

Modeling spatiotemporally varying protein-protein interactions in CyLaKS, the Cytoskeleton Lattice-based Kinetic Simulator

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Interaction of cytoskeletal filaments, motor proteins, and crosslinking proteins drives important cellular processes such as cell division and cell movement. Cytoskeletal networks also exhibit nonequilibrium self-assembly in reconstituted systems. An emerging problem in cytoskeletal modeling and simulation is spatiotemporal alteration of the dynamics of filaments, motors, and associated proteins. This can occur due to motor crowding, obstacles along the filament, motor interactions and direction switching, and changes, defects, or heterogeneity in the filament binding lattice. How such spatiotemporally varying cytoskeletal filaments and motor interactions affect their collective properties is not fully understood. We developed the Cytoskeleton Lattice-based Kinetic Simulator (CyLaKS) to investigate such problems. The simulation model builds on previous work by incorporating motor mechanochemistry into a simulation with many interacting motors and/or associated proteins on a discretized lattice. CyLaKS also includes detailed-balance in binding kinetics, movement, and lattice heterogeneity. The simulation framework is flexible and extensible for future modeling work, and is available on GitHub for others to freely use or build upon. Here we illustrate the use of CyLaKS to study long-range motor interactions, microtubule lattice heterogeneity, motion of a heterodimeric motor, and how changing crosslinker number affects filament separation.

I. INTRODUCTION

The cellular cytoskeleton performs important biological roles [1], including mitosis [2] and cytokinesis [3] in cell division and cell movement [4, 5]. Key cytoskeletal components include filaments, motor proteins, and other associated proteins such as crosslinkers. Actin and microtubules are the best-studied filaments [1]. Assemblies of actin and myosin motors participate in cytokinesis [3, 6], cell motility [7–9], and muscle contraction [10–12]. Networks of microtubules, kinesin motors, and dynein motors function in mitotic spindle assembly [2, 13–16] and chromosome segregation [17–20], and beating of cilia and flagella [21–23]. The remarkable ability of the cytoskeleton to dynamically reorganize and exert force is not fully understood [1, 4]. Theory and simulation are used to study how basic interactions of filaments, motors and associated proteins can lead to the variety of cytoskeletal structures and dynamics found in cells and reconstituted systems [24–34].

A particular challenge in cytoskeletal theory and modeling is how to study motor and crosslinker behavior that is spatiotemporally altered. For example, kinesin motor activity can change in dense regions along microtubules [35, 36] in ways that differ for different types of motors [36]. These effects may be in part due to short-range interactions between motors [37, 38]. Additionally, patchy obstacles created by other proteins binding to the microtubule lattice can alter kinesin and dynein movement [39]. Kinesins that regulate microtubule length and dynamics typically show altered motility at microtubule ends [40–49]. Some kinesin-5 motors can switch their direction of motion along microtubules [50–54], an effect that is not well understood but may be regulated by crowding on the microtubule lattice [54]. Molecular crowders in solution can inhibit the diffusion of kinesin-1 motor domains and slow stepping [55]. All of these examples illustrate how motor stepping can be altered by the local spatial environment.

In addition, microtubules themselves can have significant spatial and temporal variation. Microtubules can be heterogeneous at the tubulin dimer level if they contain a mixture of tubulin isoforms or are post-translationally modified [56–58]. Motor and non-motor microtubule associated proteins (MAPs) appear to alter microtubule lattice structure and induce defects [59–62]. Such changes can alter the binding of kinesin-1 motors [63, 64], an effect that might be explained by elastic anisotropy [65]. Our recent work found that long-range interactions between kinesin-4 motors can explain both changes in motor processivity and velocity at low density and dense accumulation of motors and microtubules ends [34]. How spatiotemporally varying cytoskeletal filaments and motor interactions affect collective motor behavior remains incompletely understood.

Several methods and packages for molecular simulation of filaments and motors are widely used, including Cytosim [66], MEDYAN [67], AFINES [68], and others [69]. These packages were designed for cytoskeletal assemblies, typically dozens of filaments (or more) with associated proteins that form a larger structure or network. As a result, the models are coarse-grained to be tractable for these systems. Effects typically neglected in current software packages include steric exclusion between proteins bound to filaments, explicit modeling of discrete binding sites, and mechanochemistry such as the stepping cycle of motors. Here we build on these methods and develop the Cytoskeleton Lattice-based Kinetic Simulator (CyLaKS)[70]. CyLaKS is designed to facilitate modeling and simulation of cytoskeletal filaments (represented as long, thin rods with a lattice of binding sites for motors and other proteins),

motor proteins, and other filament-binding proteins for problems in which spatiotemporal variation of motor or filament properties is significant. CyLaKS uses kinetic Monte Carlo-Brownian dynamics (kMC-BD) methods [71–79]. A primary goal in developing CyLaKS was to build on previous work modeling the mechanochemical cycle of individual motor proteins [80–86] by incorporating the motor ATP hydrolysis cycle in a simulation in which many motors can interact along filaments. Explicitly modeling motor mechanochemistry allows results such as nontrivial force-velocity and force-processivity relations [87]. In addition, we implemented detailed-balance in binding kinetics and movement for a physically motivated treatment of force-dependent protein binding/unbinding and diffusion. Finally, we have structured the simulation in a flexible, extensible framework, making it straightforward to elaborate the model to include spatially varying effects such as heterogeneity in the lattice and short- and long-range interactions between motors.

Here we describe the model components and simulation techniques, then illustrate how CyLaKS can be used to study long-range motor interactions, filaments with heterogeneous binding lattices, motion of a heterodimeric motor, and filament separation due to force from crosslinkers. Examples of these simulations are available as demos on the CyLaKS GitHub page[70]. Additionally, CyLaKS is hosted on Dockerhub to facilitate broad access without the requirement that the code be locally compiled.

II. MODEL AND SIMULATION

Building on our previous work, CyLaKS implements Brownian dynamics to model physical movements in solution and a kinetic Monte Carlo algorithm to model state changes (such as protein binding and unbinding) and chemical reactions (such as ATP hydrolysis) [71–79]. Proteins in CyLaKS are not modeled while free in solution, i.e., when not bound to a filament, and therefore do not undergo Brownian dynamics. Similarly, filaments in CyLaKS currently do not undergo any kind of state change, e.g., dynamic instability, and therefore are not subject to kinetic Monte Carlo. Thus, the BD substep only affects filaments and the kMC substep only affects proteins. However, this is straightforward to extend in the future. Each simulation timestep includes first a kinetic Monte Carlo (kMC) substep, then a Brownian dynamics (BD) substep. The simulation alternates between these substeps until it has reached the specified total run time.

We implement the kMC substep with a hybrid tau-leaping algorithm [88], which samples from the binomial and Poisson distributions to predict the number of kMC events that will occur in a timestep. The binomial distribution is used for events with a constant probability throughout the simulation, such as ATP hydrolysis by a motor head or protein binding (these probabilities are constant in time and identical for every site in the absence of long-range coupling) [72]. For events with a probability that varies, we sample the Poisson distribution. This can occur, for example, when protein unbinding is force dependent, or if long-range motor coupling gives different binding kinetics to each lattice site. We compute the pairwise partition function of each object that an event can act on to calculate the average number of events in the timestep [72]. We then sample the Poisson distribution to choose the number of events that occur. Events are executed in random order on randomly selected members of the appropriate population. Multiple events can target the same object, e.g., binding of the second head and unbinding of the first head for a protein with one head bound. We enforce that no two events can act on the same object in the same timestep, a good approximation if the timestep is sufficiently small. Each kMC substep implements the following algorithm:

1. Loop over all active objects and sort into appropriate populations.
2. If appropriate, check equilibration status of each protein species. This is done by finding the average number of proteins bound for each species in a time window t_c . If the change in number bound between two windows is less than twice their standard deviations added in quadrature, the protein species is considered equilibrated. Once all species are equilibrated, the simulation is considered equilibrated.
3. Sample the appropriate statistical distribution for each possible event. If the event has a constant probability, use the binomial distribution. If the event has a probability that can change in space or time, sum all relevant pairwise partition functions and use them to sample the Poisson distribution.
4. If two or more events target the same object, discard at random until only one remains. The probability of each event determines the relative weight when sampling to discard.
5. Execute each event in a random order on random members from the appropriate population.

The position of filaments are updated during the BD substep. Due to the relatively large net force that can act on filaments, we run N_{BD} iterations for every kMC iteration that runs. This allows the filaments to reach mechanical equilibrium given the positions of bound motors/crosslinker. To do this, we use a smaller timestep $t_{BD} = dt/N_{BD}$ during the substep. The BD substep implements the following algorithm:

1. Update associated protein positions.
2. Sum to find the net systematic (non-random) force and torque acting on each filament.
3. Calculate the translational displacement of each filament's center of mass due to the systematic force. Movement is projected into parallel and perpendicular directions relative to the long axis of the filament.
4. Calculate the rotational displacement of each filament's orientation vector due to the systematic torque. The direction of this displacement is always perpendicular to the long axis of the filament.
5. Calculate the random center of mass displacements and random reorientation due to thermal noise.
6. Apply the displacements and update filament positions.

