



## Examining the thermodynamic stability of mixed principal element oxides in AlCoCrFeNi high-entropy alloy by first-principles

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### ABSTRACT

Understanding the complex oxidation behavior of alloys consisting of multiple principal elements is critical to realize their potential for high temperature structural applications. We examine the thermodynamic stability of primary and mixed oxides for one such extensively examined high-entropy alloy (HEA), AlCoCrFeNi, using first-principles calculations. Our predictions indicate that  $\text{Cr}_2\text{O}_3$  and  $\text{Al}_2\text{O}_3$  are the most stable oxides both at the ground state and elevated temperatures, with the relative ordering for oxide stability at higher temperatures being similar to that at 0 K. The presence of both Al with Cr are most likely to form protective oxide layers, while that produced by Ni and Cr are the least stable. Nevertheless, the gradient of formation energies for the stable mixed  $\text{Cr}_2\text{O}_3$ -type oxides with increasing concentration of other principal elements becomes steeper with increasing temperature.

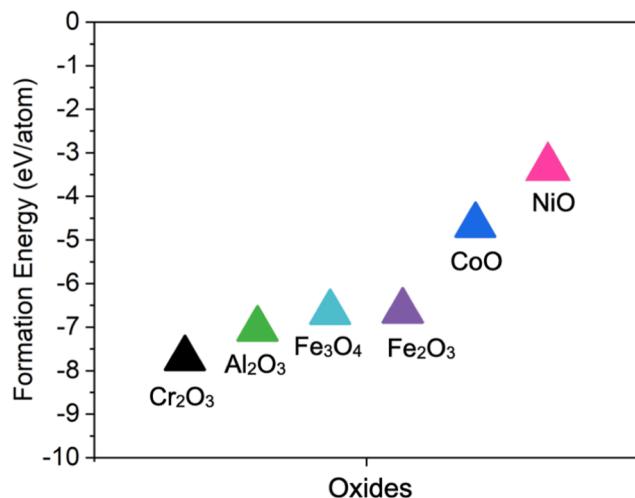
Since the first report on high-entropy alloy (HEA) in 2004 [1], extensive studies have been performed on different classes (e.g., refractories and those composed of transitional metals) of HEAs, which are near equimolar concentrated solid solutions of five or more elements. These intriguing materials have garnered significant interest due to their potential for notable structural properties at high temperatures [2], which situates them as a possible cost-efficient alternative for Ni-based superalloys. Nevertheless, elevated temperature applications such as in gas turbine blades, require a thorough understanding of high-temperature oxidation and an alloy design to mitigate the risks. The complexity of HEA oxidation emerges from the various simple and mixed oxide chemistries that can form due to the presence of multiple principal elements. A systematic computational approach can enable a fundamental physics-based understanding of the complex oxidation mechanisms, to supplement and streamline the experimental scrutiny and material design. The first step towards such modeling is to identify the stable oxides for a given composition of the alloy. In the case of the widely-reported AlCoCrFeNi [3–5] HEA, the presence of Cr and Al in the alloy contributes to the formation of protective chromia (chromium (III) oxide) and alumina (aluminum (III) oxide) scales on the surface, preventing uninhibited oxidation of the HEA [6].

Sparse experimental [6–11] and computational [12,13] studies on

AlCoCrFeNi oxidation exist, but a fundamental understanding of the thermodynamic stability of simple and mixed oxides that form in this HEA is limited. Butler *et al.* [6] studied the effect of varying Al content in  $\text{Al}_x(\text{NiCoCrFe})_{100-x}$  (where  $x = 8, 10, 12, 15, 20$ , and 30 at.%) during oxidation at 1050 °C for 50 h, and found a continuous external chromia ( $\text{Cr}_2\text{O}_3$ ) scale at all concentrations of Al. The alumina ( $\text{Al}_2\text{O}_3$ ) formed discontinuously at low Al concentration ( $x = 8, 10, 12$ ) while a thick  $\text{Al}_2\text{O}_3$  layer was reported for higher fractions of Al ( $x = 15, 20$ , and 30 at.%) in the HEA, corroborating that an increase in Al content improves the oxidation resistance. Oxidation of AlCoCrFeNi (with 1.24 at. % Al) in the temperature range of 800 °C to 1000 °C was compared against the commercially available 825 Ni-based alloys and the duplex 2205 stainless steel (DSS) [7]. Experiments showed that at 1000 °C, the HEA had the least mass gain, while the DSS (that has a high concentration of Fe) gained the highest mass; for the HEA and the Ni-based alloy with 25 at. % and 30 at. % Fe content, respectively, mass gain recedes after 60–70 hours. In absence of Al, the protective oxide layer for the commercial alloys primarily contain chromia and Fe-oxides. Al assists in the formation of a protective thin chromia layer on the HEA surface, while alumina containing internal oxidation zones were found in the bulk material [9]. The local atomic environment of oxygen on the surface [12,14] and in the interstitial sites [13,15] were reported to be

