

# Artificial Pinning Centers and The Quest of High Critical Current Densities in HTS Nanocomposites

Judy Wu, Mohan Panth, Victor Ogunjimi, Bibek Gautam, Jack Shi, Mary Ann Sebastian, Timothy Haugan, Charles Ebbing, Di Zhang, Jie Jian, Jijie Huang, Yifan Zhang, and Haiyan Wang

**Abstract**— After theoretical discovery of quantized magnetic vortices in type II superconductors by Abrikosov, which received 2003 Nobel Prize in Physics, vortex pinning has been an important topic of research for high critical current densities in applied magnetic fields desired for a variety of applications in electric and electronic devices and systems. The small vortex core size in high temperature superconductors (HTSs), of a few nanometers, has prompted an intensive research in development of nanoscale artificial pinning centers (APCs) in so-called HTS nanocomposites. Exciting results of much enhanced in-field critical current densities and pinning force densities have been achieved. This talk intends to highlight the progress made recently in HTS nanocomposites towards controllable generation of APCs with desired morphologies, dimension, concentration, and pinning efficiency for targeted applications. The future research in HTS nanocomposites to meet the need of practical applications will also be discussed.

**Index Terms**— HTS nanocomposite film, artificial pinning center, vortex pinning, pinning efficiency, interface engineering

## I. INTRODUCTION

After the discovery of the high-temperature superconductivity (HTS) in 1986 by Bednorz and Müller [1], many prototypes of electronic and electric applications based on HTS materials have been explored and demonstrated [2] ranging from lightweight electric propulsion and power generation in aircraft, to more efficient and reliable wind-

powered generators, to high efficiency power grid, high-field magnets for accelerators, fusion and medical applications, etc [3]–[9]. HTS materials have high electrical current carrying capability that is quantitatively described by critical current density ( $J_c$ ) and critical current ( $I_c$ ), which are regarded as one of most important parameters for practical applications [10], [11]. Therefore, HTS materials can assist reducing energy loss, size and weight, and environment footage of electrical systems. For example, an HTS wind turbine of increased maximum power output by 60% from 5 MW to 8 MW has shown to have reduced weight/volume by about 35% as compared to its counterpart made of copper [9]. However, significant market penetration HTS technologies performance-cost balanced HTS materials. Further enhancement of in-field  $J_c$  and  $I_c$ , especially HTS REBa<sub>2</sub>Cu<sub>3</sub>O<sub>7</sub> (REBCO, with RE regarding rare earth) coated conductors that employs a strategy of epitaxy of HTS films on flexible metal tapes of textured surface templates, has been the focus of HTS research for large  $I_c$  on the order of a few hundreds to thousands Amperes per centimeter width in long length to meet the requirement of power applications [2], [12], [13].

$J_c$  is an intrinsic property of HTS materials but often obstructed by extrinsic factors such as growth defects. Intrinsically,  $J_c$  is highly anisotropic in HTS materials due to their layered structures. Higher  $J_c$  by orders of magnitude has

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Judy Wu, Mohan Panth, Victor Ogunjimi, and Bibek Gautam are with the Department of Physics and Astronomy, the University of Kansas, Lawrence, Kansas 66045, USA (email: jwu@ku.edu; panthm@ku.edu; victorogunjimi@ku.edu; gautambik@gmail.com)  
Mary Ann Sebastian is with the University of Dayton Research Institute Dayton, OH 45469, USA and with the Air Force Research Laboratory, AFRL/RQQM, OH 45433, USA (email: maryann.sebastian@udri.udayton.edu)

Timothy Haugan is with the Air Force Research Laboratory, AFRL/RQQM, OH 45433, USA (email: timothy.haugan@us.af.mil)

Charles Ebbing is with the University of Dayton Research Institute Dayton, OH 45469, USA (email: Charles.Ebbing@udri.udayton.edu)

Di Zhang, Jijie Huang, Yifan Zhang, and Haiyan Wang are with the School of Materials Engineering, Purdue University, West Lafayette, IN 47907, USA (email: zhan2923@purdue.edu; huangjj83@mail.sysu.edu.cn; fantonyzhang@gmail.com; hwang00@purdue.edu)

been observed along the ab-planes than that along the c-axis [14]. This requires HTS films to be c-axis oriented to allow  $J_c$  in ab-plane. Furthermore, epitaxy of HTS films is required to eliminate in-plane grain boundaries (GBs) of GB angles in exceeding  $\sim 2\text{--}3^\circ$  above which an exponential decrease of  $J_c$  with GB angle has been observed due to the d-wave symmetry [15–18]. Reducing the large-angle GBs and hence its limiting effect on  $J_c$  has motivated exciting process in the research and development of the coated conductors [13], [19]. High  $J_c$ 's (77K, SF) in exceeding  $1 \text{ MA/cm}^2$  and  $I_c$ 's > hundreds to thousands Amperes per centimeter width on many kilometers of lengths of coated conductors [2], [12], [13], [19]–[21].

