

Alkali metal halide coated perovskite redox catalysts for anaerobic oxidative dehydrogenation of *n*-butane

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Abstract

Oxidative dehydrogenation (ODH) of *n*-butane has the potential to efficiently produce butadiene without equilibrium limitation or coke formation. Despite extensive research efforts, single-pass butadiene yields are limited to <23% in conventional catalytic ODH with gaseous O₂. This article reports molten LiBr as an effective promoter to modify a redox-active perovskite oxide, i.e. La_{0.8}Sr_{0.2}FeO₃ (LSF), for chemical looping–oxidative dehydrogenation of *n*-butane (CL-ODHB). Under the working state, the redox catalyst is composed of a molten LiBr layer covering the solid LSF substrate. Characterizations and *ab-initio* molecular dynamics (AIMD) simulations indicate that peroxide species formed on LSF react with molten LiBr to form active atomic Br, which act as reaction intermediates for C-H bond activation. Meanwhile, molten LiBr layer inhibits unselective CO₂ formation, leading to 42.5% butadiene yield. The redox catalyst design strategy can be extended to CL-ODH of other light alkanes such as *iso*-butane conversion to *iso*-butylene, providing a generalized approach for olefin production.

Teaser

Core-shell structured “perovskite oxide@molten LiBr” redox catalyst anaerobically converts *n*-butane into butadiene.

Introduction

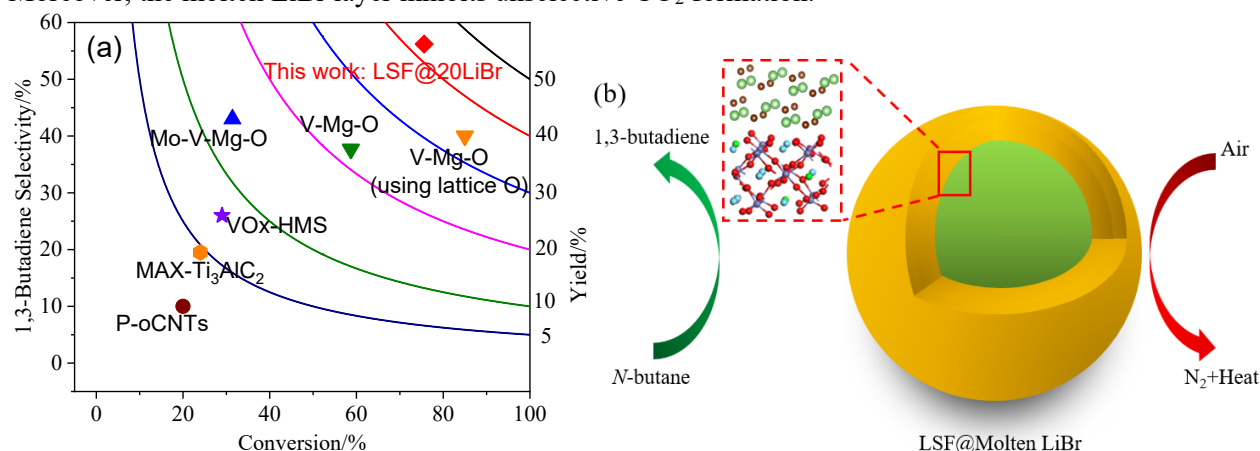
1,3-butadiene is an important chemical in the manufacturing of synthetic rubbers, specialty plastics, and various other chemical products.¹ The global 1,3-butadiene demand was 12 million metric tons in 2018 and is estimated to reach 15 million metric tons in 2023.² At present, 95% of 1,3-butadiene is produced as a byproduct from steam cracking of naphtha and purified by a butadiene recovery process.³ However, steam cracking is highly energy and emission intensive. Moreover, 1,3-butadiene only represents 4 – 5 wt.% of the product from steam cracking of naphtha, with the major products being ethylene and propylene. As an alternative route for on-purpose production, 1,3-butadiene can be obtained from direct catalytic dehydrogenation (DH) of *n*-butane. However, this process faces several challenges such as high endothermicity ($\Delta H_r=134$ kJ/mol), limited selectivity, and severe coke formation.¹

Oxidative dehydrogenation of *n*-butane (ODHB) has been proposed to address the limitations in direct DH. ODHB has the advantage of being an exothermic reaction, and requires lower reaction temperature (<500°C)¹. However, one of the most significant challenges in *n*-butane ODH is the effectiveness for *n*-butane conversion and selective formation of 1,3-butadiene. As shown in **Figure 1(a)**, conventional *n*-butane ODH catalysts include supported VO_x and/or MoO_x catalysts^{4–7}, the 1,3-butadiene yields are generally limited to ~20%. Recently, modified oxygenated carbon nanotube (oCNT)⁸, boron nitride (BN),⁹ and MAX phase materials¹⁰ have also been reported for *n*-butane ODH but the butadiene yields remain lower than 10% for these catalysts. Moreover, the use of gaseous O₂ in *n*-butane ODH leads to several other challenges: (1) gaseous O₂ is costly and energy-intensive to produce; and (2) mixing *n*-butane and O₂ requires extensive safety precautions.

To address the disadvantages of *n*-butane ODH, a chemical-looping strategy can be adopted (**Figure 1b**). In short, chemical-looping ODH of *n*-butane (CL-ODHB) is carried out in two steps. Step 1 is an ODH reaction, where *n*-butane is selectively oxidized to butadiene and H₂O with the lattice oxygen from an oxide based redox catalyst. Step 2 is air re-oxidation, where the reduced metal oxide regains its lattice oxygen by

53 reacting with gaseous oxygen in the air. This approach avoids direct contact between *n*-butane and air, and
 54 does not require pure O₂ as a feedstock. As a novel approach especially for chemical production, chemical
 55 looping strategy has been explored for fossil fuel combustion^{11,12}, methane selective oxidation^{13–18},
 56 thermochemical water/CO₂ splitting^{19–26}, air separation^{27–29}, and selective oxidative dehydrogenation of
 57 ethane, propane and ethylbenzene^{30–36}. However, effective redox catalysts for *n*-butane ODH have yet to be
 58 reported, largely due to the high operating temperatures required, and hence low product selectivity, for
 59 typical chemical looping materials.

60 Molten salt has been used as an effective promoter for catalytic light alkanes conversion. For example,
 61 Lercher et al. reported Dy₂O₃/MgO supported molten alkali metal chloride for ethane and propane ODH in
 62 the presence of gaseous O₂, and the active species were assigned to OCl[−] ion.^{37,38} McFarland and Metiu et
 63 al. reported the use of molten halide salts for methane conversion and propane ODH.^{39–42} In this work, we
 64 report a molten LiBr covered La_{0.8}Sr_{0.2}FeO₃ (LSF@LiBr) redox catalyst for effective chemical looping ODH
 65 of *n*-butane. 1,3-butadiene yields up to 42.5% were achieved at 500°C, far exceeding the previously reported
 66 values for O₂-cofeed butane ODH and butane ODH using lattice oxygen in terms of single-pass yield (**Figure**
 67 **1a**) at comparable or higher space-time yields (**Table S1**). Detailed characterizations and computational
 68 studies indicated that the active lattice oxygen species within LSF oxidize the molten LiBr shell into atomic
 69 Br, as a reaction intermediate, for C-H bond activation of *n*-butane and 1-butene into butadiene product.
 70 Moreover, the molten LiBr layer inhibits unselective CO₂ formation.



71
 72 **Figure 1. Comparison of catalyst performance and schematic of the redox catalyst.** (a) A comparison
 73 of reported *n*-butane ODH catalyst performance^{4–8,10} and the CL-ODHB catalyst reported in this work; (b)
 74 A schematic of the CL-ODHB redox catalyst.

