

**Engineering oxygen vacancy-rich CeO_x overcoating onto Ni/Al₂O₃ by atomic layer
deposition for bi-reforming of methane**

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Abstract

Atomic layer deposition (ALD) was applied to develop CeO_x-overcoated Ni/Al₂O₃ catalyst for bi-reforming of methane (BRM), as the combination of dry reforming of methane (DRM) and steam reforming of methane (SRM). Non-stoichiometric CeO_x thin films were successfully deposited on Ni/Al₂O₃ particles by ALD, which constructed a beneficial Ni-CeO_x interface and modified the catalyst property. Ascribed to the unique ALD growth mode, a high amount of Ce(III) and oxygen vacancies existed in the ALD-deposited CeO_x overcoating. A reduction process before the BRM reaction contributed to the further reduction of Ce(IV) to Ce(III), resulting in more oxygen vacancies. The oxygen vacancies at the Ni-CeO_x interface enabled a high rate of CO₂ activation

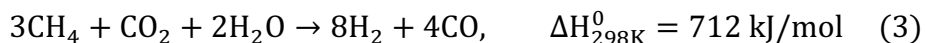
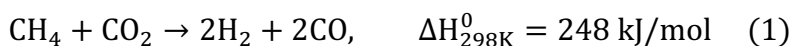
and enabled the balance between the activation of CO₂ and H₂O for BRM. Due to its oxygen vacancies as activation sites for CO₂ and H₂O, CeO_x ALD overcoating significantly improved the activity of Ni/Al₂O₃ catalyst and achieved a better control in the H₂/CO ratio with a suitable ratio of H₂O/CO₂/CH₄ feed. CeO_x overcoatings enhanced the reducibility of Ni(II) sites and assisted in preventing Ni from oxidation during the BRM reaction. Less carbon deposition was achieved by the Ni/Al₂O₃ catalyst with CeO_x overcoating as ascribed to its better reactant activation capacity.

Keywords: Non-stoichiometric CeO_x; atomic layer deposition (ALD); bi-reforming of methane (BRM); oxygen vacancy

1. Introduction

With the rising greenhouse gas (GHG) emissions, the net-zero target by 2050 set in the Paris Agreement and Conference of the Parties necessitates a technically feasible strategy to chemically recycle captured CO₂ into value-added products for the decarbonization roadmap [1, 2]. Dry reforming of methane (DRM, eq. 1) exhibits remarkable potential in consuming the GHG (i.e., CH₄ and CO₂), utilizing the off-peak energy, and producing syngas (i.e., H₂ and CO) with H₂/CO molar ratio of ~1 as industrial C1-block, whereas the current steam reforming of methane (SRM, eq. 2, with H₂/CO molar ratio of ~3) faces high H₂/CO ratio with the formation of side-product CO₂ [3]. Without reconstructing the present infrastructure, bi-reforming of methane (BRM), which incorporates DRM into SRM, can achieve industrial utilization of CO₂ and production of valuable syngas with desired H₂/CO ratio [1, 3, 4]. Especially, syngas with an H₂/CO molar ratio of ~2 (metgas) can be achieved (eq. 3) by BRM and it is optimal for the production of methanol and dimethyl ether, which are blueprinted as the renewable CO₂-recycling synthetic fuels to substitute

the conventional fossil fuels in the near future [3, 5-7]. Nickel, with low cost and high reactivity for CH₄, has been widely investigated as methane reforming catalysts [1, 8, 9]. However, Ni-based catalysts face the challenge of sintering and coking. Especially, the side reactions (e.g., CH₄ cracking and Boudouard reactions) result in carbon growth and high pressure drop in fixed bed reactors [10-12]. To inhibit carbon growth and accumulation, constructing a metal-oxide interface (e.g., introducing promoter or overcoating) and enhancing the concentration of interfacial oxygen surrounding Ni sites can kinetically accelerate the removal rate of carbon intermediates via CO₂ oxidation [13].



CeO₂, with reversible valence states and oxygen vacancies, has been proven to be effective to provide active O sites and enhance the performance of catalysts for methane reforming [14]. The intimate contact between Ni and CeO₂ exhibits a strong influence on the catalytic behavior. For instance, Yan et. al utilized plasma-synthesized Ni/CeO₂-SiO₂ with closer Ni-CeO₂ contact than that of the catalyst prepared by the calcination method for DRM, and achieved better activity and stability due to the more reactive O species at Ni-CeO₂ interface [8]. Besides, the morphology of CeO₂ (e.g., nanorod, nanoparticles, or thin-film) has been reported to play a decisive role on the concentration of oxygen vacancies [15-18], which can participate in CO₂ activation [19]. To develop a highly active and stable catalyst for methane reforming, it is desirable to deposit CeOx with high concentration of oxygen vacancies and construct a sufficient metal-oxide interface.

Atomic layer deposition (ALD) is a gas phase self-limiting thin film coating technology based on cycle-repeatedly sequential surface reactions [20]. With a desired number of ALD cycles, the layer-by-layer growth could be achieved at the atomic level. For heterogeneous catalysts, ALD has been applied to prepare highly dispersed metal clusters as the active catalytic sites, from single atoms to nm-scale nanoparticles (NPs) [20-23]; ALD can also synthesize ultrathin oxide layer or overcoating, which exhibits unique features in generating additional active sites [21, 24], blocking the undesired sites [25], or constructing functional structure [25, 26] for heterogeneous catalysts. Studies showed that the encapsulating structure of ALD oxide film became discontinuous and partially encapsulating on the active metal sites after high-temperature treatment, which effectively exposed the active metal sites and created desirable metal-oxide interfaces [25, 27-29]. Ascribed to the growth mode of ALD, studies showed that the composition of ALD oxide thin film could be non-stoichiometric and exhibited unique properties, which differs from the oxides prepared by traditional methods [24, 29, 30]. Considering the importance of interfacial oxygen species, depositing a suitable oxide onto Ni/Al₂O₃ catalyst as overcoating can effectively construct an ideal metal-oxide interface and tune the catalytic performance. In this work, a highly active and coke-resistant CeO_x-Ni/Al₂O₃ catalyst was synthesized by Ni ALD on Al₂O₃ support, followed by CeO_x ALD. CeO_x ALD exhibited unique properties and enhanced the catalytic performance of Ni/Al₂O₃, enabling to tune the H₂/CO ratio for the BRM reaction.

