# Projected sensitivity of DMR adio-m<sup>3</sup>: A search for the QCD axion below 1 $\mu$ eV

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The QCD axion is one of the most compelling candidates to explain the dark matter abundance of the Universe. With its extremely small mass ( $\ll 1~{\rm eV}/c^2$ ), axion dark matter interacts as a classical field rather than a particle. Its coupling to photons leads to a modification of Maxwell's equations that can be measured with extremely sensitive readout circuits. DMRadio-m³ is a next-generation search for axion dark matter below 1  $\mu$ eV using a > 4 T static magnetic field, a coaxial inductive pickup, a tunable LC resonator, and a DC-SQUID readout. It is designed to search for QCD axion dark matter over the range 20 neV  $\lesssim m_a c^2 \lesssim 800~{\rm neV}$  (5 MHz  $< \nu < 200~{\rm MHz}$ ). The primary science goal aims to achieve Dine-Fischler-Srednicki-Zhitnitsky sensitivity above  $m_a c^2 \approx 120~{\rm neV}$  (30 MHz), with a secondary science goal of probing Kim-Shifman-Vainshtein-Zakharov axions down to  $m_a c^2 \approx 40~{\rm neV}$  (10 MHz).

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#### I. INTRODUCTION

The strong *CP* problem describes an unnaturally finetuned symmetry of nature that suggests an explanation

Published by the American Physical Society under the terms of the Creative Commons Attribution 4.0 International license. Further distribution of this work must maintain attribution to the author(s) and the published article's title, journal citation, and DOI. Funded by SCOAP<sup>3</sup>. beyond the Standard Model (SM) of particle physics. The leading solution to this problem is the introduction of a new Peccei-Quinn symmetry, which is spontaneously broken at some high-energy scale  $f_a$ , producing a pseudo-Goldstone boson, the axion a [1–4]. Interactions with quantum chromodynamics (QCD) give the axion a potential, which solves the strong CP problem, gives the axion mass  $m_a c^2 \approx 5.7$  neV ( $10^{15}$  GeV/ $f_a$ ) [5], and produces a relic axion abundance in the early Universe that satisfies the conditions to be dark matter (DM) [6–8]. Over the last few years, the axion has emerged as a leading DM candidate.

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Recent theoretical work has opened a wide range of interesting parameter space for both QCD axion and axion-like particle (ALP) models [9–13]. In particular, the mass range 1 neV  $\lesssim m_a c^2 \lesssim 1~\mu eV$  is interesting for grand unification theories (GUTs) [11,14–22], string theory models [23–30], and naturalness arguments [12,31]. Other ALP models in this mass range simultaneously explain both the DM abundance and matter-antimatter asymmetry [32].

Its small mass and cold temperature give axion DM a very high per-state occupation, making it interact as a wavelike classical field. Depending on the precise model, the axion may couple to any SM particle, but one of the least model-dependent couplings is the axion-photon coupling  $g_{a\gamma\gamma}$  [14]. For the QCD axion,  $g_{a\gamma\gamma}$  is directly proportional to  $m_a$ , with an uncertainty on the proportionality constant spanning an order of magnitude in uncertainty and represented by the Kim-Shifman-Vainshtein-Zakharov (KSVZ) [33,34] and Dine-Fischler-Srednicki-Zhitnitsky (DFSZ) [35,36] models. A more generic class of ALP breaks this proportionality and can have a wide range of masses and  $g_{a\gamma\gamma}$  couplings.

The axion-photon coupling produces a modified Ampère's law, behaving as an effective current that can be written approximately as

$$\mathbf{J}_{\mathrm{eff}} pprox g_{a\gamma\gamma} \frac{\sqrt{\hbar c}}{\mu_0} \sqrt{2\rho_{\mathrm{DM}}} \cos\left(\frac{m_a c^2 t}{\hbar}\right) \mathbf{B},$$
 (1)

with local DM density  $\rho_{\rm DM} \approx 0.45~{\rm GeV/cm^3}$  [37] and axion frequency  $\nu_a = m_a c^2/(2\pi\hbar)$ . A powerful approach to searching for ADM is to deploy a large, static **B** field to drive  ${\bf J}_{\rm eff}$  through a pickup structure and search for excess power in a narrow axion signal bandwidth  $\Delta\nu_{\rm sig}/\nu_a \approx 10^{-6}$  set by the Standard Halo Model [38].

