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ARTICLE

Superior High Temperature Performance of 8 kV NiO/Ga₂O₃ Vertical Heterojunction Rectifiers

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NiO/β-Ga₂O₃ vertical rectifiers exhibit near-temperature-independent breakdown voltages (V_B) of >8 kV to 600K. For 100 μm diameter devices, the power figure of merit (V_B^2/R_{ON}), where R_{ON} is the on-state resistance, was 9.1 GW.cm⁻² at 300K and 3.9 GW.cm⁻² at 600K. By sharp contrast, Schottky rectifiers fabricated on the same wafers show V_B of ~1100V at 300K, with a negative temperature coefficient of breakdown of 2V/K. The corresponding figures of merit for Schottky rectifiers were 0.22 GW.cm⁻² at 300K and 0.59 MW.cm⁻² at 600K. The on-off ratio remained >10¹⁰ up to 600K for heterojunction rectifiers but was 3 orders of magnitude lower over the entire temperature range for Schottky rectifiers. The power figure of merit is higher by a factor of approximately 6 than the 1-D unipolar limit of SiC. The reverse recovery times were ~26 ± 2 ns for both types of devices and was independent of temperature. We also fabricated large area, 1mm² rectifiers. These exhibited V_B of 4 kV at 300K and 3.6 kV at 600K. The results show the promise of using this transparent oxide heterojunction for high temperature, high voltage applications. [bstract text goes here.](#)

Introduction

The ultra-wide bandgap semiconductors with bandgaps > 3.4 eV include diamond, AlN and Ga₂O₃ and have the potential for significantly higher voltage operation with lower switching losses than commercially available SiC and GaN power devices. The various polytypes of Ga₂O₃ are attracting attention for their potential application in power switching, solar-blind UV detectors and lateral transistors with enhanced two-dimensional electron gases densities^(1-7,8). It is relatively easy to grow bulk crystals of the stable monoclinic β-polymorph from the melt, which enables large-diameter, high-quality substrates for homoepitaxy at potentially low cost⁽²⁾. This is attractive for lower manufacturing costs since the material comprises a significant component of the cost of manufacture.

Ga₂O₃ has a high critical electric field strength, which allows for higher operating voltages and lower switching losses in power electronics⁽¹⁻⁶⁾. Its ultrawide bandgap also makes it promising for high temperatures and radiation environment applications. As a result of these advantages, Ga₂O₃ is being considered for several power electronics applications, including inverters, motor drives, and power supplies. There is particular interest in kV-class vertical rectifiers for use in electric vehicles and their charging infrastructure, as well as power management

systems for improved switching efficiency for next generation power grids and efficiently interfacing renewable energy sources with these grids^(1,4,5). One of the goals is to achieve a high breakdown voltage and low on resistance, which is a benefit for rectifiers because of lower switching losses. A figure of merit for power electronic devices is defined as (V_B^2/R_{ON}) where V_B is the reverse breakdown voltage and R_{ON} is the on-state resistance^(1,3,4). To achieve a high-power figure of merit, a rectifier must have a low drift layer concentration, with high electron mobility, as well as low R_{ON} , and optimized edge termination to prevent current crowding^(1,5-21). The breakdown voltage is larger for thicker drift layers, but this degrades on-resistance. In addition, vertical geometry devices are desirable, because of their higher power conversion efficiency and absolute currents compared to lateral devices^(1,3,4,5). Power rectifiers are also building blocks for many advanced power handling systems.

The lack of a practical p-type doping capability for Ga₂O₃ has led to integration with p-type oxides to form p-n heterojunctions with the n-type Ga₂O₃⁽⁹⁻¹⁶⁾. The most successful of these has been NiO, generally deposited by sputtering. The forward current transport mechanism in such junctions is typically recombination at low biases and trap-assisted tunneling at higher bias^(10, 21-26). Promising rectifier performance has been reported with this approach⁽¹⁴⁻³⁶⁾, including V_B of 8.32 kV, with figure of merit 13.2 GW.cm⁻²⁽¹⁵⁾.