2. Experimental

2.1. Catalyst preparation

Ni/Al₂O₃ catalyst was synthesized by depositing Ni NPs onto α -Al₂O₃ NPs (Alfa Aesar, 99+%, 80 nm, US3008) using ALD in a home-made fluidized bed reactor [31], as shown in Figure S1. Bis(cyclopentadienyl)nickel (NiCp₂, Alfa Aesar) and hydrogen (Airgas, 99.99%) were used as precursors, and N₂ (Airgas, 99.99%) was used as a carrier gas or flush gas. Before ALD, α -Al₂O₃ NPs were loaded in the reactor and preheated at 150 °C overnight to remove moisture. Then, the reactor temperature was set at 300 °C for Ni ALD. For a typical Ni ALD cycle, NiCp₂ was dosed into the ALD reactor by heating a NiCp₂ bubbler at 90 °C and delivering the vaporized NiCp₂ with 6 mL/min N₂ for 300 s to initiate the first half-reaction. The ALD reactor was flushed by N₂ flush for 600 s to remove excess NiCp₂ and by-products, followed by vacuum evacuation for 20 s. For the second half-reaction, 20 mL/min H₂ was dosed into the reactor for 300 s to react with the chemisorbed NiCp₂ and generate Ni NPs, followed by the clean-up using N₂ flush and evacuation. In this work, 5 cycles of Ni ALD were applied to synthesize Ni NPs and the catalyst was labeled as Ni/Al₂O₃.

CeO_x ALD was conducted to deposit CeO_x overcoating onto the Ni/Al₂O₃ catalyst in the same ALD reactor. Tris(i-propylcyclopentadienyl)cerium (Ce(iPrCp)₃, Strem Chemicals, 99.9%) and deionized water were used as the precursors for CeO_x ALD and N₂ was used as a carrier gas. The reactor temperature was set at 200 °C. For a typical CeO_x ALD cycle, Ce(iPrCp)₃ was dosed into the reactor by heating a Ce(iPrCp)₃ bubbler at 150 °C and delivering the vaporized Ce(iPrCp)₃ with 15 mL/min N₂ for 60 s, followed by the reactor clean-up using N₂ flush and evacuation. Then, H₂O was dosed into the reactor for 60 s to react with the chemisorbed Ce(iPrCp)₃ and generate the CeO_x overcoating, followed by inert gas flush and vacuum evacuation process. In this work, 10, 30, 60, and 90 cycles of CeO_x ALD were applied on the Ni/Al₂O₃ catalyst, and the catalyst was

labeled as 10CeO_x-Ni/Al₂O₃, 30CeO_x-Ni/Al₂O₃, 60CeO_x-Ni/Al₂O₃, and 90CeO_x-Ni/Al₂O₃, respectively. For ease of characterization, 200 cycles of CeO_x ALD were applied on Ni/Al₂O₃ and the catalyst was labeled as CeO_x-Ni/Al₂O₃.

For comparison, Al₂O₃ ALD was conducted to deposit Al₂O₃ overcoating onto the Ni/Al₂O₃ catalyst in the same reactor. Trimethylaluminum (TMA, Sigma-Aldrich) and deionized water were used as the precursors for Al₂O₃ ALD and N₂ was used as the carrier gas. The ALD reaction temperature was 150 °C for Al₂O₃ ALD. For a typical Al₂O₃ ALD cycle, TMA was dosed into the reactor for 300 s, followed by the reactor clean-up using N₂ flush and evacuation. Then, H₂O was dosed into the reactor for 300 s to react with the chemisorbed TMA and generate Al₂O₃ thin film, followed by the reactor clean-up process. 10 cycles of Al₂O₃ were applied to achieve the similar thickness of CeO_x thin film on 60CeO_x-Ni/Al₂O₃ based the ALD thin film growth rates. The catalyst was labeled as Al₂O₃-Ni/Al₂O₃.

For comparison, liquid-based incipient wetness method was conducted to deposit CeO₂ as a promoter onto the Ni/Al₂O₃ catalyst. Ni/Al₂O₃ particles were impregnated in an aqueous solution of Ce(NO₃)₃ (Alfa Aesar, 99.99%) for 1 h (with a similar amount of CeO_x on 60CeO_x-Ni/Al₂O₃), dried at 100 °C in an oven, and then calcinated in the air in a tubular furnace at 500 °C for 3 h. The catalyst was labeled as iwCeO₂/Ni/Al₂O₃.

2.2. Bi-reforming of methane reaction

A home-made fixed bed reactor system was built for bi-reforming of methane reaction, as shown in Figure S2. The reactant control and delivery system were achieved by mass flow controllers

(MKS Instruments) for controlling gas flow rates and a syringe pump (Chemyx Fusion 101) for controlling water flow rate. To ensure the gasification of water, heating tapes (Omega Engineering) were used to heat up the water feeding line to 120 °C. A quartz tube with an inner diameter of 10 mm was used as a reactor, which was placed vertically and heated by a tubular furnace (Carbolite Gero, Ltd.). A K-type thermocouple (Omega Engineering) was positioned right above the catalyst bed to monitor the reactor temperature. One on-line gas chromatograph (SRI 8610C) was used to analyze the products, with a 6-foot Haysep D column and TCD detector. A cold trap tank was used to condense any by-product water from the product gas before it entered into the GC.

For the BRM reaction, ~50 mg catalyst particles were loaded on ~30 mg quartz wool in the quartz tube reactor. A reduction procedure was conducted at 800 °C for 1 h using 20% H_2 /80%Ar (v/v%) mixture with a flow rate of 100 mL/min. After reduction, the temperature was set at a desired temperature and the reactant gases (i.e., CH_4 , CO_2 , and gas-phase H_2O) were introduced into the reactor.

