



# Ion-selective electrodes based on laser-induced graphene as an alternative method for nitrite monitoring

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## Abstract

Nitrite is an important food additive for cured meats; however, high nitrite levels pose adverse health effects to humans. Hence, monitoring nitrite concentration is critical to comply with limits imposed by regulatory agencies. Laser-induced graphene (LIG) has proven to be a scalable manufacturing alternative to produce high-performance electrochemical transducers for sensors. Herein, we expand upon initial LIG studies by fabricating hydrophilic and hydrophobic LIG that are subsequently converted into ion-selective sensors to monitor nitrite in food samples with comparable performance to the standard photometric method (Griess method). The hydrophobic LIG resulted in an ion-selective electrode with improved potential stability due partly to a decrease in the water layer between the electrode and the nitrite poly(vinyl) chloride-based ion-selective membrane. These resultant nitrite ion-selective sensors displayed Nernstian response behavior with a sensitivity of  $59.5 \text{ mV dec}^{-1}$ , a detection limit of  $0.3 \pm 0.1 \text{ mg L}^{-1}$  (mean  $\pm$  standard deviation), and a broad linear sensing range from  $10^{-5}$  to  $10^{-1} \text{ M}$ , which was significantly larger than currently published nitrite methods. Nitrite levels were determined directly in food extract samples of sausage, ham, and bacon for 5 min. These sensor metrics are significant as regulatory agencies limit nitrite levels up to  $200 \text{ mg L}^{-1}$  in finished products to reduce the potential formation of nitrosamine (carcinogenic compound). These results demonstrate the versatility of LIG as a platform for ion-selective-LIG sensors and simple, efficient, and scalable electrochemical sensing in general while demonstrating a promising alternative to monitor nitrite levels in food products ensuring regulatory compliance.

**Keywords** Graphene · Solid-contact ion selective electrodes · Potentiometry · Electrochemical Sensors · Food safety · Food additives

## Introduction

Nitrite salts are one of the most important additives applied in the curing process of meat products [1–3]. These salts not only improve the color and flavor of cured meats but also play a major role as inhibitors of microbial growth, in particular, *Clostridium botulinum* [4–7]. Nonetheless, the use of nitrite salts as a preservative and curing agent has raised concerns about human health as nitrite reacts with

hemoglobin to form methemoglobin, which reduces the capacity of blood to carry oxygen, in addition to reacting with secondary amines and amides to form the potentially carcinogenic compounds, N-nitrosamines [8, 9]. Thus, limitations to nitrite levels in food products and drinking water have been implemented, with regulations varying from country to country, as studies began to show that low contents of nitrite salts do not promote relevant levels of N-nitrosamines formation [10–12]. For instance, in the USA, sodium nitrite has a maximum limit that varies with cured meat type from 120 to 200 ppm, according to the USDA, and as low as 1 ppm in drinking water, according to the EPA [13, 14]. Given the importance of quantifying nitrite, there is a need for reliable and rapid methods to monitor its levels in food products; ideally, methods that do not require complex or costly manufacturing processes and are easy to use, with minimal sample preparation.

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The range of analytical methods for nitrite monitoring has been comprehensively reviewed by other groups [15–17] with electrochemical sensors providing rapid, sensitive, and portable alternatives to other analytical methodologies, including spectrophotometric [18], chromatographic [19–21], capillary electrophoresis [22], spectrofluorimetric [23–25], colorimetric [26–29], and electrochemiluminescent [30] techniques. The current standard Griess method (AOAC official method 973.31), a colorimetric method, requires trained personnel and is time-limited since the solutions expire 8 h after preparation, and time-consuming with sample preparation and dilutions required to accommodate its linear range [31].

Carbon nanomaterials such as graphene are being explored in various electrochemical applications due to their large surface area, high electrical conductivity, mechanical resistance, and thermal conductivity [32–34]. In particular, 3D-carbon nanomaterials, such as graphene sponge, carbon nanofibers, micro/nanostructure printed graphene, and laser-induced graphene, build upon these material properties by providing an electrode with much higher surface area for increased analyte-to-electrode interaction and biorecognition agent loading, and consequently higher biosensor sensitivity [35]. There are many methods for fabrication of 3D-graphene structures, including electrochemical deposition [36], freeze-drying [37], and hydrothermal synthesis [38]; however, issues with integrating as-fabricated 3D graphene into electrochemical sensors reduce their high-throughput and scalable fabrication. To simplify the 3D-graphene sensor fabrication, various printing techniques, including inkjet [39, 40], screen [41], and 3D printing [42, 43], have been explored. However, post-print annealing techniques such as high-temperature [44], photonic [45], and rapid-pulse laser annealing [39] are required to improve electrical conductivity (similar to printed metals, i.e.,  $< 1 \text{ k } \Omega$ ) and 3D nano/micro structuring.

Another promising approach for 3D-graphene-based sensors is to use a laser treatment that combines direct-write printing and post-print annealing to fabricate highly porous, 3D-graphene-based structures. In 1991, Schumann et al. demonstrated that a UV laser treatment to polymers such as polyimide and polybenzimidazole converted them into conductive materials [46]. The Tour group at Rice University in 2014 used a  $\text{CO}_2$  laser to convert polyimide [47] and other materials [48] into a 3D porous graphene structure, known as laser-induced graphene (LIG). Such LIG material has disordered graphitic structures that expose edge sites, promoting efficient electron transfer of electroactive species [49, 50]. Additionally, LIG surface chemical and physical properties such as porosity, thickness, electrical conductivity, and surface hydrophobicity can be tuned [51]. Recent studies in LIG formation and surface properties, including ours [52, 53], have demonstrated that controlling laser

power, focus, and the number of lasing steps can create LIG with super-hydrophilic or super-hydrophobic surfaces, even in the open ambient in some cases, improving conductivity and electrochemical performance for sensing applications [51, 54–56]. Understanding these properties allows for the reliable fabrication of scalable electrodes.

Potentiometric ion-selective electrodes have been applied for sensitive and selective ion monitoring [57, 58] in many applications that include in-field water environment analysis (heavy metals, perchlorate, calcium, and iodide) [59–64] to in vivo biomedical applications (potassium, calcium, nitric oxide, lithium) [65–69]. Traditional liquid-junction ISEs have an inner liquid (electrolyte) that requires maintenance due to liquid leaching. In contrast, solid-contact ion-selective electrodes (SC-ISEs) remove this inner liquid allowing the ion-selective membrane to make direct contact with the transducing layer. To replace the liquid-junction, SC-ISEs must exhibit minimal potential drift between the transducer and ion-selective membrane [70, 71]. LIG-based electrodes have the potential to fulfill these requirements and to be a promising solid-contact transducer for the fabrication of SC-ISEs, as explored in recent studies regarding fertilizer monitoring in soil ( $\text{NO}_3^-$  and  $\text{NH}_4^+$ ) [72], evaluating human hydration levels and pH in urine ( $\text{K}^+$  and  $\text{NH}_4^+$ ) [73, 74], as well as human sweat monitoring [75, 76], and surface water quality monitoring ( $\text{NO}_3^-$ ) [52]. Despite their advantages, LIG-ISE for nitrite sensing has not been explored. Most electrochemical detection of nitrite is based on electrochemical oxidation or reduction. However, problems with electrode-passivation and fouling effects can occur, reducing the sensitivity of the method, which has been circumvented with the use of power ultrasound to clean the electrode [77], nevertheless, affecting portability and in-field applications. Additionally, most electrochemical sensors for nitrite require multiple and laborious steps to fabricate the electrodes, with detection ranges that are not within the regulated levels for food analysis (upper limit of 200 ppm) [78]. The detection ranges are often in the nanomolar range, except for a few cases, requiring several dilutions and sample preparation steps, and are mostly limited to proof-of-concept demonstration in water samples [78].

