}{2}$). In the reference configuration we choose a Cartesian coordinate system (X^1, X^2, X^3) such that

$$\mathbf{N}_3 = \frac{\partial}{\partial X^3}. \quad (3.64)$$

In general, \mathbf{N}_1 makes an angle α with the X_1 -axis, and thus

$$\mathbf{N}_1 = \cos \alpha \frac{\partial}{\partial X^1} + \sin \alpha \frac{\partial}{\partial X^2}, \quad \mathbf{N}_2 = \cos(\alpha + \theta) \frac{\partial}{\partial X^1} + \sin(\alpha + \theta) \frac{\partial}{\partial X^2}. \quad (3.65)$$

The second set of universality constraints for inhomogeneous monoclinic solids include those of orthotropic solids, i.e., Eqs. (3.42). There is one extra universality constrain that reads:

$$\ell_3^{ab}(F^{-1})^A{}_b W_{8,A} = 0. \quad (3.66)$$

This is equivalent to $(N_1^B N_2^A + N_1^A N_2^B) W_{8,A} = 0$, and is trivially satisfied for $B = 3$. For $B = 1, 2$ it gives us

$$\begin{aligned} 2 \cos \alpha \cos(\alpha + \theta) W_{8,1} + \sin(2\alpha + \theta) W_{8,2} &= 0, \\ \sin(2\alpha + \theta) W_{8,1} + 2 \sin \alpha \sin(\alpha + \theta) W_{8,2} &= 0. \end{aligned} \quad (3.67)$$

These need to be satisfied for arbitrary α , and θ , and hence

$$W_{8,1} = W_{8,2} = 0. \quad (3.68)$$

The first three universality constraints in (3.42), and (3.42)₅ and (3.42)₇ imply that

$$W_{1,A} = W_{2,A} = W_{3,A} = W_{5,A} = W_{7,A} = 0, \quad A = 1, 2, 3. \quad (3.69)$$

The constraint (3.42)₄ implies that

$$\frac{\partial W_4}{\partial X^A} N_1^A = \cos \alpha \frac{\partial W_6}{\partial X^1} + \sin \alpha \frac{\partial W_6}{\partial X^2} = 0, \quad (3.70)$$

which must hold for any α , and hence

$$\frac{\partial W_4}{\partial X^1} = \frac{\partial W_4}{\partial X^2} = 0. \quad (3.71)$$

The constraint (3.42)₆ implies that

$$\frac{\partial W_6}{\partial X^A} N_2^A = \cos(\alpha + \theta) \frac{\partial W_6}{\partial X^1} + \sin(\alpha + \theta) \frac{\partial W_6}{\partial X^2} = 0. \quad (3.72)$$

This needs to hold for any $0 < \theta < \frac{\pi}{2}$, and hence

$$\frac{\partial W_6}{\partial X^1} = \frac{\partial W_6}{\partial X^2} = 0. \quad (3.73)$$

From Eqs. (3.68), (3.69), (3.71), and (3.73) one has

$$\frac{\partial W}{\partial X^1} = f_1(\mathbf{X}, I_9), \quad \frac{\partial W}{\partial X^2} = f_2(\mathbf{X}, I_9), \quad \frac{\partial W}{\partial X^3} = f_3(\mathbf{X}, I_4, I_6, I_8, I_9). \quad (3.74)$$

Using (3.74)₁, one can write

$$W(\mathbf{X}, I_i) = \int_{X_0^1}^{X^1} f_1(X^1, X^2, X^3, I_9) dX^1 + h(X^2, X^3, I_i). \quad (3.75)$$

Taking partial derivative with respect to X^2 of both sides one obtains

$$\begin{aligned}\frac{\partial W}{\partial X^2} &= \int_{X_0^1}^{X^1} \frac{\partial f_1(X^1, X^2, X^3, I_9)}{\partial X^2} dX^1 + \frac{\partial h(X^2, X^3, I_i)}{\partial X^2}, \\ &= \int_{X_0^1}^{X^1} \frac{\partial f_2(X^1, X^2, X^3, I_9)}{\partial X^1} dX^1 + \frac{\partial h(X^2, X^3, I_i)}{\partial X^2}, \\ &= f_2(X^1, X^2, X^3, I_9) - f_2(X_0^1, X^2, X^3, I_9) + \frac{\partial h(X^2, X^3, I_i)}{\partial X^2}.\end{aligned}\quad (3.76)$$

From (3.76) and (3.74)₂ one concludes that

$$\frac{\partial h(X^2, X^3, I_i)}{\partial X^2} = f_2(X_0^1, X^2, X^3, I_9). \quad (3.77)$$

Thus

$$h(X^2, X^3, I_i) = h(X_0^2, X^3, I_i) + \int_{X_0^2}^{X^2} f_2(X_0^1, X^2, X^3, I_4, I_9) dX^2. \quad (3.78)$$

Using the above relation in (3.75), one writes

$$W(\mathbf{X}, I_i) = h(X_0^2, X^3, I_i) + \int_{X_0^1}^{X^1} f_1(X^1, X^2, X^3, I_9) dX^1 + \int_{X_0^2}^{X^2} f_2(X_0^1, X^2, X^3, I_9) dX^2. \quad (3.79)$$

Taking partial derivative with respect to X^3 of the above relation one obtains

$$\begin{aligned}\frac{\partial W}{\partial X^3} &= \frac{\partial h(X_0^2, X^3, I_i)}{\partial X^3} + \int_{X_0^1}^{X^1} \frac{\partial f_1(X^1, X^2, X^3, I_9)}{\partial X^3} dX^1 + \int_{X_0^2}^{X^2} \frac{\partial f_2(X_0^1, X^2, X^3, I_9)}{\partial X^3} dX^2, \\ &= \frac{\partial h(X_0^2, X^3, I_i)}{\partial X^3} + \int_{X_0^1}^{X^1} \frac{\partial f_3(X^1, X^2, X^3, I_4, I_6, I_8, I_9)}{\partial X^1} dX^1 \\ &\quad + \int_{X_0^2}^{X^2} \frac{\partial f_3(X_0^1, X^2, X^3, I_4, I_6, I_8, I_9)}{\partial X^2} dX^2, \\ &= \frac{\partial h(X_0^2, X^3, I_i)}{\partial X^3} + f_3(X^1, X^2, X^3, I_4, I_6, I_8, I_9) - f_3(X_0^1, X_0^2, X^3, I_4, I_6, I_8, I_9).\end{aligned}\quad (3.80)$$

Thus using (3.74)₃ one concludes that

$$\frac{\partial h(X_0^2, X^3, I_i)}{\partial X^3} = f_3(X_0^1, X_0^2, X^3, I_4, I_6, I_8, I_9). \quad (3.81)$$

Hence

$$h(X_0^2, X^3, I_i) = h(X_0^2, X_0^3, I_i) + \int_{X_0^3}^{X^3} f_3(X_0^1, X_0^2, X^3, I_4, I_6, I_8, I_9) dX^3. \quad (3.82)$$

Table 1 Universal inhomogeneities for compressible transversely isotropic, orthotropic, and monoclinic solids

Symmetry class	Energy function	Universal energy function
Transversely isotropic	$W(X^1, X^2, X^3, I_1, I_2, I_3, I_4, I_5)$	$\overline{W}(I_1, I_2, I_3, I_4, I_5) + \widetilde{W}(X^2, X^3, I_4)$
Orthotropic	$W(X^1, X^2, X^3, I_1, I_2, I_3, I_4, I_5, I_6, I_7)$	$\overline{W}(I_1, I_2, I_3, I_4, I_5, I_6, I_7) + \widetilde{W}(X^3, I_4, I_6)$ + $\widehat{W}(X^2, X^3, I_4) + \widehat{W}(X^1, X^3, I_6)$
Monoclinic	$W(X^1, X^2, X^3, I_1, I_2, I_3, I_4, I_5, I_6, I_7, I_8, I_9)$	$\overline{W}(I_1, I_2, I_3, I_4, I_5, I_6, I_7, I_8, I_9)$ + $\widetilde{W}(X^3, I_4, I_6, I_8, I_9)$

Using the above relation in (3.79), one obtains

$$W(\mathbf{X}, I_i) = h(X_0^2, X_0^3, I_i) + \int_{X_0^1}^{X^1} f_1(X^1, X^2, X^3, I_9) dX^1 + \int_{X_0^2}^{X^2} f_2(X_0^1, X^2, X^3, I_9) dX^2 \\ + \int_{X_0^3}^{X^3} f_3(X_0^1, X_0^2, X^3, I_4, I_6, I_8, I_9) dX^3. \quad (3.83)$$

Note that the second and third terms on the right-hand side are mechanically inconsequential, and hence, we have proved the following result.

Proposition 3.3 *For compressible nonlinear monoclinic solids universal deformations are homogeneous, the universal material preferred directions are everywhere the same three constant unit vectors \mathbf{N}_1 , \mathbf{N}_2 , and \mathbf{N}_3 , such that \mathbf{N}_3 is perpendicular to the plane of \mathbf{N}_1 and \mathbf{N}_2 , and the universal inhomogeneity has the following form*

$$W(\mathbf{X}, I_1, I_2, I_3, I_4, I_5, I_6, I_7, I_8, I_9) = \overline{W}(I_1, I_2, I_3, I_4, I_5, I_6, I_7, I_8, I_9) \\ + \widetilde{W}(X^3, I_4, I_6, I_8, I_9), \quad (3.84)$$

where the Cartesian X^3 -coordinate line is along \mathbf{N}_3 .

Table 1 summarizes our results for inhomogeneous compressible anisotropic solids.

4 Incompressible Inhomogeneous Transversely Isotropic Elastic Solids

For a body made of an incompressible transversely isotropic solid, the equilibrium equations in the absence of body forces read:

$$p_{,b} g^{ab} = 2 [W_1 b^{ab} - W_2 c^{ab} + W_4 n^a n^b + W_5 \ell^{ab}]_{|b}. \quad (4.1)$$

This is equivalent to exactness of the 1-form

$$\xi = g_{am} [W_1 b^{mn} - W_2 c^{mn} + W_4 n^m n^n + W_5 \ell^{mn}]_{|n} dx^a = \xi_a dx^a, \quad (4.2)$$

where

$$\begin{aligned}\xi_a &= [W_1 b_a^n - W_2 c_a^n + W_4 n_a n^n + W_5 \ell_a^n]_{|n} \\ &= W_{1,n} b_a^n - W_{2,n} c_a^n + W_{4,n} n_a n^n + W_{5,n} \ell_a^n + W_1 b_a^n|_n - W_2 c_a^n|_n + W_4 (n_a n^n)|_n \\ &\quad + W_5 \ell_a^n|_n.\end{aligned}\quad (4.3)$$

The exactness of ξ implies that $d\xi = \mathbf{0}$ [39], or equivalently, $\xi_{a|b} = \xi_{b|a}$, where

$$\begin{aligned}\xi_{a|b} &= W_1 b_a^n|_{nb} - W_2 c_a^n|_{nb} + W_4 (n_a n^n)|_{nb} + W_5 \ell_a^n|_{nb} \\ &\quad + W_{1,n} b_a^n|_{|b} - W_{2,n} c_a^n|_{|b} + W_{4,n} (n_a n^n)|_{|b} + W_{5,n} \ell_a^n|_{|b} \\ &\quad + W_{1,b} b_a^n|_n - W_{2,b} c_a^n|_n + W_{4,b} (n_a n^n)|_n + W_{5,b} \ell_a^n|_n \\ &\quad + W_{1|nb} b_a^n - W_{2|nb} c_a^n + W_{4|nb} n_a n^n + W_{5|nb} \ell_a^n.\end{aligned}\quad (4.4)$$

Note that $W_i = W_i(\mathbf{X}, I_1, I_2, I_4, I_5)$, $i = 1, 2, 4, 5$, and thus

$$\begin{aligned}W_{1,b} &= (F^{-1})^A_n W_{1,A} + W_{11} I_{1,b} + W_{12} I_{2,b} + W_{14} I_{4,b} + W_{15} I_{5,b}, \\ W_{2,b} &= (F^{-1})^A_n W_{2,A} + W_{12} I_{1,b} + W_{22} I_{2,b} + W_{24} I_{4,b} + W_{25} I_{5,b}, \\ W_{4,b} &= (F^{-1})^A_n W_{4,A} + W_{14} I_{1,b} + W_{24} I_{2,b} + W_{44} I_{4,b} + W_{45} I_{5,b}, \\ W_{5,b} &= (F^{-1})^A_n W_{5,A} + W_{15} I_{1,b} + W_{25} I_{2,b} + W_{45} I_{4,b} + W_{55} I_{5,b}.\end{aligned}\quad (4.5)$$

Note also that

$$\begin{aligned}W_{1|bn} &= (W_{1,b})_{|n} = W_{11} I_{1|bn} + W_{12} I_{2|bn} + W_{14} I_{4|bn} + W_{15} I_{5|bn} + W_{11,n} I_{1,b} + W_{12,n} I_{2,b} \\ &\quad + W_{14,n} I_{4,b} + W_{15,n} I_{5,b} + [(F^{-1})^A_b W_{1,A}]_{|n}.\end{aligned}\quad (4.6)$$

The last term on the right hand-side is simplified as

$$\begin{aligned}[(F^{-1})^A_b W_{1,A}]_{|n} &= \frac{\partial}{\partial x^n} [(F^{-1})^A_b W_{1,A}] - \gamma^m{}_{nb} (F^{-1})^A_m W_{1,A} \\ &= (F^{-1})^B_n (F^{-1})^A_{b,B} W_{1,A} + (F^{-1})^A_b \frac{\partial}{\partial x^n} W_{1,A} - \gamma^m{}_{nb} (F^{-1})^A_m W_{1,A}.\end{aligned}\quad (4.7)$$

Notice that

$$\begin{aligned}\frac{\partial}{\partial x^n} W_{1,A} &= (F^{-1})^B_n W_{1,AB} + \frac{\partial}{\partial X^A} [W_{11} I_{1,n} + W_{12} I_{2,n} + W_{14} I_{4,n} + W_{15} I_{5,n}] \\ &= (F^{-1})^B_n W_{1,AB} + W_{11,A} I_{1,n} + W_{12,A} I_{2,n} + W_{14,A} I_{4,n} + W_{15,A} I_{5,n}.\end{aligned}\quad (4.8)$$

Thus

$$\begin{aligned}[(F^{-1})^A_b W_{1,A}]_{|n} &= [(F^{-1})^B_n (F^{-1})^A_{b,B} - \gamma^m{}_{nb} (F^{-1})^A_m] W_{1,A} + (F^{-1})^A_b (F^{-1})^B_n W_{1,AB} \\ &\quad + (F^{-1})^A_b [W_{11} I_{1,n} + W_{12} I_{2,n} + W_{14} I_{4,n} + W_{15} I_{5,n}] \\ &= [(F^{-1})^B_n (F^{-1})^A_{b,B} - \gamma^m{}_{nb} (F^{-1})^A_m] W_{1,A}\end{aligned}$$

$$\begin{aligned}
& + \frac{1}{2} \left[(F^{-1})^A{}_b (F^{-1})^B{}_n + (F^{-1})^B{}_b (F^{-1})^A{}_n \right] W_{1,AB} \\
& + (F^{-1})^A{}_b \left[W_{11} I_{1,n} + W_{12} I_{2,n} + W_{14} I_{4,n} + W_{15} I_{5,n} \right]. \tag{4.9}
\end{aligned}$$

Let us denote the independent third-order derivatives of the energy function by $W_{ijk} = \frac{\partial^3 W}{\partial I_i \partial I_j \partial I_k}$, ($i \leq j \leq k$). Thus

$$\begin{aligned}
W_{11,n} &= (F^{-1})^A{}_n W_{11,A} + W_{111} I_{1,n} + W_{112} I_{2,n} + W_{114} I_{4,n} + W_{115} I_{5,n}, \\
W_{12,n} &= (F^{-1})^A{}_n W_{12,A} + W_{112} I_{1,n} + W_{122} I_{2,n} + W_{124} I_{4,n} + W_{125} I_{5,n}, \\
W_{14,n} &= (F^{-1})^A{}_n W_{14,A} + W_{114} I_{1,n} + W_{124} I_{2,n} + W_{144} I_{4,n} + W_{145} I_{5,n}, \\
W_{15,n} &= (F^{-1})^A{}_n W_{15,A} + W_{115} I_{1,n} + W_{125} I_{2,n} + W_{145} I_{4,n} + W_{155} I_{5,n}. \tag{4.10}
\end{aligned}$$

Hence³

$$\begin{aligned}
W_{1|bn} &= W_{11} I_{1|bn} + W_{12} I_{2|bn} + W_{14} I_{4|bn} + W_{15} I_{5|bn} \\
& + W_{111} I_{1,n} I_{1,b} + W_{112} (I_{2,n} I_{1,b} + I_{1,n} I_{2,b}) + W_{114} (I_{4,n} I_{1,b} + I_{1,n} I_{4,b}) \\
& + W_{115} (I_{5,n} I_{1,b} + I_{1,n} I_{5,b}) + W_{122} I_{2,n} I_{2,b} + W_{124} (I_{4,n} I_{2,b} + I_{4,b} I_{2,n}) \\
& + W_{125} (I_{5,n} I_{2,b} + I_{2,n} I_{5,b}) + W_{144} I_{4,n} I_{4,b} + W_{145} (I_{5,n} I_{4,b} + I_{5,b} I_{4,n} + W_{155} I_{5,n} I_{5,b}) \\
& + \left[(F^{-1})^B{}_b (F^{-1})^A{}_n B - \gamma^m{}_{nb} (F^{-1})^A{}_m \right] W_{1,A} \\
& + \frac{1}{2} \left[(F^{-1})^A{}_n (F^{-1})^B{}_b + (F^{-1})^B{}_n (F^{-1})^A{}_b \right] W_{1,AB} \\
& + \left[(F^{-1})^A{}_n I_{1,b} + (F^{-1})^A{}_b I_{1,n} \right] W_{11,A} + \left[(F^{-1})^A{}_n I_{2,b} + (F^{-1})^A{}_b I_{2,n} \right] W_{12,A} \\
& + \left[(F^{-1})^A{}_n I_{4,b} + (F^{-1})^A{}_b I_{4,n} \right] W_{14,A} + \left[(F^{-1})^A{}_n I_{5,b} + (F^{-1})^A{}_b I_{5,n} \right] W_{15,A}. \tag{4.11}
\end{aligned}$$

Similarly,

$$\begin{aligned}
W_{2|bn} &= W_{12} I_{1|bn} + W_{22} I_{2|bn} + W_{24} I_{4|bn} + W_{25} I_{5|bn} \\
& + W_{112} I_{1,n} I_{1,b} + W_{122} (I_{2,n} I_{1,b} + I_{1,n} I_{2,b}) + W_{222} I_{2,n} I_{2,b} \\
& + W_{244} I_{4,n} I_{4,b} + W_{255} I_{5,n} I_{5,b} + W_{124} (I_{4,n} I_{1,b} + I_{4,b} I_{1,n}) \\
& + W_{125} (I_{5,n} I_{1,b} + I_{1,n} I_{5,b}) + W_{224} (I_{4,n} I_{2,b} + I_{4,b} I_{2,n}) \\
& + W_{225} (I_{5,n} I_{2,b} + I_{5,b} I_{2,n}) + W_{245} (I_{5,n} I_{4,b} + I_{5,b} I_{4,n}) \\
& + \left[(F^{-1})^B{}_b (F^{-1})^A{}_n B - \gamma^m{}_{nb} (F^{-1})^A{}_m \right] W_{2,A} \\
& + \frac{1}{2} \left[(F^{-1})^A{}_n (F^{-1})^B{}_b + (F^{-1})^B{}_n (F^{-1})^A{}_b \right] W_{2,AB} \\
& + \left[(F^{-1})^A{}_n I_{1,b} + (F^{-1})^A{}_b I_{1,n} \right] W_{12,A} + \left[(F^{-1})^A{}_n I_{2,b} + (F^{-1})^A{}_b I_{2,n} \right] W_{22,A} \\
& + \left[(F^{-1})^A{}_n I_{4,b} + (F^{-1})^A{}_b I_{4,n} \right] W_{24,A} + \left[(F^{-1})^A{}_n I_{5,b} + (F^{-1})^A{}_b I_{5,n} \right] W_{25,A}, \tag{4.12}
\end{aligned}$$