2.3. Catalyst characterizations

Transmission electron microscopy (TEM) was conducted using an FEI Tecnai F20 TEM instrument to measure the Ni particle size and acquire the morphology of the catalysts. X-ray photoelectron spectroscopy (XPS) was conducted using a Kratos Axis 165 X-ray photoelectron spectrometer to determine the chemical states of different elements. XRD was conducted on an X-Pert Multi-purpose diffractometer to access the phase information of the catalysts.

H₂-temperature programmed reduction (H₂-TPR) was conducted using a Micromeritics AutoChem II 2920 instrument. The catalysts were first pretreated in Ar at 300 °C for 1 h. Then, H₂-TPR was performed using 10%H₂/90%Ar (v/v%) from 50 to 900 °C with a temperature increasing rate of 10 °C/min. The H₂ pulse chemisorption experiment was also conducted on this Micromeritics AutoChem II 2920 instrument. The sample was first pretreated in a H₂/Ar (mixed at 10/90 vol%) flow for 1 h and flushed in Ar for 1 h at 700 °C. After cooling down to 50 °C in Ar, the samples underwent the cycles of H₂/Ar pulse and Ar pulse.

Thermogravimetric analysis (TGA) was conducted using a TA Instrument Q50 analyzer. The sample underwent a temperature ramping from room temperature to 200 °C, holding at 200 °C for 1 h, and temperature ramping from 200 to 800 °C at 10 °C /min in 40 mL/min Ar.

CO₂-temperature programmed desorption (CO₂-TPD) and O₂-temperature programmed oxidation (O₂-TPO) were conducted using the methane reforming reactor. A mass spectrometer (Stanford Research System, QMS 200) with a pressure-time mode was used to detect and record the gas signal. The m/e value of the MS signal was taken to identify the gas species (e.g., 40 for Ar, 28 for CO, 44 for CO₂, and 32 for O₂). For CO₂-TPD, the catalyst was first reduced at 800 °C using H₂, then CO₂ saturation in 20 mL/min 20%CO₂/80%Ar (v/v%) mixture for 1 h at 80 °C and Ar flush in 20 mL/min Ar for 1 h at 80 °C. After this pretreatment, CO₂-TPO was performed in Ar, starting from 80 to 700 °C with a temperature increasing rate of 10 C/min. For O₂-TPO, the spent catalysts were first pretreated in Ar at 100 °C for 1 h r and then oxidized in 20%O₂/80%Ar (v/v%) from 100 to 800 °C.

3. Results and Discussion

3.1. Material characterizations

TEM was conducted to determine the morphology of the Ni/Al₂O₃ and 60CeO_x-Ni/Al₂O₃ catalysts. As shown in Figure 1a, the average size of Ni NPs (in oxidized state) on the ALD-prepared Ni/Al₂O₃ was 2.7 ± 0.9 nm, which is much smaller than those prepared by the traditional incipient wetness method. After 60 cycles of CeO_x ALD, the average size of Ni NPs (in oxidized state) on 60CeO_x-Ni/Al₂O₃ was about 2.9 ± 1.0 nm, which was almost the same as that of the pristine Ni/Al₂O₃. Since the CeO_x ALD process was conducted at a mild temperature of 200 °C, there was no obvious sintering of Ni NPs during the CeO₂ ALD coating process. For the reduced catalysts, the average size of the reduced Ni/Al₂O₃ catalyst is 9.7 ± 2.3 nm and the average size of the reduced 60CeO_x-Ni/Al₂O₃ catalyst is 6.2 ± 1.5 nm, which indicates the CeO_x overcoating inhibited the sintering of the Ni during the high-temperature reduction process. As a bottom-up synthesis strategy, ALD can create an ultra-thin CeO_x overcoating on Ni/Al₂O₃ surface conformally and help prevent sintering. The lattice spacing of 0.203 nm could be observed with the HRTEM analysis, which was ascribed to the (111) of metallic Ni. The element mapping result in Figure 1f exhibited the uniform distribution of CeO_x overcoating on both Ni and Al₂O₃, which confirms the Ni-CeO_x interface. In addition, XRD was conducted to determine the phase structure of Ni/Al₂O₃ and CeO_x-Ni/Al₂O₃, as shown in Figure S3. It could be seen that the main peaks were assigned to α -Al₂O₃, with a small amount of NiO. The peaks assigned to any cerium oxide could be hardly seen, probably due to the low loading or the amorphous structure.