A less studied aspect has been the elevated temperature performance of such devices⁽³⁷⁻⁴²⁾. In this paper we report an investigation of the temperature dependence of the performance of NiO/Ga₂O₃ and also co-fabricated Au/Ni/Ga₂O₃ vertical rectifiers on the same wafers. While the breakdown voltage of the latter fall-off quickly with increasing temperature, the heterojunction rectifiers exhibit nearly temperature-

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independent V_B to 600K. While we focused on small area devices (100 μ m), we also fabricated large area (1 mm²) to examine the scaling properties.

Experimental

We made both vertical geometry Schottky rectifiers and NiO/Ga₂O₃ rectifiers on the same wafers. The bilayer NiO thickness of 10 /10 nm and the length of the NiO extension beyond the top contact (12 μ m) to form field plate-like overhang was held constant⁽¹⁷⁾. The drift region thickness was 10 μ m and these layers were grown by halide vapor phase epitaxy (HVPE) on a (001) Sn-doped (10¹⁹ cm⁻³) β -Ga₂O₃ single crystal substrate. The samples were purchased from Novel Crystal Technology, Japan. A schematic of the two device structures is shown in Figure 1 (top).

Ohmic contacts were made to the back of the doped substrates using a Ti/Au deposited by e-beam evaporation and annealed at 550 C for 180s under N₂. The front surface was cleaned by UV/Ozone exposure for 15 mins to remove contamination⁽¹⁷⁾. The 10/10 nm NiO bilayer was deposited after the Ohmic contacts by rf (13.56 MHz) magnetron sputtering at a working pressure of 3mTorr. The hole concentration in these films was adjusted using the Ar/O₂ ratio. The structure was then annealed at 300°C under O₂. Finally, a top contact of 20/80 nm Ni/Au (100 μ m or 1mm diameter) was deposited onto the NiO layer and also formed the Schottky contact on those devices. The NiO was extended 12 μ m beyond the contact metal to form a field-plate-like overhang. C⁻²-V plots for the drift layer doping showed the carrier concentration was 6.7x10¹⁵ cm⁻³. The device design for NiO thickness and extension were guided by TCAD simulations⁽¹⁷⁾.

The current density-voltage (J-V) characteristics were measured on Tektronix 370-A and 371-B curve tracers and

Agilent 4156C parameter analyser. For the reverse voltages >2kV, a Glassman power supply was employed and all the measurements were performed in Fluorinert atmosphere to avoid breakdown of the air at these high voltages. The reverse breakdown voltage was defined as the bias for a reverse current reaching 0.1 A/cm². The devices did not suffer permanent damage at this condition, with identical I-V characteristics as before measurement, but increasing the voltage a further 50-200 V led to permanent failure through breakdown at the NiO/Ga₂O₃ contact periphery. The on-resistance values were calculated assuming the current spreading length is 10 μ m and a 45° spreading angle. We also subtracted the resistance of the cable, probe and chuck, which was around 10 Ohm.

Results and Discussion

Figure 2 shows the forward J-V characteristics and associated on-state resistances from (a) Schottky (SBD) rectifiers and (b) heterojunction (HJD) rectifiers of 100 μ m diameter as a function of temperature. The on-resistance was obtained from the slope of the forward I-V characteristics. The turn-on voltages decrease with increasing temperature in both types of devices, while R_{ON} increases due to the decreased carrier mobility at higher temperatures⁽⁴⁻⁶⁾. A Richardson plot for the Schottky rectifiers showed a $e\Phi_{b0}$ value of 0.6 eV and a Richardson's

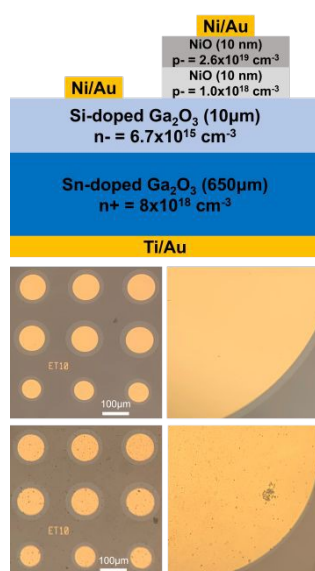


Figure 1. (top) Schematic of structures and images of devices (center) before and (bottom) after operation at 600K.

