

# Relationship between thermal and electrical conductivity curves of soils with a unimodal pore size distribution: Part 1. A unified series-parallel resistor model

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## ABSTRACT

Soil thermal conductivity ( $\lambda$ ) and electrical conductivity ( $\sigma$ ) characterize heat and electricity conduction through soils. Both  $\lambda$  and  $\sigma$  are affected by similar factors, such as soil water content ( $\theta$ ), texture, bulk density ( $\rho_b$ ), temperature, structure, and organic matter content. Little is known about the quantitative relationship between  $\lambda$  and  $\sigma$ , and how soil texture and  $\rho_b$  modify the relationship. In this part one of a two-part series, we examine the correlation between  $\lambda(\theta)$  and  $\sigma(\theta)$  curves and develop a new model for normalized  $\sigma$  curves of soils with a unimodal pore size distribution. We introduce an Ohm's law analogy to describe the  $\lambda$  and  $\sigma$  curves conceptually, based on a cubic cell unit model. A unified series-parallel resistor model considering  $\theta$  and  $\rho_b$  effects is established for both  $\lambda(\theta)$  and  $\sigma(\theta)$  curves by considering heat and electrical conduction pathways (solid, solid-liquid, and liquid pathways) in the hydration, menisci, and continuous liquid ranges. Simultaneous measurements of  $\theta$ ,  $\lambda$  and  $\sigma$  with thermo-TDR sensors on two soils are used to examine the model performance at various values of  $\rho_b$  and  $\theta$ . The modeled and measured  $\lambda(\theta)$  and  $\sigma(\theta)$  curves provide consistent trends, and the normalized  $\lambda$  and  $\sigma$  values vs. degree of saturation confirm the existence of an earlier reported "mirror image" phenomenon between the functions.

## 1. Introduction

Soil thermal conductivity ( $\lambda$ ), which measures the ability of a soil to conduct heat, is a vital parameter in heat transfer investigations (Farouki, 1986; Revil, 2000). Soil electrical conductivity ( $\sigma$ ), which reflects the mobility of electrons in soils, is often used as an indirect indicator of soil physical and chemical properties, such as water content ( $\theta$ ), salinity and clay fraction (Sudduth et al., 2005; Stadler et al., 2015). Both  $\lambda$  and  $\sigma$  have been used to estimate soil physical properties, study surface energy balance and land-atmosphere interactions (Logsdon et al., 2010). Understanding the quantitative relationship between  $\lambda$  and  $\sigma$  is essential for predicting the coupling mechanisms of water, heat, and solute transport in soils.

Soil  $\lambda$  and  $\sigma$  are both affected by common factors such as  $\theta$ , soil bulk density ( $\rho_b$ ), mineral composition, particle size distribution and temperature (Nadler and Frenkel, 1980; Farouki, 1986; Logsdon et al., 2010). Inspired by the similarities between heat transfer and electrical flux in soils, some efforts have been made to reveal the interrelations

between  $\lambda$  and  $\sigma$ . Woodside and Messmer (1961) studied soil heat transfer using a series-parallel resistor model following the theory of electrical flow in two-phase media. Revil (2000) proposed a theoretical  $\lambda$  model for saturated granular sediments, in which the pore topography effect was reflected by using an electrical cementation exponent that could be obtained from  $\sigma$  measurements. Hamamoto et al. (2010) studied  $\lambda$ ,  $\sigma$ , and air/solute diffusivities under variably saturated fluid conditions and examined the analogies between the four parameters following an extended form of Archie's law. They proposed the "water bridge effect" (i.e., thermal conduction through the solid phase is enhanced as water content increases), "water blockage effect" (i.e., air diffusion decreases as water content increases), and "air blockage effect" (i.e., solute diffusion and electrical conduction decrease as air fraction increases) to describe the  $\lambda$ ,  $\sigma$ , and air/solute diffusivities in response to the degree of water saturation ( $S$ ). The analogies among the parameters showed a "mirror image" relationship between  $\lambda$  and  $\sigma$  using an extended form of Archie's second law (Hamamoto et al., 2010).

Some empirical equations have been developed to describe the  $\lambda$ - $\sigma$

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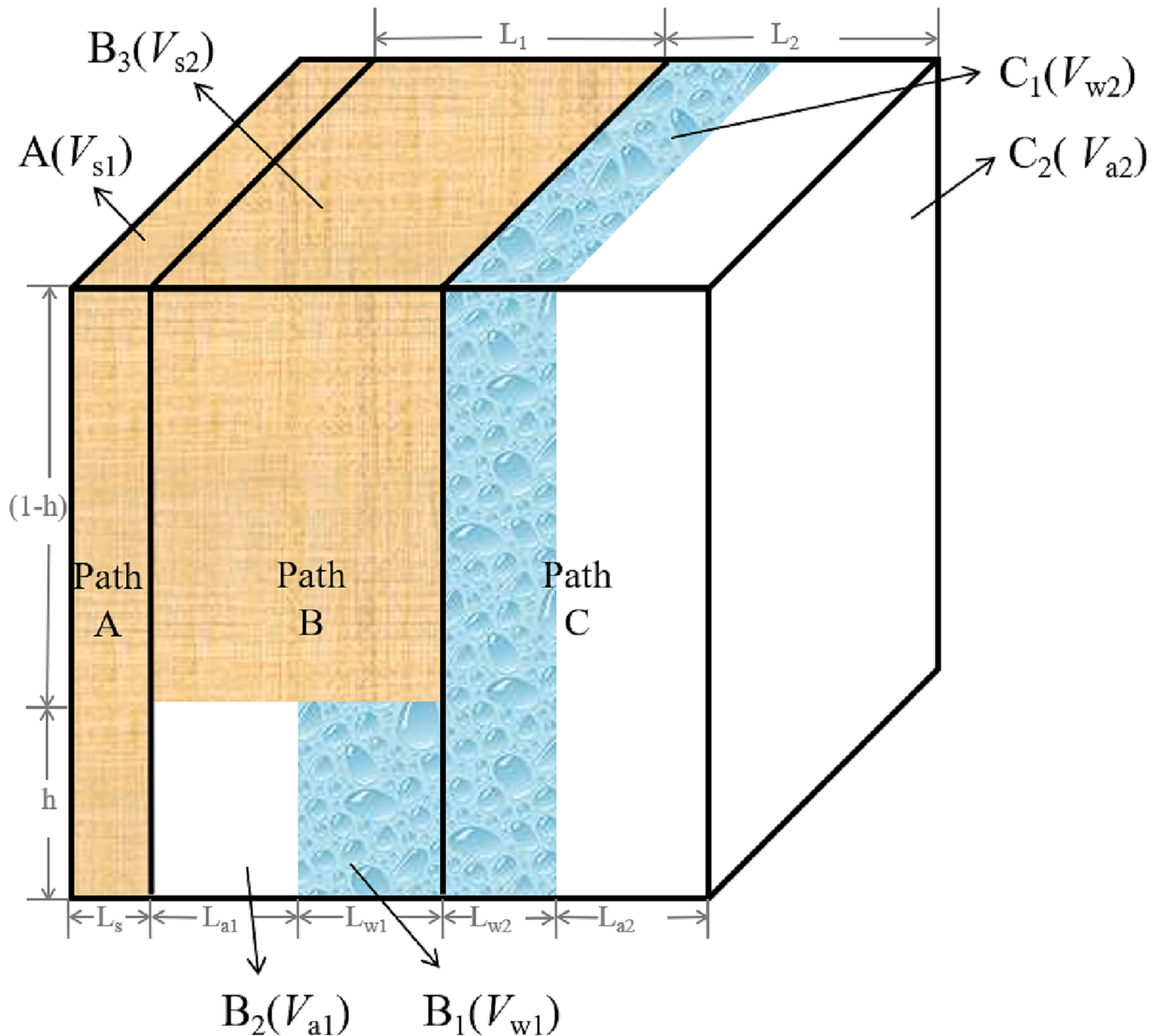
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**Fig. 1.** A diagram of the soil cubic cell showing the unified series-parallel resistor model framework. Paths A, B, and C represent the solid contact path, the coupled path of solids and miniscule pores, and the continuous liquid path, respectively. In Path A,  $L_s$  is the horizontal length and  $V_{s1}$  is the corresponding volume. In Path B, the solid phase ( $B_3$ ) and soil pores are arranged in series, soil liquid ( $B_1$ ) and air ( $B_2$ ) are arranged in parallel in the miniscule pores.  $W$ ,  $L_{a1}$ , and  $L_{w1}$  are the horizontal lengths of solids, air, and liquid, respectively, and  $V_{s2}$ ,  $V_{a1}$  and  $V_{w1}$  are the volumes of the corresponding components. In Path C,  $L_{a2}$  and  $L_{w2}$  are the horizontal lengths of air and liquid, respectively, and  $V_{a2}$  and  $V_{w2}$  are the volumes of the air and liquid paths, respectively.

relationships. Singh et al. (2001) proposed a general relationship between  $\lambda$  and electrical resistivity ( $1/\sigma$ ). Sreedeeep et al. (2005) further improved the model by including soil type and  $S$ . In geotechnical applications, Fragkogiannis et al. (2010) presented an empirical correlation for  $\lambda$  of subsurface soil based on  $1/\sigma$  obtained from electrical tomography and geotechnical data. Wang et al. (2017) built a linear quantitative formula between  $\lambda$  and  $1/\sigma$  by using a statistical analysis of observed  $\lambda$ - $\sigma$  values. These  $\lambda$ - $\sigma$  relationships are empirical and usually require soil-specific calibrations. There is a need for an in-depth investigation of the variations of  $\lambda$  or  $\sigma$  with soil type,  $\theta$ , porosity ( $n$ ), and eventually to establish a universal  $\lambda$ - $\sigma$  relationship (Nouveau et al., 2016).