75 Results

76 Structural characterization of the redox catalyst

77 LSF@LiBr has a core-shell structure, where the core material is LSF and shell material is LiBr. The
 78 surface enrichment of LiBr was first confirmed using XPS. As shown in **Figure 2(a)**, LSF@LiBr samples
 79 are surface-enriched with Br, and all the LSF related cations, i.e. Fe, Sr and La, are suppressed. The atomic
 80 concentration of Li is not shown here because the XPS signal sensitivity to Li is poor. The surface enrichment
 81 of Br is further confirmed with energy dispersive spectroscopy (EDS) in scanning transmission electron
 82 microscope (STEM). As shown in **Figure 2(b)**, the surface of the redox catalyst is enriched with Br while
 83 the bulk is enriched with La, Sr and Fe, consistent with the XPS results. The structure of LSF@LiBr under
 84 the working temperature (500°C) is further confirmed with *in-situ* XRD (**Figure 2(c)**), with temperature
 85 ramping from room temperature to 500°C under air. At room temperature, only LSF phase was observed.
 86 At 100°C, there appeared another phase which can be assigned to lithium oxide bromide (Li₃OBr). Above
 87 100°C, Li₃OBr phase disappeared and LiBr phase appeared. LSF phase was present throughout the
 88 temperature ramping program. The absence of crystallite LiBr phase at room temperature is likely to be due
 89 to the fact the LiBr tends to absorb moisture under air, forming amorphous lithium oxide hydrate. Above
 90 460°C, LiBr phase disappeared due to the melting of surface LiBr. This was further confirmed with
 91 thermogravimetric analysis-differential scanning calorimetry (TGA-DSC) results in **Figure 2(d)**. As shown
 92 in **Figure 2(d)**, LSF@20LiBr has a heat absorption peak ranging from ~460 to 550°C, with a peak
 93 temperature at 513°C. This shows that surface LiBr is in a molten state at 500°C. It is noted that the melting
 94 point of surface LiBr is much lower than that of bulk LiBr (m.p. = 552°C). As will be discussed in the

following sections, the optimal working temperature of LSF@20LiBr is at 500°C. Thus, under the working temperature, the LSF core is covered with a layer of molten LiBr. A similar core-shell arrangement has been confirmed for LSF@10LiCl and LSF@10NaBr (Figure S1), and can also be inferred for other halide modified LSF investigated in the current study.

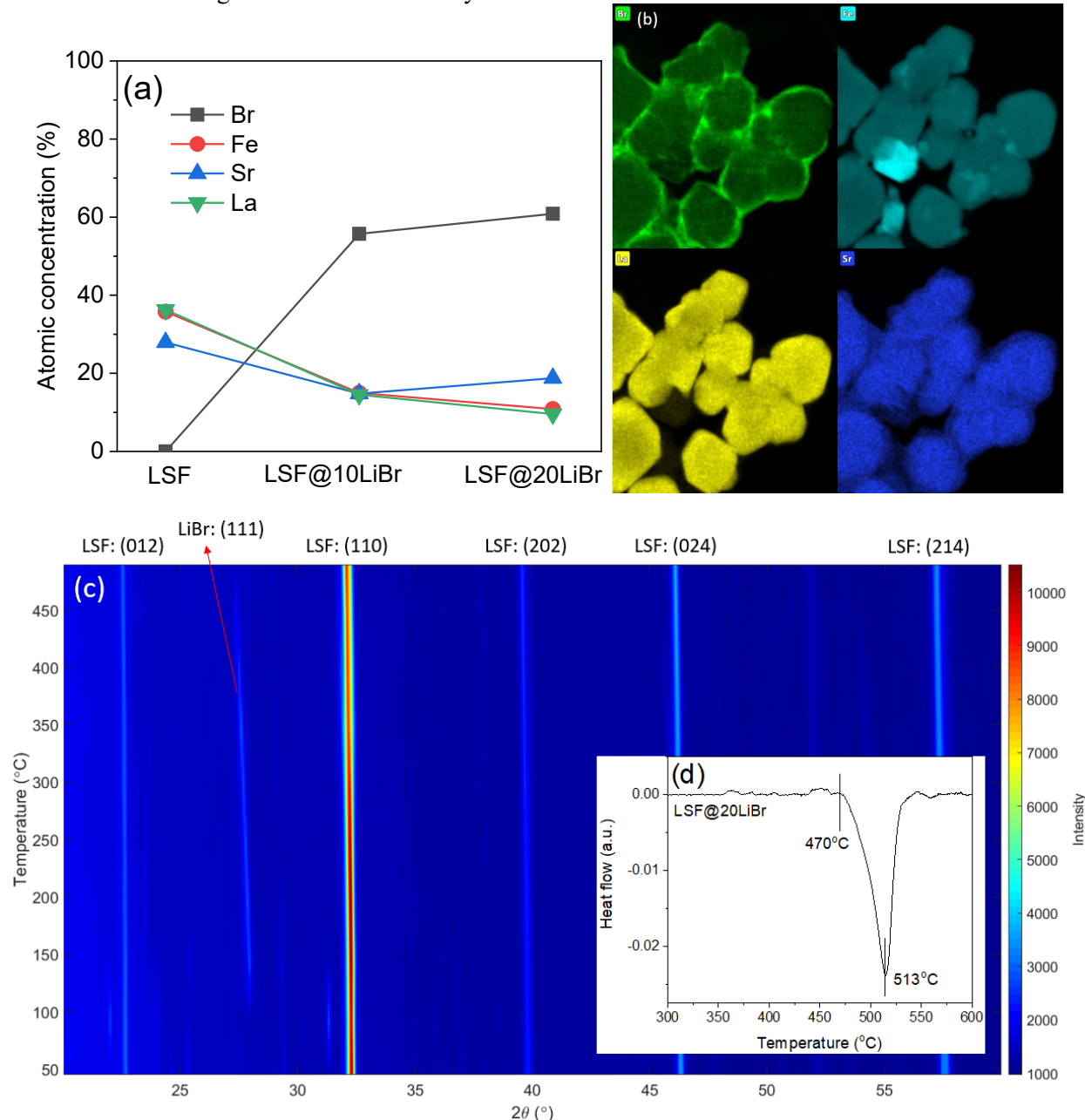


Figure 2. Redox catalyst characterizations. (a) Surface atomic concentration obtain from XPS on LSF, LSF@10LiBr and LSF@20LiBr; (b) STEM-EDS on LSF@20LiBr; (c) *In-situ* XRD pattern on LSF@20LiBr with temperature ramping from room temperature to 500°C under air, the color intensity corresponds to the XRD peak intensity; (d) TGA-DSC on LSF@20LiBr to measure surface LiBr melting point on LSF.