Since most HTS applications require high  $J_c$  and  $I_c$  in applied magnetic field of a few to tens of Tesla, generating strong pins in HTS, or so-called artificial pinning centers (APCs), becomes critically important and has prompted intensive research during almost the past two decades on APC/REBCO nanocomposites films and coated conductors. Exciting progress has been made. Overall, this research has been driven by many basic questions such as: what impurity materials may form nanoscale APCs through phase segregation in REBCO matrix? Can aligned columnar defect array form along the c-axis of REBCO to address the issue of  $J_c$  anisotropy? What controls the APC morphology, dimension, and orientation? Do all formed APCs contribute to pinning and what is the upper limit of their pinning efficiency? This paper intends to highlight the efforts and achievements in answering these questions through understanding the growth mechanism of APC/REBCO nanocomposites, using which to control the microstructures of APCs in APC/REBCO nanocomposites for desired pinning landscape, and their impact on  $J_c$ .

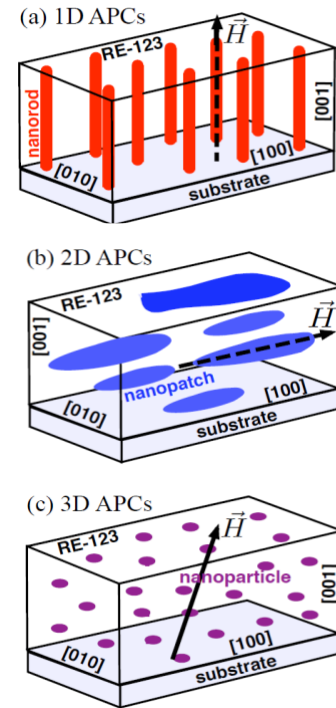
## II. RESULT and DISCUSSION

### A. Artificial Pinning Centers (APCs)

Various APCs of different morphologies, including c-axis aligned one-dimensional nanorods (1D-APCs), ab-plane aligned two-dimensional planar defects (2D-APCs), and three-dimensional nanoparticles (3D-APCs) have been reported (Fig. 1) through the addition of impurity dopants such as  $\text{BaZrO}_3$  (BZO),  $\text{BaHfO}_3$  (BHO),  $\text{BaSnO}_3$  (BSO),  $\text{YBa}_2(\text{Nb/Ta})\text{O}_6$ ,  $\text{Y}_2\text{O}_3$ , etc. in REBCO (RE=rare-earth elements: Y, Er, Gd, Nd, Sm) and enhanced pinning has been achieved in these APC/REBCO nanocomposite films [11], [13], [19]–[47]. Among others, BZO-1D APCs have been comprehensively studied after the first report by MacManus-Driscoll *et al* [48] since they can form as c-axis aligned arrays in a broad range of BZO doping concentration with areal density proportional approximately linearly to the BZO doping, which is important to obtain optimal pinning in applications targeted at specific magnetic fields.

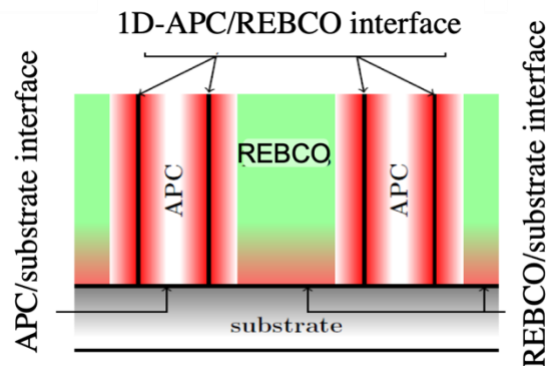
### B. Critical Role of Strain Field on APC Self-organization

In physical vapor deposition (such as magnetron sputtering and pulsed laser deposition) and chemical vapor deposition, epitaxial APC/REBCO nanocomposite films grow in the layer-by-layer mode. Since the sources of APC and REBCO are