CyLaKS is written in C/C++ and uses a combination of templated functions and class inheritance to achieve modularity while retaining reasonable performance. Basic molecular components such as binding and catalytic heads, linear and angular springs, and discrete binding sites all inherit from a common *Object* class. This allows us to take advantage of *class polymorphism*, a property of C++ classes that allows containers such as vectors or arrays to hold different data structures, as long as they inherit from each other. Additionally, we can define the same function differently for different inheritance classes. Using these two properties together allows us to hold all active molecular species in one container, then iterate through it and call an *Update* function for each member that will do different things depending on the species it belongs to. This structure decouples the main kMC-BD algorithm from the details of the species. This allows for the addition of new species or mechanisms without modifying the majority of the code. Furthermore, classes that are specialized versions of others inherit directly from the more general class by design; for example, a catalytic head is a specialized version of a binding head. This design allows us to re-use common code between classes while adding additional components needed by the specialized class. This improves code readability and ease of validation since algorithms only need to be written once despite how many times they are re-used.

To increase overall performance, proteins in CyLaKS are not explicitly modeled while in solution, i.e., when all binding heads are unbound. They are instead drawn from a reservoir list when they first bind to an object. Additionally, unbound springs and/or unbound heads of partially bound proteins are not explicitly modeled. We assume their motion averages out due to diffusion when using distances to calculate kinetic rates. Finally, all interactions (springs, long-range potentials, etc) have a cutoff distance to avoid modeling low-probability events that would largely waste computational resources.

A. Filaments

The current filament model in CyLaKS is based on a microtubule idealized as a rigid single protofilaments where each tubulin dimer corresponds to a discrete binding site on a 1-D lattice (Fig. 1a). Binding sites are modeled individually and the data structure tracks each site's lab-frame position, neighboring sites, and index in the 1-D lattice array of the parent filament. As a result, extensions to the filament model to incorporate a semi-flexibility with rigid sub-units that can hinge at their joints would be straightforward. Similarly, the data structure allows us to easily expand the 1-D lattice to greater dimensions. CyLaKS thus could model both actin filaments and multi-protofilament microtubules relatively easily.

We implement the Brownian dynamics algorithm of Tao et al. [89], as in our previous work [71–79]. The microtubule center-of-mass position $\vec{r}$ evolves according to

$$\vec{r}(t + \delta t) = \vec{r}(t) + \boldsymbol{\Xi}^{-1}(t) \cdot \vec{F}_S(t) \delta t + \delta \vec{r}, \quad (1)$$

where $\boldsymbol{\Xi}^{-1}$ is the inverse friction tensor of the filament, $\vec{F}_S$ is the deterministic (systematic) force acting on the filament, $k_B T$ is the thermal energy, and δt is the timestep. Diffusion occurs due to the random displacement $\delta \vec{r}$, which is anisotropic and Gaussian-distributed with variance $2k_B T \boldsymbol{\Xi}^{-1}(t) \delta t$. The inverse friction tensor $\boldsymbol{\Xi}^{-1}(t)$ is

$$\boldsymbol{\Xi}^{-1}(t) = \gamma_{\parallel}^{-1} \hat{u}(t) \otimes \hat{u}(t) + \gamma_{\perp}^{-1} [\mathbf{I} - \hat{u}(t) \otimes \hat{u}(t)] \quad (2)$$

where $\gamma_{\parallel}$ and $\gamma_{\perp}$ are the translational friction coefficients for motion parallel and perpendicular to the axis of the filament, respectively, and $\hat{u}(t)$ is the filament orientation vector at time t . The operators $\hat{u}(t) \otimes \hat{u}(t)$ and $\mathbf{I} - \hat{u}(t) \otimes \hat{u}(t)$ project onto directions that are parallel and perpendicular to the filament, respectively.

Filament rotation is described by the time evolution of the orientation vector $\hat{u}$,

$$\hat{u}(t + \delta t) = \hat{u}(t) + \gamma_r^{-1} \vec{T}_S(t) \times \hat{u}(t) \delta t + \delta \hat{u} \quad (3)$$

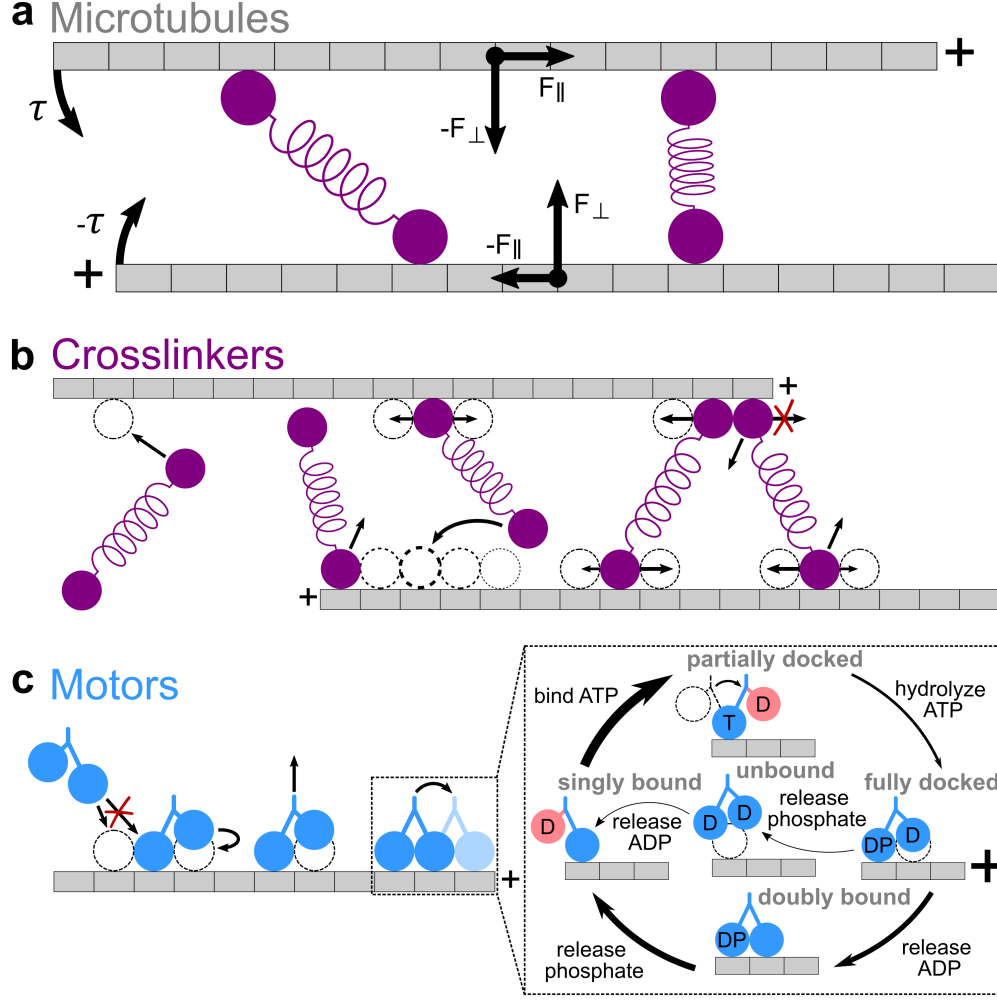


FIG. 1. CyLaKS model components (a) Microtubules. Microtubules (filaments) are modeled as single protofilaments, where each tubulin dimer corresponds to a discrete site on a 1-D lattice. Each microtubule has a plus- and minus-end. Associated proteins exert force and torque on filaments, causing 2-D translation and rotation about each filament's center of mass. (b) Crosslinkers. Each crosslinker head can independently bind to, unbind from, and diffuse on the filament lattice. The relative probability of the second head binding to each sites is represented by dotted circles of different thickness. The relative probability of heads diffusing is represented by arrow length. Steric exclusion prevents more than one crosslinker head from occupying the same binding site. Crosslinker heads cannot diffuse off filament ends. (c) Motor proteins. Motors can bind to, unbind from, and step toward the plus-ends of filaments. Inset, mechanochemical cycle. Motor heads can be bound to ADP (D), ATP (T), ADP-Pi (DP), or nothing (empty). Red coloring labels head which cannot bind to the microtubule due to internal tension. Arrow thickness represents the relative probability of each transition. Steric exclusion prevents more than one motor head from occupying the same binding site.

where γ_r is the orientational friction coefficient of the filament, $\vec{T}_S(t)$ is the deterministic torque on the filament about its center of mass at time t , and $\delta\hat{u}$ is a random reorientation that is anisotropic and Gaussian-distributed with variance $2k_B T \gamma_r^{-1} [\mathbf{I} - \hat{u}(t) \otimes \hat{u}(t)]$.

The filament friction coefficients are

$$\gamma_{\parallel} = \frac{2\pi\eta L}{\ln(L/2R)}, \quad (4)$$

$$\gamma_{\perp} = 2\gamma_{\parallel}, \quad (5)$$

$$\gamma_r = \frac{\pi\eta L^3}{3[\ln(L/2R) - 4/5]}, \quad (6)$$

where η is the viscosity of the fluid, L is the length of the filament, and R is the radius of the filament [90].

B. Binding kinetics

Protein binding to filaments has an associated free-energy change, which includes the binding energy and the energy in a connected spring if it is stretched or compressed. The energy change upon binding is denoted as $\Delta U_0 = U_{\text{bound}} - U_{\text{unbound}}$. Then the association (binding) and dissociation (unbinding) rates can be written

$$k_a = k_a^0 \exp[-\beta(1 - \lambda)\Delta U_0], \quad (7)$$

$$k_d = k_d^0 \exp[\beta\lambda\Delta U_0], \quad (8)$$

where $\beta = 1/k_B T$ is the inverse thermal energy and λ a dimensionless constant with $0 \leq \lambda \leq 1$. Here λ weighs how strongly the interaction affects binding or unbinding. A value of $\lambda = 1/2$ sets the energy dependence of binding equal to that of unbinding and is typically used as a baseline in modeling, absent other information [91]. Lower values of λ mean that the interaction affects binding more than unbinding, and increasing λ means that the interaction affects unbinding more than binding. If $\lambda = 0$ or $\lambda = 1$, the interaction affects only binding and unbinding, respectively. We typically assume $\lambda = 1/2$ in the absence of experimental measurements. Note that the equilibrium behavior described by the dissociation constant $K_d = k_d/k_a = K_d^0 \exp\{2\beta\Delta U\}$ is independent of λ .