³The factor “ $\frac{1}{2}$ ” on the sixth line is missing in Eqs. (4.7)-(4.9) in [40]. However, this typo did not affect any of the results of that work.

$$\begin{aligned}
W_{4|bn} = & W_{14} I_{1|bn} + W_{24} I_{2|bn} + W_{44} I_{4|bn} + W_{45} I_{5|bn} \\
& + W_{114} I_{1,n} I_{1,b} + W_{224} I_{2,n} I_{2,b} + W_{444} I_{4,n} I_{4,b} + W_{455} I_{5,n} I_{5,b} \\
& + W_{124}(I_{2,n} I_{1,b} + I_{1,n} I_{2,b}) + W_{144}(I_{4,n} I_{1,b} + I_{4,b} I_{1,n}) \\
& + W_{244}(I_{4,n} I_{2,b} + I_{2,n} I_{4,b}) + W_{145}(I_{5,n} I_{1,b} + I_{5,b} I_{1,n}) \\
& + W_{245}(I_{5,n} I_{2,b} + I_{2,n} I_{5,b}) + W_{445}(I_{5,n} I_{4,b} + I_{5,b} I_{4,n}) \\
& + [(F^{-1})^B_b (F^{-1})^A_{n,B} - \gamma^m_{nb} (F^{-1})^A_m] W_{4,A} \\
& + \frac{1}{2} [(F^{-1})^A_n (F^{-1})^B_b + (F^{-1})^B_n (F^{-1})^A_b] W_{4,AB} \\
& + [(F^{-1})^A_n I_{1,b} + (F^{-1})^A_b I_{1,n}] W_{14,A} + [(F^{-1})^A_n I_{2,b} + (F^{-1})^A_b I_{2,n}] W_{24,A} \\
& + [(F^{-1})^A_n I_{4,b} + (F^{-1})^A_b I_{4,n}] W_{44,A} + [(F^{-1})^A_n I_{5,b} + (F^{-1})^A_b I_{5,n}] W_{45,A}, \tag{4.13}
\end{aligned}$$

and

$$\begin{aligned}
W_{5|bn} = & W_{15} I_{1|bn} + W_{25} I_{2|bn} + W_{45} I_{4|bn} + W_{55} I_{5|bn} \\
& + W_{115} I_{1,n} I_{1,b} + W_{225} I_{2,n} I_{2,b} + W_{445} I_{4,n} I_{4,b} + W_{555} I_{5,n} I_{5,b} \\
& + W_{125}(I_{2,n} I_{1,b} + I_{1,n} I_{2,b}) + W_{145}(I_{4,n} I_{1,b} + I_{4,b} I_{2,n}) \\
& + W_{155}(I_{5,n} I_{1,b} + I_{1,n} I_{5,b}) + W_{245}(I_{4,n} I_{2,b} + I_{4,b} I_{2,n}) \\
& + W_{255}(I_{5,n} I_{2,b} + I_{2,n} I_{5,b}) + W_{455}(I_{5,n} I_{4,b} + I_{5,b} I_{4,n}) \\
& + [(F^{-1})^B_b (F^{-1})^A_{n,B} - \gamma^m_{nb} (F^{-1})^A_m] W_{5,A} \\
& + \frac{1}{2} [(F^{-1})^A_n (F^{-1})^B_b + (F^{-1})^B_n (F^{-1})^A_b] W_{5,AB} \\
& + [(F^{-1})^A_n I_{1,b} + (F^{-1})^A_b I_{1,n}] W_{15,A} + [(F^{-1})^A_n I_{2,b} + (F^{-1})^A_b I_{2,n}] W_{25,A} \\
& + [(F^{-1})^A_n I_{4,b} + (F^{-1})^A_b I_{4,n}] W_{45,A} + [(F^{-1})^A_n I_{5,b} + (F^{-1})^A_b I_{5,n}] W_{55,A}. \tag{4.14}
\end{aligned}$$

The symmetry $\xi_{a|b} = \xi_{b|a}$ forces the coefficient of each partial derivative of the energy function to be symmetric. Following the notation introduced in [42], we define \mathcal{A}_{ab}^κ to be the matrix of the coefficient of W_κ , where κ is a multi-index. The first nine terms are identical to those of homogeneous isotropic solids: $\kappa \in \mathcal{K}_{\text{Iso}} = \{1, 2, 11, 22, 12, 111, 222, 112, 122\}$. They read

$$\begin{aligned}
\mathcal{A}_{ab}^1 &= b_{a|bn}^n, \\
\mathcal{A}_{ab}^2 &= -c_{a|bn}^n, \\
\mathcal{A}_{ab}^{11} &= b_{a|n}^n I_{1,b} + (b_{a|n}^n I_{1,n})_{|b}, \\
\mathcal{A}_{ab}^{22} &= -c_{a|n}^n I_{2,b} - (c_{a|n}^n I_{2,n})_{|b}, \\
\mathcal{A}_{ab}^{12} &= (b_{a|n}^n I_{2,n})_{|b} + b_{a|n}^n I_{2,b} - [(c_{a|n}^n I_{1,n})_{|b} + c_{a|n}^n I_{1,b}], \\
\mathcal{A}_{ab}^{111} &= b_{a|n}^n I_{1,n} I_{1,b}, \\
\mathcal{A}_{ab}^{222} &= -c_{a|n}^n I_{2,n} I_{2,b},
\end{aligned}$$

$$\begin{aligned}\mathcal{A}_{ab}^{112} &= b_a^n (I_{1,b} I_{2,n} + I_{1,n} I_{2,b}) - c_a^n I_{1,n} I_{1,b}, \\ \mathcal{A}_{ab}^{122} &= b_a^n I_{2,b} I_{2,n} - c_a^n (I_{1,b} I_{2,n} + I_{1,n} I_{2,b}),\end{aligned}\quad (4.15)$$

where $b_a^n = b^{mn} g_{ma}$, and $c_a^n = c^{mn} g_{ma}$. It is well known that the symmetry of the above nine terms admits six families of deformations [8, 20, 34]. For both homogeneous and inhomogeneous transversely isotropic solids, we have 25 extra terms:

$$\begin{aligned}\mathcal{K} = \{4, 5, 44, 55, 14, 15, 24, 25, 45, 444, 555, 114, 115, 124, 125, \\ 144, 145, 155, 224, 225, 244, 245, 255, 445, 455\}.\end{aligned}\quad (4.16)$$

These terms read [42]:

$$\begin{aligned}\mathcal{A}_{ab}^4 &= (n_a n^n)_{|nb}, \\ \mathcal{A}_{ab}^5 &= \ell_a^n |_{nb}, \\ \mathcal{A}_{ab}^{44} &= (n_a n^n)_{|n} I_{4,b} + (n_a n^n I_{4,n})_{|b}, \\ \mathcal{A}_{ab}^{55} &= \ell_a^n |_n I_{5,b} + (\ell_a^n I_{5,n})_{|b}, \\ \mathcal{A}_{ab}^{14} &= b_a^n |_n I_{4,b} + (b_a^n I_{4,n})_{|b} + (n_a n^n)_{|n} I_{1,b} + (n_a n^n I_{1,n})_{|b}, \\ \mathcal{A}_{ab}^{15} &= b_a^n |_n I_{5,b} + (b_a^n I_{5,n})_{|b} + \ell_a^n |_n I_{1,b} + (\ell_a^n I_{1,n})_{|b}, \\ \mathcal{A}_{ab}^{24} &= (n_a n^n)_{|n} I_{2,b} + (n_a n^n I_{2,n})_{|b} - [c_a^n |_n I_{4,b} + (c_a^n I_{4,n})_{|b}], \\ \mathcal{A}_{ab}^{25} &= \ell_a^n |_n I_{2,b} + (\ell_a^n I_{2,n})_{|b} - [c_a^n |_n I_{5,b} + (c_a^n I_{5,n})_{|b}], \\ \mathcal{A}_{ab}^{45} &= (n_a n^n)_{|n} I_{5,b} + (n_a n^n I_{5,n})_{|b} + \ell_a^n |_n I_{4,b} + (\ell_a^n I_{4,n})_{|b},\end{aligned}\quad (4.17)$$

and

$$\begin{aligned}\mathcal{A}_{ab}^{444} &= n_a n^n I_{4,n} I_{4,b}, \\ \mathcal{A}_{ab}^{555} &= \ell_a^n I_{5,n} I_{5,b}, \\ \mathcal{A}_{ab}^{114} &= b_a^n (I_{4,n} I_{1,b} + I_{4,b} I_{1,n}) + n_a n^n I_{1,n} I_{1,b}, \\ \mathcal{A}_{ab}^{115} &= b_a^n (I_{5,n} I_{1,b} + I_{5,b} I_{1,n}) + \ell_a^n I_{1,n} I_{1,b}, \\ \mathcal{A}_{ab}^{124} &= b_a^n (I_{4,n} I_{2,b} + I_{4,b} I_{2,n}) - c_a^n (I_{4,n} I_{1,b} + I_{4,b} I_{1,n}) + n_a n^n (I_{2,n} I_{1,b} + I_{2,b} I_{1,n}), \\ \mathcal{A}_{ab}^{125} &= b_a^n (I_{5,n} I_{2,b} + I_{5,b} I_{2,n}) - c_a^n (I_{5,n} I_{1,b} + I_{5,b} I_{1,n}) + \ell_a^n (I_{2,n} I_{1,b} + I_{2,b} I_{1,n}), \\ \mathcal{A}_{ab}^{144} &= b_a^n I_{4,n} I_{4,b} + n_a n^n (I_{4,n} I_{1,b} + I_{4,b} I_{1,n}), \\ \mathcal{A}_{ab}^{145} &= b_a^n (I_{5,n} I_{4,b} + I_{5,b} I_{4,n}) + n_a n^n (I_{5,n} I_{1,b} + I_{5,b} I_{1,n}) + \ell_a^n (I_{4,n} I_{1,b} + I_{4,b} I_{1,n}), \\ \mathcal{A}_{ab}^{155} &= b_a^n I_{5,n} I_{5,b} + \ell_a^n (I_{5,n} I_{1,b} + I_{5,b} I_{1,n}), \\ \mathcal{A}_{ab}^{224} &= n_a n^n I_{2,n} I_{2,b} - c_a^n (I_{4,n} I_{2,b} + I_{4,b} I_{2,n}), \\ \mathcal{A}_{ab}^{225} &= \ell_a^n I_{2,n} I_{2,b} - c_a^n (I_{5,n} I_{2,b} + I_{5,b} I_{2,n}), \\ \mathcal{A}_{ab}^{244} &= -c_a^n I_{4,n} I_{4,b} + n_a n^n (I_{4,n} I_{2,b} + I_{4,b} I_{2,n}), \\ \mathcal{A}_{ab}^{245} &= n_a n^n (I_{5,n} I_{2,b} + I_{5,b} I_{2,n}) + \ell_a^n (I_{4,n} I_{2,b} + I_{4,b} I_{2,n}) - c_a^n (I_{5,n} I_{4,b} + I_{5,b} I_{4,n}),\end{aligned}$$

$$\begin{aligned}
\mathcal{A}_{ab}^{255} &= \ell_a^n (I_{5,n} I_{2,b} + I_{5,b} I_{2,n}) - c_a^n I_{5,n} I_{5,b}, \\
\mathcal{A}_{ab}^{445} &= n_a n^n (I_{5,n} I_{4,b} + I_{5,b} I_{4,n}) + \ell_a^n I_{4,n} I_{4,b}, \\
\mathcal{A}_{ab}^{455} &= n_a n^n I_{5,n} I_{5,b} + \ell_a^n (I_{5,n} I_{4,b} + I_{5,b} I_{4,n}).
\end{aligned} \tag{4.18}$$

It turns out that the known universal deformations are invariant with respect to certain Lie subgroups of the special Euclidean group [15]. In [42] we conjectured that for each family of universal deformations the corresponding universal material preferred direction vector \mathbf{N} is invariant under the same Lie subgroup. For each of the six families of universal deformations we found the corresponding universal material preferred directions.

For inhomogeneous incompressible transversely isotropic solids, in addition to the universality constraints (4.15), (4.17), and (4.18), there are the following eighteen extra sets of universality constraints (each term must be symmetric in (ab) for $A = 1, 2, 3$, and $B \geq A$):

$$\begin{aligned}
C_{ab}^{1A} &= (F^{-1})_n^A b_{a|b}^n + (F^{-1})_b^A b_{a|n}^n + b_a^n [(F^{-1})_b^B (F^{-1})_n^A - \gamma^m_{nb} (F^{-1})_m^A], \\
C_{ab}^{2A} &= (F^{-1})_n^A c_{a|b}^n + (F^{-1})_b^A c_{a|n}^n + c_a^n [(F^{-1})_b^B (F^{-1})_n^A - \gamma^m_{nb} (F^{-1})_m^A], \\
C_{ab}^{11A} &= b_a^n [(F^{-1})_n^A I_{1,b} + (F^{-1})_b^A I_{1,n}], \\
C_{ab}^{22A} &= c_a^n [(F^{-1})_n^A I_{2,b} + (F^{-1})_b^A I_{2,n}], \\
C_{ab}^{12A} &= b_a^n [(F^{-1})_n^A I_{2,b} + (F^{-1})_b^A I_{2,n}] - c_a^n [(F^{-1})_n^A I_{1,b} + (F^{-1})_b^A I_{1,n}], \\
C_{ab}^{1AB} &= b_a^n [(F^{-1})_n^A (F^{-1})_b^B + (F^{-1})_b^A (F^{-1})_n^B], \\
C_{ab}^{2AB} &= c_a^n [(F^{-1})_n^A (F^{-1})_b^B + (F^{-1})_b^A (F^{-1})_n^B],
\end{aligned} \tag{4.19}$$

and

$$\begin{aligned}
C_{ab}^{4A} &= (F^{-1})_n^A (n_a n^n)_{|b} + (F^{-1})_b^A (n_a n^n)_{|n} \\
&\quad + n_a n^n [(F^{-1})_b^B (F^{-1})_n^A - \gamma^m_{nb} (F^{-1})_m^A], \\
C_{ab}^{5A} &= (F^{-1})_n^A \ell_{a|b}^n + (F^{-1})_b^A \ell_{a|n}^n + \ell_a^n [(F^{-1})_b^B (F^{-1})_n^A - \gamma^m_{nb} (F^{-1})_m^A], \\
C_{ab}^{14A} &= b_a^n [(F^{-1})_n^A I_{4,b} + (F^{-1})_b^A I_{4,n}] + n_a n^n [(F^{-1})_n^A I_{1,b} + (F^{-1})_b^A I_{1,n}], \\
C_{ab}^{15A} &= b_a^n [(F^{-1})_n^A I_{5,b} + (F^{-1})_b^A I_{5,n}] + \ell_a^n [(F^{-1})_n^A I_{1,b} + (F^{-1})_b^A I_{1,n}], \\
C_{ab}^{24A} &= -c_a^n [(F^{-1})_n^A I_{4,b} + (F^{-1})_b^A I_{4,n}] + n_a n^n [(F^{-1})_n^A I_{2,b} + (F^{-1})_b^A I_{2,n}], \\
C_{ab}^{25A} &= -c_a^n [(F^{-1})_n^A I_{5,b} + (F^{-1})_b^A I_{5,n}] + \ell_a^n [(F^{-1})_n^A I_{2,b} + (F^{-1})_b^A I_{2,n}], \\
C_{ab}^{44A} &= n_a n^n [(F^{-1})_n^A I_{4,b} + (F^{-1})_b^A I_{4,n}], \\
C_{ab}^{45A} &= n_a n^n [(F^{-1})_n^A I_{5,b} + (F^{-1})_b^A I_{5,n}] + \ell_a^n [(F^{-1})_n^A I_{4,b} + (F^{-1})_b^A I_{4,n}], \\
C_{ab}^{55A} &= \ell_a^n [(F^{-1})_n^A I_{5,b} + (F^{-1})_b^A I_{5,n}], \\
C_{ab}^{4AB} &= n_a n^n [(F^{-1})_n^A (F^{-1})_b^B + (F^{-1})_b^A (F^{-1})_n^B], \\
C_{ab}^{5AB} &= \ell_a^n [(F^{-1})_n^A (F^{-1})_b^B + (F^{-1})_b^A (F^{-1})_n^B].
\end{aligned} \tag{4.20}$$

The set of universality constraints (4.19) are identical to those of inhomogeneous isotropic solids [40]. For a given family of deformations and material preferred directions that are

consistent with (4.15), (4.17), and (4.18), the corresponding inhomogeneities that respect (4.19) and (4.20) are called the *universal inhomogeneities*. In the following subsections, for each of the six families of universal deformations the corresponding universal inhomogeneities will be determined. This will be done by looking at each term in (4.19) and (4.20) and examining its symmetries. If a particular term cannot be symmetric, the corresponding derivative of W has to vanish, giving us a constraint on the form of W .

4.1 Family 0: Homogeneous Deformations

With respect to the Cartesian coordinates $\{X^A\}$ and $\{x^a\}$ in the reference and current configurations, respectively, a homogeneous deformation has the representation $x^a(\mathbf{X}) = F^a{}_A X^A + c^a$, where $[F^a{}_A]$ is a constant matrix and $[c^a]$ is a constant vector. The incompressibility constraint is then $\det[F^a{}_A] = 1$. For a homogeneous deformation the right Cauchy-Green tensor has the constant components $C_{AB} = F^a{}_A F^a{}_B \delta_{ab}$, which implies that \mathbf{C}^b is invariant under the action of $T(3) \subset SE(3)$ —the group of translations. In [42] it was assumed that $\mathbf{N}(\mathbf{X})$ is invariant under $T(3)$ as well, i.e., \mathbf{N} is a constant unit vector. We choose the Cartesian coordinates (X^1, X^2, X^3) such that

$$\mathbf{N} = \frac{\partial}{\partial X^1}, \quad (4.21)$$

i.e., $N^A = \delta_1^A$. With this assumption the universality constraints (4.17) and (4.18) are satisfied. For homogeneous deformations, the first five sets of universality constraints (4.19) are trivially satisfied. The last two sets force the deformation to be the identity [40]. This implies that

$$W_{1,AB} = W_{2,AB} = 0, \quad A, B = 1, 2, 3. \quad (4.22)$$

For isotropic solids, the relations $W_{1,AB} = (W_{1,A})_{,B} = 0$, and $W_{2,AB} = (W_{2,A})_{,B} = 0$ imply that

$$\begin{aligned} \frac{\partial W_1}{\partial X^1} &= f_1(I_1, I_2), & \frac{\partial W_1}{\partial X^2} &= f_2(I_1, I_2), & \frac{\partial W_1}{\partial X^3} &= f_3(I_1, I_2), \\ \frac{\partial W_2}{\partial X^1} &= g_1(I_1, I_2), & \frac{\partial W_2}{\partial X^2} &= g_2(I_1, I_2), & \frac{\partial W_2}{\partial X^3} &= g_3(I_1, I_2). \end{aligned} \quad (4.23)$$

Note that

$$\frac{\partial f_1(I_1, I_2)}{\partial I_2} = \frac{\partial g_1(I_1, I_2)}{\partial I_1}, \quad \frac{\partial f_2(I_1, I_2)}{\partial I_2} = \frac{\partial g_2(I_1, I_2)}{\partial I_1}, \quad \frac{\partial f_3(I_1, I_2)}{\partial I_2} = \frac{\partial g_3(I_1, I_2)}{\partial I_1}. \quad (4.24)$$

From (4.23)₁, one concludes that

$$W_1(\mathbf{X}, I_1, I_2) = f_0(I_1, I_2) + f_1(I_1, I_2)X^1 + f_2(I_1, I_2)X^2 + f_3(I_1, I_2)X^3. \quad (4.25)$$

