

# Effect of Drift Layer Doping and NiO Parameters in Achieving 8.9 kV Breakdown in 100 $\mu\text{m}$ Diameter and 4kV /4A in 1mm Diameter NiO/ $\beta$ -Ga<sub>2</sub>O<sub>3</sub> Rectifiers

Running title: 8.9 kV Breakdown in NiO/ $\beta$ -Ga<sub>2</sub>O<sub>3</sub> Rectifiers

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The effect of doping in the drift layer and the thickness and extent of extension beyond the cathode contact of a NiO bilayer in vertical NiO/ $\beta$ -Ga<sub>2</sub>O<sub>3</sub> rectifiers is reported. Decreasing the drift layer doping from  $8 \times 10^{15}$  to  $6.7 \times 10^{15} \text{ cm}^{-3}$  produced an increase in reverse breakdown voltage ( $V_B$ ) from 7.7kV to 8.9 kV, the highest reported to date for small diameter devices (100 $\mu\text{m}$ ). Increasing the bottom NiO layer from 10 to 20 nm did not affect the forward current-voltage characteristics but did reduce reverse leakage current for wider guard rings and reduced the reverse recovery switching time. The NiO extension beyond the cathode metal to form guard rings had only a slight effect ( $\sim 5\%$ ) in reverse breakdown voltage. The use of NiO to form a pn heterojunction made a huge improvement in  $V_B$  compared to conventional Schottky rectifiers, where the breakdown voltage was  $\sim 1\text{kV}$ . The on-state resistance ( $R_{ON}$ ) was increased from  $7.1 \text{ m}\Omega\cdot\text{cm}^2$  in Schottky rectifiers fabricated on the same wafer to  $7.9 \text{ m}\Omega\cdot\text{cm}^2$  in heterojunctions. The maximum power figure of merit ( $V_B$ )<sup>2</sup>/ $R_{ON}$  was  $10.2 \text{ GW}\cdot\text{cm}^{-2}$  for the 100 $\mu\text{m}$  NiO/Ga<sub>2</sub>O<sub>3</sub> devices. We also fabricated large area (1 mm<sup>2</sup>) devices on the same wafer, achieving  $V_B$  of 4 kV and 4.1 A forward current. The figure-of-merit was  $9 \text{ GW}\cdot\text{cm}^{-2}$  for these devices. These parameters are the highest reported for large area Ga<sub>2</sub>O<sub>3</sub> rectifiers. Both the small

area and large area devices have performance exceeding the unipolar power device performance of both SiC and GaN.

## I. INTRODUCTION

The increasing electrification of automobiles and the need to switch renewable energy sources in the existing power grid has increased demand for energy efficient power electronics capable of higher voltage and currents than existing Si devices. This has focused attention on the wide and ultra-wide bandgap semiconductors <sup>(1-5)</sup>, with the latter including diamond, AlN and Ga<sub>2</sub>O<sub>3</sub>. The ability to grow large diameter, high quality crystals from melt-grown methods and the attendant low cost of production has spurred interest in  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> <sup>(1-5)</sup>. One of the goals is to achieve a high -power figure of merit for power electronic devices, defined as  $(V_B)^2/R_{ON}$  where  $V_B$  is the reverse breakdown voltage and  $R_{ON}$  is the on-state resistance <sup>(1,3,4)</sup>. To achieve a high-power figure of merit, a rectifier must have a low drift layer concentration, with high electron mobility, as well as low  $R_{ON}$ , and optimized edge termination to prevent current crowding <sup>(1, 5-21)</sup>. The breakdown voltage is larger for thicker drift layers, but this degrades on-resistance. To achieve a low  $R_{ON}$ , a thin drift layer with high electron mobility is required. In addition, vertical geometry devices are desirable, because of their higher power conversion efficiency and absolute currents compared to lateral devices <sup>(1,3,4,5)</sup>. Power rectifiers are also building blocks for many advanced power handling systems.

A drawback with Ga<sub>2</sub>O<sub>3</sub> is the absence of facile p-type doping. All of the potential acceptor dopants have large ionization energies and are not significantly ionized at room temperature. This has led to the use of p-type oxides, principally polycrystalline NiO, to form p-n heterojunctions with n-type Ga<sub>2</sub>O<sub>3</sub> <sup>(6-14)</sup>. The forward current transport mechanism in such junctions is typically recombination at low biases and trap-assisted

tunneling at higher bias <sup>(10, 21-26)</sup>. Promising rectifier performance has been reported with this approach <sup>(12-14, 21-39)</sup>, including  $V_B$  of 8.32 kV, with figure of merit  $13.2 \text{ GW.cm}^{-2}$  <sup>(12)</sup>.

Optimization of the heterojunction rectifier device structure is crucial to achieve both high  $V_B$  and low  $R_{ON}$ , as well as providing management of the maximum electric fields within the structure to enhance further the device voltage blocking capability <sup>(41-47)</sup>. The design variables include the thickness and doping of the layers, doping in the drift layer and the use of the NiO as a guard ring by extending it beyond the metal cathode. In this paper we report an investigation of the effect of these parameters on the performance of NiO/Ga<sub>2</sub>O<sub>3</sub> vertical rectifiers. A new highest  $V_B$  for these devices is achieved.

## II. EXPERIMENTAL

We made both vertical geometry Schottky rectifiers and NiO/ Ga<sub>2</sub>O<sub>3</sub> rectifiers on the same wafers. The parameters investigated are shown in the schematic of the vertical heterojunction rectifiers in Figure 1. We varied the thickness of the second layer in the bilayer NiO (10 or 20 nm, with fixed thickness of the top layer held constant at 10 nm) and the length of the NiO extension beyond the cathode contact (12-20  $\mu\text{m}$ ) to form guard rings. The choice of these parameters was guided by TCAD simulations with the Silvaco Atlas code of electric field distributions, as reported previously <sup>(14)</sup>. Finally, we had two different drift region doping levels at a fixed thickness of 10  $\mu\text{m}$ . The epitaxial layers were grown by halide vapor phase epitaxy (HVPE) on a (001) Sn-doped ( $10^{19} \text{ cm}^{-3}$ )  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> single crystal substrate. These samples were purchased from Novel Crystal Technology, Japan.

Ohmic contacts were made to the rear surface using a Ti/Au metal stack deposited by e-beam evaporation. This was annealed at 550°C for 180s under N<sub>2</sub>. The front surface was exposed to UV/Ozone exposure for 15 mins to remove contamination. The NiO bilayer was deposited by rf (13.56 MHz) magnetron sputtering at a working pressure of 3mTorr<sup>(14,41)</sup>. The hole concentration in these films was adjusted using the Ar/O<sub>2</sub> ratio. The structure was then annealed at 300°C under O<sub>2</sub>. Finally, a cathode contact of 20/80 nm Ni/Au (100 μm diameter) was deposited onto the NiO layer. The NiO was extended from 12-20 μm beyond the contact metal to form a guard ring. Figure 2 shows the C<sup>-2</sup>-V plots for the two different drift layer doping levels. These show the carrier concentrations were 6.7x10<sup>15</sup> cm<sup>-3</sup> and 8x10<sup>15</sup> cm<sup>-3</sup>, respectively.

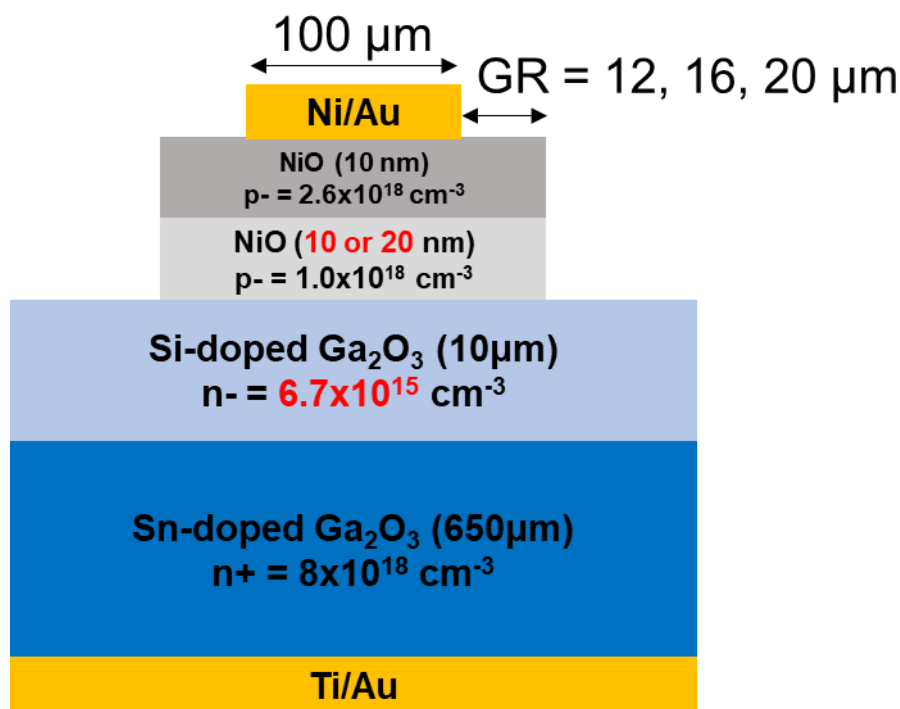


Fig 1. Schematic of NiO/Ga<sub>2</sub>O<sub>3</sub> heterojunction rectifier. The extension of the NiO beyond the Ni/Au contact to act as a guard ring was investigated for different extension lengths, as well as the thickness of the bottom NiO layer and the drift layer doping.

The current density-voltage (J-V) characteristics were measured on a Tektronix 370-A curve tracer, 371-B curve and Agilent 4156C. For the highest reverse voltages, a Glassman power supply was employed. The reverse breakdown voltage was defined as the bias for a reverse current reaching  $0.1 \text{ A.cm}^2$ . The high bias measurements were performed in Fluorinert atmosphere at  $25^\circ\text{C}$ . The devices did not suffer permanent damage at this condition but increasing the voltage a further 50-200 V led to permanent failure through breakdown at the contact periphery. The on-resistance values were calculated assuming the current spreading length is  $10 \text{ }\mu\text{m}$  and a  $45^\circ$  spreading angle. We also subtracted the resistance of the cable, probe and chuck, which was around  $10 \text{ }\Omega$ .