The change in free energy upon binding can depend on the state of the system, e.g., when proteins cooperatively bind, the effective free energy of the bound state depends on nearby proteins that are also bound. If such a state change makes the new binding-energy difference $U_{\text{bound}} - U_{\text{unbound}} = \Delta U$, the association and dissociation rates change accordingly. As an example, consider an attractive cooperative interaction that lowers the free energy of the bound state. This will lower ΔU relative to ΔU_0 in Eqs. 7 and 8, resulting in the association rate k_a increasing and dissociation rate k_d decreasing.

C. Crosslinkers

Non-motor crosslinking proteins (crosslinkers) are modeled as two independent binding heads connected by a linear spring (Fig. 1b). We assume that each head binds separately, so crosslinkers bind one head (entering the one-head-bound or singly bound state) before the second (entering the two-heads-bound or crosslinking state). As currently implemented, we require that the second head cannot bind to the same filament as the first. Additionally, when in the two-head-bound state, each crosslinker head diffuses and unbinds independently. Crosslinkers are not explicitly modeled while in solution (when both heads are unbound), and are drawn from a reservoir list when their first head binds to an unoccupied site. This occurs at rate $Nk_{\text{on}}c_{\text{bulk}}$, where N is the number of unoccupied sites available, k_{on} the per-site crosslinker association rate, and c_{bulk} is the concentration of unbound crosslinkers in solution. We assume an infinite reservoir of crosslinkers are available so that c_{bulk} is constant throughout the simulation. Singly bound crosslinkers can unbind at rate $k_{\text{off},1}$, or diffuse to adjacent unoccupied sites at rate $2D_1/\Delta^2$, where D_1 is the one-head-bound diffusion coefficient and Δ is the length of a lattice site (approximately 8 nm for tubulin dimers).

Singly bound crosslinkers can also form crosslinks by binding their second head to unoccupied sites on adjacent filaments. At physiological concentrations, this occurs at a much higher rate than the initial binding of the first head from solution [92, 93]. We assume the binding chemistry (and thus k_{on}) of the first and second head with respect to filaments are identical since crosslinkers are homodimers [45]. The second head is constrained near the adjacent filament by the already-bound first head, which results in the observed higher binding rate. To model this, we implement an *effective concentration* for the second head. The second head then binds to unoccupied sites on adjacent microtubules at a per-site rate of $k_{\text{on},2}^*c_{\text{eff}}$, where $k_{\text{on},2}^*$ is the energy-dependent on-rate of the second head (which changes based on the spring extension required to reach a given site) and c_{eff} is the effective concentration of the second head. In most cases this effective concentration is not experimentally measured, but we can estimate it as outlined in the *Parameters* section.

Once a crosslink forms, the crosslinker spring energy is

$$E_s = \frac{1}{2}k_s(r - r_0)^2, \quad (9)$$

where k_s is the spring constant, r the length of the crosslinker as currently bound, and r_0 the unperturbed length. We expect crosslinker states with higher energy to form less often and unbind more frequently once they form. This behavior is reflected in the kinematic rates of crosslinkers via the Boltzmann factors described by Eqs. 7 and 8. In this scenario, *association* corresponds to the second head binding and forming a crosslink, and *dissociation* corresponds to the second head unbinding and reverting the crosslinker to the one-head-bound state. Following this, we can obtain

the energy-dependent binding rate $k_{\text{on},2}^*$ and unbinding rate k_{off}^* ,

$$k_{\text{on},2}^* = k_{\text{on}} \exp\left[-\frac{1}{4}\beta k_s(r - r_0)^2\right], \quad (10)$$

$$k_{\text{off},2}^* = k_{\text{off},2}^0 \exp\left[\frac{1}{4}\beta k_s(r - r_0)^2\right], \quad (11)$$

where we have set $\lambda = 1/2$ and used $\Delta U = E_s$ given by Eq. 9. As discussed earlier, we use the same k_{on} for both the first and second head binding since crosslinkers are homodimers [45]. However, we do not rule out the possibility of some mechanism that may alter the off-rate when both heads are bound. Thus we use a separate base off-rate $k_{\text{off},2}^0$ for two-head-bound crosslinkers.

Each head of two-head-bound crosslinkers diffuse independently with a diffusion coefficient D_2^0 that is scaled by the appropriate Boltzmann factor for the change in spring extension during a diffusive step. A diffusive step that stretches/compresses the spring is energetically unfavorable and occurs at lower rate, while a diffusive step that relaxes the spring stretch/compression is energetically favorable and occurs at higher rate. Therefore, in this case, we consider *association* to be diffusing towards rest and *dissociation* to be diffusing away from rest, giving us

$$D_{2,\text{to}} = D_2^0 \exp\left[-\frac{1}{2}\beta \Delta E_{s,\text{to}}\right], \quad (12)$$

$$D_{2,\text{fr}} = D_2^0 \exp\left[\frac{1}{2}\beta \Delta E_{s,\text{fr}}\right], \quad (13)$$

where $\Delta E_{s,\text{to}}$ denotes a change in energy of a step that relaxes the spring, and $\Delta E_{s,\text{fr}}$ is the change in energy of a step that extends/compresses the spring. To obtain Eqs. 12 & 13, we have again set $\lambda = 1/2$, i.e., set the energy-dependence equal between diffusing away from spring rest and diffusing towards spring rest.

Steric interactions prevent two crosslinker heads from occupying the same lattice site.

D. Motors

CyLaKS was designed to facilitate studies of many interacting motors while also incorporating molecular details such as stepping via a mechanochemical cycles[80–86]. We implement motors as two coupled catalytic heads. Each head can bind to and unbind from the filament as a passive binding head would. However, they can also bind a ligand and transition through a nucleotide hydrolysis cycle based on the kinesin-1 stepping cycle (Fig. 1c) [87, 94–99]. Details of this cycle may differ between motor species, but any basic mechanochemical cycle that facilitates asynchronous binding and unbinding of two binding heads can lead to similar stepping behavior [96, 100].

Like crosslinkers, motors are not explicitly modeled while in solution (when both heads are unbound). Motor heads bind to filaments at rate $Nk_{\text{on}}c_{\text{bulk}}$, where N is the number of unoccupied sites available, k_{on} the per-site motor-microtubule association rate, and c_{bulk} the motor concentration in solution. As with crosslinkers, only one head can bind at a time. Furthermore, we assume that the first motor head to bind is always the leading head, i.e., closer to the plus-end for plus-end-directed motors. The biochemical states possible for each motor head are bound to ATP, APP, ADP·Pi, or no ligand (empty).

We assume that any motor not attached to a microtubule has both motor heads bound to ADP. Upon binding to the microtubule, the motor head releases ADP, becoming empty. While empty or ATP-bound, motor heads are strongly bound and cannot unbind from the microtubule. ATP binding to the empty head at rate k_{ATP} induces a conformational change that swings the second (unbound) head forward, partially docking the motor. The first (bound) head then hydrolyzes ATP to ADP·Pi at rate k_{hydro} , which fully docks the motor. Next, the motor can either unbind its first (bound) head at rate $k_{\text{off},1}$, which terminates its run, or bind its second (unbound) head at rate $k_{\text{on}}c_{\text{eff}}$, continuing its run. The ratio between $k_{\text{off},1}$ and $k_{\text{on}}c_{\text{eff}}$ determines how many steps occur on average before the motor unbinds. While the motor is doubly bound, the rear head unbinds with rate $k_{\text{off},2}$ and the front head cannot unbind. Upon rear head unbinding, the motor has completed one ATP hydrolysis cycle and moved forward one site.

Both the run length and velocity of motors depend on the force being applied, e.g., from an optical trap or molecular load [87]. Andreasson et al. found that this force dependence could be properly accounted for by a 3-state model, where ATP binding and hydrolysis is condensed into one step. The rate of ATP binding while in the singly bound state is modified as

$$k_{\text{ATP}} = \begin{cases} k_{\text{ATP}}^0 \exp[\beta F_{\text{ext}} \delta_{\text{ATP}}], & F_{\text{ext}} < 0 \\ k_{\text{ATP}}^0, & F_{\text{ext}} \geq 0 \end{cases} \quad (14)$$

where F_{ext} is the external force acting on the motor and δ_{ATP} is a distance parameter that controls the strength of force dependence. External force is negative if applied in the opposite direction of motor stepping and positive if in the stepping direction. The rate of unbinding while in the fully docked state is modified as

$$k_{\text{off},1} = \begin{cases} k_{\text{off},1}^- \exp[-\beta F_{\text{ext}} \delta_{\text{off},1}^-], & F_{\text{ext}} < 0 \\ k_{\text{off},1}^+ \exp[\beta F_{\text{ext}} \delta_{\text{off},1}^+], & F_{\text{ext}} \geq 0 \end{cases} \quad (15)$$

where $\pm$ superscripts correspond to assisting and hindering loads, respectively. In this form, forces always act to enhance the unbinding rate of motors while in the docked state. However, this enhancement does not necessarily have to be symmetric. In our simulations, we typically set $k_{\text{off},1}^+ = k_{\text{off},1}^-$ and $\delta_{\text{off},1}^+ = \delta_{\text{off},1}^-$. Finally, we also modify the rear-head unbinding rate of doubly bound motors as

$$k_{\text{off},2} = k_{\text{off},2}^0 \exp[\beta(F_{\text{ext}} + F_{\text{int}})\delta_{\text{off},2}], \quad (16)$$

where F_{int} is the internal necklinker tension of the motor, estimated to be approximately 26 pN for kinesin-1 [87].