**Fig. 1.** Schematic definition of (a) 1D, (b) 2D, and (c) 3D APCs. Reproduced with permission from Wu and Shi 2017 Supercond. Sci. Technol. 30 103002. Copyright 2017 Institute of Physics, United Kingdom

coated together, APCs form through phase segregation from the REBCO matrix at the initial stage of the growth, which is affected by the growth condition, lattice mismatch at interfaces and elastic properties of the APC and HTS materials. For APC/REBCO nanocomposite films, there are three coherent or semi-coherent (with defects) interfaces including APC/REBCO, APC/substrate and REBCO/substrate interfaces as shown schematically in Fig. 2. Strains arise because of the lattice mismatches at these interfaces serve as the driving force for the phase segregation, or so-called strain-mediated self-organization, and hence nucleation and evolution of APCs through the film thickness. The strain field is accommodated through lattice expansion and compression in the



**Fig. 2.** Strain field initiated from the strained interfaces plays a critical role in strain-mediated APC self-organization. Reproduced with permission from Wu and Shi 2017 Supercond. Sci. Technol. 30 103002. Copyright 2017 Institute of Physics, United Kingdom

nanocomposite and therefore complicated by the different elastic properties of REBCO, APC and substrate materials. The accommodation is the least in the substrate since its thickness is larger by many orders of magnitude than dimension of APC and REBCO film thickness. Therefore, the contribution of the substrate elastic property is often neglected assuming only REBCO and APCs will accommodate to the strain field generated. In both APC and REBCO, the strain may extend from the interfaces and the extension depends on their elastic properties typically in the range of a few to tens of nanometers. This leads to a highly non-uniform strain field in the APC/REBCO nanocomposite films. Interestingly, the reported APCs have different morphologies of 1D, 2D and 3D, different dimensions and orientations. While often the lattice mismatch between APC and REBCO is the first consideration in APC material selection, how it affects the APC morphology, dimension and orientation quantitatively requires a systematic study. In addition, the role of the elasticity of the two involved lattices should also be considered. To shed lights on this, an APC/REBCO nanocomposite film was investigated in an elastic strain model with consideration of the elastic constants and the lattice mismatches at three interfaces shown in Fig. 2 including the REBCO/substrate interface, the 1D APC/REBCO interface the 1D APC/substrate interface [49]. By minimizing the elastic energy, a few interesting insights have been obtained.

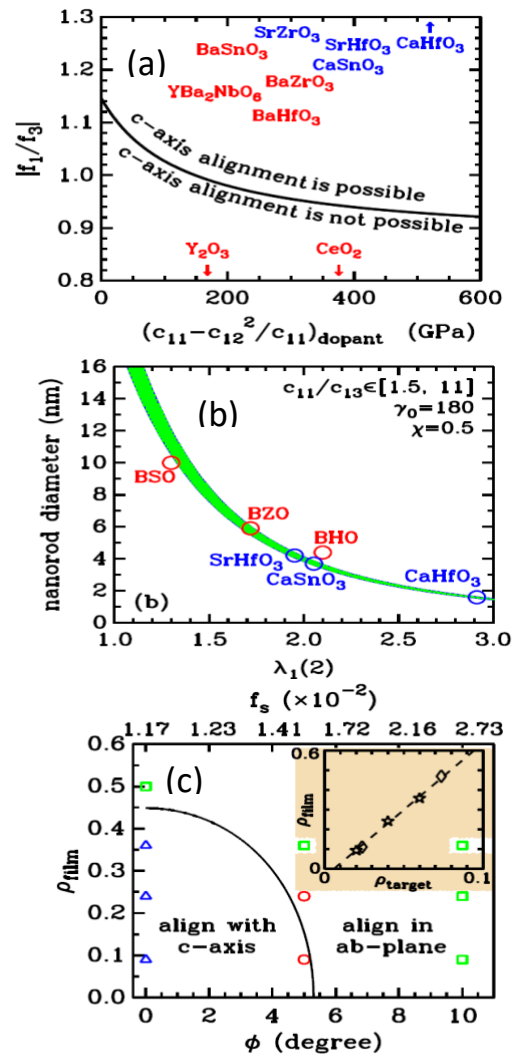
### C. Effects of strain field on APC morphology, dimension and orientation