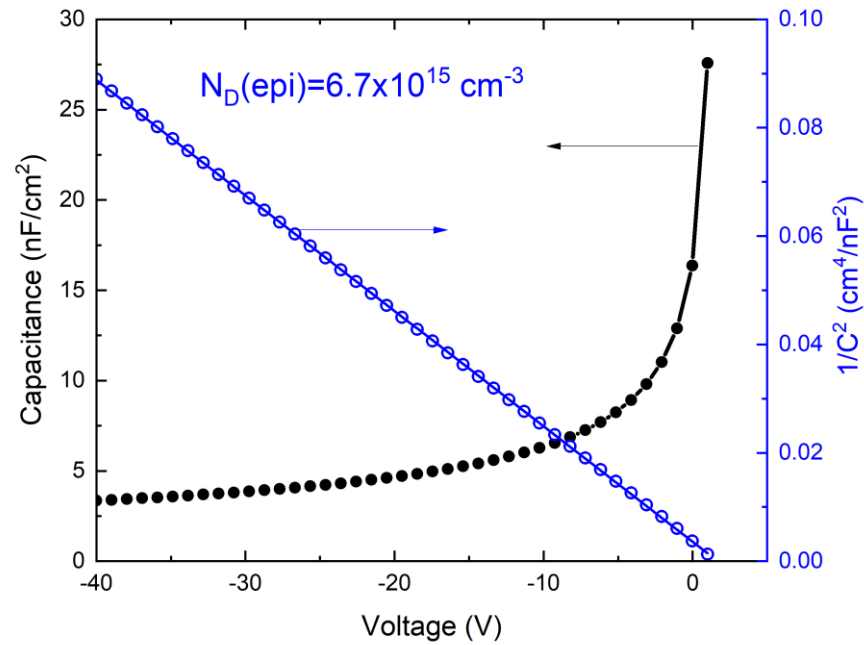


Fig. 2. C-V characteristics for determining carrier density in drift region for the two different types of wafers investigated. The drift layer thickness was  $\sim 10 \text{ }\mu\text{m}$  in both cases.

### III. RESULTS AND DISCUSSION

### **A. Small Area Rectifiers to Achieve High Breakdown Voltage**

Figure 3 shows the forward current densities and  $R_{ON}$  values for rectifiers with different guard ring dimensions fabricated with (a) 10/10 nm NiO bilayer or (b) 10/20 nm NiO bilayer. These were fabricated on the drift region with the lower carrier density. There is very little difference in these forward current density characteristics for either the NO bilayer thickness or the guard ring diameter.

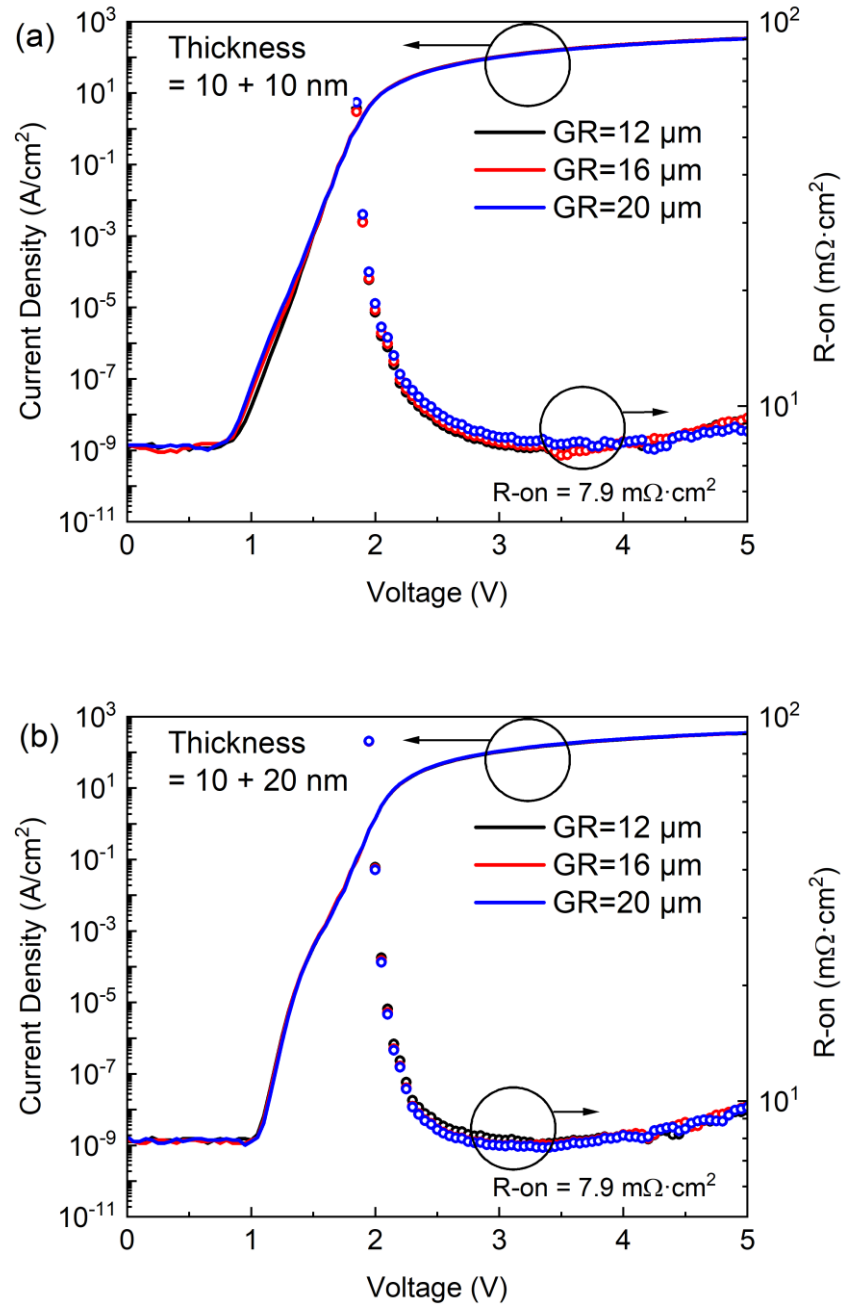


Fig. 3. Forward current densities and  $R_{ON}$  values for rectifiers with different guard rings dimensions fabricated with (a) 10/10 nm NiO bilayer or (b) 10/20 nm NiO bilayer.

Figure 4 shows a comparison of the results from the NiO/Ga<sub>2</sub>O<sub>3</sub> heterojunction rectifiers with the Schottky rectifier fabricated on the same wafer. The on-resistance for

the former was  $7.9 \text{ m}\Omega \cdot \text{cm}^2$ . For the Schottky rectifiers, this parameter was slightly lower, as expected, at  $7.1 \text{ m}\Omega \cdot \text{cm}^2$ . Both types of devices had forward current densities  $> 100 \text{ A}\cdot\text{cm}^{-2}$  at 5 V. The turn-on voltage was 1.9-2.1 V for the heterojunction rectifiers.

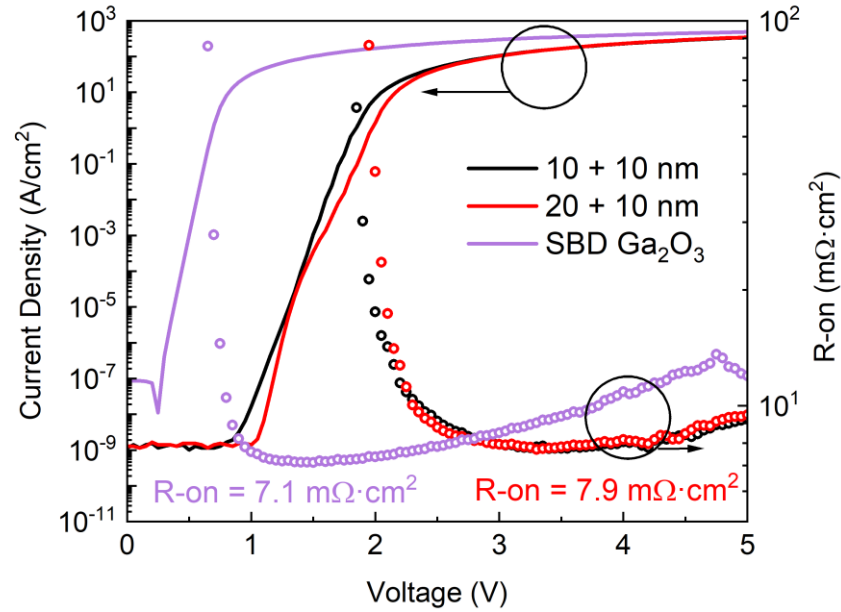


Fig. 4 Comparison of forward current density characteristics for Schottky and NiO/Ga<sub>2</sub>O<sub>3</sub> rectifiers.

Figure 5 shows the reverse I-V characteristics out to -100V for (a) NiO/Ga<sub>2</sub>O<sub>3</sub> rectifiers with 10/10 nm NiO bilayers or (b) 10/20 nm NiO bilayers. While the guard ring diameter makes little difference to devices with the 10/10 nm NiO bilayer, there is a reduction in reverse current density for the smaller guard rings. A comparison of the heterojunction results with those from the Schottky rectifiers all fabricated on the lower drift layer doping structure is shown in Figure 6 for a fixed guard ring diameter of 12  $\mu\text{m}$  in the latter type of device. As expected, the leakage current from the heterojunction rectifiers is lower than that of the Schottky rectifier and reducing the doping in the drift layer also lowers the reverse current density<sup>(20,21,48-51)</sup>. Similar trends were observed for

the two types of devices fabricated on the higher drift layer doping. The p-n junction has a larger effective barrier for current transport than the metal gate Schottky rectifiers.