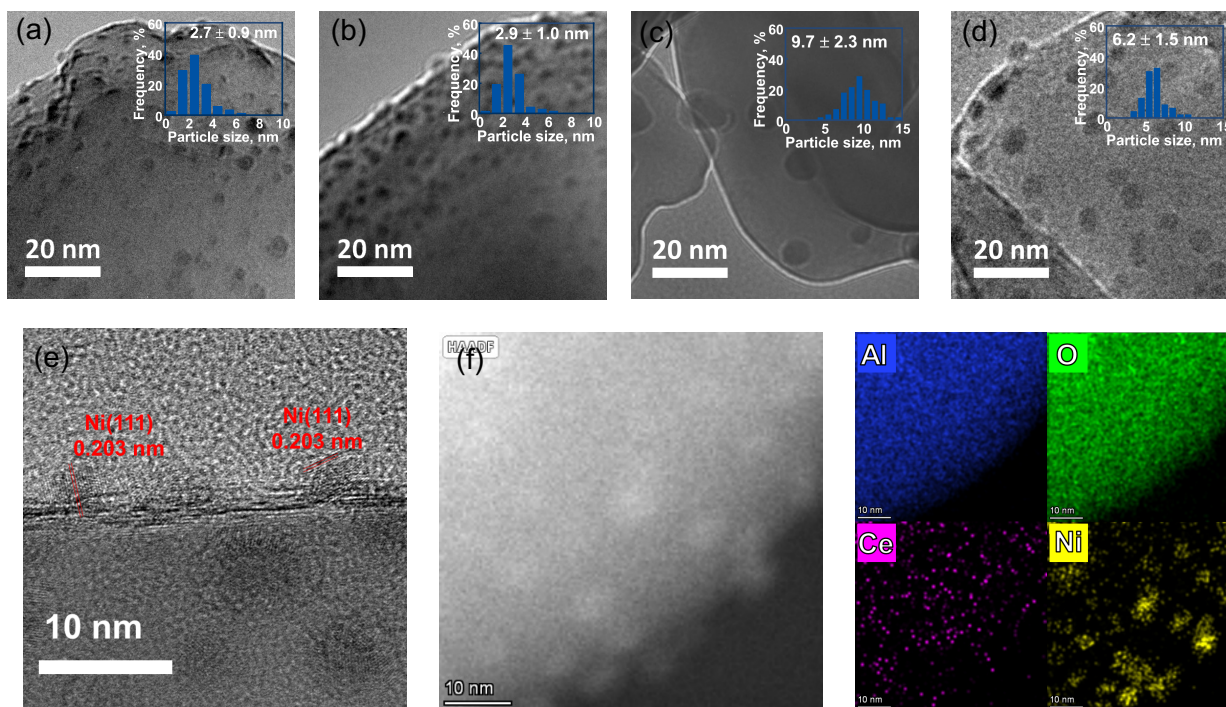
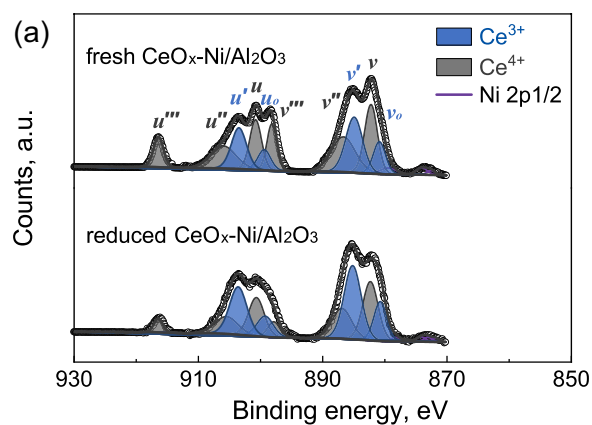


Figure 1. TEM images of (a) fresh Ni/Al₂O₃, (b) fresh 60CeO_x-Ni/Al₂O₃, (c) reduced Ni/Al₂O₃, and (d-f) reduced 60CeO_x-Ni/Al₂O₃. (f) EDS elemental mapping of Al, O, Ce, and Ni for reduced 60CeO_x-Ni/Al₂O₃. The inset images show the size distribution of Ni NPs.



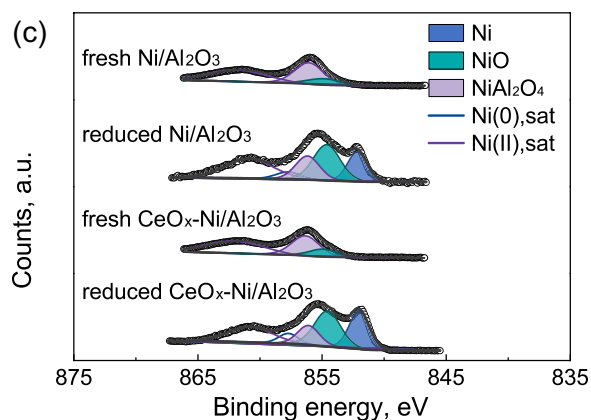
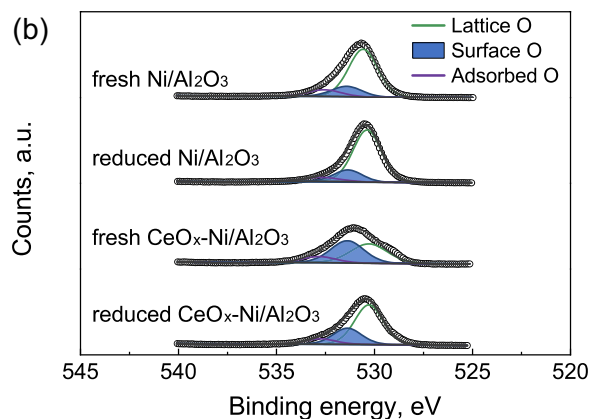


Figure 2. XPS spectra of (a) Ce3d for fresh CeO_x-Ni/Al₂O₃ and reduced CeO_x-Ni/Al₂O₃, (b) O 1s, and (c) Ni 2p_{3/2} for fresh Ni/Al₂O₃, reduced Ni/Al₂O₃, fresh CeO_x-Ni/Al₂O₃, and reduced CeO_x-Ni/Al₂O₃.

To examine the property of CeO_x thin films prepared by ALD, XPS was conducted on the fresh and reduced ALD-prepared CeO_x-Ni/Al₂O₃ and iwCeO₂/Ni/Al₂O₃ catalysts in Figure 2 and Figure S4. All spectra were calibrated by fixing adventitious carbon at 284.5 eV (C1s in Figure S4). For the Ce element in Figure 2a, the Ce(IV) peaks included ν at 882.3 eV, ν'' at 886.7 eV, ν''' at 897.8 eV, u at 899.3 eV, u'' at 903.5 eV, and u''' at 916.4 eV [32, 33]. The Ce(III) peaks included ν_o at 880.8 eV, ν' at 885.2 eV, u_o at 899.3 eV and u' at 903.5 eV [32, 33]. To have a quantitative