Historically, ADM experiments have focused on the mass range 1  $\mu eV \lesssim m_a c^2 \lesssim 40 \ \mu eV$ , where the axion is able to resonantly excite a microwave cavity [39-46]. However, the cavity resonance requires a detector size L comparable to the axion Compton wavelength,  $m_a cL/\hbar \sim 1$ , and makes probing masses below 1  $\mu$ eV impractical. At lower axion masses, the magnetoquasistatic (MQS) limit applies, and  $J_{\text{eff}}$  can be treated as inducing magnetic fields that are detectable with an inductive pickup and enhanced with a lumped-element resonator [47-51]. This has been experimentally realized with a toroidal magnet with the ABRACADABRA-10 cm prototype [52-54] and SHAFT [55], and in a solenoidal geometry with ADMX-SLIC [56] and the BASE Penning trap [57]. DMRadio-Pathfinder also performed a resonant search for dark photons (DPs) in the MQS regime with a solenoidal pickup [58]. In this paper, we present an optimized lumped-element experimental design called DMRadio-m<sup>3</sup>, capable of probing ADM over the mass range 20 neV ≤  $m_a c^2 \lesssim 800 \text{ neV}$  (5 MHz  $< \nu < 200 \text{ MHz}$ ) with a 5 yr scan time, achieving DFSZ sensitivity for masses above  $\sim 120 \text{ neV}/c^2 (30 \text{ MHz}).$ 

#### II. LUMPED-ELEMENT DETECTION

The challenge facing any ADM experiment is one of signal-to-noise ratio (SNR). The ADM field contains enough power per square meter to illuminate an LED, but the self-impedance of photon-electron coupling implies that any practical receiver will only extract a tiny fraction of this power [59]. Resonant circuits—either microwave cavities or LC lumped-element circuits—have much lower impedance on resonance and can extract more power from the axion field.

For a readout circuit inductively coupled to  $J_{\text{eff}}$ , the induced voltage can be expressed as

$$|\tilde{V}_{pp}|^2 = 4g_{a\gamma\gamma}^2 \rho_{\rm DM} \left(\frac{c^5}{\hbar \mu_0}\right) m_a^2 c_{\rm PU}^2 L_{\rm eff} B_0^2 V_{\rm PU}^{5/3} \qquad (2)$$

(see the Appendix). Here,  $B_0$  and  $V_{\rm PU}$  are the characteristic magnetic field and pickup volume,  $L_{\rm eff}$  is the effective inductance of the pickup and readout circuit at the axion frequency  $2\pi\nu_a=m_a/\hbar$  and should ideally be dominated by the effective inductance of the pickup,  $L_{\rm PU}$ .  $c_{\rm PU}$  is a dimensionless proportionality constant that depends on the geometry. When coupled to a capacitor, the impedance of the resulting circuit  $Z_L(\nu)$  decreases significantly at the resonance frequency,  $\nu_r$ . If  $\nu_r$  is tuned close to the axion driving frequency, the current driven through the circuit from axion conversion,  $\tilde{I}_{\rm sig}$ , can be enhanced by multiple orders of magnitude—expressed in terms of the resonator quality Q:

$$|\tilde{I}_{\text{sig}}|^2 = 4g_{\text{ayy}}^2 \rho_{\text{DM}} \left(\frac{\hbar c}{\mu_0}\right) \frac{c_{\text{PU}}^2 B_0^2 V_{\text{PU}}^{5/3}}{L_{\text{eff}}} \left(\frac{Q^2}{1 + (2Q\Delta)^2}\right), \quad (3)$$

which holds for small fractional detunings ( $\Delta \ll 1$ ). The signal follows the Lorentzian response of the resonator circuit and depends on the fractional detuning of resonance from the axion frequency,  $\Delta = (2\pi\hbar\nu_r - m_ac^2)/m_ac^2$ . This gives the resonator characteristic width  $\Delta\nu_r = \nu_r/Q$ .

The sensitivity for a resonant search is determined by its scan rate: the rate at which one can scan through frequencies searching for the axion induced signal current. The scan rate is set by the desired  $g_{a\gamma\gamma}$  sensitivity and SNR at each resonator tuning, and the total equivalent current noise  $|\tilde{I}_N|^2$  at that frequency. At a single resonator tuning, the integration time  $\tau$  required to achieve this SNR at  $g_{a\gamma\gamma}$  is given by a modified Dicke radiometer equation,

$$SNR(\nu) = \frac{|\tilde{I}_{sig}|^2}{|\tilde{I}_N(\nu)|^2} \sqrt{\tau \Delta \nu_{sig}}.$$
 (4)

The current noise  $|\tilde{I}_N(\nu)|^2$  is dominated by thermal Johnson-Nyquist noise and the noise of the first-stage

amplifier,  $\eta_A(\nu)$ . The amplifier noise consists of both the imprecision and backaction noise (see the Appendix).