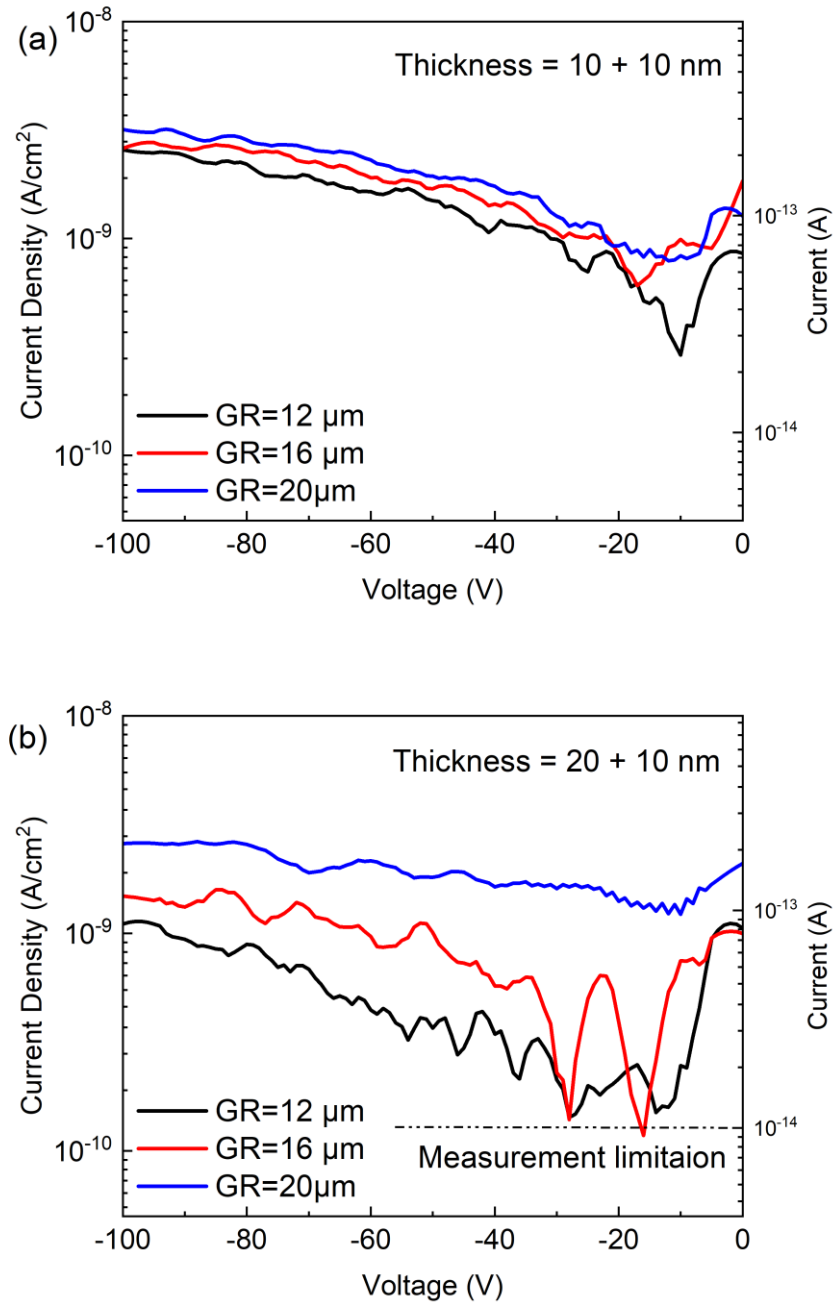


Fig. 5. Reverse I-V characteristics out to -100V for (a) NiO/Ga<sub>2</sub>O<sub>3</sub> rectifiers with 10/10 nm NiO bilayers or (b) 10/20 nm NiO bilayers.

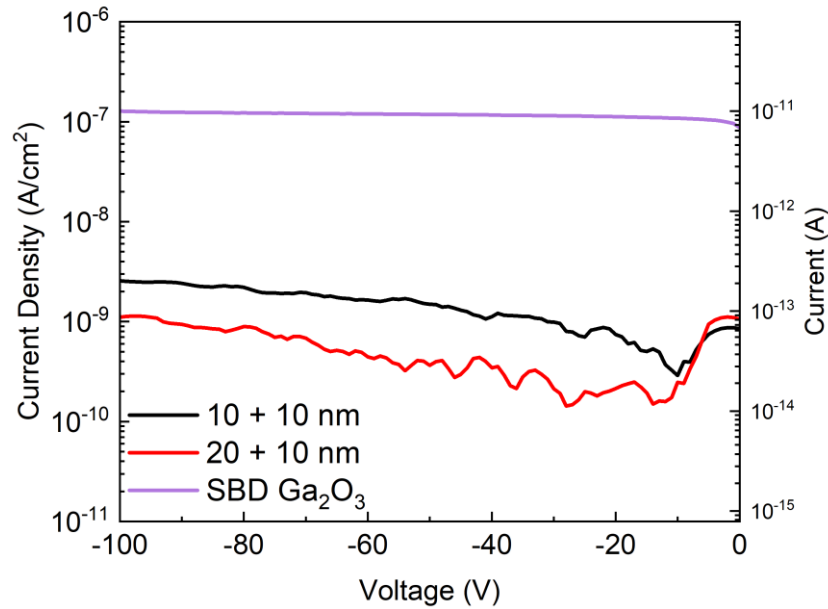


Fig. 6. Comparison of low bias reverse current characteristics between Schottky rectifiers and NiO/Ga<sub>2</sub>O<sub>3</sub> rectifiers with either 10/10 nm or 10/20 nm bilayers. All these were fabricated on the sample with drift layer doping  $6.7 \times 10^{15} \text{ cm}^{-3}$ .

The reverse J-V characteristics over the full bias range are shown in Figure 7 (a) for the devices fabricated on the  $6.7 \times 10^{15} \text{ cm}^{-3}$  drift layers with different NiO thicknesses as well as different guard ring diameters. Once again, for comparison, we show the result for the Schottky rectifier and for a heterojunction device fabricated on the wafer with larger drift layer concentration of  $8 \times 10^{15} \text{ cm}^{-3}$ . The key points from this data are firstly, that the lower doping produces a higher reverse breakdown voltage, with a maximum of 8.9 kV. This is the highest reported to date for Ga<sub>2</sub>O<sub>3</sub> rectifiers of any type<sup>(12)</sup>. The second point is that the heterojunction really increases reverse breakdown voltage compared to the Schottky rectifier. The  $V_b$  of the latter was 750V, while the

device reached 1218 V before permanent burn out. The final point is that the NiO thickness and guard ring extension length made only a relatively small difference in  $V_B$ .

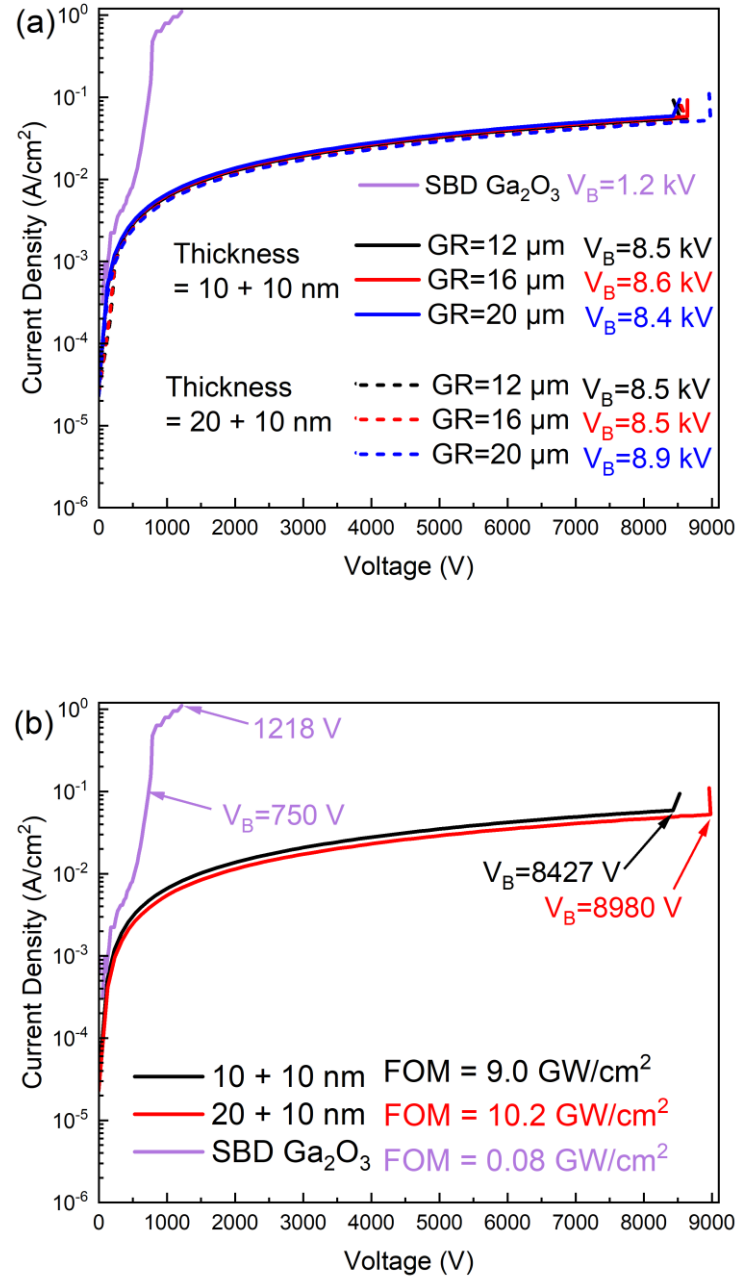


Fig. 7. (a). Reverse current characteristics from Schottky rectifier and NiO/Ga<sub>2</sub>O<sub>3</sub> heterojunction rectifiers with different guard ring extensions and NiO layer thicknesses.

(b) comparison between Schottky and NiO/Ga<sub>2</sub>O<sub>3</sub> heterojunction rectifiers fabricated on the lowest drift layer doping wafer.

Figure 7(b) shows a comparison of the breakdown voltages for the devices fabricated on the lower drift layer doped layers, as a function of the NiO thickness. The power figure of merit was 10.2 GW.cm<sup>-2</sup> for the optimized heterojunction rectifier, compared to 0.08 GW/cm<sup>-2</sup> for the Schottky rectifier. The theoretical maximum is ~34 GW.cm<sup>-2</sup>, showing that further improvement should be possible as the edge termination and epi layer quality continue to evolve<sup>(4, 12)</sup>. The average electric field strength is 8.7 MV/cm. For biases >100 V, the reverse leakage current follows a  $\ln(I) \propto V$  relation. This indicates the dominant leakage mechanism is electron variable-range-hopping via defect-related states in the drift region<sup>(10,12)</sup>. This has been reported in detail by numerous groups<sup>(9,10,12,14)</sup>.

Figure 8 shows the on-off ratio of NiO/Ga<sub>2</sub>O<sub>3</sub> heterojunction rectifiers in which the bias was switched from 5V forward to the reverse voltage shown on the x-axis. For comparison, the results for a Schottky rectifier fabricated on the same wafer are included. The values are still >10<sup>11</sup> when switching to 100V and approximately two orders of magnitude higher than that of the Schottky rectifier over this bias range. This again emphasizes an advantage of the p-n heterojunction in achieving excellent rectification characteristics.

Figure 9 shows the reverse recovery switching waveform when switching from 50 mA forward current to -10V for heterojunction rectifiers with (a) 10/10 nm or (b) 10/20 nm bilayers as a function of guard ring extension. The reverse recovery times are ~21 ns and are tabulated in Table 1. These measurements were made with a custom switching

circuit, as described previously<sup>(41-43)</sup>. We used  $di/dt$  values around 2.9 A/us. Others have reported use of values in the range 100-400 A/us<sup>(48,63)</sup>. Figure 10 shows a comparison of switching waveforms of Schottky and NiO/Ga<sub>2</sub>O<sub>3</sub> heterojunction rectifiers. The relative indifference to device structure demonstrates that charge storage in the p-n junction is not a significant factor compared to the Schottky device<sup>(13,14)</sup>. The Schottky diode had higher forward current due to lower effective barrier height.