Thus

$$\begin{aligned} W(\mathbf{X}, I_1, I_2) &= \int f_0(I_1, I_2) dI_1 + X^1 \int f_1(I_1, I_2) dI_1 + X^2 \int f_2(I_1, I_2) dI_1 \\ &\quad + X^3 \int f_3(I_1, I_2) dI_1 + R(\mathbf{X}, I_2), \end{aligned} \quad (4.26)$$

for some function $R(\mathbf{X}, I_2)$. Hence

$$\begin{aligned}
W_2(\mathbf{X}, I_1, I_2) &= \int \frac{\partial f_0(I_1, I_2)}{\partial I_2} dI_1 + X^1 \int \frac{\partial f_1(I_1, I_2)}{\partial I_2} dI_1 + X^2 \int \frac{\partial f_2(I_1, I_2)}{\partial I_2} dI_1 \\
&\quad + X^3 \int \frac{\partial f_3(I_1, I_2)}{\partial I_2} dI_1 + \frac{\partial R(\mathbf{X}, I_2)}{\partial I_2} \\
&= \int \frac{\partial f_0(I_1, I_2)}{\partial I_2} dI_1 + X^1 \int \frac{\partial g_1(I_1, I_2)}{\partial I_1} dI_1 + X^2 \int \frac{\partial g_2(I_1, I_2)}{\partial I_1} dI_1 \\
&\quad + X^3 \int \frac{\partial g_3(I_1, I_2)}{\partial I_1} dI_1 + \frac{\partial R(\mathbf{X}, I_2)}{\partial I_2} \\
&= \int \frac{\partial f_0(I_1, I_2)}{\partial I_2} dI_1 + g_1(I_1, I_2)X^1 + g_2(I_1, I_2)X^2 + g_3(I_1, I_2)X^3 \\
&\quad + \frac{\partial R(\mathbf{X}, I_2)}{\partial I_2}.
\end{aligned} \tag{4.27}$$

Substituting the above identity into (4.23)₂ one concludes that

$$\frac{\partial}{\partial X^1} \frac{\partial R(\mathbf{X}, I_2)}{\partial I_2} = \frac{\partial}{\partial X^2} \frac{\partial R(\mathbf{X}, I_2)}{\partial I_2} = \frac{\partial}{\partial X^3} \frac{\partial R(\mathbf{X}, I_2)}{\partial I_2} = 0. \tag{4.28}$$

This implies that

$$\frac{\partial R(\mathbf{X}, I_2)}{\partial I_2} = r(I_2), \tag{4.29}$$

and hence $R(\mathbf{X}, I_2) = R_1(\mathbf{X}) + R_2(I_2)$. Using this in (4.26), up to a mechanically inconsequential \mathbf{X} -dependent term one concludes that for an incompressible isotropic solid the energy function is a linear function of the Cartesian coordinates, i.e.,

$$W(\mathbf{X}, I_1, I_2) = \overline{W}(I_1, I_2) + \mathbf{H}(I_1, I_2) \cdot \mathbf{X}, \tag{4.30}$$

for some vector $\mathbf{H}(I_1, I_2)$.⁴

In the case of inhomogeneous transversely isotropic solids, one still has the constraints (4.22). The first nine sets of universality constraints (4.20) are trivially satisfied for homogeneous deformations and constant \mathbf{N} . The last two sets of constraints in (4.20) are nontrivial. The universality constraints corresponding to Eq. (4.20)₁₀ read

$$n_a [N^A (F^{-1})^B{}_b + N^B (F^{-1})^A{}_b] W_{4,AB} = n_b [N^A (F^{-1})^B{}_a + N^B (F^{-1})^A{}_a] W_{4,AB}. \tag{4.31}$$

Knowing that $N^A = \delta_1^A$, the above constraints are rewritten as

$$[n_a (F^{-1})^A{}_b - n_b (F^{-1})^A{}_a] W_{4,1A} = 0, \quad a, b = 1, 2, 3. \tag{4.32}$$

This is equivalent to

$$F^a{}_M F^b{}_N [n_a (F^{-1})^A{}_b - n_b (F^{-1})^A{}_a] W_{4,1A} = 0, \quad M, N = 1, 2, 3, \tag{4.33}$$

⁴In [40] from (4.22) it was incorrectly concluded that $W(\mathbf{X}, I_1, I_2) = \overline{W}(I_1, I_2)$. Proposition 4.1 in [40] should be corrected to read: “For inhomogeneous incompressible nonlinear isotropic solids, Family 0 deformations are universal for any energy function of the form $W(\mathbf{X}, I_1, I_2) = \overline{W}(I_1, I_2) + \mathbf{H}(I_1, I_2) \cdot \mathbf{X}$.”

which is simplified to read

$$C_{M1} W_{4,1N} - C_{N1} W_{4,1M} = 0, \quad M, N = 1, 2, 3. \quad (4.34)$$

These are three constraints corresponding to $(M, N) = (1, 2)$, $(1, 3)$, and $(2, 3)$, and read

$$\begin{aligned} C_{11} W_{4,12} - C_{21} W_{4,11} &= 0, \\ C_{11} W_{4,13} - C_{31} W_{4,11} &= 0, \\ C_{21} W_{4,13} - C_{31} W_{4,12} &= 0. \end{aligned} \quad (4.35)$$

Notice that these need to be satisfied for an arbitrary matrix $[C_{AB}]$ with unit determinant. This means that $W_{4,11} = W_{4,12} = W_{4,13} = 0$.

The universality constraints corresponding to Eq. (4.20)₁₁ read

$$\begin{aligned} \ell_a^n \left[(F^{-1})^A{}_n (F^{-1})^B{}_b + (F^{-1})^B{}_n (F^{-1})^A{}_b \right] W_{5,AB} \\ = \ell_b^n \left[(F^{-1})^A{}_n (F^{-1})^B{}_a + (F^{-1})^B{}_n (F^{-1})^A{}_a \right] W_{5,AB}, \quad a, b = 1, 2, 3. \end{aligned} \quad (4.36)$$

This can be simplified to read

$$C^K{}_1 \left[C_{M1} W_{5,KN} + C_{MK} W_{5,1N} - C_{N1} W_{5,KM} - C_{NK} W_{5,1M} \right] = 0, \quad M, N = 1, 2, 3. \quad (4.37)$$

These are three constraints corresponding to $(M, N) = (1, 2)$, $(1, 3)$, and $(2, 3)$, and read

$$\begin{aligned} & (2C^1{}_1 C_{21} + C^2{}_1 C_{22} + C^3{}_1 C_{23}) W_{5,11} - (2C^1{}_1 C_{11} + C^3{}_1 C_{13}) W_{5,12} + C^3{}_1 C_{21} W_{5,13} \\ & - C^2{}_1 C_{11} W_{5,22} - C^3{}_1 C_{11} W_{5,23} = 0, \\ & (2C^1{}_1 C_{31} + C^2{}_1 C_{32} + C^3{}_1 C_{33}) W_{5,11} + C^2{}_1 C_{31} W_{5,12} - (2C^1{}_1 C_{11} + C^2{}_1 C_{12}) W_{5,13} \\ & - C^2{}_1 C_{11} W_{5,23} - C^3{}_1 C_{11} W_{5,33} = 0, \\ & (2C^1{}_1 C_{31} + C^2{}_1 C_{32} + C^3{}_1 C_{33}) W_{5,12} - (2C^1{}_1 C_{21} + C^2{}_1 C_{22} + C^3{}_1 C_{23}) W_{5,13} \\ & + C^2{}_1 C_{31} W_{5,22} + (C^3{}_1 C_{31} - C^2{}_1 C_{21}) W_{5,23} - C^3{}_1 C_{21} W_{5,33} = 0. \end{aligned} \quad (4.38)$$

These must be satisfied for an arbitrary matrix $[C_{AB}]$ with unit determinant. If $[C_{AB}]$ is diagonal, one concludes that $W_{5,12} = W_{5,13} = 0$. Considering simple shear in the $X^1 X^2$ -plane ($C_{13} = C_{23} = 0$), one concludes that $W_{5,11} = W_{5,22} = W_{5,23} = 0$. Substituting these in the above equations, one concludes that $W_{5,33} = 0$. Therefore, $W_{4,AB} = 0$.

In summary, for the universality constraints to hold one must have

$$(W_{1,A})_B = (W_{2,A})_B = (W_{4,1})_B = (W_{5,A})_B = 0, \quad A, B = 1, 2, 3. \quad (4.39)$$

Using arguments similar to those used in deriving (4.30), one can show that the above constraints imply the following proposition.

Proposition 4.1 *For inhomogeneous incompressible nonlinear transversely isotropic solids with material preferred direction parallel to the X^1 -axis in a Cartesian coordinate system (X^1, X^2, X^3) , Family 0 deformations are universal for any energy function of the following form*

$$W(\mathbf{X}, I_1, I_2, I_4, I_5) = \overline{W}(I_1, I_2, I_4, I_5) + \mathbf{H}(I_1, I_2, I_4, I_5) \cdot \mathbf{X} + \widetilde{W}(X^2, X^3, I_4). \quad (4.40)$$

Remark 4.2 Note that the last term of the energy function in (4.40) has a form identical to that of compressible orthotropic solids (3.34).

4.2 Family 1: Bending, Stretching, and Shearing of a Rectangular Block

Consider a rectangular block and a Cartesian coordinate system (X, Y, Z) with coordinate planes parallel to the faces of the block. In the current configuration cylindrical coordinates (r, θ, z) are used. With respect to these coordinates, the Family 1 deformations have the following representation

$$\begin{aligned} r(X, Y, Z) &= \sqrt{C_1(2X + C_4)}, & \theta(X, Y, Z) &= C_2(Y + C_5), \\ z(X, Y, Z) &= \frac{Z}{C_1 C_2} - C_2 C_3 Y + C_6, \end{aligned} \quad (4.41)$$

where C_1, \dots, C_6 are constants. The right Cauchy-Green strain reads

$$[C_{AB}] = \begin{bmatrix} \frac{C_1}{2X+C_4} & 0 & 0 \\ 0 & C_2^2 [C_1(2X + C_4) + C_3^2] & -\frac{C_3}{C_1} \\ 0 & -\frac{C_3}{C_1} & \frac{1}{C_1^2 C_2^2} \end{bmatrix}, \quad (4.42)$$

and is independent of Y and Z , i.e., \mathbf{C}^b is invariant under the action of $T(2) \subset SE(3)$. In [42] it was assumed that \mathbf{N} has the same symmetry, i.e.,

$$\mathbf{N}(X, Y, Z) = \begin{bmatrix} N^1(X) \\ N^2(X) \\ N^3(X) \end{bmatrix}, \quad (4.43)$$

where $(N^1(X))^2 + (N^2(X))^2 + (N^3(X))^2 = 1$. It was shown that the universal material preferred direction has the following possible forms

$$\mathbf{N} = \begin{bmatrix} \pm 1 \\ 0 \\ 0 \end{bmatrix}, \quad \mathbf{N} = \begin{bmatrix} 0 \\ \cos \psi(X) \\ \pm \sin \psi(X) \end{bmatrix}, \quad (4.44)$$

where $\psi(X)$ is an arbitrary function. Notice that (4.44)₁ corresponds to a uniform distribution of fibers parallel to the X -axis. In the other universal material preferred direction distribution (4.44)₂, for fixed X fibers make an angle $\psi(X)$ with the Y -axis, and are distributed uniformly in the YZ -plane.

In [40] it was shown that the constraints (4.19) imply that

$$\frac{\partial W_1}{\partial Y} = \frac{\partial W_1}{\partial Z} = \frac{\partial W_2}{\partial Y} = \frac{\partial W_2}{\partial Z} = 0. \quad (4.45)$$

The above relations hold for inhomogeneous transversely isotropic solids as well. For the universal material preferred direction (4.44)₁, one can show that⁵

$$\begin{aligned} C_{[ab]}^{4A} &= 0, \text{ for } (A, a, b) = (2, 1, 2) \Rightarrow C_1^2 = 0, \\ C_{[ab]}^{4A} &= 0, \text{ for } (A, a, b) = (3, 1, 2) \Rightarrow C_1^3 C_2 C_3 = 0, \\ C_{[ab]}^{5A} &= 0, \text{ for } (A, a, b) = (2, 1, 2) \Rightarrow [C_1(C_4 + 2X)]^{\frac{3}{2}} C_4 = 0, \\ C_{[ab]}^{5A} &= 0, \text{ for } (A, a, b) = (3, 1, 2) \Rightarrow C_2 C_3 [C_1(C_4 + 2X)]^{\frac{5}{2}} = 0. \end{aligned} \quad (4.46)$$

These constraints cannot be satisfied, and hence

$$\frac{\partial W_4}{\partial Y} = \frac{\partial W_4}{\partial Z} = \frac{\partial W_5}{\partial Y} = \frac{\partial W_5}{\partial Z} = 0. \quad (4.47)$$

Similarly, for the universal material preferred direction (4.44)₂ one has the following constraints:

- $C_{[ab]}^{4A} = 0$, for $(A, a, b) = (2, 1, 2)$ requires that

$$C_2 \sqrt{C_1(C_4 + 2X)} \cos \psi [2(C_4 + 2X)\psi' \sin \psi - 3 \cos \psi] = 0. \quad (4.48)$$

- $C_{[ab]}^{4A} = 0$, for $(A, a, b) = (3, 1, 2)$ implies that

$$C_2 \sqrt{C_1(C_4 + 2X)} [C_1 C_2^2 C_3 \cos^2 \psi + (C_4 + 2X)\psi' \cos 2\psi + \sin 2\psi] = 0. \quad (4.49)$$

- $C_{[ab]}^{5A} = 0$, for $(A, a, b) = (2, 1, 2)$ requires that

$$\begin{aligned} C_2 \sqrt{C_1(C_4 + 2X)} \{ &2(C_4 + 2X)\psi' [C_1 C_2^2 \sin 2\psi (C_1 C_4 + 2C_1 X + C_3^2) + C_3 \cos 2\psi] \\ &- 2C_1 C_2^2 \cos^2 \psi [5C_1(C_4 + 2X) + 3C_3^2] + 3C_3 \sin 2\psi \} = 0. \end{aligned} \quad (4.50)$$

- $C_{[ab]}^{5A} = 0$, for $(A, a, b) = (3, 1, 2)$ requires that

$$\begin{aligned} (C_4 + 2X)^2 \psi' \cos 2\psi &[C_1^2 C_2^4 (C_1(C_4 + 2X) + C_3^2) + 1] \\ &+ (C_4 + 2X) \{ C_1^3 C_2^6 C_3 \cos 2\psi (C_1 C_4 + 2C_1 X + C_3^2) \\ &+ \sin 2\psi [2C_1^3 C_2^4 (C_4 + 2X) + 1] \\ &+ C_1 C_2^2 C_3 [C_1^2 C_2^4 (C_1 C_4 + 2C_1 X + C_3^2) - 2] \} = 0. \end{aligned} \quad (4.51)$$

None of the above constraints can be satisfied, and hence, (4.47) holds for this case as well. From (4.45) and (4.47) one concludes that up to a mechanically inconsequential function of (X, Y, Z) , the energy function must have the form $W = W(X, I_1, I_2, I_4, I_5)$. For energy functions of this form, in (4.19) and (4.20) one only needs to check the symmetry of the terms with $A = 1$, and $A = B = 1$. All those terms are symmetric.

⁵ All the symbolic computations in this paper were performed using Mathematica Version 12.3.0.0, Wolfram Research, Champaign, IL.

Proposition 4.3 For inhomogeneous incompressible nonlinear transversely isotropic solids with any of the universal material preferred directions given in (4.44), Family 1 deformations are universal for any energy function of the form $W = W(X, I_1, I_2, I_4, I_5)$.

4.3 Family 2: Straightening, Stretching, and Shearing of a Sector of a Cylindrical Shell

Consider a sector of a cylindrical shell that is parametrized by cylindrical coordinates (R, Θ, Z) . In the deformed configuration Cartesian coordinates (x, y, z) are used. Family 2 deformations have the following representation

$$\begin{aligned} x(R, \Theta, Z) &= \frac{1}{2} C_1 C_2^2 R^2 + C_4, & y(R, \Theta, Z) &= \frac{\Theta}{C_1 C_2} + C_5, \\ z(R, \Theta, Z) &= \frac{C_3}{C_1 C_2} \Theta + \frac{1}{C_2} Z + C_6, \end{aligned} \quad (4.52)$$

and hence

$$[C_{AB}] = \begin{bmatrix} C_1^2 C_2^4 R^2 & 0 & 0 \\ 0 & \frac{C_3^2 + 1}{C_1^2 C_2^2} & \frac{C_3}{C_1 C_2} \\ 0 & \frac{C_3}{C_1 C_2} & \frac{1}{C_2^2} \end{bmatrix}. \quad (4.53)$$

It is seen that the right Cauchy-Green strain is independent of Θ and Z . In [42] it was assumed that \mathbf{N} has the same symmetry, i.e.,

$$\mathbf{N}(R, \Theta, Z) = \begin{bmatrix} N^1(R) \\ N^2(R) \\ N^3(R) \end{bmatrix}, \quad (4.54)$$

such that $(N^1(R))^2 + R^2(N^2(R))^2 + (N^3(R))^2 = 1$. It was shown that there are two solutions for the universal material preferred direction:

$$\mathbf{N} = \begin{bmatrix} \pm 1 \\ 0 \\ 0 \end{bmatrix}, \quad \mathbf{N} = \begin{bmatrix} 0 \\ \frac{1}{R} \cos \chi(R) \\ \pm \sin \chi(R) \end{bmatrix}, \quad (4.55)$$

where $\chi(R)$ is an arbitrary function. In the case of (4.55)₁ fibers are distributed radially. In the solution (4.55)₂, if $\cos \psi(R) \neq 0$, ± 1 fibers are distributed helically, if $\cos \psi(R) = 0$ they are distributed parallel to the axis of the shell, and if $\cos \psi(R) = \pm 1$ they are concentric circles in the (R, Θ) -plane.

In [40] it was shown that the constraints (4.19) imply that

$$\frac{\partial W_1}{\partial \Theta} = \frac{\partial W_1}{\partial Z} = \frac{\partial W_2}{\partial \Theta} = \frac{\partial W_2}{\partial Z} = 0. \quad (4.56)$$

The above relations hold for inhomogeneous transversely isotropic solids as well. For the universal material preferred direction $(4.55)_1$, one can show that

$$\begin{aligned} C_{[ab]}^{4A} &= 0, \text{ for } (A, a, b) = (2, 1, 2) \Rightarrow C_1^2 C_2^3 = 0, \\ C_{[ab]}^{4A} &= 0, \text{ for } (A, a, b) = (3, 1, 2) \Rightarrow C_1 C_2^3 C_3 = 0, \\ C_{[ab]}^{5A} &= 0, \text{ for } (A, a, b) = (2, 1, 2) \Rightarrow C_1^4 C_2^7 R^2 = 0, \\ C_{[ab]}^{5A} &= 0, \text{ for } (A, a, b) = (3, 1, 2) \Rightarrow C_1^3 C_2^7 C_3 R^2 = 0. \end{aligned} \quad (4.57)$$

These constraints cannot be satisfied, and thus

$$\frac{\partial W_4}{\partial \Theta} = \frac{\partial W_4}{\partial Z} = \frac{\partial W_5}{\partial \Theta} = \frac{\partial W_5}{\partial Z} = 0. \quad (4.58)$$

Similarly, for the universal material preferred direction $(4.55)_2$ one has the following constraints:

- $C_{[ab]}^{4A} = 0$, for $(A, a, b) = (2, 1, 2)$ requires that

$$\cos \chi(R) [R \chi'(R) \sin \chi(R) + \cos \chi(R)] = 0. \quad (4.59)$$

- $C_{[ab]}^{4A} = 0$, for $(A, a, b) = (3, 1, 2)$ implies that

$$\sin 2\chi(R) - 2R \chi'(R) \cos 2\chi(R) = 0. \quad (4.60)$$

- $C_{[ab]}^{5A} = 0$, for $(A, a, b) = (2, 1, 2)$ requires that

$$\begin{aligned} R \chi'(R) [(1 + C_3^2) \sin 2\chi(R) - C_1 C_3 R \cos 2\chi(R)] \\ + \cos \chi(R) [3C_1 C_3 R \sin \chi(R) + 4(1 + C_3^2) \cos \chi(R)] = 0. \end{aligned} \quad (4.61)$$

- $C_{[ab]}^{5A} = 0$, for $(A, a, b) = (3, 1, 2)$ requires that

$$-R(1 + C_1^2 R^2 + C_3^2) \chi'(R) \cos 2\chi(R) + (3 + C_1^2 R^2 + 3C_3^2) \sin 2\chi(R) + 2C_1 C_3 R = 0. \quad (4.62)$$

None of the above constraints can be satisfied,⁶ and thus, (4.58) holds for this case as well. From (4.56) and (4.58) one concludes that up to a mechanically inconsequential function of (R, Θ, Z) , the energy function must have the form $W = W(R, I_1, I_2, I_4, I_5)$. For energy functions of this form, in (4.19) and (4.20) one only needs to check the symmetry of the terms with $A = 1$, and $A = B = 1$. All those terms are symmetric.

