



A highly sensitive, easy-and-rapidly-fabricable microfluidic electrochemical cell with an enhanced three-dimensional electric field

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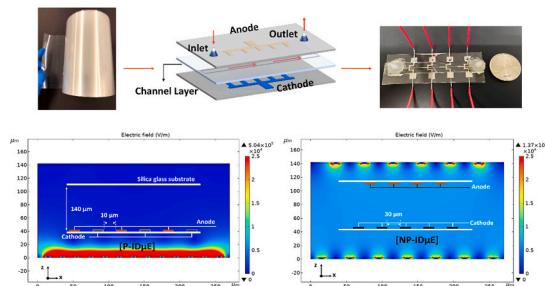
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HIGHLIGHTS

- Simple protocol for constructing non-planar interdigitated microelectrodes (NP-ID μ E).
- Three-dimensional electric field penetration in NP-ID μ E based electrochemical cell (NP- μ FEC).
- Lab-on-a-chip microfluidic platform for heavy metals detection in water matrices.

GRAPHICAL ABSTRACT



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ABSTRACT

An NP- μ FEC is a reusable, novel microfluidic electrochemical cell with multiple non-planar interdigitated microelectrode arrays, minimal sample volume, and enhanced electric field penetration for highly sensitive electrochemical analysis. (i) The NP- μ FEC features spatial 3-electrode architecture, and a small sample volume ($\sim 4 \mu\text{L}$). (ii) Here, $[\text{Fe}(\text{CN})_6]^{3-/4-}$ redox couple are used as an electrochemical reporter. The effects on the electrochemical properties of NP- μ FEC due to the change in the reference electrode (RE) and counter electrode (CE)'s position with respect to the working electrode (WE) position are analyzed. For NP- μ FEC, the position of the RE with respect to the WE does not affect the CV, DPV electrochemical profiles. However, the spacing between the CE and WE plays a significant role. (iii) The enhanced three-dimensional electric field penetration in NP- μ FEC is validated by finite element analysis simulation using COMSOL Multiphysics. (iv) Without electrode surface modifications, NP- μ FEC shows a detection limit (DL) of $\sim 2.54 \times 10^{-6} \text{ M}$ for aqueous $[\text{Fe}(\text{CN})_6]^{3-/4-}$ probe. (v) The DL for Cu^{2+} , Fe^{3+} , and Hg^{2+} are $30.5 \pm 9.5 \mu\text{g L}^{-1}$, $181 \pm 58.5 \mu\text{g L}^{-1}$, and $12.4 \pm 1.95 \mu\text{g L}^{-1}$, respectively, which meets the US Environmental Protection Agency (EPA)'s water contamination level for Cu, Fe, and is close to that for Hg (EPA limits are $1300 \mu\text{g L}^{-1}$, $300 \mu\text{g L}^{-1}$, and $2 \mu\text{g L}^{-1}$, respectively). (vi) Further, using a pressure-sensitive adhesive layer to form the channel and create the NP- μ FEC configuration simplifies the manufacturing process, making it cost-effective and allowing for rapid adoption in any research lab. NP- μ FEC is used to detect heavy metal ions in water. This demonstrates that cost-effective, easy-to-fabricate NP- μ FEC can be a new sensitive electrochemical platform.

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1. Introduction

Rapid, cost-effective, highly sensitive, and label-free detection characteristics of microfluidic electrochemical cells (μ FECs) are receiving increasing attention [1–3]. In the past decades, significant efforts have been made to design and optimize μ FECs' electrode architecture to fabricate analytical devices with high sensitivity, accuracy, and reproducibility [4–6]. Microelectrodes (μ Es), an essential component in μ FECs, offer higher sensitivity than macroelectrodes of conventional size due to their smaller area-edge effects [4]. Various μ E geometries have been evaluated and applied to μ FECs [7–9]. A pair of comb-like metal electrodes on a planar insulating substrate, as shown in Fig. 1(a), is called planar interdigitated microelectrodes (P-ID μ Es). The interdigitated layout of the electrode fingers endow P-ID μ Es with promising advantages, e.g., the fast establishment of the steady-state, low ohmic drop, and increased signal-to-noise ratio [1,4]. However, for the P-ID μ Es, the electric field is chiefly localized near the μ E surface (two-dimensional (2D) electric field), as shown in Fig. 1(b) [10,11]. The 2D electric field limits the penetration of the electric field, leading to a loss in sensitivity for P-ID μ E, specifically for impedance-based sensing [12–14].

Researchers have employed different methodologies to address this problem, such as (i) including nanomaterials to increase the active electrode surface area or (ii) designing elaborate device structures [15–18]. It is shown by Noda et al. that CNT forests on μ Es significantly enhance transducer detection performance [15]. For Noda et al., the P-ID μ E-based transducer sensitivity improved considerably by extending the “active detection area” using carbon spacer/carbon nanostructures. Morallon and co-workers employed a μ FEC with hybrid μ Es comprised of graphene oxide decorated with gold nanoparticles to successfully detect uric acid and ascorbic acid in urine samples at detection limits of 0.62 μ M and 1.4 μ M, respectively [16]. Recently, Bratov et al. introduced the concept of three-dimensional (3D) ID μ E with electrode fingers separated by an insulating SiO_2 barrier [10,17]. This 3D electrode architecture prolongs the current transmission path along the barrier's surface, enhancing the device's sensitivity toward probing reactions of biomolecules attached to the barrier surface. However, all of the above μ FEC and others in the literature require complicated, time-consuming, and expensive device construction processes despite the mentioned advantages [18,19].

Our previous papers demonstrated that packing a 2-electrode non-

planar ID μ E (NP-ID μ E) based μ FEC platform (hereafter NP- μ FEC) allows us to use it as an excellent electrochemical impedance transducer [20,21]. The 2-electrode NP- μ FEC is a sensitive affinity-based impedance sensor that uses electrochemical impedance spectroscopy (EIS), which has enhanced 3D electric field penetration. However, detection of molecules that lack suitable capture probes (like dopamine, uric acid, and heavy metals), EIS cannot be used as the detection mode. Therefore, for detecting these molecules, the electrochemical behavior of NP- μ FEC, specifically in the DC modes (like cyclic voltammetry (CV) and differential pulse voltammetry (DPV)), needs to be characterized and fundamentally examined. Therefore, inspired by our previous 2-electrode design, to check the application capability of NP- μ FEC in the DC detection modes (CV, DPV), a new 3-electrode NP- μ FEC is proposed in this work. Here, a fundamental study using simulations and experiments is undertaken to visualize and demonstrate the new 3-electrode NP- μ FEC as an analytical tool. Unless otherwise noted, the NP- μ FEC appearing hereafter means the 3-electrode NP- μ FEC.

The characteristics of the NP- μ FEC are a small sample volume ($\sim 4 \mu\text{L}$), reusability, easy assembly, and enhanced 3D electric field. Furthermore, to understand and check the applicability of NP- μ FEC, especially for the DC working modes (CV and DPV), a series of electrochemical comparisons between NP- μ FEC and regular P- μ FEC are fundamentally examined. Furthermore, COMSOL modeling of the electric field in both NP- μ FEC and regular P- μ FEC is done to critically examine the effect of the electric field on the electrochemical data. Finally, based on the fundamental understanding of the physicochemical characteristics of NP- μ FEC, an optimized channel height of NP- μ FEC is used for the highly sensitive detection of heavy metal ions in aqueous solutions.

Current microfluidic electrochemical platforms with 3D electrodes suffer from complicated, time-consuming, and expensive construction [10,17]. Here, the NP- μ FEC is proposed that overcomes the current limitations mentioned above. In summary, the NP- μ FEC platform described here has the following advantages over existing platforms in literature:

- (1) **Fabrication:** NP- μ FEC consists of three layers, a top and bottom glass layers decorated with μ E arrays and a middle double-sided polyester-based pressure-sensitive adhesive (PSA) layer with the desired channel pattern ($60 \text{ mm} \times 500 \mu\text{m} \times 140 \mu\text{m}$ in length \times width \times height, respectively) sandwiched between μ E layers. This