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**Fig. 1.** The formation energies of single element primary oxides of Al, Co, Cr, Fe, and Ni that constitute the HEA, as computed at the ground state (0 K).

important for preferential oxidation; Liu *et al.* [13] concluded that oxygen in an interstitial site is more stable near a Cr atom than a Ni atom.

Here, we examine the thermodynamic stability of simple and mixed oxides that can form during the oxidation of AlCoCrFeNi using *ab initio* computations. Complementing the previous studies where the HEAs incorporate oxygen on the surface and in the interstitial sites, our independent treatment of the bulk oxides contributes to understanding the oxidation mechanisms in various complex alloys composed of Al-Co-Cr-Fe-Ni elements.

The first-principles calculations are performed with Vienna Ab initio Simulation Package (VASP) [16,17]. The oxide structures are obtained from the Materials Project database [18]. The generalized gradient approximation (GGA) as parameterized by Perdew–Burke–Ernzerhof (PBE) is chosen as the exchange–correlation functional [19,20]. A  $5 \times 5 \times 5$  k-point grid with the Monkhorst–Pack method [21] is used to sample the reciprocal space with a cutoff energy of 500 eV, which ensured the energy (charge) is converged to within  $10^{-7}$  eV ( $10^{-3}$  eV), with the residual stresses and forces less than 0.02 GPa and  $10^{-3}$  eV/Å, respectively.

Before the energetic calculations, the ions and forces of the system are first relaxed, and self-consistency calculations are performed on the relaxed structures. The formation energy of  $A_xB_yO_z$  oxide is obtained from  $E_{A_xB_yO_z} = G_{A_xB_yO_z} - xG_A - yG_B - zG_O$ , where  $G_{A_xB_yO_z}$  is the Gibbs free energy of oxide, while  $G_i$  is the Gibbs free energy of one  $i$  atom placed at the center of the simulation cell [22]. The total energy for the oxide and the individual atoms are used to compute the Gibbs free energy in the above equation. The mixed oxides are constructed using the special quasi-random structures (SQS) method within the mcsqs utility in the Alloy Theoretic Automated Toolkit (ATAT) that can generate random solid solutions [23] with varying concentrations of foreign elements. We note that the initial structure of both Cr<sub>2</sub>O<sub>3</sub> and Al<sub>2</sub>O<sub>3</sub> consists of 10 atoms in a trigonal unit cell. Among the 4 cations in the 10-atom unit cell, 1, 2, and 3 cations are respectively altered from parent cation to foreign cation to create mixed oxides with 25%, 50%, and 75% of foreign element addition. The supercell size is carefully chosen to

contain the minimum number of atoms per unit cell. We perform selective simulations on larger supercells to verify and eliminate any role of size effect on the results. We add foreign metals to the oxides for mixed oxide formation by fractionally replacing the base metal with the foreign element. The size of the supercell was chosen accordingly to accommodate a minimum number of atoms required for creating the composition of the mixed oxide. For example, a unit cell with 10 atoms is sufficient to accommodate 25%, 50%, and 75% of foreign cations. So, a supercell of  $1 \times 1 \times 1$  is used for SQS. As we need a minimum of 4 parent cations to create mixed oxides, the supercell size is different for each simulated case.