For a search with many discrete resonator tunings, the scan rate is approximated by the continuous function

$$\frac{d \log \nu_r}{dt} = \pi (6.4 \times 10^5) \left( \frac{c^2}{\mu_0^2} \right) \frac{g_{a\gamma\gamma}^4 \rho_{\rm DM}^2}{\rm SNR^2} \nu_r 
\times c_{\rm PU}^4 Q B_0^4 V_{\rm PU}^{10/3} \bar{\mathcal{G}}(\nu_r, k_B T, \eta_A(\nu_r)), \quad (5)$$

where  $\bar{\mathcal{G}}(\nu_r, k_B T, \eta_A(\nu_r))$  is a dimensionless factor that defines the effect of the amplifier matching on the scan rate (see the Appendix). Explicitly, it is a tradeoff between the Lorentzian signal gain and the frequency-dependent system noise. Together, these two set the sensitivity bandwidth,  $\Delta \nu_{\rm sens}$ , which determines the spacing between adjacent resonator tunings. Since the thermal noise and amplifier backaction components follow the same Lorentzian line shape as the signal gain, were they the only noise sources, we would have constant SNR over all frequencies, and  $\Delta \nu_{\rm sens}$  could grow arbitrarily large. However, at frequencies sufficiently far from  $\nu_r$ , the amplifier imprecision noise dominates, decreasing the SNR. For a scattering-mode circuit tuned for optimal single-frequency power transfer, the sensitivity bandwidth nearly matches the resonator line width,  $\Delta \nu_{\rm sens} \approx \nu_r/Q$ . Alternatively, for a matching circuit tuned for optimal scan speed, modestly reducing onresonance SNR for a larger  $\Delta \nu_{\rm sens}$  can significantly improve the scan rate. In the thermal noise limit, the optimal coupling yields  $\bar{\mathcal{G}}(\nu_r, k_B T, \eta) \approx 2\pi\hbar\nu_r (6\sqrt{3}k_B T\eta)^{-1}$ .

#### III. DETECTOR DESIGN

DMRadio-m³ uses a static > 4 T solenoid magnet to drive  $J_{\rm eff}$  along the axis of a coaxial inductive pickup [see Fig. 1(b)]. The coaxial pickup couples to a tunable capacitor to form an LC resonator circuit, targeting a quality factor of  $Q > 10^5$ . The circuit is read out by conventional DC-SQUIDs with a target noise level of 20 times the standard quantum limit (SQL). The coaxial pickup and capacitor are cooled to an operating temperature of  $T \approx 20$  mK, while the magnet sits at 4 K. We discuss each of these in detail below.

DMRadio-m<sup>3</sup> builds on the experience of ABRACADABRA-10 cm, DMRadio-Pathfinder, DMRadio-50L (currently under construction.) All three detectors use a superconducting inductive pickup to search for ADM or DPs below 20 neV. DMRadio-Pathfinder and DMRadio-50L [60] utilize a resonant readout approach, and ABRACADABRA-10 cm and DMRadio-50L utilize a toroidal magnet. The toroidal geometry works well at low frequencies (i.e., low axion masses) because it completely encloses the magnetic field, allowing the use of lossless superconducting materials. Loss is only introduced through coupling to lossy materials near the detector, which can be efficiently screened. However, at frequencies above ~50 MHz, irreducible capacitances associated with the readout begin to short the signal and rapidly reduce the signal sensitivity at higher frequencies [61]. A change of geometry is required to probe higher axion masses.