Several models have been established to estimate  $\sigma$  and  $\lambda$  from easily measurable soil properties and parameters. For soils with low  $\theta$  values and solute concentrations, Rhoades et al. (1989) considered that

electricity was conducted via three pathways acting in parallel in a cubic cell unit, including a solid pathway, a liquid pathway, and a solid-liquid series-coupled pathway. Because heat conduction and electrical conduction in partially saturated soils share similar pathways, Tarnawski and Leong (2012) modified and applied the cubic cell model to estimate  $\lambda$  of various soils. Tokoro et al. (2016) further studied the  $\lambda$ - $\theta$  model with the assumption that heat conduction in soils occurred mainly through three pathways. The advantage of the series-parallel resistor model is that it includes heat and electricity transport pathways through each soil phase, which makes it a useful tool for analyzing the physical mechanisms of heat and electrical conduction processes in soils.

Our objective in this study is to develop a unified model that describes  $\lambda$  and  $\sigma$  in response to  $\theta$  and  $\rho_b$  values of partially saturated soils with a unimodal pore size distribution. In this Part 1 of a two-part series, we describe the unified series-parallel resistor model, which is

developed based on an Ohm's law analogy considering soil conductors (i.e., soil solid, liquid and air) acting in parallel or in series in a cubic cell unit. The model is then used to explore how the mechanisms of  $\lambda$  and  $\sigma$  change with  $\theta$  for soils of various texture and  $\rho_b$ . A laboratory experiment is performed to verify the model results. Finally, a new normalized  $\sigma$  model is derived from the Lu et al. (2007)  $\lambda$  model based on the "mirror image" relationship between  $\lambda$  and  $\sigma$ .

## 2. Development of the unified series-parallel resistor model

The unified series-parallel resistor model is applied to investigate the relationship between  $\lambda$ - $\theta$  and  $\sigma$ - $\theta$  curves. The proposed model framework is built on the concept of a cubic cell unit that has been used by Tarnawski and Leong (2012) to model  $\lambda$  variations with soil texture, with the assumption that (1) the soil has a unimodal particle size distribution; (2) there are similarities between heat conduction and electricity conduction in soils, and (3) both processes can be quantified with the cubic cell unit setting.

The cubic cell unit includes three separate components (Fig. 1), representing the solid phase (yellow section), air phase (blank section) and liquid phase (blue section). In the cubic cell model, heat conduction and electrical conduction occur via three pathways arranged in parallel, i.e., solid-to-solid contacts (Path A), a coupled pathway of miniscule pores (miniscule portion of soil water and air arranged in parallel) and solids (Path B), and a continuous liquid pathway (Path C). In Path A, heat and electrical conductions occur only through the solids or the surface of solid particles (i.e., surface conductance). In Path B, the solid phase ( $B_3$ ) and soil pores are arranged in series in the miniscule pores, and soil liquid ( $B_1$ ) and soil air ( $B_2$ ) are arranged in parallel. The pores included in Path C consist of continuous liquid ( $C_1$ ) and air ( $C_2$ ), which are arranged in parallel.

For simplification of model development, the side length of the cubic cell unit is assumed to be 1 (dimensionless) (Fig. 1). The dimensionless horizontal lengths of Paths A, B and C are denoted as  $L_s$ ,  $L_1$ , and  $L_2$ , respectively. The dimensionless horizontal lengths of soil air and liquid in Path B are indicated by  $L_{a1}$  and  $L_{w1}$ , respectively, and in Path C by  $L_{a2}$  and  $L_{w2}$ , respectively. The terms  $h$  and  $(1-h)$  are the vertical lengths of the soil liquid/air and the vertical length of the solids in Path B, respectively, which are coupled in series (Fig. 1). These side lengths can be varied to reflect the different ratios of solids, liquid, and air in the cubic cell unit. According to Fig. 1, the corresponding volumes of A,  $B_3$ ,  $B_1$ ,  $B_2$ ,  $C_1$ , and  $C_2$  are  $V_{s1}$ ,  $V_{s2}$ ,  $V_{w1}$ ,  $V_{a1}$ ,  $V_{w2}$ , and  $V_{a2}$ , respectively. It should be noted that the volumes defined here simply represent the apparent sizes involved in heat and electrical conductions within the cubic cell unit, not the actual volume of the physical soil.

Following an Ohm's Law analogy, the electrical or thermal resistance ( $R$ ) through the cubic cell unit is,

$$R = \frac{L}{cA} \quad (1)$$

where  $L$  is the electrical and heat conduction length through the conduit,  $c$  represents either apparent  $\lambda$  or  $\sigma$ ,  $A$  is the cross-sectional area of the heat or electricity conduction path.

By applying Eq. [1] to each component within the cubic cell unit, the electrical or thermal resistance of each path in Fig. 1 is derived,

$$R_{V_{s1}} = \frac{1}{c_s L_s} \quad (2)$$

$$R_{V_{s2}} = \frac{1-h}{c_s L_2} \quad (3)$$

$$R_{V_{w1}} = \frac{h}{c_w L_{w1}} \quad (4)$$

$$R_{V_{a1}} = \frac{h}{c_a L_{a1}} \quad (5)$$

$$R_{V_{w2}} = \frac{1}{c_w L_{w2}} \quad (6)$$

$$R_{V_{a2}} = \frac{1}{c_a L_{a2}} \quad (7)$$

where  $c_s$ ,  $c_w$ , and  $c_a$  represent the thermal or electrical conductivities of soil solids, liquid, and air, respectively.

Based on Eqs. [2]-[7], a unified series-parallel resistor model for  $\lambda(\theta)$  and  $\sigma(\theta)$  is proposed. In the model scheme, we differentiate soil water into three water content ranges by considering the interactions of water with soil solids: (1) the hydration range, where water is adsorbed on the surface of solid particles, (2) the menisci range, where water bridges are formed between soil particles (from maximum adsorbed water up to the point where a continuous liquid pathway is formed), and (3) the continuous liquid range, where liquid water replaces air steadily until saturation is achieved. For model development, we assume that as  $\theta$  increases (e.g., during a wetting process), water is adsorbed onto solid particles first, then fills in the relatively smaller pores in Path B, and finally enters the larger pores in Path C. Within each water range, the apparent electrical or thermal resistance ( $R_a$ ) of the cubic cell unit is derived. Therefore, the unified series-parallel resistor model is represented by a piecewise function according to the three water content ranges.

In the hydration range, water is adsorbed on soil particles by hydrogen bonding or intermolecular forces due to Van der Waals forces (Lu and Dong, 2015). The  $\theta$  value ranges between zero and the maximum adsorbed water content ( $\theta_{ads}$ ), and  $L_{a1} = L_1$ ,  $L_{w1} = L_{w2} = 0$ ,  $L_{a2} = L_2$ . In this range, the adsorbed water hardly affects the  $\lambda$  or  $\sigma$  values. Thus, the electrical or thermal resistivity is,

$$\frac{1}{R_a} = \frac{1}{R_{V_{s1}}} + \frac{1}{R_{V_{s2}} + R_{V_{a1}}} + \frac{1}{R_{V_{a2}}}, 0 \leq \theta \leq \theta_{ads} \quad (8)$$

In the menisci range, water fills in the miniscule pores gradually. As  $\theta$  increases,  $L_{a1}$  decreases and  $L_{w1}$  increases gradually while  $L_2$  remains unchanged. At the point of  $L_{a1} = 0$ , the miniscule pores (i.e., the total pore volume of Paths  $B_1$  and  $B_2$ ,  $n_{wm}$ ,  $L_1 h$ ) are filled completely with water. We define this water content as  $\theta_c$ , which equals to the sum of  $\theta_{ads}$  and  $n_{wm}$ . Thus, in the menisci range,  $\theta$  varies from  $\theta_{ads}$  to  $\theta_c$ , and  $R_a$  is represented by,

$$\frac{1}{R_a} = \frac{1}{R_{V_{s1}}} + \frac{1}{R_{V_{s2}} + \frac{1}{\frac{1}{R_{V_{a1}}} + \frac{1}{R_{V_{w1}}}}} + \frac{1}{R_{V_{a2}}}, \theta_{ads} < \theta \leq \theta_c \quad (9)$$

In Path C, as  $\theta$  is further increased, continuous water steadily replaces air in larger pores. During this process,  $L_{a2}$  decreases gradually while  $L_{a1}$  and  $L_{w1}$  remain constant. Thus, the  $R_a$  of the continuous liquid range ( $\theta_c < \theta \leq n$ ) is calculated with,

$$\frac{1}{R_a} = \frac{1}{R_{V_{s1}}} + \frac{1}{R_{V_{s2}} + R_{V_{w1}}} + \frac{1}{R_{V_{a2}}} + \frac{1}{R_{V_{w2}}}, \theta_c < \theta \leq n \quad (10)$$

Equations [8]-[10] form the unified series-parallel resistor model for soil electrical and thermal resistivities. The individual terms of the model are defined in Eqs. [2]-[7].

It is evident that by defining the physical length for each transport path, the unified series-parallel model developed here has extended the Tarnawski and Leong (2012)  $\lambda$  model, and it describes the  $\lambda$  and  $\sigma$  curves simultaneously and quantitatively. This provides a useful way to investigate the relationship between  $\lambda$  and  $\sigma$  and the coupled transport of heat and solutes in soils.