In the present work, we successfully developed a nitrite-selective potentiometric sensor based on LIG to measure nitrite levels in cured meats. For this purpose, we systematically fabricated hydrophilic and hydrophobic LIG-electrodes using a  $\text{CO}_2$  laser and evaluated the electrochemical and material properties. To characterize the material changes, we evaluated the resulting LIG surfaces for their morphology (SEM), surface composition and chemical structure (XPS and Raman), and static contact angle, providing a correlation between the LIG platform and the resultant electrochemical properties. We showed that the double-lasing process reduces the surface oxygen

content, increases the contact angle, and the  $sp^2$  carbon content, exhibiting a better performance as a material for ion-sensing applications. The resulting LIG-ISE sensor is capable of monitoring nitrite in cured meats, with results comparable to the standard method (Griess method) and within the range imposed by the USDA regulations [13].

## Experimental section

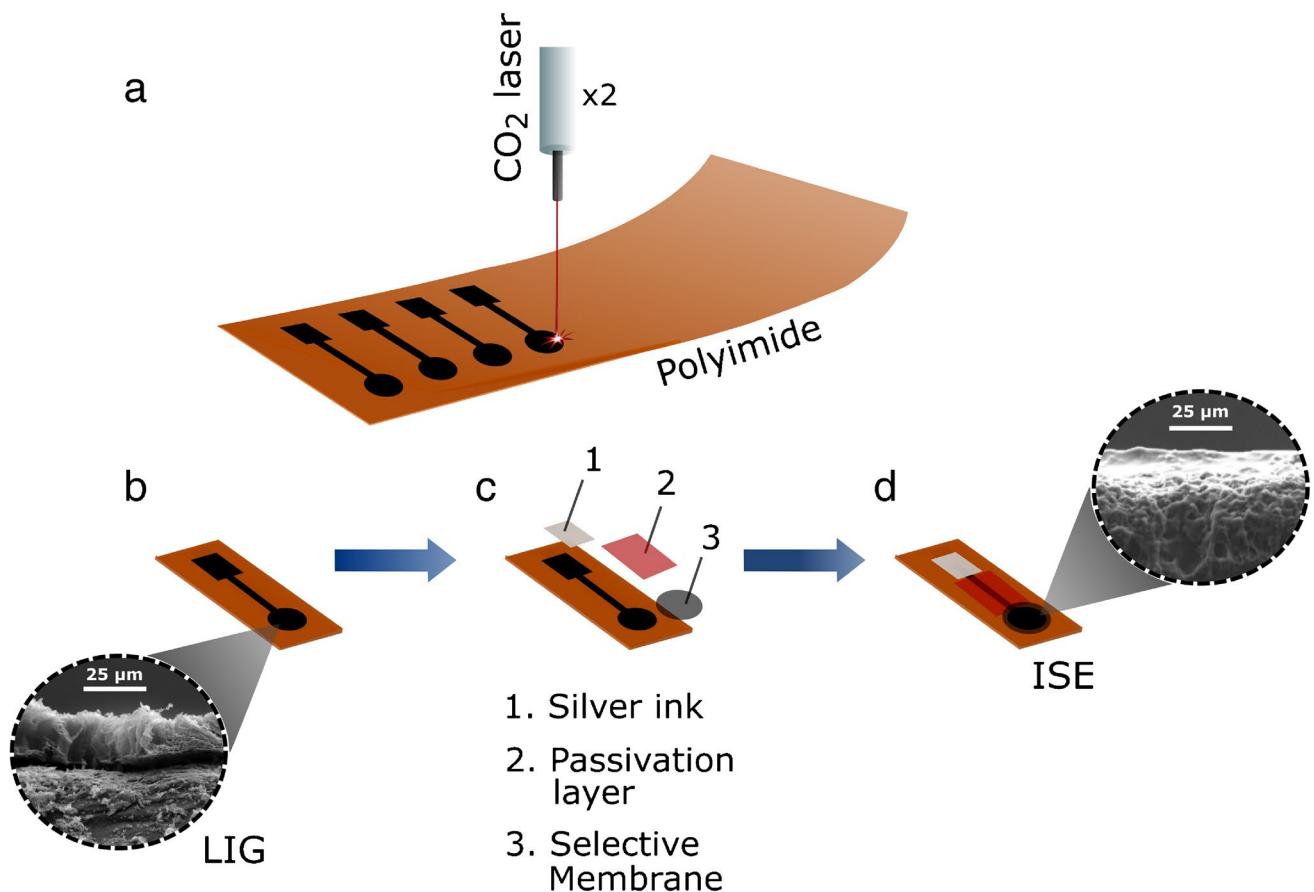
### Materials

Nitrite ionophore VI, tetrahydrofuran (THF), high-molecular-weight polyvinyl(chloride) (PVC), 2-nitrophenyl octyl ether (2-NPOE), sodium nitrite, sodium nitrate, potassium hexacyanoferrate (II) trihydrate, potassium ferricyanide, and the Griess reagent kit for nitrite determination (G-7921) were purchased from Millipore Sigma (Saint Louis, MO, USA). Commercial polyimide (PI) was purchased from McMaster-Carr (Elmhurst, IL, USA), and silver-chloride epoxy ink (Cl-1001) from Engineering

Materials Systems (Delaware, OH, USA). Sodium chloride, potassium chloride, potassium sulfate, and ELISA microplates were obtained from Thermo Fisher Scientific (Waltham, MA, USA). Sausage, ham, and bacon were purchased at a local grocery store. All chemicals were analytical grade, and solutions were prepared using deionized (DI) water with a resistivity of approximately 18.2  $M\Omega \text{ cm}$ .

### Fabrication of LIG-electrodes

Hydrophilic and hydrophobic electrodes were fabricated using a 75-W M2 Epilog CO<sub>2</sub> laser, wavelength 10.6 mm, (Epilog Laser, CO, USA), and a polyimide film, thickness  $\sim 0.127$  mm, under ambient conditions, as previously reported [52]. Hydrophilic LIG-electrodes (1X-LIG) were fabricated using a single-lasing process. Meanwhile, hydrophobic LIG-electrodes (2X-LIG) were fabricated using a successive double-lasing process. The electrodes presented a circular working area (5 mm in diameter), shown in Fig. 1, and a squared contact pad (9 mm<sup>2</sup>) at the other end protected with conductive silver paste. The portion between the two



**Fig. 1** Fabrication steps for a LIG-based ion-selective electrode (ISE). **a** Laser-induction process onto a polyimide film. **b** Cross-sectional SEM image of the working electrode area. **c** Application of the

three main components that make up the ISE. **d** Cross-sectional SEM image of the working area covered with the ion-selective membrane

ends was isolated by applying a passivation layer of fast-drying nitrocellulose-based lacquer.

The nitrite-selective membrane was prepared by dissolving 6.4 wt.% nitrite ionophore VI, the main compound of the membrane used to promote the ionic exchange, 24.7 wt.% PVC, the polymeric substrate, 68.9 wt.% 2-NPOE, the plasticizer that helps solubilize the ionophore and is inert to ion exchange, in 1 mL of THF, the solvent that allows the mixing of the other components, which will be completely evaporated. The mixture of chemicals was stirred using a vortex until the compounds were completely dissolved; then, 10  $\mu$ L of the fresh membrane was drop-casted onto the working area of the LIG-electrodes. After overnight drying, the ion-selective electrodes (ISEs) were conditioned in 1 mM NaNO<sub>2</sub> for 24 h before being tested, as a crucial step for the selective membrane to reach an optimum target-ion concentration and ensure that the measured potential would be stable [79, 80].

