

1 **A cavity ion source for high-efficiency neodymium isotope-ratio
2 analyses in the geosciences.**

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6 **Abstract:**

7 The principles governing ionization techniques used in thermal ionization mass spectrometers are
8 relatively well understood and have remained largely unchanged for many decades. Though significant
9 advances have been made in ion signal quantification for isotope ratio measurements, particularly for
10 analyses of small samples by using multiple detector systems and low-noise amplifiers, the fundamental
11 approach to sample ionization has received little focus. Modern TIMS techniques attempting to achieve
12 parts-per-million level isotope ratios precisions are realizing limits imposed by the physics of the
13 ionization source. A type of high-ionization efficiency thermal source employed in nuclear physics
14 communities for decades is the so-called cavity thermal ionization source. Here, we provide a proof-of-
15 concept study that shows cavity sources may provide a path forward to achieve a new level of precision in
16 isotope ratio measurements from solid samples. We document our new, simple, cavity ion source design,
17 show preliminary results from Nd isotope measurements, and discuss this new data in the context of
18 current precision limits imposed during traditional thermal ionization methods. We show that, within the
19 limits of our testbed mass spectrometer, mass fractionation within the cavity ion source appears similar to
20 that from filament ion sources. We also demonstrate that oxide-versus-metal ion production plays a
21 significant role in cavity ionization processes for Nd. Cavity ion sources may provide a viable path
22 forward to achieving isotope ratios precisions at the sub-ppm precision level.

23 **Introduction**

24 Mass spectrometers used to measure isotope ratios of geologic samples have long been standard
25 equipment in many geoscience laboratories. For the solid Earth geosciences, and geochronology in
26 particular, the thermal ionization mass spectrometer (TIMS) has been an essential tool. Thermal
27 ionization mass spectrometers are used to analyze the isotopic composition of a range of elements whose
28 first ionization potential is sufficiently low such that substantial ionization can occur before complete
29 sample evaporation from the filament (see Carlson, 2014 for a review). Multi-collector inductively

30 coupled plasma mass spectrometers (MC-ICPMS), introduced to the geosciences in the 1990's, use high-
31 temperature plasma sources that can readily ionize elements across the periodic table. At first MC-
32 ICPMS instruments were primarily used to analyze elements that were inefficiently ionized in a TIMS
33 instrument. Recently, ICP instruments have been used to analyze elements once thought to be securely
34 within the domain of TIMS procedures, such as Nd ² and W (Archer et al., 2019) such that the benefits of
35 TIMS analyses become less apparent. ICP analyses are, however, not without their downsides and TIMS
36 instruments remain on the analytical cutting edge due to their comparative simplicity of design, operation,
37 and relatively simple mass spectrum. Both types of instruments appear to be approaching roadblocks that
38 limit the quest for increasing precision and sensitivity in isotope ratio analyses. Overall efficiency,
39 adopted here as the fraction of analyte atoms that end up being detected by the mass spectrometer, is a
40 major factor limiting both functional sample size and ultimate achievable precision during isotope ratio
41 measurements. Distinct hardware obstacles define the sensitivity limits in ICP and TIMS, limits that are
42 unlikely to be overcome without substantial redesign of the ionization and ion transfer systems.

43 Though TIMS instruments have been, and remain, staples of Earth science facilities, they have
44 physical limits to their capabilities. In many cases, especially when dealing with small samples sizes or
45 very precise measurements, total efficiency proves to be the main limitation. This is because internal
46 precisions on isotope ratio measurements via TIMS often approach limits imposed by counting statistics
47 uncertainty (shot noise or Poisson noise). Lowering this barrier to higher precision will require counting
48 more ions either by increasing ionization efficiency, increasing measurement time, or both. The addition
49 of high-ohm feedback resistor amplifiers does not improve the precision on measurements of large ion
50 beams because ion counting statistics, not signal-to-noise ratio, is the limiting factor. Consequently,
51 advances in low-noise detection systems do not provide a path forward for these kinds of measurements.
52 Improvement is primarily needed on the front end of mass spectrometers to improve both the fraction of
53 atoms ionized and the efficiency of transmission of generated ions to the detector systems. In modern
54 TIMS instruments, the efficiency of ion transmission and detection can exceed 80% such that the highest
55 fraction of analyte atoms is lost during the evaporation and ionization process. However, ion sources
56 capable of producing a factor of 10-40 times more ions from a given amount of analyte compared to
57 conventional flat-filament TIMS sources have been developed, so-called thermal ionization cavity (TIC)
58 sources. Despite their obvious potential benefits, TIC ion sources have yet to achieve routine use in the
59 geosciences (see review in Maden et al., 2018). We have taken a new approach to the TIC source and
60 developed an ion source capable of analyzing large sample sizes at high ion beam intensities for long
61 durations with the goal of pushing precision limits below those currently possible with the traditional flat-
62 filament sources used in conventional TIMS.

63 **Current precision limits in TIMS analyses**

64 Standard TIMS instruments employ flat-filament ionizing surfaces wherein the analyte is loaded onto
65 a thin, flat strip of refractory high-work function metal. Ionization efficiency is improved for some
66 elements through the use of multiple filaments where one filament is kept at much higher temperature to
67 serve as an ionization surface for neutral atoms evaporated off of one or more “sample” filaments. The
68 flat-filament ionization assembly, though suitable for the vast array of TIMS applications, suffers from
69 two major drawbacks when considering achievement of parts-per-million isotope ratio precision.

70 First, in conventional TIMS flat filament sources, increasing sample size does not always translate to
71 proportionately longer runs or higher ion beam intensities. In fact, loading more analyte can decrease the
72 total efficiency⁶ such that e.g. a factor of two increase in sample size translates to less than a factor of 2
73 increase in total ions counted. More problematical is that large sample sizes often result in variable mass
74 dependencies for the mass fractionation experienced during sample evaporation and ionization,
75 confounding attempts to accurately correct for that fractionation. These factors combine to restrict our
76 sample size to ~700 ng of Nd^{7,8}, much less than is typically separated from an individual rock dissolution
77 (~2 ug of Nd). A common explanation for the fall-off in ionization efficiency for large samples suggests
78 that large sample sizes limit the amount of analyte in direct contact with the filament, thereby favoring
79 evaporation over ionization. While possible, making longer isotope ratio measurements, by pooling
80 individual ~700 ng Nd loads from a single sample dissolution, becomes increasingly time-inefficient; an
81 analysis with 3-4 ppm internal precision already requires 9-12 hours of continuous measurement of 4e-11
82 A signals for ¹⁴²Nd⁺⁸⁻¹⁰.

83 The second major limitation in flat filament TIMS methods relates to the mass fractionation that
84 occurs during evaporation and ionization. At a basic level, mass fractionation during thermal ionization is
85 a straightforward and well-understood process¹¹⁻¹⁴. During evaporation and ionization, lighter isotopes
86 are preferentially removed from the solid phase such that the isotope ratios collected early in an analysis
87 have a lower heavy/light isotope ratio and this increases with time. This bias must be removed from the
88 analysis, and is often corrected by assuming that the fractionation is mass dependent and follows an
89 exponential mass dependency^{12,13}. Although the exponential mass dependency is simply an empirical fit
90 to the observed mass fractionation in TIMS analysis, it has been shown to be appropriate in the vast
91 majority of TIMS analyses. However, in analyses requiring part per million precision, the measured
92 ratios can deviate from exponential law fractionation^{7,14,15}. These measured deviations from exponential
93 law are typically interpreted as reflecting an ion beam that is derived from the combination of emission
94 from a number of variably fractionated reservoirs on a filament. This type of “mixing” imparts a linear,
95 not exponential, overprint on the otherwise exponential mass fractionation of isotope compositions^{7,12,14-}

96 ¹⁶. The exact mass dependency of the fractionation present in an ion beam derived from an unknown
97 number of reservoirs with an unknown extent of fractionation is impossible to accurately correct. The
98 problem is compounded in runs involving larger sample sizes as they more often contain periods of
99 complex mass fractionation during analysis. Thus, common practice involves removing sections of an
100 analysis that show clear signs of non-exponential mass fractionation (i.e., decreasing heavy/light isotope
101 composition with time) so as to avoid generating biases induced by inappropriate mass fractionation
102 correction ^{7,8,14–16}. This practice, however, may not completely account for such effects that contribute to
103 reproducibility at the parts-per-million level.

104 In this work, we explore the possibility that an alternative ion source design may overcome these
105 limiting factors and ultimately allow sub-ppm isotope ratio precisions. A suite of ion source designs has
106 been shown to generate ions at a rate many times higher than traditional TIMS methods ^{5,17,18}. These ion
107 sources, which we will refer to as thermal ionization cavity sources (TIC), have gained use in the nuclear
108 physics and on-line isotope separator communities but have never gained significant traction within the
109 geosciences. The main limitations include the complexity of the cavity designs along with the very high
110 temperatures involved that stress vacuum systems and exacerbate the need for ultrapure cavity materials
111 in order to minimize background signals. In this work we present a simple TIC ion source design that
112 shows the potential for TIC to produce very large ion beams for extended periods of time, with predicted
113 precisions that are a necessary prerequisite to push isotope ratio precision into the sub-ppm range.

114 In summary, isotope ratio precisions in the ppm range are limited by two main factors: 1) the number
115 of ions counted, and 2) variable mass fractionation behavior. As sample size increases in flat-filament
116 TIMS, ionization efficiency decreases and non-exponential mass fractionation increases. Both work in
117 the direction of leading to less precise isotope ratios.