comparison, the Ce(III) contents were calculated from the $(v_o + v' + u_o + u')$ % for the ALD-prepared and IW-prepared catalysts. Besides, the characteristic u''' peak, without any overlapping with other peaks, could represent the relative Ce(IV) content and was used to indicate the Ce(IV) amount. The Ce(III) content of the fresh ALD-prepared CeO_x-Ni/Al₂O₃ was 38.0%, with u''' peak as Ce(IV) representative at 4.7%. Based on the Ce 3d results, there was more Ce(III) in the ALD-prepared CeO_x-Ni/Al₂O₃ catalyst. For cerium oxide, the content of Ce(III) is generally considered a significant indicator of the oxygen storage capacity, which assists the surface reaction and enhances the catalytic activity [33]. For the ALD-prepared catalyst, the higher amount of Ce(III) should be ascribed to the unique ALD growth mode, because Ce(iPrCp)₃ and H₂O would react to form Ce(OH)₃ initially, and the ultra-thin film structure could favor the existence of Ce(III) [34-36]. Therefore, the ALD-prepared CeO_x overcoating had more Ce(III) than that prepared by the traditional liquid method and could participate in the surface reaction during methane reforming. During the H₂-reduction process, the chemical states of Ce in Figure 2a and O in Figure 2b also significantly changed. In the spectrum of Ce 3d, there was a higher Ce(III) content for CeO_x-Ni/Al₂O₃, with the Ce(III) ratio of 50.8% based on $(v_o + v' + u_o + u')$ % and the diagnostic peak (u''') of 1.9 % for Ce(IV). For the IW-prepared iwCeO₂/Ni/Al₂O₃ catalyst, the fresh catalyst had a Ce(III) content at 22.4% and u''' % peak as Ce(IV) representative at 6.4%. After reduction, the reduced catalyst had a Ce(III)% content of 42.7 % and u''' % of 4.6 % for the iwCeO₂/Ni/Al₂O₃ catalyst. Compared with the spectra of the fresh CeO_x-Ni/Al₂O₃ catalysts with Ce(III)% of 40.0 % and u''' % of 4.8 %, the Ce(III) content for the reduced catalyst was higher, indicating the reduction of Ce(IV). Owing to the variable valences of Ce(III) and Ce(IV), Ce(IV) was reduced to Ce(III) during H₂-reduction, and more oxygen vacancies were generated to keep the electronic balance of Ce(III) [18, 41].

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247 The oxygen species were investigated using XPS for Ni/Al₂O₃, ALD-overcoated CeO_x-Ni/Al₂O₃,
248 ALD-overcoated Al₂O₃-Ni/Al₂O₃, and IW-promoted iwCeO₂/Ni/Al₂O₃. The O species were
249 deconvoluted to three peaks, including the lattice O at ~ 530.5 eV for O of the metal oxide, the
250 surface O at ~ 531.5 eV for low coordinated oxygen atoms, and the adsorbed O at ~532.7 eV from
251 adsorbed H₂O [37]. Especially, the surface oxygen consists of hydroxyl oxygen and deficient
252 oxygen sites, which are important surface species. As shown in Figure 2b, the content of surface
253 O in Ni/Al₂O₃ was about ~15%, which was smaller than ~45% of the CeO_x-Ni/Al₂O₃ catalyst. For
254 comparison, the content of surface O for the ALD-overcoated Al₂O₃-Ni/Al₂O₃ catalyst reached
255 ~54% and the content of surface O for IW-promoted iwCeO₂/Ni/Al₂O₃ reached ~23% in Figure
256 S4. For the ALD-overcoated catalysts, the high content of the surface O indicated a large number
257 of hydroxyls, regardless of CeO_x ALD or Al₂O₃ ALD overcoating. Besides, the higher content of
258 surface O in the iwCeO₂/Ni/Al₂O₃ catalyst indicated that the CeO₂ promoter also increased the
259 surface O for Ni/Al₂O₃ and didn't decrease after high temperature reduction, which was ascribed
260 to the oxygen vacancies with Ce⁴⁺/Ce³⁺. Therefore, the surface O of the ALD-overcoated CeO_x-
261 Ni/Al₂O₃ resulted from both the hydroxyl groups and oxygen vacancies. For O 1s of the samples
262 after reduction, the surface O for ALD-overcoated CeO_x-Ni/Al₂O₃ was about 26.4 %, which was
263 higher than 17.2% for Ni/Al₂O₃, 20.1% for Al₂O₃-Ni/Al₂O₃, and 21.0% for iwCeO₂/Ni/Al₂O₃. For
264 the ALD-overcoating catalysts (i.e., CeO_x-Ni/Al₂O₃ and Al₂O₃-Ni/Al₂O₃), the surface O
265 significantly decreased after high-temperature reduction, which was ascribed to the removal of
266 hydroxyl groups at high temperature, whereas the CeO_x-Ni/Al₂O₃ catalyst still had a high amount
267 of surface oxygen. Comparing CeO_x-Ni/Al₂O₃ and Al₂O₃-Ni/Al₂O₃, the higher surface O of CeO_x-
268 Ni/Al₂O₃ should result from the oxygen vacancies. The higher amount of oxygen vacancies after

reduction for reduced $\text{CeO}_x\text{-Ni/Al}_2\text{O}_3$ was also confirmed by the spectra of Ce 3d. For the bi-reforming of methane, the high amount of oxygen vacancies could serve as the activation sites for CO_2 and enhance the catalytic performance.