Proposition 4.4 *For inhomogeneous incompressible nonlinear transversely isotropic solids with any of the universal material preferred directions given in (4.55), Family 2 deformations are universal for any energy function of the form $W = W(R, I_1, I_2, I_4, I_5)$.*

⁶Note that we are finding the universal inhomogeneities for an arbitrary universal material preferred direction in $(4.55)_2$, and hence, $\cos \chi(R) \neq 0$, in general, i.e., (4.59) cannot be satisfied.

4.4 Family 3: Inflation, Bending, Torsion, Extension, and Shearing of a Sector of an Annular Wedge

Family 3 deformations, with respect to the cylindrical coordinates (R, Θ, Z) and (r, θ, z) in the reference and current configurations, respectively, have the following representation

$$r(R, \Theta, Z) = \sqrt{\frac{R^2}{C_1 C_4 - C_2 C_3} + C_5}, \quad \theta(R, \Theta, Z) = C_1 \Theta + C_2 Z + C_6, \\ z(R, \Theta, Z) = C_3 \Theta + C_4 Z + C_7, \quad (4.63)$$

and hence

$$[C_{AB}] = \begin{bmatrix} \frac{R^2}{K(KC_5 + R^2)} & 0 & 0 \\ 0 & C_3^2 + C_1^2 \left[\frac{R^2}{K} + C_5 \right] & C_1 C_2 \left[\frac{R^2}{K} + C_5 \right] + C_3 C_4 \\ 0 & C_1 C_2 \left[\frac{R^2}{K} + C_5 \right] + C_3 C_4 & C_4^2 + C_2^2 \left[\frac{R^2}{K} + C_5 \right] \end{bmatrix}, \quad (4.64)$$

where $K = C_1 C_4 - C_2 C_3$. Notice that \mathbf{C}^\dagger is independent of Θ and Z . In [42] it was assumed that \mathbf{N} has the same symmetry, i.e.,

$$\mathbf{N}(R, \Theta, Z) = \begin{bmatrix} N^1(R) \\ N^2(R) \\ N^3(R) \end{bmatrix}, \quad (4.65)$$

where $(N^1(R))^2 + R^2(N^2(R))^2 + (N^3(R))^2 = 1$. It was shown that there are two solutions for the universal material preferred direction:

$$\mathbf{N} = \begin{bmatrix} \pm 1 \\ 0 \\ 0 \end{bmatrix}, \quad \mathbf{N} = \begin{bmatrix} 0 \\ \frac{1}{R} \cos \psi(R) \\ \pm \sin \psi(R) \end{bmatrix}, \quad (4.66)$$

where $\psi(R)$ is an arbitrary function.

In [40] it was shown that for this family of deformations constraints (4.19) imply that

$$\frac{\partial W_1}{\partial \Theta} = \frac{\partial W_1}{\partial Z} = \frac{\partial W_2}{\partial \Theta} = \frac{\partial W_2}{\partial Z} = 0. \quad (4.67)$$

The above relations hold for inhomogeneous transversely isotropic solids as well. For the universal material preferred direction (4.66)₁, one can show that

$$C_{[ab]}^{4A} = 0, \text{ for } (A, a, b) = (2, 1, 2) \Rightarrow C_4 (-2C_2 C_3 C_5 + 2C_1 C_4 C_5 + R^2) = 0, \\ C_{[ab]}^{4A} = 0, \text{ for } (A, a, b) = (3, 1, 2) \Rightarrow C_3 (-2C_2 C_3 C_5 + 2C_1 C_4 C_5 + R^2) = 0, \\ C_{[ab]}^{5A} = 0, \text{ for } (A, a, b) = (2, 1, 2) \Rightarrow C_4 (-4C_2 C_3 C_5 + 4C_1 C_4 C_5 + R^2) = 0, \\ C_{[ab]}^{5A} = 0, \text{ for } (A, a, b) = (3, 1, 2) \Rightarrow C_3 (-4C_2 C_3 C_5 + 4C_1 C_4 C_5 + R^2) = 0. \quad (4.68)$$

These constraints cannot be satisfied, and hence

$$\frac{\partial W_4}{\partial \Theta} = \frac{\partial W_4}{\partial Z} = \frac{\partial W_5}{\partial \Theta} = \frac{\partial W_5}{\partial Z} = 0. \quad (4.69)$$

Similarly, for the universal material preferred direction (4.66)₂ $C_{[ab]}^{4A} = 0$, for $(A, a, b) = (2, 1, 2)$ requires that:

$$\begin{aligned}
 & (C_1 C_4 C_5 - C_2 C_3 C_5 + R^2) \left\{ 2C_1^3 C_4^2 C_5 - 4C_1^2 C_2 C_3 C_4 C_5 + C_1^2 C_2 C_4^2 C_5 R \sin 2\psi(R) \right. \\
 & - C_1^2 C_4 R^2 + \cos 2\psi(R) [2C_1^3 C_4^2 C_5 - C_1^2 C_4 (4C_2 C_3 C_5 + R^2) + 2C_1 C_2^2 C_3^2 C_5 \\
 & + C_2^2 C_4 R^4] + 2C_1 C_2^2 C_3^2 C_5 - 2C_1 C_2^2 C_3 C_4 C_5 R \sin 2\psi(R) \\
 & - 2R\psi'(R)(C_2 C_3 - C_1 C_4) (-C_1 C_4 C_5 + C_2 C_3 C_5 - R^2) \\
 & \times [C_2 R \cos 2\psi(R) - C_1 \sin 2\psi(R)] \\
 & - 3C_1 C_2 C_4 R^3 \sin 2\psi(R) + C_2^3 C_3^2 C_5 R \sin 2\psi(R) + C_2^2 C_3 R^3 \sin 2\psi(R) \\
 & \left. - C_2^2 C_4 R^4 \right\} = 0. \tag{4.70}
 \end{aligned}$$

The constraints $C_{[ab]}^{4A} = 0$, for $(A, a, b) = (3, 1, 2)$, $C_{[ab]}^{5A} = 0$, for $(A, a, b) = (2, 1, 2)$, and $C_{[ab]}^{5A} = 0$, for $(A, a, b) = (3, 1, 2)$ require vanishing of some lengthy expressions that we do not report here. None of these four constraints can be satisfied, and thus, (4.69) holds for this case as well. Similar to Family 2 deformations, from (4.67) and (4.69) one concludes that up to a mechanically inconsequential function of (R, Θ, Z) , the energy function must have the form $W = W(R, I_1, I_2, I_4, I_5)$. For energy functions of this form, in (4.19) and (4.20) one only needs to check the symmetry of the terms with $A = 1$, and $A = B = 1$. All those terms are symmetric.

Proposition 4.5 *For inhomogeneous incompressible nonlinear transversely isotropic solids with any of the universal material preferred directions given in (4.66), Family 3 deformations are universal for any energy function of the form $W = W(R, I_1, I_2, I_4, I_5)$.*

Physically, this universal inhomogeneity and directions can be understood as follows: A particular case consists of a single homogeneous cylindrical tube with helical preferred directions. Now, consider a series of encased homogeneous cylindrical tubes in the reference configuration, each with its own helical material preferred directions as described in [16]. The solution from Proposition 4.5 is a continuous version of this problem where the variation in helical fibers and material properties only depends on R .

4.5 Family 4: Inflation/Inversion of a Sector of a Spherical Shell

Family 4 deformations with respect to the spherical coordinates (R, Θ, Φ) and (r, θ, ϕ) in the reference and current configurations, respectively, have the following representation

$$r(R, \Theta, \Phi) = (\pm R^3 + C_1^3), \quad \theta(R, \Theta, \Phi) = \pm \Theta, \quad \phi(R, \Theta, \Phi) = \Phi. \tag{4.71}$$

Thus

$$[C_{AB}] = \begin{bmatrix} \frac{R^4}{(C_1^3 \pm R^3)^{4/3}} & 0 & 0 \\ 0 & (C_1^3 \pm R^3)^{2/3} & 0 \\ 0 & 0 & (C_1^3 \pm R^3)^{2/3} \sin^2 \Theta \end{bmatrix}, \tag{4.72}$$

which can be written as [15]

$$\mathbf{C}^b(\mathbf{X}) = \frac{R^4}{(C_1^3 \pm R^3)^{4/3}} \hat{\mathbf{R}} \otimes \hat{\mathbf{R}} + \frac{(C_1^3 \pm R^3)^{2/3}}{R^2} (\mathbf{1} - \hat{\mathbf{R}} \otimes \hat{\mathbf{R}}), \quad (4.73)$$

where $\mathbf{1}$ is the identity tensor, and $\hat{\mathbf{R}} = \frac{\mathbf{X}}{|\mathbf{X}|}$. This implies that at a given point \mathbf{X} , \mathbf{C}^b is invariant under all those rotations that fix \mathbf{X} . Yavari and Goriely [42] assumed that $\mathbf{N}(\mathbf{X})$ has the same symmetry, i.e., it is invariant under all those rotations that fix \mathbf{X} . Thus, $\mathbf{N}(\mathbf{X})$ is parallel to \mathbf{X} , and knowing that it is a unit vector one concludes that

$$\mathbf{N}(\mathbf{X}) = \pm \frac{\mathbf{X}}{|\mathbf{X}|} = \pm \hat{\mathbf{R}}. \quad (4.74)$$

This means that the universal material preferred direction is radial, i.e., with respect to the spherical coordinates

$$\mathbf{N}(\mathbf{X}) = \begin{bmatrix} \pm 1 \\ 0 \\ 0 \end{bmatrix}. \quad (4.75)$$

In [40] it was shown that for this family of deformations constraints (4.19) imply that

$$\frac{\partial W_1}{\partial \Theta} = \frac{\partial W_1}{\partial \Phi} = \frac{\partial W_2}{\partial \Theta} = \frac{\partial W_2}{\partial \Phi} = 0. \quad (4.76)$$

The above relations hold for inhomogeneous transversely isotropic solids as well. For the universal material preferred direction (4.75), one can show that

$$\begin{aligned} C_{[ab]}^{4A} &= 0, \text{ for } (A, a, b) = (2, 1, 2) \Rightarrow 4C_1^3 R - R^4 = 0, \\ C_{[ab]}^{4A} &= 0, \text{ for } (A, a, b) = (3, 1, 3) \Rightarrow 4C_1^3 R - R^4 = 0, \\ C_{[ab]}^{5A} &= 0, \text{ for } (A, a, b) = (2, 1, 2) \Rightarrow -8C_1^3 R^5 + R^8 = 0, \\ C_{[ab]}^{5A} &= 0, \text{ for } (A, a, b) = (3, 1, 3) \Rightarrow -8C_1^3 R^5 + R^8 = 0. \end{aligned} \quad (4.77)$$

These constraints cannot be satisfied, and hence

$$\frac{\partial W_4}{\partial \Theta} = \frac{\partial W_4}{\partial \Phi} = \frac{\partial W_5}{\partial \Theta} = \frac{\partial W_5}{\partial \Phi} = 0. \quad (4.78)$$

From (4.76) and (4.78) one concludes that up to a mechanically inconsequential function of (R, Θ, Φ) , the energy function must have the form $W = W(R, I_1, I_2, I_4, I_5)$. For any energy function of this form, in (4.19) and (4.20) one only needs to check the symmetry of the terms with $A = 1$, and $A = B = 1$. All those terms are symmetric.

Proposition 4.6 *For inhomogeneous incompressible nonlinear transversely isotropic solids with the universal material preferred directions given in (4.75), Family 4 deformations are universal for any energy function of the form $W = W(R, I_1, I_2, I_4, I_5)$.*

Again, this result can be understood physically as the continuous limit of a finite number of encased homogeneous spherical shells with different material properties.

4.6 Family 5: Inflation, Bending, Extension, and Azimuthal Shearing of an Annular Wedge

Family 5 deformations with respect to the cylindrical coordinates (R, Θ, Z) and (r, θ, z) in the reference and current configurations, respectively, have the following representation

$$r(R, \Theta, Z) = C_1 R, \quad \theta(R, \Theta, Z) = C_2 \log R + C_3 \Theta + C_4, \quad z(R, \Theta, Z) = \frac{1}{C_1^2 C_3} Z + C_5. \quad (4.79)$$

Thus

$$[C_{AB}] = \begin{bmatrix} C_1^2 (C_2^2 + 1) & C_1^2 C_2 C_3 R & 0 \\ C_1^2 C_2 C_3 R & C_1^2 C_3^2 R^2 & 0 \\ 0 & 0 & \frac{1}{C_1^4 C_3^2} \end{bmatrix}, \quad (4.80)$$

which only depends on R . Yavari and Goriely [42] assumed that \mathbf{N} has the same symmetry, i.e.,

$$\mathbf{N}(R, \Theta, Z) = \begin{bmatrix} N^1(R) \\ N^2(R) \\ N^3(R) \end{bmatrix}, \quad (4.81)$$

where $(N^1(R))^2 + (N^2(R))^2 + (N^3(R))^2 = 1$. They obtained the following two solutions for universal material preferred directions

$$\mathbf{N} = \begin{bmatrix} 0 \\ \frac{1}{R} \cos \eta \\ \pm \sin \eta \end{bmatrix}, \quad \mathbf{N} = \begin{bmatrix} \cos \xi \\ \pm \frac{1}{R} \sin \xi \\ 0 \end{bmatrix}, \quad (4.82)$$

for arbitrary constants η , and ξ . Unfortunately, there was a mistake in checking the universality constraints for solution (4.82)₁: This solution satisfies all the universality constraints other than the symmetry of the coefficient of W_4 for $(a, b) = (1, 3)$, which gives $C_2 \cos \eta \sin \eta = 0$. Note that $\sin \eta = 0$ in (4.82)₁ corresponds to $\cos \xi = 0$ in (4.82)₂. This means that the correct set of universal material preferred directions for Family 5 are:

$$\mathbf{N} = \begin{bmatrix} 0 \\ 0 \\ \pm 1 \end{bmatrix}, \quad \mathbf{N} = \begin{bmatrix} \cos \xi \\ \pm \frac{1}{R} \sin \xi \\ 0 \end{bmatrix}, \quad (4.83)$$

for an arbitrary constant ξ .

In [40] it was shown that the for Family 5 deformations constraints (4.19) imply that

$$\frac{\partial W_1}{\partial R} = \frac{\partial W_1}{\partial \Theta} = \frac{\partial W_1}{\partial Z} = \frac{\partial W_2}{\partial R} = \frac{\partial W_2}{\partial \Theta} = \frac{\partial W_2}{\partial Z} = 0. \quad (4.84)$$

The above relations hold for inhomogeneous transversely isotropic solids as well.

For the universal material preferred direction $(4.83)_1$, all the terms in $(4.20)_{(1-9)}$ are symmetric. In the last two sets of equations the following four terms are not symmetric:

$$\begin{aligned} C_{[ab]}^{4AB} &\neq 0, \text{ for } (A, B, a, b) = (1, 3, 1, 3), \\ C_{[ab]}^{4AB} &\neq 0, \text{ for } (A, B, a, b) = (2, 3, 1, 3), \\ C_{[ab]}^{5AB} &\neq 0, \text{ for } (A, B, a, b) = (1, 3, 1, 3), \\ C_{[ab]}^{5AB} &\neq 0, \text{ for } (A, B, a, b) = (2, 3, 1, 3). \end{aligned} \quad (4.85)$$

This implies that

$$\frac{\partial^2 W_4}{\partial R \partial Z} = \frac{\partial^2 W_4}{\partial \Theta \partial Z} = \frac{\partial^2 W_5}{\partial R \partial Z} = \frac{\partial W_5}{\partial \Theta \partial Z} = 0. \quad (4.86)$$

From (4.84) and (4.86) one concludes that $W(\mathbf{X}, I_1, I_2, I_4, I_5) = \bar{W}(I_1, I_2, I_4, I_5) + \tilde{W}(R, \Theta, I_4, I_5) + \hat{W}(Z, I_4, I_5)$. For an energy function of this form, in (4.19) and (4.20) one only needs to check the symmetry of the terms with $A = 1$, and $A = B = 1$. It turns out that all those terms are symmetric.

For the universal material preferred direction $(4.83)_2$, one can show that

$$\begin{aligned} C_{[ab]}^{4A} &= 0, \text{ for } (A, a, b) = (1, 1, 2) \Rightarrow C_1 \cos \xi [C_2 \cos \xi + C_3 \sin \xi] = 0, \\ C_{[ab]}^{4A} &= 0, \text{ for } (A, a, b) = (2, 1, 2) \Rightarrow C_1 [(1 + C_2^2) \cos^2 \xi - C_3^2 \sin^2 \xi] = 0, \\ C_{[ab]}^{4A} &= 0, \text{ for } (A, a, b) = (3, 2, 3) \Rightarrow \\ C_1^3 C_3 &[(-1 + C_2^2) \cos^2 \xi + C_3 \sin \xi (2C_2 \cos \xi + C_3 \sin \xi)] = 0, \\ C_{[ab]}^{5A} &= 0, \text{ for } (A, a, b) = (1, 1, 2) \Rightarrow \\ C_1^3 \{ &2C_2 [1 + C_2^2 + C_3^2 + (1 + C_2^2) \cos 2\xi] + C_3 (1 + 3C_2^2 + C_3^2) \sin 2\xi \} = 0, \\ C_{[ab]}^{5A} &= 0, \text{ for } (A, a, b) = (2, 1, 2) \Rightarrow \\ C_1^3 \{ &[(1 + C_2^2)^2 + C_3^4] \cos 2\xi + (1 + C_2^2 - C_3^2) (1 + C_2^2 + C_3^2 + C_2 C_3 \sin 2\xi) \} \\ &= 0, \\ C_{[ab]}^{5A} &= 0, \text{ for } (A, a, b) = (3, 2, 3) \Rightarrow \\ C_1^6 C_3 \{ &2C_2 [1 + C_2^2 + C_3^2 + (1 + C_2^2) \cos 2\xi] + C_3 (1 + 3C_2^2 + C_3^2) \sin 2\xi \} &= 0. \end{aligned} \quad (4.87)$$

None of the above constraints can be satisfied,⁷ and hence

$$\frac{\partial W_4}{\partial R} = \frac{\partial W_4}{\partial \Theta} = \frac{\partial W_4}{\partial Z} = \frac{\partial W_5}{\partial R} = \frac{\partial W_5}{\partial \Theta} = \frac{\partial W_5}{\partial Z} = 0. \quad (4.88)$$

From (4.84) and (4.88) one concludes that the energy function must be homogeneous. This means that Family 5 deformations are not universal for inhomogeneous incompressible transversely isotropic solids with the universal material preferred directions $(4.83)_2$.

⁷Note that we are finding the universal inhomogeneities of the energy function for an arbitrary member of this class. That means that $\cos \xi \neq 0$, in general, i.e., $(4.87)_1$ cannot be satisfied.

Proposition 4.7 For inhomogeneous incompressible nonlinear transversely isotropic solids with the universal material preferred directions given in (4.83)₁, Family 5 deformations are universal for any energy function of the form $W(\mathbf{X}, I_1, I_2, I_4, I_5) = \overline{W}(I_1, I_2, I_4, I_5) + \overline{W}(R, \Theta, I_4, I_5) + \overline{W}(Z, I_4, I_5)$. Family 5 deformations are not universal for inhomogeneous incompressible transversely isotropic solids with the universal material preferred directions (4.83)₂.