118 **Previous cavity source designs**

119 Cavity ion sources were initially proposed in the 1970's ^{17,18} as a method to achieve isotope
120 separation of milligram-sized samples for nuclear studies. Since that time many iterations have been
121 developed, but to our knowledge only online isotope separators ¹⁹ and one other geoscience laboratory ²⁰
122 currently use the technology. A recent publication ⁵ contains a thorough review of the development
123 history of TIC sources. Despite a wide variety of ionization geometries and mass analyzers, including
124 magnetic sector ^{5,20–22}, quadrupole ^{23,24}, and time-of-flight analyzers ²⁵, all cavity ion sources share some
125 similarities. The essential components of TIC sources are a high-aspect-ratio cavity drilled into a high-
126 work-function metal such as Re, Ta, or W. Sample material is loaded into the rear of this cavity, which is

127 then electrically heated to high temperatures. Initial designs were simple and focused on generating large
128 ion beams from large samples for isotope separator laboratories ^{17,18}, and these forms of TIC sources
129 remain in use among the nuclear physics community ¹⁹ though typically used for smaller samples.
130 However, recent TIC source developments have been driven to achieve maximum ionization efficiency
131 from very small (picogram) samples sizes of high ionization potential elements (e.g., U, Pu, Am), usually
132 driven by the analytical needs of the nuclear forensics community ^{20,26}.

133 The physics of ionization in a cavity have been well-summarized ^{27,28}. The dominant mechanism of
134 ionization at temperatures <2700 K, in typical-sized cavities, seems to be thermal ionization from the
135 cavity walls. This situation is similar to traditional flat-filament TIMS sources, except that confined
136 analyte atoms do not immediately escape the hot enclosure after evaporation. Instead, any atom that
137 evaporates, but does not ionize will likely come into contact with another hot inner surface of the cavity.
138 Thus, the proportion of atoms that eventually get ionized is increased as each atom has many more
139 opportunities to be ionized by thermal contact with hot cavity walls. Maden et al. (2016) developed
140 modeling code that accounted for space charge within the cavity and showed that space charge along the
141 cavity walls, dominantly derived from thermally-emitted electrons, aids in ion extraction from the cavity.
142 At temperatures above ~2700 K, a quasi-neutral plasma may exist inside the cavity, thus increasing
143 ionization ²⁷ but potentially creating an environment where ion movement becomes diffusive, thus
144 changing extraction properties ²⁸. Independent of whether a quasi-plasma exists within a particular cavity
145 design, TIC sources have been shown to provide higher ionization efficiencies than traditional flat
146 filament arrangements, with ionization increases of up to a factor of 40 for elements of geologic interest.
147 Despite decades of development by many different laboratory research groups, TIC sources have never
148 achieved routine use in the geoscience community. Below, we highlight two recent cavity arrangements
149 both aimed at converting modern-style TIMS mass spectrometers to TIC sources for use in isotope ratio
150 analyses and summarize their results.

151 Driven by the goal of developing a mass spectrometer that could be quickly converted between a
152 cavity and flat-filament source, the research group at Oak Ridge National Laboratory employed a TIC
153 source first on a Finnigan MAT262 ^{29,30}, followed by installation on a Thermo-Fisher Triton TIMS
154 instrument ^{21,26}. This TIC geometry was created by inserting an electrically insulated barrel within the
155 commercial Triton barrel configuration. This new inner barrel was held at the +10 kV operating voltage
156 of the Triton instrument while the outer, conventional barrel was stepped down to +8.5 kV. Cavity rods
157 were mounted on the inner barrel such that the conventional filaments, now held at -1.5 kV relative to the
158 cavity rod, provided electron bombardment current upon heating. In this way 21 cavity samples could be
159 installed on a single modified barrel yet the Triton software and data collection system remained

160 unaffected by the presence of the cavity ion source. Using this TIC setup, the Oak Ridge group showed
161 that small (<10 ng) loads of Nd and Sr could have total efficiencies approaching 20 – 30% ^{21,26}. However,
162 the stability and longevity of analytical runs were limited by alignment inefficiencies and arcing within
163 the source due to the complexity of the cavity arrangement. Additionally, the dramatic total efficiency
164 improvements found on the MAT262 instrument were apparently not seen on the Triton installation ²¹,
165 perhaps due to the modification of the MAT262 ion lens system for cavity ion beams ^{29,30} and the design
166 constraint that the Triton ion focusing system remain unaltered for normal filament operations.

167 More recently, the research group at ETH Zurich has transitioned a multi-collector magnetic sector
168 mass spectrometer (Finnigan MAT262) to a TIC machine ^{5,20}. This design employs a dual-piece cavity
169 assembly, a +10 kV accelerating voltage, and a cavity arrangement that utilizes a flat carbon plate to
170 prevent electrons from impacting the ion beam while providing precise cavity location control. An
171 additional advance is provided by a redesigned electrostatic focusing lens stack and positional drive
172 system capable of actively moving cavity tip location, aiding in optimizing ion transmission. Thus far,
173 the ETH TIC has produced total efficiency data on U ^{5,20} analyses that showed >10 times improvement in
174 the total efficiency relative to flat-filament TIMS. The ETH TIC is distinct from the Oak Ridge design in
175 that it can accommodate only one cavity at a time, it contains a modified lens stack, and it uses larger
176 cavity dimensions. Nevertheless, the ETH source has produced total ionization gains relative to flat
177 filament TIMS that were better than the Oak Ridge Triton cavity setup ²¹, but not substantially improved
178 from the initial Oak Ridge cavity installed on a modified Finnigan MAT262 ^{29,30}.

179 Though cavity ion sources have shown substantial improvements in ionization efficiency ^{20,28,30} in
180 isotope ratio measurements they have yet to become standard analytical tools in the geoscience
181 community. The reasons for this are not entirely clear, but what is evident is that most recent cavity ion
182 source developments have focused on achieving utmost efficiency from very small sample sizes. This
183 analytical focus, though an obvious use for high-efficiency cavities, suffers from competition with design
184 improvements that allow for quantitative measurement of small ion beam sizes ³¹ as the signal-to-noise
185 ratio often dominates the uncertainty budget of isotope ratio measurements of small samples using
186 Faraday cup detectors. In the present work, we take a different approach and focus on improvements that
187 can be made to analyses where element abundance is not the main limiting factor. Our aim is to use
188 cavities to generate relatively large ($5e^{-10}$ amp) ion beams from large sample sizes ($>1 \mu\text{g}$) and measure
189 them for long periods of time (several hours) to achieve isotope ratio precisions at the level of parts per
190 million or better. This approach allows us to relax design constraints aimed at peak ionization efficiency,
191 such as operating cavities at very high temperatures, that, in part, lead to some of the issues that have kept

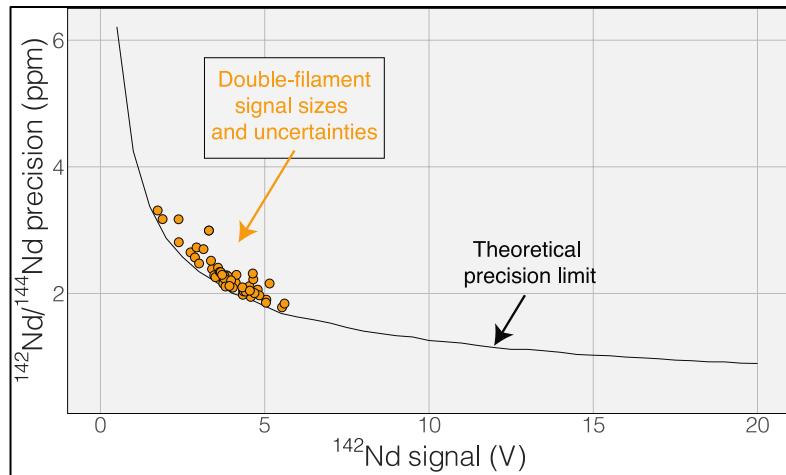
192 cavity ion sources from common use, e.g. contamination of the source region by evaporated cavity
193 material and background signals from insufficiently pure cavity metals.

194 **Analytical background and approach**

195 The elements samarium (Sm) and neodymium (Nd) are extremely useful for the geoscience
196 community, as well as nuclear forensic ³², applications. Particularly relevant to the geosciences are the
197 two radioactive isotopes of Sm, ¹⁴⁶Sm and ¹⁴⁷Sm, that undergo alpha decay to ¹⁴²Nd and ¹⁴³Nd,
198 respectively ³³. Due to the slightly different chemical behavior of Sm and Nd, the long-lived ¹⁴⁷Sm-¹⁴³Nd
199 decay system, with a half-life of ~106 billion years, has been widely implemented in the geosciences
200 community since the 1970's. The variations in ¹⁴³Nd/¹⁴⁴Nd induced by radioactive decay of ¹⁴⁷Sm over
201 geologic time are readily detectable with isotope ratio precisions of better than 0.01%, making this system
202 relatively easy to utilize with modern analytical systems. The other decay system, ¹⁴⁶Sm-¹⁴²Nd, has a
203 much shorter half-life of ~103 million years and, due to the low abundance of ¹⁴⁶Sm at the start of the
204 Solar System, imparted much smaller variations in the daughter isotope ratio ¹⁴²Nd/¹⁴⁴Nd. Quantification
205 of the variability in ¹⁴²Nd/¹⁴⁴Nd allows for detection of changes in Sm/Nd during the lifetime of ¹⁴⁶Sm,
206 lasting for the first 500 million years of Solar System history, allowing for accurate chronology of Solar
207 System materials ³⁴, tracking of silicate differentiation on Earth and other rocky solar system bodies
208 (Boyett and Carlson, 2005; Carlson et al., 2014; Harper and Jacobsen, 1992), and identification of Hadean
209 reservoirs still present on the modern Earth ^{9,10}. These small ¹⁴²Nd/¹⁴⁴Nd variations are only detectable
210 with isotope ratio measurements that are precise at the parts-per-million level, as the total natural
211 variation in ¹⁴²Nd/¹⁴⁴Nd in Earth materials is only ~50 ppm. Thus, very precise isotope ratio
212 measurements are required to fully utilize the short-lived ¹⁴⁶Sm-¹⁴²Nd system.