For the *ab initio* molecular dynamics (AIMD) simulations, a larger supercell is constructed with at least 120 atoms by relaxing the forces and stresses of the unit cell, and replicating the SQS-derived structure in all three directions. An additional increase in the number of atoms essentially raises the computational cost with negligible change in the results. The system is equilibrated constraining the number of atoms (N), volume (V), and temperature (T) under the canonical (NVT) ensemble using the Nose–Hoover thermostat with a coupling time of 5 picoseconds. These simulations are initially run for 5000 steps with 1 picosecond timestep, but the energy typically converges after 2000 steps.

**Thermodynamic stability of primary oxides:** The oxides of each element in AlCoCrFeNi can have multiple oxidizing states depending on the variable oxidation number and a given oxide may have more than one stable phase. For instance, Cr has oxidation numbers of +3, +2, and +1 [24], and Cr<sub>2</sub>O<sub>3</sub> has two phases, viz., trigonal and cubic, though only the former is stable. Likewise, the oxides of Al, Co, Fe, and Ni have multiple stable oxidizing states. Since the common oxidation states of all the elements of this HEA are well reported, we calculate the ground state formation energies to interrogate the relative thermodynamic stabilities of the various oxides (Fig. 1). The formation energies are computed per molecule of the oxide. For consistency, Fig. 1 displays energies per atom of the oxides. The lower the formation energy, *i.e.*, the more negative the magnitude, the more stable is the material. The negative sign is a result of the formation energy calculation from the Gibbs free energies of the various constituents of the system. Hong *et al.* [12] found the cohesive energy of chromia to be slightly higher than alumina due to the low Pauling electronegativity and valance electron count of Al<sub>2</sub>O<sub>3</sub>. We find that Cr<sub>2</sub>O<sub>3</sub> has the lowest formation energy followed by Al<sub>2</sub>O<sub>3</sub> amongst all the oxides that can form in AlCoCrFeNi HEA, in accord with earlier experimental reports that suggest the formation of Cr<sub>2</sub>O<sub>3</sub> and Al<sub>2</sub>O<sub>3</sub> as the primary oxide layers for this alloy [6,7,25]. While our results, in agreement with certain prior reports but in contrast to Ellingham diagrams (at higher temperatures), indicate that Cr<sub>2</sub>O<sub>3</sub> is more stable than Al<sub>2</sub>O<sub>3</sub> in the ground state, we do note that above 1250 K, Cr<sub>2</sub>O<sub>3</sub> is volatile and dissociates, rendering Al<sub>2</sub>O<sub>3</sub>, as the most stable oxide that forms a passivating layer. We plan to perform additional calculations in the future on the mechanical stability of these oxides at the ground state and at higher temperatures to address this issue. The relatively high formation energies for NiO and CoO impede their occurrence in this HEA [26]. Note that certain oxides of reactive elements (REs), such as HfO<sub>2</sub>, assume lower formation energy than Cr<sub>2</sub>O<sub>3</sub> and form very stable oxides quickly, but are not often used due to the high cost associated with REs [9].

The results from our AIMD simulations for the thermodynamic stability of the oxides at 1000, 1250, and 1500 K, are presented in Table 1.

**Table 1**

The formation energy per atom (eV/atom) of single element primary oxides of Al, Co, Cr, Fe, and Ni that constitute the HEA, computed at ground state (0 K) and at elevated temperatures (1000 K, 1250 K, and 1500 K).

Temperature	Cr <sub>2</sub> O <sub>3</sub>	Al <sub>2</sub> O <sub>3</sub>	Fe <sub>3</sub> O <sub>4</sub>	Fe <sub>2</sub> O <sub>3</sub>	CoO	NiO
0 K	-7.7187	-7.0415	-6.6605	-6.6296	-4.663	-3.3271
1000 K	-7.2185	-6.3539	-6.0493	-6.0819	-4.4088	-2.6247
1250 K	-7.1845	-6.3284	-6.0129	-6.0426	-4.3526	-2.5652
1500 K	-7.1502	-6.2959	-5.9562	-6.011	-4.2984	-2.5147