Table 2 summarizes our results for inhomogeneous incompressible transversely isotropic solids.

5 Incompressible Orthotropic Elastic Solids

For inhomogeneous orthotropic solids

$$\xi_a = g_{am} [W_1 b^{mn} - W_2 c^{mn} + W_4 n_1^m n_1^n + W_5 \ell_1^{mn} + W_6 n_2^m n_2^n + W_7 \ell_2^{mn}]_{|n}. \quad (5.1)$$

In order to satisfy the symmetry $\xi_{a|b} = \xi_{b|a}$ for an arbitrary energy function the coefficient of each partial derivative of W must be symmetric. There are five groups of terms. The first four were derived in [42]. In order for this work to be self contained, all the five groups are reported below. The first four groups of terms that must be symmetric for both incompressible and compressible orthotropic solids are:

- i) Nine terms that need to be symmetric for isotropic solids as well:

$$\mathcal{K}_{\text{iso}} = \{1, 2, 11, 22, 12, 111, 222, 112, 122\}. \quad (5.2)$$

- ii) 25 terms associated to \mathbf{N}_1 :

$$\begin{aligned} \mathcal{K}_i = \{4, 5, 44, 55, 14, 15, 24, 25, 45, 444, 555, 114, 115, 124, 125, \\ 144, 145, 155, 224, 225, 244, 245, 255, 445, 455\}. \end{aligned} \quad (5.3)$$

- iii) 25 terms associated to \mathbf{N}_2 :

$$\begin{aligned} \mathcal{K}_i = \{6, 7, 66, 77, 16, 17, 26, 27, 67, 666, 777, 116, 117, 126, 127, \\ 166, 167, 177, 226, 227, 266, 267, 277, 667, 677\}. \end{aligned} \quad (5.4)$$

- iv) 24 terms corresponding to coupling of \mathbf{N}_1 and \mathbf{N}_2 :

$$\begin{aligned} \mathcal{K}_{ii} = \{46, 47, 56, 57, 146, 147, 156, 157, 246, 247, 256, 257, 446, 447, \\ 456, 457, 556, 557, 466, 467, 566, 567, 477, 577\}. \end{aligned} \quad (5.5)$$

- v) 33 terms that correspond to the inhomogeneity of the energy function. 18 of these are identical to those of isotropic (4.19) and transversely isotropic solids (4.20).

In [42] it was noticed that \mathcal{K} and \mathcal{K}_{ii} universality constraints have forms identical to those of \mathcal{K} universality constraints (4.16). This implies that $(\mathbf{N}_1, \mathbf{N}_2, \mathbf{N}_3)$ is universal for orthotropic solids if i) \mathbf{N}_1 , \mathbf{N}_2 , and \mathbf{N}_3 are universal for transversely isotropic solids, and ii) the three pairs $(\mathbf{N}_1, \mathbf{N}_2)$, $(\mathbf{N}_2, \mathbf{N}_3)$, and $(\mathbf{N}_3, \mathbf{N}_1)$ satisfy the \mathcal{K}_{iii} universality constraints. We

Table 2 Universal deformations, universal material preferred directions, and universal inhomogeneities for incompressible transversely isotropic solids for the six known families of universal deformations

Family	Universal deformations	Universal material preferred directions	Universal inhomogeneities
0	$x^a(X) = F^a_A X^A + c^a$	Any constant unit vector \mathbf{N}	$W = \bar{W}(I_1, I_2, I_4, I_5) + \mathbf{H}(I_1, I_2, I_4, I_5) \cdot \mathbf{X} + \tilde{W}(X^2, X^3, I_4)$
1	$\begin{cases} r(X, Y, Z) = \sqrt{C_1(2X + C_4)} \\ \theta(X, Y, Z) = C_2(Y + C_5) \\ z(X, Y, Z) = \frac{Z}{C_1 C_2} - C_2 C_3 Y + C_6 \end{cases}$	$\hat{\mathbf{N}} = \begin{bmatrix} \pm 1 \\ 0 \\ 0 \end{bmatrix}, \quad \hat{\mathbf{N}} = \begin{bmatrix} 0 \\ \cos \psi(X) \\ \pm \sin \psi(X) \end{bmatrix}$	$W = W(X, I_1, I_2, I_4, I_5)$
2	$\begin{cases} x(R, \Theta, Z) = \frac{1}{2} C_1 C_2^2 R^2 + C_4 \\ y(R, \Theta, Z) = \frac{1}{2} C_1 C_2^2 \Theta + C_5 \\ z(R, \Theta, Z) = \frac{C_3}{C_1 C_2} \Theta + \frac{1}{C_2} Z + C_6 \end{cases}$	$\hat{\mathbf{N}} = \begin{bmatrix} \pm 1 \\ 0 \\ 0 \end{bmatrix}, \quad \hat{\mathbf{N}} = \begin{bmatrix} 0 \\ \cos \chi(R) \\ \pm \sin \chi(R) \end{bmatrix}$	$W = W(R, I_1, I_2, I_4, I_5)$
3	$\begin{cases} r(R, \Theta, Z) = \sqrt{\frac{R^2}{C_1 C_4 - C_2 C_3}} + C_5 \\ \theta(R, \Theta, Z) = C_1 \Theta + C_2 Z + C_6 \\ z(R, \Theta, Z) = C_3 \Theta + C_4 Z + C_7 \end{cases}$	$\hat{\mathbf{N}} = \begin{bmatrix} \pm 1 \\ 0 \\ 0 \end{bmatrix}, \quad \hat{\mathbf{N}} = \begin{bmatrix} 0 \\ \cos \chi(R) \\ \pm \sin \chi(R) \end{bmatrix}$	$W = W(R, I_1, I_2, I_4, I_5)$
4	$\begin{cases} r(R, \Theta, \Phi) = (\pm R^3 + C_1^3) \\ \theta(R, \Theta, \Phi) = \pm \Theta \\ \phi(R, \Theta, \Phi) = \Phi \end{cases}$	$\hat{\mathbf{N}} = \begin{bmatrix} \pm 1 \\ 0 \\ 0 \end{bmatrix}$	$W = W(R, I_1, I_2, I_4, I_5)$
5	$\begin{cases} r(R, \Theta, Z) = C_1 R \\ \theta(R, \Theta, Z) = C_2 \log R + C_3 \Theta + C_4 \\ z(R, \Theta, Z) = \frac{1}{C_1^2 C_3} Z + C_5 \end{cases}$	$\hat{\mathbf{N}} = \begin{bmatrix} 0 \\ 0 \\ \pm 1 \end{bmatrix}$	$W = \bar{W}(I_1, I_2, I_4, I_5) + \tilde{W}(R, \Theta, I_4, I_5) + \widehat{W}(Z, I_4, I_5)$

follow the notation introduced in [42], and let $(n, m) = (\mathbf{n}_1, \mathbf{n}_2)$, and $(\ell^{ab}, \kappa^{ab}) = (\ell_1^{ab}, \ell_2^{ab})$. The coefficients of the derivatives of the energy function associated to the set \mathcal{K}_{ii} are:

$$\begin{aligned}\mathcal{A}_{ab}^{46} &= [n_a I_{6,n} n^n]_{|b} + I_{6,b} [n_a n^n]_{|n} + [m_a I_{4,n} m^n]_{|b} + I_{4,b} [m_a m^n]_{|n}, \\ \mathcal{A}_{ab}^{47} &= [n_a I_{7,n} n^n]_{|b} + I_{7,b} [n_a n^n]_{|n} + (\kappa_a^n I_{4,n})_{|b} + \kappa_a^n |n I_{4,b}, \\ \mathcal{A}_{ab}^{56} &= (l_a^n I_{6,n})_{|b} + l_a^n |n I_{6,b} + (m_a I_{5,n} m^n)_{|b} + (m_a m^n)_{|n} I_{5,b}, \\ \mathcal{A}_{ab}^{57} &= (l_a^n I_{7,n})_{|b} + l_a^n |n I_{7,b} + (\kappa_a^n I_{5,n})_{|b} + \kappa_a^n |n I_{5,b},\end{aligned}\quad (5.6)$$

and

$$\begin{aligned}\mathcal{A}_{ab}^{146} &= b_a^n (I_{4,b} I_{6,n} + I_{4,n} I_{6,b}), \\ \mathcal{A}_{ab}^{147} &= b_a^n (I_{4,b} I_{7,n} + I_{4,n} I_{7,b}), \\ \mathcal{A}_{ab}^{156} &= b_a^n (I_{5,b} I_{6,n} + I_{5,n} I_{6,b}), \\ \mathcal{A}_{ab}^{157} &= b_a^n (I_{5,b} I_{7,n} + I_{5,n} I_{7,b}), \\ \mathcal{A}_{ab}^{246} &= c_a^n (I_{4,b} I_{6,n} + I_{4,n} I_{6,b}), \\ \mathcal{A}_{ab}^{247} &= c_a^n (I_{4,b} I_{7,n} + I_{4,n} I_{7,b}), \\ \mathcal{A}_{ab}^{256} &= c_a^n (I_{5,b} I_{6,n} + I_{5,n} I_{6,b}), \\ \mathcal{A}_{ab}^{257} &= c_a^n (I_{5,b} I_{7,n} + I_{5,n} I_{7,b}), \\ \mathcal{A}_{ab}^{446} &= n_a n^n (I_{4,b} I_{6,n} + I_{4,n} I_{6,b}), \\ \mathcal{A}_{ab}^{447} &= n_a n^n (I_{4,b} I_{7,n} + I_{4,n} I_{7,b}), \\ \mathcal{A}_{ab}^{456} &= n_a n^n (I_{5,b} I_{6,n} + I_{5,n} I_{6,b}) + l_a^n (I_{4,b} I_{6,n} + I_{4,n} I_{6,b}), \\ \mathcal{A}_{ab}^{457} &= n_a n^n (I_{5,b} I_{7,n} + I_{5,n} I_{7,b}) + l_a^n (I_{4,b} I_{7,n} + I_{4,n} I_{7,b}), \\ \mathcal{A}_{ab}^{466} &= m_a m^n (I_{4,b} I_{6,n} + I_{4,n} I_{6,b}), \\ \mathcal{A}_{ab}^{467} &= m_a m^n (I_{4,b} I_{7,n} + I_{4,n} I_{7,b}) + \kappa_a^n (I_{4,b} I_{6,n} + I_{4,n} I_{6,b}), \\ \mathcal{A}_{ab}^{477} &= \kappa_a^n (I_{4,b} I_{7,n} + I_{4,n} I_{7,b}), \\ \mathcal{A}_{ab}^{556} &= l_a^n (I_{5,b} I_{6,n} + I_{5,n} I_{6,b}), \\ \mathcal{A}_{ab}^{557} &= l_a^n (I_{5,b} I_{7,n} + I_{5,n} I_{7,b}), \\ \mathcal{A}_{ab}^{566} &= m_a m^n (I_{5,b} I_{6,n} + I_{5,n} I_{6,b}), \\ \mathcal{A}_{ab}^{567} &= m_a m^n (I_{5,b} I_{7,n} + I_{5,n} I_{7,b}) + \kappa_a^n (I_{5,b} I_{6,n} + I_{5,n} I_{6,b}), \\ \mathcal{A}_{ab}^{577} &= \kappa_a^n (I_{5,b} I_{7,n} + I_{5,n} I_{7,b}).\end{aligned}\quad (5.7)$$

For inhomogeneous incompressible orthotropic solids, in addition to the universality constraints (4.19), and (4.20) there are the following 15 extra sets of universality constraints (each term must be symmetric in (ab) for $A = 1, 2, 3$, and $B \geq A$):

$$C_{ab}^{6A} = (F^{-1})^A_n (m_a m^n)_{|b} + (F^{-1})^A_b (m_a m^n)_{|n} + m_a m^n [(F^{-1})^B_b (F^{-1})^A_n]_{,B}$$

$$\begin{aligned}
& - \gamma^m_{\quad nb} (F^{-1})^A_m \Big] , \\
C_{ab}^{7A} &= (F^{-1})^A_n \kappa_a^n |_b + (F^{-1})^A_b \kappa_a^n |_n + \kappa_a^n \left[(F^{-1})^B_b (F^{-1})^A_{n,B} - \gamma^m_{\quad nb} (F^{-1})^A_m \right] , \\
C_{ab}^{16A} &= b_a^n \left[(F^{-1})^A_n I_{6,b} + (F^{-1})^A_b I_{6,n} \right] + m_a m^n \left[(F^{-1})^A_n I_{1,b} + (F^{-1})^A_b I_{1,n} \right] , \\
C_{ab}^{17A} &= b_a^n \left[(F^{-1})^A_n I_{7,b} + (F^{-1})^A_b I_{7,n} \right] + \kappa_a^n \left[(F^{-1})^A_n I_{1,b} + (F^{-1})^A_b I_{1,n} \right] , \\
C_{ab}^{26A} &= -c_a^n \left[(F^{-1})^A_n I_{6,b} + (F^{-1})^A_b I_{6,n} \right] + m_a m^n \left[(F^{-1})^A_n I_{2,b} + (F^{-1})^A_b I_{2,n} \right] , \\
C_{ab}^{27A} &= -c_a^n \left[(F^{-1})^A_n I_{7,b} + (F^{-1})^A_b I_{7,n} \right] + \kappa_a^n \left[(F^{-1})^A_n I_{2,b} + (F^{-1})^A_b I_{2,n} \right] , \\
C_{ab}^{46A} &= n_a n^n \left[(F^{-1})^A_n I_{6,b} + (F^{-1})^A_b I_{6,n} \right] + m_a m^n \left[(F^{-1})^A_n I_{4,b} + (F^{-1})^A_b I_{4,n} \right] , \\
C_{ab}^{47A} &= n_a n^n \left[(F^{-1})^A_n I_{7,b} + (F^{-1})^A_b I_{7,n} \right] + \kappa_a^n \left[(F^{-1})^A_n I_{4,b} + (F^{-1})^A_b I_{4,n} \right] , \\
C_{ab}^{56A} &= \ell_a^n \left[(F^{-1})^A_n I_{6,b} + (F^{-1})^A_b I_{6,n} \right] + m_a m^n \left[(F^{-1})^A_n I_{5,b} + (F^{-1})^A_b I_{5,n} \right] , \\
C_{ab}^{57A} &= \ell_a^n \left[(F^{-1})^A_n I_{7,b} + (F^{-1})^A_b I_{7,n} \right] + \kappa_a^n \left[(F^{-1})^A_n I_{5,b} + (F^{-1})^A_b I_{5,n} \right] , \\
C_{ab}^{66A} &= m_a m^n \left[(F^{-1})^A_n I_{6,b} + (F^{-1})^A_b I_{6,n} \right] , \\
C_{ab}^{67A} &= \kappa_a^n \left[(F^{-1})^A_n I_{6,b} + (F^{-1})^A_b I_{6,n} \right] + m_a m^n \left[(F^{-1})^A_n I_{7,b} + (F^{-1})^A_b I_{7,n} \right] , \\
C_{ab}^{77A} &= \kappa_a^n \left[(F^{-1})^A_n I_{7,b} + (F^{-1})^A_b I_{7,n} \right] , \\
C_{ab}^{6AB} &= m_a m^n \left[(F^{-1})^A_n (F^{-1})^B_b + (F^{-1})^B_n (F^{-1})^A_b \right] , \\
C_{ab}^{7AB} &= \kappa_a^n \left[(F^{-1})^A_n (F^{-1})^B_b + (F^{-1})^B_n (F^{-1})^A_b \right] . \tag{5.8}
\end{aligned}$$

5.1 Family 0

In [42] it was shown that for homogeneous orthotropic solids homogeneous deformations are universal for any three constant unit vectors $(\mathbf{N}_1, \mathbf{N}_2, \mathbf{N}_3)$ that are mutually orthogonal. In the reference configuration we choose the Cartesian coordinates (X^1, X^2, X^3) such that

$$\mathbf{N}_1 = \frac{\partial}{\partial X^1}, \quad \mathbf{N}_2 = \frac{\partial}{\partial X^2}, \quad \mathbf{N}_3 = \frac{\partial}{\partial X^3}. \tag{5.9}$$

The universality constraints still imply (4.39). For homogeneous deformations and constant $(\mathbf{N}_1, \mathbf{N}_2, \mathbf{N}_3)$, only the last two sets of universality constraints in (5.8) are nontrivial, and imply that

$$(W_{6,2})_B = (W_{7,A})_B = 0, \quad A, B = 1, 2, 3. \tag{5.10}$$

Using a fairly lengthy but standard argument (similar to those of §3.2) one can show that the constraints (4.39) and (5.10) imply the following result.

Proposition 5.1 *For inhomogeneous incompressible nonlinear orthotropic solids, Family 0 deformations are universal for any energy function of the following form*

$$\begin{aligned}
W(\mathbf{X}, I_1, I_2, I_4, I_5, I_6, I_7) &= \overline{W}(I_1, I_2, I_4, I_5, I_6, I_7) + \mathbf{H}(I_1, I_2, I_4, I_5, I_6, I_7) \cdot \mathbf{X} \\
&+ \widetilde{W}(X^3, I_4, I_6) + \widehat{W}(X^2, X^3, I_4) + \widehat{W}(X^1, X^3, I_6), \tag{5.11}
\end{aligned}$$

where $(\mathbf{N}_1, \mathbf{N}_2, \mathbf{N}_3)$ are constant unit vectors given in (5.9).

Remark 5.2 Note that the last three terms of the energy function in (5.11) have identical forms to that of compressible orthotropic solids (3.60).

5.2 Family 1

In [42] it was shown that for Family 1 universal deformations the universal material preferred directions are

$$\mathbf{N}_1 = \begin{bmatrix} \pm 1 \\ 0 \\ 0 \end{bmatrix}, \quad \mathbf{N}_2 = \begin{bmatrix} 0 \\ \cos \psi(X) \\ \pm \sin \psi(X) \end{bmatrix}, \quad \mathbf{N}_3 = \begin{bmatrix} 0 \\ \sin \psi(X) \\ \mp \cos \psi(X) \end{bmatrix}, \quad (5.12)$$

where $\psi(X)$ is an arbitrary function. The constraints (4.45) and (4.47) hold for orthotropic solids as well. Similarly, from (5.8)_{1–2} one concludes that

$$\frac{\partial W_6}{\partial Y} = \frac{\partial W_6}{\partial Z} = \frac{\partial W_7}{\partial Y} = \frac{\partial W_7}{\partial Z} = 0. \quad (5.13)$$

All the other universality constraints are satisfied. Therefore, we have the following result.

Proposition 5.3 *For inhomogeneous incompressible nonlinear orthotropic solids with any of the universal material preferred directions given in (5.12), Family 1 deformations are universal for any energy function of the form $W = W(X, I_1, I_2, I_4, I_5, I_6, I_7)$.*

5.3 Families 2 and 3

In [42] it was shown that for Families 2 and 3 the following family of material preferred directions are universal.

$$\mathbf{N}_1 = \begin{bmatrix} \pm 1 \\ 0 \\ 0 \end{bmatrix}, \quad \mathbf{N}_2 = \begin{bmatrix} 0 \\ \frac{\cos \chi(R)}{R} \\ \pm \sin \chi(R) \end{bmatrix}, \quad \mathbf{N}_3 = \begin{bmatrix} 0 \\ \frac{\sin \chi(R)}{R} \\ \mp \cos \chi(R) \end{bmatrix}, \quad (5.14)$$

where $\chi(R)$ is an arbitrary function. The constraints (4.56) and (4.58) still hold. Similarly, from (5.8)_{1–2} one concludes that

$$\frac{\partial W_6}{\partial \Theta} = \frac{\partial W_6}{\partial Z} = \frac{\partial W_7}{\partial \Theta} = \frac{\partial W_7}{\partial Z} = 0. \quad (5.15)$$

All the other universality constraints are satisfied. Thus, we have the following result.

Proposition 5.4 *For inhomogeneous incompressible nonlinear orthotropic solids with any of the universal material preferred directions given in (5.14), Family 2 and 3 deformations are universal for any energy function of the form $W = W(R, I_1, I_2, I_4, I_5, I_6, I_7)$.*

Yavari and Goriely [42] showed that for homogeneous incompressible orthotropic solids Family 4 deformations are not universal. This is the case for inhomogeneous incompressible orthotropic solids as well.