213 Modern precisions in the measurement of ¹⁴²Nd/¹⁴⁴Nd are on the order of 3-4 ppm ^{2,7,10}. This level of
214 precision requires measurement times on the order of a dozen hours with beams around 5e-11 amperes
215 (equivalent to 5V on a 10^{11} Ω resistor). As shown by ⁷, internal precision in the ¹⁴²Nd/¹⁴⁴Nd isotope ratio
216 of multidynamic TIMS measurements is only slightly poorer than the theoretical limits imposed by shot
217 noise (Figure 1). This means that the internal precision is chiefly dependent on the number of ions
218 detected during a given measurement.

219 *Figure 1: Uncertainty in*
 220 *$^{142}\text{Nd}/^{144}\text{Nd}$ plotted as a function*
 221 *of the average ^{142}Nd signal size*
 222 *during a 6-hour analysis. The*
 223 *actual measurements are shown in*
 224 *orange and track the theoretical*
 225 *limit imposed by shot noise*
 226 *(Poisson noise), modeled using a*
 227 *multi dynamic collection routine*
 228 *that dramatically decreases the*
 229 *impact of collector efficiency variations*⁷. *The close correlation between measured and calculated*
 230 *uncertainty suggests that the uncertainty budget is dominated by shot noise such that increasing signal*
 231 *size would be the most effective route to improving the internal precision of any given analysis.*

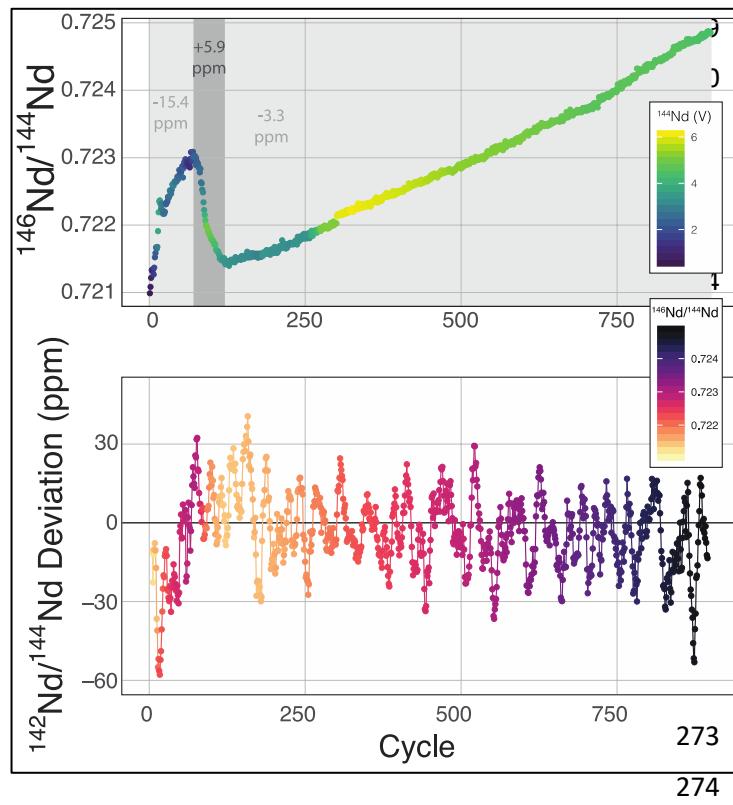


232 While the internal uncertainty budget is dominated by shot noise, modern measurements achieve
 233 internal precisions that push the limits of external reproducibility. In our experience, the external
 234 reproducibility on modern double-filament Nd-isotope measurements remains ~4-5 ppm, with
 235 measurements of standards producing measured $^{142}\text{Nd}/^{144}\text{Nd}$ values that do not agree within the limits of
 236 internal uncertainties. Our interpretation of this irreproducibility relies on observations of changing mass
 237 fractionation, and deviations from exponential law, during any particular analysis (Figure 2). Though this
 238 may seem to limit internal precision gains made by higher ion yields, cavity ion sources may provide a
 239 means to more accurately quantify, and correct for, non-exponential mass fractionation and isobaric
 240 interferences.

241 Mass fractionation during a TIMS measurement that deviates from exponential law is typically
 242 interpreted to reflect an ion beam composed of a mixture of ions derived from sample regions on the
 243 filament that have experienced different fractionation histories^{7,12,14-16}. This process will vary from
 244 analysis to analysis, potentially leading to significant external variability. The combination of ions
 245 originating from variably fractionated sample domains on the filament will generate isotope ratio
 246 deviations in predictable directions, calculated by considering the particular ratios used in mass
 247 fractionation corrections. For instance, while using $^{146}\text{Nd}/^{144}\text{Nd}$ to correct $^{142}\text{Nd}/^{144}\text{Nd}$, mixing of the ions
 248 emitted from variably fractionated domains on a filament will produce positive deviations from
 249 exponential law, most easily visualized on a three-isotope plot^{14,15}, creating an artificial increase in
 250 $^{142}\text{Nd}/^{144}\text{Nd}$. In fact, this type of behavior is readily observable at the ppm precision level, as shown in
 251 Figure 2. During the analysis highlighted in Figure 2 (a typical analysis of JNdI standard solution from⁸),

252 data taken while the sample was reversely fractionating (decreasing $^{146}\text{Nd}/^{144}\text{Nd}$ with time) have a
 253 $^{142}\text{Nd}/^{144}\text{Nd}$ ratio that is ~ 10 ppm higher (+5.9 versus -3.3 relative to a $^{142}\text{Nd}/^{144}\text{Nd} = 1.141832$), on
 254 average, than the rest of the cycles measured during the analysis. While the analysis shown in Figure 2 is
 255 readily filtered to remove portions of the analysis that may be affected by non-exponential mass
 256 fractionation at the >15 ppm level, other, less obvious, periods of such behavior within an analysis may
 257 not be so readily removed.

258



274 *Figure 2: Mass fractionation during a single Nd-isotope measurement using the methods described in ⁷. The top panel shows the measured $^{146}\text{Nd}/^{144}\text{Nd}$ ratio without mass fractionation correction as a function of the cycle number (each cycle is ~ 45 seconds with the total run lasting ~ 13 hours) with symbol colors corresponding to the ^{142}Nd signal size in volts across a $10^{11} \Omega$ resistor. The grey fields show three sections of the run, divided by fractionation trends, with the numbers indicating the average deviation from exponentially-corrected $^{142}\text{Nd}/^{144}\text{Nd}$ over that section of the analysis (all fractionation corrected to an assumed*

275 $^{142}\text{Nd}/^{144}\text{Nd} = 1.141832$) The bottom panel shows a ten-point moving average of the deviation of each
 276 fractionation-corrected $^{142}\text{Nd}/^{144}\text{Nd}$ ratio from exponential law fractionation correction. Each measured
 277 $^{142}\text{Nd}/^{144}\text{Nd}$ ratio was time- and fractionation-corrected using a multi-dynamic collection scheme ⁷, and
 278 then normalized to a $^{142}\text{Nd}/^{144}\text{Nd} = 1.141832$. The variably colored line connecting data points shows the
 279 sequence of cycles to aid interpretation.

280 Given the above considerations regarding precision and reproducibility during high precision Nd
 281 isotope analyses, we endeavored to implement a cavity ion source in a different manner than what has
 282 been attempted previously. Instead of optimal ionization from very small sample sizes, we aim to use the
 283 cavity ion source to generate large ($>5\text{e-}10$ A) Nd ion beams for long periods of time (several hours).

284 Our development and design aimed to test whether cavity ion sources can provide a path towards sub-
285 ppm Nd-isotope ratio precisions by, 1) generating large ion beams from large samples for long periods of
286 time, thus driving down shot noise uncertainty, and 2) providing a means to more accurately correct for
287 mass fractionation during TIMS analyses. Our approach and implementation thus allowed us to simplify
288 a cavity ion source design as very high temperatures are not necessarily needed for our approach. This
289 allows us to avoid engineering issues such as deposition of evaporated metal on insulators within the
290 source housing ²⁶ and controlling outgassing of the source components during high temperature operation
291 that may lead to high-voltage arcs ⁵.

292 The present work did not aim to produce higher total efficiencies than those achieved in modern
293 TIMS instruments as previous publications have clearly shown that cavity ion have sources the ability to
294 generate higher total efficiency for Nd than flat-filament TIMS ^{23,24,26}. Thus, we did not focus our design
295 efforts on optimizing the ionization efficiency by, for instance, testing a wide range of loading techniques
296 or additives ^{20,21}, or by substantially modifying the cavity dimensions; these improvements are clearly
297 possible with cavity ionization. Instead, we focused our design on testing whether large Nd⁺ ion beams
298 can be generated for long periods of time, producing total ion counting statistics that could drive down
299 internal precisions.