The first question to answer in the elastic strain model simulation is why some impurity materials would form 1D APCs while others are not. Fig. 3a depicts an APC morphology phase boundary (solid line) calculated as function of the ratio absolute value of  $f_1/f_3$  of the lattice mismatches  $f_1$  and  $f_3$  between YBCO matrix and APC dopant in ab-plane and c-axis, respectively, and the elastic constants of the APC ( $C_{ij}$ ,  $i, j=1, 2, 3$ ) [49]. The simulation has revealed a phase boundary (solid line) between c-axis aligned 1D APCs preferred energetically above the line and not preferred below the line by considering both lattice mismatch and elastic properties of the APC and REBCO matrix. Also included in Fig. 3a are experimentally confirmed c-axis aligned 1D APCs (red) of BZO [33]–[35] BSO [39], BHO [31], [32], [50] and  $\text{YBa}_2\text{NbO}_6$  (YBNO) [29], [30] and  $\text{CeO}_2$  and  $\text{Y}_2\text{O}_3$  3D APCs [36], [51], [52]. It should be noted that some 3D APC impurity materials such as  $\text{Y}_2\text{O}_3$  may form nanocolumns possibly due to special growth conditions [53]. The agreement between experiment and theory confirms the critical role of the strain field initiated in nucleation, phase segregation and diffusion of the APCs in the REBCO matrix and hence the resulting APC morphology. Also included in Fig. 3a are four simulation predicted 1D APC materials of  $\text{CaHfO}_3$ ,  $\text{SrHfO}_3$ ,  $\text{CaSnO}_3$  and  $\text{SrZrO}_3$  (blue) using their reported elastic constants [54]–[56]. Confirmation of these 1D APCs experimentally would be important to further application of the simulation for APC material prediction.

Fig. 3b depicts the calculated diameter range of the 1D APCs as function of the APC strain decay constant  $\lambda_1(2)$  with the ratio of  $C_{11}/C_{13}$  of the APC material selected in the range of 1.5–1.1

for a comparison with experiment [57]. It also includes a few examples of 1D APCs demonstrated experimentally (red). Interestingly, the diameters of these 1D APCs agree well with that from the simulation. In addition, the simulation predicts the four possible 1D APC materials of  $\text{CaHfO}_3$ ,  $\text{SrHfO}_3$ ,  $\text{CaSnO}_3$  and  $\text{SrZrO}_3$  (blue) may have smaller diameters, which is desirable for enhanced pinning especially at low temperatures to be comparable to the coherence length of REBCO.

An additional question is on the correlation of the strain field and the orientation of the APC. In order to answer the question, an APC orientation phase diagram was calculated using the elastic strain energy model with consideration of the REBCO/substrate lattice mismatch and strain field overlap at variable APC concentrations [58]. The solid line in Fig. 3c is the calculated phase boundary [59], [60] of the BZO APC orientation in YBCO matrix as a function of BZO APC volume concentration in the nanocomposite film ( $\rho_{\text{film}}$ ) estimated from