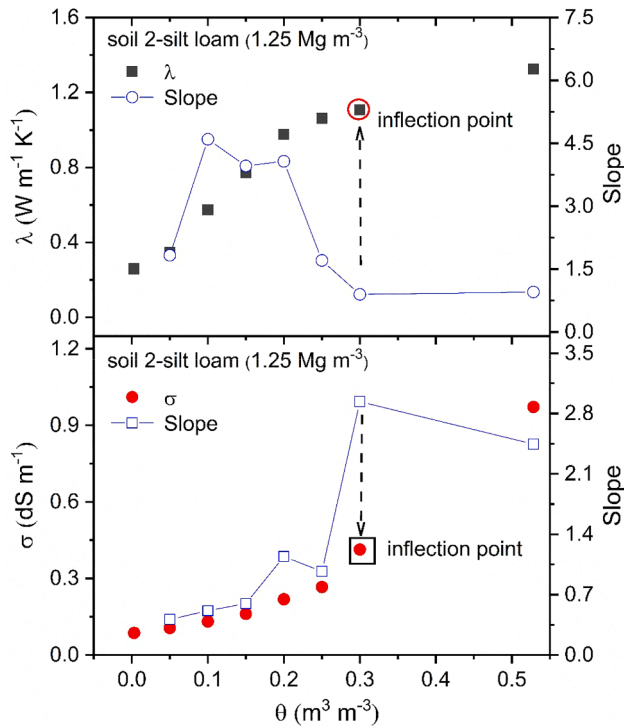


Fig. 2. Determination of the inflection point of thermal conductivity ( $\lambda$ ) and electrical conductivity ( $\sigma$ ) using the slopes of the  $\lambda(\theta)$  or  $\sigma(\theta)$  curves. Here soil 2 (a silt loam) is used as an example.

### 3. Assumptions and parameterization of the unified series-parallel resistor model

In this section, we present the model assumptions and the parameterization procedures for generating  $\lambda$  and  $\sigma$  curves of two hypothetical soils H1 and H2 with different textures.

#### 3.1. Assumptions of the unified series-parallel model

Following the model framework defined in Fig. 1, the volume of each soil component is defined based on the following assumptions:

(1) The soils are classified into fine-texture and coarse-texture groups using a sand fraction ( $f_{sa}$ ) of 0.40 following Lu et al. (2007). Compared to fine-texture soils ( $f_{sa} \leq 0.40$ ), coarse-texture soils ( $f_{sa} > 0.40$ ) have a larger proportion of pores in Path C, and a smaller proportion of miniscule pores in Path B. Miniscule pores are those having water meniscus between soil particles (Clapp and Hornberger, 1978; Campbell, 1985; Tarnawski and Leong, 2012).

(2) During the wetting process, water first fills in relatively small soil pores (Path B) and then enters the larger pores (Path C).

(3) Some cation exchanges occur between the solid and liquid phases over the entire range of water content. According to Waxman and Smits

(1968), at a specified saturation, the effective concentration of exchangeable ions was a linear function of the saturation and the concentration of exchangeable ions. Thus, the  $\sigma_w$  value at a specified saturation ( $\sigma_w'$ ) is expressed as the product of  $S$  and the  $\sigma_w$  at saturation,

$$\sigma_w' = \sigma_w S \quad (11)$$

Thus, parameter  $c_w$  in Eqs. [4] and [6] is replaced by  $\sigma_w'$  when calculating the  $\sigma$  values.

#### 3.2. Parameterization of the unified series-parallel model

Model parameters ( $\theta_{ads}$ ,  $\theta_c$ ,  $c$  values of soil solids, air and liquid, and side lengths) are determined with the purpose of obtaining the cubic cell unit, which represents soils of various textures,  $\theta$  and  $\rho_b$ . For  $\theta_{ads}$ , the values from Lu et al. (2018) are used (Table A1 in Appendix A), i.e., the  $\theta_{ads}$  value is set as  $0.01 \text{ m}^3 \text{ m}^{-3}$  for soil H1 (sand) and  $0.08 \text{ m}^3 \text{ m}^{-3}$  for soil H2 (silt loam).

The parameter  $\theta_c$  represents the inflection point of the  $\lambda(\theta)$  and  $\sigma(\theta)$  curves, which corresponds to the peak slope of  $\lambda$  versus  $\theta$  and the dip in the  $\sigma$  versus  $\theta$ , which equals the sum of  $\theta_{ads}$  and  $n_{wm}$  in our model. As an example, for soil 2, according to the change rates of  $\lambda$  and  $\sigma$  with  $\theta$  (details of  $\lambda$  and  $\sigma$  measurements are described in Part 2), the two curves have approximately the same  $\theta_c$  value of  $0.30 \text{ m}^3 \text{ m}^{-3}$  (Fig. 2).

The apparent thermal and electrical conductivity values (i.e., the  $c$  value in Eq. [1]) of soil solids, air, and liquid are obtained from the literature (Appendix B). For soils H1 and H2, the  $\lambda_s$ ,  $\lambda_w$ , and  $\sigma_s$  values are set as 0.025, 0.56  $\text{W m}^{-1} \text{ K}^{-1}$ , and 0.0001  $\text{dS m}^{-1}$ , respectively (de Vries, 1963; McNeill, 1980; Palacky, 1987; Tarnawski and Leong, 2012); the  $\sigma_s$  and  $\sigma_w$  values are set as 0.025 and 0.40  $\text{dS m}^{-1}$  for soil H1, and 0.08 and 3.00  $\text{dS m}^{-1}$  for soil H2 (Palacky, 1987). By considering the influences of the quartz content (Table 1), the calculated  $\lambda_s$  values are 6.82 and 3.16  $\text{W m}^{-1} \text{ K}^{-1}$  for soils H1 and H2, respectively (Johansen, 1975).

The desired  $\rho_b$  ranges for the two soils are determined by altering the length parameters  $W$ ,  $L_2$ ,  $L_s$  and  $h$  in the cubic cell unit (Fig. 1). For soils H1 and H2, the  $\rho_b$  ranges from 1.15 to 1.60  $\text{Mg m}^{-3}$ , and the side lengths are calculated accordingly using the procedures listed in Appendix C. Finally, the proper values for  $L_1$ ,  $L_2$  and  $h$  are obtained (Fig. C9). Table 1 presents a summary of the specific properties and length parameters of the two hypothetical soils. For soil H1,  $L_s$ ,  $L_1$ ,  $L_2$ , and  $h$  are in the ranges of 0.01–0.01, 0.58–0.65, 0.34–0.41, and 0.07–0.09, respectively, and the corresponding values for soil H2 are in the ranges of 0.03–0.04, 0.58–0.65, 0.31–0.39, and 0.15–0.17, respectively (Table 1).

Fig. 3 outlines the procedures for obtaining soil  $\lambda$  and  $\sigma$  curves by using the unified series-parallel resistor model.

### 4. Results and discussion

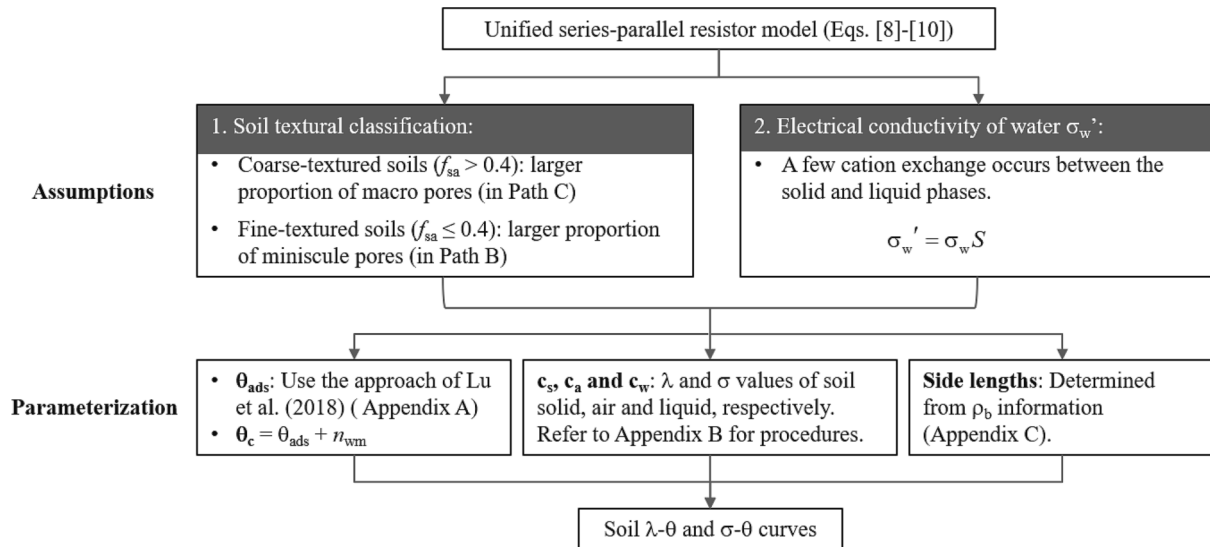
In this section, we present the results from the unified series-parallel resistor model as well as the measurements representing four soils at various  $\theta$  and  $\rho_b$  values. The effects of soil texture,  $\theta$ , and  $\rho_b$  on the  $\lambda$  and  $\sigma$  curves and the analogy between  $\lambda$  and  $\sigma$  are discussed.