300 **Cavity design**

301 ***Mass spectrometer testbed and heating design***

302 Our cavity configurations were tested on a Carnegie-built single detector magnetic sector mass
303 spectrometer. This instrument is a 60-degree sector, 15-inch radius, Nier geometry magnetic sector mass
304 spectrometer with a single fixed faraday detector that can be moved to accommodate a secondary electron
305 multiplier. Ion beam intensities were measured by a Keithley 642 Electrometer, which was digitized
306 using a Keithley 2001 Digital Voltmeter and later by a Schumberger Solartron 7060 Systems Voltmeter.
307 All magnet control, data collection, and data reductions were performed using a custom LabVIEW
308 program written in-house.

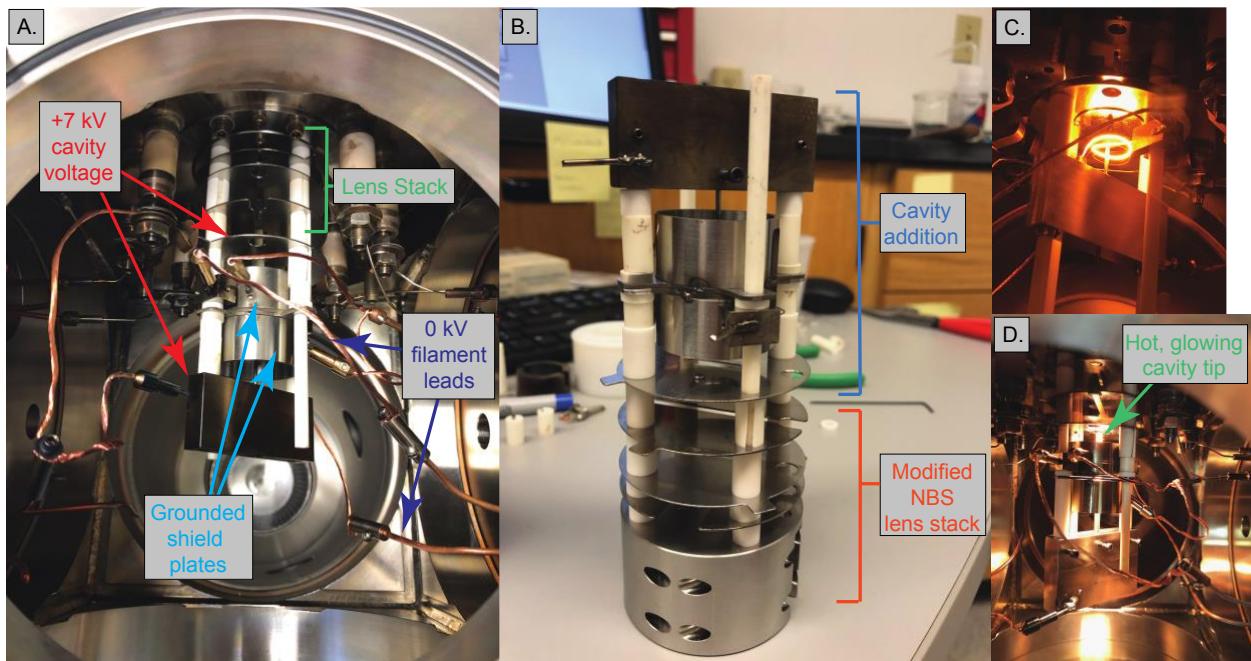
309 Our cavity ion source was heated using electron impact heating. This type of heating has been the
310 most common design implemented in TIC sources and we chose this design to avoid the requirement for
311 very large currents at high voltage required to resistively heat a cavity. A 0.4 mm diameter tantalum
312 filament was used as electron source and held at ground potential. Current was passed through this
313 filament using a Kepco JQE 0-50V, 0-10A power supply. Upon heating the filament provided an electron

314 current that impacted, and heated, the cavity source. The bombardment (heating) current was monitored
315 by the current absorbed by the cavity power supply and controlled manually. The voltage to the cavity
316 was provided by a Spellman SL2000 power supply capable of producing +15 kV at 110 mA. The
317 electron bombardment current was monitored by the Spellman power supply, where the current readings
318 were equivalent to the electron bombardment current from the grounded filament to the cavity. We
319 operated our cavity source at voltages between +5 to +7 kV. The electron bombardment currents during
320 an analysis scaled with the cavity voltage; heating power extended up to ~300 W, requiring 60 mA
321 bombardment current with a +5 kV cavity and 42 mA with a +7 kV cavity.

322 Two different ion optical lens systems were employed during our operation. The original lens system
323 on the 15-inch mass spectrometer is an NBS thin lens ³⁹. This ion source consisted of several lens
324 elements made of 0.4 mm thick stainless steel with voltages provided by a resistor chain that output
325 voltages from +5 kV to ground. During our testing of the TIC source we determined that many of the
326 optical elements of the original lens system were likely unnecessary as they had little impact on detected
327 ion current across a range of voltage settings. Consequently, we simplified the lens system by removing
328 the discriminator and draw-out plates, keeping only x-focus and z-focus (y being the ion optical axis)
329 plates in addition to a defining plate and final collimating slits, all kept at the same dimensions as the
330 initial configuration. Data collected using this modified Shields source is presented in Table 1. This
331 configuration was, unfortunately, limited in its voltage range such that during many analyses the x- or z-
332 focus plates were at their maximum voltage difference, potentially limiting ion transmission. As a
333 potential improvement, we opted to test a second ion lens system. This second optical design was
334 modeled after a simplified lens system designed for a triple-filament ionizing source ⁴⁰. In this Loveless
335 and Russell source focusing system, only one set of four thick plate electrodes is employed, along with a
336 pair of grounded collimating slits as in the initial design. The four electrodes are held at a potential close
337 to the ionization source forcing the ions to follow damped oscillatory paths that are focused at the
338 collimating slit (Figure 4). We employed a slightly larger version of the Loveless and Russell source
339 design for several of our analyses (Table 1).

340 The 15-inch mass spectrometer ion extraction system is mounted on four ceramic rods (Figure 3A,B),
341 having a ~0.01 mm smaller bore than the lens plates, to prevent differential thermal expansion from
342 breaking the ceramic rods. In the case of both lens stack systems, we built the cavity ion source directly
343 out from this existing lens system such that our cavity source would be easy to position reproducibly in
344 the center of the lens system. A large, grounded, cylindrical shielding plate surrounded most of the hot
345 cavity to prevent cavity material from being deposited on the ceramic insulating rods. This shielding
346 plate also surrounded the electron bombardment filament through which the filament heating leads where

347 positioned. Finally, cavities were held by a stainless-steel block that was fixed to two of the ceramic
 348 mounting rods extending from the lens stack (Figure 3). This block was held in place using set screws,
 349 and the entire assembly was affixed to long ceramic rods mounted to a base block mounted inside the
 350 source housing. Our cavity design left the cavity attached to the mount at its base, away from the
 351 ionization tip. The stainless steel block was held snugly against ceramic tubes cut to length to maintain a
 352 constant cavity y-position in front of the extraction lens system. Likewise, the cavity was held in the
 353 stainless steel block with a set screw, and positioned manually using a measured mounting block such that
 354 the length of cavity sticking out in front of the stainless block was reproducible. However, the cavity
 355 ionization tip was freely floating, meaning that the cavity position may have changed during an analysis
 356 through sagging during high-temperature operation, altering the focal properties. Unfortunately, this
 357 sagging was only observable through a change in the lens stack voltages that achieved optimal ion
 358 transmission and was impossible to accurately quantify. This is distinct from the ETH design which fixes
 359 the ion source location by attaching the cavity tip to a graphite plate that controls the ion extraction
 360 location in x,y,z space ⁵.



361

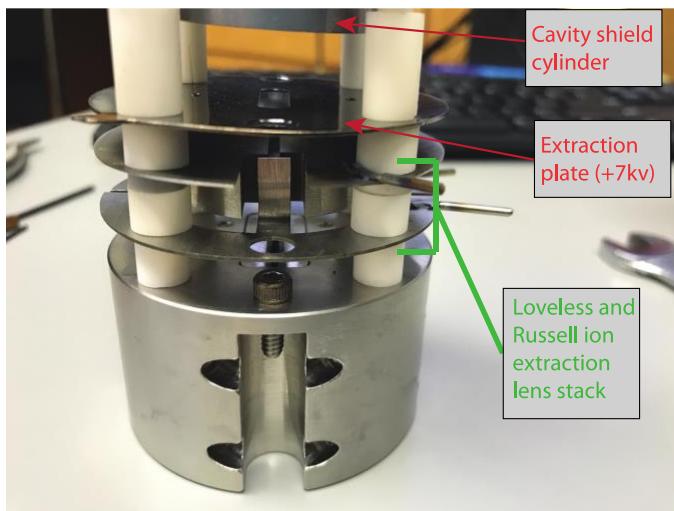
362 *Figure 3: Images of the cavity ion source mounted on the Carnegie 15-inch single-collector instrument.*
 363 *A: The cavity ion source installed inside of the source housing of the 15-inch mass spectrometer with the*
 364 *modified Shields lens stack. B: the cavity assembly mounted on rods extended out from the modified*
 365 *version of the NBS lens stack. C: The cavity heated up without the shield plate in place so that the*
 366 *electron-emitting filament can be seen (the original, unmodified, NBS lens system is shown in this figure).*

367 *D: The cavity under operating conditions, with the hot tip of the cavity visible and the electron-emitting*
368 *filament hidden behind the shield plates. Note that this version had the tip of the cavity closer to the*
369 *extraction lens plate than that shown in B. The performance characteristics were not detectably different*
370 *between these two systems.*