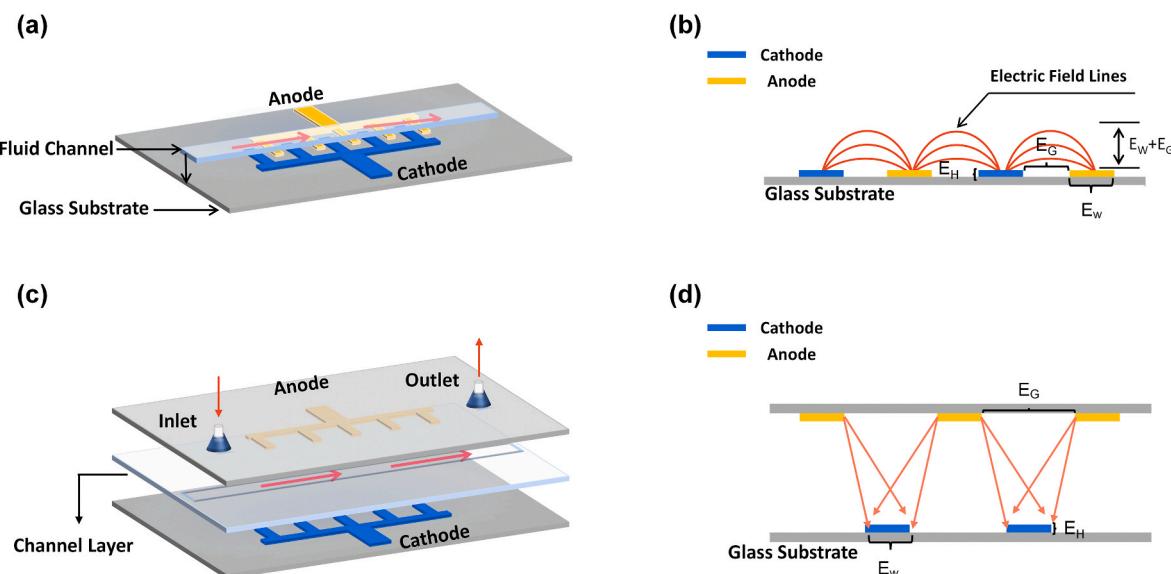


Fig. 1. (a) Schematic diagram of P-ID μ E. (b) Distribution of electric fields within P-ID μ E. Here, E_H , E_W , E_G represents the electrode height, width, and gap between adjacent electrode fingers, respectively. (c) Schematic diagram of the NP-ID μ E and (d) its corresponding electric field distribution.

strategy allows constructing of a μ FEC configuration without extensive fabrication while having a small sample volume ($\sim 4 \mu\text{L}$) [22]. The detailed fabrication protocols of μ E and NP- μ FEC are shown in Figs. S1 and S2, respectively. Further, the PSA layer provides the advantages of (i) a reasonably wide operating temperature window (-40°C – 120°C), (ii) fast and easy electrode assembly, and (iii) excellent reagent-resist properties. Thus, the fabrication process of NP- μ FEC is simple, cost-effective, and accelerates NP- μ FEC adoption as an alternative to P- μ FEC by other research groups.

(2) **3D Electric Field:** An advantage of the NP- μ FEC is allowing a vertical distributed electric field. The spatial orientation of the μ E arrays enables the electric field to penetrate through the whole channel layer. As a result, the electric field is no longer confined to the μ E surface, which tremendously increases the sensitivity of impedance sensors (Fig. 1(d)). Furthermore, any changes between the μ E layers will contribute to the final output signal even without electrode or channel modifications [20,21].

(3) **Fully Integrated:** It is well documented that any alterations and modifications in electrode design, such as the distances between the electrodes (working electrode (WE), counter electrode (CE), and reference electrode (RE)) and their relative positions can significantly alter electrochemical systems and lead to a drop in device performance [23–26]. Furthermore, previous studies demonstrated that an internal RE positioned inside the micro-channel benefits μ FECs' sensitivity because of a smaller ohmic drop [27,28]. Therefore, in this work, the NP- μ FEC with four pairs of NP-ID μ E arrays inserted within a single microfluidic channel is ideally suited for electrochemical characterizations. The electrochemical behavior of the NP- μ FEC is compared against a conventional P- μ FEC using a well-known redox probe potassium Ferri/ferrocyanide ($\text{K}_3/\text{K}_4\text{Fe}(\text{CN})_6$). It is essential to note that the solution is static (no flow) to exclude the contribution of forced convection. Under this static condition, the effect of the distance between the electrodes (WE, CE, and RE) and their final positions on the electrochemical behavior of NP- μ FEC are studied in detail. Finite element analysis (FEA) using COMSOL Multiphysics 5.5 is adapted to visualize the electric field distribution between the NP- μ FEC vs. P- μ FEC. (i) Comparisons between the NP- μ FEC and P- μ FEC demonstrate that the transformation in electrode architecture leads to linear diffusion-controlled redox processes in NP- μ FEC in contrast to a radial diffusion behavior in P- μ FEC. For NP- μ FEC, the RE's position does not affect the CV and DPV electrochemical profiles. However, the spacing between the CE and WE significantly affects the electrochemical behavior. (ii) COMSOL Multiphysics validates enhanced 3D electric field penetration in the NP- μ FEC. (iii) Without any electrode surface modifications (like metal nanoparticles or CNT), the NP- μ FEC shows a detection limit (DL) of $\sim 2.54 \times 10^{-6} \text{ M}$ for aqueous $[\text{Fe}(\text{CN})_6]^{3-/4-}$ probe, which is similar to that of the P- μ FEC ($\sim 1.8 \times 10^{-6} \text{ M}$). Thus it can be concluded that, even though the transition of μ E arrays from planar distribution to non-planar distribution will increase the diffusion distance of ions, this does not significantly influence the μ FEC's performance.

An anomalous lowering of DL is seen with increasing channel height of NP- μ FEC till it reaches a critical height ($420 \mu\text{m}$), beyond which the DL increases with an increase in channel height. Therefore, the DL of Cu^{2+} , Fe^{3+} , and Hg^{2+} was determined to evaluate the potential and performance of NP- μ FEC as an electrochemical platform at $420 \mu\text{m}$ channel height. The DL of NP- μ FEC for Cu^{2+} , Fe^{3+} , and Hg^{2+} are $30.5 \pm 9.5 \mu\text{g L}^{-1}$, $181 \pm 58.5 \mu\text{g L}^{-1}$, and $12.4 \pm 1.95 \mu\text{g L}^{-1}$, respectively, which meets the US Environmental Protection Agency (EPA)'s water contamination level for Cu, Fe and is close to that for Hg ($1300 \mu\text{g L}^{-1}$, $300 \mu\text{g L}^{-1}$, and $2 \mu\text{g L}^{-1}$, respectively). Therefore, this demonstrates that our

cost-effective, easy-to-fabricate NP- μ FEC can be an ideal new electrochemical analytical tool for other research groups.

2. Experimental section

2.1. Materials and chemicals

Potassium chloride (KCl) and potassium Ferri/ferrocyanide ($\text{K}_3/\text{K}_4\text{Fe}(\text{CN})_6$) are purchased from Sigma-Aldrich. Mercury (II) chloride (98+%), Copper (II) chloride dihydrate (99+%), and **Tris (2,2'-bipyridyl)ruthenium(II) chloride hexahydrate** ($\geq 98\%$) are purchased from Thermo Scientific. Iron (III) chloride (anhydrous, 98+%) is obtained from Alfa Aesar. The de-ionized (DI) water used in the experiments is obtained from a Milli-Q® Direct 8 Water Purification System. Acetone ($\geq 99.5\%$, ACS) and isopropyl alcohol (99%, ASC) purchased from VWR Chemicals BDH® are used to clean chips. Sulfuric acid (H_2SO_4 , Catalog No.A300C-212) and hydrogen peroxide (H_2O_2 , Catalog No.H312-500) are acquired from Fisher Scientific™ and used for the removal of organic contaminants [29]. Hexamethyldisilazane (HMDS) and AZ 1512 are obtained from MicroChem Corp and used to prepare photoresist layers. AZ300 MIF developer is supplied by EDM Performance Materials Corp and used to make the underlying pattern visible in the developing process. Finally, a double-sided PSA tape (ARcare® 90106NB) from Adhesives Research, Inc. is adopted to use both an intermediate fluid channel and an adhesive layer to bond the top and bottom Pt μ E layers. The glass substrate is from Globe Scientific Incorporated.

2.2. Electrochemical characterizations

$\text{K}_3[\text{Fe}(\text{CN})_6]$ and $\text{K}_4[\text{Fe}(\text{CN})_6]$ (1:1, mole ratio) redox couple in KCl (1 M) are used to assess the electrochemical performance of this novel non-planar system. The CV, EIS, and DPV signals are obtained using a Gamry (Reference 600+) potentiostat. Since platinum (Pt)-based RE provides a good option due to its longevity and easy fabrication, all electrodes (WE, CE, RE) are Pt, as shown in Fig. 2 [30]. For the DPV testing, the Step Size and the Pulse Size are 10 and 25 mV, respectively. The Sample Period is 1s, and the Pulse Time is 0.1s.

3. Results & discussion

The distances between the electrodes (WE, CE, and RE) and their relative placements are essential parameters for measuring the performance and reliability of NP- μ FEC. The NP- μ FEC has four sets of non-planar ID μ E arrays. The length of one entire μ E array is 10 mm, and the horizontal distance between adjacent μ E arrays is $\sim 4 \text{ mm}$, as shown in Fig. 2 (a). The P- μ FEC has two sets of planar ID μ E arrays. The length of one μ E array is 10 mm, and the horizontal distance between adjacent μ E arrays is $\sim 6 \text{ mm}$, as shown in Fig. 2(g). Table 1 summarizes the geometric details of the Pt μ E arrays. Different combinations of the μ E arrays are used as WE, CE, and RE to study the relationship between electrochemical characterization techniques like CV, DPV, and EIS with changing distances between the WE, CE, and RE.