## Surface characterization

Bare electrodes were characterized considering the two lasing processes, which provided hydrophilic and hydrophobic graphene-based surfaces. Sheet resistances of both electrodes were measured with a Hall measurement system (MMR H5000, MMR Technologies, San Jose, CA, USA) using the Van der Pauw method with a 1  $\times$  1 cm sample and electrical contact at the four corners. The static contact angle measurements were performed using a ramé-hart model 90 goniometer (ramé-hart instrument co., Succasunna, NJ, USA), applying a 3- $\mu$ L droplet of pure water onto the surface of the electrodes. Angle measurements were performed using the software DROPIimage Pro (ramé-hart instrument co., Succasunna, NJ, USA).

Raman spectra were obtained using a DXR Raman Microscope (Thermo Fisher, Waltham, MA, USA), with acquisitions of 32 scans under an exposure time of 7.5 s and a 2 cm<sup>-1</sup> resolution. A 780-nm laser operating at 20 mW with a 10 $\times$  objective was used. The results were analyzed with OMNIC™ 9.7 software (Thermo Fisher, Waltham, MA, USA).

The surface chemistry of the bare LIG-electrodes was analyzed through X-ray photoelectron spectroscopy (XPS), performed with a Kratos Amicus/ESCA 3400 (Kratos Analytical, Manchester, UK). Unmonochromated Mg K<sub>α</sub> X-rays were irradiated on the samples with 240 W, and the energy of photoelectrons vertically emitted were analyzed using a DuPont type analyzer. The pass energy was set at 150 eV, and the raw data were processed using CasaXPS (Casa Software Ltd., Teignmouth, UK).

Top-view and cross-sectioned images from scanning electron microscopy (SEM) were obtained using a FEI Quanta 250 field emission microscope (FEI Technologies, Hillsboro,

OR, USA) at 150 $\times$ , 500 $\times$ , and 1500 $\times$  magnification, and at an accelerating voltage of 10 kV. The material samples were coated with 2-nm iridium to increase the conductivity.

## Electrochemical characterization and sensing

Cyclic voltammetry (CV) and constant current chronopotentiometry (CP) measurements were performed using a CH Instruments electrochemical analyzer (model CHI7018E, CH Instruments Inc., Austin, TX, USA). All experiments were conducted with the developed electrodes as the working electrode and an external Ag/AgCl electrode with a 1 M KCl liquid junction as the reference electrode. CP and CV analyses used a three-electrode set-up with a platinum wire electrode as the counter electrode and an Ag/AgCl electrode as the reference electrode. Open-circuit potentiometry (OCP) was used to calibrate the sensors, conduct the selectivity and water layer tests, and nitrite sensing. All OCP measurements were obtained using a PalmSens4 potentiostat (PalmSens, Netherlands) equipped with a MUX8-R2 multiplexer.

Cyclic voltammetric measurements for 1X-LIG and 2X-LIG were performed in 5 mM ferro/ferricyanide redox probe, prepared in 0.1 M KCl as the electrolyte, with potential sweep ranging from -0.4 to 1.0 V, and scan rates of 10, 25, 50, 75, 100, and 150 mV s<sup>-1</sup>. These voltammograms were used to estimate the electroactive surface area (ESA) of the electrodes (see Supplementary information for details, Eq. S1).

Analysis based on chronopotentiometry and water layer test were used to measure the potential stability of the ISEs. For the CP measurements, after a previous conditioning step in 0.1 M NaNO<sub>2</sub> for 24 h, a current of  $\pm$ 1 nA was applied for 60 s each (120 s total), and the potential was recorded with electrodes immersed in 0.1 M NaNO<sub>2</sub>.

The water layer test was carried out by measuring the OCP of the ISEs made from both 1X-LIG and 2X-LIG electrodes over 24 h. The electrodes were first exposed to a 1 mM solution of target ion (NaNO<sub>2</sub>) for 4 h, followed by 1 mM solution of an interfering ion (KCl) for another 4 h, and finally returned to the initial target ion solution for a 16-h incubation step, with rinsing steps between transfers [72].

The developed ISEs based on 1X-LIG and 2X-LIG substrate were calibrated from 10<sup>-7</sup> to 10<sup>-1</sup> M NaNO<sub>2</sub> with additions at each 0.5 log. Calibrations were performed in DI water under agitation at 300 rpm. Ionic activity coefficients were calculated using the extended Debye-Hückel equation (Eq. S3 in Supplementary information). Selectivity coefficients were obtained by the fixed-interference method [81] for three specimens of ions common in cured food (Cl<sup>-</sup>, NO<sub>3</sub><sup>-</sup>, and H<sub>2</sub>PO<sub>4</sub><sup>-</sup>). For this analysis, similar to the calibrations described above, a large range of NaNO<sub>2</sub>

concentrations was added into a constant concentration of 1 mM of each interfering ion. Then, the selectivity coefficients were calculated using Eq. S5 (see Supplementary information). The “response time” was the time required to reach 95% of the steady-state signal ( $t_{95}$ ) after each target ion addition. The sensitivity was obtained as the mean slope of the linear portion of the calibration curve, and the limit of detection (LOD) was calculated using the  $3\sigma$  method [82].

For sensing purposes, the OCP method was used to measure the electrical potential difference between the reference electrode and the working electrode, also called electromotive force (emf). By substituting the measured emf value into the respective linear equation obtained from the calibration curve in DI water, it is possible to estimate the concentration of target ions, using ionic activity equation (see Supplemental information Eq. S2-S3). This ionic activity relates to the actual concentration of the target ion in the solution (see Supplemental, Fig. S4e). The standard colorimetric method for nitrite detection using the Griess reagent kit [83] was performed to validate the method proposed in this work. The Griess method is based on quantitative diazotization of nitrite with sulfanilic acid, and the formed salt reacts with N-(1-naphthyl)ethylenediamine (NED), forming an azo dye that can be quantitatively estimated by spectrophotometry with readings at 548 nm, according to the information stated in the kit manual. A linear calibration curve is obtained by measuring the absorbance of different nitrite concentrations (Fig. 4b).

### Preparation of food samples

Three different types of cured meat were tested to validate the developed sensors (Fig. S1). For extracting nitrite from the food samples, 30 g of each food product were sliced and crushed using a mortar and pestle to increase the surface area and facilitate nitrite extraction, then stirred in 300 mL DI water at 70 °C for 10 min, following previous established protocol [84]. The extracted solution was filtered to remove large food fragments and then centrifuged at 3260 g-force for 15 min, using a Thermo Scientific Sorvall ST-8R centrifuge (Waltham, MA, USA). Finally, the supernatant was filtered with a 0.45-μm sterile syringe filter made of surfactant-free cellulose acetate (Corning Incorporated, Germany).