Isothermal CL-BODH on modified LSF

Modifying LSF with a molten halide salt layer increases both *n*-butane conversion and 1,3-butadiene selectivity. As shown in Figure 3(a), unmodified LSF exhibited 71% butane conversion but only 2% 1,3-butadiene selectivity at 500°C. In fact, 93% of the *n*-butane was converted into CO_x unselectively. In the meantime, it is noted that blank thermal conversion of *n*-butane at 500°C was minimal (~0.2%), and the thermally cracked products are mostly C₂ and C₃ products rather than 1,3-butadiene. Different promoters were applied to modify the LSF substrate for improved ODH performance. These promoters include LiBr, LiCl, KBr, NaBr, mixture of LiBr and LiCl, mixture of LiBr and KBr, and Li₂CO₃. It was determined that

LiBr with 20% weight loading was the most effective. Up to 75.6% *n*-butane conversion and 56.2% 1,3-butadiene selectivity were obtained on LSF@20LiBr, corresponding to 42.5% 1,3-butadiene yield. Meanwhile, LiCl promoter, NaBr, and KBr promoters all exhibited lower conversions and selectivities. We also compared the commercial LSF substrate with LSF synthesized in-house, and they exhibited very similar performances (**Figure S2**). Other halogenated species such as C₄H₉Br was determined to be minimal at the product stream by measuring the M/Z=137 signal with a downstream quadrupole mass spectrometry (QMS, MKS Cirrus II) in **Figure S3**. The mass spectrometry data also confirmed minimal coke formation based on the negligible CO and CO₂ signals in the air reoxidation step. **Figure 3(b)** provided detailed product distributions and showed the cyclic stability of LSF@20LiBr with 20 CL-ODHB cycles. To determine whether loss of LiBr by vaporization would be of a potential concern, LSF@20LiBr was treated at 500°C with argon gas for 15 hours in TGA. **Figure S4** shows that rate of LiBr loss is very slow (0.019 wt.%/hr). This is consistent with the minimal deactivation observed within the 20 CL-ODHB cycles tested. The loss of LiBr during long-term operations can potentially be solved by bleeding in LiBr for replenishment from an engineering standpoint, similar to an industrial approach which replenishes HCl intermittently.⁴³

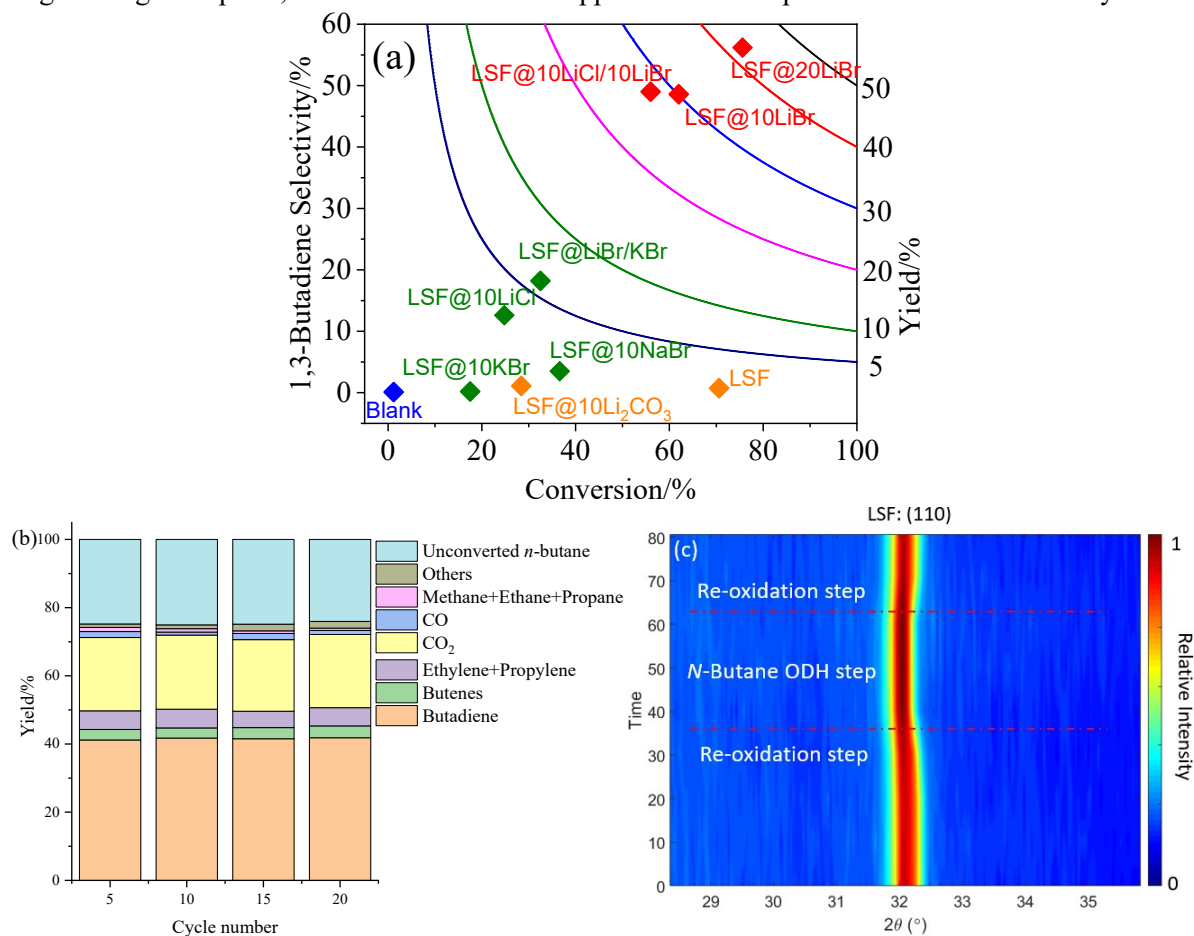


Figure 3. Effect of redox catalyst compositions, product distributions, and *in-situ* XRD. (a) CL-ODHB performance comparison of LSF, blank and LSF with different promoters: Temperature = 500°C; Space velocity = 450 h⁻¹. (b) Detailed product distributions showing carbon-based yields and 20 CL-ODHB cycles on LSF@20LiBr: Temperature = 500°C; Space velocity = 450 h⁻¹; Butenes include 1-butene, trans-2-butene and cis-2-butene; Others include propadiene, acetylene, *i*-butane and C₅₊. (c) *In-situ* XRD on LSF@20LiBr under 500°C with *n*-butane ODH step and air re-oxidation step.

Active species and reaction pathway for CL-ODHB

The mechanism for the *n*-butane redox ODH and the effectiveness of molten LiBr layer was determined via both experimental and simulation studies. As shown in **Figure 3(c)** above, *in-situ* XRD was conducted with *n*-butane redox ODH cycles at 500°C to determine the dynamic phase change of LSF@20LiBr. Although only the LSF phase can be observed at 500°C throughout the redox reactions, its lattice parameters were enlarged during the ODH (reduction) step as illustrated in **Figure 3(c)** by the diffraction peak of the

(110) plane. As can be seen, *n*-butane ODH on LSF caused the peak to slightly shift from 32.1° to 32.0°, and no other phase changes were observed. Re-oxidation with air shifted the peak back to its original position. The cycle stability of phase structure was verified by running 5 redox cycles in the *in-situ* XRD (Figure S5). Based on a previous study on a LSF@Li₂CO₃ redox catalyst in the context of ethane ODH, such a peak position transition corresponds to the transition between Fe⁴⁺ and Fe³⁺ oxidation state in LSF and this would lead to evolution of active lattice oxygen into peroxide species in the form of Li₂O₂.³⁰ The presence of peroxide as active species also agrees with early studies of Lunsford and more recent work using *in-situ* characterizations for oxidative coupling of methane.^{44,45}