3.1. CV characterization

3.1.1. NP- μ FEC CV

The voltammetric behavior for different μ E configurations is shown in Fig. 2. The corresponding background currents are shown in Fig. S3. As shown in Fig. 2(d), for the WE/CE_1/RE_1 configuration, the voltammogram of 10 mM $\text{K}_3[\text{Fe}(\text{CN})_6]$ and $\text{K}_4[\text{Fe}(\text{CN})_6]$ (1:1, mole ratio) in KCl (1 M) at a scan rate (ν) of 100 mV s^{-1} shows oxidation at anodic peak potential (E_{pa}) of 75 mV and a back reduction at cathodic peak potential (E_{pc}) at -75 mV vs. Pt RE, such that the peak-to-peak separation (ΔE_{p}) is ca. 150 mV . As ν is increased, E_{pa} values move to more positive values while E_{pc} potentials are shifted to more negative values, increasing the

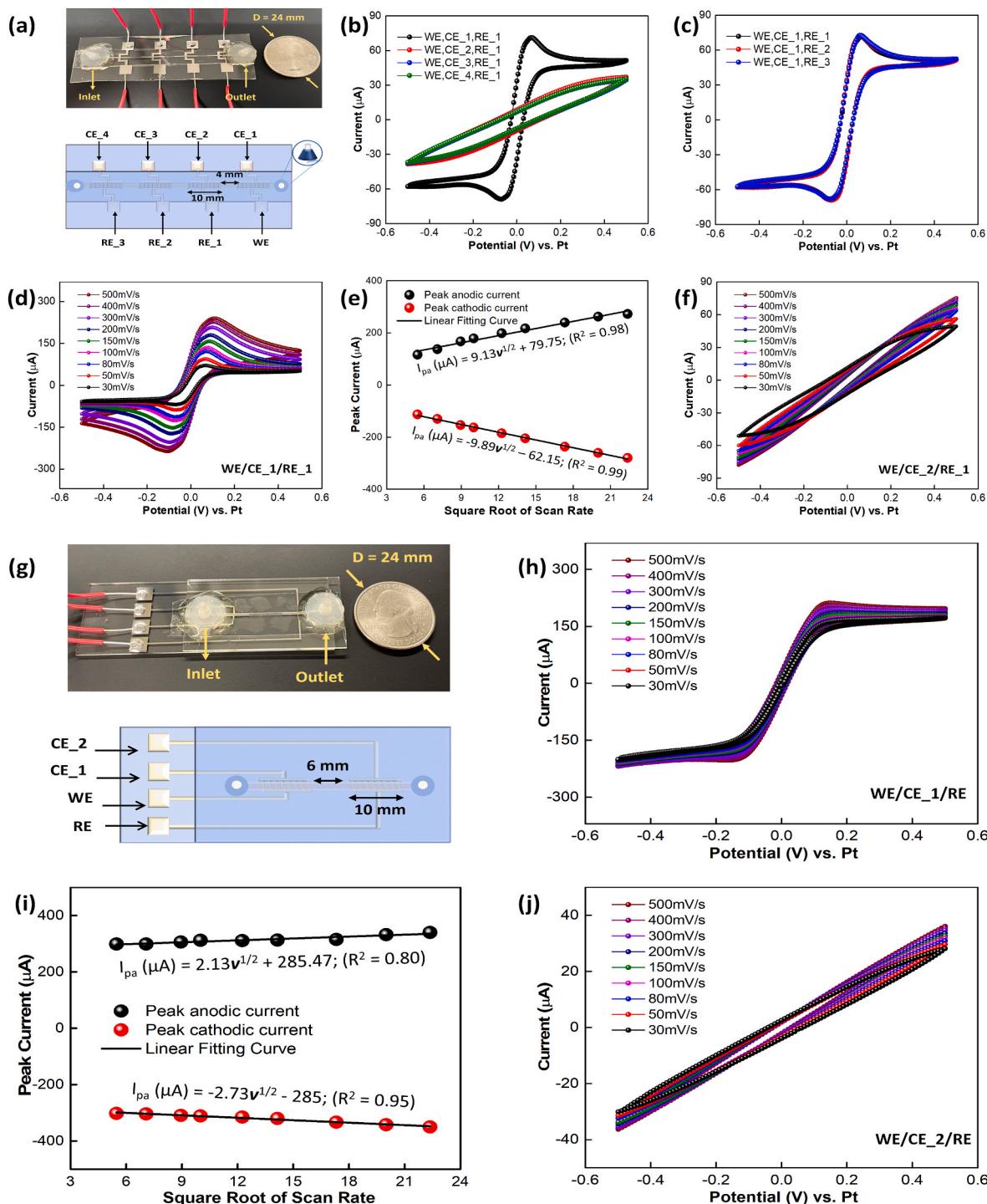


Fig. 2. (a) Picture (top) and schematic diagram (bottom) of NP- μ FEC. Results (b)–(f) are obtained based on NP- μ FEC. Here, the solution is $[\text{Fe}(\text{CN})_6]^{3-/-4-}$ (0.01 M) in KCl (1 M). (b) CV results at different CE positions with $\nu = 30 \text{ mV s}^{-1}$. (c) CV results at different RE positions with $\nu = 30 \text{ mV s}^{-1}$. (d) CV results under different ν based on WE/CE_1/RE_1 configuration. (e) Peak current plots (I_{pa} , I_{pc}) versus the square root of scan rates ($\nu^{1/2}$). The equation of the anodic peak current (I_{pa}) line: $I_{pa} (\mu\text{A}) = 9.13 \times \nu^{1/2} + 79.75$; Coefficient of determination (R^2) = 0.98. The equation of the cathodic peak current (I_{pc}) line: $I_{pc} (\mu\text{A}) = -9.89 \times \nu^{1/2} - 62.15$; $R^2 = 0.99$. (f) CV results under different ν based on WE/CE_2/RE_1 configuration. (g) Picture (top) and schematic diagram (bottom) of P- μ FEC. Results (h)–(j) are acquired based on P- μ FEC. Here, the solution is $[\text{Fe}(\text{CN})_6]^{3-/-4-}$ (0.01 M) in KCl (1 M). (h) CV results under different ν based on WE/CE_1/RE configuration. (i) Peak current plots (I_{pa} , I_{pc}) versus $\nu^{1/2}$. The equation of I_{pa} line: $I_{pa} (\mu\text{A}) = 2.13 \times \nu^{1/2} + 285.47$; $R^2 = 0.80$. The equation of I_{pc} line: $I_{pc} (\mu\text{A}) = -2.73 \times \nu^{1/2} - 285$; $R^2 = 0.95$. (j) CV results obtained at different ν based on WE/CE_2/RE configuration.

magnitude of ΔE_p ($(\Delta E_p @ \nu): 170 \text{ mV} @ 150 \text{ mV s}^{-1}; 210 \text{ mV} @ 400 \text{ mV s}^{-1}$). Conversely, lowering ν results in decreasing ΔE_p ($\Delta E_p = 125 \text{ mV} @ \nu = 30 \text{ mV s}^{-1}$). In all cases, the apparent formal potential E^0 of $[\text{Fe}(\text{CN})_6]^{3-/-4-}$ at the Pt WE are equal to $(E_{pa} + E_{pc})/2 = \sim 0 \text{ mV}$ and independent of ν .

The effect of ν on peak currents of the cyclic voltammograms is also monitored. It is observed that for all the ν studied, the ratio of the cathodic and anodic processes' peak currents (I_{pc}/I_{pa}) is consistently nearing 0.95, indicating the chemical reversibility as expected for the $[\text{Fe}(\text{CN})_6]^{3-/-4-}$ redox process. Furthermore, as shown in Fig. 2(e), from

Table 1
Parameter setting for COMSOL simulation.

Parameter	Value
Electrode Height (E_H)	0.1 μm
Electrode Width (E_W)	10 μm
Solution Electrical Conductivity	$\sim 9 \text{ S m}^{-1}$
Solution Relative Conductivity	80
Glass Substrate Electrical Conductivity	$1 \times 10^{-15} \text{ S m}^{-1}$
Glass Substrate Relative Permittivity	4.68
P- μ FEC Double Layer Capacitance	$\sim 2.6 \times 10^{-6} \text{ F}$
NP- μ FEC Double Layer Capacitance	$\sim 1.6 \times 10^{-6} \text{ F}$

30 to 500 mV s^{-1} , peak currents (I_{pa} , I_{pc}) vs. square root of scan rate ($\nu^{1/2}$) show good adherence to linearity, demonstrating classical Nernstian diffusion-controlled redox behavior [3,31,32].

$$i_p = 0.446nFAC^o \left(\frac{nFvD_0}{RT} \right)^{1/2} \quad (1)$$

The Randle-Sevcik Equation (1) can calculate the cumulative active electrode surface area (A_{real}). Using the literature value of diffusion coefficients ($7.3 \times 10^{-6} \text{ cm}^2 \text{ s}^{-1}$ for $[\text{Fe}(\text{CN})_6]^{3-}$ [31]; $6.3 \times 10^{-6} \text{ cm}^2 \text{ s}^{-1}$ for $[\text{Fe}(\text{CN})_6]^{4-}$ [32]), the corresponding A_{real} are determined as $4.37 \times 10^{-2} \text{ cm}^2$ and $4.62 \times 10^{-2} \text{ cm}^2$, respectively. These calculated values agree with the actual cumulative geometrical surface area (A_{geom} , $\sim 1.25 \times 10^{-2} \text{ cm}^2$) of Pt WE.