### Data analysis

The data analysis for calibration curves, including regression analysis, calculations of sensitivity, and LOD was performed using MATLAB (R2020a, The MathWorks Inc., Natick, MA, USA). The *t* test with a significance level of 0.05 was performed to compare the two methods for nitrite determination and to compare the two different surfaces of electrodes (hydrophilic and hydrophobic LIG) using JMP

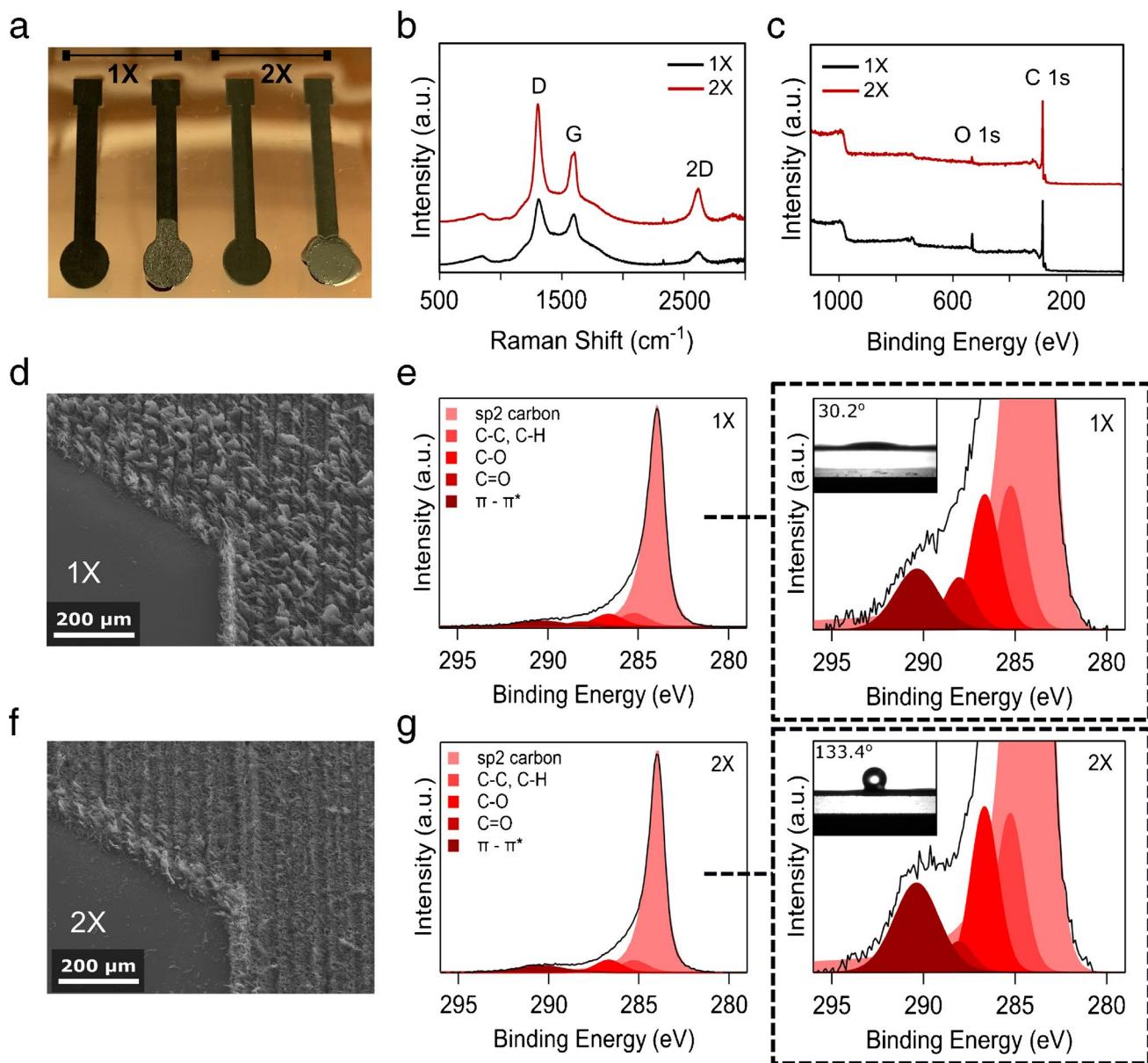
Pro v.15 statistical software (SAS Institute, Cary, NC, USA). All figures were plotted in SigmaPlot 14 (Systat Software Inc., San Jose, CA).

## Results and discussion

### Surface characterization of bare electrodes

The LIG-electrodes were patterned in a dipstick design presenting a 5-mm diameter circle with a 15-mm long stem and a 9-mm<sup>2</sup> contact pad (Fig. 2a). The circular part of the electrodes was used as the working area (with 19.63 mm<sup>2</sup>) for the subsequent deposition of the ion-selective membrane. The surface morphology of the electrodes was evaluated using SEM (Fig. 2d-f). Overall, the lasing process generated a highly porous 3-dimensional structure resulting in a high surface area. More specifically, 1X-LIG presented vertically aligned fibers [85] of various heights (Fig. 2d and S2a-b). Such features were flattened by the second lasing process, which made the surface more homogeneous and exposed the rastering traces created by the lasing process. The influence of the single- and double-lasing process on the morphology of LIG has been previously reported by Chen et al. (2021) when tuning the lasing process for the fabrication of hydrophobic LIG [53]. Hjort et al. (2022) observed similar changes in surface morphology after the second lasing process when developing ion selective electrodes for nitrate sensing [52]. Furthermore, cross-sectional images of the SC-ISEs confirm that the ion-selective membrane applied to 1X-LIG generates thinner films due to the membrane flowing over the electrode stem, which considerably impacts the water layer test, further discussed below (Fig. S5b-e). Static water contact angle measurements demonstrated the difference in surface wettability generated by the different lasing processes. The second lasing process significantly increased the hydrophobicity of the LIG-electrodes changing it from  $30.2^\circ \pm 1.3^\circ$  (first lasing) to  $133.4^\circ \pm 0.4^\circ$ . This near-superhydrophobic surface presents a strong water repulsion characteristic that is relevant for the development of ion-selective electrodes, considering the importance of suppressing the water layer formation on the surface of the electrode [86].

The distinct lasing settings used to fabricate the electrodes provided two different material composition surfaces and corresponding properties. Raman spectroscopy confirmed the well-established graphitic configuration for LIG-materials [47, 52] and was also used to compare the structures of both hydrophilic and hydrophobic surfaces, 1X-LIG and 2X-LIG (Fig. 2b). The three typical peaks, D, G, and 2D, roughly at 1350 cm<sup>-1</sup>, 1580 cm<sup>-1</sup>, and 2700 cm<sup>-1</sup>, respectively, are obtained for materials based on graphene with a certain level of lattice defects. The D peak represents defects promoted by breaks and bends in sigma bonds, while the G



**Fig. 2** **a** 1X-LIG and 2X-LIG before and after applying the ion-selective membrane. **b** Raman spectra comparing the three typical LIG peaks for both types of electrodes. **c** XPS survey exhibiting the clear decrease of oxygen content from 1X-LIG to 2X-LIG. SEM images of bare **d** 1X-LIG electrodes showing the difference in porosity com-

pared with **f** 2X-LIG. **e** XPS spectra of bare electrodes showing the decrease of carbonyl groups from 1X-LIG to **g** 2X-LIG, and respective increase of  $\pi-\pi^*$  bonds, with insets providing a zoom of the five peaks and the respective contact angle measurements

peak is related to in-plane vibration of  $sp^2$  carbon atoms, distinctive for graphitic material. In turn, the 2D peak is unique for graphene structures, which provides useful information about the stacking order and the number of graphene layers [87]. Thus, based on the values obtained for G and 2D peaks, it is possible to calculate the  $I_{2D}/I_G$  ratio regarding the number of graphene layers that were formed, that is, monolayer, bilayer, or multilayer. The 1X-LIG exhibited  $I_{2D}/I_G \approx 0.25$ , and similarly, the 2X-LIG exhibited  $I_{2D}/I_G \approx 0.44$ , which means both are based on multilayered graphene (with