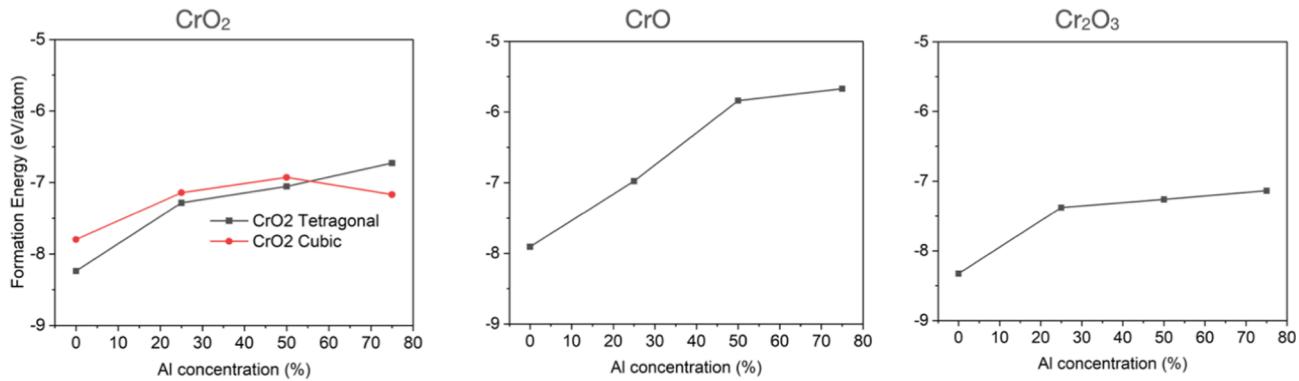


Fig. 2. The formation energies of (a)  $\text{CrO}_2$ , (b)  $\text{CrO}$  and (c)  $\text{Cr}_2\text{O}_3$  at the ground state computed for varying concentrations of Al present in the oxide.