E. Cooperative binding and movement

CyLaKS can model both short- and long-range cooperative interactions between motors and crosslinkers bound to a filament [34]. Based on previous work [38], we implemented a model of short-range binding cooperativity as an attractive nearest-neighbor interaction. The interaction energy when one motor (or crosslinker) head binds near an adjacent bound head is $-\epsilon k_{\text{B}}T$, assuming an interaction range of one lattice site. When implementing this interactions, we set $\lambda = 1$, leading to

$$k_{\text{on}} = k_{\text{on}}^0, \quad (17)$$

$$k_{\text{off}} = k_{\text{off}}^0 \exp[-n\epsilon], \quad (18)$$

where $n = 0, 1, 2$ is the number of neighbors. Note that Eqs. 17 & 18 do not differ for singly and doubly bound unbinding rates because both are affected in the same way.

As currently implemented in CyLaKS, each type of protein (crosslinkers and motors) can have a different value of ϵ for interactions with proteins of the same type or different types. We assume that binding heads belonging to the same protein (for example, the two binding heads of a given motor) do not interact with each other.

Long-range binding cooperativity between proteins is currently modeled as an attractive potential $E(x - x_m)$, where

$$E(x - x_m) = \begin{cases} -E_0 \left[1 - \left(\frac{x - x_m}{D} \right)^2 \right], & |x - x_m| \leq D \\ 0, & |x - x_m| > D \end{cases} \quad (19)$$

which is negative up to the cutoff distance D and zero beyond that distance. Here x is the distance along lattice, x_m is the position of the motor that is inducing the interaction, and E_0 is the strength of the interaction energy. The curvature of the potential is determined by $2E_0/D^2$, and we currently assume that the interaction induced by multiple motors can superimpose up a maximum of E^* . We set $\lambda = 1/2$ in Boltzmann factors involving long-range cooperativity, giving

$$k_{\text{on}} = k_{\text{on}}^0 \exp \left[\frac{1}{2} \beta \min \{ \sum_i -E(x - x_i), E^* \} \right], \quad (20)$$

$$k_{\text{off}} = k_{\text{off}}^0 \exp \left[-\frac{1}{2} \beta \min \{ \sum_i -E(x - x_i), E^* \} \right], \quad (21)$$

where the sum is over bound motors. Note that Eqs. 20 & 21 do not differ for singly and doubly bound unbinding rates because both are affected in the same way.

Based on fitting to our collaborators' data, we believe the long-range attractive interaction (Eq. 19) also affects the motor stepping cycle [34]. There are many possible mechanisms for how a long-range interaction could achieve this. We choose necklinker tension as a potential candidate, extending on the model proposed by Andreasson et al. for kinesin-1 [87]. In their model, the necklinker between the two motor heads can exert ~ 26 pN of tension when motors are doubly bound. This tension affects kinematic rates of transitions in the motor stepping cycle, and by changing the necklinker tension, the rates change as well. We considered a model in which the long-range interaction can reduce the internal necklinker tension of doubly bound motors. This allows us to introduce a new transition in the model

(doubly bound to partially docked) that has a negligible probability of occurring under normal conditions [34]. This transition occurs with rate

$$k_{\text{ATP},2} = k_{\text{ATP}}^0 \exp[-\beta(F_{\text{int}} + F_{\text{ext}})\delta_{\text{ATP}}], \quad (22)$$

where δ_{ATP} is a distance parameter that controls how strongly front-head ATP binding is affected by force. If ATP binds to the front head, the rear head detaches from the microtubule and swings forward, skipping the singly bound state. Using parameters previously estimated for kinesin-1 (Table I), the doubly bound off- and ATP-binding rates are 2375 and $1.1810 \times 10^{-9} \text{ s}^{-1}$, respectively. As necklinker tension (F_{int}) is reduced by the long-range interaction (Eq. 19), the doubly bound unbinding rate (Eq. 16) decreases and the doubly bound ATP-binding rate (Eq. 22) increases. We implement this reduction of tension by multiplying the doubly bound ATP binding and motor unbinding rates by $\exp[\beta/2 \min\{\sum_i -E_i, E^*\}]$ and $\exp[-\beta/2 \min\{\sum_i -E_i, E^*\}]$, respectively.

F. Parameters

Parameters and their sources are summarized in table I. Here we discuss the estimation of parameters not directly constrained by experiments. The effective concentration of singly bound proteins is estimated as the concentration of a confined single molecule: for singly bound crosslinkers, we assume the second head explores a half-sphere of radius $r_0 = 32 \text{ nm}$, the measured rest length of PRC1 crosslinkers [93]. We choose a half-sphere because crosslinkers can only bind to adjacent microtubules, not the microtubule barrel to which they are already bound. Then c_{eff} is

$$c = \frac{1}{V_{1/2}} = \frac{3}{2\pi r_0^3} = 1.5 \times 10^{22} \text{ m}^{-3} = 0.024 \text{ mol/m}^3 \approx 25 \text{ } \mu\text{M}. \quad (23)$$

For motors, we use $r_0 = 7.5 \text{ nm}$ as the length between bound and unbound heads. We also assume the head only explores a quarter-sphere on average, i.e., above the microtubule and in front of the already-bound head. This gives $c_{\text{eff}} \approx 4 \text{ mM}$.

The off-rate of crosslinking PRC1 heads has not been experimentally measured. However, it has been observed that PRC1 binds at least 28 times more strongly to anti-parallel microtubule overlaps (i.e., the common area between overlapping microtubules that are aligned along their longitudinal axes) versus single or parallel microtubules [92]. The effective concentration increase due to binding (summarized in c_{eff}) partially accounts for this. However, we found that decreasing $k_{\text{off},2}$ by a factor of 10 compared to $k_{\text{off},1}$ could give the overlap enhancement found experimentally.

Both the one-head-bound and crosslinking diffusion coefficient of PRC1 have been measured experimentally [102]. We directly use the value for singly bound heads. To determine the diffusion coefficient when crosslinking, we take into account the effects of force dependence into account. A simulation diffusion coefficient of $0.065 \text{ } \mu\text{m}^2\text{s}^{-1}$ leads to an effective crosslinking diffusion coefficient of $0.021 \text{ } \mu\text{m}^2\text{s}^{-1}$, as measured [102].

For motors, the hydrolysis rate k_{hydro} is determined by the average velocity expected for the motor because ATP hydrolysis is the rate-limiting step of the mechanochemical cycle (Fig. 1c). For Kif4A, a hydrolysis rate of 95 s^{-1} yields an average velocity of 600 nm/s . For kinesin-1, a hydrolysis rate of 110 s^{-1} yields an average velocity of 800 nm/s . The value of $k_{\text{off},1}$ controls the processivity because motors can only unbind while in the fully docked state. For model Kif4A, a singly bound off rate of 8 s^{-1} yields an average processivity of $1.5 \text{ } \mu\text{m}$. For kinesin-1, a singly bound off rate of 10 s^{-1} yields an average processivity of $1.2 \text{ } \mu\text{m}$.

For the Kif4A model, we fit the parameters of the short- and long-range interaction to data on low-density Kif4A motility. We implemented this using the nonlinear least-squares optimization routine from the SciPy python library [104]. The fit estimated the six parameters ϵ , D , E_0 , E^* , $\delta_{\text{off},2}$, and δ_{ATP} ; final parameters were determined by hand adjustment.

G. Validation

To validate the simulations, we compared simulation results to theory for microtubule, crosslinker, and motor movement (Fig. 2). For microtubules (Fig. 2a-c), we predicted and measured the diffusion parallel and perpendicular to the filament long axis. In the absence of applied force, the center of mass diffuses with $\langle x^2 \rangle = 2Dt$ (Fig. 2b). Under a constant applied external force $\vec{F}_s$, the filament velocity is $\vec{v} = \Xi^{-1}(t) \cdot \vec{F}_s(t)$ (Fig. 2c).

For crosslinkers, we measured both crosslinker diffusion and formation of a crosslink when one bound head is fixed (Fig. 2d-f). The PRC1 diffusion coefficient when one head is bound matches experimental results [102]. The measured diffusion coefficient of crosslinking PRC1 is $0.024 \pm 0.003 \text{ } \mu\text{m}^2\text{s}^{-1}$ [102]. A slightly larger bare simulation diffusion coefficient of $0.0655 \text{ } \mu\text{m}^2\text{s}^{-1}$ gives an effective PRC1 diffusion coefficient of $0.021 \text{ } \mu\text{m}^2\text{s}^{-1}$ because of force-dependent

TABLE I. Parameters used in CyLaKS.