5.4 Family 5

In [42] the following universal material preferred directions were reported.

$$\left\{ \begin{array}{l} \mathbf{N}_1 = \begin{bmatrix} 0 \\ 0 \\ \pm 1 \end{bmatrix}, \quad \mathbf{N}_2 = \begin{bmatrix} \cos \xi \\ \pm \frac{1}{R} \sin \xi \\ 0 \end{bmatrix}, \quad \mathbf{N}_3 = \begin{bmatrix} \sin \xi \\ \mp \frac{1}{R} \cos \xi \\ 0 \end{bmatrix}, \\ \\ \mathbf{N}_1 = \begin{bmatrix} \pm 1 \\ 0 \\ 0 \end{bmatrix}, \quad \mathbf{N}_2 = \begin{bmatrix} 0 \\ \frac{1}{R} \cos \eta \\ \pm \sin \eta \end{bmatrix}, \quad \mathbf{N}_3 = \begin{bmatrix} 0 \\ \frac{1}{R} \sin \eta \\ \mp \cos \eta \end{bmatrix}. \end{array} \right. \quad (5.16)$$

As was mentioned in §4.6, there was a mistake in one of the families of universal material preferred directions. In $(5.16)_2$ either $\cos \eta = 0$, or $\sin \eta = 0$, which are already included in $(5.16)_1$. Therefore, the correct families of universal material preferred directions are (we have relabelled them so that \mathbf{N}_3 is parallel to the Z -axis):

$$\mathbf{N}_1 = \begin{bmatrix} \cos \xi \\ \pm \frac{1}{R} \sin \xi \\ 0 \end{bmatrix}, \quad \mathbf{N}_2 = \begin{bmatrix} \sin \xi \\ \mp \frac{1}{R} \cos \xi \\ 0 \end{bmatrix}, \quad \mathbf{N}_3 = \begin{bmatrix} 0 \\ 0 \\ \pm 1 \end{bmatrix}, \quad (5.17)$$

where ξ is an arbitrary constant.

In [40] it was shown that the for Family 5 deformations constraints (4.19) imply that

$$\frac{\partial W_1}{\partial R} = \frac{\partial W_1}{\partial \Theta} = \frac{\partial W_1}{\partial Z} = \frac{\partial W_2}{\partial R} = \frac{\partial W_2}{\partial \Theta} = \frac{\partial W_2}{\partial Z} = 0. \quad (5.18)$$

The above relations hold for inhomogeneous orthotropic isotropic solids as well. If we check the universality constraints for the pair $(\mathbf{N}_1, \mathbf{N}_2)$ given in (5.17), from §4.6 we know that $W_{4,A} = W_{5,A} = W_{6,A} = W_{7,A} = 0$, and hence the energy function must be uniform:

Proposition 5.5 *For inhomogeneous incompressible nonlinear orthotropic solids Family 5 deformations are not universal.*

Table 3 summarizes our results for inhomogeneous incompressible orthotropic solids.

6 Incompressible Monoclinic Elastic Solids

In the case of monoclinic solids

$$\xi_a = g_{am} \left[W_1 b^{mn} - W_2 c^{mn} + W_4 n_1^m n_1^n + W_5 \ell_1^{mn} + W_6 n_2^m n_2^n + W_7 \ell_2^{mn} + \frac{1}{2} W_8 \ell_3^{mn} \right]_{|n}. \quad (6.1)$$

The universality constraint $\xi_{a|b} = \xi_{b|a}$ forces the coefficient of each partial derivative of W to be symmetric. Yavari and Goriely [42] showed that for monoclinic solids there are an extra 78 terms corresponding to the following set:

$$\mathcal{K}_v = \{8, 18, 19, 28, 29, 48, 49, 58, 59, 68, 69, 78, 79, 88, 89,$$

$$118, 119, 128, 129, 148, 149, 158, 159, 168, 169, 178, 179, 188, 189, 199, 228, 229,$$

Table 3 Universal deformations, universal material preferred directions, and universal inhomogeneities for incompressible orthotropic solids for the six known families of universal deformations

Family	Universal deformations	Universal material preferred directions	Universal inhomogeneities
0	$x^a(X) = F^a_A X^A + c^a$	Any three mutually orthogonal constant unit vectors $(\hat{\mathbf{N}}_1, \hat{\mathbf{N}}_2, \hat{\mathbf{N}}_3)$	$W = \bar{W}(I_1, I_2, I_4, I_5, I_6, I_7) + \mathbf{H}(I_1, I_2, I_4, I_5, I_6, I_7) \cdot \mathbf{X}$ $+ \hat{W}(X^3, I_4, I_6) + \hat{W}(X^2, X^3, I_4) + \hat{W}(X^1, X^3, I_6)$
1	$\begin{cases} r(X, Y, Z) = \sqrt{C_1(2X+C_4)} \\ \theta(X, Y, Z) = C_2(Y+C_5) \\ z(X, Y, Z) = \frac{Z}{C_1C_2} - C_2C_3Y + C_6 \end{cases}$	$\hat{\mathbf{N}}_1 = \begin{bmatrix} \pm 1 \\ 0 \\ 0 \end{bmatrix}, \quad \hat{\mathbf{N}}_2 = \begin{bmatrix} 0 \\ \cos\psi(X) \\ \pm \sin\psi(X) \end{bmatrix}, \quad \hat{\mathbf{N}}_3 = \begin{bmatrix} 0 \\ \sin\psi(X) \\ \mp \cos\psi(X) \end{bmatrix}$	$W = W(X, I_1, I_2, I_4, I_5, I_6, I_7)$
2	$\begin{cases} x(R, \Theta, Z) = \frac{1}{2}C_1C_2^2R^2 + C_4 \\ y(R, \Theta, Z) = \frac{1}{C_1}C_1C_2^2R^2 + C_5 \\ z(R, \Theta, Z) = \frac{C_3}{C_1C_2}\Theta + \frac{1}{C_2}Z + C_6 \end{cases}$	$\hat{\mathbf{N}}_1 = \begin{bmatrix} \pm 1 \\ 0 \\ 0 \end{bmatrix}, \quad \hat{\mathbf{N}}_2 = \begin{bmatrix} 0 \\ \cos\chi(R) \\ \pm \sin\chi(R) \end{bmatrix}, \quad \hat{\mathbf{N}}_3 = \begin{bmatrix} 0 \\ \sin\chi(R) \\ \mp \cos\chi(R) \end{bmatrix}$	$W = W(R, I_1, I_2, I_4, I_5, I_6, I_7)$
3	$\begin{cases} r(R, \Theta, Z) = \sqrt{\frac{R^2}{C_1C_4-C_2C_3}} + C_5 \\ \theta(R, \Theta, Z) = C_1\Theta + C_2Z + C_6 \\ z(R, \Theta, Z) = C_3\Theta + C_4Z + C_7 \end{cases}$	$\hat{\mathbf{N}}_1 = \begin{bmatrix} \pm 1 \\ 0 \\ 0 \end{bmatrix}, \quad \hat{\mathbf{N}}_2 = \begin{bmatrix} 0 \\ \cos\chi(R) \\ \pm \sin\chi(R) \end{bmatrix}, \quad \hat{\mathbf{N}}_3 = \begin{bmatrix} 0 \\ \sin\chi(R) \\ \mp \cos\chi(R) \end{bmatrix}$	$W = W(R, I_1, I_2, I_4, I_5, I_6, I_7)$

$$248, 249, 258, 259, 268, 269, 278, 279, 288, 289, 299, 448, 449, 458, 459, 468, 469, 478, 479, 488, 489, 499, 558, 559, 568, 569, 578, 579, 588, 589, 599, 668, 669, 678, 679, 688, 689, 699, 778, 779, 788, 789, 799, 888, 889, 999\}.$$
(6.2)

We follow the notation in [42] and write $(n, m) = (\mathbf{n}_1, \mathbf{n}_2)$, and $(\ell^{ab}, \kappa^{ab}, q^{ab}) = (\ell_1^{ab}, \ell_2^{ab}, \ell_3^{ab})$. The terms corresponding to the set $\mathcal{K}_{\mathbf{a}\mathbf{b}}$ are:

$$\begin{aligned}
\mathcal{A}_{ab}^8 &= q_a^n |_{nb}, \\
\mathcal{A}_{ab}^{18} &= q_a^n |_n I_{1,b} + (q_a^n I_{1,n})|_b + (b_a^n I_{8,n})|_b + b_a^n |_n I_{8,b}, \\
\mathcal{A}_{ab}^{19} &= (b_a^n I_{9,n})|_b + b_a^n |_n I_{9,b}, \\
\mathcal{A}_{ab}^{28} &= q_a^n |_n I_{2,b} + (q_a^n I_{2,n})|_b - (c_a^n I_{8,n})|_b - c_a^n |_n I_{8,b}, \\
\mathcal{A}_{ab}^{29} &= -(c_a^n I_{9,n})|_b - c_a^n |_n I_{9,b}, \\
\mathcal{A}_{ab}^{48} &= q_a^n |_n I_{4,b} + (q_a^n I_{4,n})|_b + (n_a n^n I_{8,n})|_b + (n_a n^n)|_n I_{8,b}, \\
\mathcal{A}_{ab}^{49} &= (n_a n^n I_{9,n})|_b + (n_a n^n)|_n I_{9,b}, \\
\mathcal{A}_{ab}^{58} &= q_a^n |_n I_{5,b} + (q_a^n I_{5,n})|_b + (\ell_a^n I_{8,n})|_b + \ell_a^n |_n I_{8,b}, \\
\mathcal{A}_{ab}^{59} &= (\ell_a^n I_{9,n})|_b + \ell_a^n |_n I_{9,b}, \\
\mathcal{A}_{ab}^{68} &= q_a^n |_n I_{6,b} + (q_a^n I_{6,n})|_b + (m_a m^n I_{8,n})|_b + (m_a m^n)|_n I_{8,b}, \\
\mathcal{A}_{ab}^{69} &= (m_a m^n I_{9,n})|_b + (m_a m^n)|_n I_{9,b}, \\
\mathcal{A}_{ab}^{78} &= q_a^n |_n I_{7,b} + (q_a^n I_{7,n})|_b + (\kappa_a^n I_{8,n})|_b + \kappa_a^n |_n I_{8,b}, \\
\mathcal{A}_{ab}^{79} &= (\kappa_a^n I_{9,n})|_b + \kappa_a^n |_n I_{9,b}, \\
\mathcal{A}_{ab}^{88} &= q_a^n |_n I_{8,b} + (q_a^n I_{8,n})|_b, \\
\mathcal{A}_{ab}^{89} &= q_a^n |_n I_{9,b} + (q_a^n I_{9,n})|_b, \\
\mathcal{A}_{ab}^{118} &= b_a^n (I_{1,b} I_{8,n} + I_{1,n} I_{8,b}), \\
\mathcal{A}_{ab}^{119} &= b_a^n (I_{1,b} I_{9,n} + I_{1,n} I_{9,b}), \\
\mathcal{A}_{ab}^{128} &= b_a^n (I_{2,b} I_{8,n} + I_{2,n} I_{8,b}) - c_a^n (I_{1,b} I_{8,n} + I_{1,n} I_{8,b}), \\
\mathcal{A}_{ab}^{129} &= b_a^n (I_{2,b} I_{9,n} + I_{2,n} I_{9,b}) - c_a^n (I_{1,b} I_{9,n} + I_{1,n} I_{9,b}), \\
\mathcal{A}_{ab}^{148} &= b_a^n (I_{4,b} I_{8,n} + I_{4,n} I_{8,b}) + n_a n^n (I_{1,b} I_{8,n} + I_{1,n} I_{8,b}), \\
\mathcal{A}_{ab}^{149} &= b_a^n (I_{4,b} I_{9,n} + I_{4,n} I_{9,b}) + n_a n^n (I_{1,b} I_{9,n} + I_{1,n} I_{9,b}), \\
\mathcal{A}_{ab}^{158} &= b_a^n (I_{5,b} I_{8,n} + I_{5,n} I_{8,b}) + \ell_a^n (I_{1,b} I_{8,n} + I_{1,n} I_{8,b}), \\
\mathcal{A}_{ab}^{159} &= b_a^n (I_{5,b} I_{9,n} + I_{5,n} I_{9,b}) + \ell_a^n (I_{1,b} I_{9,n} + I_{1,n} I_{9,b}), \\
\mathcal{A}_{ab}^{168} &= b_a^n (I_{6,b} I_{8,n} + I_{6,n} I_{8,b}) + m_a m^n (I_{1,b} I_{8,n} + I_{1,n} I_{8,b}), \\
\mathcal{A}_{ab}^{169} &= b_a^n (I_{6,b} I_{9,n} + I_{6,n} I_{9,b}) + m_a m^n (I_{1,b} I_{9,n} + I_{1,n} I_{9,b}), \\
\mathcal{A}_{ab}^{178} &= b_a^n (I_{7,b} I_{8,n} + I_{7,n} I_{8,b}) + \kappa_a^n (I_{1,b} I_{8,n} + I_{1,n} I_{8,b}),
\end{aligned}
(6.3)$$

$$\begin{aligned}
\mathcal{A}_{ab}^{179} &= b_a^n (I_{7,b} I_{9,n} + I_{7,n} I_{9,b}) + \kappa_a^n (I_{1,b} I_{9,n} + I_{1,n} I_{9,b}) , \\
\mathcal{A}_{ab}^{188} &= b_a^n I_{8,b} I_{8,n} + q_a^n (I_{1,b} I_{8,n} + I_{1,n} I_{8,b}) , \\
\mathcal{A}_{ab}^{189} &= b_a^n (I_{8,b} I_{9,n} + I_{8,n} I_{9,b}) + q_a^n (I_{1,b} I_{9,n} + I_{1,n} I_{9,b}) , \\
\mathcal{A}_{ab}^{199} &= b_a^n I_{9,b} I_{9,n} , \tag{6.4}
\end{aligned}$$

$$\begin{aligned}
\mathcal{A}_{ab}^{228} &= -c_a^n (I_{2,b} I_{8,n} + I_{2,n} I_{8,b}) , \\
\mathcal{A}_{ab}^{229} &= -c_a^n (I_{2,b} I_{9,n} + I_{2,n} I_{9,b}) , \\
\mathcal{A}_{ab}^{248} &= -c_a^n (I_{4,b} I_{8,n} + I_{4,n} I_{8,b}) + n_a n^n (I_{2,b} I_{8,n} + I_{2,n} I_{8,b}) , \\
\mathcal{A}_{ab}^{249} &= -c_a^n (I_{4,b} I_{9,n} + I_{4,n} I_{9,b}) + n_a n^n (I_{2,b} I_{9,n} + I_{2,n} I_{9,b}) , \\
\mathcal{A}_{ab}^{258} &= -c_a^n (I_{5,b} I_{8,n} + I_{5,n} I_{8,b}) + l_a^n (I_{2,b} I_{8,n} + I_{2,n} I_{8,b}) , \\
\mathcal{A}_{ab}^{259} &= -c_a^n (I_{5,b} I_{9,n} + I_{5,n} I_{9,b}) + l_a^n (I_{2,b} I_{9,n} + I_{2,n} I_{9,b}) , \\
\mathcal{A}_{ab}^{268} &= -c_a^n (I_{6,b} I_{8,n} + I_{6,n} I_{8,b}) + m_a m^n (I_{2,b} I_{8,n} + I_{2,n} I_{8,b}) , \\
\mathcal{A}_{ab}^{269} &= -c_a^n (I_{6,b} I_{9,n} + I_{6,n} I_{9,b}) + m_a m^n (I_{2,b} I_{9,n} + I_{2,n} I_{9,b}) , \\
\mathcal{A}_{ab}^{278} &= -c_a^n (I_{7,b} I_{8,n} + I_{7,n} I_{8,b}) + \kappa_a^n (I_{2,b} I_{8,n} + I_{2,n} I_{8,b}) , \\
\mathcal{A}_{ab}^{279} &= -c_a^n (I_{7,b} I_{9,n} + I_{7,n} I_{9,b}) + \kappa_a^n (I_{2,b} I_{9,n} + I_{2,n} I_{9,b}) , \\
\mathcal{A}_{ab}^{288} &= -c_a^n I_{8,b} I_{8,n} + q_a^n (I_{2,b} I_{8,n} + I_{2,n} I_{8,b}) , \\
\mathcal{A}_{ab}^{289} &= -c_a^n (I_{8,b} I_{9,n} + I_{8,n} I_{9,b}) + q_a^n (I_{2,b} I_{9,n} + I_{2,n} I_{9,b}) , \\
\mathcal{A}_{ab}^{299} &= -c_a^n I_{9,b} I_{9,n} , \tag{6.5}
\end{aligned}$$

$$\begin{aligned}
\mathcal{A}_{ab}^{458} &= n_a n^n (I_{5,b} I_{8,n} + I_{5,n} I_{8,b}) + l_a^n (I_{4,b} I_{8,n} + I_{4,n} I_{8,b}) , \\
\mathcal{A}_{ab}^{459} &= n_a n^n (I_{5,b} I_{9,n} + I_{5,n} I_{9,b}) + l_a^n (I_{4,b} I_{9,n} + I_{4,n} I_{9,b}) , \\
\mathcal{A}_{ab}^{468} &= n_a n^n (I_{6,b} I_{8,n} + I_{6,n} I_{8,b}) + m_a m^n (I_{4,b} I_{8,n} + I_{4,n} I_{8,b}) , \\
\mathcal{A}_{ab}^{469} &= n_a n^n (I_{6,b} I_{9,n} + I_{6,n} I_{9,b}) + m_a m^n (I_{4,b} I_{9,n} + I_{4,n} I_{9,b}) , \\
\mathcal{A}_{ab}^{478} &= n_a n^n (I_{7,b} I_{8,n} + I_{7,n} I_{8,b}) + \kappa_a^n (I_{4,b} I_{8,n} + I_{4,n} I_{8,b}) , \\
\mathcal{A}_{ab}^{479} &= n_a n^n (I_{7,b} I_{9,n} + I_{7,n} I_{9,b}) + \kappa_a^n (I_{4,b} I_{9,n} + I_{4,n} I_{9,b}) , \\
\mathcal{A}_{ab}^{488} &= n_a n^n I_{8,b} I_{8,n} + q_a^n (I_{4,b} I_{8,n} + I_{4,n} I_{8,b}) , \\
\mathcal{A}_{ab}^{489} &= n_a n^n (I_{8,b} I_{9,n} + I_{8,n} I_{9,b}) + q_a^n (I_{4,b} I_{9,n} + I_{4,n} I_{9,b}) , \\
\mathcal{A}_{ab}^{499} &= n_a n^n I_{9,b} I_{9,n} , \\
\mathcal{A}_{ab}^{558} &= l_a^n (I_{5,b} I_{8,n} + I_{5,n} I_{8,b}) , \\
\mathcal{A}_{ab}^{559} &= l_a^n (I_{5,b} I_{9,n} + I_{5,n} I_{9,b}) ,
\end{aligned}$$

$$\begin{aligned}
\mathcal{A}_{ab}^{568} &= \ell_a^n (I_{6,b} I_{8,n} + I_{6,n} I_{8,b}) + m_a m^n (I_{5,b} I_{8,n} + I_{5,n} I_{8,b}) , \\
\mathcal{A}_{ab}^{569} &= \ell_a^n (I_{6,b} I_{9,n} + I_{6,n} I_{9,b}) + m_a m^n (I_{5,b} I_{9,n} + I_{5,n} I_{9,b}) , \\
\mathcal{A}_{ab}^{578} &= \ell_a^n (I_{7,b} I_{8,n} + I_{7,n} I_{8,b}) + \kappa_a^n (I_{5,b} I_{8,n} + I_{5,n} I_{8,b}) , \\
\mathcal{A}_{ab}^{579} &= \ell_a^n (I_{7,b} I_{9,n} + I_{7,n} I_{9,b}) + \kappa_a^n (I_{5,b} I_{9,n} + I_{5,n} I_{9,b}) ,
\end{aligned} \tag{6.6}$$