DMRadio-m<sup>3</sup> uses a solenoid magnet, with a bore volume of  $V \approx 2 \text{ m}^3$ , and a characteristic field of  $B_0 > 4 \text{ T}$ . This geometry creates a large-volume, high-field region and

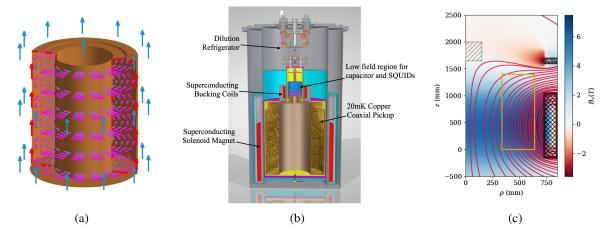


FIG. 1. (a) Cartoon of the DMRadio- $m^3$  coaxial pickup in a uniform magnetic field. The magnet (not shown) drives an oscillating  $J_{eff}$  (blue arrows) along the axis of the coax, which drives an azimuthal magnetic field (purple arrows), and a current along the coax (red arrows). Voltage accumulates across the slit on the top. (b) Cross section of DMRadio- $m^3$  with major components labeled. Total height is  $\sim$ 2.5 m. (c) Conceptual magnetic field design that produces high field across the volume of the coax (gold box) and a low-field region for sensitive electronics (gray dashed region). Color shading represents the vertical component of the primary field  $B_z$ , while the red lines indicate the magnetic field flux lines. The field is generated by the solenoid coils in the black-hashed region, and bucking coils with counterflowing current in the black-dotted region.

drives  $J_{\rm eff}$  along the axis of the solenoid [see Fig. 1(a)]. Unlike the toroid, the solenoid exposes the magnetic field, requiring that the pickup sit in the large primary field. Because SQUIDs cannot operate in such a field, DMRadio-m³ uses a set of bucking coils to bend the field lines outward, producing a low-field region directly above the high-field region. The resulting magnetic field has significant variation within the bore of the magnet, reaching a peak value of  $\approx 7$  T off-axis; but with a characteristic value of  $\approx 7$  T along the central axis in the high-field region. The low-field region sits approximately 20 cm above the high-field region and has a maximum field of  $\approx 7$  T off-axis; but with a characteristic value of  $\approx 7$  T off-axis; but with a characteristic value of  $\approx 7$  T along the central axis in the high-field region. The low-field region and has a maximum field of  $\approx 7$  T off-axis; but with a characteristic value of  $\approx 7$  T off-axis; but with a

DMRadio-m³ detects the axion-induced  $J_{\rm eff}$  via a coaxial inductive pickup in the high-field region of the magnet [see Fig. 1(a)]. The geometry maximizes the coupling to  $J_{\rm eff}$ , while minimizing the pickup inductance  $L_{\rm PU}$ . Because it sits inside the magnetic field, it is challenging to make the pickup from lossless superconducting material. Instead, the pickup is made from oxygen-free, high-conductivity (OFHC) copper. The finite conductivity of copper sets an upper limit on the achievable quality factor of the LC resonator. At DMRadio-m³ frequencies and at temperatures < 100 mK, the anomalous surface resistance of copper is lower than at ~GHz frequencies and, combined with the large volume-to-surface ratio, the resonator goal of  $Q > 10^5$  is achievable.

While the inductive pickup can sit in the primary field without unacceptably degrading Q, the same does not extend to the tunable capacitor, which must be superconducting, or to the SQUIDs, which require an ultralow field to operate. These are instead placed in the low-field region above the coaxial pickup. To bridge the distance between the pickup and the low-field region without introducing excessive parasitic inductance, the coax funnels to a narrow neck coupled to the matching circuit above. To probe the mass range from 20 neV  $\lesssim m_a c^2 \lesssim 800$  neV, DMRadio-m³ uses a set of interchangeable coaxial pickups that are exchanged during the run of the experiment. The coaxial pickups are currently being designed, and they aim to keep  $c_{\rm PU}$  and  $V_{\rm PU}$  maximized over the entire search range while avoiding resonant modes that may short our signal.

The matching circuit must optimally couple to the pickup and convey the signal to the SQUID readout (see Fig. 2) and consists of the coupling transformer, a tunable capacitor, and the inductive coupling to the SQUID amplifier. Any additional inductance in the circuit that is not directly coupled to the signal flux reduces the coupled power. In the series transformer configuration of Refs. [48,49], the coupled axion power is maximized by minimizing the transformer inductance  $L_0 \ll L_{\rm PU}$ , which is technically challenging given the nominal  $L_{\rm PU} \lesssim 200$  nH. However, in the parallel transformer configuration of Fig. 2, axion signal power is maximized by making the transformer inductance  $L_0 \gg L_{\rm PU}$ , which can be