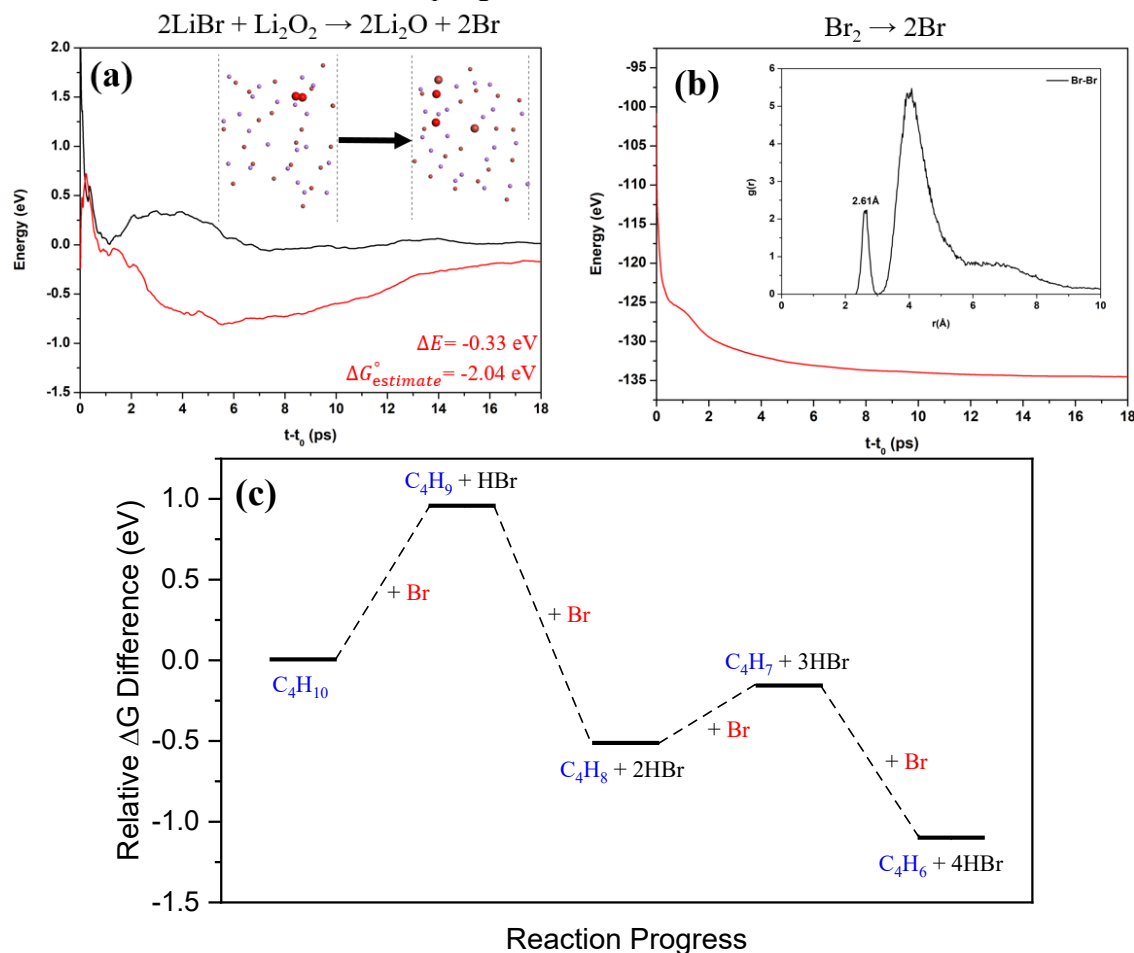


Figure 4. ODH reaction pathway. AIMD calculation of (a) $2\text{LiBr} + \text{Li}_2\text{O}_2 \rightarrow 2\text{Li}_2\text{O} + 2\text{Br}$ and (b) $\text{Br}_2 \rightarrow 2\text{Br}$ within LiBr molten salt, and (c) *n*-C₄H₁₀ reacting with Br-containing molten LiBr

The interaction of Li₂O₂ and LiBr was further studied with AIMD. It was determined that it is energetically favorable for Li₂O₂ to oxidize LiBr into atomic Br, as shown in Figure 4(a). Furthermore, as shown by the AIMD results of the evolution of Br₂ inside molten LiBr (Figure 4b), the Br-Br bond cleaves to form two atomic Br after 1 ps and the equilibrated state at 18 ps showed an average Br-Br distance of 2.61 Å, larger than the bond length of Br₂(g) (2.28 Å). This showed that molecular Br₂ is unstable in molten LiBr and tends to decompose into two atomic Br. The atomic Br subsequently diffuses to the molten LiBr salt and gas interface to react with C₄H₁₀, producing butadiene in a stepwise fashion and forming HBr as a byproduct (Figure 4c). The as-formed HBr then reacts spontaneously with Li₂O and forms LiBr and H₂O, with $\Delta G = -202.2$ kJ/mol at 500°C (equivalent to 2.10 eV) calculated from HSC Chemistry 9. The reactions for the two half-cycles of CL-ODHB are summarized in Table 1. It is noted that these reactions are reversible, meaning that species such as Br and peroxide will be under a dynamic equilibrium. The re-oxidation half-cycle can proceed via Reaction 1' to 4' as shown in Table 1. R1' ($\text{O}_2 + 2\text{Li}_2\text{O} \rightleftharpoons 2\text{Li}_2\text{O}_2$) has a ΔG of 58.5 kJ/mol at 500°C (equivalent to 0.60 eV) based on HSC, indicating that an appreciable O₂²⁻ concentration can present. Previous studies using DFT-based thermodynamic calculations also suggested that Li₂O₂ is stable under high O₂ partial pressures.⁴⁶ R2' ($\text{O}_2 + 2\text{LiBr} \rightleftharpoons \text{Li}_2\text{O}_2 + 2\text{Br}$) has a ΔG of 176.6 kJ/mol at 500°C (equivalent to 1.83 eV) based on HSC, showing that this reaction can also take place, albeit to a lesser extent. Metiu et al.

also suggested that alkali halide can be oxidized to peroxide based on AIMD calculations, although this study focused on the oxidation of LiI rather than LiBr.⁴² R3' ($2\text{Br} + 2\text{Li}_2\text{O} \rightleftharpoons \text{Li}_2\text{O}_2 + 2\text{LiBr}$) is the reverse reaction of R2 in the ODHB half-cycle. The evolved Li_2O_2 species in these reactions then react with LSF to re-oxidize the Fe cation to a higher oxidation state, as has been reported previously.³⁰ We also note that other supported catalysts besides $\text{LSF}@20\text{LiBr}$, such as $\text{La}_{0.8}\text{Sr}_{0.2}\text{Fe}_{0.8}\text{Co}_{0.2}\text{O}_3@20\text{LiBr}$ ($\text{LSFC}@20\text{LiBr}$) and $\text{La}_{0.8}\text{Sr}_{0.2}\text{MnO}_3@20\text{LiBr}$ ($\text{LSM}@20\text{LiBr}$), can also catalyze CL-ODHB of butadiene. $\text{LSFC}@20\text{LiBr}$ and $\text{LSM}@20\text{LiBr}$ exhibited lower *n*-butane conversions, higher butenes selectivities and lower butadiene selectivities than $\text{LSF}@20\text{LiBr}$, indicating that the subsequent dehydrogenation of butenes to butadiene is less pronounced in these redox catalysts (**Table S1**).

Table 1. Summary of the key reactions in the ODH and re-oxidation half-cycles (the complete CL-ODHB cycle has an overall reaction: $\text{C}_4\text{H}_{10} + \text{O}_2 = \text{C}_4\text{H}_6 + 2\text{H}_2\text{O}$).