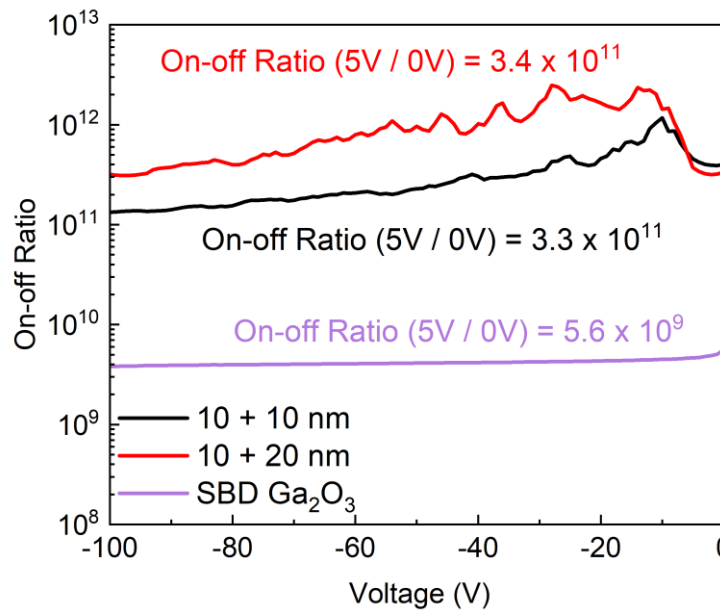


Fig. 8. On-off ratio of 100  $\mu$ m diameter NiO/Ga<sub>2</sub>O<sub>3</sub> heterojunction rectifiers in which the bias was switched from 5V forward to the voltage shown on the x-axis. For comparison, the results for a Schottky rectifier fabricated on the same wafer are included.

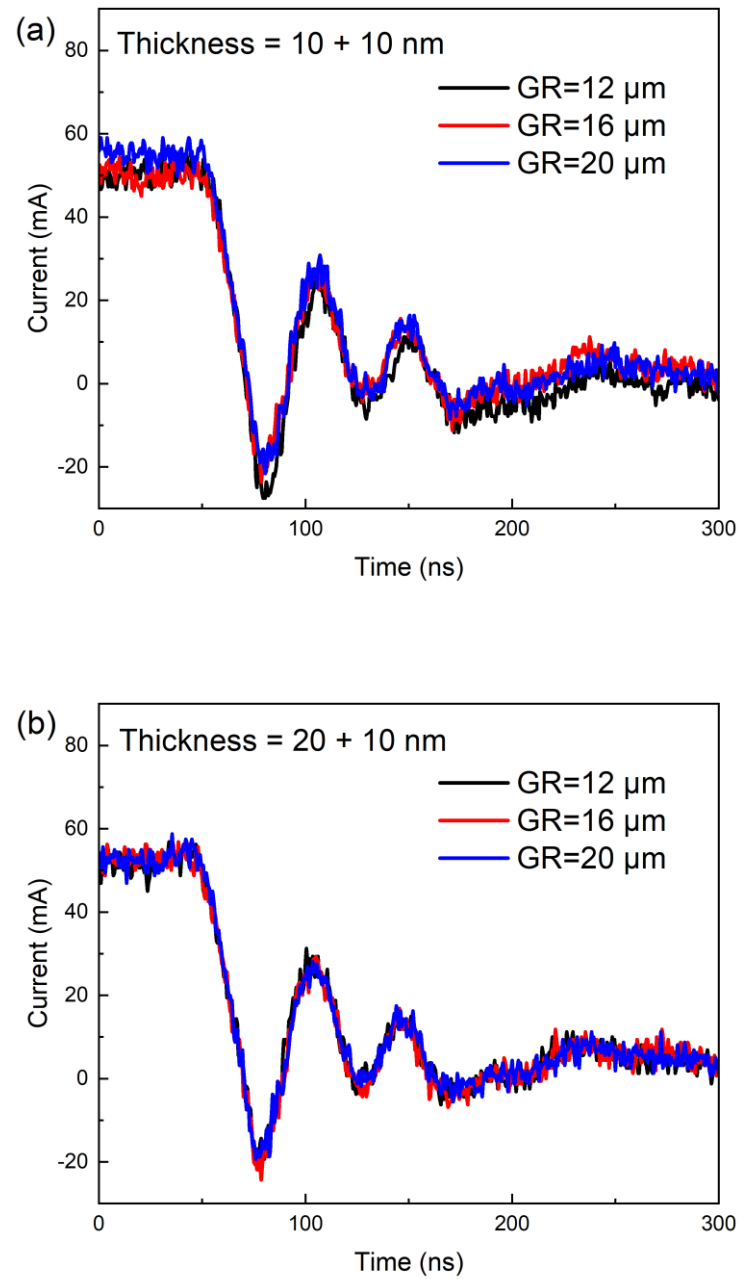


Fig. 9. (a) Switching waveform for NiO/Ga<sub>2</sub>O<sub>3</sub> heterojunction rectifiers with (a) 10/10 nm or (b) 10/20 nm bilayers as a function of guard ring extension.

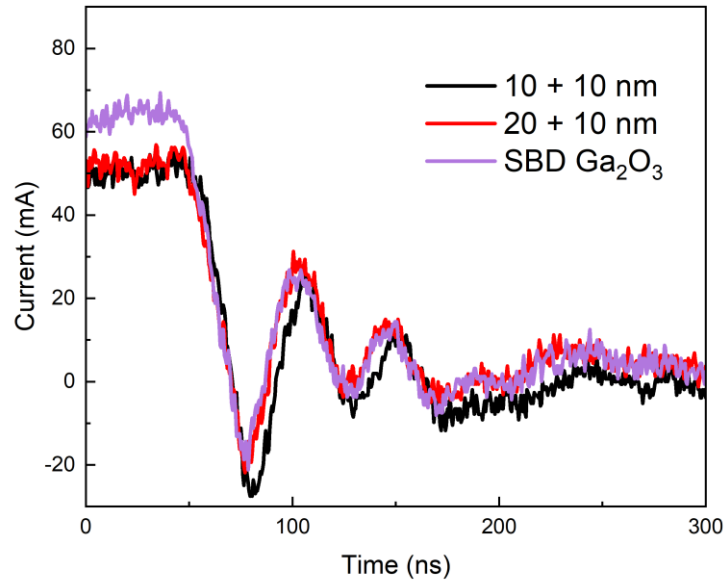


Fig. 10. Comparison of switching waveforms of Schottky and NiO/Ga<sub>2</sub>O<sub>3</sub> heterojunction rectifiers.

Table 1. Summary of reverse recovery parameters for heterojunction and Schottky rectifiers

|          | $T_{rr}$<br>(ns) | $I_{rr}$<br>(mA) | $dI/dT$<br>(A/ $\mu$ s) | $I_F$<br>(mA) |
|----------|------------------|------------------|-------------------------|---------------|
| 10+10 nm | 19.6             | 27.5             | 2.9                     | 50            |
| 20+10 nm | 13.8             | 21.6             | 2.9                     | 50            |
| Schottky | 14.6             | 21.4             | 2.5                     | 65            |

Figure 11 shows a literature compilation of  $R_{on}$  versus  $V_B$  results for all the common types of rectifiers fabricated in the Ga<sub>2</sub>O<sub>3</sub> materials system. These include metal gate Schottky barrier or junction barrier Schottky rectifiers, along with NiO/Ga<sub>2</sub>O<sub>3</sub>

Fig. 11. Compilation of  $R_{on}$  versus  $V_B$  of conventional and NiO/Ga<sub>2</sub>O<sub>3</sub> heterojunction small area rectifiers reported in the literature.

### B. Large Area Devices to Achieve High Forward Current

There has been much less reported on large area  $\text{Ga}_2\text{O}_3$  rectifiers, which are needed to achieve large absolute forward conduction currents<sup>(47, 55-64)</sup>. These are typically referred to as Ampere-class power devices. A recent review has discussed switching performance, packaging and approaches to thermal management<sup>(47)</sup>.

We fabricated  $1 \text{ mm}^2$  devices with the same structure as shown in Figure 1. Figure 12 shows the forward J-V characteristics of two such devices with different NiO thicknesses, with a maximum forward current of 4.1 A at 10 V forward bias. The  $R_{\text{ON}}$  values are  $1.8\text{-}1.9 \text{ m}\Omega\cdot\text{cm}^2$ . While rectifier arrays have achieved currents in the range 33-100 A, the 4 A for an individual device is still behind those of Gong et al.<sup>(48)</sup> and Zhou et al.<sup>(63)</sup>, where 12 A was achieved. Large area packaged  $\text{Ga}_2\text{O}_3$  SBDs with an anode size of  $3\times 3 \text{ mm}^2$  have been reported with forward current of over 15 A<sup>(55)</sup>.

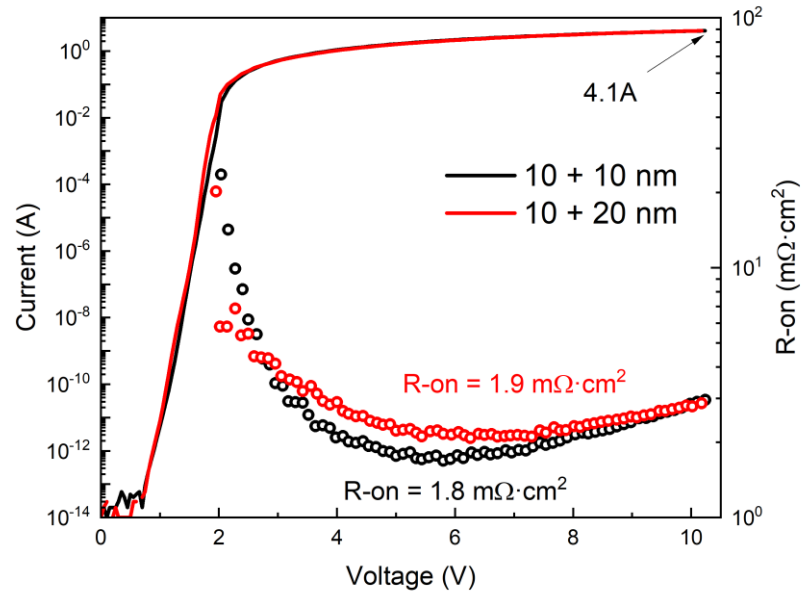


Fig. 12. Forward current characteristics for  $1 \text{ mm}^2$  heterojunction rectifiers for two different NiO thicknesses.

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The reverse J-V characteristics are shown in Figure 13 for two different types of structure with varying NiO thickness. Figure 13 (a) shows the low voltage ( -100V) range, while (b) shows the  $V_B$  values are around 4kV. These are the highest reported for Ampere-class  $\text{Ga}_2\text{O}_3$  rectifiers. Once again, the NiO thickness does not have a significant impact on the magnitude of the breakdown voltage.