3.1.2. Influence of RE and CE's relative placement on NP- μ FEC CV

Keeping the WE and CE positions the same and altering the RE's position (WE/CE_1/RE_1,2,3) does not affect the redox behavior, as demonstrated by the near-identical voltammograms in Fig. 2(c). However, in conventional bulky 3-electrode systems, the position of RE relative to the WE is observed to significantly impact the potential drop (iR_{cell}) between the RE and WE. Therefore, positioning the RE close to the WE is recommended in such set-ups for precise control over the WE potential [33–35]. However, in NP- μ FEC, no noticeable impact of the RE position alterations relative to WE is observed even when the distance between the RE and WE (d_{rw}) is as long as $\sim 32 \text{ mm}$ (when RE is at RE_3), suggesting higher electrochemical operational flexibility in NP- μ FEC.

However, significant changes are observed when the CE's position is progressively offset from the WE, as demonstrated in Fig. 2(b) and (f). Upon switching from WE/CE_1/RE_1 to WE/CE_2/RE_1, the current curves show significantly less prominent redox features and a considerable reduction in the overall current intensity. The voltammograms with WE/CE_2,3,4/RE_1 configuration show similar behavior, as shown in Figs. S3(c) and (d). However, with an increase in the scanning range from (+550 to -550 mV) to (+900 to -900 mV), redox peaks are reobserved (Fig. S3(e)). Fig. S4 shows the CV results obtained at different CE positions. Compared with other configurations, for WE/CE_1/RE_1 (WE and CE are interdigitated), well-defined cyclic voltammograms with relatively narrower ΔE_p and high peak currents are obtained. However, for WE/CE_2,3,4/RE_1 (WE and CE are non-interdigitated), massive shifts in peak potentials (E_{pa} , E_{pc}) are observed with the increase of concentration, and these results in considerable gains in ΔE_p (Table S1). This usually indicates a high barrier to electron transfer, and electron transfer reactions are sluggish [36]. Hence more negative (positive) potentials are required to observe reduction (oxidation) reactions, giving rise to more significant ΔE_p .

Figs. S5 and S6 show that the ohmic drop iR_{cell} between RE_1/2/3 and WE is approximately 5.4 mV, 7.4 mV, and 9.6 mV, respectively. Since there are no apparent changes in the ohmic drop, there are no minimal changes in the cyclic voltammograms (Fig. 2(c)). However, dramatic changes are observed with the increase of the spacing between the CE and WE (d_{cw}), as exemplified by the loss of the classical “duck-shape” features of cyclic voltammograms. When the CE and WE are increasingly offset, the ohmic drop between the CE and WE increases

from ~ 2.3 to 45.6 mV (Fig. S7). Therefore, in NP- μ FEC, the spacing d_{cw} plays a more critical role than the d_{rw} on the NP- μ FEC's electrochemical performance.

In addition, since the cyclic voltammograms are obtained under the stagnant condition, convective contribution to the overall current density can be ignored. Furthermore, at the high ionic strength liquid of 1 M KCl, the contribution of electromigration can also be neglected [28]. Hence, mass transport is chiefly dominated by diffusion. With the stepwise movement of CE away from the WE, the diffusional gradient of reagents/products weaken significantly. This will decrease the current density leading to poor electrochemical performance. All these findings suggest that in NP- μ FECs, the interdigitated layout of the CE and WE is the best option for CV and DPV. This provides us with valuable preliminary suggestions on the future design or optimization of the NP- μ FEC as an analytical tool.

3.1.3. P- μ FEC CV

The promising results observed in NP- μ FEC motivated us to contrast the CV results of NP- μ FEC against P- μ FEC. Fig. 2(g) is the schematic diagram of the P- μ FEC configuration. The voltammetric responses of two different electrode configurations (WE/CE_1/RE and WE/CE_2/RE) are studied and shown in Fig. 2(h) and (j), respectively. The corresponding background currents are shown in Fig. S8(a).

3.1.4. Influence of RE and CE's relative placement on P- μ FEC CV

For the WE/CE_1/RE configuration, the I (current) vs. E (applied potential) profile at $\nu = 100 \text{ mV s}^{-1}$ shows a sigmoidal behavior reminiscent of a steady-state electrochemical process characteristic of a predominantly radial diffusion field [23,37,38]. In this case, $[\text{Fe}(\text{CN})_6]^{3/4-}$ get reduced/oxidized between the WE and CE electrode fingers. This process is sometimes referred to as redox cycling. A key observation is that ΔE_p decreases in magnitude gradually as the ν is progressively increased ($(\Delta E_p @ \nu)$: 360 mV @ 30 mV s^{-1} ; 330 mV @ 100 mV s^{-1} ; 280 mV @ 500 mV s^{-1}), as shown in Fig. S8(b). This behavior of the P- μ FEC marks a stark contrast to the NP- μ FEC, which shows an opposite trend in the variations of ΔE_p with ν . By contrast, the formal potential E^0 of $[\text{Fe}(\text{CN})_6]^{3/4-}$ in the P- μ FEC equals $\sim 0 \text{ mV}$ and therefore mirrors the behavior of NP- μ FEC in being ν independent. The effects of ν on the peak currents in the cyclic voltammograms are illustrated in Fig. 2(i). The linear relationship between the peak currents (I_{pa} , I_{pc}) and $\nu^{1/2}$ further confirms a classical Nernstian behavior in P- μ FEC, where diffusion is the rate-limiting step [1]. The Randle-Sevcik Equation (1) can estimate the cumulative WE surface area, A_{real} [39]. The value of A_{real} estimated using the Randle-Sevcik analyses on the cathodic processes and the anodic processes are equal to $1.14 \times 10^{-2} \text{ cm}^2$ and $1.25 \times 10^{-2} \text{ cm}^2$, respectively, which is consistent with the actual cumulative working electrode surface area A_{geom} of $1.25 \times 10^{-2} \text{ cm}^2$.

Fig. 2(j) shows the CV test results obtained at WE/CE_2/RE under different scan rates. Significantly less prominent redox features and reduced current intensities are observed when the CE is fixed at CE_2. By comparing the results in Fig. 2(h) and (j), it is also found that in the P- μ FEC, when the spacing d_{cw} is decreased to $\sim 10 \mu\text{m}$, that is, WE and CE are interdigitated, well-defined CV curves appear. This finding further confirms the previous assumption that for both P-ID μ E and NP-ID μ E based μ FECs, the spacing d_{cw} plays a more critical role in the final electrochemical performance.

3.1.5. NP- μ FEC vs. P- μ FEC

Based on the analysis above, the difference in the electrochemical characteristics between the NP- μ FEC and P- μ FEC (when the CE and WE are interdigitated) is:

- Different electrochemical processes: NP- μ FEC demonstrates a semi-infinite linear diffusion, while the P- μ FEC shows radial diffusion. However, the semi-infinite linear diffusion enables NP- μ FEC one significant benefit: it can easily interrogate the valuable

information related to redox processes (like E_{pa} , E_{pc} , I_{pa} , I_{pc}), while for P- μ FEC is challenging.

(ii) Different peak-to-peak separation (ΔE_p) behavior: Interestingly, for both NP- μ FEC and P- μ FEC, ΔE_p changes slightly with v . It is hypothesized that this deviation could be due to slow electron transfer to the bare μ Es [39]. However, for NP- μ FEC, ΔE_p increases with v , while for P- μ FEC, ΔE_p decreases with v . From Table S4, it is found that for NP- μ FEC, the overall intensity in ΔE_p is much smaller than that of the P- μ FEC. This relatively narrower ΔE_p means a higher charge-transfer ability is observed in the non-planar configuration [40].

3.2. COMSOL multiphysics simulation

For both planar and non-planar μ FEC, to see changes in the electric fields as the CE and WE are more and more offset from each other and compare the difference in the electric field distribution in the NP- μ FEC and P- μ FEC. Detailed FEA using COMSOL Multiphysics 5.5. is carried out to determine the actual electric field distribution within the NP- μ FEC vs. P- μ FEC. In addition, FEA is also employed to see the influence of the transition in μ E arrays (from coplanar to non-planar interdigitated structure) on the distribution of concentration profiles of aqueous $[\text{Fe}(\text{CN})_6]^{3-/-4-}$ couple.

Table 1 summarizes the simulation parameters. The effect of double-layer capacitance is considered in the COMSOL simulation. And relevant double-layer capacitance values are obtained based on EIS results

(Tables S3 and S5). To avoid long pre-processing, solving, and post-processing periods, the geometries of the P- μ FEC and NP- μ FEC are simplified to a representative 2D model, as shown in Fig. 3(a) [41]. Besides, the periodic distribution characteristics further reduce the model to a few representative pairs of electrode fingers. The gap (E_G) of the planar ID μ E arrays is set to 10 μ m, while the E_G of non-planar ID μ E arrays is set to 30 μ m to ensure a consistent number of electrode fingers per unit length in these two electrode structures. Of note, the electric field distribution in the P- μ FEC and NP- μ FEC at a potential drop of +1.0 V vs. Pt is taken as an example. The electric field distribution is recorded and plotted across the whole microfluidic channel, as Fig. 3(b)–(d) demonstrates. Fig. 4 shows the corresponding spatial distribution of the electric field in the P- μ FEC and NP- μ FEC.