and

$$\begin{aligned}
\mathcal{A}_{ab}^{588} &= \ell_a^n I_{8,b} I_{8,n} + q_a^n (I_{5,b} I_{8,n} + I_{5,n} I_{8,b}) , \\
\mathcal{A}_{ab}^{589} &= \ell_a^n (I_{8,b} I_{9,n} + I_{8,n} I_{9,b}) + q_a^n (I_{5,b} I_{9,n} + I_{5,n} I_{9,b}) , \\
\mathcal{A}_{ab}^{599} &= \ell_a^n I_{9,b} I_{9,n} , \\
\mathcal{A}_{ab}^{668} &= m_a m^n (I_{6,b} I_{8,n} + I_{6,n} I_{8,b}) , \\
\mathcal{A}_{ab}^{669} &= m_a m^n (I_{6,b} I_{9,n} + I_{6,n} I_{9,b}) , \\
\mathcal{A}_{ab}^{678} &= m_a m^n (I_{7,b} I_{8,n} + I_{7,n} I_{8,b}) + \kappa_a^n (I_{6,b} I_{8,n} + I_{6,n} I_{8,b}) , \\
\mathcal{A}_{ab}^{679} &= m_a m^n (I_{7,b} I_{9,n} + I_{7,n} I_{9,b}) + \kappa_a^n (I_{6,b} I_{9,n} + I_{6,n} I_{9,b}) , \\
\mathcal{A}_{ab}^{688} &= m_a m^n I_{8,b} I_{8,n} + q_a^n (I_{6,b} I_{8,n} + I_{6,n} I_{8,b}) , \\
\mathcal{A}_{ab}^{689} &= m_a m^n (I_{8,b} I_{9,n} + I_{8,n} I_{9,b}) + q_a^n (I_{6,b} I_{9,n} + I_{6,n} I_{9,b}) , \\
\mathcal{A}_{ab}^{699} &= m_a m^n I_{9,b} I_{9,n} , \\
\mathcal{A}_{ab}^{778} &= \kappa_a^n (I_{7,b} I_{8,n} + I_{7,n} I_{8,b}) , \\
\mathcal{A}_{ab}^{779} &= \kappa_a^n (I_{7,b} I_{9,n} + I_{7,n} I_{9,b}) , \\
\mathcal{A}_{ab}^{788} &= \kappa_a^n I_{8,b} I_{8,n} + q_a^n (I_{7,b} I_{8,n} + I_{7,n} I_{8,b}) , \\
\mathcal{A}_{ab}^{789} &= \kappa_a^n (I_{8,b} I_{9,n} + I_{8,n} I_{9,b}) + q_a^n (I_{7,b} I_{9,n} + I_{7,n} I_{9,b}) , \\
\mathcal{A}_{ab}^{799} &= \kappa_a^n I_{9,b} I_{9,n} , \\
\mathcal{A}_{ab}^{888} &= q_a^n I_{8,b} I_{8,n} , \\
\mathcal{A}_{ab}^{889} &= q_a^n (I_{8,b} I_{9,n} + I_{8,n} I_{9,b}) , \\
\mathcal{A}_{ab}^{999} &= q_a^n I_{9,b} I_{9,n} .
\end{aligned} \tag{6.7}$$

For inhomogeneous incompressible monoclinic solids, in addition to the universality constraints (4.19), and (4.20) there are the following 16 extra sets of universality constraints (each term must be symmetric in (ab) for $A = 1, 2, 3$, and $B \geq A$):

$$\begin{aligned}
C_{ab}^{8A} &= (F^{-1})^A_n q_{a|b}^n + (F^{-1})^A_b q_{a|b}^n + q_a^n [(F^{-1})^B_b (F^{-1})^A_{n,B} - \gamma^m_{nb} (F^{-1})^A_m] , \\
C_{ab}^{18A} &= b_a^n [(F^{-1})^A_n I_{8,b} + (F^{-1})^A_b I_{8,n}] + q_a^n [(F^{-1})^A_n I_{1,b} + (F^{-1})^A_b I_{1,n}] , \\
C_{ab}^{19A} &= b_a^n [(F^{-1})^A_n I_{9,b} + (F^{-1})^A_b I_{9,n}] , \\
C_{ab}^{28A} &= -c_a^n [(F^{-1})^A_n I_{8,b} + (F^{-1})^A_b I_{8,n}] + q_a^n [(F^{-1})^A_n I_{2,b} + (F^{-1})^A_b I_{2,n}] , \\
C_{ab}^{29A} &= -c_a^n [(F^{-1})^A_n I_{9,b} + (F^{-1})^A_b I_{9,n}] ,
\end{aligned}$$

$$\begin{aligned}
C_{ab}^{48A} &= n_a n^n \left[(F^{-1})^A{}_n I_{8,b} + (F^{-1})^A{}_b I_{8,n} \right] + q_a^n \left[(F^{-1})^A{}_n I_{4,b} + (F^{-1})^A{}_b I_{4,n} \right], \\
C_{ab}^{49A} &= n_a n^n \left[(F^{-1})^A{}_n I_{9,b} + (F^{-1})^A{}_b I_{9,n} \right], \\
C_{ab}^{58A} &= q_a^n \left[(F^{-1})^A{}_n I_{5,b} + (F^{-1})^A{}_b I_{5,n} \right] + \ell_a^n \left[(F^{-1})^A{}_n I_{8,b} + (F^{-1})^A{}_b I_{8,n} \right], \\
C_{ab}^{59A} &= \ell_a^n \left[(F^{-1})^A{}_n I_{9,b} + (F^{-1})^A{}_b I_{9,n} \right], \\
C_{ab}^{68A} &= m_a m^n \left[(F^{-1})^A{}_n I_{8,b} + (F^{-1})^A{}_b I_{8,n} \right] + q_a^n \left[(F^{-1})^A{}_n I_{6,b} + (F^{-1})^A{}_b I_{6,n} \right], \\
C_{ab}^{69A} &= m_a m^n \left[(F^{-1})^A{}_n I_{9,b} + (F^{-1})^A{}_b I_{9,n} \right], \\
C_{ab}^{78A} &= \kappa_a^n \left[(F^{-1})^A{}_n I_{8,b} + (F^{-1})^A{}_b I_{8,n} \right] + q_a^n \left[(F^{-1})^A{}_n I_{7,b} + (F^{-1})^A{}_b I_{7,n} \right], \\
C_{ab}^{79A} &= \kappa_a^n \left[(F^{-1})^A{}_n I_{9,b} + (F^{-1})^A{}_b I_{9,n} \right], \\
C_{ab}^{88A} &= q_a^n \left[(F^{-1})^A{}_n I_{8,b} + (F^{-1})^A{}_b I_{8,n} \right], \\
C_{ab}^{89A} &= q_a^n \left[(F^{-1})^A{}_n I_{9,b} + (F^{-1})^A{}_b I_{9,n} \right], \\
C_{ab}^{8AB} &= q_a^n \left[(F^{-1})^A{}_n (F^{-1})^B{}_b + (F^{-1})^B{}_n (F^{-1})^A{}_b \right]. \tag{6.8}
\end{aligned}$$

6.1 Family 0

In [42] it was shown that for homogeneous incompressible monoclinic solids homogeneous deformations are universal for any three constant unit vectors $(\mathbf{N}_1, \mathbf{N}_2, \mathbf{N}_3)$ such that \mathbf{N}_1 and \mathbf{N}_2 are non-parallel, and \mathbf{N}_3 is normal to the plane of \mathbf{N}_1 and \mathbf{N}_2 . We assume that the angle between \mathbf{N}_1 and \mathbf{N}_2 is θ ($0 < \theta < \frac{\pi}{2}$), and hence, $g = \mathbf{N}_1 \cdot \mathbf{N}_2 = \cos \theta$. In the reference configuration let us choose the Cartesian coordinates (X^1, X^2, X^3) such that⁸

$$\mathbf{N}_1 = \frac{\partial}{\partial X^1}, \quad \mathbf{N}_2 = \cos \theta \frac{\partial}{\partial X^1} + \sin \theta \frac{\partial}{\partial X^2}, \quad \mathbf{N}_3 = \frac{\partial}{\partial X^3}, \tag{6.9}$$

i.e.,

$$N_1^A = \delta_1^A, \quad N_2^A = \begin{cases} \cos \theta, & A = 1 \\ \sin \theta, & A = 2 \\ 0, & A = 3 \end{cases}. \tag{6.10}$$

For monoclinic solids the constraints (4.39) still hold. Notice that only the last two sets of constraints in (5.8) are nontrivial. The universality constraint (5.8)₁₄ implies that

$$C_{MK} N_2^K N_2^A W_{6,AN} = C_{NK} N_2^K N_2^A W_{6,AM}, \quad M, N = 1, 2, 3. \tag{6.11}$$

Explicitly, we have

$$\begin{aligned}
& (C_{M1} \cos^2 \theta + C_{M2} \cos \theta \sin \theta) W_{6,1N} + (C_{M1} \cos \theta \sin \theta + C_{M2} \sin^2 \theta) W_{6,2N} \\
& = (C_{N1} \cos^2 \theta + C_{N2} \cos \theta \sin \theta) W_{6,1M} + (C_{N1} \cos \theta \sin \theta + C_{N2} \sin^2 \theta) W_{6,2M}. \tag{6.12}
\end{aligned}$$

⁸In order to make the calculations simpler we have chosen $\alpha = 0$ in (3.65).

These are three constraints corresponding to $(M, N) = (1, 2), (1, 3), (2, 3)$, and read

$$\begin{aligned}
 & (C_{12} \cos^2 \theta + C_{22} \cos \theta \sin \theta) W_{6,11} - (C_{11} \cos \theta \sin \theta + C_{12} \sin^2 \theta) W_{6,22} \\
 & + (-C_{11} \cos^2 \theta + C_{22} \sin^2 \theta) W_{6,12} = 0, \\
 & (C_{13} \cos^2 \theta + C_{23} \cos \theta \sin \theta) W_{6,11} + (C_{13} \cos \theta \sin \theta + C_{23} \sin^2 \theta) W_{6,12} \\
 & - (C_{11} \cos^2 \theta + C_{12} \cos \theta \sin \theta) W_{6,13} - (C_{11} \cos \theta \sin \theta + C_{12} \sin^2 \theta) W_{6,23} = 0, \\
 & (C_{13} \cos^2 \theta + C_{23} \cos \theta \sin \theta) W_{6,12} + (C_{13} \cos \theta \sin \theta + C_{23} \sin^2 \theta) W_{6,22} \\
 & - (C_{12} \cos^2 \theta + C_{22} \cos \theta \sin \theta) W_{6,13} - (C_{12} \cos \theta \sin \theta + C_{22} \sin^2 \theta) W_{6,23} = 0. \tag{6.13}
 \end{aligned}$$

Suppose $[C_{AB}]$ is diagonal. From (6.13)₂, one concludes that $\cos \theta W_{6,13} + \sin \theta W_{6,23} = 0$, which must hold for any $\theta \in (0, \frac{\pi}{2})$. This implies that $W_{6,13} = W_{6,23} = 0$. Substituting this back into (6.13)₂ one concludes that $(C_{13} \cos \theta + C_{23} \sin \theta) (\cos \theta W_{6,11} + \sin \theta W_{6,12}) = 0$, which implies that $W_{6,11} = W_{6,12} = 0$. Substituting these into (6.13)₃ one obtains $(C_{13} \cos \theta \sin \theta + C_{23} \sin^2 \theta) W_{6,22} = 0$, which implies that $W_{6,22} = 0$. Therefore, we have shown that

$$(W_{6,1})_A = (W_{6,2})_A = 0, \quad A = 1, 2, 3. \tag{6.14}$$

The universality constraint (5.8)₁₅ implies that

$$\begin{aligned}
 & (C_{M1} \cos \theta + C_{M2} \sin \theta) (C_1^K \cos \theta W_{7,KN} + C_2^K \sin \theta W_{7,KN}) \\
 & + (C_{MK} C_1^K \cos \theta + C_{MK} C_2^K \sin \theta) (\cos \theta W_{7,1N} + \sin \theta W_{7,2N}), \tag{6.15}
 \end{aligned}$$

is symmetric in (MN) . For $M = 1, N = 3$, and diagonal $[C_{AB}]$, the universality constraint is simplified to read

$$C_{11} (2 \cos \theta W_{7,13} + \sin \theta W_{7,23}) + C_{22} \sin \theta W_{7,23} = 0. \tag{6.16}$$

This must hold for arbitrary C_{11} and C_{22} , and hence, $W_{7,13} = W_{7,23} = 0$. Substituting this back into the universality constraint and considering simple shear deformations for which $C_{12} = C_{13} = 0$, one concludes that $\cos \theta W_{7,11} + 2 \sin \theta W_{7,12} = 0$, which must hold for an arbitrary θ . Thus, $W_{7,11} = W_{7,12} = 0$. Substituting these back into the constraint for simple shear, one concludes that $W_{7,33} = 0$. For $M = 2, N = 3$, and simple shear deformations for which $C_{12} = C_{13} = 0$, the universality constraint is simplified to read: $C_{23} (2C_{22} + C_{33}) \sin^2 \theta W_{7,22} = 0$, which implies that $W_{7,22} = 0$. Therefore, we have concluded that $W_{7,AB} = (W_{7,A})_B = 0, A, B = 1, 2, 3$.

For homogeneous deformations and uniform material preferred directions only the last set of constraints in (6.8) are non-trivial and are rewritten in terms of the referential quantities as (for $K, N = 1, 2, 3$)

$$\begin{aligned}
 & C_{MN} [N_1^M N_2^A \delta_K^B + N_2^M N_1^B \delta_K^A + N_1^M N_2^B \delta_K^A + N_2^M N_1^A \delta_K^B] W_{8,AB} \\
 & = C_{MK} [N_1^M N_2^A \delta_N^B + N_2^M N_1^B \delta_N^A + N_1^M N_2^B \delta_N^A + N_2^M N_1^A \delta_N^B] W_{8,AB}. \tag{6.17}
 \end{aligned}$$

Thus, we have

$$\begin{aligned}
 & C_{1N} (\cos \theta W_{8,1K} + \sin \theta W_{8,2K}) + (C_{N1} \cos \theta + C_{N2} \sin \theta) W_{8,1K} \\
 & = C_{1K} (\cos \theta W_{8,1N} + \sin \theta W_{8,2N}) + (C_{K1} \cos \theta + C_{K2} \sin \theta) W_{8,1N}. \tag{6.18}
 \end{aligned}$$

Equation (6.18) are three constraints corresponding to $(K, N) = (1, 2)$, $(1, 3)$, and $(2, 3)$, and read

$$\begin{aligned} (2C_{12} \cos \theta + C_{22} \sin \theta) W_{8,11} - 2C_{11} \cos \theta W_{8,12} - C_{11} \sin \theta W_{8,22} &= 0, \\ (2C_{13} \cos \theta + C_{23} \sin \theta) W_{8,11} + C_{13} \sin \theta W_{8,12} - (2C_{11} \cos \theta + C_{12} \sin \theta) W_{8,13} \\ - C_{11} \sin \theta W_{8,23} &= 0, \\ (2C_{13} \cos \theta + C_{23} \sin \theta) W_{8,12} - (2C_{12} \cos \theta + C_{22} \sin \theta) W_{8,13} + C_{13} \sin \theta W_{8,22} \\ - C_{12} \sin \theta W_{8,23} &= 0. \end{aligned} \quad (6.19)$$

The above constraints need to be satisfied for an arbitrary matrix $[C_{AB}]$ with unit determinant. For simple shear in the $X^2 X^3$ -plane ($C_{12} = C_{13} = 0$), (6.19)₃ gives $C_{23} \sin \theta W_{8,12} - C_{22} \sin \theta W_{8,13} = 0$, which must hold for arbitrary C_{23} , and hence $W_{8,12} = W_{8,13} = 0$. Thus, (6.19) is simplified to read

$$\begin{aligned} (2C_{12} \cos \theta + C_{22} \sin \theta) W_{8,11} - C_{11} \sin \theta W_{8,22} &= 0, \\ (2C_{13} \cos \theta + C_{23} \sin \theta) W_{8,11} - C_{11} \sin \theta W_{8,23} &= 0, \\ C_{13} \sin \theta W_{8,22} - C_{12} \sin \theta W_{8,23} &= 0. \end{aligned} \quad (6.20)$$

For simple shear in the $X^1 X^2$ -plane ($C_{13} = C_{23} = 0$), (6.20)₂ gives $C_{11} \sin \theta W_{8,23} = 0$, which implies that $W_{8,23} = 0$. Thus

$$\begin{aligned} (2C_{12} \cos \theta + C_{22} \sin \theta) W_{8,11} - C_{11} \sin \theta W_{8,22} &= 0, \\ (2C_{13} \cos \theta + C_{23} \sin \theta) W_{8,11} &= 0, \\ C_{13} \sin \theta W_{8,22} &= 0. \end{aligned} \quad (6.21)$$

The last two equations imply that $W_{8,11} = W_{8,22} = 0$. Thus, (6.19) implies that $(W_{8,1})_A = (W_{8,2})_A = 0$, $A = 1, 2, 3$.

In summary, the universality constraints give us the following

$$\begin{aligned} (W_{1,A})_B &= (W_{2,A})_B = (W_{5,A})_B = (W_{7,A})_B = 0, & A, B &= 1, 2, 3, \\ (W_{4,1})_A &= (W_{6,1})_A = (W_{6,2})_A = (W_{8,1})_A = (W_{8,2})_A = 0, & A &= 1, 2, 3. \end{aligned} \quad (6.22)$$

Using a lengthy but standard argument (similar to those of §3.2) one can show that the constraints (6.22) imply the following result.

Proposition 6.1 *For inhomogeneous incompressible nonlinear monoclinic solids, Family 0 deformations are universal for any energy function of the following form*

$$\begin{aligned} W(\mathbf{X}, I_1, I_2, I_4, I_5, I_6, I_7, I_8, I_9) &= \overline{W}(I_1, I_2, I_4, I_5, I_6, I_7, I_8, I_9) \\ &+ \mathbf{H}(I_1, I_2, I_4, I_5, I_6, I_7, I_8, I_9) \cdot \mathbf{X} \\ &+ \widetilde{W}(X^3, I_4, I_6, I_8, I_9), \end{aligned} \quad (6.23)$$

where $(\mathbf{N}_1, \mathbf{N}_2, \mathbf{N}_3)$ are constant unit vectors such that \mathbf{N}_3 is parallel to the Cartesian X^3 -axis.

Remark 6.2 Note that the last term of the energy function in (6.23) has a form identical to that of compressible monoclinic solids (3.84).

6.2 Family 1

In [42] it was shown that for Family 1 deformations of homogeneous incompressible monoclinic solids the universal material preferred directions are

$$\hat{\mathbf{N}}_1 = \begin{bmatrix} 0 \\ \cos \psi_1(X) \\ \pm \sin \psi_1(X) \end{bmatrix}, \quad \hat{\mathbf{N}}_2 = \begin{bmatrix} 0 \\ \cos \psi_2(X) \\ \pm \sin \psi_2(X) \end{bmatrix}, \quad (6.24)$$

where $\psi_1(X)$ and $\psi_2(X)$ are arbitrary functions such that $\psi_1(X) \neq \psi_2(X)$. The constraints (4.45), (4.47), and (5.13) hold for monoclinic solids as well. The constraints $C_{[ab]}^{8A} = 0$, for $(A, a, b) = (2, 1, 2)$ and $(A, a, b) = (3, 1, 2)$, require vanishing of some lengthy expressions that we do not report here. Neither of these two constraints can be satisfied, and hence

$$\frac{\partial W_8}{\partial Y} = \frac{\partial W_8}{\partial Z} = 0. \quad (6.25)$$

All the other universality constraints are satisfied. Therefore, we conclude that $W = \overline{W}(X, I_1, I_2, I_4, I_5, I_6, I_7, I_8, I_9) + \widetilde{W}(X, Y, Z, I_9)$. Noting that the term $\widetilde{W}(X, Y, Z, I_9)$ is mechanically inconsequential, we have proved the following result.