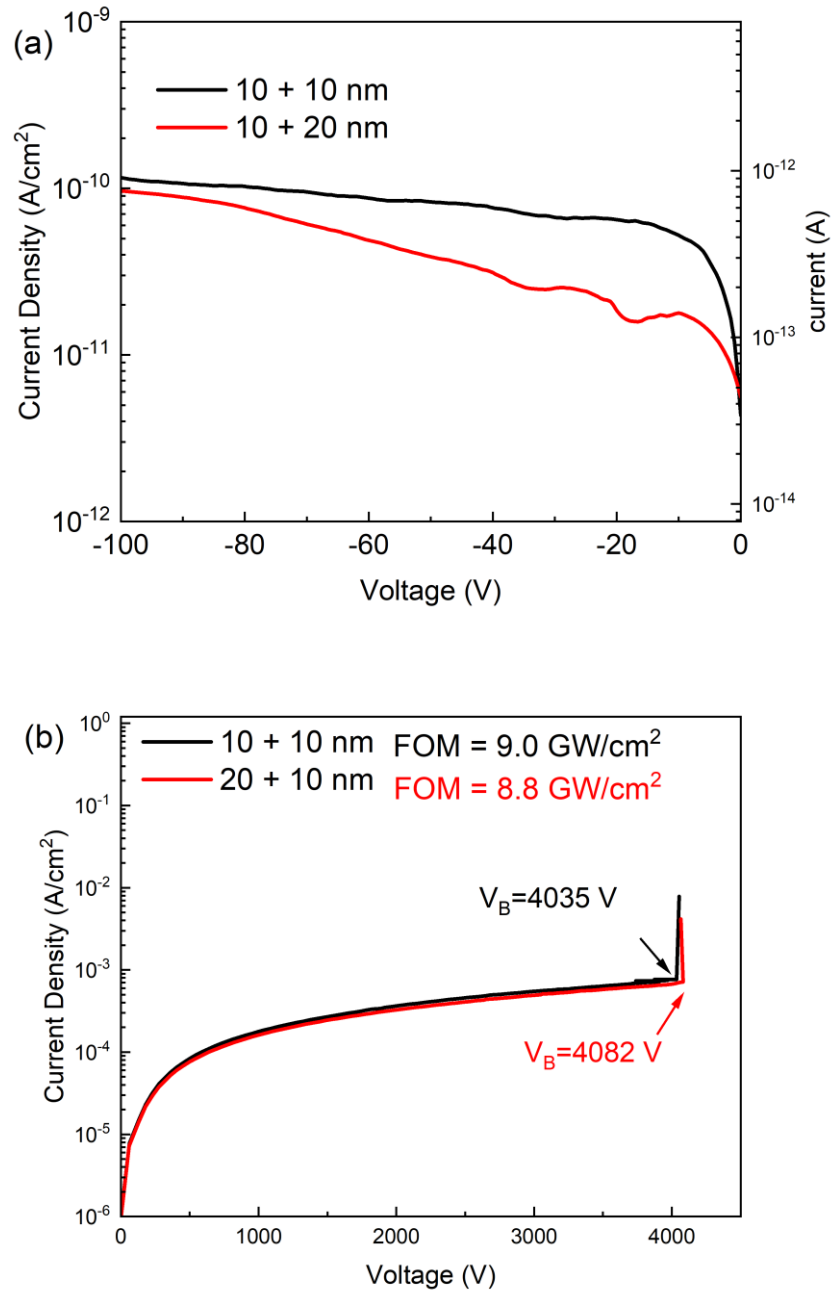


Fig. 13. Reverse J-V characteristics out to (a) -100V for NiO/Ga<sub>2</sub>O<sub>3</sub> rectifiers with 10/10 nm 10/20 nm NiO bilayers. (b) over full bias range to show V<sub>B</sub>.

Figure 14 shows the on-off ratio of 1 mm<sup>2</sup> NiO/Ga<sub>2</sub>O<sub>3</sub> heterojunction rectifiers in which the bias was switched from 5V forward to the voltage shown on the x-axis. The

on-off ratio is  $>10^{12}$  over the whole bias range investigated and is slightly better for the thicker NiO layers. For switching from 10V to 0V, the ratio is  $\sim 10^{14}$  in both cases and these large area devices retain excellent rectification, showing that the increased likelihood of having defects within the active area have not degraded this property. Sdoeung et al.<sup>(65)</sup> reported that threading dislocations in HVPE layers of the type we are using are responsible for significant contributions to reverse leakage current in rectifiers. Figure 15 shows a compilation of on-off ratio versus power figure of merit of conventional and NiO/Ga<sub>2</sub>O<sub>3</sub> heterojunction rectifiers reported in the literature.

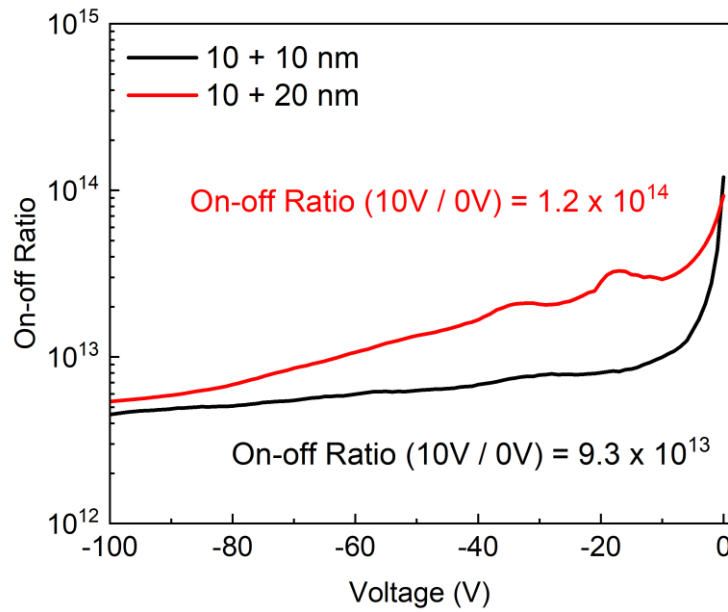


Fig. 14. On-off ratio of 1 mm<sup>2</sup> NiO/Ga<sub>2</sub>O<sub>3</sub> heterojunction rectifiers in which the bias was switched from 5V forward to the voltage shown on the x-axis.

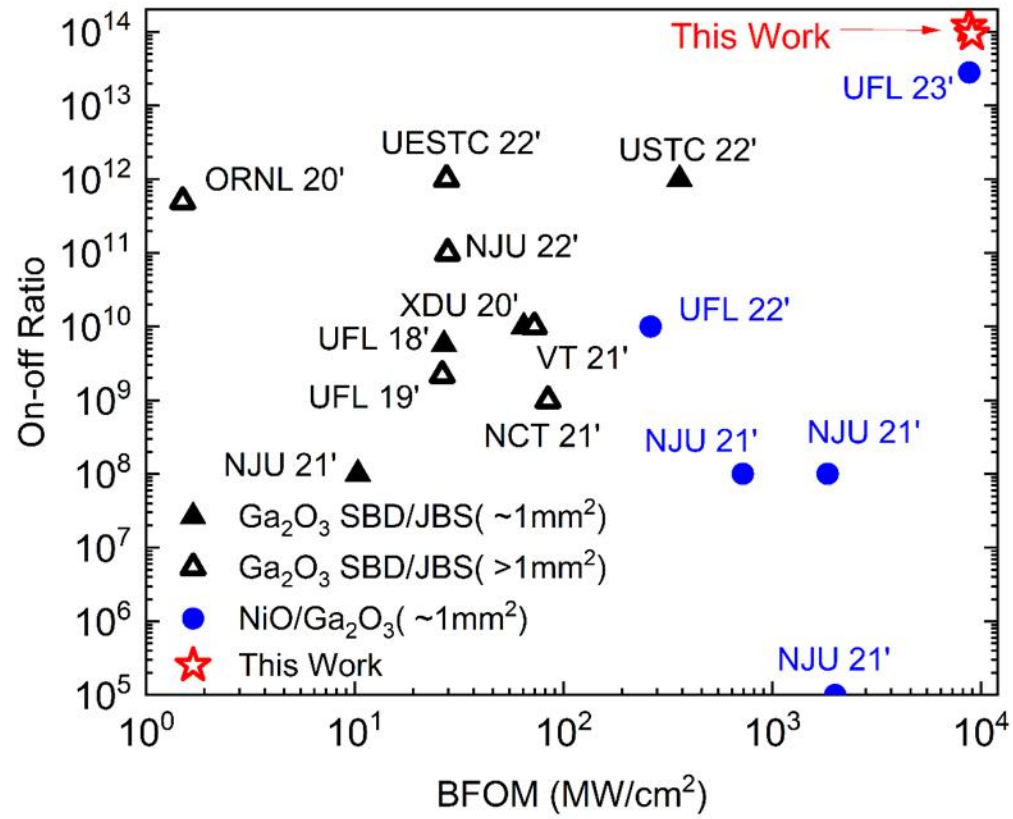


Fig. 15. Compilation of on-off ratio versus power figure of merit of conventional and NiO/Ga<sub>2</sub>O<sub>3</sub> heterojunction rectifiers reported in the literature.

Figure 16 shows a compilation of  $R_{on}$  versus  $V_B$  of large area conventional and NiO/Ga<sub>2</sub>O<sub>3</sub> heterojunction rectifiers reported in the literature. Our results represent the best combination of breakdown voltage and on-state resistance reported to date and show the impressive advances in material quality in terms of reducing both background carrier density and extended defect density.

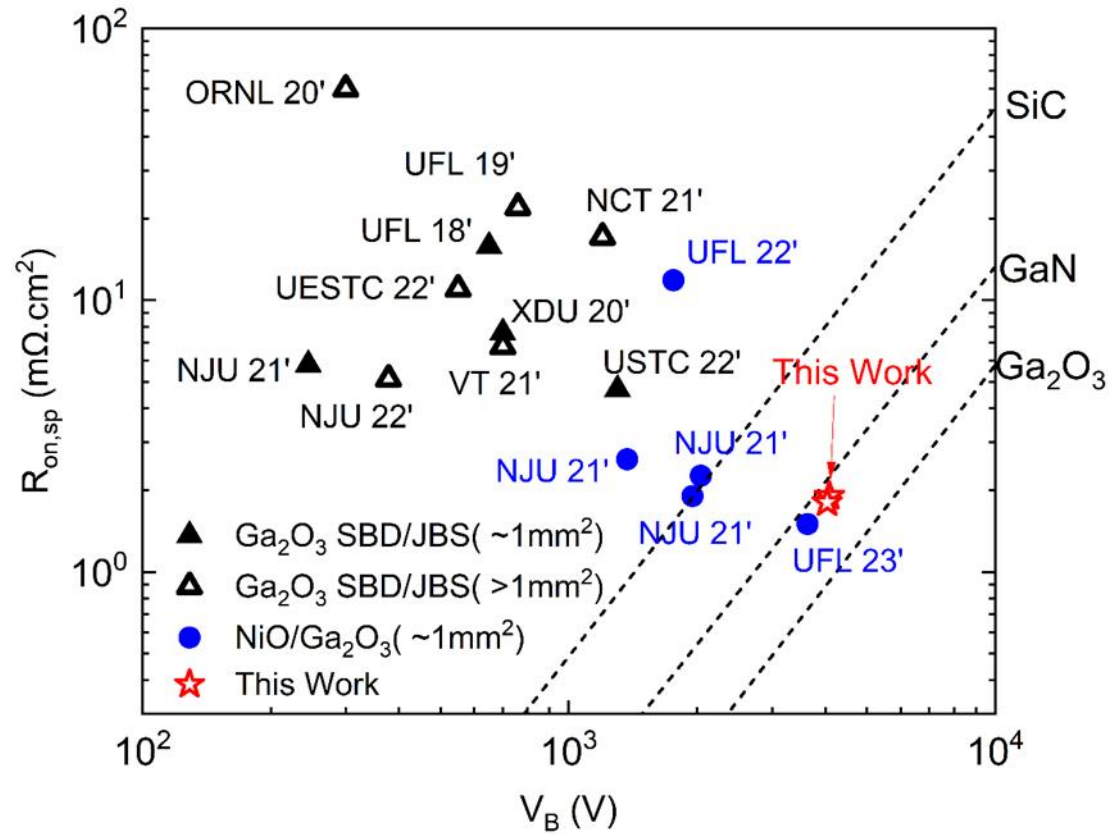


Fig.16. Compilation of  $R_{on}$  versus  $V_B$  of large area conventional and  $NiO/Ga_2O_3$  heterojunction rectifiers reported in the literature.