3.2.1. P- μ FEC 2D electric field distribution

From the simulation results, the P- μ FEC and NP- μ FEC display different electric field distributions. For the P- μ FEC, the electric field is concentrated near the electrode surface, akin to a 2D-like distribution, as shown in Figs. 3(b) and 4(a, b). Higher electric field intensity (I_{EF}) is observed at the edges of electrode fingers because of edge effects [42]. Fig. 3(b) shows us that the penetration of the electric field (in the z-axis) is around 20 μ m in the P- μ FEC, which matches the value of E_W (10 μ m) + E_G (10 μ m) and is consistent with the literature [11,43,44]. A radial distributed electric field is observed from the local magnification diagram of Fig. 3(b). However, most regions within the microfluidic channel layer show almost negligible I_{EF} .

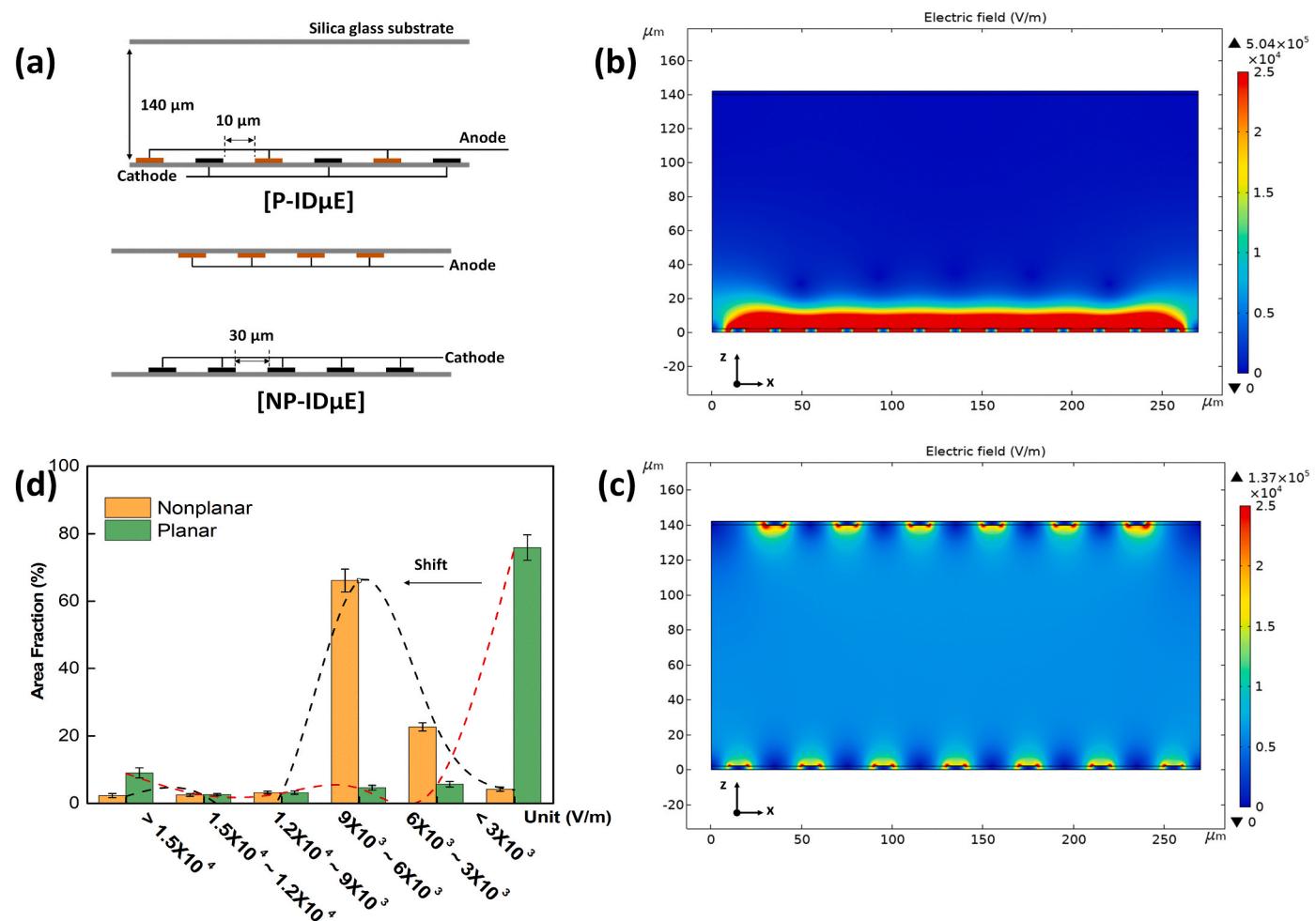


Fig. 3. (a) Cross-section μ E configuration of P- μ FEC (top) and NP- μ FEC (bottom). Simulated electric field distribution within P- μ FEC (b) and NP- μ FEC (c) channel. (d) Distribution of the effective area fractions with different I_{EF} intervals within P- μ FEC and NP- μ FEC channels. Black (Nonplanar) and red (Planar) dotted lines represent the corresponding fitted curves. (For interpretation of the references to colour in this figure legend, the reader is referred to the Web version of this article.)

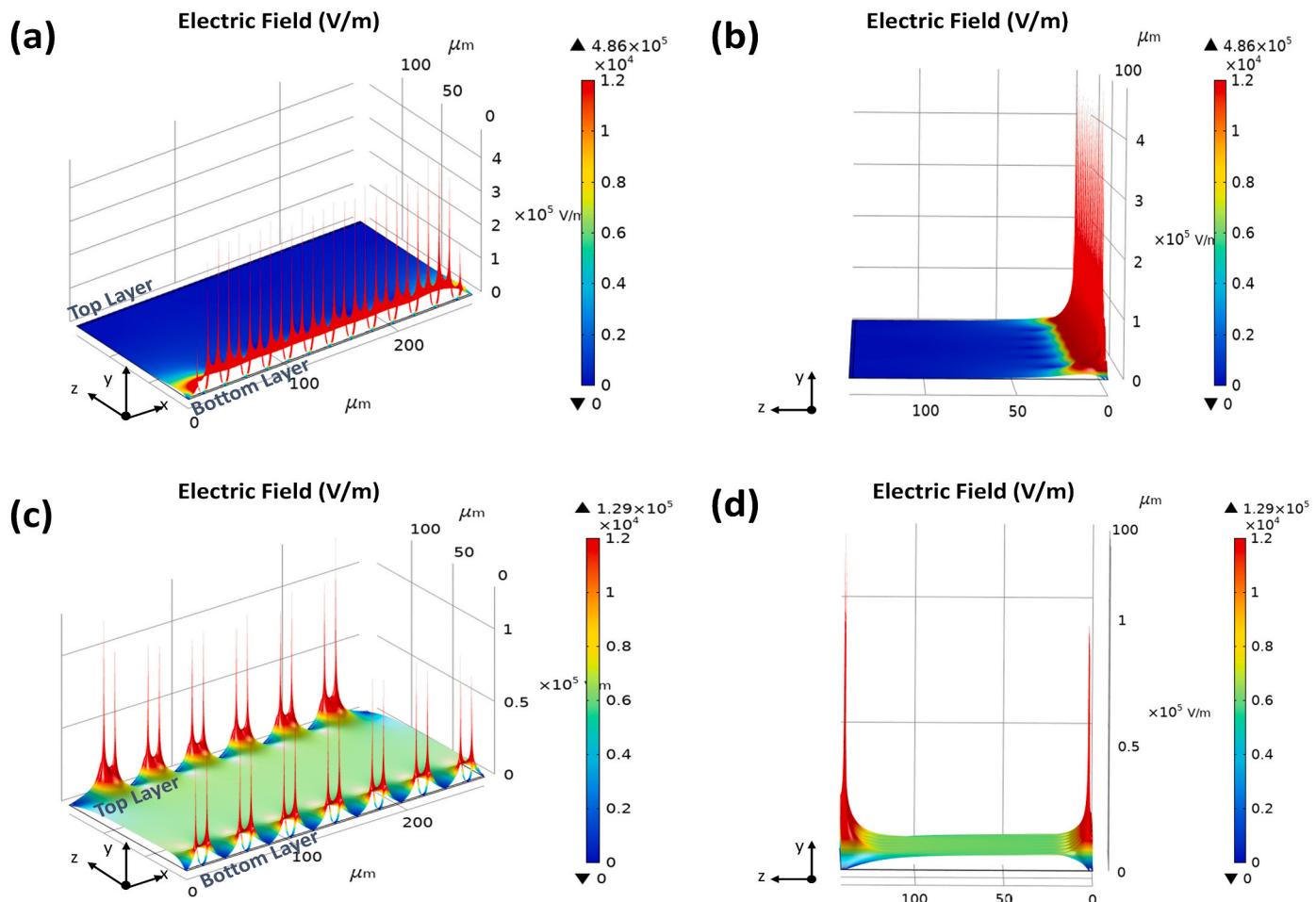


Fig. 4. (a) and (b) represent the spatial distribution of the electric field (from different angles) in P- μ FEC. (c) and (d) describe the spatial distribution of the electric field (from different angles) in NP- μ FEC.