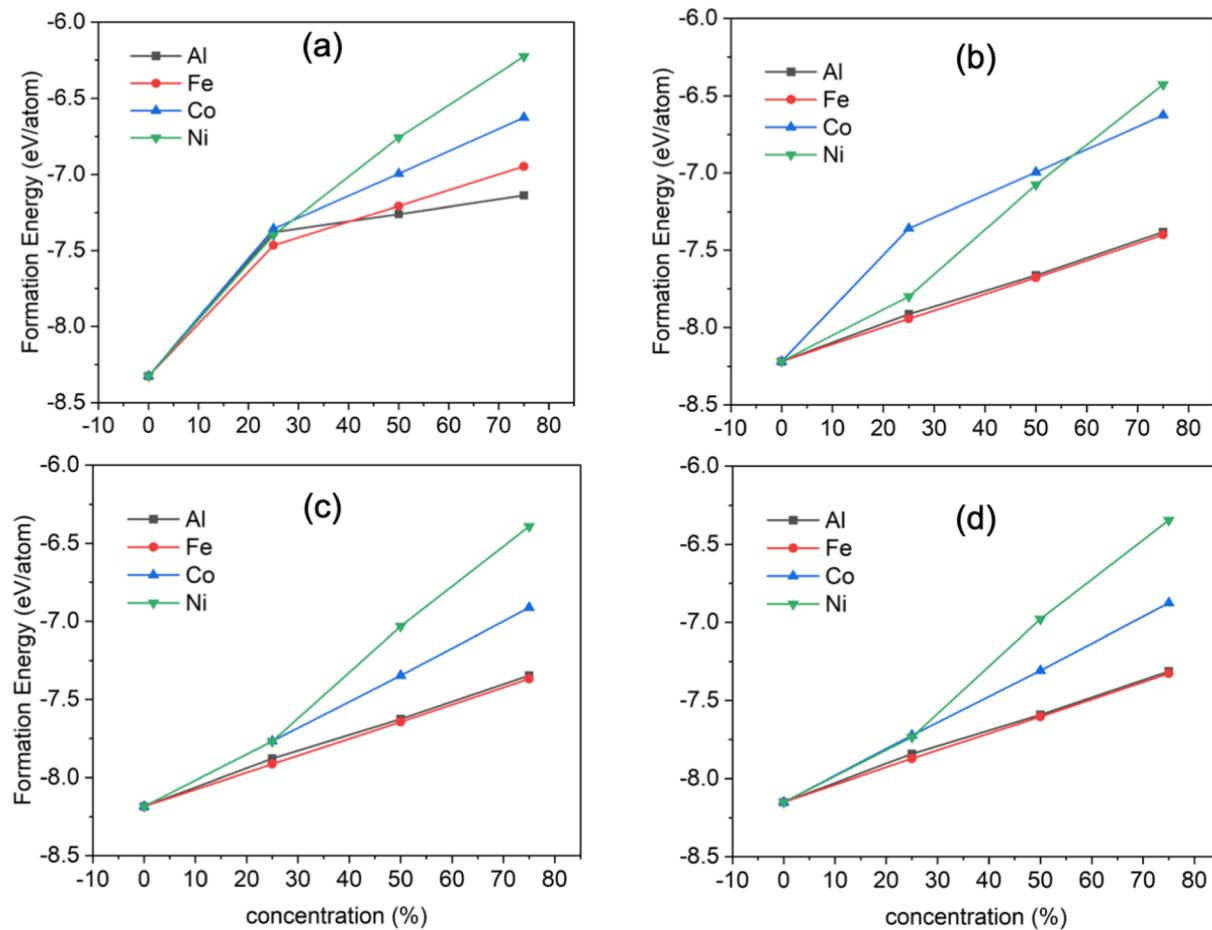


Fig. 3. The formation energies of mixed  $\text{Cr}_2\text{O}_3$ -type oxides at (a) ground state, (b) 1000 K, (c) 1250 K, and (d) 1500 K. The mixed oxides with 25%, 50%, and 75% concentration of the other principal element assume the chemical formula of  $\text{XCr}_3\text{O}_6$ ,  $\text{XCr}_2\text{O}_3$ , and  $\text{X}_3\text{CrO}_6$ , respectively, where  $\text{X} = \text{Al, Co, Fe, and Ni}$ . The mixed oxides considered here are solid solution oxide of Cr and X, where the latter as the foreign element has replaced the base metal. For instance,  $\text{XCr}_3\text{O}_6$  indicates that there is one X metal atom in a supercell of  $\text{Cr}_4\text{O}_6$  oxide, forming  $\text{XCr}_3\text{O}_6$ . We have not used the convention of brackets to avoid confusion of how many atoms are present in one mixed oxide molecule. An alternate representation is  $\text{X}_y\text{Cr}_{(1-y)}\text{O}_3$  where  $y = 0.25, 0.5$  and  $0.75$ .

While the energies demonstrate a trend similar to the ground state, a quantitative assessment indicates that formation energies increase with temperature for all the oxides. At elevated temperatures,  $\text{Cr}_2\text{O}_3$  is the most and  $\text{NiO}$  is the least stable. Nevertheless, given the volatile nature of  $\text{Cr}_2\text{O}_3$  above 1250 K when it is known to dissociate [27], the next most stable oxide is  $\text{Al}_2\text{O}_3$ , which also forms a passivating layer, and is critical for high-temperature oxidation resistance of  $\text{AlCoCrFeNi}$  high entropy alloy.

*Thermodynamic stability of Cr-oxides:* Zhu et al. [7] suggested that the

presence of Cr in the oxide scale enables  $\text{AlCoCrFeNi}$  to be a strong oxidation-resistant alloy. Although  $\text{Cr}_2\text{O}_3$  is the primary oxide, other Cr oxides may form. Since Al concentration exerts a significant influence on the oxidation resistance of  $\text{AlCoCrFeNi}$ , we scrutinize the formation energies of all possible Cr and Al mixed oxides with varying Al concentrations. For 25%, 50%, and 75% Al addition in  $\text{Cr}_2\text{O}_3$ , the mixed oxide chemistries are  $\text{AlCr}_3\text{O}_6$ ,  $\text{AlCr}_2\text{O}_3$ , and  $\text{Al}_3\text{CrO}_6$ , respectively. Additionally, we consider two phases of  $\text{CrO}_2$ , tetragonal and cubic, and  $\text{CrO}$  for the calculations. In the absence of Al,  $\text{Cr}_2\text{O}_3$  has the lowest

formation energy (-42 eV), followed by  $\text{CrO}_2$  (-24.8 eV for cubic and -23.2 eV for tetragonal) and  $\text{CrO}$  (-16.1 eV). With the increase in Al content, the formation energies of all the Cr-oxides increase, as shown in Fig. 2. Mixed oxides with high fractions of Al in  $\text{CrO}$  are least stable, while  $\text{Cr}_2\text{O}_3$  is most stable even in presence of Al and is anticipated to form a passivating layer.