Description		Value	Notes
General			
$k_B T$	Thermal energy	4.1 pN·nm	Room temperature
η	Fluid viscosity	0.1 pN·s· μm^{-2}	100 times more viscous than water
t	Total simulation time	5 – 180 min	Longer time for lower protein density
t_e	Pre-equilibration time	100 s	Time before equilibration status is checked
t_c	Equilibration check interval	10 s	Size of data window for statistics
t_s	Data snapshot interval	0.01 – 0.1 s	Time between data output
dt	Timestep	2×10^{-5} s	Time that passes each KMC-BD step
Microtubules			
L	Length	0.1 – 20 μm	Experimental values
R	Radius	12.5 nm	[101]
Δ	Site size	8 nm	[101]
N_{BD}	BD steps per KMC step	10	Ensures stable microtubule movement
Crosslinkers			
ϵ	Neighbor-neighbor energy	$2.3 k_B T$	Estimated from PRC1 binding curve [102]
k_{on}	Per-site binding rate	$2.4 \times 10^{-4} \text{ nM}^{-1} \text{ s}^{-1}$	From $k_{\text{off},1}$ and measured K_d [93]
c	Bulk concentration	0.2 – 5.0 nM	Experimental values
c_{eff}	Effective concentration of second head while singly bound	$2.5 \times 10^4 \text{ nM}$	Assumes that the second head can explore a half-sphere of radius 32 nm
$k_{\text{off},1}$	Singly bound off rate	0.14 s^{-1}	From measured lifetime of $t_{1/2} = 7 \text{ s}$ [93]
$k_{\text{off},2}^0$	Doubly bound off rate	0.014 s^{-1}	Sets occupancy in microtubule overlaps
D_1	Singly bound diffusivity	$0.13 \mu\text{m}^2 \text{ s}^{-1}$	[102]
D_2^0	Doubly bound diffusivity	$0.065 \mu\text{m}^2 \text{ s}^{-1}$	Set to match experiment [102]
r_0	Crosslinker length	32 nm	[45]
k_s	Crosslinker spring constant	$0.45 \text{ pN} \cdot \text{nm}^{-1}$	[103]
Motors			
ϵ	Neighbor-neighbor energy	1.6 or 0 $k_B T$	Toggles short-range interactions on or off [34]
D	Quadratic potential cutoff	8 or 0 μm	Toggles long-range interactions on or off [34]
E_0	Quadratic potential strength	$0.95 k_B T$	[34]
E^*	Quadratic potential ceiling	$4.75 k_B T$	[34]
k_{on}	Per-site binding rate	$3.6 \times 10^{-4} \text{ nM}^{-1} \text{ s}^{-1}$	[34]
c	Bulk concentration	0.002 – 6.0 nM	Experimental values
c_{eff}	Effective concentration of second head while singly bound	$4 \times 10^6 \text{ nM}$	Assumes that the second head can explore a quarter-sphere of radius 7.5 nm [34]
k_{ATP}^0	ATP binding rate	5000 s^{-1}	Assumes 2 mM ATP [87]
k_{hydro}	ATP hydrolysis rate	95 or 110 s^{-1}	Sets velocity to 600 or 800 nm/s to model Kif4A or kinesin-1, respectively [34, 87]
$k_{\text{off},1}^\pm$	Singly bound off rate	8 or 10 s^{-1}	Sets processivity to 1.5 or 1.2 μm to model Kif4A or kinesin-1, respectively [34, 87]
$k_{\text{off},2}^0$	Doubly bound off rate	260 s^{-1}	[87]
F_{int}	Internal necklinker tension	26 pN	[87]
$\delta_{\text{off},1}$	Singly bound unbinding distance parameter (ADPP-bound head)	0.6 nm	[87]
$\delta_{\text{off},2}$	Doubly bound unbinding distance parameter (trailing head)	0.13 or 0.35 nm	For Kif4A or kinesin-1, respectively [34, 87]
δ_{ATP}	ATP-binding distance parameter	1.2 or 4.6 nm	For Kif4A or kinesin-1, respectively [34, 87]

diffusion (Fig. 2e). For crosslink formation when one head is bound and fixed in place, the occupancy of a site on the other filament is

$$\bar{n} = \frac{c}{K_d + c}, \quad (24)$$

where $\bar{n}$ is the average fractional occupancy of the site, c is the concentration of the binding head, and $K_d = k_d/k_a$ is the dissociation constant. We use $c = c_{\text{eff}}$ when measuring the occupancy of the crosslinking head. The dissociation

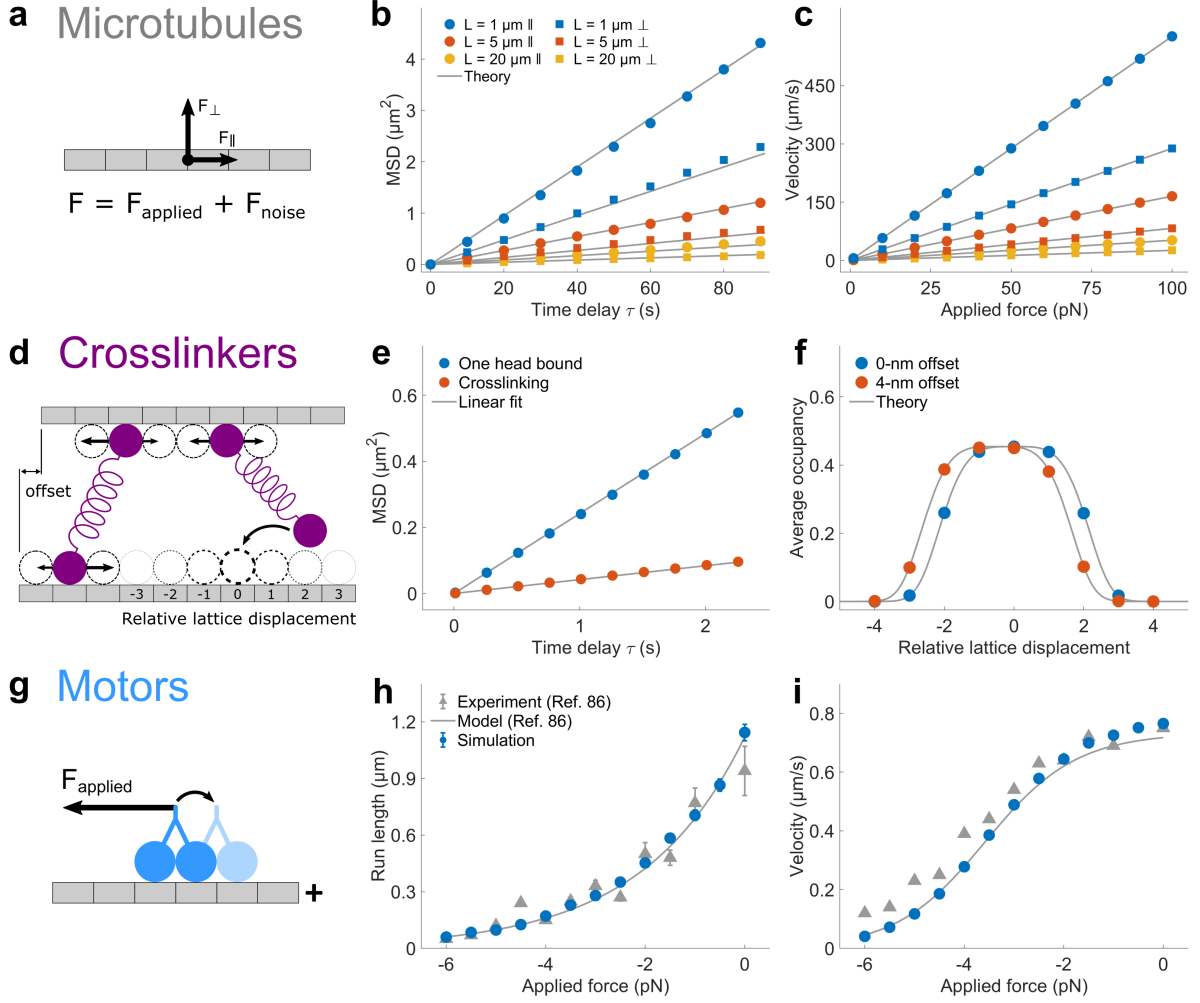


FIG. 2. Simulation validation. (a-c), Microtubules. (a) Schematic of 2D microtubule movement. (b) Plot of mean-squared-displacement (MSD) of microtubule center of mass as a function of time delay τ for varying microtubule length, for movement parallel (circles) and perpendicular (squares) to the filament long axis. Theory is the prediction from 1D diffusion. Data were averaged from six independent simulations; error bars show standard error of the mean and are smaller than the points. (c) Plot of velocity of microtubule center of mass as a function of applied force for varying microtubule length, for movement parallel (circles) and perpendicular (squares) to the filament long axis. Theory is the prediction from constant-force motion. Data were averaged from six independent simulations; error bars correspond to standard error of the mean and smaller than the points. (d-f), Crosslinkers. (d) Schematic. Two microtubules are fixed with a vertical separation of 32 nm, the length of the crosslinkers. The top microtubule is horizontally displaced by the offset distance, where an offset of 0 nm means the lattices of each microtubule are aligned. (e) Plot of crosslinker mean-squared-displacement (MSD) versus time delay τ . The diffusion coefficient is determined from a linear fit ($0.121 \mu\text{m}^2\text{s}^{-1}$ for one head bound; $0.0213 \mu\text{m}^2\text{s}^{-1}$ for crosslinking). (f) Plot of average second head occupancy versus relative lattice displacement for two different values of the microtubule offset. Theory is the prediction from statistical mechanics (see text). (g-i), Motors. (g) Schematic. Motors move under a constant hindering force. Plots of run length (h) and velocity (i) versus applied force. Experimental data and model from previous work [87]. These runs used the kinesin-1 parameter set of Table I.

constant varies for each lattice site because of the crosslinker spring extension according to Eqs. 7 and 8, giving

$$K_d^i = K_d^0 \exp \left[\frac{\beta}{2} k_s (r_i - r_0)^2 \right], \quad (25)$$

where r_i is the crosslinker extension for binding at site i . This matches the simulated occupancy for fixed microtubule position (Fig. 2f).