371 During this work we used cavities made of Ta rod with a 3.1 mm outside diameter (supplied by H
372 Cross company, 99.7% Ta). The cavities were made by electrical discharge machining 1.5 mm wide
373 holes into the Ta rod, creating cavities of various depths (10-40 mm; Table 1) and 1.5 mm diameters. The
374 diameters were chosen to match both the machining capabilities of the Carnegie machine shop and be
375 comparable to the dimensions of cavities recently shown to produce high ionization efficiencies in other
376 labs^{5,21}. Tantalum was used as the cavity material during our analyses due to the low cost and ease of
377 machining relative to Re. Analyte Nd was loaded into cavities in a 2M HCl solution containing 1ppm Nd
378 using a 10 μ L syringe (Hamilton syringe 10 μ L, Model 701 RN SYR, Part #7635-01). Carbon additive
379 was loaded in the same manner using AquaDAG solution of colloidal graphite. AquaDAG was loaded on
380 top of dried down Nd sample at the base of the cavity. During some analyses, Re powder was also added
381 to the cavity to aid in ionization. Re powder (99.7 % Re) was suspended in MilliQ water and ~2 μ L was
382 loaded on top of the Nd HCl solution before drying. For some analyses, cavities were re-used several
383 times. While cavities were not completely cleaned of Nd prior to loading another analysis, we are
384 confident that only a small fraction of the total ions detected may have come from prior sample loadings.
385 This is due to several factors. First, we typically removed and replaced the Re lining in between sample
386 loads, which significantly reduced the amount of Nd remaining in any previously used cavity. Also, we
387 discovered that upon cooling a cavity and reheating, the ion beam signal size would only return to
388 significant size when it reached heating powers close to the maximum power of the previous analysis.
389 This means that as long as subsequent analyses remained at heating power below the previous maximum,
390 very little ionization of previous analyte occurred. We attempted to clean cavities by boiling in 8M HNO₃
391 overnight, and subsequent ultrasonication, but this appeared to only have a limited effect on presence of
392 Nd in the cavity. More testing will need to be accomplished to fully clean previously used cavities.

393 During the latter stages of our analysis, we lined the Ta cavities with Re foil to create a higher work
394 function surface on the inside of the cavity. The Re foil was 0.025 mm thick 99.7% pure Re foil from
395 Thermo-Fisher (#010307-FI), which was cut to size, wrapped around a post, inserted into the cavity, and
396 expanded to firmly contact the Ta cavity walls. After initial testing, we also inserted two Re filaments
397 (99.7% pure from H Cross) in a cross pattern into the base of the cavity before loading the cylindrical foil
398 lining so that analyte loaded into the bottom of the cavity would be loaded onto Re instead of bare Ta.
399 This was an attempt to further reduce NdO⁺ production.

400 *Figure 4: An image of the Loveless and Russell ion extraction source system used in this work. In order*
401 *of top to bottom, the tip of the grounded cavity shield cylinder is exposed at the top of the image (with no*



cavity installed), followed by the +7 kV extraction plate, then the x-symmetry plates of the Loveless and Russell source, followed by the z-symmetry plates. The bottom block contains the two collimator slits and is the original part of the 15-inch mass spectrometer.

410

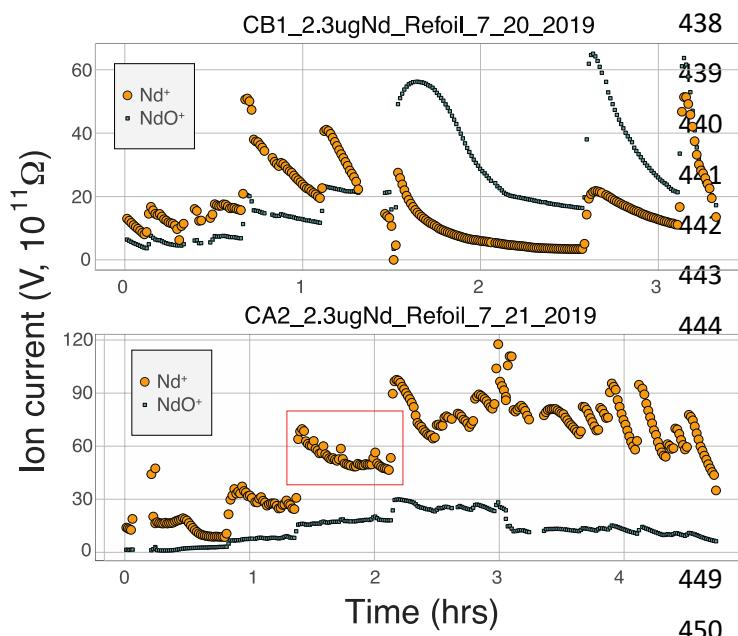
411 **Results and Discussion**

412 **Signal size:**

413 During the course of our testing and analysis we focused on generating large ion beams of Nd^+ for
414 long periods of time using cavity loads of 2 micrograms as we regularly separate 2 μg of Nd from
415 geological samples. A Nd^+ signal was detectable on our faraday detectors when the heating power
416 approached ~ 80 W (~ 12 mA with +7 kV cavity voltage). Upon first appearance of a Nd^+ beam, the signal
417 grew rapidly during initial heating before decreasing, all at a constant heating power. Ion beam tuning
418 was completed manually during heat up and before starting data collection. If signal sizes or isotope
419 ratios degraded during data collection, the run was aborted and the signal refocused and tuned. After this
420 initial signal increase, the signal size grew exponentially with increased bombardment current and
421 eventually stabilized. Once large signals were achieved, they began to slowly decay over time and
422 required an increase in the electron bombardment current to maintain the signal size. Overall, this
423 behavior is similar to the behavior of Nd^+ during double filament analyses, suggesting that similar
424 processes govern the evaporation and ionization of Nd from the surface of the cavity.

425 Several of our runs produced ion beams $> 5 \times 10^{-10}$ amps that lasted for several hours (Figures 5, 7).
426 However, there was significant variability in the total efficiency of each run. The highest signal sizes
427 were all generated using the simplified Shields lens system. However, some runs using this lens system

428 produced low total ionization yields. These low intensity runs were conducted under sub-optimal ion
 429 focusing conditions, where the voltage difference on the x-focus or z-focus plates was at a maximum.
 430 This implies that optimum focus was not achieved, and some fraction of the ion beam was not being
 431 directed into the collimating slit, likely producing a substantial reduction in total ion yield. Our
 432 interpretation of the scatter in total ion yields using the simplified Shields source is that lower ion yields
 433 represent runs where the focusing properties of the ion source was not optimal and suffered ion
 434 transmission degradation. An added component to the variable efficiencies was the different cavity
 435 loading procedures used, as described previously. Though widely varying cavity dimensions were used,
 436 no systematic variation in ionization efficiency was observed that correlated with cavity depth. More
 437 testing is required to optimize this feature of the cavity design.



438 *Figure 5: Production of Nd^+ and NdO^+ over the course of two analyses with high*
 439 *ion yields. Both measurements were*
 440 *made using the modified NBS lens*
 441 *system. The top analysis was made with*
 442 *a Ta cavity with Re foil lining only the*
 443 *cavity walls. The bottom analysis was*
 444 *made with a Ta cavity that had Re foil*
 445 *lining the walls as well as Re filaments in*
 446 *the bottom of the cavity and Re powder*
 447 *added to the sample solution during*
 448 *loading. Each step function increase in*
 449 *signal size corresponds to an increase in*

451 *the heating power.*

452 The difficulty associated with optimizing ion focusing during ionization from a cavity source has
 453 been highlighted in other work ^{5,21}. To test a new approach, and guided by modeling using the SIMION
 454 modeling software, we implemented a modified Loveless and Russell ion optics design ⁴⁰ that was shown
 455 to produce significantly higher ion transmission when using a triple-filament ion source arrangement.
 456 Our design of the power supply system allowed for independent determination of the top voltage of the
 457 four steering plates in the lens system, with each plate then separately tunable using a parallel resistor
 458 chain with ~300 V of range. Our experiments showed that the Loveless and Russell lens system had
 459 excellent ion beam steering capabilities and was insensitive to x-focus and z-focus setting; that is, the
 460 signal intensity was simple to optimize and remained relatively constant throughout each analysis. The

461 Loveless and Russell ion source system was designed to have the steering plates held at a voltage close to
462 the accelerating voltage (~5 V lower than maximum), and our optimum peak shape and ion transmission
463 occurred near the +5 kV accelerating voltage of the cavity. However, the total efficiencies were
464 substantially decreased with this lens system compared to the modified NBS source (Table 1), indicating
465 that overall ion transmission was suboptimal. Our interpretation for suboptimal focusing is that the ion
466 beam was not fully collimated and focused at the defining slit such that only a small fraction of the
467 defocused beam was transmitted through the mass spectrometer, as evidenced by the relatively
468 insensitivity to x and z voltage settings.

469 Regardless of the difficulties in ion focusing, our cavity ion source has shown a promising ability to
470 produce large ion beam sizes for long durations. When the total ion counts from our TIC source are
471 compared to flat-filament measurements, they predict sub-ppm precisions in the $^{142}\text{Nd}/^{144}\text{Nd}$ isotope ratio
472 (Figure 6). These promising results were obtained in spite of several limitations in our current approach.
473 As discussed above, our ion focusing systems suffered from suboptimal performance in both designs; the
474 modified shield lens could not achieve optimal focusing while our modified Loveless and Russell source
475 displayed a substantial decrease in ion transmission. We did not run the Nd loaded into our cavities to
476 exhaustion. Though signal sizes continued to decline near the end of analyses, substantial Nd ion beams
477 often remained upon termination of the analysis. We did not push the temperature on our cavity to the
478 extremes that might be possible, so our ionization efficiencies (Table 1) are minimum estimates. Given
479 the cavity ion source efficiency increase shown by other labs, substantial additional gains in total ion
480 yields certainly appear possible with our TIC source design if ion transmission is improved with a
481 modified focusing system and the cavities are run to higher temperature to exhaust the analyte.