## IV. SUMMARY AND CONCLUSIONS

In summary, we optimized the  $NiO$  bilayer thickness and extension of these layers beyond the cathode contact on  $NiO/\beta\text{-}Ga_2O_3$  p-n heterojunction rectifiers to achieve  $V_B$  8.9 kV with  $R_{on}$  of  $7.9 m\Omega \cdot cm^2$  and a resultant figure-of-merit ( $V_b^2/R_{on}$ ) of  $10.2 GW \cdot cm^{-2}$ . The heterojunction produces breakdown voltages far more than Schottky rectifiers fabricated on the same wafer and confirms that the  $NiO$  can act as both p-layer and guard ring material. This approach now consistently produces power figure of merits

that exceed the unipolar power device performance of both GaN and SiC. It will still be necessary to establish the long-term reliability of devices fabricated by this approach. For large area devices, the low thermal conductivity limitations of Ga<sub>2</sub>O<sub>3</sub> remain as a primary issue. In addition, more work is needed to understand the surge current capability of Ga<sub>2</sub>O<sub>3</sub>-based rectifiers and the packaging approaches needed to achieve practical operating characteristics, along with establishing the junction-to-ambient thermal resistance of junction side cooling approaches <sup>(66)</sup>.

## ACKNOWLEDGMENTS

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### Data Availability

The data that supports the findings of this study are available within the article.

### Declarations

The authors have no conflicts to disclose.