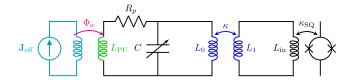


FIG. 2. Effective DMRadio-m³ circuit model.  $J_{\rm eff}$  is inductively coupled to a coaxial pickup,  $L_{\rm PU}$ , which, along with a tunable capacitor, C, forms the resonant circuit. An inductive transformer  $\kappa$  couples the signal to the SQUID amplifier. Loss in the readout is represented by the resistor  $R_p$ . On resonance,  $\nu_r \approx 1/(2\pi\sqrt{L_{\rm PU}C})$ , the circuit impedance drops, and axion power is more efficiently transferred to the receiver.

achieved more readily with a transformer inductance of  $L_0 \gtrsim 1 \ \mu H$ .

The baseline tunable capacitor consists of an array of parallel superconducting plates and sapphire dielectrics. The tuning must be able to scan the range  $10 \text{ pF} \lesssim C \lesssim 5 \text{ nF}$  with stepping precision. This can be achieved using a multiple-capacitor design with a coarse tuning to give a large capacitance swing to cover the full frequency range, and fine-tuning to give part-per-million (ppm) frequency precision. If the loss in the insertable sapphire dielectric proves to be too large, degrading the resonator Q to an unacceptable level, a fallback option includes using movable superconducting capacitor plates alone to adjust conductor overlap and resultant capacitance. The design of the tunable capacitor will build off the one currently under construction for DMRadio-50L, where many of these questions are being addressed.

Finally, the signal is amplified and read out through a phase-insensitive DC SQUID readout. To maximize the frequency-integrated axion sensitivity, the coupling transformer coefficient  $\kappa$  must maintain an optimal tradeoff between imprecision and backaction noise. This optimization is worked out for a simple series circuit in detail in Ref. [62]. For the sensitivity projections presented here, we target an amplifier noise level of  $\eta_A = 20$ —i.e., 20 times the SQL—which has been demonstrated in Ref. [63].

The optimal coupling  $\kappa$  is in general frequency dependent, reflecting the fact that at  $T \approx 20$  mK, the number of thermal noise photons  $n_T = (\exp(2\pi\hbar\nu/k_BT) - 1)^{-1}$  depends strongly on frequency, and it varies from  $n_T \approx 90$  at 5 MHz to  $n_T \approx 2$  at 200 MHz. Therefore, DMRadio-m³ utilizes a transformer capable of *in situ* variation of the coupling to maintain optimal matching to the readout amplifier.

The entire pickup structure is cooled to  $T \approx 20\,$  mK using a dilution refrigerator (DR), while the magnet is held at 4 K. DRs cooling payloads of similar heat capacity and volume to lower temperatures have been implemented previously [64,65]. DMRadio-m³ will be located in Building 750 at SLAC National Accelerator Laboratory, the former site of the SLD detector.

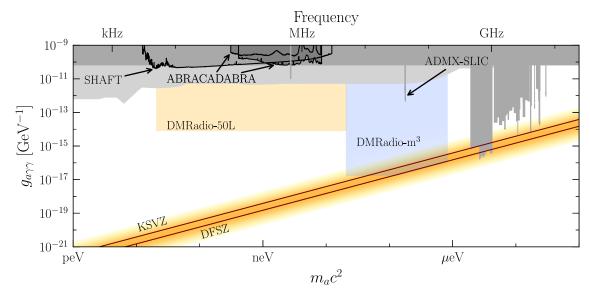


FIG. 3. Projected DMRadio-m<sup>3</sup> ADM sensitivity with a five-year scan, with projected sensitivity for DMRadio-50L, and existing bounds below 1  $\mu$ eV from ABRACADABRA-10 cm, SHAFT, ADMX-SLIC (spike around 200 neV), BASE (spike around 3 neV), and bounds from microwave cavities above 1  $\mu$ eV. DMRadio-m<sup>3</sup> targets DFSZ sensitivity above  $\approx$ 120 neV, and secondarily KSVZ above  $\approx$ 40 neV. Plot generated using code from Ref. [66].

## IV. SENSITIVITY

DMRadio-m³ will scan the full range 20 neV  $\lesssim m_a c^2 \lesssim$  800 neV in stages by sequentially stepping through a series of detector configurations, each with a different coaxial pickup. For the lowest-frequency coax  $c_{\rm PU} \approx 0.16$ , with the exact value depending on details of the final design.