Table 1

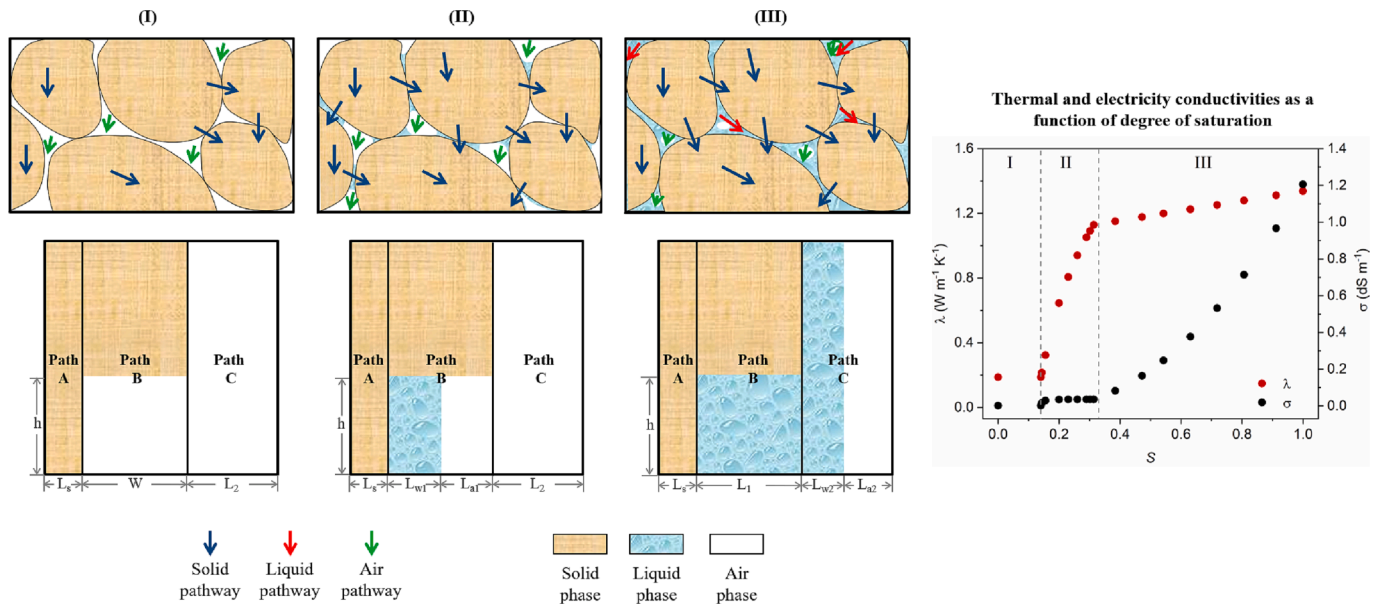
The input parameters of the series-parallel resistor model for two hypothetical soils (H1 and H2) with different textures and bulk densities ( $\rho_b$ ). Parameters  $\lambda_s$ ,  $\lambda_w$ ,  $\sigma_s$ , and  $\sigma_w$  are the thermal and electrical conductivities of solid and liquid,  $h$ ,  $L_s$ ,  $L_1$ ,  $L_2$  are the length parameters of the cubic cell model and  $n$  is the total porosity.

| Soil ID | Texture   | $\lambda_s$                      | $\lambda_w$ | $\sigma_s$         | $\sigma_w$ | $h$           | $L_s$ | $L_1$ | $L_2$ | $n$  | $\rho_b$           |
|---------|-----------|----------------------------------|-------------|--------------------|------------|---------------|-------|-------|-------|------|--------------------|
|         |           | $\text{W m}^{-1} \text{ K}^{-1}$ |             | $\text{dS m}^{-1}$ |            | dimensionless |       |       |       |      | $\text{Mg m}^{-3}$ |
| H1      | sand      | 6.82                             | 0.56        | 0.025              | 0.40       | 0.09          | 0.01  | 0.58  | 0.41  | 0.47 | 1.40               |
|         |           |                                  |             |                    |            | 0.09          | 0.01  | 0.62  | 0.37  | 0.43 | 1.51               |
|         |           |                                  |             |                    |            | 0.07          | 0.01  | 0.65  | 0.34  | 0.40 | 1.60               |
|         |           |                                  |             |                    |            | 0.18          | 0.03  | 0.58  | 0.39  | 0.57 | 1.14               |
| H2      | silt loam | 3.16                             | 0.56        | 0.040              | 3.00       | 0.16          | 0.04  | 0.62  | 0.34  | 0.53 | 1.26               |
|         |           |                                  |             |                    |            | 0.15          | 0.04  | 0.65  | 0.31  | 0.49 | 1.36               |





**Fig. 3.** Procedures to obtain soil thermal conductivity ( $\lambda$ ) and electrical conductivity ( $\sigma$ ) curves in the unified series-parallel resistor model. Parameters  $c_s$ ,  $c_a$  and  $c_w$  are the  $\lambda$  and  $\sigma$  values of soil solids, air, and liquid,  $f_{sa}$  is sand fraction,  $\sigma_w'$  is  $\sigma_w$  at a specific saturation ( $S$ ),  $\rho_b$  is soil bulk density,  $n_{wm}$  is volumetric fraction of miniscule pores, and  $\theta_{ads}$  and  $\theta_c$  are the maximum adsorbed and critical water contents of the  $\lambda$  and  $\sigma$  curves, respectively.



**Fig. 4.** A conceptual diagram showing heat and electrical conduction mechanisms in soils at different water content ranges (left). Three scenarios, i.e., hydration range (I), menisci range (II), and continuous liquid range (III), are considered. On the right, we show the thermal conductivity ( $\lambda$ ) and electrical conductivity ( $\sigma$ ) of soil H2 as a function of degree of water saturation ( $S$ ) estimated with the unified series-parallel resistor model. The length parameters of soil H2 are included in Table 1.

#### 4.1. Variations of $\lambda$ and $\sigma$ with $S$ : the unified series-parallel resistor model

Fig. 4 displays the conceptual mechanisms for heat and electrical conduction in soil. The heat and electrical fluxes are set downwards. The blue, green, and red arrows represent the conduction pathways in solid, air, and liquid phases, respectively. The  $\lambda$  and  $\sigma$  curves of soil H2, which are obtained by using the unified model, are also included.

Heat and electrical conduction mechanisms and the associated  $\lambda$  and  $\sigma$  characteristics differ in the hydration, menisci, and continuous liquid ranges.

In the hydration range ( $0 \leq \theta \leq \theta_{ads}$ ), water molecules are adsorbed onto the soil solid particle surfaces due to intermolecular forces such as van der Waals forces, cations (e.g., sodium and calcium), anions (i.e., oxygen anion or hydroxyls) or hydrogen bond of water (Lu and Dong,

2015). As a result, heat conduction within this range occurs only through the solid pathway (Path A), leading to extremely low  $\lambda$  values that are similar in value to those for dry soils ( $\lambda_{dry}$ ), and in this range the values hardly change with  $\theta$  (Section I in Fig. 4). Meanwhile, little change in  $\sigma$  is observed because electrical current flows mainly through the contacts of solid particles and along the surfaces of the soil solids (surface conductance), which essentially equals to the electrical conductivity of dry soils ( $\sigma_{dry}$ ). In this range, both  $\lambda$  and  $\sigma$  values are related to  $L_s$  that controls the volume fraction of soil solids in Path A.

The transition between the hydration range and the menisci range occurs at the maximum adsorption water content ( $\theta_{ads}$ ) where all of the soil particles are coated with an adsorbed water film (Fig. 4). Additional water, which is reflected by  $h$  and  $L_{w1}$  in the unified series-parallel model, starts to form 'water bridges' between soil particles (Ewing and

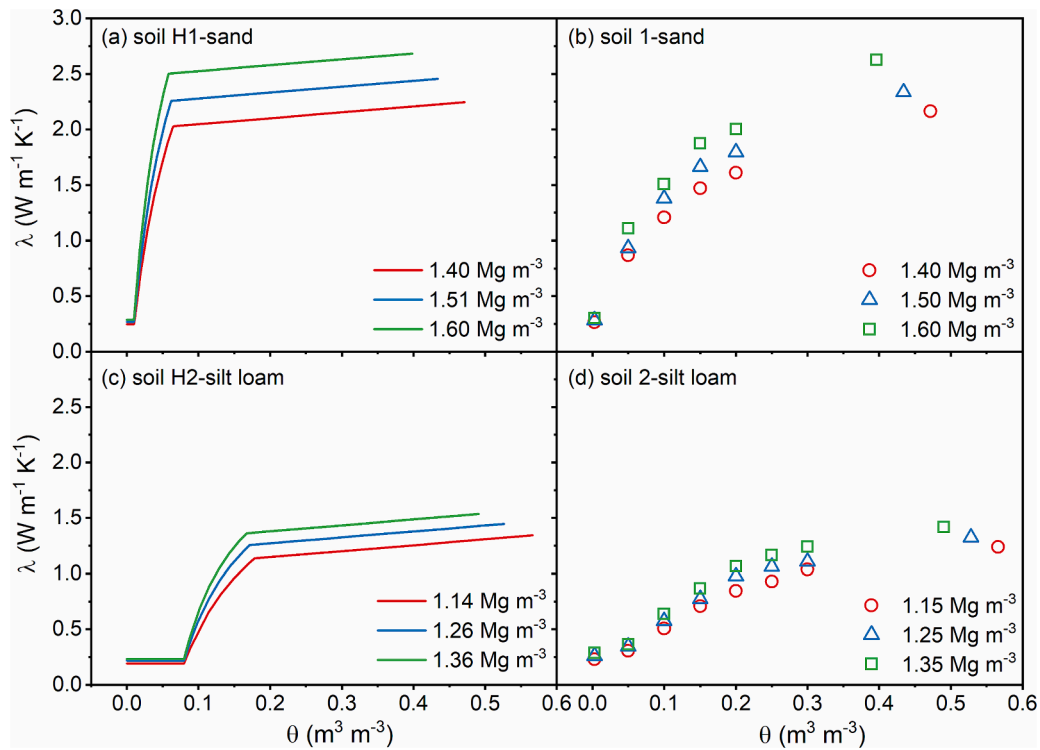


Fig. 5. Soil thermal conductivity ( $\lambda$ ) versus water content ( $\theta$ ) for a set of bulk density values of a sand soil and a silt loam soil. Series-parallel resistor model estimates are shown in (a) and (c), and observed values are presented in (b) and (d). The length parameters of the hypothetical soils are provided in Table 1, and the physical properties of soils 1 and 2 are listed in Table 1 of Part 2 of the series.