For motors, we compared to previous measurements and model of kinesin-1 movement under hindering load [87] (Fig. 2g-i). The force dependence of both the run length (Fig. 2h) and velocity (Fig. 2i) in our simulations match previous work. These simulations use the kinesin-1 parameter set (Table I), with a motor concentration of 50 pM and microtubule length of $80 \mu\text{m}$, with results averaged over 4 independent simulations.

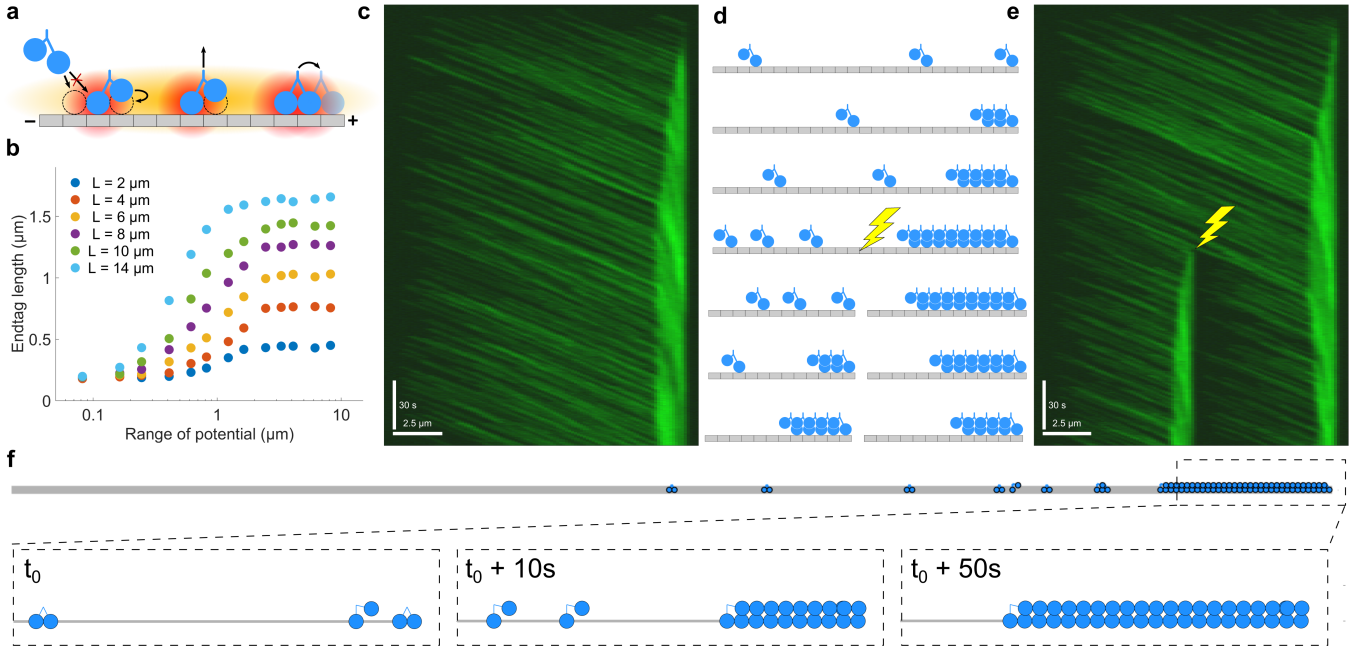


FIG. 3. Kif4A end-tag formation due to long-range motor interactions. (a) Schematic of the motor interaction model. Motors interact by short- and long-range cooperativity, and the long-range interaction affects both binding and stepping. (b) Plot of end-tag length versus potential range for varying microtubule length. (c) Simulated kymograph of end-tag formation. 67% of simulated motors are fluorescently labeled. Scale bars are $2.5 \mu\text{m}$ and 30 seconds. (d) Schematic of the microtubule ablation simulation. After an end-tag forms, the microtubule is split in half. A new end-tag forms on the new microtubule, while the old end-tag shrinks. (e) Simulated kymograph of microtubule laser ablation. 67% of simulated motors are fluorescently labeled. Scale bars are $2.5 \mu\text{m}$ and 30 seconds. (f) Snapshot created from CyLaKS post-processing graphics program for a 2 micron-long microtubule at steady state after end-tag formation. (Inset) Zoom-in of microtubule plus-end at initial time $t_0 = 90$ seconds, 10 seconds later, and 50 seconds later. Prior to t_0 , only 1 or 2 motors are transiently bound to the microtubule at any given time. Once 3 or more motors are bound, the long-range binding cooperativity triggers a cascade of further motor binding. For these parameters, full end-tag formation requires ~ 300 seconds.

III. RESULTS

Here we illustrate the types of simulations that can be done in CyLaKS using four examples. First, we build on our previous work to show how long-range interactions between Kif4A motors can lead to microtubule-length-dependent accumulation at plus-ends [34]. Second, inspired by previous work on heterogeneity in the microtubule lattice [56–58], we show how motor motility changes if the lattice contains a random mixture of sites with different motor binding affinity. Third, building on previous work on heterodimeric kinesin motors [105–110], we create a toy model of a heterodimeric motor in which one head is immobile while bound while the other head can diffuse while singly bound. The model demonstrates the expected crossover from directed to diffusive motility as the diffusion coefficient of the second head increases. Fourth, we demonstrate how varying the number of crosslinkers between two microtubules can change the equilibrium microtubule separation.

A. Length-dependent end-tags

In recent work, we used CyLaKS to study how collective motor behavior can change due to long-range interactions [34]. Kif4A is a human kinesin-4 motor that accumulates densely on microtubule plus-ends, forming end-tags. Previous work found that end-tag length increases linearly with the length of the microtubule on which they form [45]. This length dependence persists for microtubules up to $14 \mu\text{m}$ long, even though single Kif4A motors have a run length of $1 \mu\text{m}$. We found that this surprising result could not be explained by a conventional motor model with only short-range interactions between motors. A combination of short- and long-range cooperative interactions between motors allowed length-dependent end-tags to form in our model [34] (Fig. 3).

Previous work found that bound kinesin-1 motors can increase the binding rate of other motors up to $6 \mu\text{m}$ away [63]. We therefore implemented a long-range interaction as a Gaussian increase in binding affinity up to a distance D (Eqs. 20 and 21). We found that long-range interactions that only affect binding kinetics only partially explain

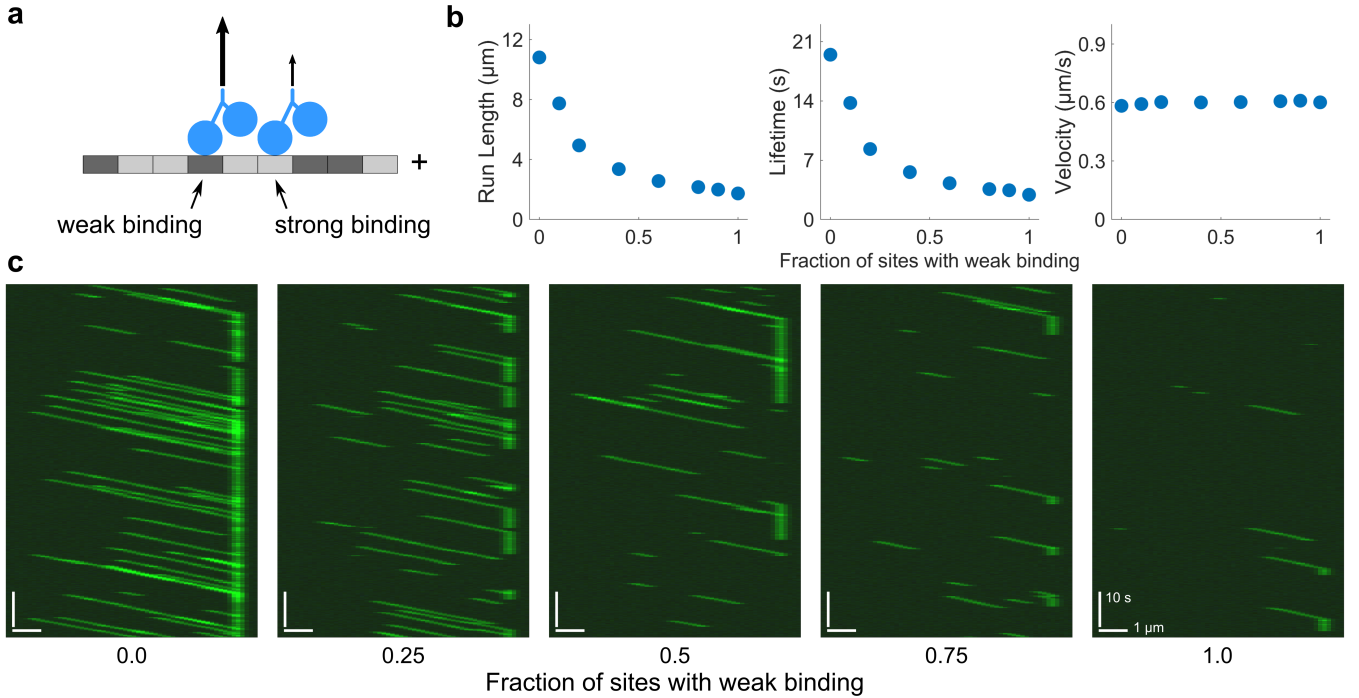


FIG. 4. Effects of modeling heterogeneous tubulin with a mix of strong- and weak-binding sites. (a) Model schematic. A fraction of tubulin sites (dark grey) are weakly binding. (b) Plots of motor run length, lifetime, and velocity as a function of the fraction of sites with weak binding. Here, $\zeta_i = 3$ and $c = 50$ pM. Motor processivity has been increased by an order of magnitude from the reference parameter set. Data points are the average of five independent runs. Error bars correspond to the standard error of the mean and are typically smaller than the points. (c) Simulated kymographs with varying fraction of weak-binding tubulin with all motors fluorescently labeled. Here $c = 150$ pM.

the data. Our experimental results showed that motor velocity significantly decreases as motors bind [34]. To predict this, the long-range interaction in our model must affect motor stepping in addition to binding. Since we lack direct experimental evidence on how the interaction might alter motor mechanochemistry, we modeled one plausible mechanism by which this might happen. We assumed that the long-range attractive potential could reduce the internal tension of the necklinker. This reduces rear-head unbinding from the microtubule and increases front-head ATP binding while doubly bound (Eqs. 16 and 22). We fit ϵ , D , E_0 , and E^* to experimental data on Kif4A at low density and found good agreement [34]. Without any changes to these model parameters, our model quantitatively matches the length-dependent end-tags found experimentally at higher motor concentration.