3.2.2. NP- μ FEC 3D electric field distribution

For the NP- μ FEC, the μ E arrays' spatial orientation lets the opposite electric field penetrate each other. Furthermore, the electric field is no longer confined to the μ E surface (Figs. 3(c) and 4(c, d)). Instead of seeing a radial distributed electric field, a vertically channel-wide electric field appears in NP- μ FEC. As a result, a more uniformly distributed electric field with enhanced intensity across the entire microfluidic channel volume is observed. This imparts NP- μ FEC with higher electrochemical sensitivity than its corresponding planar counterpart as an impedance transducer.

3.2.3. P- μ FEC vs. NP- μ FEC

The channel layer of the P- μ FEC and NP- μ FEC have been divided into six regions with different I_{EF} intervals to facilitate analysis and comparison between them (Fig. 3(d)). The locations of these six regions with varying intervals of I_{EF} in the P- μ FEC and NP- μ FEC are shown in Figs. S10 and S11, respectively. Table S6 summarizes their corresponding cross-section area fractions. It is found that the P- μ FEC has more channel area falling in a relatively stronger electric field range ($>1.5 \times 10^4 \text{ V m}^{-1}$) than that in NP- μ FEC. However, most of the channel layer ($\sim 75.77\%$) has a weak electric field strength ($<3 \times 10^3 \text{ V m}^{-1}$). For the NP- μ FEC, most of the channel ($\sim 66.00\%$) falls in a moderate electric field intensity region (from 9×10^3 to $6 \times 10^3 \text{ V m}^{-1}$).

This FEA study shows us that the transition of μ E arrays from planar distribution to non-planar distribution will "drag" a significant part of the electric field away from the μ E surface to the bulk channel, as shown in Fig. 3(d). It is also observed that with the stepwise separation between the CE and WE, the electric fields in both the P- μ FEC and NP- μ FEC

undergo a severe attenuation, as shown in Figs. S12 and S13. Time-dependent mass transport simulations across the channel of NP- μ FEC and P- μ FEC are conducted using Butler-Volmer electrode kinetics (Fig. S14). The simulated concentration profiles indicate a redox cycling in P- μ FEC and a linear diffusion process in NP- μ FEC. These findings are consistent with the observed CV results.

3.3. EIS characterization

As shown above, in both P- μ FEC and NP- μ FEC, the stepwise separation between the CE and WE dramatically decreases the I_{EF} . Therefore, it is expected that the severe decrease in I_{EF} should lead to dramatic increases in the charge transfer resistance (R_{ct}). EIS characterization is thus conducted to visualize the changes in R_{ct} due to the stepwise separation between the CE and WE for both P- μ FEC and NP- μ FEC.

3.3.1. NP- μ FEC EIS

The proposed equivalent circuit in Fig. 5(a) models the EIS signature (Nyquist Curve). In this equivalent circuit in Fig. 5(a), L is the parasitic inductor in the device due to external noises. Since the external circuit's resistance is ordinarily negligible, it is not considered in Fig. 5(a). R_c represents the resistance of the solution filling between the WE and CE. C_c is the cell capacitance originating from the NP-ID μ E electrochemical cell. Instead of an ideal double-layer capacitance (C_{dl}), the constant phase element Q is employed due to the inhomogeneity of the interface between the Pt μ E and electrolyte [3,45]. R_{ct} is the charge transfer resistance associated with the electrons' transfer from the electrolyte onto the μ E [45]. The Warburg element (W) impedes the reactants'

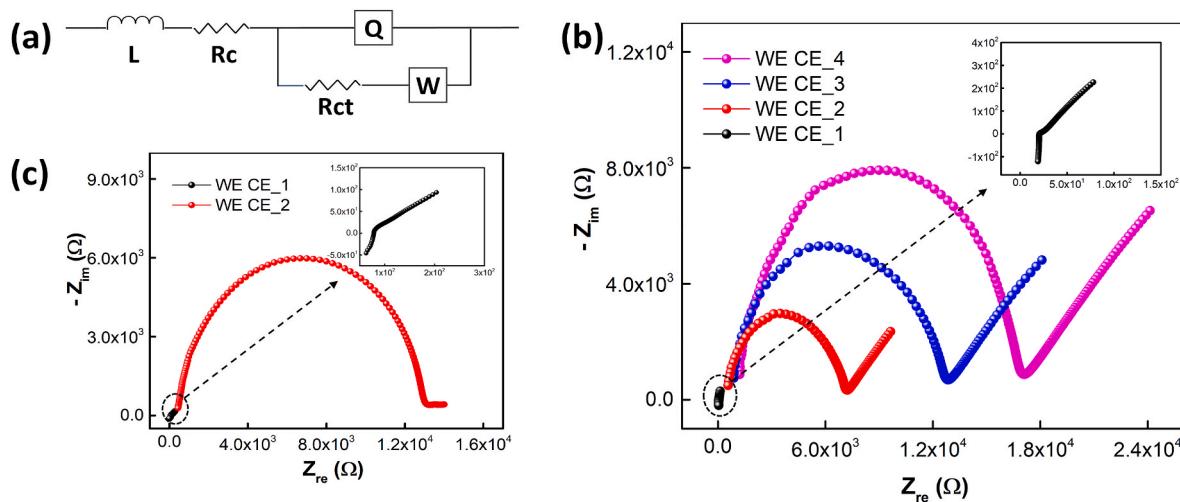


Fig. 5. (a) Equivalent circuit diagram. (b) Nyquist plots of NP- μ FEC obtained at different CE positions. (c) Nyquist plots of P- μ FEC obtained at different CE positions. The solution is $[\text{Fe}(\text{CN})_6]^{3-4-}$ (0.01 M) in KCl (1 M).

diffusion rate [3,46]. R_{ct} and W are modeled parallel to Q as co-occurring phenomena [3,45,46]. The equivalent circuit is fitted using the ZSimpWin software (Fig. S5).

During EIS measurements, the CE is moved from CE_1 to CE_4. The corresponding EIS spectra (Nyquist curve) are shown in Fig. 5(b). Significant differences in the impedance spectra are observed during the stepwise movement of the CE. When the CE is located at CE_1 ($d_{\text{cw}} = \sim 10 \mu\text{m}$, the height of the microfluidic channel is $\sim 140 \mu\text{m}$), the electron transfer process between the electrode and electrolyte solution is instantaneous, the R_{ct} is almost negligible, and thus the electrochemical response is a nearly straight line, as shown in the inset. However, the shift from CE_1 to CE_2, CE_3, and CE_4 significantly increased R_{ct} . Table S3 gives the details of each element in the equivalent circuit.

3.3.2. P- μ FEC EIS

The impedance spectra (Nyquist curve) of the P- μ FEC are shown in Fig. 5(c). Based on the established equivalent circuit, we did the circuit analysis for P- μ FEC (Fig. S9). The circuit element's simulated results are summarized in Table S5. Significant differences in the impedance spectra are observed when CE is moved from CE_2 to CE_1. For CE at CE_1, R_{ct} becomes negligible, and thus the impedance response is a nearly straight line, as shown in the inset. This dramatic decrease of R_{ct} makes the electron transfer between the CE and WE more "smooth."

3.4. DPV characterization

DPV is often used for electroanalysis, typically in aqueous solutions, as it is usually an order of magnitude more sensitive than the CV mode [47]. Hence, DPV is used to determine the detection limit (DL) of $[\text{Fe}(\text{CN})_6]^{3-4-}$ (a proof-of-concept analyte) to compare the performance of P- μ FEC and NP- μ FEC as an analytical tool.

3.4.1. NP- μ FEC DPV

Fig. 6 compares the differential pulse voltammograms of $[\text{Fe}(\text{CN})_6]^{3-4-}$ obtained at varying electrode configurations. Fig. 6(a) shows a typical voltammogram of the $[\text{Fe}(\text{CN})_6]^{3-4-}$ couple appears at a peak potential (E_{peak}) of *ca.* -15 mV with a full width at half maximum (FWHM) of $\sim 100 \text{ mV}$ at WE/CE_1/RE_1. NP- μ FEC's DL is studied for WE/CE_1/RE_1. Unless otherwise indicated, the concentrations referred to here imply the concentrations of $[\text{Fe}(\text{CN})_6]^{3-4-}$ probe. Fig. 6(b) shows an increase in DPV reduction peak currents with the rise of the concentration (Table S7). The calibration curve's linear portion falls from 1×10^{-4} to $1 \times 10^{-6} \text{ M}$ with a high coefficient of determination (R^2) equal to 0.9995, as shown in Fig. 6(c). Therefore, a preliminary value of the DL

can be calculated based on the IUPAC recommended formula (Equation (2)) [48].

$\text{DL} = \frac{K \cdot S_b}{m}$ (2) Here, k is a numerical constant, m is the slope of the plot's linear region, and S_b is the standard deviation of the blank or the ordinate intercept standard deviation [49]. According to IUPAC recommendations, a k value of 3 corresponds to a 99.87% confidence level [1]. A DL of $\sim 2.54 \times 10^{-6} \text{ M}$ is obtained using the above formula for an aqueous $[\text{Fe}(\text{CN})_6]^{3-4-}$ redox couple.