Horton, 2007). These water bridges significantly enhance heat conduction efficiency through solid particles (Path B, which dominates over Path A) because heat transfer paths through the bridge-connected particles are increased dramatically with the rapid expansion of particle-to-particle contact area. As a result, a sharp  $\lambda$  increase with  $S$  is observed (Section II in Fig. 4). In contrast, only a slight  $\sigma$  change with  $S$  is observed because electrical conduction is constrained in the solid pathway (Path A) and solid-liquid pathway (Path B), and the soil solids have extremely weak electrical conduction ability (Rhoades et al., 1989). Thus, in the menisci water range ( $\theta_{\text{ads}} < \theta \leq \theta_c$ ), the interaction between water and soil solids enhances heat conduction significantly but has limited improvement on electrical conduction, which leads to a rapid  $\lambda$  increase but a very slow  $\sigma$  change with  $S$  in Section II (Fig. 4).

With a further increase in  $S$  (i.e.,  $\theta > \theta_c$ ), the miniscule pores are filled with water completely (i.e.,  $L_{w1}$  reaches the maximum fraction) and additional water starts to replace air in large pores ( $L_{w2}$  increases and  $L_{a2}$  decreases), which forms the continuous liquid pathways for heat and electrical conduction (Fig. 4). As a result, all the pathways (i.e., the solid, solid-liquid, and liquid pathways) contribute to heat conduction and electron transfer. In this range, however, the responses of  $\lambda$  and  $\sigma$  differ considerably to  $S$  increases with the formation of a continuous liquid pathway (Section III of Fig. 4). Since the change of  $\lambda$  is due mainly to the replacement of air with liquid, and  $\lambda_w$  is only 10–20% of  $\lambda_s$ , a steady and linear  $\lambda$  increase with  $S$  occurs (Lu et al., 2007; Lu et al., 2014), but with a lower rate of change as compared to those in Stage II. In contrast, a sharp  $\sigma$  increase with  $S$  occurs because the value of  $\sigma_w$  is 6–8 times larger than that of  $\sigma_s$  (Table 1).

#### 4.2. The $\lambda$ curves: observed values vs. unified series-parallel model results

Fig. 5 presents the estimated  $\lambda$  values for two hypothetical soils with  $\rho_b$  values ranging from 1.14 to 1.61  $\text{Mg m}^{-3}$ , along with observed values from two actual soils with similar texture and bulk density as the hypothetical soils. The details for the observations are described in Part 2

of the series.

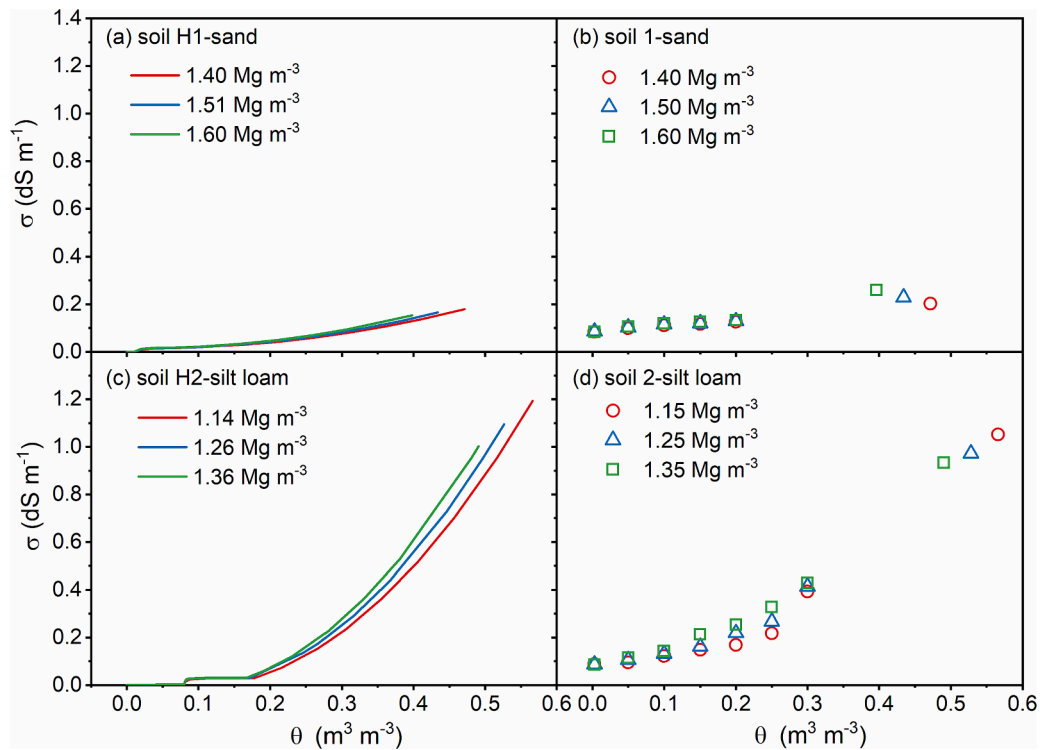
In general, the unified series-parallel resistor model captured the general trend of  $\lambda$  as a function of  $\theta$ . Regardless of soil texture,  $\lambda$  values were relatively small and showed little variation in the hydration range, increased with a large slope in the menisci range, and increased further but with a small slope in the continuous liquid range. The model estimated values at the dry and saturated states were similar to the observed values, and the characteristic water content  $\theta_{\text{ads}}$  in the  $\lambda(\theta)$  curves approximated the observations, indicating that the Johansen (1975) model and Lu et al (2018) model provided reliable  $\lambda_s$  and  $\theta_{\text{ads}}$  values, respectively.

##### 4.2.1. Soil texture effects on $\lambda(\theta)$ curves

The unified series-parallel resistor model depicted well the effects of soil texture on  $\lambda$ . Compared to the silt loam soil results, the sand soil (1) had a smaller amount of hydration water due to the low specific surface area and limited electrical charges, which led to an earlier transition (i.e., a smaller  $\theta_{\text{ads}}$  value) from the hydration range to the menisci range; (2) had a relatively small fraction of fine pores, thus the solid particles were readily connected by water molecules in the menisci water content range, resulting in a sharp  $\lambda$  response to a  $\theta$  increase (Fig. 5a and 5b). Due to its large specific surface area, abundant electrical charges, and a high fraction of fine pores, the silt loam soil had a broader hydration range (i.e., greater  $\theta_{\text{ads}}$  value) and a relatively small  $\lambda$  change rate with  $\theta$  increase in the menisci water range (Fig. 5c and 5d), as compared to that of the sand soil.

##### 4.2.2. $\rho_b$ effects on $\lambda(\theta)$ curves

At a specific water content, a larger  $\rho_b$  value generally results in a greater  $\lambda$  value (Abu-Hamdeh and Reeder, 2000; Lu et al., 2014). Soils with large  $\rho_b$  values have a large soil solid fraction and better contacts among the solid particles, which offer heat conduction pathways through the bulk soil (Logsdon et al., 2010; Sun and Lü, 2019). The series-parallel resistor model results and the observations confirmed



**Fig. 6.** Soil electrical conductivity ( $\sigma$ ) versus water content ( $\theta$ ) at several values of bulk density for a sand soil and a silt loam soil. Presented are series-parallel resistor model estimations (a and c) and observed values (b and d). The length parameters of the hypothetical soils are shown in Table 1 and the physical properties of actual soils 1 and 2 are listed in Table 1 of Part 2 of the series.

**Table 2**

Electrical conductivity values for dry soil ( $\sigma_{dry}$ ) and for saturated soil ( $\sigma_{sat}$ ), and thermal conductivity values for dry soil ( $\lambda_{dry}$ ) and for saturated soil ( $\lambda_{sat}$ ) representing various textures and bulk densities ( $\rho_b$ ).

| Soil ID | Texture   | $\rho_b$           | $\sigma_{dry}$     | $\sigma_{sat}$     | $\lambda_{dry}$                 | $\lambda_{sat}$                 |
|---------|-----------|--------------------|--------------------|--------------------|---------------------------------|---------------------------------|
|         |           | $\text{Mg m}^{-3}$ | $\text{dS m}^{-1}$ | $\text{dS m}^{-1}$ | $\text{W m}^{-1} \text{K}^{-1}$ | $\text{W m}^{-1} \text{K}^{-1}$ |
| 1       | sand      | 1.40               | 0.08               | 0.20               | 0.24                            | 2.16                            |
|         |           | 1.50               | 0.09               | 0.23               | 0.27                            | 2.34                            |
|         |           | 1.60               | 0.08               | 0.26               | 0.29                            | 2.62                            |
| 2       | silt loam | 1.15               | 0.09               | 1.05               | 0.23                            | 1.24                            |
|         |           | 1.25               | 0.08               | 0.97               | 0.26                            | 1.32                            |
|         |           | 1.35               | 0.08               | 0.94               | 0.29                            | 1.42                            |
| H1      | sand      | 1.40               | 0.001              | 0.18               | 0.23                            | 2.27                            |
|         |           | 1.51               | 0.001              | 0.16               | 0.27                            | 2.52                            |
|         |           | 1.60               | 0.001              | 0.15               | 0.30                            | 2.74                            |
| H2      | silt loam | 1.14               | 0.001              | 1.20               | 0.19                            | 1.34                            |
|         |           | 1.26               | 0.002              | 1.05               | 0.22                            | 1.41                            |
|         |           | 1.36               | 0.002              | 0.96               | 0.24                            | 1.51                            |