Figure 2 and Figure S4 depict the XPS spectra for the reduced $\text{Ni/Al}_2\text{O}_3$, reduced $\text{CeO}_x\text{-Ni/Al}_2\text{O}_3$, reduced $\text{Al}_2\text{O}_3\text{-Ni/Al}_2\text{O}_3$, and reduced $\text{iwCeO}_2\text{/Ni/Al}_2\text{O}_3$ catalysts. For Ni 2p $3/2$, the peaks could be deconvoluted into different Ni species as metallic Ni at $\sim 852.1\text{ eV}$, NiO at $\sim 854.5\text{ eV}$, NiAl_2O_4 at $\sim 856.2\text{ eV}$, and satellite peaks due to shake-up phenomena, including $\text{Ni(0)}_{\text{sat}}$ at $\sim 857.8\text{ eV}$ and $\text{Ni(II)}_{\text{sat}}$ at $\sim 860.8\text{ eV}$ [38, 39]. Especially, the spinel NiAl_2O_4 was highly thermal stable with a reduction temperature of $\sim 800\text{ }^\circ\text{C}$, whereas NiO was easily reduced to Ni at high temperatures and highly reductive DRM reaction conditions. For the fresh catalyst (Figure S4), a high amount of NiAl_2O_4 indicates that the interaction between NiO and Al_2O_3 for ALD-prepared $\text{Ni/Al}_2\text{O}_3$ was very strong, which was due to the chemisorption-based growth mechanism [40]. Under this circumstance, the presence of NiAl_2O_4 after reduction treatment could be considered an incomplete reduction, which could lead to the activity loss. Comparing the different catalysts after reduction in Figure 2c and Figure S4e, the content of NiAl_2O_4 was 17.6% for $\text{Ni/Al}_2\text{O}_3$, 13.8% for $\text{CeO}_x\text{-Ni/Al}_2\text{O}_3$, 26.4% for $\text{Al}_2\text{O}_3\text{-Ni/Al}_2\text{O}_3$, and 14.1% for $\text{iwCeO}_2\text{/Ni/Al}_2\text{O}_3$. Based on the chemical states of Ni, the CeO_x ALD overcoating, or CeO_2 IW promoter significantly enhanced the reducibility, whereas the Al_2O_3 ALD overcoating exhibited a negative effect on the reducibility due to the formation of NiAl_2O_4 . In this case, CeO_x ALD effectively weakened the metal-support interaction (i.e., Ni- Al_2O_3 interaction) and released more Ni from NiAl_2O_4 , while Al_2O_3 ALD overcoating resulted in the formation of more NiAl_2O_4 .

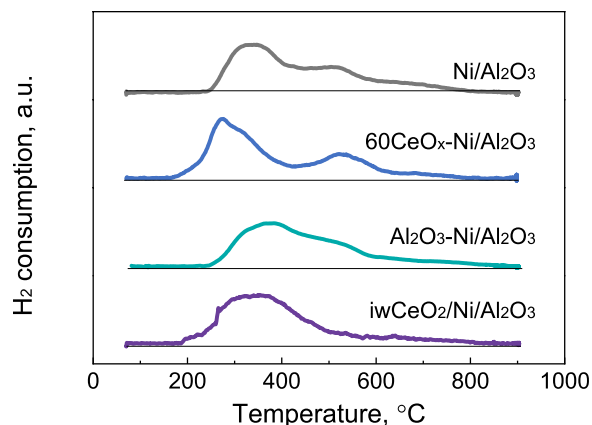


Figure 3. H₂-TPR spectra of Ni/Al₂O₃, 60CeO_x-Ni/Al₂O₃, Al₂O₃-Ni/Al₂O₃, and iwCeO₂/Ni/Al₂O₃.

To characterize the metal-support interactions and probe the effects of CeO_x ALD thin film, H₂-TPR was conducted for Ni/Al₂O₃, ALD-overcoated 60CeO_x-Ni/Al₂O₃, ALD-overcoated Al₂O₃-Ni/Al₂O₃, and IW-promoted iwCeO₂/Ni/Al₂O₃, as shown in Figure 3. Depending on the extent of Ni diffusion into the Al₂O₃ lattice, a higher reduction temperature is necessary for the species with a greater extent of diffusion/interaction and various species can be identified by TPR [42], including free NiO without any interaction, NiO-Al₂O₃ with interaction, and NiAl₂O₄ with spinel crystallization [40, 42]. For Ni/Al₂O₃, the dominant peak at ~340 °C was assigned to NiO, the peak at ~515 °C was assigned to NiO-Al₂O₃, and the peak >700 °C was assigned to NiAl₂O₄. Therefore, Ni(II) peaks in Ni/Al₂O₃ mainly consisted of free NiO and NiO-Al₂O₃, with a reduction degree at 72%. For ALD-overcoated 60CeO_x-Ni/Al₂O₃, the NiO peak was at ~280 °C and the NiO-Al₂O₃ peak was at ~520 °C. Clearly, CeO_x ALD facilitated the reduction process of the free NiO sites because the free NiO shifted to a lower temperature. The reduction degree for the 60CeO_x-Ni/Al₂O₃ was about 77%, indicating that the CeO_x ALD promoted the reduction of Ni sites. For ALD-overcoated Al₂O₃-Ni/Al₂O₃, the NiO peak and the NiO-Al₂O₃ peak almost remained in the

same position as those of Ni/Al₂O₃ with similar reduction degree at 71%, but the peaks became broadened, especially the NiO-Al₂O₃ peak, indicating that Al₂O₃ ALD films interacted with Ni sites. Regarding the reducibility, CeO_x ALD overcoating was beneficial to the catalytic activity as compared to Al₂O₃ as the overcoating material. As for iwCeO₂/Ni/Al₂O₃, the overall peak was shifted to lower temperatures, including ~320 °C for NiO and ~470 °C for NiO-Al₂O₃, with a reduction degree of 79%. Especially, the promoting effect of IW CeO₂ on NiO-Al₂O₃ might arise from the interaction between NiO-CeO₂ and the possible formation of NiO-CeO₂ after calcination, because the introduction of CeO₂ by the incipient wetness method requires a high temperature calcination at 500 °C. The difference between ALD-overcoated CeO_x-Ni/Al₂O₃ and IW-promoted iwCeO₂/Ni/Al₂O₃ could result from the morphology of ALD CeO_x films, because the role of CeO_x overcoating was prepared by surface modification instead of bulk transformation. Therefore, CeO_x ALD provided an efficient Ni-CeO_x interface and promoted the reducibility of Ni sites for the Ni/Al₂O₃ catalyst.