The projected sensitivity for DMRadio-m<sup>3</sup> is shown in Fig. 3 alongside the sensitivity of the upcoming DMRadio-50L, which will be the subject of future publications. The shape of the sensitivity reach is set by the scan strategy, which aims to cover the full mass range with as much

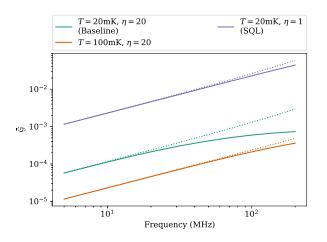


FIG. 4.  $\bar{\mathcal{G}}(\nu, k_B T, \eta_A)$  as a function of frequency for several choices of physical temperature, T, and amplifier noise  $\eta_A$ . The solid lines show the full evaluation, while the dotted lines show the linear behavior, which holds for the region where  $k_B T/\hbar \nu \gg \frac{1}{2} \eta_A$ , 1.

DFSZ sensitivity as achievable in five years of scan time, leading to the corner at  $\nu \approx 30$  MHz or  $m_a c^2 \approx 120$  neV.

An intriguing feature of the sensitivity is that much of the scan time is spent at lower masses above the DFSZ line. Above the 120 neV corner, the target  $g_{a\gamma\gamma}$  sensitivity increases  $\propto \nu$ , and the scan speed increases  $\propto \nu^3$  [see Eq. (5)]. The scan rate will be further enhanced because of the growth of  $\bar{\mathcal{G}}$ , due to the decreasing impact of thermal noise at higher frequencies—though this growth is slightly slower than  $\propto \nu_r$  and will be offset by a gradual decrease in SQUID sensitivity at higher frequency.

#### V. CONCLUSION

The axion is among the best motivated candidates to explain the DM abundance of the Universe. At present, the parameter space of ADM models is relatively unexplored. Recent advances in quantum sensors, magnet technology, and cryogenics have made searching the full ADM parameter space more feasible than ever. The region of ADM parameter space with  $m_a \lesssim 1~\mu \text{eV}$  is well motivated and particularly attractive due to its connection with GUT models.

In this paper, we have presented the baseline design and sensitivity reach of the DMRadio-m³ experiment, which uses a lumped-element approach to search for QCD ADM over a mass range of 20 neV  $\lesssim m_a c^2 \lesssim 800$  neV. This design is capable of probing at or below the KSVZ sensitivity over the full range and DFSZ sensitivity above 120 neV with a 5 yr scan time. This will make DMRadio-m³ a key component of the next generation of experimental searches for ADM.

Future upgrades to DMRadio-m<sup>3</sup> could moderately extend the DFSZ sensitivity below the 120 neV corner through the use of backaction-evading quantum sensors [67]. Future proposed experiments like DMRadio-GUT could probe DFSZ models to even lower masses through the use of beyond-SQL sensors and high-field, high-volume magnets [68].

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## APPENDIX: SCAN RATE CALCULATION

The general derivation of Eq. (5) and  $\bar{\mathcal{G}}$  can be found in Ref. [62]. Here we summarize the result for convenience. In general, the voltage across an inductive pickup,  $L_{\rm eff}$ , coupled to  $\mathbf{J}_{\rm eff}$ , will be proportional to the coupled energy  $U_{\rm DM}$  [62]

$$|V_{pp}^2| = 4 \left(\frac{c^4}{\hbar^2}\right) m_a^2 L_{\text{eff}} U_{\text{DM}}.$$
 (A1)

The coupled energy, defined as

$$U_{\rm DM} = k^2 \frac{g_{a\gamma\gamma}^2 \rho_{\rm DM}}{m_a^2} \frac{\hbar^3}{c\mu_0} \int |\mathbf{B}(\mathbf{x})|^2 dV, \qquad (A2)$$

gives a measure of the amount of energy coupled from the axion field into the pickup. The volume integral is performed over all space and is proportional to the total stored energy of the magnet. The dimensionless proportionality constant, k, is a geometric factor containing all the information about mutual coupling between the inductor and  $\mathbf{J}_{\rm eff}$ . This constant generalizes the  $C_{nml}$  form factor in a cavity haloscope. Energy conservation dictates that  $k^2 \leq \frac{1}{2}$  [59]. However, it is also clear that the voltage driven across an inductive element should go to zero as the driving frequency goes to zero  $(m_a \to 0)$ , and that therefore k should have a dependence on  $m_a$ . Given this, it is convenient to define a new dimensionless constant,  $c_{\rm PU}$ , that separates this mass dependence,