$I_{2D}/I_G < 1$ ) [88]. The higher this ratio, the better the quality of the graphene structure [89]. Previous works reported lower or similar  $I_{2D}/I_G$  ratios for LIG-materials, with values ranging from 0.30 to 0.44 [72, 90, 91]. The 2X-LIG displayed a higher D peak owing to additional bending in the carbon structures caused by the double lasing [53]. The  $I_D/I_G$  peaks for both LIG-materials were  $> 1$ , which is expected for LIG-materials and might also be attributed to the lasing process occurring in an uncontrolled atmosphere chamber [54]. These high D peaks might be related to the presence

of  $O_2$  in the air, which provides an oxidative environment, thus generating rough edges and large pores, as previously described [54]. In addition, the XPS spectra showed a slight increase of  $\pi-\pi$  interactions, which are responsible for the carbon lattice stacking, after the second lasing. This proves that the laser-induction converts the  $sp^3$  carbon structure mostly present in the PI into  $sp^2$  type.

The surface chemical composition obtained from XPS showed that LIG materials are formed by carbon (C) and oxygen (O). Electrodes fabricated with one lasing step exhibited 89.96% of C and 10.04% of O, while 96.11% of C and 3.89% of O were observed after the second lasing. A reduction of  $\sim 2.5$  times on the oxygen content after the second lasing (Fig. 2c) is directly related to the low wettability surface obtained, as the oxygen-containing functional groups exhibit high affinity with water. A similar work reported a reduction of  $\sim 3.9$  times on the oxygen content after the second lasing, which was further related to the hydrophobic surface exhibiting a static water contact angle of  $\sim 143^\circ$  [53]. The clear reduction of carbonyl groups is notable in Fig. 2e–g, which hinders hydrophilic interaction due to a lower incidence of hydrogen bonds (see Table S1 in Supplementary information). Additionally, the second lasing eliminates the vertically aligned structures (Fig. 2d–f) and creates a microporous surface that can be associated with a lower droplet adhesion force by increasing the fraction of liquid–air contact area on the surface (i.e., higher hydrophobicity) [53, 92].

Furthermore, the electrical conductivity was not significantly different ( $p=0.7720$ ) when comparing electrodes fabricated using both lasing methods, with a sheet resistance of  $0.231 \pm 0.033 \text{ k}\Omega \text{ sq}^{-1}$  for 1X-LIG and  $0.221 \pm 0.046 \text{ k}\Omega \text{ sq}^{-1}$  for 2X-LIG. These sheet resistance values are substantially lower than other published graphene-based materials, for instance,  $15\text{--}20 \text{ k}\Omega \text{ sq}^{-1}$  for LIG-based sensors fabricated with a low-cost UV-laser [72] and  $\sim 30 \text{ k}\Omega \text{ sq}^{-1}$  for inkjet-printed graphene devices [93].

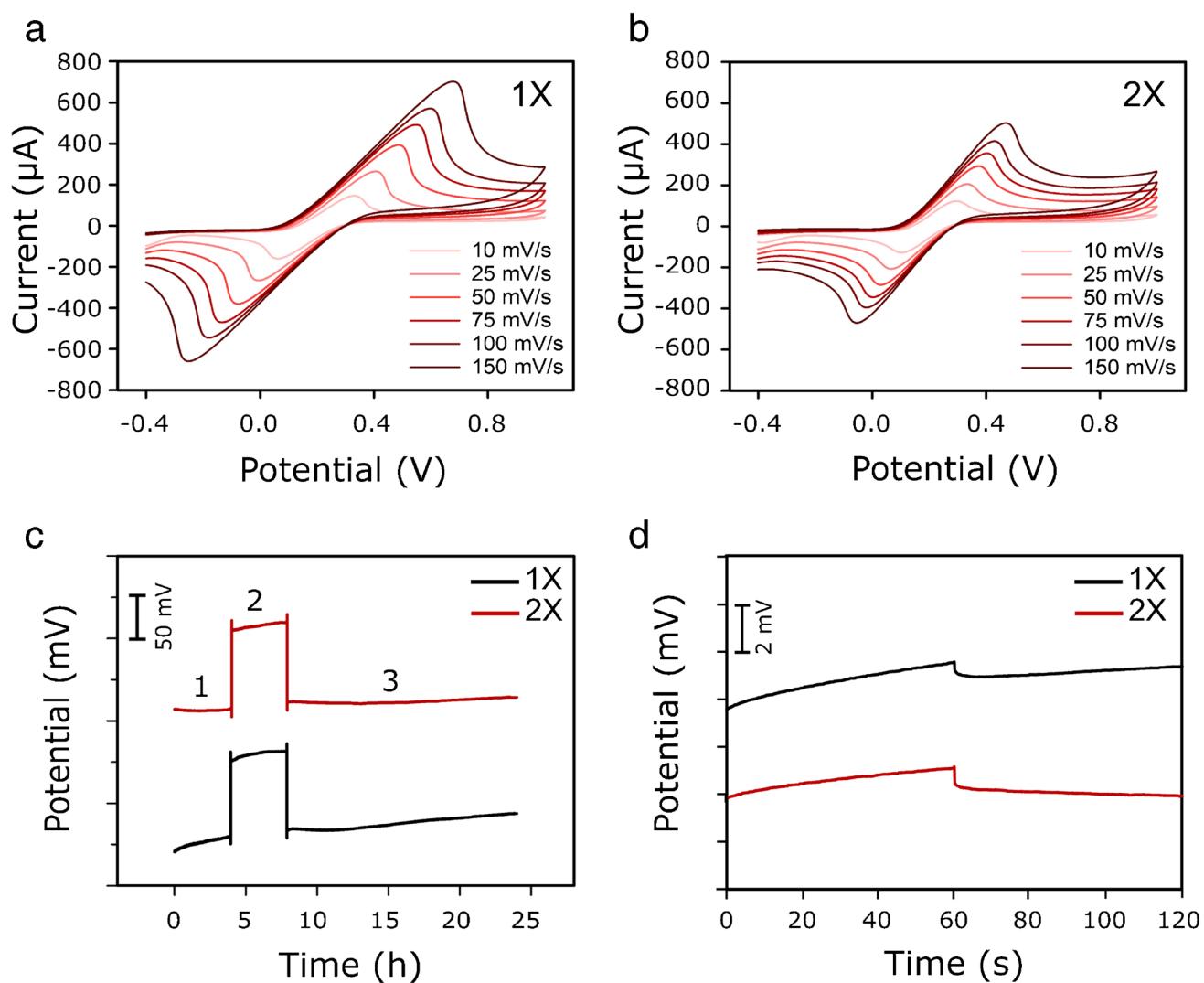
## Electrochemical characterization

Cyclic voltammetric measurements of bare electrodes were performed to evaluate both LIG-electrodes and to estimate their electroactive surface area (ESA). Redox peaks were observed for both 1X- and 2X-LIG independent of the scan rate applied (Fig. 3a–b). The peak separation ranged from 264.82 to 896.18 mV for 1X-LIG and from 191.43 to 526.38 mV for 2X-LIG. The increase in potential peak separation at faster scan rates indicates a system with limitations in the electron transfer rate [94, 95]. Similarly, the Randles–Sevcik plots (Fig. S6b–c) demonstrate a linear increase in peak current with the square root of the scan rate for both LIG-electrodes, indicating a diffusion-controlled system [94, 96]. This behavior suggests a quasi-reversible