482

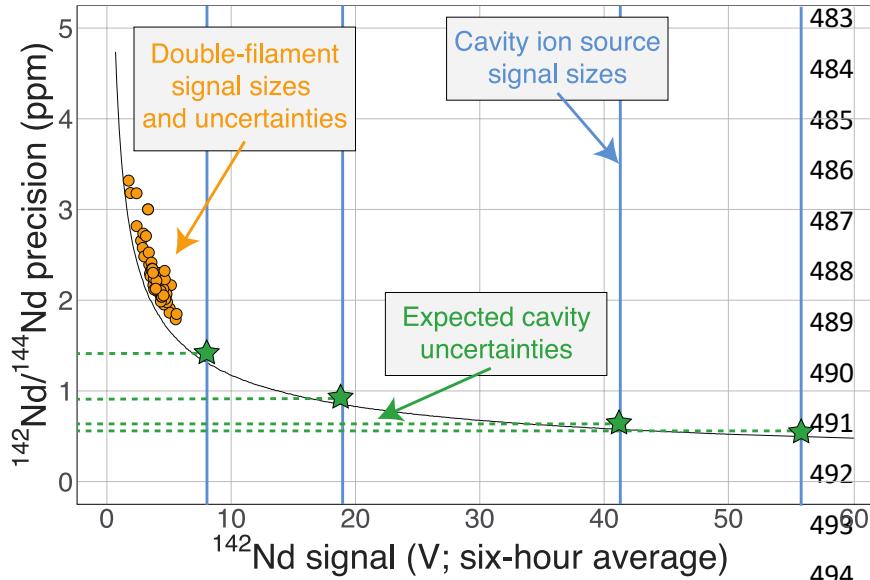


Figure 6: A modified version of Figure 1 showing the cavity ion yields. The average ^{142}Nd signal size in volts (relative to a $10^{11} \Omega$ resistor) during a 6-hour multi-dynamic Triton analysis⁷ is plotted against the internal precision achieved during that run⁸. The black curve is the precision limit imposed by shot noise while

495 the orange circles are actual double-filament analyses from samples and standards⁸. The vertical blue
 496 lines are total ion yields from the cavity ion source using 2 μg of Nd (the highest signal size line was
 497 measured using 10 μg Nd) converted to average signal size over six hours if these analyses were made on
 498 the Triton. The horizontal green dashed lines and stars are the predicted precisions of our cavity ion
 499 source analyses if mass fractionation corrections are similar, with the best analyses theoretically pushing
 500 the precision of the $^{142}\text{Nd}/^{144}\text{Nd}$ measurement below one part per million.

501

502 **Neodymium oxide production**

503 Many modern Nd isotopic analyses measure the metal ion, Nd^+ , though analyses of NdO^+ used to be
 504 common³³ and remain in use for analyses of very small analyses⁴¹. The production of NdO^+ ions occurs
 505 at a lower temperature than the metal species, so higher ionization efficiency can be achieved when
 506 analyzing NdO^+ particularly when using an oxygen bleed valve or oxygen-emitter additives to the
 507 filament. Measurement of NdO^+ does not, however, provide a likely path towards more precise and
 508 accurate $^{142}\text{Nd}/^{144}\text{Nd}$ measurements as multiple isobaric interferences, and potential oxygen isotope
 509 fractionation during an analysis, must be accounted for when measuring polyatomic oxide species⁴².

510 To our knowledge, there has been only limited documentation of the various metal/oxide ion
 511 production abilities of Nd while using a cavity ion source, though metal/oxide production has been
 512 investigated for other elements during short analysis times (<10 min^{5,20,25}). Though colloidal carbon
 513 (AquaDAG) is often used during mass spectrometry as a chemical reductant on the filament, the cavity

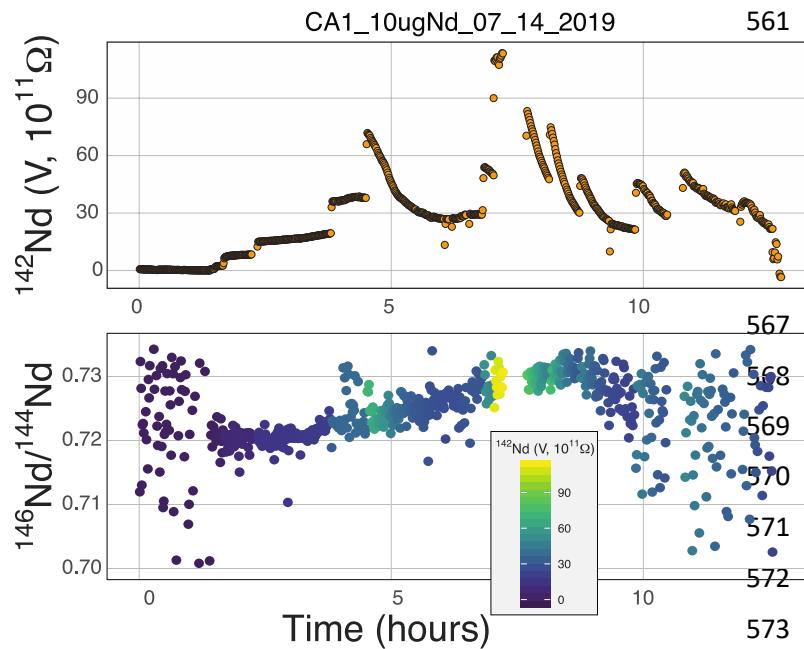
514 community has also used carbon (either colloidal graphite or organic resin bead loading) as an additive to
515 increase the work function of the ionizer, in addition to a chemical reductant, where ReC has a higher
516 work function than Re metal ^{5,21}. To evaluate the metal/oxide ionization within cavities, we tracked
517 Nd⁺/NdO⁺ for the vast majority of our analyses. During most of our analyses, NdO⁺ often had a higher
518 signal during the initial portions of the analyses, Re and C additives or a Re foil inside of the cavity aided
519 in production of Nd⁺ (Table 1), optimizing ionization of the metal ion. During some analyses, however,
520 NdO⁺ was the preferred species (Figure 5). The analysis shown in top panel of Figure 5 is from a cavity
521 that was lined with Re foil but did not have Re lining the base of the cavity. During the low-temperature
522 beginning of the analysis, Nd⁺ is the dominant ion species, but in the middle of the analysis, NdO⁺
523 becomes the dominant species. One possible interpretation is that as temperatures increase NdO⁺ begins
524 to ionize directly from the Ta base of the cavity, whereas at lower temperatures Nd evaporates as either
525 metal or oxide and is dominantly ionized as a metal during its multiple interactions with the cavity walls
526 after evaporation. An alternative interpretation invokes variable temperature along the cavity such that
527 ions may be extracted from the base of the cavity (as NdO⁺) preferentially at the beginning relative to the
528 later, higher-temperature, portions of the analysis. The lower panel of Fig. 5 shows an analysis made with
529 a cavity that had Re foil covering the inner walls of the cavity as well as the bottom of the cavity and had
530 Re powder as an additive. During this analysis Nd metal ions are dominant throughout the entire duration
531 of the run, showing that limiting the exposure of analyte to the Ta cavity walls increased the metal
532 ionization efficiency.

533 In order to additionally decrease the NdO⁺ production in our cavity designs we loaded colloidal
534 graphite (AquaDAG) along with Nd solution into the base of the cavities. This may have substantially
535 decreased the NdO⁺ production from the cavity; average Nd⁺/NdO⁺ without AquaDAG is 4.7 and the
536 average with AquaDAG is 24.5 (Table 1), though these values are dominated by a few analyses and other
537 factors may play a role. This result suggests that the presence of a reductant (or Re powder) at the base of
538 the cavity has a significant influence over the Nd⁺ production. ²¹ documented a dramatic increase in the
539 ionization efficiency of Nd with either resin-bead loads or C additives from both cavity ion sources and
540 flat filament sources. They, however, interpreted this increase to be driven by the increased work
541 function of ReC, which aids in the ionization of all species. The impact of high-work-function ReC was
542 also invoked by ⁵ who interpreted an increase in U ionization over the lifetime of individual Re cavities to
543 be due to carbon from the graphite mounting plate diffusing into the initially pure Re metal cavity. Our
544 data show that, for Nd analyses, the competing ionization of Nd⁺ and NdO⁺ may play a dominant role
545 over ReC as an ionizer. If formation of ReC was driving the Nd⁺ ionization increase, metal ionization
546 increases would be expected to match with greater production of NdO⁺ due to the increased work function

547 of ReC. Instead, the data suggest that at many times Nd^+ forms at the expense of NdO^+ and the two
 548 signals are inversely correlated during specific periods of the analyses. However, other more complex
 549 processes such as variable temperature distributions within the cavity may have a dramatic impact.

550 **Mass fractionation**

551 Our testbed mass spectrometer has only a single faraday detector so peak hopping was required to
 552 make isotope ratio measurements (typical data collection included $^{142}\text{Nd}^+$, $^{144}\text{Nd}^+$, $^{146}\text{Nd}^+$, $^{148}\text{Nd}^+$,
 553 $^{142}\text{Nd}^{16}\text{O}^+$, and $^{144}\text{Nd}^{16}\text{O}^+$, or some combination of these) therefore the isotope ratios are susceptible to ion
 554 beam intensity variations over the integration times used (between 4 and 10 seconds). Though all of our
 555 beam intensity data is time-corrected to the ^{144}Nd integration time by linear interpolation between two
 556 consecutive measurements of the isotope of interest, non-linear ion beam behavior can substantially bias
 557 resulting isotope ratios. Additionally, significant inconsistency in the ion beam intensity was produced
 558 during analyses, caused by several different factors. First, during initial manual heat-up the electron
 559 bombardment current was often manipulated to stabilize ionization, resulting in ‘jumps’ in ion beam
 560 currents that are not accounted for with a linear time-correction for ion beam intensity.