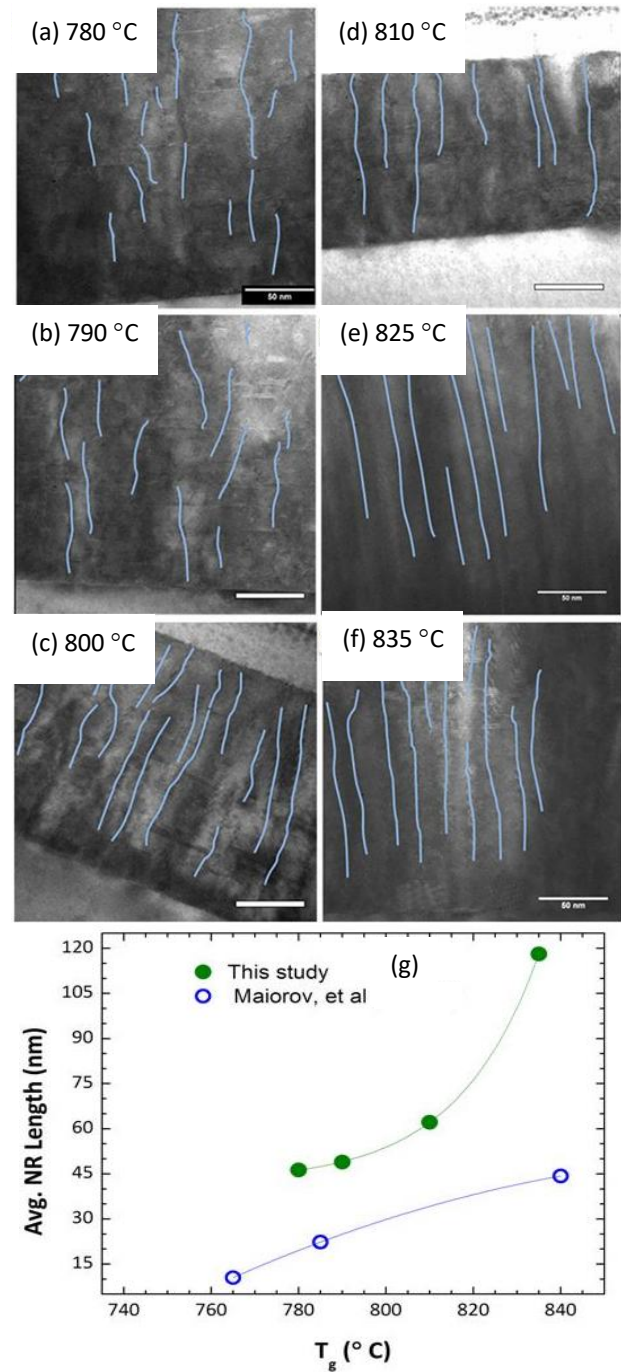
**Fig. 3.** Simulation results from the elastic strain energy model on (a) morphology of APCs, (b) diameter of 1D-APCs, and (c) orientation of APCs. Solid lines are simulation results and symbols are from experiments. Reproduced with permission from *Wu and Shi 2017 Supercond. Sci. Technol.* 30 103002. Copyright 2017 Institute of Physics, United Kingdom

the transmission electron microscopy (TEM) and the YBCO/substrate lattice mismatch  $f_s$  in the range of 1.2 to 2.7% (top scale). In this positive  $f_s$  range, the REBCO matrix is subjected to a tensile strain in the ab-plane or a compressive strain along the c-axis. The positive  $f_s$  can be obtained using SrTiO<sub>3</sub> vicinal substrates ( $\Phi$  is the vicinal angle). By increasing the vicinal angle  $\Phi$ , the ab-plane tensile strain can be quantitatively tuned from low to high. Therefore, at the lower ab-plane tensile strain and lower  $\rho_{film}$  (inside the phase boundary), the c-axis alignment remains energetically preferred for 1D APCs. Beyond this region at larger vicinal angle  $\Phi$  and higher  $\rho_{film}$ , the ab-aligned APC become energetically favorable. The symbols in Fig. 3c are experimental data [61]–[63]. The simulation result agrees well with experiment. In particular, mixed c-axis and ab-plane oriented APCs could co-exist, which has been observed experimentally (red symbols) [62].

#### D. Effects of growth condition on APC nucleation and evolution

It should be noted that the formation of APCs is critically affected by the processing conditions such as growth temperatures. Figs. 4a-f displays the cross-sectional TEM images of BZO 1D APCs grown in YBCO films at different temperatures ( $T_g$ ) in the range 780-835 °C [64]. At lower temperatures, only sparse, short segmented 1D APCs are visible. At higher temperatures, both the length (green symbols in Fig. 4g) and the concentration of the 1D APCs are significantly increased. Note the six films were made from the same PLD target at fixed BZO doping, suggesting the phase segregation of BZO in YBCO requires adequate energy. Without such an energy, BZO may remain on the YBCO lattice as chemical doping. Furthermore, the phase segregation may be hindered by the presence of other APCs such as Y<sub>2</sub>O<sub>3</sub> 3D APCs as shown in Fig. 4g (blue) [65] since the strain field is disturbed locally considerably.