$$k^2 = \left(\frac{c}{\hbar}\right)^2 m_a^2 V_{\text{PU}}^{2/3} \left(\frac{B_0^2 V_{\text{PU}}}{\int |\mathbf{B}(\mathbf{x})|^2 dV}\right) c_{\text{PU}}^2, \quad (A3)$$

and is both frequency and scale invariant. This constant can be calculated explicitly in the MQS limit, when the Compton wavelength is large compared to the size of the detector. In this limit, we can use the relationship  $V=\partial\Phi/\partial t$  and write  $\tilde{V}_{pp}=2\pi\nu_a i\tilde{\Phi}_a$  in the frequency domain, where  $\Phi_a$  is the axion induced flux through the pickup. This flux can be extracted from the Biot-Savart law as

$$\begin{split} \tilde{\Phi}_{a} &= \frac{g_{a\gamma\gamma}\sqrt{\hbar c}\sqrt{2\rho_{\rm DM}}}{4\pi} \\ &\times \int_{A} dA \int dV' \hat{\mathbf{n}} \cdot \frac{\mathbf{B}_{0}(\mathbf{r}') \times (\mathbf{r} - \mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|^{3}}, \quad (A4) \end{split}$$

where the integral dA is taken over the area of the pickup A, and the integral dV' is performed over the shielding volume containing the coax. Combining Eqs. (A1), (A2), (A3), and (A4), we can write  $c_{\rm PU}$  in the MQS limit as

$$c_{\text{PU}}^{2} = \mu_{0} \frac{\left| \int dA \int dV' \hat{\mathbf{n}} \cdot \frac{\mathbf{B}_{0}(\mathbf{r}') \times (\mathbf{r} - \mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|^{3}} \right|^{2}}{2(4\pi)^{2} B_{0}^{2} V_{\text{PU}}^{5/3} L_{\text{eff}}}.$$
 (A5)

The scale invariance can be seen explicitly by noting the scaling  $L_{\rm eff} \approx L_{\rm PU} \propto V^{1/3}$  for a constant geometry. Typical values for the DMRadio-m<sup>3</sup> geometry are  $c_{\rm PU} \approx 0.1$ –0.2.

This formulation also generalizes beyond the validity of the lumped element approximation. At frequencies where the Compton wavelength becomes comparable to the size of the detector,  $2\pi\hbar/m_ac \approx V_{\rm PU}^{-1/3}$ , the coaxial pickup no longer behaves purely inductively, and we must incorporate its full complex impedance into the calculation:  $2\pi i\nu L_{\rm PU} \rightarrow Z_{\rm PU}(\nu)$ . We can Taylor-expand any resonant circuit's impedance around the resonant frequency to find an effective inductance.

$$Z(\nu) \approx R_{\rm eff} + 4\pi i L_{\rm eff}(\nu - \nu_r) + O((\nu - \nu_r)^2). \tag{A6}$$

This expansion is generally valid over frequency bandwidths small compared to the resonance frequency—i.e., for small fractional detunings<sup>1</sup>  $\Delta \ll 1$ .

The resonant enhancement of the circuit comes directly from its impedance  $Z(\nu)$ 

$$|\tilde{I}_{\text{sig}}|^2 = \frac{|\tilde{V}_{pp}|^2}{|Z(\nu)|^2}.$$
 (A7)

<sup>&</sup>lt;sup>1</sup>A more complete discussion of lumped element detectors beyond the validity of the MQS approximation is in preparation [69].

For a generic RLC circuit,  $Z(\nu) = R + i(2\pi\nu L + (2\pi\nu C)^{-1})$ , we can evaluate

$$\frac{1}{|Z(\nu)|^2} = \frac{Q^2}{4\pi^2 \nu_r^2 L^2 \left(1 + Q^2 \frac{\nu_r^2}{\nu^2} \left(\frac{\nu^2}{\nu_r^2} - 1\right)^2\right)}$$

$$\approx \frac{Q^2}{4\pi^2 \nu_r^2 L^2 (1 + 4Q^2 \Delta^2)}, \tag{A8}$$

where  $\nu_r=(2\pi\sqrt{LC})^{-1}$  and  $Q=\sqrt{L/CR^2}$ , and the approximation holds for  $\nu\approx\nu_r$ . We see the Lorentzian behavior of the resonator stems directly from the impedance of the readout circuit.