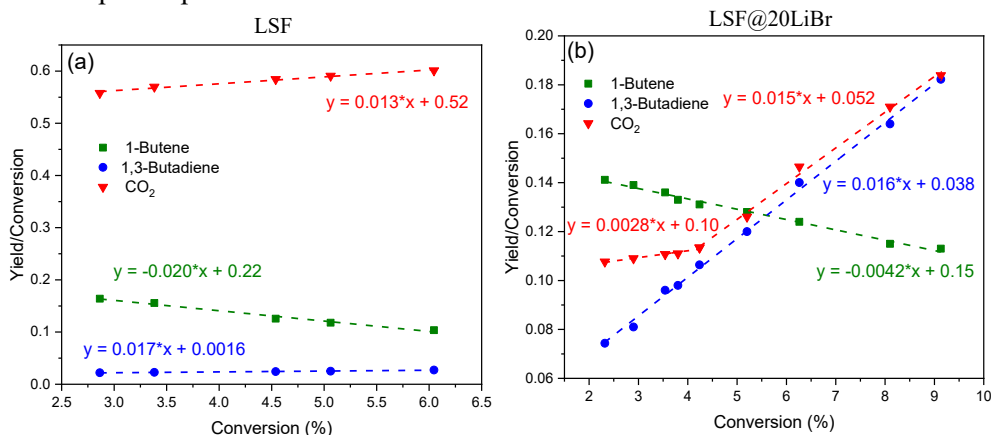
ODHB half-cycle
(1) $\text{Li}_2\text{O} + \text{O}_2^{2-} \text{ (of LSF)} \rightleftharpoons \text{Li}_2\text{O}_2 + \text{O}^{2-} \text{ (of LSF)}$
(2) $\text{Li}_2\text{O}_2 + 2\text{LiBr} \rightleftharpoons 2\text{Li}_2\text{O} + 2\text{Br}$
(3) $\text{C}_4\text{H}_{10} + 2\text{Br} \rightleftharpoons \text{C}_4\text{H}_8 + 2\text{HBr}$
(4) $\text{C}_4\text{H}_8 + 2\text{Br} \rightleftharpoons \text{C}_4\text{H}_6 + 2\text{HBr}$ (Note, Reactions 3 and 4 are lumped reactions)
(5) $\text{Li}_2\text{O} + 2\text{HBr} \rightleftharpoons 2\text{LiBr} + \text{H}_2\text{O}$
<i>Overall reaction in the ODHB half-cycle:</i> $\text{C}_4\text{H}_{10} + 2\text{O}_2^{2-} \text{ (of LSF)} = \text{C}_4\text{H}_6 + 2\text{O}^{2-} \text{ (of LSF)} + 2\text{H}_2\text{O}$
Re-oxidation half cycle
(1)' $\text{O}_2 + 2\text{Li}_2\text{O} \rightleftharpoons 2\text{Li}_2\text{O}_2$
(2)' $\text{O}_2 + 2\text{LiBr} \rightleftharpoons \text{Li}_2\text{O}_2 + 2\text{Br}$
(3)' $2\text{Br} + 2\text{Li}_2\text{O} \rightleftharpoons \text{Li}_2\text{O}_2 + 2\text{LiBr}$ (reverse reaction of Reaction 2)
(4)' $\text{Li}_2\text{O}_2 + \text{O}^{2-} \text{ (of LSF)} \rightleftharpoons \text{Li}_2\text{O} + \text{O}_2^{2-} \text{ (of LSF)}$ (reverse reaction of Reaction 1)
<i>Overall reaction in the re-oxidation half-cycle:</i> $\text{O}_2 + 2\text{O}^{2-} \text{ (of LSF)} = 2\text{O}_2^{2-} \text{ (of LSF)}$

Figure 4(c) shows that *n*-butane activation to butyl radical has a Gibbs free energy difference of 0.95 eV, while subsequent dehydrogenation to 1-butene is much more energetically favorable (-1.47 eV). Similarly, 1-butene activation to butenyl radical has a free energy difference of 0.36 eV whereas the subsequent butenyl radical dehydrogenation to 1,3-butadiene is more favorable (-0.95 eV). It is noted that the first C-H bond dissociation energy for *n*-butane is around 400 kJ/mol or 4.15 eV⁴⁷, much higher than the Gibbs free energy difference with atomic Br. It has also been reported that halogens can be used as a “soft-oxidant” for oxidative methane coupling⁴⁸ and propane ODH.^{41,42} AIMD calculations also indicate that the desorption energies for C_4H_9 and C_4H_7 are 0.30 and 0.34 eV, respectively. Therefore, the as-formed radicals are more likely to be further dehydrogenated on the outer LiBr surface than being desorbed for gas phase radical reactions (**Figure S6**). However, the as formed 1-butene can be desorbed from the molten salt surface and re-adsorbed for further dehydrogenation by Br, as will be discussed in the following section. The AIMD findings are also substantiated by gas phase kinetics simulations via Reaction Mechanism Generator (RMG) and Chemkin-Pro: given either gaseous butyl radical or butenyl radical as the feedstock, 2-butene as opposed to butadiene is determined to be the primary product when the reaction proceeds exclusively through the gas phase radical reaction pathway (**Figure S7**). In contrast, butadiene was the primary product observed experimentally (**Figure 3b**). This confirms that *n*-butane and its dehydrogenated products, e.g., 1-butene, mainly reacted with atomic Br on the catalyst surface. A simple thermodynamic comparison was also conducted to determine the reason for lower activities of LiCl, NaBr and KBr coatings. As summarized in **Table S3**, from a thermodynamic standpoint, LiCl, NaBr and KBr are all less favorable than LiBr to be oxidized into Cl or Br. The lack of halogen species in the molten shell would lead to low activity for *n*-butane activation.

To map out the reaction network, a “delplot” technique was further conducted to confirm the sequential C-H bond breakage of C_4H_{10} as predicted by AIMD.⁴⁹ **Figure 5(a)** shows the delplot for unmodified LSF. As anticipated, the formation of CO_2 on unmodified LSF is more substantial than the formation of 1,3-butadiene and 1-butene. Nevertheless, it can be seen that the delplot for 1-butene has a negative slope and with a finite Y-axis intercept, indicating that the formation of 1-butene is a primary reaction. Meanwhile,

the delplot for 1,3-butadiene has a positive slope and with a Y-axis intercept close to zero, indicating that the formation of 1,3-butadiene is a secondary reaction resulting from further ODH of 1-butene, consistent with the AIMD results. It is noted that the delplot of CO₂ has a positive slope, but also with a very large finite Y-axis intercept. This indicates that CO₂ formation is both a primary reaction resulting from non-selective oxidation of *n*-butane, and a secondary reaction resulting from secondary non-selective oxidation of 1-butene and 1,3-butadiene. This is more clearly demonstrated with the delplot of LSF@20LiBr. As can be seen in **Figure 5(b)**, while similar trends hold true for the delplots of 1-butene and 1,3-butadiene, the delplot for CO₂ shows a larger positive slope at higher conversions but flats out at lower conversions into a finite Y-axis intercept. This confirms that the formation of CO₂ is both a primary and secondary reaction. The fact that the CO₂ delplot Y-axis intercept of LSF@20LiBr (Y-axis intercept = 0.10) is much smaller than that of LSF (Y-axis intercept = 0.52) but the slopes are similar at higher conversions could indicate that the primary CO₂ formation reaction was largely eliminated the LiBr modification, and CO_x formation on LSF@20LiBr is mainly resulted from the oxidation of butane and butadiene products. A schematic drawing for the reaction pathway based on the delplot and the aforementioned characterization is shown in **Figure 5(c)**. The delplot experiments are consistent with the space velocity effect tests on LSF@20LiBr, where higher space velocity leads to larger 1-butene selectivities and smaller 1,3-butadiene and CO₂ selectivities (**Table S4**). The secondary conversion of butenes to butadiene is also verified with a 1-butene ODH experiment on LSF@20LiBr. Up to 98% 1-butene conversion can be achieved at 475°C with 65% 1,3-butadiene selectivity, leading to 63.6% 1,3-butadiene yield. More temperature effect tests on 1-butene ODH are shown in supplemental in **Table S5**.