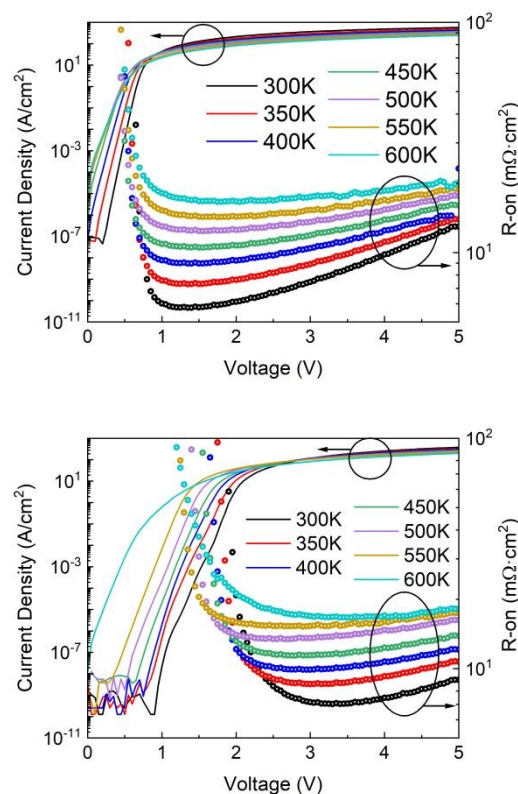


Figure 2. Forward current densities and R_{ON} values for (a) Schottky rectifiers or (b) NiO/Ga₂O₃ as a function of temperature.

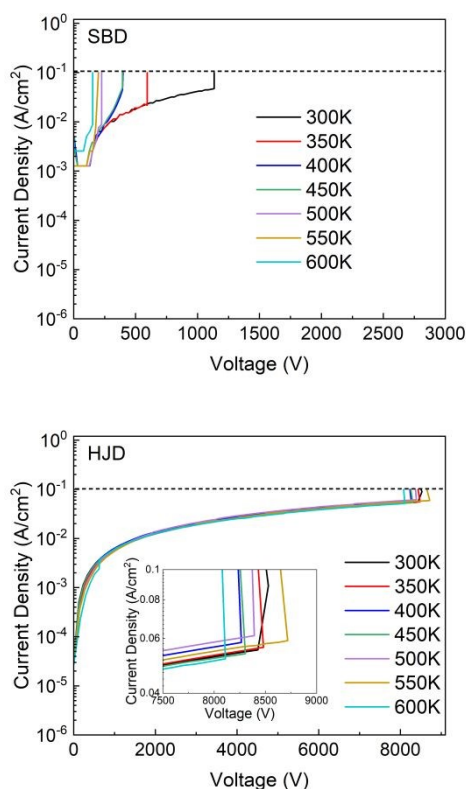


Figure 3. (top). Reverse current characteristics from (a) Schottky rectifier and (bottom) NiO/Ga₂O₃ heterojunction rectifiers as a function of temperature.

constant of $40 \text{ A.cm}^{-2} \cdot \text{K}^{-1}$. The barrier height monotonically decreased from 1.02 eV at 300K to 0.65eV at 600K. The R_{ON} values are slightly higher for the HJD, as expected⁽¹⁴⁻¹⁷⁾. Both types can conduct $>100 \text{ A.cm}^{-2}$ at 4V. Note that the R_{ON} in the heterojunction rectifiers does not continue to decrease at forward voltages beyond $\sim 3\text{V}$. It has also been shown the band alignment remains type II, staggered gap with the magnitude of the conduction and valence band offsets increasing monotonically with annealing temperature⁽¹²⁾.