As with the cyclic voltammograms, it is also observed that the variations in the positionings of the RE do not impact the NP- μ FEC's DPV response (Fig. 6(d)). For the WE/CE_2/RE_1 configuration, instead of seeing a typical DPV profile, the current (I) versus applied voltage (E) profile shows a significantly reduced current intensity with a broadened FWHM and a pronounced reduction in the redox features. Similar responses are observed for the configurations WE/CE_3,4/RE_1 (Fig. S15). The DPV results demonstrate that only when the horizontal spacing d_{cw} decreases to $\sim 10 \mu\text{m}$ (when the CE and WE are interdigitated) that NP- μ FEC can give a more pronounced electrochemical response.

3.4.2. P- μ FEC DPV

Similarly, the DPV performance of P- μ FEC for the aqueous $[\text{Fe}(\text{CN})_6]^{3-4-}$ probe is studied. Fig. 6(e) shows the DPV results obtained at different CE positions. A well-defined DPV curve shows up only when the CE and WE are interdigitated (CE is fixed at CE_1), with the distance between the adjacent WE and CE fingers being $10 \mu\text{m}$. The I_{peak} is observed at $E_{\text{peak}} = -15 \text{ mV}$ with a value of *ca.* $-32 \mu\text{A}$ and an FWHM of $\sim 220 \text{ mV}$. Fig. 6(f) shows a gradual increase in the I_{peak} with the concentration of $[\text{Fe}(\text{CN})_6]^{3-4-}$ couple. The calibration curve's linear portion falls from 1×10^{-4} to $1 \times 10^{-6} \text{ M}$ with an R^2 equal to 0.9998 (Fig. 6(g)). Using Equation (2), we can get a DL of $\sim 1.8 \times 10^{-6} \text{ M}$ for aqueous $[\text{Fe}(\text{CN})_6]^{3-4-}$ redox couple. Similarly, as the CE moves to CE_2, the characteristic features of the DPV profile are significantly weakened (Fig. 6(e)).

3.4.3. NP- μ FEC vs. P- μ FEC

Table S7 summarizes the features of DPV results obtained from the NP- μ FEC and P- μ FEC. Through careful comparison, two representative differences are outlined here:

- (i) **Different FWHM behaviors:** In the NP- μ FEC, despite the changes of $[\text{Fe}(\text{CN})_6]^{3-4-}$ concentration in the analyte solution (from 6×10^{-4} to $1 \times 10^{-5} \text{ M}$), the FWHM of the NP- μ FEC remains at a relatively stable value ($\sim 100 \text{ mV}$). In contrast, the value of FWHM in P- μ FEC experiences a gradual decrease as $[\text{Fe}$

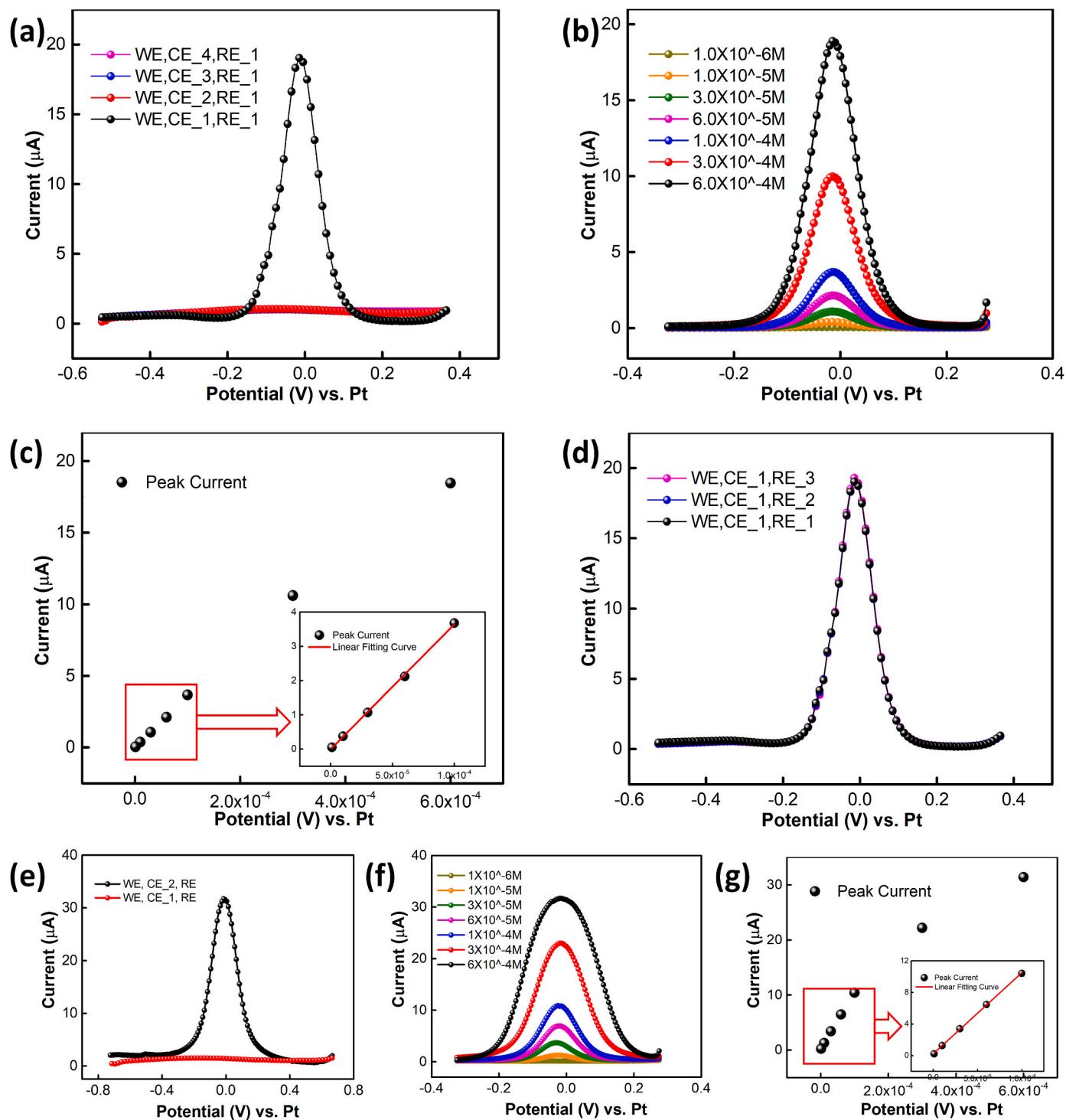


Fig. 6. Results (a)–(d) are the DPV results obtained based on NP- μ FEC. (a) DPV results obtained at different CE positions. (b) DPV results obtained using different concentrations of $[\text{Fe}(\text{CN})_6]^{3-/4-}$ redox couple. (c) Peak currents for $[\text{Fe}(\text{CN})_6]^{3-/4-}$ redox process as a function of increasing $[\text{Fe}(\text{CN})_6]^{3-/4-}$ concentration from 1×10^{-4} M to 1×10^{-6} M (linear working range). The equation of the fitting line: Peak current $I_{\text{peak}} (\mu\text{A}) = -364683.2 \times \text{Conc (M)} - 0.0068$; $R^2 = 0.9995$. (d) DPV results obtained at different RE positions. Results (e)–(g) are the DPV results obtained based on P- μ FEC. (e) DPV results obtained at different CE positions. (f) DPV results obtained from different concentrations of the $[\text{Fe}(\text{CN})_6]^{3-/4-}$ redox couple. (g) Peak currents for the $[\text{Fe}(\text{CN})_6]^{3-/4-}$ redox process with a function of increasing $[\text{Fe}(\text{CN})_6]^{3-/4-}$ concentration. From 1×10^{-4} M to 1×10^{-6} M (linear working range) the equation of the fitting line: Peak current $I_{\text{peak}} (\mu\text{A}) = -103580.64 \times \text{Conc (M)} + 0.238$; $R^2 = 0.9998$. The solution used here for (a), (d), and (e) is $[\text{Fe}(\text{CN})_6]^{3-/4-}$ (6×10^{-4} M) in KCl (1 M).

$(\text{CN})_6]^{3-/4-}$ concentration declines. The difference in the FWHM between the NP- μ FEC and P- μ FEC is probably due to the different dominating electrochemical processes for each (semi-infinite/planar diffusion in NP- μ FEC vs. radial diffusion in P- μ FEC).

(ii) Different electric current behavior: Compared to P- μ FEC, a slower decrease in the I_{peak} is observed in NP- μ FEC, as illustrated in Fig. S16. P- μ FEC has a smaller DL value ($\sim 1.8 \times 10^{-6}$ M) than the NP- μ FEC device ($\sim 2.54 \times 10^{-6}$ M). Though the transition of μ E arrays from coplanar distribution to non-planar distribution

increases ions' diffusion distance, it does not affect the electrochemical performance of NP- μ FEC as an electrochemical sensor working in the DC modes.