Besides the delplot and activation energy experiments, the reaction order for CL-ODHB with LSF@20LiBr is studied by varying the feed partial pressure of *n*-butane. As shown in **Figure 5(d)**, the formation rate of CO₂ and olefins are both linear with respect to *n*-butane partial pressure, indicating that they are both first order reactions. As investigated by several studies, chemical looping oxidation can be considered as a modified Mars-van Krevelen reaction. For a Mars-van Krevelen reaction, the overall reaction rate is only approximated to first order to the gaseous hydrocarbon reactant when the partial pressure of gaseous oxygen (P_{O₂}) is much larger than that for gaseous hydrocarbon reactant (P_R).^{50,51} As chemical looping processes with lattice oxygen involvement are usually treated to exhibit a modified Mars-van Krevelen reaction mechanism⁵², this shows that the participation of lattice oxygen is sufficiently fast and a high *n*-butane feed partial pressure is more beneficial for butadiene formation.



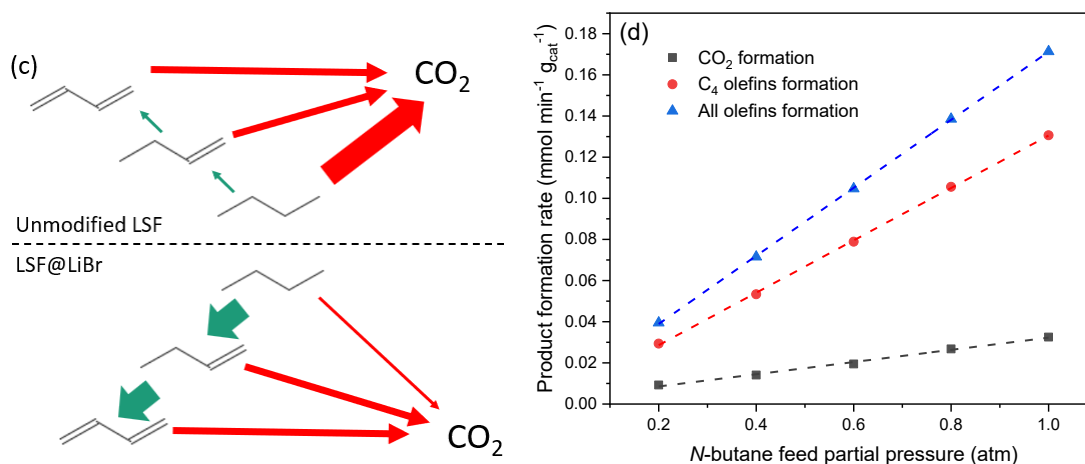


Figure 5. ODH reaction network and reaction orders. Delplots for (a) unmodified LSF and (b) LSF@20LiBr; (c) A schematic drawing for reaction pathway network, the thickness of the lines qualitatively describes the extent of reaction; and (d) Product formation rate versus *n*-butane feed partial pressure at 500°C with space velocity = 450 h⁻¹

Inhibition of CO₂ formation by the molten LiBr layer

Molten LiBr layer not only induces atomic Br for butadiene formation, but also inhibits CO₂ formation. This was examined with activation energy and pre-exponential factor measurements for CO₂ formation of LSF and LSF@LiBr in the kinetic regime (<20% conversion) with a higher space velocity (3600 h⁻¹). As shown in **Figure 6(a)**, unmodified LSF has an activation energy of 52.3 kJ/mol and pre-exponential factor of 12.1 s⁻¹ for CO₂ formation. Meanwhile, LSF@20LiBr has an activation energy of 48.3 kJ/mol and a pre-exponential factor of 9.3 s⁻¹ below the melting point temperature (~465°C). The lower pre-exponential factor of LSF@20LiBr than LSF below the melting point indicate unmelted LiBr partly covers the unselective sites for CO₂ formation. And the similar activation energy between LSF and LSF@LiBr below the melting point indicates that unmelted LiBr does not change the mechanism for CO₂ formation. The activation energy (86.6 kJ/mol) and pre-exponential factor (13.4 s⁻¹) of LSF@20LiBr is much higher above the melting point temperature. The high activation energy indicates that molten LiBr better covers the unselective sites and substantially inhibits CO₂ formation. And the high pre-exponential factor for CO₂ formation above the melting point temperature could be explained by higher active oxygen concentration in the LiBr melt, leading to higher collision frequency between hydrocarbons and active oxygen species.

The inhibition of CO₂ formation with LiBr layer was further studied with ¹⁸O₂ exchange experiments and H₂-TPR. As shown in **Figure 6(b)** in ¹⁸O₂ exchange experiments on LSF and LSF@20LiBr, LSF exhibited significantly larger surface oxygen exchange rate than LSF@20LiBr in the temperature range investigated (450 to 600°C). The suppression of the surface oxygen exchange further leads to the suppressed lattice oxygen evolution as indicated by H₂-TPR in **Figure 6(c)**. As can be seen, blank LSF exhibited lower temperature reduction peaks at 330°C and 440°C, whereas LiBr promoted LSF exhibited higher reduction peaks at 470°C and 560°C. For LSF, the first reduction peak can be ascribed to the reduction of Fe⁴⁺ to Fe³⁺ and Fe⁰, while the second reduction peak can be ascribed to the further reduction of Fe³⁺ to Fe²⁺ and Fe⁰. For LSF@20LiBr, the first reduction peak can be ascribed to the reduction of Fe⁴⁺ and Fe³⁺, based on *in-situ* XRD and prior reports.³⁰ The prolonged mass decrease at higher temperatures is largely due to the inhibited reducibility of LSF by the molten salt. The slow vaporization of LiBr may also contribute to the weight loss, albeit to a minor extent. It is noted that the overall weight loss in H₂-TPR was nearly the same for blank LSF and LiBr coated LSF, indicating that LiBr coating does not affect the overall lattice oxygen capacity of the LSF substrate.