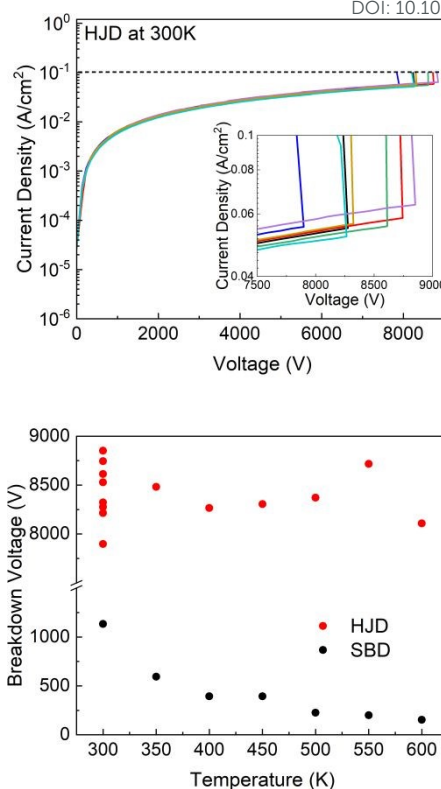


Figure 4. (top) Spread of reverse current characteristics from NiO/Ga₂O₃ heterojunction rectifiers at 300K. (bottom) Temperature dependence of breakdown voltage for Schottky barrier diodes and heterojunction diodes.

Figure 3 shows the reverse J-V characteristics for both types of devices at different temperatures. The Schottky rectifiers show a sharp reduction in the breakdown voltage as temperature increases, as shown in Figure 3 (a). By sharp contrast, the heterojunction rectifiers show very little change in breakdown voltage, as shown in Figure 3 (b). Note also that the Schottky devices have breakdown voltages of only $\sim 1100\text{V}$ at 300K, whereas the NiO/Ga₂O₃ devices remain above 8kV across the temperature range up to 600K. This is a remarkable demonstration of the utility of the NiO in forming a robust p-n junction with the Ga₂O₃ and also in providing effective edge termination to mitigate breakdown at the contact periphery. The devices did not show any visible damage after measurement at 600K, as shown in the center and bottom of Figure 1 for the Schottky and heterojunction rectifiers, respectively.

To give an example of the uniformity of the results, Figure 4 (top) shows the spread of reverse current characteristics from eight different NiO/Ga₂O₃ heterojunction rectifiers at 300K. This was from 7.9-8.7 kV, measured over an area of approximately 1cm^2 . The trends in V_{B} with temperature are shown in Figure 4 (bottom) for the two device types, with the same number of Schottky diodes measured. While the

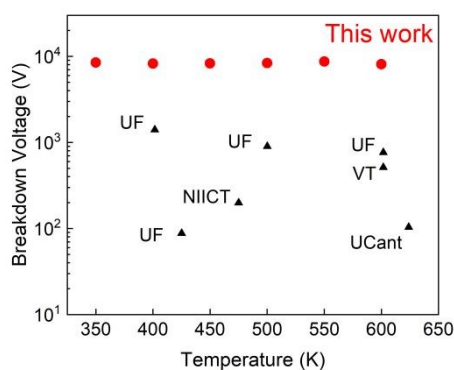


Figure 5. Compilation of maximum operation temperature versus V_B for vertical Ga_2O_3 rectifiers. Previous data comes from Virginia Tech [37], University of Canterbury [39], University of Florida [38] and NIICT [40].

heterojunction devices show no significant change in V_B up to 600K, the Schottky rectifiers show the commonly reported negative temperature coefficient. The temperature dependence of V_B follows an approximate relationship of the form (4, 37-42):

$$V_B = V_{B0} [1 + \beta(T - T_0)]$$

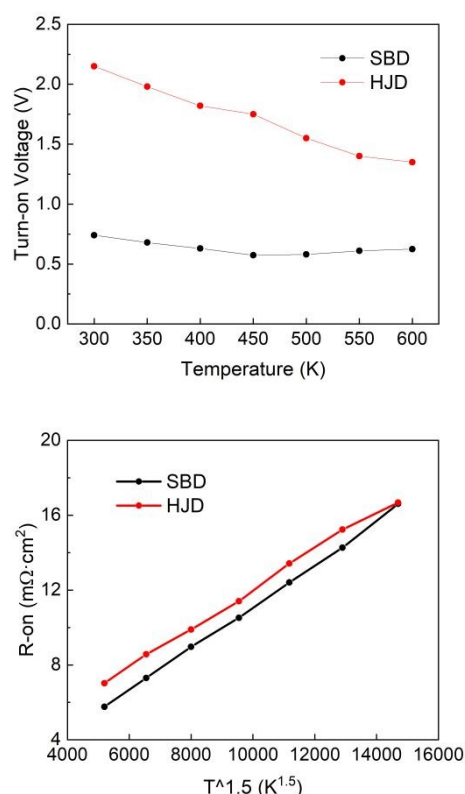


Figure 6. Temperature dependence of on-state resistance and turn-on voltage for Schottky barrier diodes and heterojunction diodes.