system that is controlled by both mass and charge transfer [96, 97]. The calculated ESA for 1X-LIG was  $49.84 \pm 4.24 \text{ mm}^2$ , representing 253.82% compared to the geometric area ( $19.63 \text{ mm}^2$ ). Alternatively, the 2X-LIG presented an ESA of  $37.41 \pm 0.97 \text{ mm}^2$ , which is 190.52% higher than the geometric area. Higher ESA compared to the geometric area is consistently observed in LIG-based electrodes [73, 91, 98, 99]. The increase in ESA compared to the geometric area is attributed to the defect-rich highly porous 3D structure of the LIG, which increases the surface area and, consequently, creates more available sites for electron transfer during redox reactions [98, 99]. Despite the significantly higher ESA ( $p=0.0080$ ) presented by the 1X-LIG electrodes, the 2X-LIG was used for further sensing application because it exhibits a hydrophobic surface, which helps improve the stability of the sensor, as discussed previously and will be further demonstrated next.

Potential drifts, standard potential ( $E^0$ ) reproducibility, and membrane delamination might be attributed to forming an aqueous film (water layer) between the selective membrane and the solid-contact interface [100, 101]. For this reason, water layer tests have become an important method to select and validate SC-ISEs. When an aqueous layer is formed, a longer time is required for the SC-ISE to reach the equilibrium potential, and substantial potential drift causes the need for frequent recalibration. Herein, SC-ISEs made with both 1X-LIG and 2X-LIG were subjected to two different solutions for a few hours, as previously described, and the potential was measured (Fig. 3c). The ISE based on 2X-LIG clearly exhibited a significant ( $p=0.0001$ ) lower potential drift,  $397.6 \pm 29.4 \text{ }\mu\text{V h}^{-1}$ , compared to the 1X-LIG,  $1262.5 \pm 36.2 \text{ }\mu\text{V h}^{-1}$ , after returning to the initial solution  $1 \text{ mM NaNO}_2$  (section c in the Fig. 3c). This difference suggests that the hydrophobicity observed for 2X-LIG hinders the formation of a water layer, as previously reported [52] and contributes to a more stable potential. Moreover, the membrane applied onto 2X-LIG electrodes was thicker than the one applied to 1X-LIG (Fig. S5e) due to the membrane flowing over the 1X-LIG electrode stem, which possibly influenced the poor performance of the single-lasing electrodes as a recent study has reported that thin ion-selective membranes might exhibit anomalous potentiometric response because of changes in the water layer composition [102].

Another study to evaluate the potential stability was accomplished using constant current chronopotentiometry by applying a current of  $\pm 1 \text{ nA}$ , which is sufficient to polarize the surface of the electrode to calculate its capacitance [103] (Fig. 3d). The capacitances of both ISEs were calculated from Eq. S6. The potential drifts and capacitances were  $11.7 \pm 3.1 \text{ }\mu\text{V s}^{-1}$  and  $91.0 \pm 23.7 \text{ }\mu\text{F}$  for 1X-LIG, respectively, and  $12.4 \pm 1.0 \text{ }\mu\text{V s}^{-1}$  and  $88.3 \pm 8.2 \text{ }\mu\text{F}$  for 2X-LIG, which are very close to previous studies



**Fig. 3** **a, b** CV measurements for both 1X-LIG and 2X-LIG bare electrodes, respectively, at scan rates from 10 to 150 mV s<sup>-1</sup>. **c** Water layer test for ISEs based on 1X-LIG and 2X-LIG, immersed in 1 mM NaNO<sub>2</sub> (1), 1 mM KCl (2), and back to 1 mM NaNO<sub>2</sub> (3)

with graphene-based ISEs, that obtained potential drifts in the range of 10 to 13  $\mu$ V s<sup>-1</sup>, and capacitances varying from 75 to 95  $\mu$ F [52, 104]. No significant difference was observed for potential drifts ( $p=0.5808$ ) and capacitances ( $p=0.8425$ ), calculated from chronopotentiometry, when comparing ISEs made on hydrophilic and hydrophobic surfaces. However, the potential drift was notably higher for the hydrophilic SC-ISE observed from the water layer test. According to Eq. S6, the calculated capacitance is inversely proportional to the potential drift, which means higher capacitances are associated with more stable potential. As previously stated, one of the conditions for providing a stable and reliable SC-ISE is ideally nonpolarizable interfaces with high exchange current densities [105], which implies higher capacitances. This statement is relevant when considering

with 2X-LIG displaying lower potential drift. **d** Chronopotentiometry responses for both SC-ISEs based on 1X-LIG and 2X-LIG, with no significant difference observed for potential drift and capacitance values

the design of SC-ISEs for continuous ion monitoring. In this study, the capacitance values for both SC-ISEs are not significantly different, and they are in the range of other published graphene-based ISEs, but the 1-day measurement of potential drift (water layer test) displayed a significant difference for both, which demonstrates the utility of the hydrophobic LIG for ion sensing and in our particular case for nitrite ion sensing. Furthermore, the SC-ISE made with 1X-LIG exhibited a larger variability in potential when reading known concentrations of NaNO<sub>2</sub> compared to 2X-LIG (Fig. S3a–b and S4a–b). Thus, it implies less accuracy and consistency, displaying a higher standard deviation for the NaNO<sub>2</sub> measurement, which was also considered when choosing the hydrophobic LIG as a high-quality, stable sensor for potentiometric detection of nitrite.

## Nitrite sensing

Open-circuit potentiometry was used to obtain calibration curves for nitrite SC-ISE fabricated from 1X- and 2X-LIG in DI water by incrementally increasing the nitrite levels in the electrochemical cell. The calibration curves demonstrated that both types of sensors performed following the Nernst equation (Eq. S7), which linearly relates the measured potential with the activity of a target ion, exhibiting sensitivities of  $58.2 \pm 2.0$  and  $59.5 \pm 0.8$  mV dec $^{-1}$ , respectively (Fig. S3). The reproducibility of both sensors was evaluated considering the relative standard deviation values (RSD, Eq. S4) for the respective sensitivities, which are based on the slope of the linear calibration curve. The RSD values were 3.4% ( $n=4$ ) and 1.3% ( $n=4$ ) for sensors based on hydrophilic (1X-LIG) and hydrophobic (2X-LIG), respectively. These low values attest to the high reproducibility of the presented sensors. Additionally, once 2X-LIG was selected to perform the sensing analysis in real samples, 20 sensors were tested with sausage, ham, and bacon, and the RSD for their sensitivity was 5.51% ( $n=20$ ), indicating that even with an increase in the sample size, the RSD remains low.

Similar calibrations were performed in the presence of different salts (NaCl, NaH<sub>2</sub>PO<sub>4</sub>, and NaNO<sub>3</sub>) to evaluate the effect of interfering ions commonly present in cured food (Fig. S4d). These calibrations enable the calculation of the selectivity coefficients (Eq. S5) for each tested ion and are reported in the last column of Table 1. These coefficients were relatively similar to a previously published work that also tested nitrite-ISE [106], where the  $\log K_{NO_{2},i}^{pot}$  for Cl<sup>-</sup>, NO<sub>3</sub><sup>-</sup>, and H<sub>2</sub>PO<sub>4</sub><sup>-</sup> ranged from -2 to -3, showing that these three ions are not strictly discriminated by the nitrite ionophore [80] with H<sub>2</sub>PO<sub>4</sub><sup>-</sup> showing the largest interference. Nonetheless, the results for nitrite determination showed that interfering ions did not negatively affect the sensor's performance in food samples.