Although the stoichiometry of the bi-reforming of methane can be realized by the combination of SRM and DRM, the competition between SRM and DRM reactions should be considered for practical application. Especially, the surface reaction competition between SRM and DRM can be determined by the activation process of H₂O and CO₂ on the surface oxygen sites. To evaluate the surface oxygen and the CO₂ affinity, CO₂ temperature-program desorption (CO₂-TPD) was performed. According to the desorption temperature, the basic sites can be classified as weak basic sites < 200 °C for physical adsorption or Brønsted basic sites (e.g., -OH group), medium basic sites at 200-350 °C for Lewis acid-base pair Ce⁴⁺-O²⁻, and strong basic sites >350 °C for oxygen vacancies or oxygen defects [33, 43]. As shown in Figure 4, the peaks for the Ni/Al₂O₃ catalyst

mainly consisted of weak basic sites due to the acidic and -OH-rich properties of Al_2O_3 . For the same reason, Al_2O_3 ALD failed to enhance the medium basic sites or strong basic sites of the catalyst. In contrast, the addition of CeO_2 enhanced both the basic sites and strong basic sites by IW or ALD method, because of the basic nature of CeO_2 . However, the ALD-deposited CeO_x exhibited stronger basic properties in terms of quantity and strength, and thus a higher CO_2 affinity than that of the IW-prepared CeO_2 . For $\text{iwCeO}_2/\text{Ni}/\text{Al}_2\text{O}_3$, the introduction of CeO_2 by the IW method significantly increased the medium basic sites and provided a small amount of the strong basic sites. For $60\text{CeO}_x\text{-Ni}/\text{Al}_2\text{O}_3$, the deposition of CeO_x by ALD brought both medium basic sites and strong basic sites, especially for the strong basic sites. In comparison, the high amount of strong basic sites indicated there were more oxygen vacancies for the catalyst with CeO_x ALD overcoating. The high CO_2 affinities and special oxygen sites for CeO_x ALD overcoated catalyst should result from the thin-film structure and unique growth mode. It has been reported that the oxygen vacancies of CeO_2 can be tuned by its morphology and structure and a thin film structure enabled the high amount of oxygen vacancies [15-18]. As ascribed to the layer growth mode of ALD thin films [36], the $\text{Ni}/\text{Al}_2\text{O}_3$ catalyst with CeO_x ALD overcoating would have enhanced catalytic activity due to the oxygen vacancies of CeO_x .

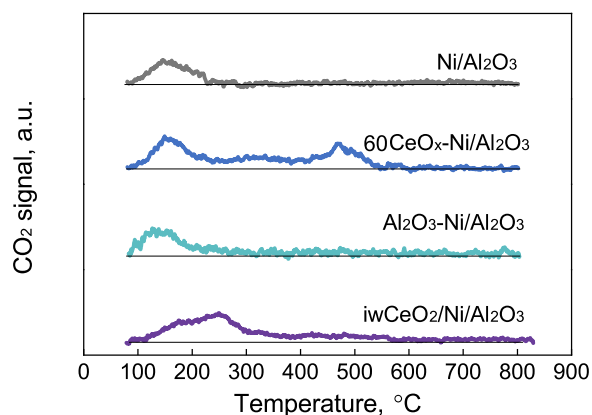


Figure 4. CO₂-TPD spectra of Ni/Al₂O₃, 60CeO_x-Ni/Al₂O₃, Al₂O₃-Ni/Al₂O₃, and iwCeO₂/Ni/Al₂O₃.

3.2. Catalytic performance for bi-reforming of methane

The equilibrium of bi-reforming of methane by co-feeding CH₄, H₂O, and CO₂ was calculated using the Gibbs reactor and Soave-Redlich-Kwong equation of state in ChemCAD, as shown in Figure S5. At varying temperatures, the equilibrium conversion of CH₄ was almost the same at all conditions, but the H₂/CO ratio was very different and varied with the feeding. Here, the H₂/CO ratio from the direct stoichiometric combination of SRM and DRM was used for the comparison with the equilibrium value (see Supporting Information). The difference between the direct stoichiometric value and the equilibrium value was mainly caused by the water-gas shift reaction or reverse water-gas shift reaction (WGS/RWGS). A higher temperature drives the equilibrium H₂/CO molar ratio towards 2, indicating a weaker effect of the WGS/RWGS at a higher temperature. Besides, the H₂/CO ratio exhibited a tunable ratio at varying inlet feed of CH₄, H₂O, and CO₂.

Bi-reforming of methane with CH₄/H₂O/CO₂=3/2/1 as a feedstock was conducted using the Ni/Al₂O₃ and ALD CeO_x-overcoated Ni/Al₂O₃ catalysts. Figures 5a and 5b show the CH₄ conversion and H₂/CO for BRM reaction at 850 °C. As shown in Figure 5a, the CH₄ conversion of Ni/Al₂O₃ reached 61.9% at the initial stage, and then gradually decreased to 56.4% after 72 h at 850 °C. In contrast, the CeO_x-overcoated Ni/Al₂O₃ catalyst exhibited better stability and activity. Notably, all CeO_x-overcoated Ni/Al₂O₃ catalysts exhibited an activation process in the initial 5 h of reaction, which might be ascribed to the formation of CeAlO₃ and further reduction of NiAl₂O₄

to metallic Ni, as discussed in our previous work [40, 44], and then a stable conversion could be reached. In this work, 60 cycles of CeO_x exhibited an optimal effect on the Ni/Al₂O₃ catalyst for the BRM reaction. The highest conversion at 87.2% was achieved for the 60CeO_x-Ni/Al₂O₃ catalyst due to the optimum loading of the CeO₂ overcoating with 60 cycles of CeO₂ ALD, which is much better than that of the uncoated, 10CeO_x-Ni/Al₂O₃, 30CeO_x-Ni/Al₂O₃, and 90CeO₂-Ni/Al₂O₃ catalysts. In Figure 5b, the H₂/CO of Ni/Al₂O₃ and CeO_x-overcoated Ni/Al₂O₃ reached ~2.05, which is close to the value of 2 for the stoichiometric combination DRM/SMR with a feedstock ratio of CH₄/H₂O/CO₂=3/2/1.