The noise power  $|\tilde{I}_N(\nu)|^2$  can be expressed in terms of a current noise power spectral density at the input coil of the readout SQUID,

$$S_{II}^{\text{tot}}(\nu) = \frac{|\tilde{I}_N(\nu)|^2}{\Delta \nu}.$$
 (A9)

This noise power can be decomposed into thermal, amplifier, and vacuum components:

$$\begin{split} S_{II}^{\text{tot}}(\nu) &= 8\pi\hbar\nu \bigg( n_T + \frac{1}{2} \bigg) \frac{\text{Re}[Z(\nu)]}{|Z(\nu)|^2} \\ &+ S_{II}^{\text{Imp}} + \frac{S_{VV}^{\text{BA}}}{|Z(\nu)|^2}, \end{split} \tag{A10}$$

where the first term in the parenthesis corresponds to the number of thermal noise photons  $n_T(\nu,k_BT)=(\exp(2\pi\hbar\nu/k_BT)-1)^{-1}$  at physical temperature T. DMRadio-m³ targets a physical temperature of T=20 mK, corresponding to  $n_T\approx 90$  noise photons at 5 MHz and  $n_T\approx 2$  noise photons at 200 MHz. The  $\frac{1}{2}$  corresponds to vacuum noise, intrinsic to any phase-insensitive measurement.  $S_{II}^{Imp}$  is the amplifier imprecision noise, expressed in terms of current noise at the amplifier input, and  $S_{VV}^{BA}$  is the amplifier backaction noise, expressed as a voltage source at the amplifier input, and both are independent of frequency in this form. Equation (A10) demonstrates the different spectral behavior of the various noise sources. The thermal, vacuum, and backaction noise are all shaped by the resonator Lorentzian, while the imprecision noise has a spectrally flat distribution. In

practice, a DC-SQUID will have an additional type of noise term,  $S_{IV}^{\rm corr}$ , that defines correlations between the imprecision and backaction noise [70,71]. These correlations complicate the optimization and are included in our sensitivity calculation, but do not qualitatively change the approach and so are omitted here for simplicity.

The amplifier noise parameter  $\eta_A$  can be written in terms of these noise powers as

$$\eta_A = \frac{\sqrt{S_{II}^{\text{Imp}} S_{VV}^{\text{BA}}}}{2\pi\hbar\nu}.$$
 (A11)

At the SQL,  $\eta_A = 1$ . For DMRadio-m<sup>3</sup>, the amplifier noise target is  $\eta_A = 20$ , including the correlated noise that we have omitted here. This corresponds to  $n_A = \eta_A/2 = 10$  added noise photons.

The amplifier noise parameter  $\eta_A$  depends on the amplifier imprecision and backaction noise, as well as  $\kappa$  coupling, in Fig. 2, which regulates the tradeoff between the two. In particular,  $S_{II}^{Imp} \propto \eta_A/\kappa^2$ , while  $S_{VV}^{BA} \propto \eta_A \kappa^2$ . A stronger coupling increases the backaction noise and decreases the input referred imprecision noise. Because of the different spectral responses of these two noise terms, the coupling  $\kappa$  can be optimized to give the fastest possible scan rate. For a careful and extensive analysis of this optimization, including noise correlations, see Ref. [62]. But the resulting effect on the scan rate can be written in terms of a single parameter shown in Fig. 4

$$\bar{\mathcal{G}}(\nu_r, \bar{\alpha}, k_B T, \eta_A) = \frac{\bar{\alpha}}{[\bar{\alpha}^2 + 2(2n_T + 1)\bar{\alpha} + \eta_A^2]^{3/2}},$$
 (A12)

where

$$\bar{\alpha} = \frac{2\eta_A^2}{2n_T + 1 + \sqrt{(2n_T + 1)^2 + 8\eta_A^2}}.$$
 (A13)

In the limit where  $n_T \gg \frac{1}{2}\eta_A$ , 1, or equivalently  $k_B T/\hbar \nu \gg \frac{1}{2}\eta_A$ , 1,  $\bar{\mathcal{G}}$  has an approximately linear dependence on  $\nu$ :

$$\bar{\mathcal{G}} \approx \frac{2\pi\hbar\nu}{6\sqrt{3}k_BT\eta_A}, \quad \frac{k_BT}{\hbar\nu} \gg \frac{1}{2}\eta_A, 1.$$
 (A14)

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