where $\beta = -2 \pm 0.6 \text{ V.K}^{-1}$. The negative temperature coefficient precludes impact ionization as the breakdown mechanism in the Schottky rectifiers. This is not unexpected, as new materials technologies generally show breakdowns dominated by defect-assisted processes until the materials growth matures. This was the case for GaN, for example (43). Previous work has shown in vertical geometry Ga_2O_3 rectifiers that impact ionization of deep acceptors is a strong contributor to breakdown (44). A low or negative temperature coefficient of breakdown does have advantages in preventing the rectifiers from being damaged by excessive voltage. A positive temperature coefficient of breakdown can lead to overvoltage conditions and device failure at high temperatures.

Figure 5 shows a compilation of reported maximum operation temperature versus V_B for vertical Ga_2O_3 rectifiers. There is a clear improvement in the present work, which we ascribe to the advances in crystal growth in lowering the drift layer carrier concentration and extended defect density in the starting wafers and also to optimization of the NiO deposition parameters.

The R_{ON} and turn-on voltages from the Schottky and heterojunction rectifiers are shown as a function of temperature in Figure 6. The R_{ON} values are higher for the heterojunctions and increase with temperature, which we ascribe mainly to the degradation in carrier mobility through

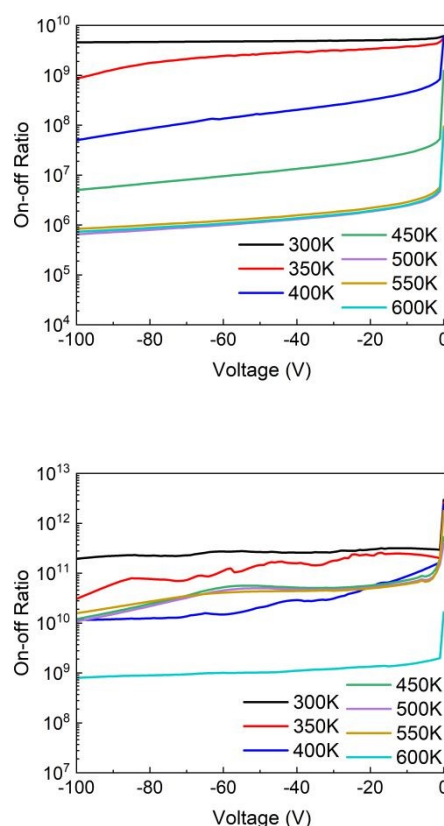


Figure 7. On-off ratio of (top) Schottky rectifiers and (bottom) NiO/ Ga_2O_3 heterojunction rectifiers in which the bias was switched from 5V forward to the voltage shown on

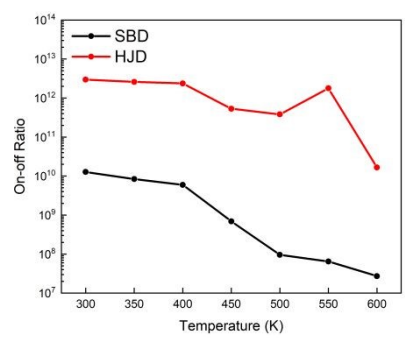


Figure 8. Temperature dependence of on/off ratio for Schottky barrier diodes and heterojunction diodes when switching from 5V forward to 0V.

phonon (lattice) scattering since we could fit the R_{ON} data to a $T^{3/2}$ dependence. Additional evidence could come from extracting mobility from the space charge limited current via the Mott-Gurney Law. The turn-on voltage exhibited a weak dependence on temperature and was lower for the Schottky rectifiers, as expected. The power figure of merits for the heterojunctions were 9.1 GW.cm^{-2} at 300K and 3.9 GW.cm^{-2} at 600K. Note that the theoretical maximum is around 34 MW.cm^{-2}