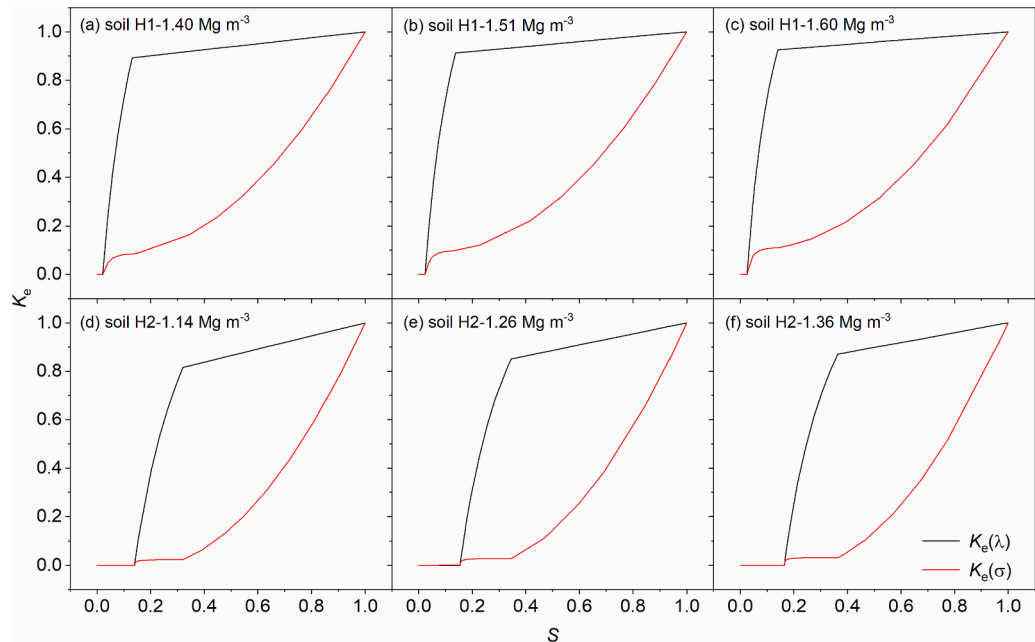
these findings and revealed that the responses of the  $\lambda(\theta)$  curves to  $\rho_b$  varied with soil water content. The effect of  $\rho_b$  occurred mainly in the hydration and menisci water ranges where heat transfer through soil particles is the dominant mode. Taking soil H1 as an example, in the hydration range ( $0 \leq \theta \leq \theta_{ads}$ ), a 6.7% increase in  $\rho_b$  produced a  $\lambda$  increase of  $0.035 \text{ W m}^{-1} \text{K}^{-1}$  (or a relative  $\lambda$  change of 13.5%). In this range,  $\lambda$  values increased with  $\rho_b$  because of greater contact areas (and thus a larger Path A) among the compacted solid particles. The  $\lambda$  increase, however, was small due to a limited number of disconnected heat conduction pathways.

As  $\theta$  increases, the less conductive air phase is displaced by a more conductive liquid phase filling the miniscule pores (path B), which forms continuous solid-liquid pathways. For a particular soil, a larger  $\rho_b$  brings about a greater proportion of miniscule pores in total pore space ( $n_{wm}/n$ ) and a greater proportion of solids, which forms additional conductive solid-liquid pathways and finally produces a greater inflection point

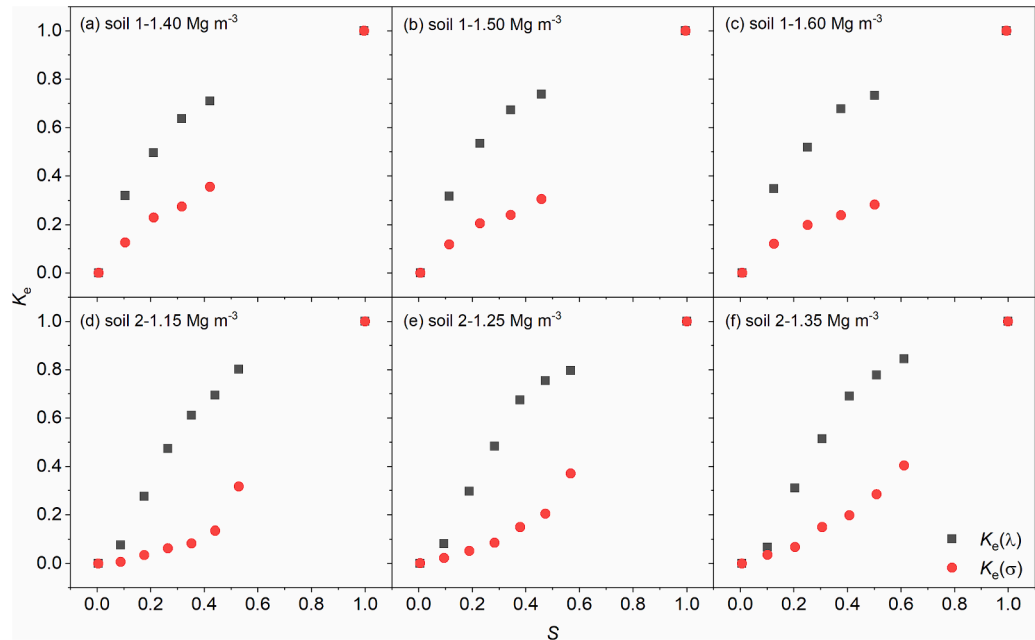
between Section II and Section III. Therefore, in this range,  $\lambda$  increases appear at elevated  $\rho_b$  values. The largest relative  $\lambda$  change occurred at the water content ( $\theta_i$ ) where ‘water bridges’ first formed. From  $\theta_{ads}$  to  $\theta_i$ , a 6.7% increase in the  $\rho_b$  value resulted in a  $\lambda$  increase of  $0.035\text{--}0.25 \text{ W m}^{-1} \text{K}^{-1}$  (or a relative  $\lambda$  change from 13.5% to 17.8%). In the water content range from  $\theta_i$  to  $\theta_c$ , a 6.7% increase in the  $\rho_b$  resulted in a  $\lambda$  increase of  $0.25\text{--}0.26 \text{ W m}^{-1} \text{K}^{-1}$  (or a relative  $\lambda$  change from 17.8% to 11.9%).

When the soil solids are completely connected by ‘water bridges’, the  $\lambda(\theta)$  curve enters the continuous liquid range ( $\theta_c < \theta \leq n$ ), where a 6.7%  $\rho_b$  increase caused a steady  $\lambda$  increase of  $0.26 \text{ W m}^{-1} \text{K}^{-1}$  (with a relative  $\lambda$  change of about 10.2%) throughout the continuous liquid pathway section (Path C).

While the  $\lambda(\theta)$  curves produced by the unified model matched observed values reasonably well, some deviations were observed between the modelled and measured  $\lambda$  data (Fig. 5). First, compared to the observations, the  $\lambda(\theta)$  curves derived from the unified model displayed a sharper inflection point, and the curves had different slopes at some  $\rho_b$  values. This is caused by the fact that the unified model ignores the gradual evolution of pore size and soil structure effects on heat conduction. Second, in the continuous liquid range, the  $\lambda$  increase caused by elevated  $\rho_b$  values in the series-parallel model were insensitive to  $\theta$  changes, while larger  $\lambda$  values occurred at larger  $\theta$  values in the observations. The root of this discrepancy is the model assumption that water first fills relatively small soil pores (Path B) and then enters the larger pores (Path C). Thus, in Path C,  $\lambda$  changes due to elevated  $\rho_b$  values related only to  $L_1$ ,  $L_2$ , and  $h$ , and were not sensitive to  $\theta$  changes (Appendix D). In practice, some macropores might be filled with water prior to the miniscule pores (Tarnawski and Leong, 2012). Future studies are required to further improve the model.



**Fig. 7.** Normalized series–parallel resistor model values ( $K_e$ ) of soil thermal conductivity ( $\lambda$ ) and bulk electrical conductivity ( $\sigma$ ) versus degree of saturation ( $S$ ) for a sand soil (H1) and a silt loam soil (H2) at selected values of bulk density.



**Fig. 8.** Normalized values ( $K_e$ ) of measured soil thermal conductivity ( $\lambda$ ) and bulk electrical conductivity ( $\sigma$ ) versus degree of saturation ( $S$ ) for a sand soil (soil 1) and a silt loam soil (soil 2) at selected values of bulk density.

**Table A3**  
The maximum adsorbed water content ( $\theta_{ads}$ ) for different soil textures. The values are from [Lu et al. \(2018\)](#).

| Soil texture    | $\theta_{ads}$ ( $m^3 m^{-3}$ ) |
|-----------------|---------------------------------|
| Sand            | 0.01                            |
| Sandy loam      | 0.04                            |
| Loam            | 0.03                            |
| Silt loam       | 0.08                            |
| Clay loam       | 0.10                            |
| Silty clay loam | 0.09                            |
| Silty clay      | 0.14                            |

4.3. The  $\sigma$  ( $\theta$ ) curve: observed values vs. unified series–parallel model results

**Fig. 6** presents the estimated  $\sigma(\theta)$  curves of two hypothetical soils with  $\rho_b$  values ranging from 1.14 to 1.61  $Mg m^{-3}$ , along with observations from two actual soils with similar textures and bulk densities as the hypothetical soils. The measurement details for the observations are described in Part 2 of the series.