Proposition 6.3 *For inhomogeneous incompressible nonlinear monoclinic solids with any of the universal material preferred directions given in (6.24), Family 1 deformations are universal for any energy function of the form $W = W(X, I_1, I_2, I_4, I_5, I_6, I_7, I_8, I_9)$.*

6.3 Families 2 and 3

In [42] it was shown that for Family 2 and 3 deformations of homogeneous incompressible monoclinic solids the universal material preferred directions are

$$\hat{\mathbf{N}}_1 = \begin{bmatrix} 0 \\ \cos \chi_1(R) \\ \pm \sin \chi_1(R) \end{bmatrix}, \quad \hat{\mathbf{N}}_2 = \begin{bmatrix} 0 \\ \cos \chi_2(R) \\ \pm \sin \chi_2(R) \end{bmatrix}, \quad (6.26)$$

where $\chi_1(R) \neq \chi_2(R)$ are arbitrary functions.

For monoclinic solids, the constraints (4.56), (4.58), and (5.15) still hold. The constraints $C_{[ab]}^{8A} = 0$, for $(A, a, b) = (2, 1, 2)$ and $(A, a, b) = (3, 1, 2)$, require vanishing of some lengthy expressions that we do not report here. Neither of these two constraints can be satisfied, and hence

$$\frac{\partial W_8}{\partial \Theta} = \frac{\partial W_8}{\partial Z} = 0. \quad (6.27)$$

All the other universality constraints are satisfied. Therefore we conclude that $W = \overline{W}(R, I_1, I_2, I_4, I_5, I_6, I_7, I_8, I_9) + \widetilde{W}(R, \Theta, Z, I_9)$. Noting that the term $\widetilde{W}(R, \Theta, Z, I_9)$ is mechanically inconsequential, we have proved the following result.

Proposition 6.4 *For inhomogeneous incompressible nonlinear monoclinic solids with any of the universal material preferred directions given in (6.26), Family 2 and 3 deformations are universal for any energy function of the form $W = W(R, I_1, I_2, I_4, I_5, I_6, I_7, I_8, I_9)$.*

Yavari and Goriely [42] showed that for homogeneous incompressible monoclinic solids Family 4 deformations are not universal. This is the case for inhomogeneous incompressible monoclinic solids as well.

6.4 Family 5

In [42] the following universal material preferred directions were reported:

$$\text{Class (i)}: \quad \hat{\mathbf{N}}_1 = \begin{bmatrix} \cos \xi_1 \\ \pm \sin \xi_1 \\ 0 \end{bmatrix}, \quad \hat{\mathbf{N}}_2 = \begin{bmatrix} \cos \xi_2 \\ \pm \sin \xi_2 \\ 0 \end{bmatrix}, \quad \xi_1 \neq \xi_2, \quad (6.28)$$

$$\text{Class (ii)}: \quad \hat{\mathbf{N}}_1 = \begin{bmatrix} 0 \\ \pm 1 \\ 0 \end{bmatrix}, \quad \hat{\mathbf{N}}_2 = \begin{bmatrix} 0 \\ \cos \eta \\ \pm \sin \eta \end{bmatrix}, \quad \sin \eta \neq 0, \quad (6.29)$$

$$\text{Class (iii)}: \quad \hat{\mathbf{N}}_1 = \begin{bmatrix} 0 \\ 0 \\ \pm 1 \end{bmatrix}, \quad \hat{\mathbf{N}}_2 = \begin{bmatrix} 0 \\ \cos \eta \\ \pm \sin \eta \end{bmatrix}, \quad \cos \eta \neq 0. \quad (6.30)$$

Noting that $\sin \eta \cos \eta = 0$, Classes (ii) and (iii) become unacceptable ($\hat{\mathbf{N}}_1 \cdot \hat{\mathbf{N}}_2 = 0$), and hence the correct universal material preferred directions are:

$$\hat{\mathbf{N}}_1 = \begin{bmatrix} \cos \xi_1 \\ \pm \sin \xi_1 \\ 0 \end{bmatrix}, \quad \hat{\mathbf{N}}_2 = \begin{bmatrix} \cos \xi_2 \\ \pm \sin \xi_2 \\ 0 \end{bmatrix}, \quad \xi_1 \neq \xi_2. \quad (6.31)$$

This means that the material preferred directions are two families of fibers that are parallel to the (R, Θ) plane and are distributed uniformly in two distinct fixed directions.

In [40] it was shown that the for Family 5 deformations constraints (4.19) imply that

$$\frac{\partial W_1}{\partial R} = \frac{\partial W_1}{\partial \Theta} = \frac{\partial W_1}{\partial Z} = \frac{\partial W_2}{\partial R} = \frac{\partial W_2}{\partial \Theta} = \frac{\partial W_2}{\partial Z} = 0. \quad (6.32)$$

The above relations hold for inhomogeneous monoclinic solids as well. As was shown in §4.6 the universality constraints (4.20) imply that $W_{4,A} = W_{5,A} = W_{6,A} = W_{7,A} = 0$. For the universal material preferred direction (6.31), one can show that

$$C_{[ab]}^{8A} = 0, \text{ for } (A, a, b) = (1, 1, 2) \Rightarrow$$

$$C_1^3 \left\{ C_3 \sin \xi_1 [(1 + C_2^2) \cos \xi_2 + C_2 C_3 \sin \xi_2] \right. \\ \left. + \cos \xi_1 [C_2 (2 + 2C_2^2 + C_3^2) \cos \xi_2 + C_3 (2C_2^2 + C_3^2) \sin \xi_2] \right\} = 0,$$

$$C_{[ab]}^{8A} = 0, \text{ for } (A, a, b) = (2, 1, 2) \Rightarrow$$

$$C_1^3 \left\{ \cos \xi_1 [(-2 + C_2^2(-6 - 4C_2^2 + C_3^2)) \cos \xi_2 \right. \\ \left. + C_2 C_3(-2 - 4C_2^2 + C_3^2) \sin \xi_2] \right. \\ \left. + C_3 \sin \xi_1 [C_2 (1 + C_2^2 + 6C_3^2) \cos \xi_2 + C_3 (C_2^2 + 6C_3^2) \sin \xi_2] \right\} = 0,$$

$$C_{[ab]}^{8A} = 0, \text{ for } (A, a, b) = (3, 2, 3) \Rightarrow$$

$$C_1^6 C_3 \left\{ C_3 \sin \xi_1 \left[(1 + C_2^2) \cos \xi_2 + C_2 C_3 \sin \xi_2 \right] \right. \\ \left. + \cos \xi_1 \left[C_2 (2 + 2C_2^2 + C_3^2) \cos \xi_2 + C_3 (2C_2^2 + C_3^2) \sin \xi_2 \right] \right\} = 0. \quad (6.33)$$

None of the above constraints can be satisfied, and hence

$$\frac{\partial W_8}{\partial R} = \frac{\partial W_8}{\partial \Theta} = \frac{\partial W_8}{\partial Z}. \quad (6.34)$$

In summary, we have proved the following result.

Proposition 6.5 *For inhomogeneous incompressible nonlinear monoclinic solids Family 5 deformations are not universal.*

Table 4 summarizes our results for inhomogeneous incompressible monoclinic solids.

7 Concluding Remarks

In this paper we studied universal deformations in inhomogeneous anisotropic bodies. Equilibrium equations in the absence of body forces, and arbitrariness of energy functions in a given class of materials impose certain constraints that we call *universality constraints*. We observed that the universality constraints of inhomogeneous solids include those of the corresponding homogeneous solids. In other words, for a given class of materials universal deformations and universal material preferred directions are determined by the universality constraints of the corresponding homogeneous solids. Universal inhomogeneities (position dependence of the energy function) are those inhomogeneities that are consistent with the universality constraints. We characterized the universal inhomogeneities for inhomogeneous compressible transversely isotropic, orthotropic, and monoclinic solids. In the case of inhomogeneous incompressible solids, for each of the six known families of universal deformations, and material preferred directions we characterized the corresponding universal inhomogeneities for inhomogeneous incompressible transversely isotropic, orthotropic, and monoclinic solids. Table 1 summarizes our results for inhomogeneous compressible transversely isotropic, orthotropic, and monoclinic solids. Tables 2, 3, and 4 summarize our results for inhomogeneous incompressible transversely isotropic, orthotropic, and monoclinic solids, respectively.

This classification of universal solutions concludes our universal program for hyperelastic materials. It provides a complete collection of solutions that can be used for applications and can be systematically analyzed by stability methods to look for the existence of nearby solutions. In our construction for incompressible solids we have assumed that the choice of material preferred directions is consistent with the underlying symmetries of the deformation (e.g., radial fibers for radial deformations). Therefore, our results do not preclude the existence of other universal solutions that would not preserve the underlying symmetry of the deformations. However, we believe that these solutions are unlikely to exist and we conjecture that this classification, like the cases of isotropic incompressible solids, and isotropic anelastic solids is complete.

Table 4 Universal deformations, universal material preferred directions, and universal inhomogeneities for incompressible monoclinic solids for the six known families of universal deformations. For inhomogeneous monoclinic solids Family 4 and Family 5 deformations are not universal. Also, note that $\hat{\mathbf{N}}_3$ is normal to the plane of $\hat{\mathbf{N}}_1$ and $\hat{\mathbf{N}}_2$

Family	Universal deformations	Universal material preferred directions	Universal inhomogeneities
0	$x^a(X) = F_A^a X^A + c^a$	Any two non-parallel constant unit vectors $\hat{\mathbf{N}}_1$ and $\hat{\mathbf{N}}_2$	$W = \overline{W}(I_1, I_2, I_4, I_5, I_6, I_7, I_8, I_9)$ $+ \mathbf{H}(I_1, I_2, I_4, I_5, I_6, I_7, I_8, I_9) \cdot \mathbf{X}$ $+ \widetilde{W}(X^3, I_4, I_6, I_8, I_9)$
1	$\begin{cases} r(X, Y, Z) = \sqrt{C_1}(2X + C_4) \\ \theta(X, Y, Z) = C_2(Y + C_5) \\ z(X, Y, Z) = \frac{Z}{C_1 C_2} - C_2 C_3 Y + C_6 \end{cases}$	$\hat{\mathbf{N}}_1 = \begin{bmatrix} 0 \\ \cos \psi_1(X) \\ \pm \sin \psi_1(X) \end{bmatrix}, \quad \hat{\mathbf{N}}_2 = \begin{bmatrix} 0 \\ \cos \psi_2(X) \\ \pm \sin \psi_2(X) \end{bmatrix}$	$W = W(X, I_1, I_2, I_4, I_5, I_6, I_7, I_8, I_9)$
2	$\begin{cases} x(R, \Theta, Z) = \frac{1}{2} C_1 C_2^2 R^2 + C_4 \\ y(R, \Theta, Z) = \frac{C_1}{C_2} + C_5 \\ z(R, \Theta, Z) = \frac{C_3}{C_1 C_2} \Theta + \frac{1}{C_2} Z + C_6 \end{cases}$	$\hat{\mathbf{N}}_1 = \begin{bmatrix} 0 \\ \cos \chi_1(R) \\ \pm \sin \chi_1(R) \end{bmatrix}, \quad \hat{\mathbf{N}}_2 = \begin{bmatrix} 0 \\ \cos \chi_2(R) \\ \pm \sin \chi_2(R) \end{bmatrix}, \quad \chi_1(R) \neq \chi_2(R)$	$W = W(R, I_1, I_2, I_4, I_5, I_6, I_7, I_8, I_9)$
3	$\begin{cases} r(R, \Theta, Z) = \sqrt{\frac{R^2}{C_1 C_4 - C_2 C_3}} + C_5 \\ \theta(R, \Theta, Z) = C_1 \Theta + C_2 Z + C_6 \\ z(R, \Theta, Z) = C_3 \Theta + C_4 Z + C_7 \end{cases}$	$\hat{\mathbf{N}}_1 = \begin{bmatrix} 0 \\ \cos \chi_1(R) \\ \pm \sin \chi_1(R) \end{bmatrix}, \quad \hat{\mathbf{N}}_2 = \begin{bmatrix} 0 \\ \cos \chi_2(R) \\ \pm \sin \chi_2(R) \end{bmatrix}, \quad \chi_1(R) \neq \chi_2(R)$	$W = W(R, I_1, I_2, I_4, I_5, I_6, I_7, I_8, I_9)$

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References

1. Adkins, J.E.: Finite deformation of materials exhibiting curvilinear aeolotropy. *Proc. R. Soc. Lond. Ser. A* **229**(1176), 119–134 (1955)
2. Adkins, J.E.: Some general results in the theory of large elastic deformations. *Proc. R. Soc. Lond. Ser. A* **231**(1184), 75–90 (1955)
3. Demirkoparan, H., Pence, T.J.: Swelling of an internally pressurized nonlinearly elastic tube with fiber reinforcing. *Int. J. Solids Struct.* **44**(11–12), 4009–4029 (2007)
4. Demirkoparan, H., Pence, T.J.: Magic angles for fiber reinforcement in rubber-elastic tubes subject to pressure and swelling. *Int. J. Non-Linear Mech.* **68**, 87–95 (2015)
5. Doyle, T.C., Ericksen, J.L.: Nonlinear elasticity. *Adv. Appl. Mech.* **4**, 53–115 (1956)
6. Dunwoody, J.: On a class of controllable deformations of isotropic incompressible elastic solids with simple material inhomogeneity. *IMA J. Appl. Math.* **70**(1), 64–79 (2005)
7. Dunwoody, J.: On a class of controllable deformations of isotropic incompressible elastic solids with simple material inhomogeneity: II. *IMA J. Appl. Math.* **70**(6), 937–953 (2005)
8. Ericksen, J.L.: Deformations possible in every isotropic, incompressible, perfectly elastic body. *Z. Angew. Math. Phys.* **5**(6), 466–489 (1954)
9. Ericksen, J.L.: Deformations possible in every compressible, isotropic, perfectly elastic material. *Stud. Appl. Math.* **34**(1–4), 126–128 (1955)
10. Ericksen, J.L., Rivlin, R.S.: Large elastic deformations of homogeneous anisotropic materials. *J. Ration. Mech. Anal.* **3**, 281–301 (1954)
11. Fosdick, R.L.: Remarks on Compatibility. *Modern Developments in the Mechanics of Continua*, pp. 109–127. Academic Press, New York (1966)
12. Golgoon, A., Yavari, A.: Nonlinear elastic inclusions in anisotropic solids. *J. Elast.* **130**(2), 239–269 (2018)
13. Golgoon, A., Yavari, A.: Line and point defects in nonlinear anisotropic solids. *Z. Angew. Math. Phys.* **69**(3), 1–28 (2018)
14. Golgoon, A., Yavari, A.: On Hashin's hollow cylinder and sphere assemblages in anisotropic nonlinear elasticity. *J. Elast.* **146**(1), 65–82 (2021)
15. Goodbrake, C., Yavari, A., Goriely, A.: The anelastic Ericksen problem: Universal deformations and universal eigenstrains in incompressible nonlinear anelasticity. *J. Elast.* **142**(2), 291–381 (2020)
16. Goriely, A.: *The Mathematics and Mechanics of Biological Growth*. Springer, New York (2017)
17. Goriely, A., Tabor, M.: Rotation, inversion and perversion in anisotropic elastic cylindrical tubes and membranes. *Proc. R. Soc. Lond. Ser. A* **469**(2153), 20130011 (2013)
18. Gurtin, M.E.: The linear theory of elasticity. In: *Handbuch der Physik, Band VIa/2*. Springer, Berlin (1972)
19. Holzapfel, G.A., Gasser, T.C., Ogden, R.W.: A new constitutive framework for arterial wall mechanics and a comparative study of material models. *J. Elast.* **61**, 1–48 (2000)
20. Klingbeil, W.W., Shield, R.T.: On a class of solutions in plane finite elasticity. *Z. Angew. Math. Phys.* **17**(4), 489–511 (1966)
21. Lu, J., Papadopoulos, P.: A covariant constitutive description of anisotropic non-linear elasticity. *Z. Angew. Math. Phys.* **51**(2), 204–217 (2000)
22. Marsden, J.E., Hughes, T.J.R.: *Mathematical Foundations of Elasticity*. Dover, New York (1994)
23. Melnik, A.V., Goriely, A.: Dynamic fiber reorientation in a fiber-reinforced hyperelastic material. *Math. Mech. Solids* **18**(6), 634–648 (2013)

24. Merodio, J., Ogden, R.W.: Finite deformation elasticity theory. In: Constitutive Modelling of Solid Continua, pp. 17–52. Springer, Berlin (2020)
25. Ogden, R.W.: Non-linear Elastic Deformations. Dover, New York (1984)
26. Petroski, H.J., Carlson, D.E.: Controllable states of elastic heat conductors. *Arch. Ration. Mech. Anal.* **31**, 127–150 (1968)
27. Pucci, E., Rajagopal, K.R., Saccomandi, G.: On the determination of semi-inverse solutions of nonlinear Cauchy elasticity: The not so simple case of anti-plane shear. *Int. J. Eng. Sci.* **88**, 3–14 (2015)
28. Qiu, G.Y., Pence, T.J.: Remarks on the behavior of simple directionally reinforced incompressible nonlinearly elastic solids. *J. Elast.* **49**(1), 1–30 (1997)
29. Rivlin, R.S.: Large elastic deformations of isotropic materials IV. Further developments of the general theory. *Philos. Trans. R. Soc. Lond. A* **241**(835), 379–397 (1948)
30. Rivlin, R.S.: Large elastic deformations of isotropic materials. V. The problem of flexure. *Proc. R. Soc. Lond. Ser. A* **195**(1043), 463–473 (1949)
31. Rivlin, R.S.: A note on the torsion of an incompressible highly elastic cylinder. In: Mathematical Proceedings of the Cambridge Philosophical Society, vol. 45, pp. 485–487. Cambridge University Press, Cambridge (1949)
32. Saccomandi, G.: Universal solutions and relations in finite elasticity. In: Topics in Finite Elasticity, pp. 95–130. Springer, Berlin (2001)
33. Saccomandi, G.: On inhomogeneous deformations in finite thermoelasticity. *IMA J. Appl. Math.* **63**(2), 131–148 (1999)
34. Singh, M., Pipkin, A.C.: Note on Ericksen's problem. *Z. Angew. Math. Phys.* **16**(5), 706–709 (1965)
35. Smith, G.F., Rivlin, R.S.: The strain-energy function for anisotropic elastic materials. *Trans. Am. Math. Soc.* **88**(835), 175–193 (1958)
36. Spencer, A.J.M.: The formulation of constitutive equation for anisotropic solids. In: Mechanical Behavior of Anisotropic Solids/Comportement Méchanique des Solides Anisotropes, pp. 3–26. Springer, Berlin (1982)
37. Spencer, A.J.M.: Modelling of finite deformations of anisotropic materials. In: Large Deformations of Solids: Physical Basis and Mathematical Modelling, pp. 41–52. Springer, Berlin (1986)
38. Truesdell, C.: The Elements of Continuum Mechanics. Springer, Berlin (1966)
39. Yavari, A.: Compatibility equations of nonlinear elasticity for non-simply-connected bodies. *Arch. Ration. Mech. Anal.* **209**(1), 237–253 (2013)
40. Yavari, A.: Universal deformations in inhomogeneous isotropic nonlinear elastic solids. *Proc. R. Soc. A* **477**(2253), 20210547 (2021)
41. Yavari, A., Goriely, A.: The anelastic Ericksen problem: Universal eigenstrains and deformations in compressible isotropic elastic solids. *Proc. R. Soc. A* **472**(2196), 20160690 (2016)
42. Yavari, A., Goriely, A.: Universal deformations in anisotropic nonlinear elastic solids. *J. Mech. Phys. Solids* **156**, 104598 (2021)
43. Yavari, A., Goriely, A.: The universal program of linear elasticity. *Math. Mech. Solids*. <https://doi.org/10.1177/108128652210913052022>
44. Yavari, A., Marsden, J.E., Ortiz, M.: On the spatial and material covariant balance laws in elasticity. *J. Math. Phys.* **47**, 85–112 (2006)
45. Yavari, A., Goodbrake, C., Goriely, A.: Universal displacements in linear elasticity. *J. Mech. Phys. Solids* **135**, 103782 (2020)

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