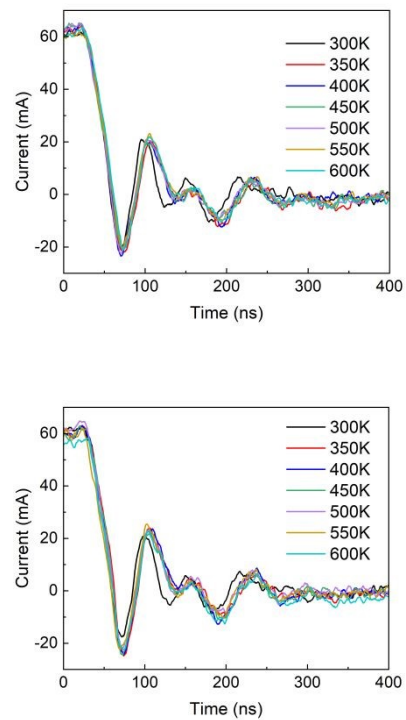


Figure 9. Temperature dependence of switching characteristics of (top) Schottky rectifiers and (bottom) NiO/Ga₂O₃ heterojunction rectifiers in which the devices were switched from 60 mA forward current to zero.

Table 1. Recovery characteristics from Schottky and heterojunction rectifiers.

Temperature (K)	T _{rr} (ns)	I _{rr} (mA)	dI/dT (A/μs)	IF (mA)
Schottky				
300	24	-23	2.7	60
350	28	-26	2.6	60
400	28	-27	2.5	60
450	25	-26	2.3	60
500	27	-25	2.1	60
550	26	-26	2.3	60
600	24	-26	2.2	60
Heterojunction				
300	25	-20	2.4	60
350	25	-27	2.0	60
400	25	-27	2.0	60
450	25	-27	1.9	60
500	23	-26	1.9	60
550	25	-24	1.9	60
600	27	-25	1.9	60

². The corresponding figures of merit for Schottky rectifiers were 0.22 GW.cm^{-2} at 300K and 0.59 MW.cm^{-2} at 600K.

The on-off ratios as a function of temperature when switching from 5V forward bias to the negative voltages shown on the x-axes are shown in Figure 7 for both types of rectifiers. The values are 1-3 orders of magnitude higher for the heterojunctions due to the lower reverse current at a given bias. Even at 600K the on-off ratio is $\sim 10^9$ for the NiO/Ga₂O₃ rectifiers.

Figure 8 shows temperature dependence of on/off ratio for (top) Schottky barrier diodes and (bottom) heterojunction diodes for switching from 5 V forward voltage to 0V. These are essentially the maximum on-off ratios achievable in the devices.

The switching characteristics of the rectifiers are also of paramount interest, since they need fast recovery times and the ability to switch large currents⁽⁴⁵⁻⁶³⁾. Figure 9 shows the temperature dependence of (top) Schottky rectifiers and (bottom) NiO/Ga₂O₃ heterojunction rectifiers of reverse recovery characteristics in which the devices were switched from 60 mA forward current to 0V. The reverse recovery times are $\sim 26 \pm 2 \text{ ns}$ and are tabulated in Table 1. The relative indifference to device structure and temperature demonstrates that charge storage in the p-n junction is not a significant factor compared to the Schottky device. We have not seen significant difference in recovery characteristics between small and large devices.

We also examined the temperature dependence of performance of the large area (1 mm^2) heterojunction rectifiers. Figure 10 (top) shows the forward current characteristics. Note that the absolute forward current is $>3\text{A}$ for all temperatures, with a breakdown voltage of 4kV at room temperature, as shown in Figure 10 (bottom). The reason for the lower