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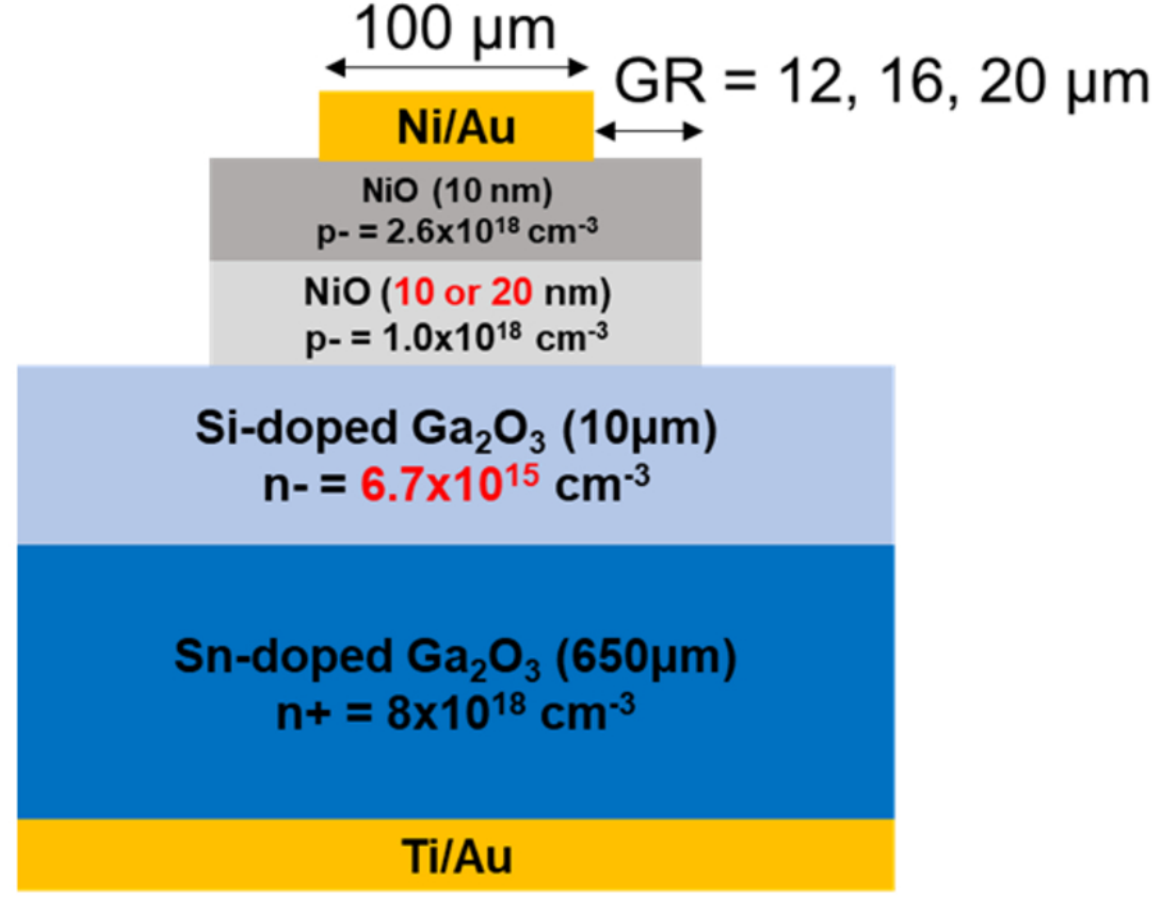
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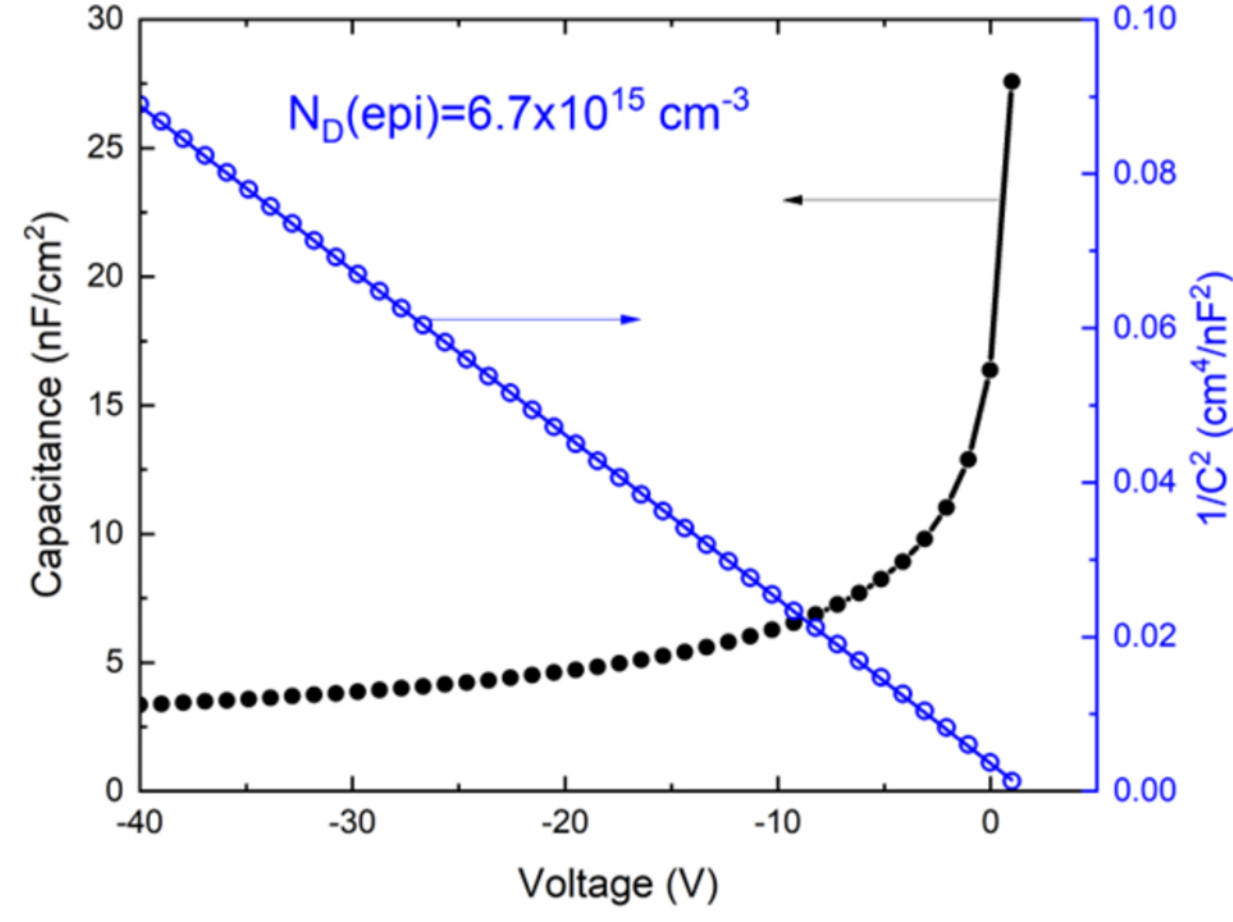
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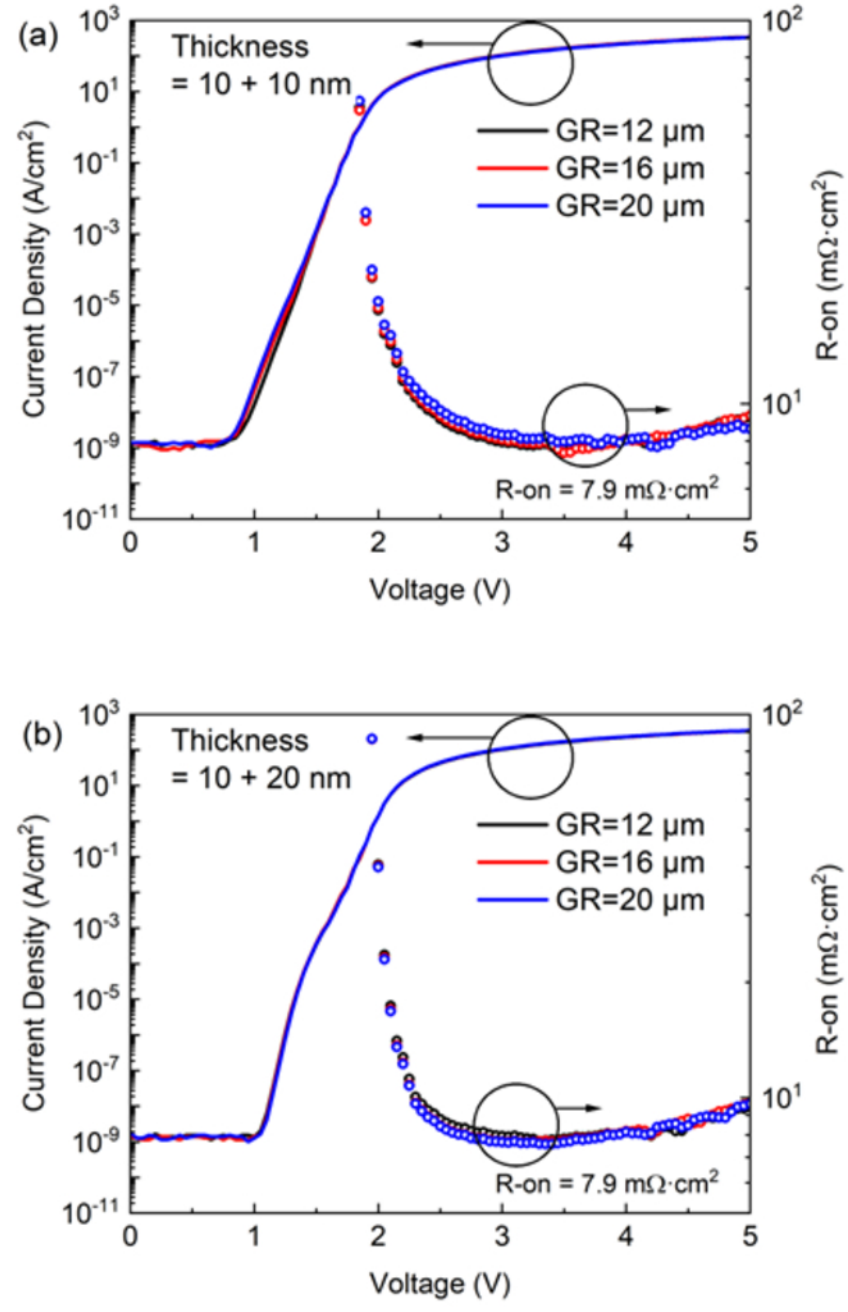
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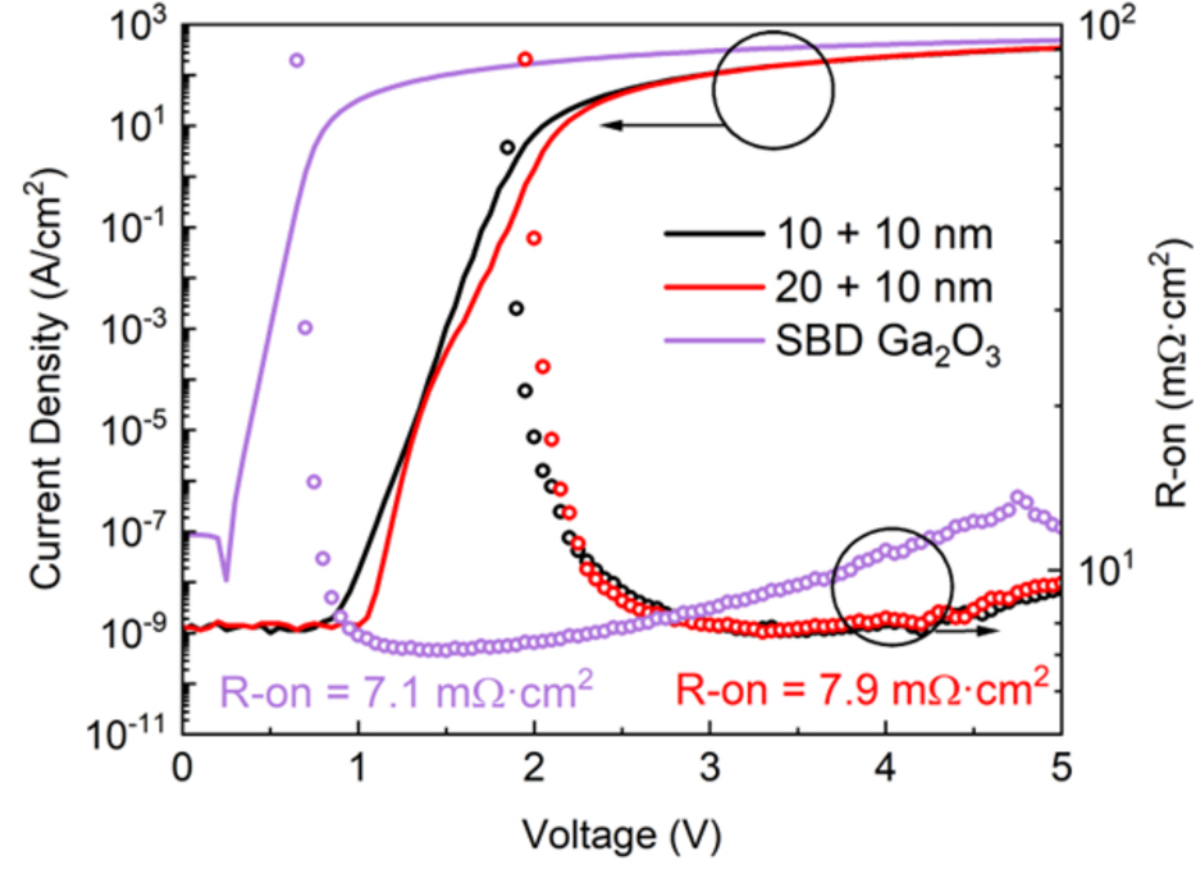
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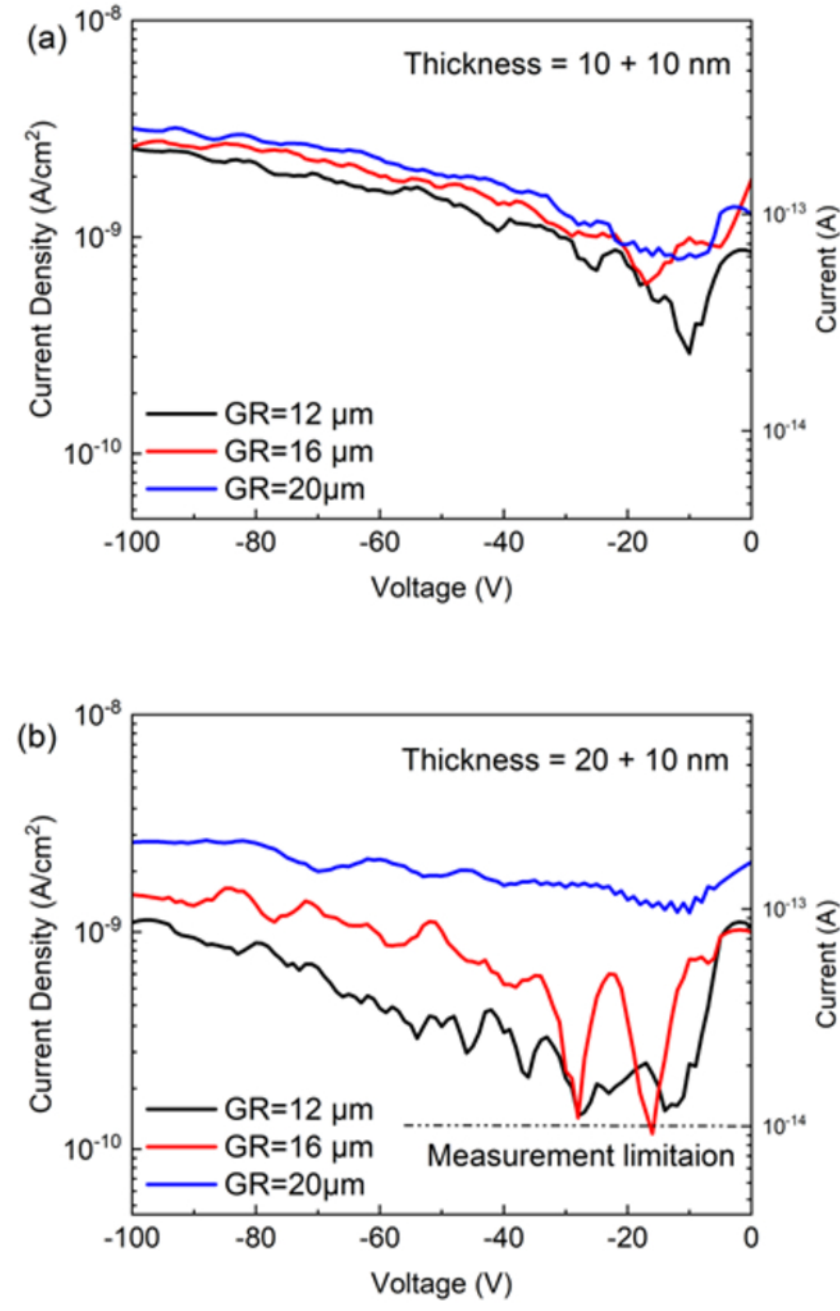
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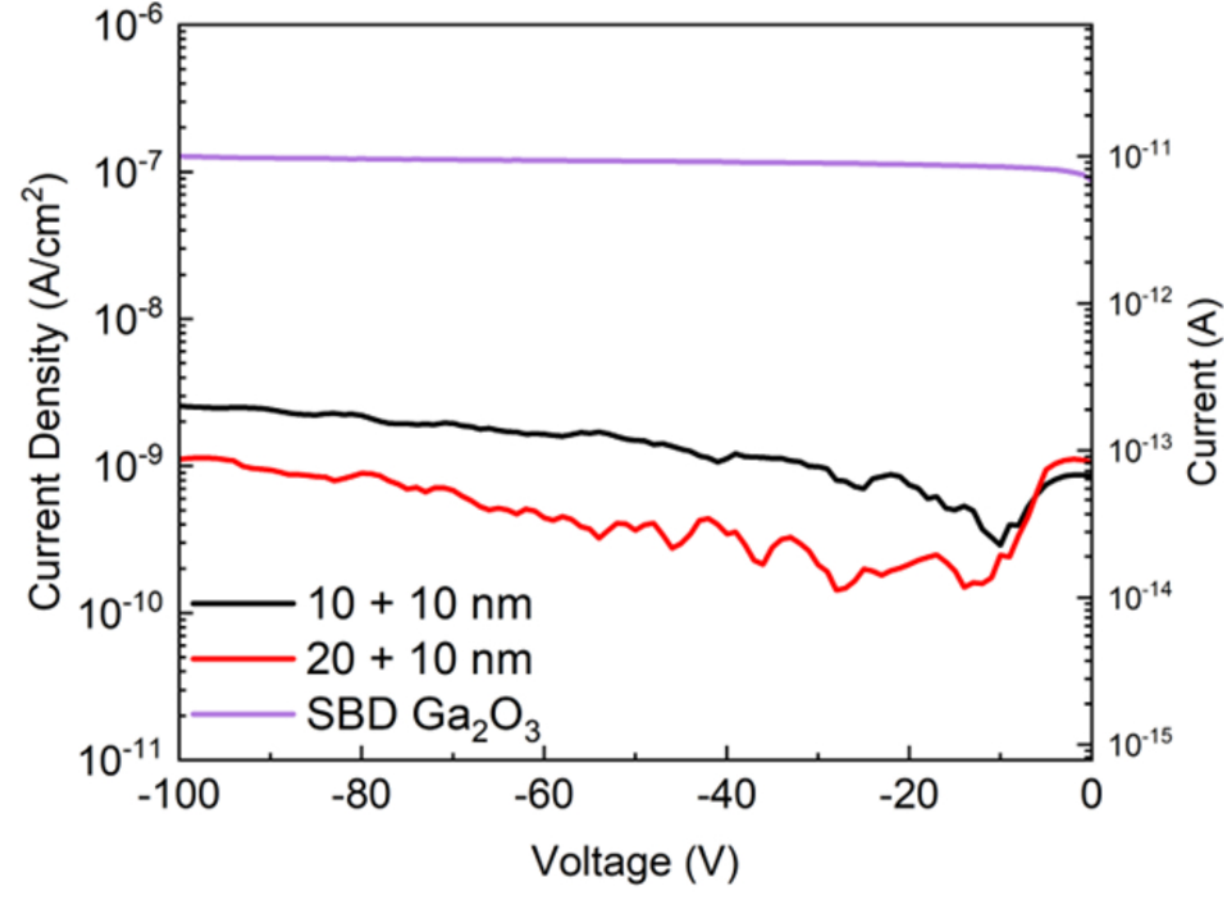