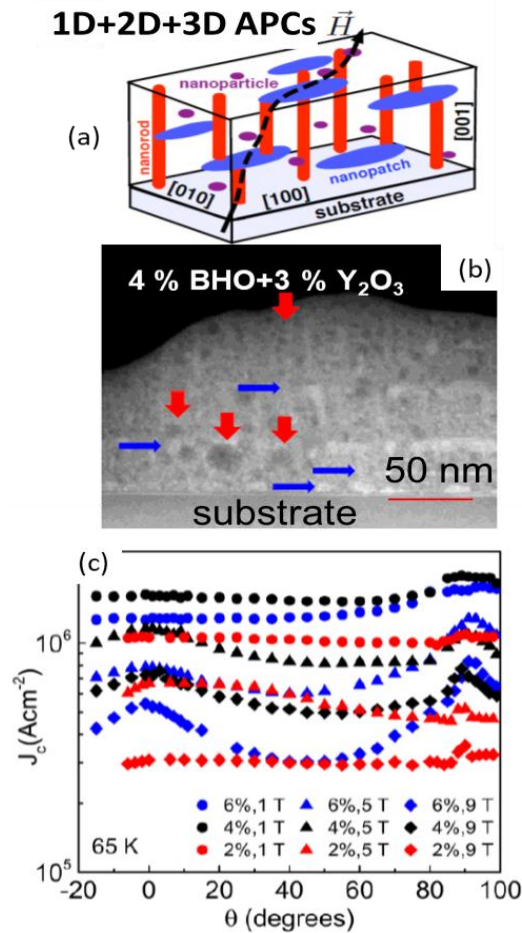
When the modulated strain field is disturbed, the strain mediated self-assembly of BZO 1D APC arrays aligned perfectly along the c-axis of REBCO may no longer be energetically favorable. This means that a mixed APC landscape could be generated through engineering the strain field by introduction of a secondary APC impurity such as Y<sub>2</sub>O<sub>3</sub>. While Y<sub>2</sub>O<sub>3</sub> may often form 3D APCs, the BZO (or other 1D APC materials) may form APCs of different morphologies. Fig. 5a shows schematically a pinning landscape that combines 1D, 2D and 3D APCs. The mixed APC morphology may provide favorable pinning landscape to reduce the anisotropy of  $J_c$  with respect to the magnetic field orientation variations. Fig. 5b exhibits a cross-sectional TEM image of a 4 vol.% BHO+3 vol.% Y<sub>2</sub>O<sub>3</sub> doped YBCO film that contains BHO 1D APC (red arrows), 2D APC (blue arrows) and 3D APCs (most probably Y<sub>2</sub>O<sub>3</sub> and possibly BHO as well) [66]. An immediate benefit of the mixed pinning landscape is in the reduced anisotropy of  $J_c$  at different orientations of magnetic field or different angle  $\theta$  that is defined as the angle between



**Fig. 4.** (a-f) Cross-sectional STEM image BZO/YBCO nanocomposite films grown at different temperatures in the range of  $T_g \sim 780$ -835 °C (g) BZO 1D APC length as a function of  $T_g$  in BZO/YBCO without (green) and with (blue) Y<sub>2</sub>O<sub>3</sub> nanoparticles

the magnetic field and the c-axis of YBCO. Fig. 5c shows the  $J_c(\theta)$  curves measured at 65 K and 1 T, 5 T, and 9 T on 2 (red), 4 (black), 6 (blue) vol. % BHO+3 vol. % Y<sub>2</sub>O<sub>3</sub>/YBCO nanocomposite films. High and less anisotropic  $J_c$  has been observed on the samples with mixed APCs. Among the three samples, the best result is observed on the 4 vol.% BHO+3 vol.% Y<sub>2</sub>O<sub>3</sub> doped YBCO, indicating the importance in balancing the APCs of difference morphologies.





**Fig. 5.** (a) schematic of a mixed pinning landscape of 1D, 2D and 3D APCs. (b) Cross-sectional view of TEM on a 4 vol. % BHO+3 vol. % Y<sub>2</sub>O<sub>3</sub>/YBCO nanocomposite film containing 1D (red), 2D (blue) and 3D APCs.  $J_c(\theta)$  measured on 2 (red), 4 (black), 6 (blue) vol. % BHO+3 vol. % Y<sub>2</sub>O<sub>3</sub>/YBCO films at 65 K.