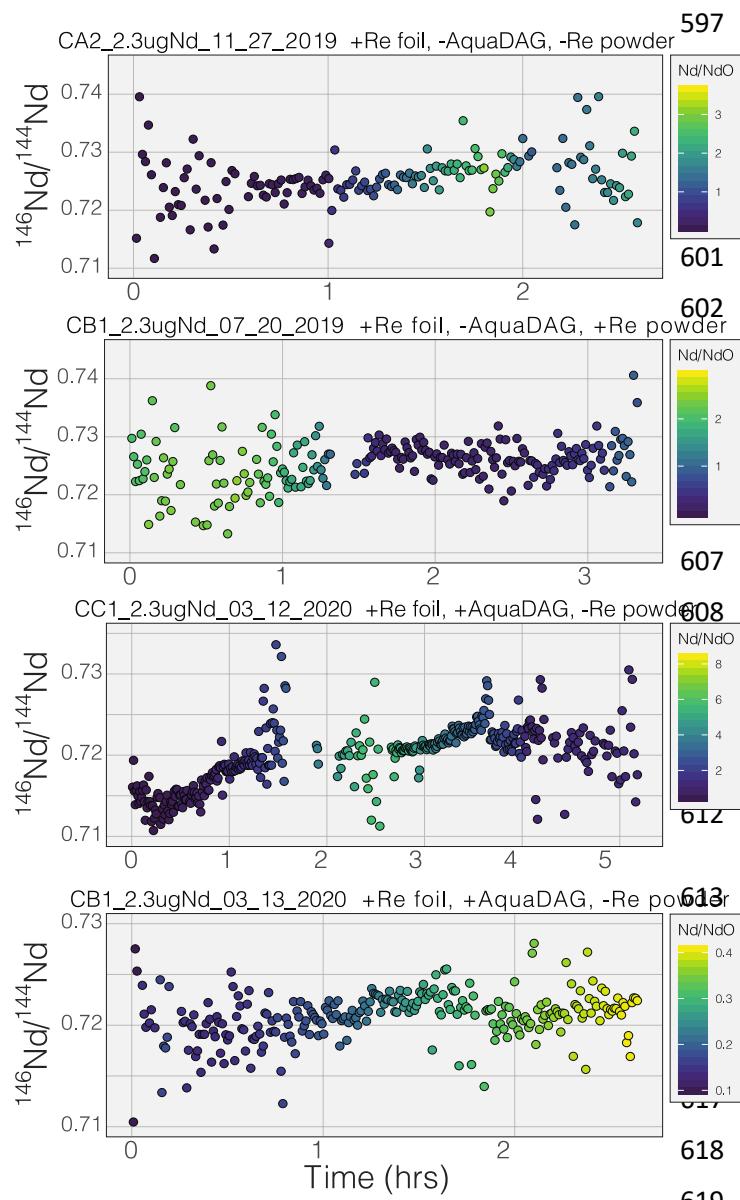
561 *Figure 7: The signal size of*
 $^{142}\text{Nd}^+$ *during an analysis of a 10ug*
Nd load in a Ta cavity with C+Re
additives (the NdO^+ signal stayed
below 2V the entire analysis). The
total ion yields from this run equate
to a hypothetical precision of <0.5
ppm. The lower panel shows the
mass fractionation throughout this
run. Scatter in the isotope ratios
are induced by step-function
changes in ion beam intensity as
well as instability in the ion

574 focusing system near the end of the analysis. This analysis shows mass fractionation that appears very
 575 similar, though of slightly greater magnitude, to double-filament analyses and contains no clear evidence
 576 for complex fractionation behavior during the majority of the analysis, though the analysis has limited
 577 isotope ratio precision for reasons laid out in the text.

578 Second, particularly during analyses using the simplified NBS lens system at high temperature, the
579 resistor chain experienced voltage disturbances that created oscillations in the lens voltages. These
580 oscillations, likely due to electron currents to the front lens plate, resulted in ion beam variability on the
581 order of several volts with a periodicity of less than a second. This instability created most of the
582 instability in isotope ratios collected near the end of analyses using the NBS source (Figure 7). This
583 problem was eliminated during analyses with the Loveless and Russell ion optics system, which was
584 powered by an independent power supply instead of a resistor-divider chain.

585 Prior to this study, published mass fractionation behavior from cavity ion sources is limited to a
586 single, short-duration (~ 7 min) analysis of U⁵ and one of Gd isotopes²⁵ though the latter may have been
587 confounded by isobaric interferences. Potential shifts in mass fractionation can substantially affect high
588 precision isotope ratio measurements^{7,14,15}. Similar to the Nd ion beam behavior, fractionation from a
589 TIC source (Figs. 7-8), at least to the precision allowed by our single-detector configuration (Figs 7-8),
590 appears to be similar to mass fractionation from a double filament ion source (Fig. 2). The first isotope
591 ratios collected during an analysis had compositions lighter than the ¹⁴⁶Nd/¹⁴⁴Nd = 0.7219 used as the
592 standard ratio for mass fractionation correction and showed ‘normal’ fractionation behavior throughout
593 the lifetime of an analysis, where the isotopic composition becomes heavier throughout the run. The
594 isotopic composition near the end of analyses reached a ¹⁴⁶Nd/¹⁴⁴Nd value that was similar to that seen
595 during flat filament analyses (0.730; ⁷), at which point the ion beam began decaying substantially.

596 Though we were not able to collect precise isotope ratios, there appeared to be no relationship between



Nd^+/NdO^+ , and $^{146}\text{Nd}^+/\text{Nd}^{144}$ and, importantly, very little ‘reverse’ fractionation .

Figure 8: The mass fractionation observed during four analyses of Nd. All isotope ratios are calculated from the metal species and the ^{146}Nd signal intensity is time-corrected for ion beam change to the ^{144}Nd integration by linear interpolation using the nearest two ^{146}Nd measurements. Symbol colors correspond to the Nd^+/NdO^+ during each integration, again time-corrected to the ^{144}Nd integration using linear interpolation. Note that the color scales are different in the four panels.

Though no ‘reverse’ fractionation is detected in our cavity ion source analyses we do not have sufficient isotope-ratio precision to completely rule this phenomenon out ($^{142}\text{Nd}/^{144}\text{Nd}$ precisions were typically >40 ppm for a given run; Table 1). If cavity ion source

620 measurements do produce periods of non-exponential mass fractionation, the higher ion beam intensities
 621 provide a path towards correcting such behavior. The secondary y-axis in Figure 9 shows the within-
 622 integration standard deviations on the $^{142}\text{Nd}/^{144}\text{Nd}$ measurement using simple ion counting statistics and
 623 uncertainty propagation (and an 8-second integration time). The typical signal sizes achievable for our
 624 modern double-filament ^{142}Nd analyses (~ 4 V) are shown by the horizontal dashed line, which
 625 corresponds to a within-integration uncertainty of ~ 32 ppm, in excellent agreement with our multi-
 626 collector instrument observations ⁸. As expected, the per-integration uncertainty of any isotope ratio
 627 dramatically decreases with signal size. If measurements of ion beam currents $\sim 5\text{e-}10$ amps (50 V on a
 628 $10^{11} \Omega$ resistor) are made, the standard deviation on any given integration would drop to ~ 9 ppm, allowing

629 non-exponential fractionation effects to be resolved much more precisely (Figure 9). This calculation
 630 shows that even if cavity ion sources are susceptible to mass dependency fractionation variations during
 631 an analysis, they provide a path towards more accurate data by allowing for more precise filtering of
 632 integrations that have affected by this phenomena.

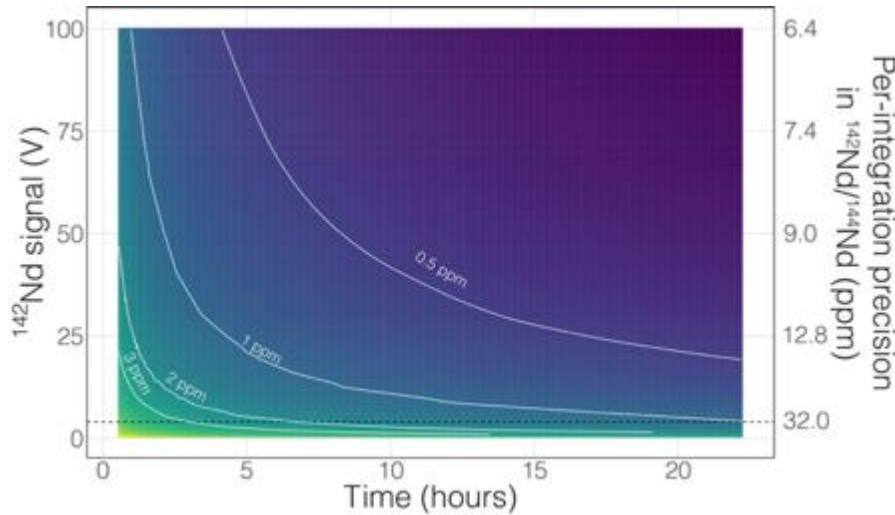


Figure 9: A simple calculation showing the total uncertainty in the $^{142}\text{Nd}/^{144}\text{Nd}$ ratio as a function of signal size and analytical times. The colors show precisions in the total $^{142}\text{Nd}/^{144}\text{Nd}$, with white curves highlighting precision contours. The secondary y-axis shows the

643
 644 within-integration (8-second integrations) $^{142}\text{Nd}/^{144}\text{Nd}$ standard deviation based on the Nd ion beam
 645 signal size. The horizontal dashed line indicates the typical 4 V $^{142}\text{Nd}^+$ signal reached in double filament
 646 ion sources, which have standard deviations ~ 32 ppm. We show that cavity ion sources are capable of
 647 generating >50 V Nd^+ ion beams for several hours, though such results are not standard in our suite of
 648 analyses and more work is required to make such analyses routine. Such large beams would allow for
 649 more precise tracking of non-exponential fractionation behavior during an analysis (with internal
 650 standard deviations <10 ppm), providing a path towards more accurate isotope ratios.