3.5. NP- μ FEC for detection of heavy metal ions in aqueous matrices

NP- μ FEC is used to detect heavy metal ions in aqueous solutions. It is expected that with the continual increase in the channel height, the enlarged diffusion distance of ions should deteriorate the NP- μ FEC's device performance leading to decreased sensitivity (increased **DL**). However, the **DL** to aqueous $[\text{Fe}(\text{CN})_6]^{3-4-}$ redox probe in NP- μ FEC has an anomalous change with the height of the channel, as shown in Fig. 7 (a). NP- μ FEC experiences higher sensitivity (lowered **DL**) until the fluid channel height equals 420 μm . Post 420 μm , the sensitivity decreases (an increase in **DL**) with an increase in channel height. The **DL** is lower at 420 μm from 140 μm by about 46%. We hypothesize that this is due to two possible competing mechanisms. For NP- μ FECs, the ratio of the analyte volume in the channel compared to the total electrode surface is approximately the channel height. It has been shown elsewhere that consumption of the analyte by the electrochemical reaction rapidly changes the analyte concentration, affecting the signal magnitude [4, 50]. Hence with the increase in the height of the microfluidic channel, as the amount of analyte in the channel increases, the **DL** should decrease. However, the diffusion distance increases with increasing height, which should increase the **DL** [51, 52]. Hence it can be hypothesized that as the channel height increases from 140 to 420 μm , the **DL** decreases due to an increase in the total amount of analyte in the neighborhood, with a corresponding increase in measurement sensitivity. In contrast, beyond 420 μm , the **DL** increases again due to the increase in diffusion length. Thus, the lowest **DL** is observed at 420 μm for the given electrode and channel geometry. Therefore, the increase in ions overcomes the increased diffusion distance leading to lowered **DLs** till the height of the channel reaches 420 μm in NP- μ FEC. Beyond this height, the **DL** increases as the diffusion distance increases.

Therefore, an NP- μ FEC with a height of 420 μm is employed for the rest of the heavy metals' detection work (Fig. 7(b)). Three common heavy metals (Copper (Cu), Iron (Fe), and Mercury (Hg)) and ($[\text{Ru}(\text{bpy})_3]^{2+}$) are analyzed. DPV results are demonstrated in Figs. S17 and S18. A detailed, comprehensive study of the reproducibility, sensitivity and selectivity of our NP- μ FEC will be done in future work as it is beyond the scope of this paper. Here, the signal-to-noise (SNR) is calculated as the peak current divided by half of the fluctuation in the baseline reading from the pure KCl solution [53]. Using Equation (2), the theoretical **DL** for Cu^{2+} , Fe^{3+} , Hg^{2+} , and ($[\text{Ru}(\text{bpy})_3]^{2+}$) is $30.5 \pm 9.5 \mu\text{g L}^{-1}$ (SNR ~ 2.1), $181 \pm 58.5 \mu\text{g L}^{-1}$ (SNR ~ 2.0), $12.4 \pm 1.95 \mu\text{g L}^{-1}$ (SNR ~ 5.0), $83 \pm 9 \mu\text{g L}^{-1}$ (SNR ~ 2.7), respectively, which meets EPA's water contamination level for Cu, Fe (1300 $\mu\text{g L}^{-1}$, 300 $\mu\text{g L}^{-1}$, respectively) and is close to the EPA level for Hg (2 $\mu\text{g L}^{-1}$). Therefore, this

demonstrates that the cost-effective, simple fabrication of NP- μ FEC can be a new electrochemical analytical tool for other research groups.

4. Conclusions

An assembly of non-planar interdigitated microelectrodes (NP-ID μ E) is introduced in this work. The fabrication of NP-ID μ E-based microfluidic electrochemical cell (NP- μ FEC) and its electrochemical characteristics are studied. The reported NP- μ FEC has many advantages over the classical conventional P- μ FEC. NP-ID μ E, even with non-planar electrode geometry, is easy to assemble with an enhanced three-dimensional (3D) electric field and a relatively high SNR. The convenient fabrication process and the 3D electric field feature NP- μ FEC more attractive as an electrochemical tool, whether working in the AC (EIS) or DC (CV and DPV, among others) detection modes.

Electrochemical characterizations (CV, DPV, and EIS) are carried out to illustrate, examine and fundamentally understand the electrochemical behaviors of the NP- μ FEC. The effect of the spatial orientation of the μ E arrays on the electrochemical behavior is studied in detail. The representative findings are summarized here:

- (i) From the CV tests, for the NP- μ FEC (when the counter electrode (CE) and the working electrode (WE) are interdigitated), the electrochemical process is predominantly controlled by semi-infinite diffusion, which differs from the radial diffusion in the P- μ FEC. This enables NP- μ FEC to more easily interrogate the valuable information related to redox processes, while P- μ FEC is challenging.
- (ii) The effect of the distance between the electrodes (WE, CE, and reference electrode (RE)) and their positions are carefully studied. CV studies show that the inserted RE position's change does not affect the final electrochemical performance of NP- μ FEC. However, the spacing between the CE and WE significantly affects the electrochemical performance.
- (iii) Finite element analysis (FEA) simulation results demonstrate that for the NP- μ FEC, most of the cross-section area of the micro-channel layer ($\sim 66.00\%$) falls in a relatively strong electric field intensity (I_{EF}) range (from 9×10^3 to $6 \times 10^3 \text{ V m}^{-1}$). However, for the P- μ FEC, most of its channel ($\sim 75.77\%$) falls in a relatively weak I_{EF} interval ($< 3 \times 10^3 \text{ V m}^{-1}$).
- (iv) NP- μ FEC shows excellent performance to aqueous $[\text{Fe}(\text{CN})_6]^{3-4-}$ redox couple. Furthermore, DPV tests show that the NP- μ FEC has a similar detection limit (**DL**) ($\sim 2.54 \times 10^{-6} \text{ M}$) to that ($\sim 1.8 \times 10^{-6} \text{ M}$) in the P- μ FEC.
- (v) Interestingly, an anomalous lowering of the **DL** is observed in NP- μ FEC with an increase in channel height to a critical height of 420 μm . An NP- μ FEC with a channel height of 420 μm is employed for heavy metal detection. **DL** for Cu^{2+} ($30.5 \pm 9.5 \mu\text{g L}^{-1}$) and Fe^{3+} ($181 \pm 58.5 \mu\text{g L}^{-1}$) that meet the EPA recommended limits

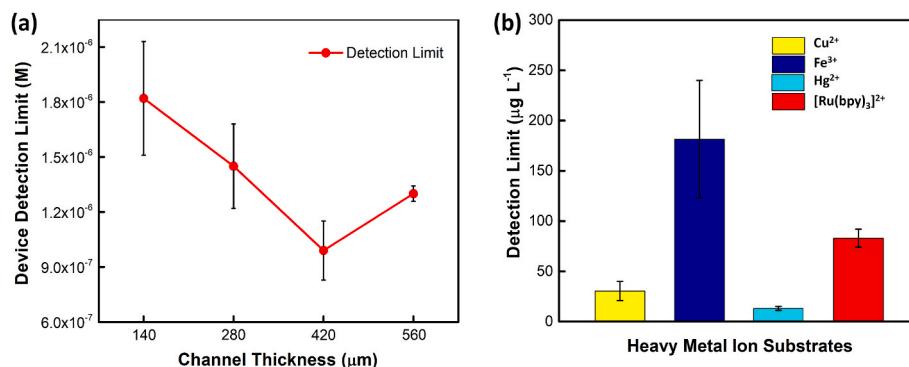


Fig. 7. (a) **DL** to aqueous $[\text{Fe}(\text{CN})_6]^{3-4-}$ redox probe based on NP- μ FEC using different channel thickness. **DL** equals $1.82 \times 10^{-6} \text{ (M)}$, $1.45 \times 10^{-6} \text{ (M)}$, $9.9 \times 10^{-7} \text{ (M)}$, $1.3 \times 10^{-6} \text{ (M)}$ when the channel thickness is 140 μm , 280 μm , 420 μm , 560 μm , respectively. (b) Theoretical **DL** results for different metals (Cu, Fe, Hg) or metal compound ($[\text{Ru}(\text{bpy})_3]^{2+}$) based on NP- μ FEC (thickness = 420 μm).

demonstrate that cost-effective, simple fabrication of NP- μ FEC can be a new analytical tool for other research groups.

The cumulative results demonstrate the NP- μ FEC's general effectiveness for efficient probing electrochemical properties of electroactive analytes. This provides the promise of NP- μ FEC as a lab-on-a-chip microfluidic platform for sensitive electrochemical analysis and detection of analytes' where samples are limited in volume.

CRediT authorship contribution statement

Zhenglong Li: performed Experiments, Writing – original draft, Conceptualization. **Yu-Hsuan Cheng:** performed Writing and Editing. **Charmi Chande:** performed Writing and Editing. **Sayandev Chatterjee:** performed Writing and Editing. **Sagnik Basuray:** performed, Writing – review & editing, Conceptualization.

Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

Data availability

Data will be made available on request.

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Appendix A. Supplementary data

Supplementary data to this article can be found online at <https://doi.org/10.1016/j.aca.2022.340488>.

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