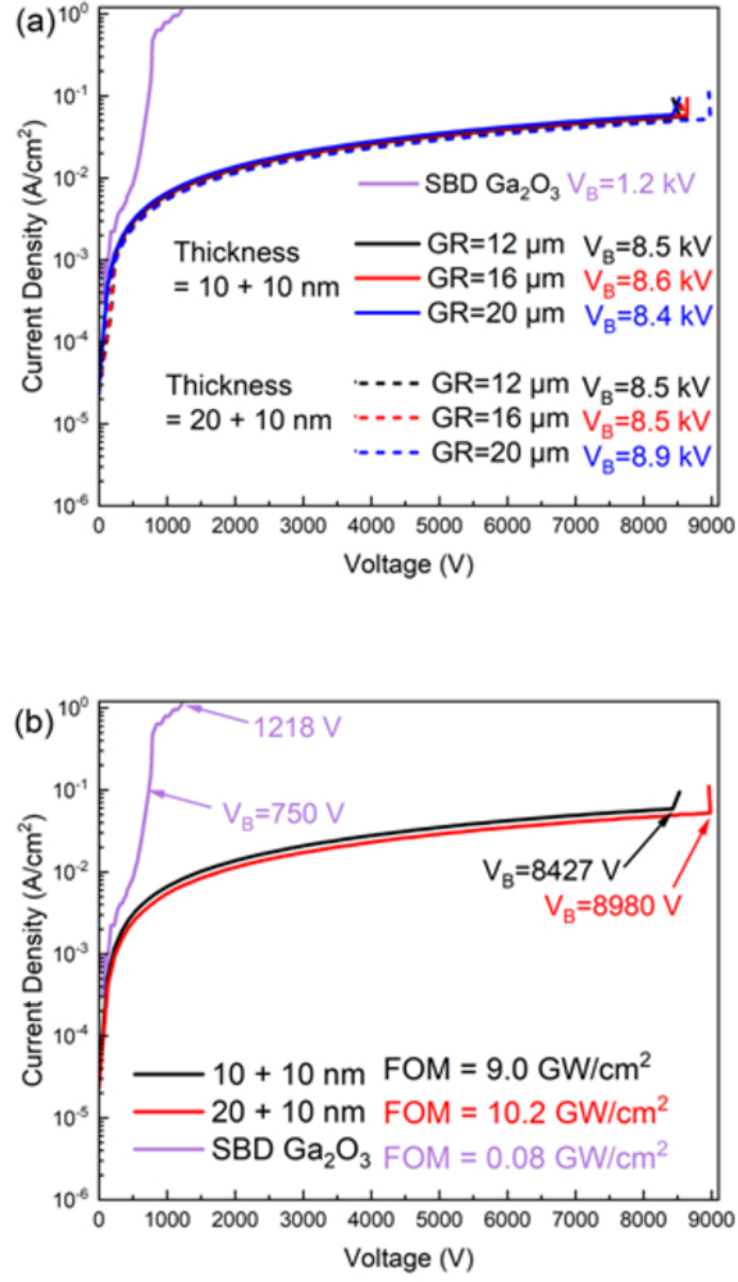


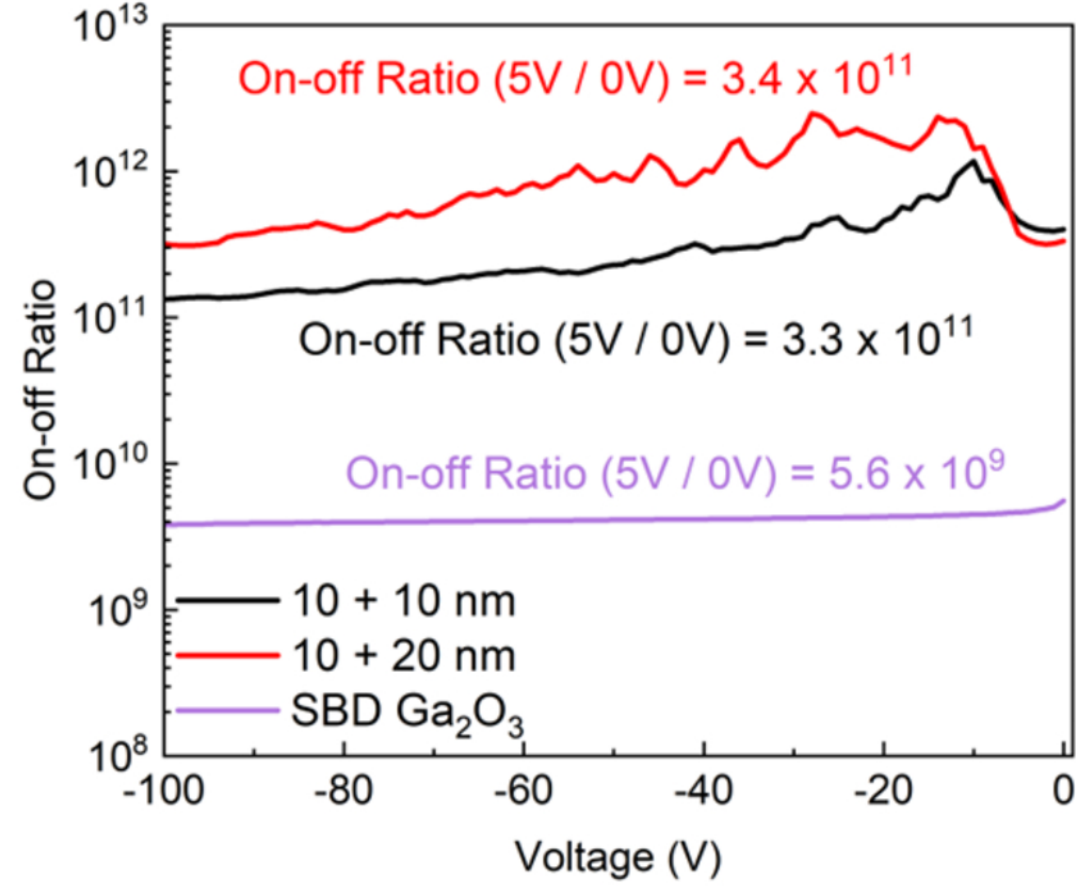


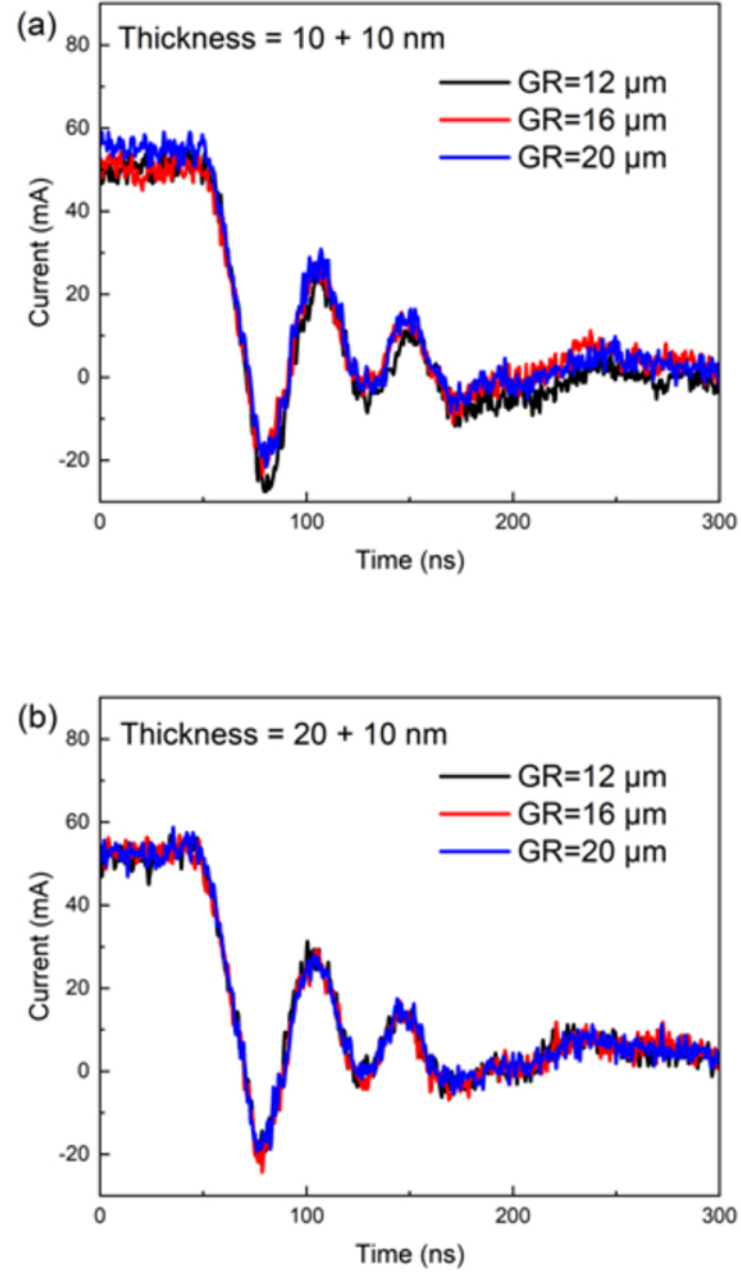












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