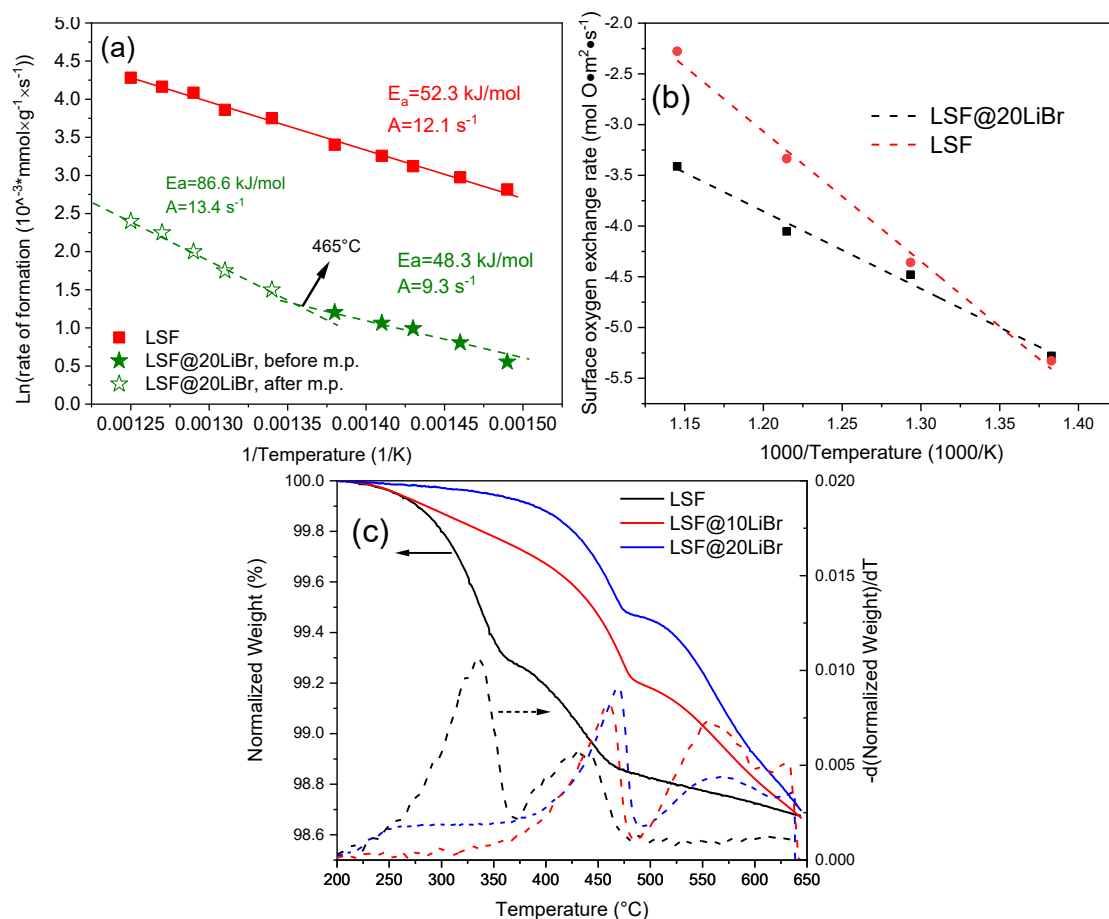


Figure 6. Kinetic parameters and reducibility of the redox catalysts. (a) Activation energy and pre-exponential factor for CO₂ formation of LSF and LSF@20LiBr; (b) Surface oxygen exchange rate of LSF and LSF@20LiBr quantified with ¹⁸O₂-exchange experiment; (c) H₂-TPR of LSF and LSF@20LiBr.

Extension to chemical looping ODH of *iso*-butane

The LSF@LiBr redox catalyst can be extended for chemical looping *iso*-butane ODH to isobutylene, and isobutylene is a useful starting material for the synthesis of methyl tertiary butyl ether, methacrylates and many other important chemical products.⁹ At 475°C, 51.0% *iso*-butane conversion and 43.3% *iso*-butylene selectivity was achieved, accounting for 22.2% *iso*-butylene yield. This exceeds most literature values for O₂-cofeed *iso*-butane ODH (Figure 7).^{53–57} The lower conversion and selectivity in *iso*-butane CL-ODHB than those in *n*-butane CL-ODHB is probably due to the lack of secondary conversion of 1-butene to 1,3-butadiene in *n*-butane CL-ODHB. More detailed product distributions with respect to temperature is shown in Table S6. The promising *iso*-butylene yields indicates that the types of alkane feedstocks could be extended and LSF@LiBr is a general redox catalyst for chemical looping oxidative dehydrogenation of light alkanes.

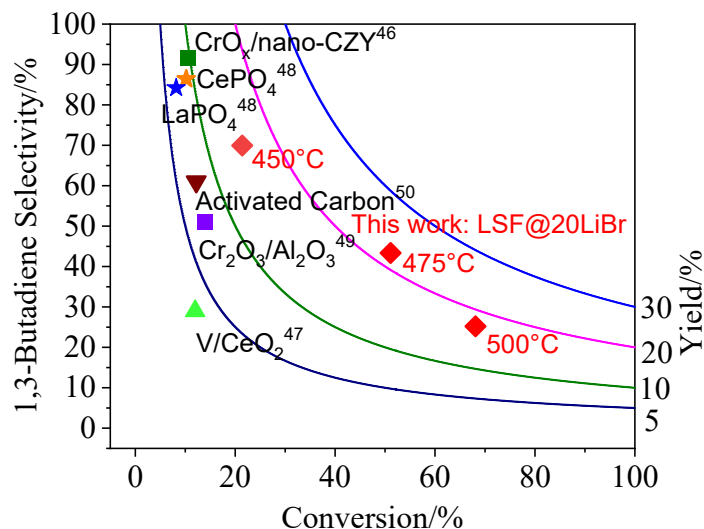


Figure 7. Extension to *iso*-butane ODH applications. A comparison of reported *iso*-butane ODH catalyst performance^{53–57} and the CL-ODHB catalyst reported in this work.

Discussion

1,3-butadiene is an important chemical building block. However, on-purpose butadiene production via catalytic dehydrogenation of *n*-butane is equilibrium limited, energy intensive, and coke prone. Oxidative dehydrogenation (ODH) of *n*-butane has the potential to efficiently produce butadiene without equilibrium limitation or coke formation. Despite of the extensive research efforts, single-pass butadiene yields are limited to <23% in conventional catalytic ODH with gaseous O₂. Moreover, the use of gaseous oxygen requires costly air separation units and raises safety concerns.

This work focuses on anaerobic ODH by utilizing the lattice oxygen species from a core-shell structured “perovskite@molten LiBr” redox catalyst. The modified perovskite (La_{0.8}Sr_{0.2}FeO₃ or LSF) is reduced with *n*-butane during the ODH step and then re-oxidized with air via a cyclic redox mode. By doing so, we integrate air separation with catalytic ODH while avoiding the direct contact between O₂ and *n*-butane. In this study, we demonstrated 42.5% butadiene yield, nearly doubling the maximum yield reported in literature. Experimental characterizations and AIMD simulations were carried out to determine the role of the molten LiBr shell, indicating that peroxide species formed on LSF react with the molten LiBr to form atomic Br as effective reaction intermediates for C-H bond activation. The as-formed butyl radical is sequentially dehydrogenated to form 1-butene, butenyl radicals, and then butadiene as the final product. The mechanistic findings provide a generalized approach for anaerobic ODH of light hydrocarbons for olefin production, as validated by experimental results on efficient *iso*-butane ODH to *iso*-butylene.

Despite of the promising results, we did observe a slow (~0.019 wt.%/hr) LiBr loss at high temperatures. This may cause the loss of butadiene selectivity over long-term operations. Further investigations on the effect of long-term LiBr loss, and strategies for on stream replenishment of the LiBr promoter would be important from a practical standpoint.

Materials and Methods

CL-ODHB catalysts preparation

La_{0.8}Sr_{0.2}FeO₃ (LSF) was purchased from Praxair Surface Technologies. To synthesize halogen salts coated LSF materials, an incipient wet impregnation method was applied. For example, to synthesize 20 wt% LiBr coated LSF, or LSF@20LiBr, 5 g of LSF was first weighed and placed into a beaker. Then, calculated amount of LiBr (ACS reagent, ≥99.0%) was dissolved in 5 mL of D.I. water and stirred to form a transparent solution. The solution was then placed onto LSF powders dropwise until it wetted the surface. The sample was then dried at 80°C. This procedure was repeated until all the LiBr solution has been added onto the LSF powder. The dried solids were then transferred into a ceramic sintering boat and sintered in a muffle furnace under air at 500°C for 5 h.

As a comparison, in-house LSF was synthesized using a modified Pechini method. Stoichiometric amounts of Fe(NO₃)₃·9H₂O (98%, Sigma-Aldrich), La(NO₃)₃·6H₂O (99.9%, Sigma-Aldrich), and Sr(NO₃)₂

(99%, Noah chemical) were dissolved in deionized water with stirring at 30 °C. Citric acid was then added to the solution at a 3:1 molar ratio to metal ions (Fe^{3+} , La^{3+} , and Sr^{2+}). The solution was stirred at 50 °C for 0.5 h to form a chelating solution. Ethylene glycol was then added to the solution to promote gel formation. The molar ratio between ethylene glycol and citric acid was 2:1. The solution was kept at 80 °C with stirring until a viscous gel formed. The gel was dried overnight at 130 °C in a convection oven. The sample was then calcined in a tube furnace at 950 °C for 12 h under continuous air flow to form in-house LSF. The subsequent LiBr impregnation method was the same as in synthesis of commercial LSF@LiBr.