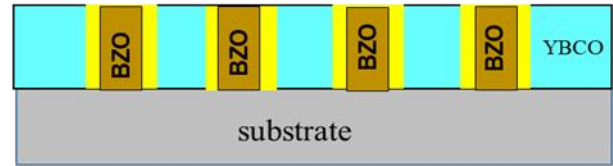
#### E. Impact of APC/REBCO strained interface on $J_c(H)$

While strain field plays a critical role in nucleation and evolution of APCs and hence provides the control on the APC morphology, dimension and orientation, the strain initiated from the large lattice mismatch at APC/REBCO interface may lead to formation of defects when the strain is too high to bear by the APC and REBCO lattices. Consequently, a defective APC/REBCO interface APC/REBCO interface forms and leads to degradation of superconducting properties of the BZO/YBCO nanocomposites especially reduced pinning efficiency of the 1D APCs [67]-[69]. In a comparative study on BZO/YBCO (with lattice mismatch of  $\sim 7.7\%$ ) and BHO/YBCO (with lattice mismatch of  $\sim 6.9\%$ ) nanocomposite films, a semi-coherent APC/YBCO interface in the former is blamed for the much lower pinning efficiency of BZO 1D APCs than that their counterpart BHO 1D APCs which form a more coherent interface with YBCO [70]. Since the specific pinning force (or pinning force per unit length) of the 1D APCs is proportional to the radial derivative of the pinning energy at the 1D APC/YBCO interface [71], a coherent interface without degradation of superconductivity is desired for optimal pinning.

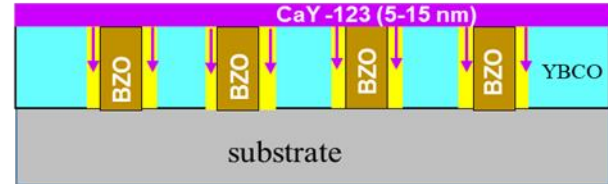
This result raises a question whether a general approach could be developed to obtain a coherent 1D APC/REBCO interface for high pinning efficiency.

In order to answer this question, we have developed a multilayer (ML) scheme to dynamically enlarge the c-lattice constant of YBCO after or during the BZO 1D-APC formation through Ca doping into the tensile strained BZO/YBCO interface [72]. As shown schematically in Fig. 6a, the bottom BZO/YBCO layer (Step 1) of thickness in the range of tens to hundreds of nm is identical to the case of single layer (SL) BZO/YBCO

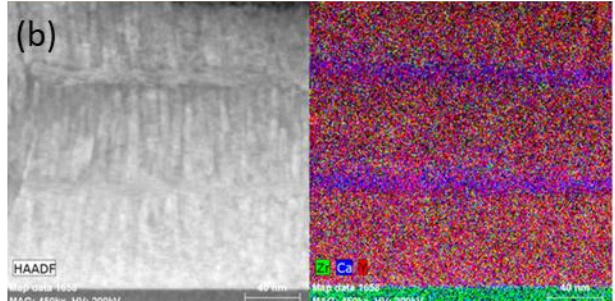
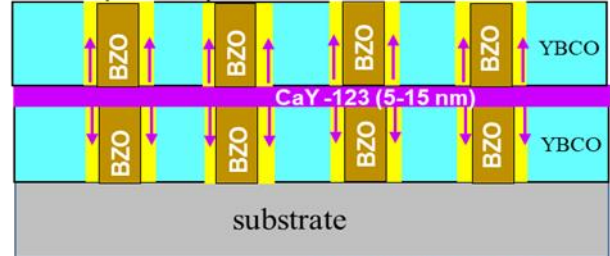
#### (a) Step 1: deposition of BZO/YBCO



#### Step 2: deposition of Ca<sub>0.3</sub>Y<sub>0.7</sub>Ba<sub>2</sub>Cu<sub>3</sub>O<sub>7</sub>



#### Step 3: deposition of BZO/YBCO



**Fig. 6.** (a) Schematic illustration of the ML approach and (b) cross-sectional TEM and EDX map on a 6 vol% BZO/YBCO ML sample.

nanocomposite films. This means the BZO 1D APCs would have the same morphology and concentration in this layer. Step 2 is for deposition of a thin (5-15 nm thick) Ca<sub>0.3</sub>Y<sub>0.7</sub>Ba<sub>2</sub>Cu<sub>3</sub>O<sub>7-x</sub> (CaY123) spacer layer on the BZO/YBCO nanocomposite film to allow Ca diffusion during the in-situ film growth. These two steps can be repeated for thicker samples. The tensile strained BZO/YBCO interface has been found to provide a diffusion channel for Ca, yielding Ca/Cu substitution on the Cu-

O planes of YBCO near the interface. Since Ca ion is 30% larger than Cu ion, this leads to enlarged c-lattice constant up to 1.24 nm and hence reduced BZO/YBCO lattice mismatch from 7.7% to 1.4% as confirmed in a TEM study [73]. This prevents formation of defects at the BZO/YBCO interface and leads to enhanced  $J_c$  in magnetic fields up to 9 T at H//c-axis and other orientations [73]–[76]. It should be noted that Ca/Y and Ca/Ba substitutions are also possible on YBCO lattice. Without any strain, Ca+2/Y+3 substitution would be the most favored energetically considering the smallest difference of ~11% in the ionic radii of Ca+2 and Y+3, which is consistent to the reported Ca/Y substitution in YBCO for the overdoping effect due to the valance difference in Ca+2 and Y+3 [77].