Regardless of soil texture,  $\sigma$  values were small and did not vary much in the hydration range, increased slowly in the menisci range, and grew rapidly in the continuous liquid water range, indicating that the unified



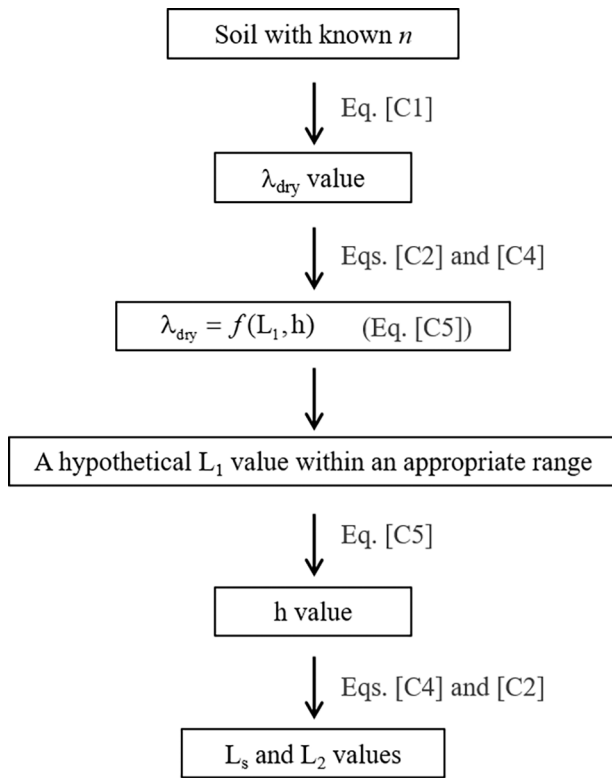


Fig. C1. The detailed procedure used to determine parameters  $L_s$ ,  $h$ ,  $L_1$ , and  $L_2$ .  $n$  is the total porosity, and  $\lambda_{dry}$  is thermal conductivity of dry soil.

series-parallel resistor model captured the overall trend of the  $\sigma$  versus  $\theta$  relationship.

#### 4.3.1. Soil texture effects on $\sigma(\theta)$ curves

Compared to the silt loam soil, the sand soil had less hydration water due to the low specific surface areas and limited electrical charges, which led to an earlier transition (i.e., a lower  $\theta_{ads}$  value) from the hydration range to the menisci range. Due to a large specific surface area, abundant electrical charges, and a high fraction of fine pores, the silt loam soil had a broader hydration range (i.e., greater  $\theta_{ads}$  value) and a relatively large  $\sigma$  versus  $\theta$  slope in the continuous liquid range (Fig. 6c and 6d), as compared to that of the sand soil. Thus, the unified series-parallel resistor model was able to capture soil texture effects on  $\sigma$ .

#### 4.3.2. $\rho_b$ effects on $\sigma(\theta)$ curves

It is accepted that for a given soil, larger  $\rho_b$  results in larger  $\sigma$  values at the same  $\theta$  (Logsdon et al., 2010). The series-parallel resistor model results and the observations not only confirmed these findings, but also revealed that the response of the  $\sigma(\theta)$  curves to  $\rho_b$  varied with soil water content, in a way similar to that of the  $\lambda(\theta)$  curves: (1) At a specific  $\theta$ , greater  $\sigma$  values were observed at elevated  $\rho_b$  values; and (2)  $\sigma$  increases with  $\rho_b$  occurred mainly in the menisci stage where the solid-liquid pathway dominated electrical conduction. Taking soil H1 as an example, in the hydration range ( $0 \leq \theta \leq \theta_{ads}$ ), electrical current flows mainly through the discontinuous solid-to-solid pathway, and the influence of elevated  $\rho_b$  on  $\sigma$  values was negligible because of the extremely low  $\sigma_s$  values.

In the menisci range ( $\theta_{ads} < \theta \leq \theta_c$ ), water molecules in the pores form ‘water bridges’ among soil solids, allowing electricity to be conducted mainly in the solid-to-solid pathway (Path B). Thus, from  $\theta_{ads}$  to  $\theta_i$ , a significant  $\rho_b$  effect on  $\sigma$  was observed: A 6.7%  $\rho_b$  increase caused a  $\sigma$  increase of  $0.080 \times 10^{-3} \text{ dS m}^{-1}$  (or a relative  $\sigma$  change from 0.4% to 28.1%). As  $\theta$  further increased, ‘water bridges’ increased, and  $\sigma$  varied from  $0.80$  to  $2.65 \times 10^{-3} \text{ dS m}^{-1}$  (or a relative  $\sigma$  change from 28.1% to

8.8%) due to the elevated  $\rho_b$ .

In the continuous liquid range ( $\theta_c < \theta \leq n$ ), electrical conduction was greatly enhanced due to the further magnified conduction in the liquid phase (Path C): a 6.7% increase in the  $\rho_b$  values caused a  $\sigma$  increase of  $2.65\text{--}12.90 \times 10^{-3} \text{ dS m}^{-1}$  (or a relative  $\sigma$  change from 8.8% to 8.3%). In this range, the decrease in relative  $\sigma$  change might be attributed to the fact that in higher  $\rho_b$  soils, the ratios of macropores in total pore space ( $1 - n_{wm}/n$ ) are reduced, which leaves fewer continuous liquid pathways in Path C.

As mentioned previously, due to the assumption of a clear-cut differentiation of hydration water and menisci water, the  $\sigma(\theta)$  curves generated with the unified model displayed a sharper transition between the hydration range and the menisci range, while the phenomenon did not occur in the observations (Fig. 6). Further research is required to address this issue.

#### 4.4. Analogy between $\lambda$ and $\sigma$

Prior analysis showed that for a particular soil, both  $\lambda$  and  $\sigma$  increased with increasing  $\theta$  and  $\rho_b$ , but the magnitudes of  $\lambda$  and  $\sigma$  increases varied considerably within various ranges of soil water (Fig. 4). In the hydration water range (section I),  $\lambda$  and  $\sigma$  values were small and hardly changed. In the menisci water range (section II),  $\lambda$  increased rapidly with  $\theta$  while  $\sigma$  increased slowly. In the continuous liquid range (section III), the increase in  $\lambda$  slowed down as compared to that in the menisci water range, while in contrast,  $\sigma$  increased exponentially with increasing  $\theta$  values. These trends of  $\lambda$  and  $\sigma$  increases as a function of  $\theta$  have also been reported by Hamamoto et al. (2010). It is worth noting that a hump appears in the electrical conductivity curve at the transition between the hydration range and the menisci range. This is caused by the fact that in the hydration range, electrical conduction occurs mainly through the solid pathway. As  $\theta$  increases (i.e., the menisci range), however, the solid-liquid pathway contributes significantly to electrical conduction. Thus, the  $\sigma$  values calculated with Eq. [9] increase sharply at the transition point, because the electrical conductivity of liquid is 4–100 times greater than that of the solid.

We applied the normalization approach to quantify the relationship between the  $\lambda(\theta)$  and  $\sigma(\theta)$  curves. The dimensionless  $\lambda$  and  $\sigma$  values are calculated by using Eqs. [12] and [13],

$$K_e(\lambda) = \frac{\lambda - \lambda_{dry}}{\lambda_{sat} - \lambda_{dry}} \quad (12)$$

$$K_e(\sigma) = \frac{\sigma - \sigma_{dry}}{\sigma_{sat} - \sigma_{dry}} \quad (13)$$

where  $K_e(\lambda)$  and  $K_e(\sigma)$  are the normalized thermal conductivity and electrical conductivity;  $\lambda_{dry}$  and  $\lambda_{sat}$  represent the thermal conductivities of dry and saturated soils, respectively;  $\sigma_{dry}$  and  $\sigma_{sat}$  are the bulk electrical conductivities of dry and saturated soils, respectively. We applied Eq. [8] to calculate the  $\lambda$  or  $\sigma$  values of the dry soils, and Eq. [10] to calculate the  $\lambda$  or  $\sigma$  values of the saturated soils.

Table 2 presents the conductivity values of the sand and silt loam soils at dry and saturated conditions. For both soils, the  $\lambda_{dry}$  and  $\sigma_{dry}$  values are limited to a narrow range, while the  $\sigma_{sat}$  values varied significantly between soil textures and among different  $\rho_b$  treatments.

Figs. 7 and 8 show the dynamics of  $K_e(\lambda)$  and  $K_e(\sigma)$  results as a function of  $S$  and  $\rho_b$ . For comparison, the unified series-parallel resistor model results and the observed values are presented. Two distinct features are clear. First,  $K_e(\lambda)$  and  $K_e(\sigma)$  versus  $S$  can be divided into three saturation ranges (a detailed description of the trend is provided in section 4.1). In Section I, both  $K_e(\lambda)$  and  $K_e(\sigma)$  hardly varied due to the limited conduction pathways. As  $S$  increased (Section II), ‘water bridges’ developed, which enhanced the formation of solid-to-solid pathways. As a result, a sharp  $K_e(\lambda)$  increase but only a slight  $K_e(\sigma)$  increase were observed due to the high  $\lambda$  and low  $\sigma$  of soil solids. In Section III,

continuous liquid pathways were formed and the  $K_e(\lambda)$  and  $K_e(\sigma)$  responded differently to increasing  $S$ . A gradual  $K_e(\lambda)$  increase was observed, while  $K_e(\sigma)$  increased exponentially.

Second, for all soil textures and  $\rho_b$  values, the shapes of the  $K_e(\lambda)$ - $S$  and  $K_e(\sigma)$ - $S$  curves were rather symmetrical about the  $y = x$  line. The same phenomenon has been reported as the “mirror image” effect for  $\sigma$  and  $\lambda$  by Revil (2000) and Hamamoto et al. (2010). In Part 2 of this study, we use the “mirror image” analogy to establish a  $\sigma$  model based on the  $\lambda$  model.