**Thermodynamic stability of mixed oxides:** The other principal elements (Co, Fe, and Ni) in the HEA can also form a mixed oxide with  $\text{Cr}_2\text{O}_3$ . As discussed above,  $\text{NiO}$  and  $\text{CoO}$  are the least stable primary oxides. When Ni is mixed with  $\text{Cr}_2\text{O}_3$ , the increase in the formation energy is almost linear, as shown in Fig. 3a. Thus, the Ni-Cr mixed oxides are unstable, especially at high Ni concentrations. Co addition has a similar effect on  $\text{Cr}_2\text{O}_3$ , though the oxides with high Co content have enhanced thermodynamic stability than high Ni-containing ones. Mixed oxides of Fe and Cr exhibit low formation energies, producing relatively stable oxides. An earlier experimental report on the oxidation behavior of  $\text{AlCrCoFeNi}$ , 825 Ni-based alloys, and 2205 duplex stainless steel (DSS) revealed that 2205 DSS was the poorest among the three alloys with the scale containing considerable Fe-oxide. Results from our simulations corroborate that, unlike  $\text{Cr}_2\text{O}_3$  and  $\text{Al}_2\text{O}_3$ ,  $\text{Fe}_3\text{O}_4$  is not a passivating oxide scale. It implies that a HEA with Cr but devoid of Al will have poor oxidation resistance, especially at high temperature, with the oxide layer predominantly composed of  $\text{Fe}_3\text{O}_4$ . Although the formation energy scarcely changes with an increasing Al content in  $\text{Cr}_2\text{O}_3$ , we find that the addition of 25% of other principal elements in  $\text{Cr}_2\text{O}_3$ , e.g., to form  $\text{XCr}_3\text{O}_6$  (where X = Al, Co, Fe, Ni), assumes near-equal formation energies. The differences in oxide stabilities are more notable when a higher fraction of the principal elements form mixed oxides.

At elevated temperatures, the energies of mixed oxides in  $\text{Cr}_2\text{O}_3$  are reproduced in Fig. 3(b-d). The temperatures presented in Fig. 3 are chosen to examine the high-temperature response of these oxides as applicable to potential aerospace and power generation industries. While the exact values of the temperatures do not offer direct quantitative guidance, but the trends provide qualitative insight on the oxide stabilities. Similar to 0 K results, Al and Fe form low energy stable oxides with Cr while a high concentration of Ni renders  $\text{Cr}_2\text{O}_3$  unstable.  $\text{Cr}_2\text{O}_3$  forms comparably stable mixed oxides with both Al and Fe for significantly high proportions of the principal elements, even at elevated temperatures. Interestingly, the rate of increase of formation energy with increasing concentration of principal elements displays a constant gradient, in contrast to the saturating profile noted from ground state calculations. The results assert that in the presence of other principal elements,  $\text{Cr}_2\text{O}_3$  becomes less stable at a faster rate at higher temperatures than in the ground state.

In summary, we have examined the thermodynamic stability of primary and mixed oxides in  $\text{AlCoCrFeNi}$  high-entropy alloy from first-principles and *ab initio* molecular simulations. From the predictions for the formation energies, we corroborate that Cr and Al form the most stable oxides, i.e., chromia and alumina, in agreement with experimental literature. Given the presence of multiple principal elements, we find that mixed oxides of chromia are stable even when containing high percentages of Al. At elevated temperatures, the mixed oxides exhibit a similar trend for relative stabilities as in their ground states, although the increase in formation energies with increasing concentration of principal elements is steeper than that at 0 K. Further efforts, including examining the thermodynamic stability of spinels that can affect the oxidation pathways in multicomponent alloys, are required to elucidate the fundamentals of the complex oxidation mechanisms in HEAs. This assessment of the preferential oxide formation in a model HEA provides guidelines for designing oxidation-resistant multicomponent alloys.

## CRediT authorship contribution statement

**Indranil Roy:** Data curation, Formal analysis, Investigation, Methodology, Visualization. **Chinedu Ekuma:** Formal analysis, Methodology. **Ganesh Balasubramanian:** Conceptualization, Investigation,

Funding acquisition, Project administration.

## Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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## Data Availability

Data will be made available upon reasonable request.

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