651 There are also more obvious benefits to the higher beam sizes that cavity ion sources will provide
 652 over traditional flat filament sources. First, there is the clear time-savings in that higher signal sizes
 653 achieve desired precision more quickly than small beams. This is shown in Figure 9 with a calculation
 654 that models the uncertainty of the fractionation-corrected $^{142}\text{Nd}/^{144}\text{Nd}$ as a function of analytical time and
 655 signal size. As expected, there is a decreasing precision return over time meaning that each additional
 656 hour of data collection achieves less of a relative precision increase than the last hour. The current state-
 657 of-the-art TIMS analyses for ^{142}Nd , measuring 4 V signals for 9-12 hours, are reaching a point where time
 658 quadrupling the analytical time to double the precision is becoming inviable. Even if analyzing a 4 V
 659 beam for 25 hours was possible, the precision increase would only be on the order of a few tenths of ppm
 660 in the isotope ratio precision. However, analysis of a 50 V beam for a ~ 2 hours will achieve internal
 661 precisions much lower than can be achieved currently. Thus, analyses at the same, or better, precision

662 level could be achieved in less than half the time. Analyses of 50V beams for this length of time with
663 double filament assemblies have not been shown to be possible, so cavity ion sources provide a new path
664 forward.

665 Finally, the higher ionization efficiency and signal sizes achievable with cavity ion sources will
666 provide more accurate and readily quantifiable interference corrections. This utility can, once again, be
667 illustrated with ^{142}Nd measurements. The main interfering elements of concern during ^{142}Nd
668 measurements are Ce (with an interference of ^{142}Ce on the Nd isotope of interest) and Sm (with several
669 isobaric interferences on important Nd isotopes). Accurately detecting any interfering element is a major
670 concern when dealing with isobaric interferences on isotope ratios measured at the ppm precision level.
671 Figure 10 shows the effect of signal size on detecting, and accurately correcting, potential interferences.
672 To correct the isobaric ^{142}Ce interference, ^{140}Ce is measured and a $^{142}\text{Ce}/^{140}\text{Ce}$ ratio of 0.12565 is assumed.
673 This correction is on the order of five ppm with a $^{140}\text{Ce}/^{146}\text{Nd}$ of 6.3×10^{-5} and falls with decreasing
674 Ce/Nd. Figure 10 shows two lines that calculate the ^{140}Ce signal at a given ppm correction in $^{142}\text{Nd}/^{144}\text{Nd}$
675 with varying $^{140}\text{Ce}/^{146}\text{Nd}$. When measuring Nd isotope compositions in Faraday detectors attached to
676 amplifiers equipped with $10^{11} \Omega$ resistors, a 50 μV signal is difficult to accurately quantify. If the ^{142}Nd
677 ion beam is 4 V, a ^{140}Ce signal of 50 μV would relate to a correction of -1.5 ppm, meaning that
678 interferences below \sim 1.5 ppm corrections will not be accurately quantified. With a 50 V ^{142}Nd beam,
679 however, a 50 μV ^{140}Ce signal will only represent a 0.1 ppm correction on $^{142}\text{Nd}/^{144}\text{Nd}$. Thus, higher
680 signal sizes will allow us to more accurately correct for interferences, even if such interferences are not
681 reduced by cavity measurements. Although lower noise faraday amplifiers are finding increasing use in
682 the detection of small interferences, the use of such amplifiers in combination with relatively low gain
683 amplifiers complicates multi-dynamic measurement schemes that switch ion beams between different
684 faradays in order to compensate for inefficient ion retention.

685 As well as the obvious need to accurately quantify any interfering signal, the unknown state of mass
686 fractionation of Ce and Sm leads to uncertainty in the amount of signal correction to be applied⁷. Garçon
687 et al. (2018) showed that for a ^{142}Nd analysis, the unknown fractionation state of interfering elements adds
688 excess uncertainty at the \sim 5 ppm level with $^{140}\text{Ce}/^{146}\text{Nd} > 1.6 \times 10^{-3}$ and $^{147}\text{Sm}/^{146}\text{Nd} > 1.2 \times 10^{-4}$. These
689 decrease to $^{140}\text{Ce}/^{146}\text{Nd} > 0.3 \times 10^{-3}$ and $^{147}\text{Sm}/^{146}\text{Nd} > 0.2 \times 10^{-4}$ when considering measurements with 1
690 ppm precision. More precise quantification of the interfering elements, even if their relative signals
691 compared to the analyte of interest, can lead to more accurate application of interference corrections,
692 especially if quantification of mass fractionation of the interfering elements can be achieved by, for
693 instance measurement of $^{147}\text{Sm}/^{149}\text{Sm}$ ratios during the analysis. Higher signals will clearly allow for

694 more precise and accurate interference corrections, even if for instance the Nd/Sm ratio were to stay the
695 same, leading to more accurate data.

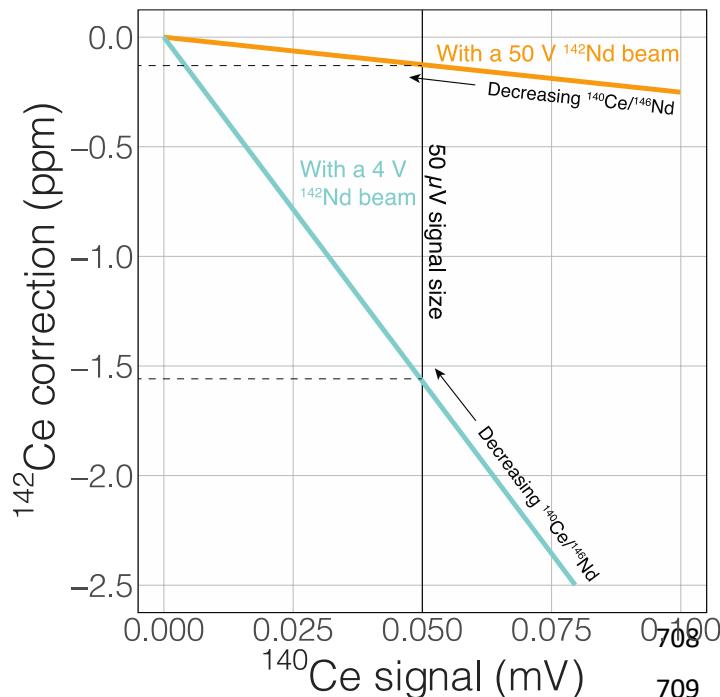


Figure 10: The magnitude of correction for the isobaric interference of ^{142}Ce on the ^{142}Nd measurement as a function of the ^{140}Ce signal and varying Ce/Nd ratios. Two lines are shown, one with a 50V ^{142}Nd beam and the other with a 4V beam. All calculations were made assuming measurement on a Faraday cup and amplifier equipped with a $10^{11} \Omega$ resistor. A larger Nd signal will allow for more precise detection and application of important interferences, even if such interferences are not reduced. The same logic and calculations can be applied to

710 many different types of analyses. Note that at the same ^{140}Ce

711 **Conclusions:**

712 We present a proof-of-concept cavity thermal ionization mass spectrometer (TIC) ion source that
713 could be used to achieve very high isotope ratio precision for large (microgram) sample sizes. Modern
714 Nd-isotope analyses are currently limited to precisions of ~4-6 ppm due to counting statistics and non-
715 exponential mass fractionation effects. We have developed a cavity ion source, heated by electron
716 bombardment, that is capable of producing $> 5\text{e}^{-10}$ amp (50 V on a $10^{11} \Omega$ resistor) Nd $^+$ ion beam sizes for
717 several hours. Though more development is required to make these highly productive analyses routine,
718 the expected precision from these cavity ion source analyses, when measured using modern multi-
719 collector instruments, based on shot-noise limitations alone can approach 0.5 ppm for the isotope ratio of
720 interest, $^{142}\text{Nd}/^{144}\text{Nd}$. We show that generation of large ion beams is possible from TIC sources and that
721 the metal to oxide ratio, Nd $^+$ /NdO $^+$, plays a major role in the total ionization of Nd $^+$ from a TIC source.
722 This ratio can likely be optimized using a combination of Re ionizing material and carbon additives, the
723 latter serving as a reductant at the ionizing surface. Although our single-detector testbed mass
724 spectrometer is not capable of making precise isotope ratio measurements, we show that mass
725 fractionation from a TIC ion source appears to be similar to double filament sources. An improvement in

726 precision to sub-ppm levels in Nd-isotope ratios would allow full utilization of the paired $^{146,147}\text{Sm}$ -
727 $^{142,143}\text{Nd}$ decay systems and produce a significant advance in the understanding of early Solar System
728 events on Earth and other rocky bodies.

729 **Acknowledgements:**

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733 assistance in various stages of mass spectrometer setup and troubleshooting.

734

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