It is interesting that the modelled  $K_e(\sigma)$ - $S$  curves of soils H1 and H2 were concave up in Sections II and III but concave down near the transition between Sections I and II (Fig. 7). This phenomenon results from the assumptions and simplifications in model development, which have been explained in section 4.3. In the measurements, however, the above situation occurred only for the sand soil and not for the silt loam soil (Fig. 8). Tuli and Hopmans (2004) reported similar instances. This might be related to the interaction between soil particles and adsorbed water which governs electrical conduction in the dry range. For the sand soil with low clay content, most of the adsorbed water molecules distribute on particle surfaces, which results in higher  $\sigma$  values than occur for the silt loam soil, due to the large number of water bridges linking sand grains. For the silt loam soil, because of its higher clay content, the adsorbed water molecules are allocated on the clay surfaces as well as inside the aggregates, and more water is required to form the same number of bridges as found in the sand soil. Thus, a concave down portion does not appear near the transition between Sections I and II for the silt loam soil.

#### 4.5. Limitations and potential directions

In this study, the soil water status was divided into three water content ranges, and a piecewise function was applied to describe the  $\lambda$  and  $\sigma$  curves, which produced abrupt  $\lambda$  and  $\sigma$  changes at the transitional water contents because the model ignored the gradual evolution of pore size and soil structure effects on heat and electrical conductions. We propose two potential approaches that may produce continuous functions for the unified series-parallel model by addressing the gradual evolution of soil pore size distribution. First, it is essential to develop techniques that can quantify the transitional water between soil pores in the hydration, menisci, and continuous liquid ranges, which will enable a smooth transition between the three water ranges. For example,

probability density functions may better describe variations of  $\lambda$  and  $\sigma$  at the inflection point. Secondly, it may be necessary to introduce the matric potential of soil water into the cubic cell model, which can characterize soil pore size distribution and the status of soil water, and the variations of  $\lambda$  and  $\sigma$  with soil water status.

## 5. Conclusions

In soils with a unimodal pore size distribution, the efficiency of heat and electrical conduction differ significantly in the hydration range, menisci range, and continuous liquid range. In this study, a representative cubic unit cell, that describes the  $\lambda(\theta)$  and  $\sigma(\theta)$  curves using an Ohm's law analogy, was introduced to evaluate the effects of soil texture and  $\rho_b$  on heat and electrical conduction through the solid, solid-liquid, and liquid pathways for various water content ranges. Model results showed that although  $\lambda$  and  $\sigma$  responded differently to soil water content, a “mirror image” phenomenon existed between the normalized thermal conductivity and electrical conductivity (i.e.,  $K_e(\lambda)$  and  $K_e(\sigma)$ ). The model results generally agreed with observed values, indicating that the cubic unit cell model could be applied to quantify soil heat and electrical conduction, which could inform future studies of coupled heat and solute transfer in soils.

## Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

## Data availability

Data will be made available on request.

## Acknowledgements

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## Appendix A

### Table A1

## Appendix B

### Determination of $\lambda$ and $\sigma$ of soil solids, air, and liquid

The  $\lambda$  values of liquid ( $\lambda_w$ ) and air ( $\lambda_a$ ) are 0.56 and 0.025 W m<sup>-1</sup> K<sup>-1</sup> at 20°C, and that of solids ( $\lambda_s$ ) is 2–7.7 W m<sup>-1</sup> K<sup>-1</sup> for soils with various quartz contents (de Vries, 1963; Tarnawski and Leong, 2012). For hypothetical soils H1 and H2, the  $\lambda_s$  values are determined from their mineral compositions, i.e., the contents of quartz and other minerals following (Johansen, 1975),

$$\lambda_s = \lambda_q^q \lambda_o^{1-q} \quad (B1)$$

where  $\lambda_q$  and  $\lambda_o$  are thermal conductivities of quartz (7.7 W m<sup>-1</sup> K<sup>-1</sup>) and other minerals, respectively;  $q$  is the quartz content, which is assumed to be equal to the sand content. In this study,  $\lambda_o$  is taken as 2.0 W m<sup>-1</sup> K<sup>-1</sup> for soils with  $q > 0.2$ , and 3.0 W m<sup>-1</sup> K<sup>-1</sup> for soils with  $q \leq 0.2$  (Johansen, 1975).

Angenheister (1982) and Palacky (1987) found  $\sigma$  values of solids ( $\sigma_s$ ) for sand, loam, and clay to vary in the range of 0.001–0.025, 0.04–0.50, and 0.07–2.0, respectively, and that of air ( $\sigma_a$ ) was 0.0001 dS m<sup>-1</sup> at 20°C. For soils with various clay contents, the  $\sigma$  values of liquid ( $\sigma_w$ ) varied from 0.1 to 100 dS m<sup>-1</sup> (McNeill, 1980; Palacky, 1987). In our study,  $\sigma_w$  values of two hypothetical soils are determined within this range, and following the fact that the presence of clay minerals increases the  $\sigma_w$  because of their electrically ‘active’ surface. Thus, for the hypothetical soils, the  $\lambda_a$ ,  $\lambda_w$ , and  $\sigma_a$  values are set as 0.025 W m<sup>-1</sup> K<sup>-1</sup>, 0.56 W m<sup>-1</sup> K<sup>-1</sup>, and 0.0001 dS m<sup>-1</sup>, respectively. The  $\sigma_s$  and  $\sigma_w$  values are set as 0.025 dS m<sup>-1</sup> and 0.40 dS m<sup>-1</sup> for soil H1, and 0.040 dS m<sup>-1</sup> and 3.00 dS m<sup>-1</sup> for soil H2 by considering clay contents.

## Appendix C

### Determination of side length parameters

According to Lu et al. (2007), the  $\lambda_{dry}$  value can be estimated from soil porosity  $n$ ,

$$\lambda_{dry} = 0.51 - 0.56n \quad (C1)$$

In the unified series-parallel resistor model scheme,  $n$  is expressed as,

$$n = L_1 h + L_2 + \theta_{ads} \quad (C2)$$

By combining Eqs. [8], [C1], and [C2], a relationship among  $L_1$ ,  $L_2$  and  $h$  is obtained,

$$\lambda_{dry} = 0.51 - 0.56(L_1 h + L_2) = L_s \lambda_s + \frac{\lambda_s \lambda_a L_1}{(1-h)\lambda_a + h\lambda_s} + L_2 \lambda_a \quad (C3)$$

From the model,  $L_s$  is expressed as a function of  $L_1$  and  $L_2$ ,

$$L_s = 1 - L_1 - L_2 \quad (C4)$$

Thus, Eq. [C3] is simplified as,

$$\lambda_{dry} = 0.51 - 0.56(L_1 h + L_2) = (1 - L_1 - L_2)\lambda_s + \frac{\lambda_s \lambda_a L_1}{(1-h)\lambda_a + h\lambda_s} + L_2 \lambda_a \quad (C5)$$

Parameters  $h$ ,  $L_1$ ,  $L_s$ , and  $L_2$  are all in the range of 0–1 and can be combined within reasonable bound constraints according to Eq. [C5]. For a specific soil,  $\lambda_{dry}$  is estimated from Eq. [C1] if  $n$  is known. Thus, Eq. [C5] can be expressed as,

$$\lambda_{dry} = (1 - L_1 + L_1 h - n)\lambda_s + \frac{\lambda_s \lambda_a L_1}{(1-h)\lambda_a + h\lambda_s} + (n - L_1 h)\lambda_a \quad (C6)$$

From Eq. [C6], the combination of  $L_1$  and  $h$  within a reasonable range can be derived. Then,  $L_2$  is estimated with Eq. [C2]. The detailed procedure used to determine the parameters is shown in Fig. C9.

Take soil H1 as an example. At a desired  $\rho_b$ , the corresponding  $h$  value is derived from Eq. [C6] and a designated  $L_1$  value, and the values of  $L_2$  and  $L_s$  are then estimated with Eqs. [C2] and [C4], respectively. In this study, we obtain the appropriate combinations of length parameters by considering the various ranges of  $n$  for different soil samples.

## Appendix D

### Change in section III $\lambda$ values caused by an increase in $\rho_b$

In our unified series-parallel resistor model, we assume that water first fills relatively small soil pores (Path B) before entering larger pores (Path C). Thus, the  $\lambda$  value due to the continuous liquid pathways (Path C) contribution in section III can be expressed as,

$$\begin{aligned} \lambda &= \lambda_w L_{w2} + \lambda_a L_{a2} \\ &= \lambda_w L_{w2} + \lambda_a (L_2 - L_{w2}) \\ &= \lambda_w (\theta - \theta_{ads} - L_1 h) + \lambda_a (L_2 - \theta + \theta_{ads} + L_1 h) \end{aligned} \quad (D1)$$

At a specific water content, the  $\lambda$  change ( $\Delta\lambda$ ) due to a change in  $\rho_b$  ( $\rho_{b1}$  and  $\rho_{b2}$ ) is,

$$\Delta\lambda = \lambda_2 - \lambda_1 = (\lambda_a - \lambda_w)(L_{1-2}h_2 - L_{1-1}h_1) + \lambda_a(L_{2-2} - L_{2-1}) \quad (D2)$$

where  $\lambda_1$ ,  $h_1$ ,  $L_{1-1}$ ,  $L_{2-1}$  and  $\lambda_2$ ,  $h_2$ ,  $L_{1-2}$ ,  $L_{2-2}$  are the thermal conductivity,  $h$ ,  $L_1$ ,  $L_2$  of soil at  $\rho_{b1}$  and  $\rho_{b2}$ , respectively.

Thus, it is obvious that an increase in  $\lambda$  caused by an increase in  $\rho_b$  at a specific  $\theta$  is only related to the side length  $L_1$ ,  $L_2$ , and  $h$  from Eq. [D2]. As water content increases, the side lengths of the cubic cell model remain constant at a specific  $\rho_b$ , which results in a constant  $\lambda$  increase occurring due to an elevated  $\rho_b$  in this range.

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