Here we extend our previous work by examining how the range of the motor interaction affects end-tag length (Fig. 3a-e). The interaction range must be at least $1 \mu\text{m}$ to begin to approach the experimental values (Fig. 3b). We also find that for end-tag formation specifically, length saturates at a range of $2.5 \mu\text{m}$. To illustrate the dynamics of end-tag formation, we generated a simulated motor kymograph (Fig. 3c). Our model predicts that breaking a microtubule in two would cause the original end-tag to shrink while a new end-tag forms at the plus-end of the new microtubule (Fig. 3d). Both of these predictions are matched by our simulations (Fig. 3e).

B. Tubulin heterogeneity

The molecular details of motor and MAP interaction with tubulin affect binding movement, causing different tubulin isomers and post-translational modification to influence protein binding and motor movement [111–113]. Previous work found that differences in the tubulin carboxy-terminal tail (CTT) were associated with a decrease in the run length of kinesin-1 while leaving velocity unaffected [111]. However, these same CTT mutants reduced both the velocity and run length of kinesin-2. These raises the possibility that heterogeneous microtubules made up of a mix of different tubulin isoforms or modifications could cause dimer-specific variation in motor or MAP behavior. To model these effects in CyLaKS, we allow each lattice site to have different interactions with a motor or MAP. Here, we illustrate the effects of specifying site-specific binding affinity ζ_i for site i , which scales the dissociation constant

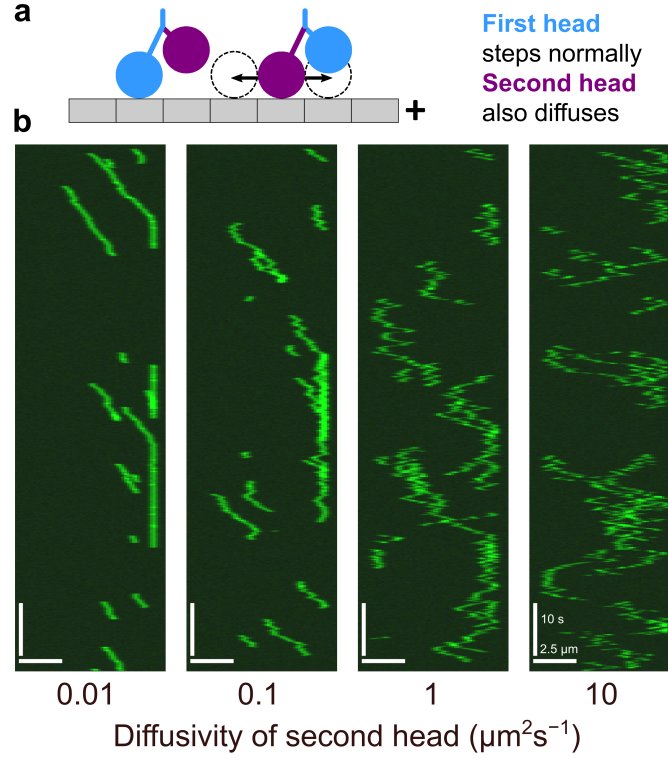


FIG. 5. Kinesin heterodimer simulations. (a) Model schematic. Kinesin heterodimers are constructed of one normal head (blue) and one mutant head (purple) which diffuses while singly bound. (b) Simulated kymographs of kinesin heterodimer for $D = 0.01, 0.1, 1$, and $10 \mu\text{m}^2 \text{s}^{-1}$. All simulated molecules are fluorescently labeled.

for binding as

$$K_{D,i} = \zeta_i^2 K_D^0, \quad (26)$$

where K_D^0 is the original value of the dissociation constant. The parameter ζ_i is squared in this expression because we currently implement it by dividing the binding rate and multiplying the unbinding rate by the same factor.

We then examined the effects of introducing a variable, randomly located fraction of weak-binding sites with $\zeta = 3$ for a high-processivity motor (Fig. 4). We varied the fraction of weak-binding sites from 0 to 1. As expected, the average motor run length and lifetime drop as the fraction of weak-binding sites increases, while the motor velocity is unchanged. Remarkably, when just 5% of sites on a 1000-site lattice are weakly binding, the processivity and lifetime of motors are both significantly affected (Fig. 4b). We also see that when all sites are weakly binding, the motor processivity and lifetime decreases by a factor of 9, as expected. Simulated kymographs show a dramatic reduction in motor activity as the fraction of sites with weak binding is increased (Fig. 4c).

C. Heterodimeric motors

Some kinesin motors in cells are heterodimeric, for which the two motor heads that make up the dimer have different behavior [105–110]. Engineered kinesin heterodimers can be created with differences in catalysis between the two heads [114–116]. The explicit modeling of motor mechanochemistry in CyLaKS makes simulated heterodimers straightforward to model.

To illustrate this capability, we created a heterodimeric motor with one head that can diffuse when singly bound (Fig. 5). One (normal) head is immobile while singly bound, while the other (mutant) can diffuse along the lattice while singly bound. We assume that the normal catalytic head is always the first to bind and is leading. With our typical parameter set, the heterodimer spends about 5% of its time in a state that can diffuse. To see when one-head diffusion might have a significant effect, we decreased the effective concentration of the second motor head by a factor of 40. This increases the amount of time the motor spends in the a diffusible state to about 40% of the cycle. To keep overall motor processivity constant, we decreased the off rate of docked motors by a factor of 40.

With these parameters, we observe significant changes in motor activity as we increase diffusion coefficient of the second head (Fig. 5b). For low diffusion coefficient, processive runs still occur and motors pause at the ends of microtubules. For intermediate diffusion coefficient, the effects of diffusion are noticeable as fluctuations about the mean velocity during a processive run. For high diffusion coefficient, both processive movement and end pausing are reduced by the diffusion.

D. Filament separation

In assemblies of many microtubules such as the mitotic spindle and reconstituted microtubule bundles, the spacing between microtubules can vary due to interactions defined by crosslinking motors and MAPs [93, 117–120]. While crosslinking motors and crosslinkers are typically 30–50 nm long [93, 121], the lateral separation between the surface of microtubules in the fission yeast spindle is typically 5–15 nm [117, 119]. This suggests that additional physical effects beyond just the length of motors or crosslinkers may be important for microtubule spacing in the spindle.

We developed a model of crosslinker-mediated control of the spacing of a pair of microtubules and studied it both analytically and in CyLaKS (Fig. 6). Two filaments can change their lateral separation h but are otherwise fixed in position. A fixed number of crosslinkers can diffuse along the lattice, and force exerted by the crosslinkers determines the filament separation. Crosslinkers that bind at an angle between the filaments are typically stretched (Fig. 6a), inducing force that pull the filaments closer together than the crosslinker length.

For relatively short microtubules (up to 20 sites), the free energy of crosslinker binding and average separation can be computed by explicit enumeration of all possible binding states. To do this computationally, we first insert a single crosslinker in all possible binding states and note the crosslinker spring energy of each as well as possible binding states of additional crosslinkers. Then a second crosslinker is added and the procedure is iteratively continued to many crosslinkers, while ignoring crosslinker permutations. In this procedure we enforce steric interactions so that only one crosslinker can bind to each lattice site, and crosslinker crossing is not allowed. The crosslinker partition function is then

$$Z(h) = \sum_i e^{-\beta E_i}, \quad (27)$$

where E_i is the crosslinker spring energy for a particular configuration i and the sum is over all possible arrangements of crosslinkers for a given separation h . The total free energy is then

$$F_h = -\beta \ln[Z(h)] + U_{\text{WCA}}(h + \sigma), \quad (28)$$

where U_{WCA} is the Weeks–Chandler–Anderson repulsive potential between microtubules, which acts on the microtubule centers separated by a distance $h + \sigma$, where σ is the microtubule diameter (Fig. 6b). The average separation is then

$$\langle h \rangle = \frac{\sum_i h_i e^{-\beta F(h_i)}}{\sum_i e^{-\beta F(h_i)}}. \quad (29)$$

Simulations in CyLaKS accurately sample the Boltzmann distribution as microtubule separation varies (Fig. 6c). Here we used crosslinkers 32-nm long, as found for PRC1 [93]. When we vary crosslinker number for microtubules with 13 or 100 sites, we find that microtubule separation is typically smaller than 32 nm, with a particular drop for smaller crosslinker number (Fig. 6d,e). Altering the model to neglect crosslinker steric exclusion or discrete sites along the microtubule tends to predict slightly lower separation (Fig. 6d).