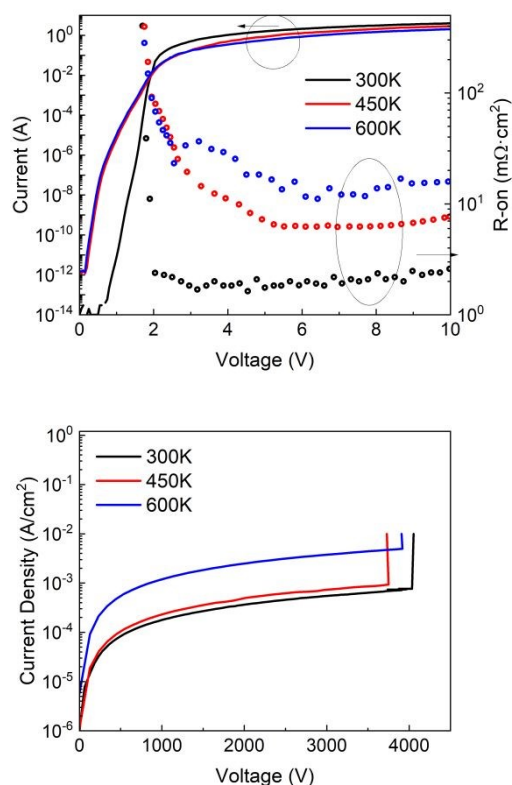


Figure 10. (top) Forward current densities and R_{ON} values and (bottom) reverse current characteristics from 1mm^2 NiO/Ga₂O₃ heterojunction rectifiers as a function of temperature.

breakdown is not clear and could be due to a higher probability of having intrinsic defects or an issue with field crowding. The power figure-of-merit is $6.4\text{ GW}\cdot\text{cm}^{-2}$ at 300K and $0.8\text{ MW}\cdot\text{cm}^{-2}$ at 600K. The on-off ratio remained above 10^8 at 600K, for switching to -100V, as shown in Figure 11.

Conclusions

Since the breakdown, forward I-V and on resistance did not degrade to much at 300°C, the concerns of low thermal conductivity of gallium oxide should be of less concern provided the long-term reliability can be established. The power figure of merits reported here are around 26 % of the theoretical maximum for Ga₂O₃ ⁽¹⁵⁾. It is anticipated that continued reduction in defect density, as well as adding other edge termination technology such as field plates, implanted guard rings, mesa etching as possible methods to improve field uniformity can enhance future performance closer to this maximum. This is because bulk Ga₂O₃ crystals are known to have internal planar defects, i.e., plate-like voids and stacking faults, and it is known that higher dislocation densities lead to higher leakage currents in Ga₂O₃ rectifiers ⁽⁶⁴⁻⁶⁶⁾. This is because the dislocations can act as recombination centers for electrons and holes, leading to an increased probability of carrier

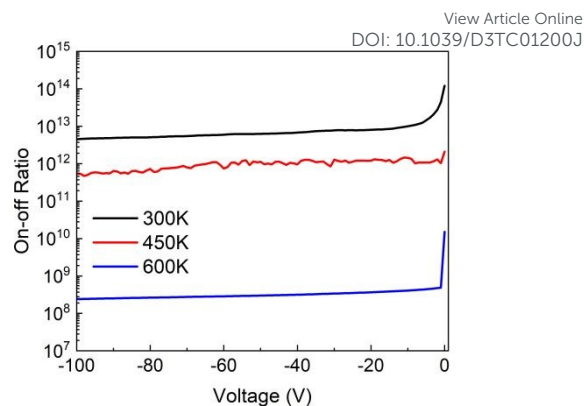


Figure 11. On-off ratio of 1mm^2 NiO/Ga₂O₃ heterojunction rectifiers in which the bias was switched from 10V forward to the voltage shown on the x-axis.

recombination and subsequent leakage current and hence lower breakdown voltage.

The NiO/ Ga₂O₃ heterojunction rectifier is potentially an ideal structure for high-voltage and high-power applications, where it can offer better efficiency and reduced energy losses compared to traditional semiconductors. The wide bandgap of both NiO (~3.9 eV) and β -Ga₂O₃ (4.8eV) also makes power rectifiers from this heterojunction attractive for high-temperature applications. These properties make Ga₂O₃ power rectifiers promising for high-power and high-temperature applications such as electric vehicles, power electronics, and aerospace.

Conflicts of interest

There are no conflicts to declare.

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