Previous studies have developed sensors that can detect nitrite at very low detection limits, often in the nanomolar range (Table 2); however, not only these sensors require noble metals and other expensive materials to fabricate, but also need extensive sample pre-treatments. Most of them show a limited detection range regarding the upper limit

imposed by federal regulations in the USA [13] ( $\approx 4 \times 10^{-3}$  M or 200 ppm of nitrite), which results in the need of several dilutions and sample preparation. Furthermore, nitrite sensors based on potentiometric techniques are not very common (Table 2), showing an opportunity for implementing this little-explored approach. As usual for potentiometric techniques, the sensor developed herein can detect nitrite in a wide range that spans four orders of magnitude (Fig. 4a), 0.33 to 4600 ppm, far exceeding the federally set limit for cured meats as well as for drinking water (1 ppm according to U.S. Environmental Protection Agency) [14]. Additionally, the developed sensing method does not require sample dilutions or pre-treatments, avoiding major intrinsic errors, and exhibits a relative low cost per sensor, approximately US\$ 1.20, considering only material expenses.

A review paper published in 2019 compared more than a hundred graphene-based electrochemical sensors for nitrite detection, and all of them used either voltammetry or amperometry as the electrochemical technique [78]. In many of these works, in addition to the excessive and laborious steps to obtain the modified electrodes, the detection ranges were not as wide as expected, except for a few cases where they were within the regulated levels for food but only tested in water sources. The ability to address all existing challenges regarding the stability and reliability of the measured potential, solid contact surface structure, and selectivity, the present nitrite sensor, based on a potentiometric technique, offers an alternative method with an unusual approach and outstanding sensing performance.

Before measuring the potential of food extracts, the sensors were calibrated by measuring the emf of six different nitrite solutions with known concentrations ranging from 10 to 10,000  $\mu$ M (Fig. S4e). Average measurement time was 5 min, and response time at 95% of the steady-state signal (t95) was 9 s. The emf obtained for each sensor corroborated with the known nitrite concentrations by applying it to the linear equations obtained from the calibrations. A correlation relating expected and experimental values are shown in Fig. 4c, where the experimental values are notably close to the expected ones, especially at higher concentrations, exhibiting a mean absolute percentage error (MAPE) of 6.7% (Eq. S8). These MAPE

**Table 1** Electrochemical performance of nitrite SC-ISE based on 2X-LIG and selectivity coefficients at 1 mM interfering-ion concentration ( $n=4$ ). Values given are mean  $\pm$  standard deviations

Sensitivity (mV/dec)	LOD ( $\mu$ M)	Range of detection (M)	Standard potential $E^\circ$ (mV)	Response time (s)	Selectivity coefficient
$-59.5 \pm 0.8$	$7.2 \pm 3.6$	$10^{-5}$ to $10^{-1}$	$-13.1 \pm 4.0$	$9 \pm 2$	$\log K_{i,Cl^-}^{pot} -1.74 \pm 0.05$
					$\log K_{i,(H_2PO_4)^-}^{pot} -3.17 \pm 0.02$
					$\log K_{i,NO_3^-}^{pot} -1.39 \pm 0.05$

**Table 2** Comparison of recently published reports on electrochemical nitrite sensors

Transducer	Functionalization	Electrochemical technique	LOD ( $\mu\text{M}$ )	Detection range (M)	Sample	Ref
GCE	Hemoglobin/AuNPs-CMK-8/GC	DPV	0.0021	$5 \times 10^{-9}$ to $10^{-3}$	Extract of meat	[107]
GCE	FeT4MPyP/CuTSP	DPV	0.1	$5 \times 10^{-7}$ to $7.5 \times 10^{-6}$	Extract of sausage and vegetables	[108]
GCE	Cu/MWCNT/RGO	SWV	0.03	$10^{-7}$ to $7.5 \times 10^{-5}$	Extract of sausage, salami, and cheese	[84]
GCE	TiO <sub>2</sub> -Ti <sub>3</sub> C <sub>2</sub> T <sub>X</sub> nanohybrid/CTAB/CS	DPV	0.85	$3 \times 10^{-6}$ to $1.25 \times 10^{-3}$	Water and milk	[109]
Au-SPE	2-ATP/PVA/GA/AuNPs	DPV	4	$\sim 10^{-5}$ to $10^{-3}$	Exhaled breath condensate	[110]
GCE	Au-HNTs-GO	Amperometry	0.03	$10^{-7}$ to $6.2 \times 10^{-2}$	Tap water	[111]
GCE	Fe-BZIM/Nafion	CV and CP	< 1	$10^{-6}$ to $10^{-4}$	-	[112]
GCE	GO-MWCNT-Pt/Mb	Amperometry	0.93	$10^{-6}$ to $1.2 \times 10^{-2}$	Rain, river, and tap water	[113]
GCE	MWCNT/nitrite-selective membrane	Potentiometry	0.6	$10^{-6}$ to $10^{-2}$	Seawater	[114]
LIG	Bare-LIG	DPV	0.8	$5 \times 10^{-6}$ to $4.5 \times 10^{-4}$	Tap water and pickle water	[115]
LIG	CS	DPV	0.9	$2 \times 10^{-6}$ to $10^{-3}$	Tap water and lake water	[116]
LIG	MWCNT-AuNPs	SWV	0.9	$10^{-5}$ to $1.4 \times 10^{-4}$	Tap water and PBS	[117]
LIG	ION-RGO	DPV	7.21	$10^{-5}$ to $4 \times 10^{-4}$	PBS buffer	[118]
LIG	Bare-LIG	DPV	0.27	$10^{-5}$ to $7 \times 10^{-5}$	Buffered solution	[119]
LIG	Nitrite-selective membrane	OCP	7.2	$10^{-5}$ to $10^{-1}$	Extract of cured meat	This work

ATP, aminothiophenol; PVA, polyvinyl alcohol; GA, glutaraldehyde; SPE, screen-printed electrode; HNTs, natural halloysite nanotubes; GO, graphene oxide; AuNPs, gold nanoparticles; CMK-8, mesoporous carbon composites; CP, chronopotentiometry; CS, chitosan; CTAB, hexadecyl trimethyl ammonium bromide; CuTSP, copper tetrasulfonated phthalocyanine; CV, cyclic voltammetry; DPV, differential pulse voltammetry; FeT4MPyP, iron (III) tetra-(N-methyl-4-pyridyl)-porphyrin; GCE, glassy carbon electrode; LIG, laser-induced graphene; Mb, myoglobin; ION-RGO, iron oxide nanoparticle with reduced graphene oxide; MWCNT, multiwall carbon nanotubes; OCP, open-circuit potentiometry; RGO, reduced graphene oxide; SWV, Square wave voltammetry.