The crosslinker tilt (the average angle between the crosslinker axis and the normal between the two microtubules, θ) decreases as the number of crosslinkers increases (Fig. 6g,h). This is caused both by steric interactions and changes in the scale of the free energy. First, as crosslinker number increases, steric exclusion prevents crosslinkers from tilting at high angle because other crosslinker heads are bound on adjacent sites. Second, as more crosslinkers bind, the overall magnitude of the free energy increases because each bound molecule adds a contribution to the free energy. This makes the potential increase more rapidly about the minimum (a separation around 30 nm). Since this minimum-free-energy separation is close to the crosslinker rest length, the crosslinkers will be more perpendicular to the microtubules as crosslinker number increases.

IV. DISCUSSION

We developed the the Cytoskeleton Lattice-based Kinetic Simulator (CyLaKS) to facilitate modeling of cytoskeletal systems in which spatiotemporal changes and heterogeneity of the filament, motors, and/or associated proteins are

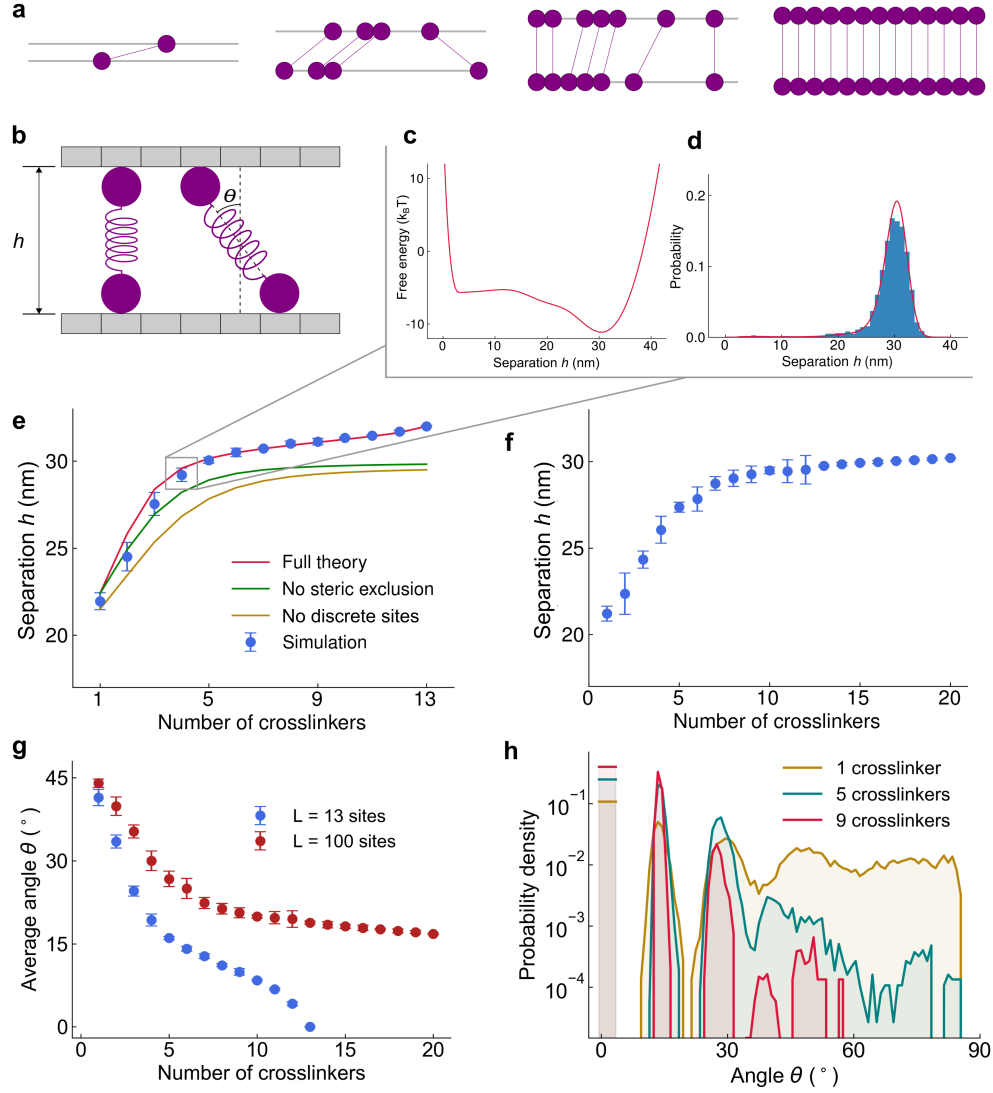


FIG. 6. Change in microtubule separation with varying crosslinker number. (a) Snapshot created from CyLaKS post-processing graphics program from simulations with varying number of crosslinkers bound to a pair of microtubules. Each microtubule contains 13 crosslinker binding sites. Microtubule separation increases with the number of bound crosslinkers. (b) Schematic of the model. The microtubule separation h varies due to forces from crosslinkers. (c) Plot of free energy as a function of microtubule separation for 13-site microtubules with 4 32-nm-long crosslinkers, from semi-analytic theory. (d) Probability as a function of microtubule separation for 13-site microtubules with 4 32-nm-long crosslinkers from semi-analytic theory (red) and simulation (blue). (e) Average microtubule separation as a function of number of crosslinkers for 13-site microtubules, comparing full semi-analytic theory (red), simulation (blue), and theory neglecting steric exclusion (green) and both steric exclusion and discrete lattice sites (gold). (f) Average microtubule separation as a function of number of crosslinkers for 100-site microtubules. (g) Average angle between the crosslinker axis and the normal between the filaments, as defined in (b), as a function of number of crosslinkers for the 13-site and 100-site microtubule pairs. (h) Probability distribution of crosslinker angle θ for 1, 5, and 9 crosslinkers bound to 13-site microtubules. Crosslinkers are often bound at an angle of exactly zero, but never for small θ near zero due to the discrete binding sites. Therefore for $\theta = 0$ data we plot the probability of a bound crosslinker, not the probability density: for this point, we have increased the width in the plot to make it visible.

significant. We built on previous theory and modeling of single motor mechanochemistry [80–86] by incorporating a model of motor ATP hydrolysis into a simulation with many interacting motors. This extends the approach of existing cytoskeletal simulation packages [66–69] to include a more detailed motor model. CyLaKS also implements detailed-balance in binding kinetics and movement, to model force-dependent protein binding/unbinding and diffusion. It is also designed to model spatiotemporally varying interactions and structure, such as filament lattice heterogeneity and short- and long-range interactions between motors. The framework is flexible and extensible, making it straightforward

to elaborate the model.

In this paper we have shown examples of problems that CyLaKS can model. End-tags of kinesin-4 motors can form due to long-range interactions between motors. These end-tags depend on microtubule length, and dynamically adjust if the microtubule is ablated into two filaments. Implementing a heterogeneous microtubule lattice with a randomly located fraction of weak binding dimers shows that motor run length and lifetime decrease as the fraction of weak-binding sites increases, because motors unbind more quickly from the weak sites. Because CyLaKS is designed to model explicit motor stepping, it is straightforward to model an artificial motor heterodimer in which one head is fixed in place when singly bound, while the other head can diffuse. The overall motor movement then shows a crossover from directed runs to diffusion as the second head diffusion coefficient increases. Finally, we used both CyLaKS and analytic theory to show that crosslinker forces can lead to an equilibrium microtubule separation shorter than the crosslinker length.

CyLaKS can be used to model motor and crosslinker behavior that is spatiotemporally altered. Problems including short-range interactions between motors [37, 38] and motor response to patchy obstacles [39] are straightforward to simulate. Closely related are changes in motor behavior due to crowding, both crowding along the filament lattice [40–45, 54] or due to crowders in solution [55], and motor direction switching [50–54]. Changes in the filament lattice, for example due to heterogeneous isoforms or post-translational modification [111–113] or lattice structure changes or defects [59–64] can be modeled in CyLaKS. The implementation of molecularly detailed spatiotemporal variation in CyLaKS facilitates models using mechanisms suggested by experiments, rather than more coarse-grained models. This can allow a closer integration between modeling and experiments that can guide future work. Future biological applications could include motor traffic along microtubules in cells, which can play a role in neurodegenerative diseases.

Extensions to CyLaKS to include additional mechanisms are straightforward and would be of interest in future work. The source code is available on GitHub [70] for download and modification. The current major limitations of CyLaKS are that it is only two-dimensional, microtubules are modeled as single protofilaments and have no dynamic instability, and visualization is currently achieved through post-processing in MATLAB. Incorporating dynamic instability is straightforward because changes to microtubules only require altering the filament-specific code. Similarly, extending the filament model to include semi-flexibility (for example, to model actin) would be relatively easy as discussed above. However, modeling the full microtubule barrel and subsequently transitioning to three-dimensional space will be more challenging. Parallelizing the code could also help retain reasonable performance with larger three-dimensional systems.

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Author contribution statement

SAF and MDB formulated the mathematical model used in CyLaKS. SAF wrote the simulation code. SAF and MDB wrote the analysis code. SAF developed the analytic theory and ran simulations related to end-tags, tubulin heterogeneity, and kinesin heterodimers. DGS developed the analytic theory and ran simulations related to filament separation. SAF, DGS, and MDB wrote the manuscript. SAF and MDB edited the manuscript.

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