CL-ODHB catalysts characterization

The physiochemical properties of the CL-ODHB catalysts were characterized with X-ray diffraction (XRD), X-ray photoelectron spectroscopy (XPS), Scanning transmission electron microscopy-Energy dispersive X-ray spectroscopy (STEM-EDS) and Differential scanning calorimetry (DSC). *Ex-situ* XRD was measured with a Rigaku SmartLab X-ray diffractometer to analyze the crystalline phases of catalysts under room temperature, with a radiation source of monochromatic $\text{CuK}\alpha$ ($\lambda=0.1542$) and operating condition at 40 kV and 44mA. *In-situ* XRD was measured with an Empyrean X-ray diffractometer in an Anton-Parr XRK-900 reactor chamber with a $\text{Cu K}\alpha$ ($\lambda = 0.1542$ nm) radiation source operated at 45 kV and 40 mA to generate XRD patterns under 500°C and under cyclic *n*-butane ODH and air re-oxidation steps. XPS was measured with a non-monochromatic $\text{MgK}\alpha$ (1254 eV) excitation source to quantify the near-surface elemental composition. A PHOIBIS 150 hemispherical energy analyzer (SPECS GmbH) was used to record and generate XPS patterns. STEM-EDS was measured with a ThermoFisher Titan 80-300 probe aberration corrected STEM with monochromator equipped with a SuperX EDS system at Analytical Instrumentation Facility (AIF) at NC State University. DSC was measured with a thermogravimetric analyzer (TA Instruments, Q600) instrument. In DSC measurements, 50 mg of samples were placed in an Al_2O_3 crucible inside the TA. Then, the system was heated up to 300 C with 5°C/min and held at 300°C for 1 h under 100 mL/min Ar flow to remove moisture. Then the system was further heated to 600 C with 5°C/min under 100 mL/min Ar flow and the heat adsorption signal was recorded.

Oxygen exchange rates measurement

Oxygen exchange rates were measured using $^{18}\text{O}_2$ -exchange experiments with a pulse experiment setup. A constant flow of 10% $^{16}\text{O}_2$ (50 ml min^{-1} , balance N_2) was used as the carrier gas and pulses of 1 mL of 10% $^{18}\text{O}_2$ (balance He) were dosed onto samples for oxygen isotopic exchange. The detailed experimental setup and methodologies were reported by Bouwmeester et al.⁵⁸ A downstream quadrupole mass spectrometer (QMS, MKS Cirrus II) was used to record the signals for oxygen isotopes, namely $^{16}\text{O}_2$, $^{16}\text{O}^{18}\text{O}$ and $^{18}\text{O}_2$. The quantification of these species were done by taking the integration of the characteristic peak Mass 32, Mass 34 and Mass 36, respectively.

Reactive performance testing

The as-prepared CL-ODHB catalysts were first sieved into 180-800 μm . In a typical experiment, 4 g of the catalyst particles were loaded into a fixed bed quartz U-tube reactor with I.D. = 1/8 inches. The reactor was then heated in a tubular furnace, with the testing temperature = 450 to 550°C. As an ODH step, 80 Vol.% of *n*-butane or *iso*-butane (Ar balance) were flown into the heated reactor for 15 seconds, with a total flow rate of 30 mL/min. The product distribution was monitored with a downstream GC (Agilent Technologies 7890B) with a flame ionization detector (FID) channel for hydrocarbon analysis and two thermal conductivity detector (TCD) channels for H_2 and CO/CO_2 . Then, the reactor was purged with 30 mL/min of Ar for 3 mins. Next, 20 Vol.% of O_2 (Ar balance) were flown into the heated reactor with a flow rate of 30 mL/min as the air re-oxidation step.

All the gaseous products in the ODHB step were collected using a gas bag, which was then analyzed by GC to obtain the overall product selectivity and yield over the entire ODHB half-cycle. Specifically, (1) the gas bag was connected to the downstream of the reactor 30s before start of the ODHB step; (2) the gaseous products of the entire ODHB step was injected into the gas bag; (3) the gas bag was connected for an additional 30s to ensure all the product gases are collected. The content of the gas bag was then injected into a GC sampling loop (Agilent Technologies 7890B) with a flame ionization detector (FID) channel for hydrocarbon analysis and two thermal conductivity detector (TCD) channels to quantify H_2 and CO/CO_2 . All species were quantified based on calibrated peak area and conversions, selectivities and yields were calculated based on these equations:

$$N\text{-butane conversion} = \frac{\text{Converted } n\text{-butane}}{\text{Feed } n\text{-butane}}$$

$$\text{Butadiene selectivity} = \frac{\text{Formed butadiene}}{\text{Converted } n\text{-butane}}$$

$$\text{Butadiene yield} = \frac{\text{Formed butadiene}}{\text{Feed } n\text{-butane}}$$

The selectivity and yield of other products (CO_x, butenes et al.) were obtained in the similar approach.

Computational tools

Ab initio molecular dynamics (AIMD) simulations were carried out using the Vienna *ab initio* Simulation Package (VASP). DFT electronic energies and the forces acting on the atoms were calculated with the Perdew-Burke-Ernzerhof (PBE) exchange correlation functional and the all-electron projector augmented wave (PAW) model. The kinetic energy cutoff was set to 350 eV for the plane-wave expansion of the electronic wave function. The DFT-D3 method was applied to include vdW interaction corrections. All calculations were performed at the Gamma point assuming spin-paired configurations.

The AIMD simulations for all the studied molten salt systems were performed at constant particle number, volume and temperature, respectively with a Nosé thermostat that keeps the temperature around 800 K, which is close to the experimental values (~573 K). The atomic motions were treated classically with a time-step of 1 fs. The internal energies were calculated from the MD simulations as the time average kinetic (E_{kin}) and potential energy:⁴²

$$\langle E \rangle_t = \frac{1}{t - t_0} \int_{t_0}^t (E_{DFT}(\tau) + E_{kin}(\tau)) d\tau$$

where E_{DFT} and E_{kin} represent the DFT total energy and the classical kinetic energy, respectively. t_0 represents the cutoff time to allow the system to equilibrate. The motions prior to time t_0 were discarded such that the systems are sufficiently randomized to “forget” the initial conditions. The energies of the gas-phase molecules were calculated by fixing their center of mass, followed by adding $3/2 k_B T$ as the translational contributions to the overall kinetic energy, where k_B is the Boltzmann constant. The estimated Gibbs free energy was calculated by $\Delta G_{estimate}^0 = \Delta E + p\Delta V - T\Delta S_{estimate}^0$, where the volume change (ΔV) was assumed to originate purely from changes in the number of gas phase molecules (Δn_{gas}) and is estimated by the ideal gas law ($p\Delta V = \Delta n_{gas} k_B T$). The entropies are obtained from the NIST-JANAF database (<https://janaf.nist.gov/>). Consistent with previous studies,^{42,59} zero-point energy (ZPE) corrections are not considered here because the required CPU time to accurately calculate the ZEP of tens of thousands of snapshots is prohibitively high.

Gas-phase thermo-conversions for butyl and butenyl radicals were calculated via Reaction Mechanism Generator (RMG)-3.1.0 and Chemkin-Pro. To build a comprehensive reaction network, a tolerance factor of 0.01 was used in the RMG simulation, using 90 Vol.% *n*-butane as feedstock (balance with Ar). The temperature was screened from 1000 to 1500 K, while the pressure was screened from 1 to 10 bar. To limit model size and avoid unreasonable products, maximum carbon number was set as 8 and maximum oxygen number was set as 4. After the model was built, Chemkin-Pro was used to simulate gas-phase kinetics with respect to reaction time, using zero-D batch reactor model. The condition for the simulation was set as 500°C and 1 atm, with 80 Vol.% butyl radical or butenyl radical as feedstock (balance with Ar). The residence time for the simulation was 1 s and steady-state product distributions were achieved.

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