Fig. 7 compares the  $J_c(H)$  curves measured at different temperatures of 65 K and 77 K respectively on a pair of 6 vol.% BZO/YBCO ML (solid) and SL (open) samples. At 77 K, the former shows higher  $J_c(H)$  at higher H fields. At 65 K, the ML sample has significantly higher  $J_c(H)$  over the entire field range of 0-9.0 T. Specifically at 9 T, the  $J_c$  in the ML film is about five times of that of the SL counterpart. This result sheds light on the importance controlling the APC/REBCO interface and demonstrates the ML approach provides a promising scheme to improve the interface and the pinning efficiency of BZO 1DAPCs.

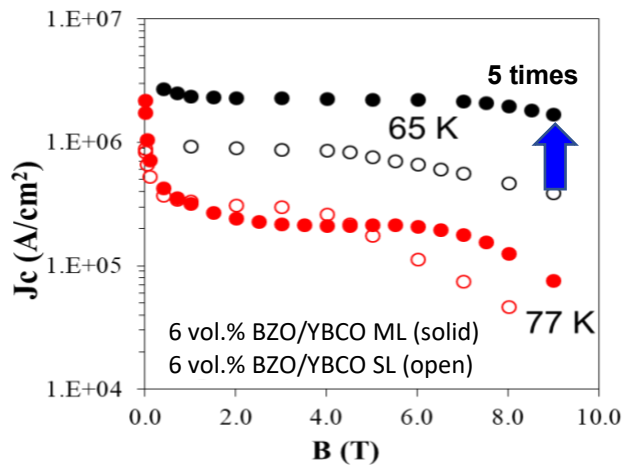


Fig. 7.  $J_c(H)$  curves measured on 6 vol.% BZO/YBCO ML (solid) and SL (open) film respectively at H//c-axis.

### III. CONCLUSIONS

In summary, significant progress has been made in the last two decades in research and development of APCs in REBCO films and coated conductors. Various APCs with different morphologies of 1D, 2D and 3D, together with pinning landscapes of APCs of mixed morphologies have been reported with improved pinning and hence enhanced  $J_c(H)$ . At a more fundamental level, a good understanding of the growth mechanism of the APCs in the APC/REBCO nanocomposites films has been achieved using the elastic-strain energy modeling and simulation. In particular, the effect of the strain field initiated from the mismatched interfaces on the APC morphology, dimension and orientation has been evaluated and

the understanding has allowed interpretation of the experimental observations as well as prediction of APC microstructures. More recently, the effect of APC/REBCO interface on the specific pinning efficiency of 1D APCs has been investigated, revealing the formed APCs may not contribute to pinning or to the full strength due to the defective interface. This has motivated new schemes to be developed for engineering the APC/REBCO interface. Among others, the ML scheme was shown effective to reduce the interface strain by dynamically enlarging the c-axis of YBCO and hence reducing the BZO/YBCO lattice mismatch from 7.7% to 1.4% near the interface. The resulted coherent BZO/YBCO interface justifies well the much enhanced  $J_c(H)$  by up to five folds at 65 K and 9 T in ML samples as compared to the SL counterparts. This result suggests further enhancement of  $J_c(H)$  and the peak field of pinning force density approaching the accommodation field defined from the APC concentration could be achieved with a thorough understanding of the interface effect and new interface engineering schemes to be developed. Besides temperatures near  $T_c$ , further extension of the benefit of enhanced pinning to lower temperatures would be important and requires a systematic investigation. Furthermore, a more interactive approach between pinning landscape simulation based on requirement of specific applications and controllable APC growth would be necessary in future research. Finally, besides consideration of pinning, other properties, such as mechanical strength and thermal conduction, may be implemented to APC/REBCO nanocomposites to address the need for high  $J_c(H)$ , high mechanical strength, thermal uniformity, etc. for practical applications.

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