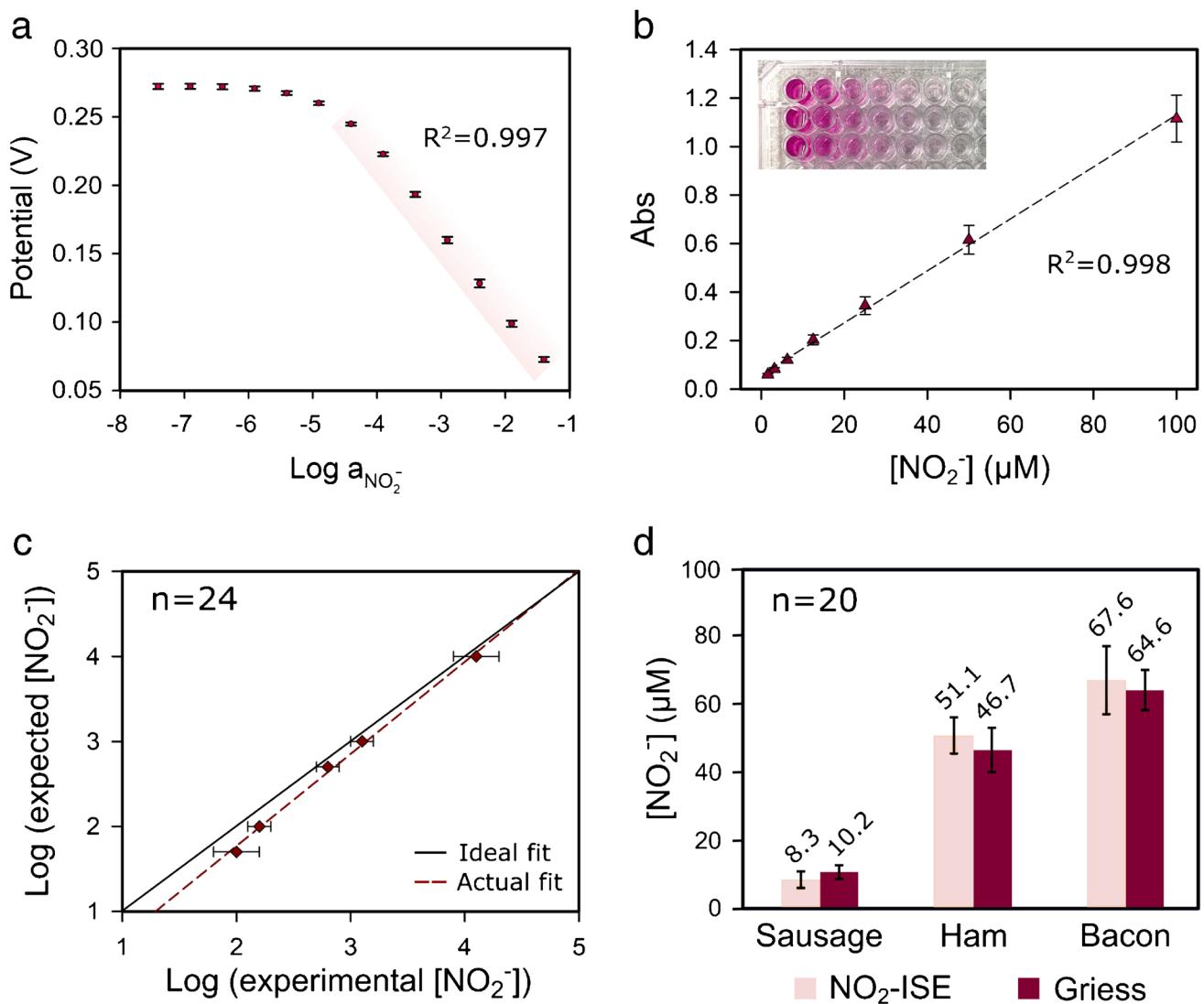
results are indicative of the high reliability of the developed method. The application of MAPE as a loss function for regression analysis is relevant both from practical and theoretical points of view because of the existence of an optimal (real) model that allows for verification of empirical values, where the consistency can be proved [120].

To validate the method, a standard spectrophotometric assay that uses Griess reagents for nitrite detection [83, 121] was compared to the potentiometric response obtained with the developed nitrite sensor. There were no significant differences for samples analysis of sausage ( $p=0.2369$ ), ham ( $p=0.3025$ ), and bacon ( $p=0.6141$ ) when comparing both potentiometric and spectrophotometric techniques (Fig. 4d). For the Griess method, a linear calibration curve was obtained by measuring the absorbance of solutions with different nitrite concentrations (Fig. 4b). In this work, all food samples tested complied with federal legislation, with nitrite levels below 200 ppm. Based on the present method and the Griess standard method, respectively, the sausage samples exhibited  $3.8 \pm 1.1$  ppm and  $4.7 \pm 0.9$  ppm, ham

samples exhibited  $23.5 \pm 2.4$  ppm and  $21.5 \pm 3.0$  ppm, and bacon samples exhibited  $31.2 \pm 4.6$  and  $29.7 \pm 2.7$  ppm of nitrite. It is relevant to mention that these sensors can be used multiple times to test different samples in sequence. Additional studies should be performed in future works to precisely describe how many times these sensors can be used and their shelf-life under storage. Furthermore, there is a growing interest in using SC-ISE sensors for continuous measurements for in-field applications, and in this case, it would be desirable to add other conductive materials, such as metal nanoparticles or conductive polymers to the LIG surface to increase capacitance that could improve potential stability, and consequently reduce potential drift [122, 123].

## Conclusions

This work reports the successful development of a solid-contact-ion selective electrode (SC-ISE) by utilizing a laser-induced graphene (LIG) platform capable of monitoring



**Fig. 4** **a** Calibration curve with half-log step additions ranging from  $10^{-7}$  to  $10^{-1}$  M of  $\text{NaNO}_2$ , showing a highlighted linear range,  $n=4$ . **b** Calibration curve obtained by measuring the absorbance of different nitrite concentrations using the Griess reagents kit, inset: triplicate of  $\text{NaNO}_2$  (100, 50, 25, 12.5, 6.25, 3.125, 1.5625  $\mu\text{M}$ ) reacting with these reagents. **c** Comparison between expected and experimental

potential readings at five different nitrite concentrations 50, 100, 500,  $10^3$ , and  $10^4$   $\mu\text{M}$ , exhibiting a slight offset from the ideal correlation. **d** Validation of the developed method compared to the standard method, with no significant differences for all three types of meat, units in  $\mu\text{M}$  ( $\alpha < 0.05$ )

nitrite levels in cured food products over regulatory compliance ranges. The hydrophobic LIG-electrodes proved more suitable as SC-ISE than the hydrophilic LIG because it hindered the formation of a water layer with significantly lower potential drift, contributing to a more stable potential. These sensors exhibited a wide linear range spanning four orders of magnitude of nitrite concentration ( $10^{-5}$  to  $10^{-1}$  M), near-theoretical sensitivity of 59.5 mV/dec, and a considerably low detection limit when compared to the limits imposed by federal regulations. These analytical characteristics resemble or exceed previous nitrite sensing studies [78] and far exceed the federal limit of  $\sim 200$  ppm in cured meat [13].

Importantly, other ions commonly found in cured meats did not prevent the sensors from detecting the target ion. In just 5 min, the ISE-LIG sensor could quantitatively detect nitrite in extracts of cured meats with no significant difference from the standard method. In summary, the ISE-LIG sensor not only demonstrates a sensitive and rapid method for nitrite monitoring but also has the potential for widespread adoption given its fabrication using inexpensive and high-throughput laser induction technique that eliminates multiple preparation steps and does not require modification of electrodes with nanomaterials as in previous reports [84, 107, 110]. Furthermore, this sensing platform can be easily

modified for many ions relevant to human health, precision agriculture, surface and drinking water quality, and food contaminant monitoring, which suggests its widespread use in future potentiometric sensing applications.

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**Data availability** The data presented in this study are available on request from the corresponding authors.

## Declarations

**Competing interests** The authors declare no competing interests.

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