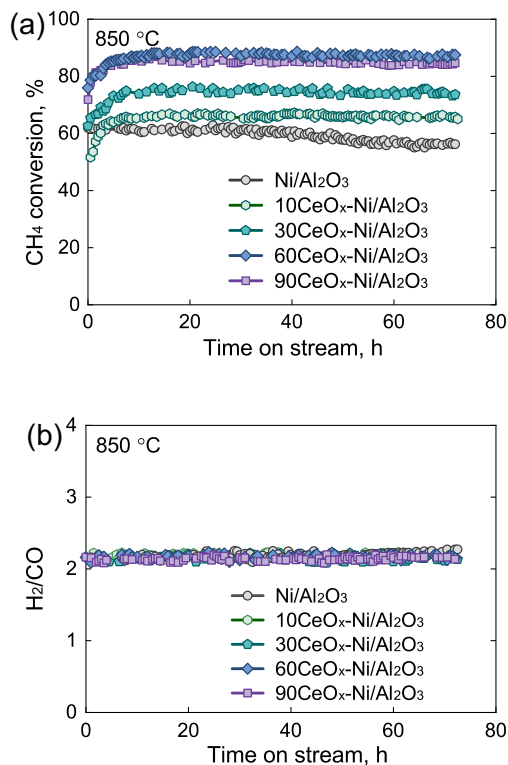


Figure 5. (a) CH₄ conversion and (b) H₂/CO ratio of BRM as a function of time on stream using Ni/Al₂O₃, 10CeO_x-Ni/Al₂O₃, 30CeO_x-Ni/Al₂O₃, 60CeO_x-Ni/Al₂O₃, and 90CeO_x-Ni/Al₂O₃. Reaction conditions: 50 mg catalyst, 30 mL/min CH₄, 10 mL/min CO₂, 20 mL/min H₂O (gas phase), at 850 °C.

385

386 Bi-reforming of methane with $\text{H}_2\text{O}/\text{CO}_2/\text{CH}_4=2/1/3$ was also tested at 750 °C, as shown in Figure

387 6. The deactivation of $\text{Ni}/\text{Al}_2\text{O}_3$ at 750 °C was more severe than the test at 850 °C using the same

388 catalyst. The CH_4 conversion for $\text{Ni}/\text{Al}_2\text{O}_3$ decreased from 39.4% to 19.8% in 72 h, which could

389 be ascribed to the oxidation of the Ni surface and coke formation at a lower reaction temperature.

390 The Al_2O_3 ALD overcoated $\text{Al}_2\text{O}_3\text{-Ni}/\text{Al}_2\text{O}_3$ catalyst and the CeO_2 IW promoted $\text{iwCeO}_2/\text{Ni}/\text{Al}_2\text{O}_3$

391 catalyst exhibited better stability than that of $\text{Ni}/\text{Al}_2\text{O}_3$, but there was still gradual deactivation. In

392 contrast, the CeO_x ALD overcoated $60\text{CeO}_x\text{-Ni}/\text{Al}_2\text{O}_3$ catalyst greatly enhanced the stability and

393 activity for BRM, with a stable conversion at 53.5% during a test of 150 h. As for the product, the

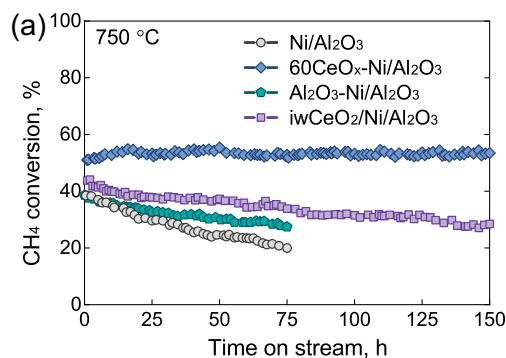
394 H_2/CO ratio of BRM using the $\text{Ni}/\text{Al}_2\text{O}_3$ catalyst increased from 2.45 to 2.88, which could be

395 ascribed to the limited water-gas shift reaction. For the $60\text{CeO}_x\text{-Ni}/\text{Al}_2\text{O}_3$ catalyst, the H_2/CO ratio

396 was kept at ~ 2.34 . Therefore, the CeO_x ALD overcoating successfully decorated the Ni sites and

397 enhanced the catalytic performance due to its high oxygen vacancy properties and sufficient Ni-

398 CeO_x interface.



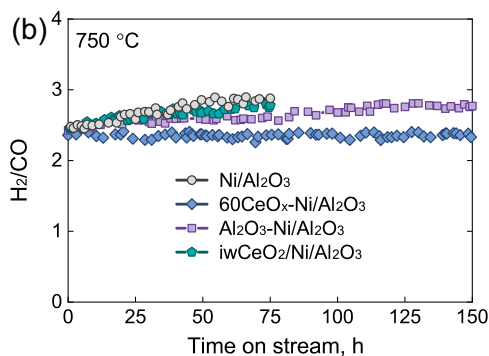


Figure 6. (a) CH_4 conversion and (b) H_2/CO ratio of BRM as a function of time on stream using $\text{Ni}/\text{Al}_2\text{O}_3$, $60\text{CeO}_x\text{-Ni}/\text{Al}_2\text{O}_3$, $\text{Al}_2\text{O}_3\text{-Ni}/\text{Al}_2\text{O}_3$, and $\text{iwCeO}_2/\text{Ni}/\text{Al}_2\text{O}_3$ as catalysts. Reaction conditions: 50 mg catalyst, 30 mL/min CH_4 , 10 mL/min CO_2 , and 20 mL/min H_2O (gas phase), and 750 °C.

The catalytic behavior of uncoated $\text{Ni}/\text{Al}_2\text{O}_3$ and $60\text{CeO}_x\text{-Ni}/\text{Al}_2\text{O}_3$ for methane reforming was systematically tested at different temperatures. Figure 7 depicts the CH_4 conversion and H_2/CO molar ratio for BRM with an inlet feed of $\text{H}_2\text{O}/\text{CO}_2/\text{CH}_4=2/1/3$ at different temperatures. In Figure 7a, the enhanced activity was observed for $60\text{CeO}_2\text{-Ni}/\text{Al}_2\text{O}_3$ at varying temperatures, verifying the promoting effects of CeO_x ALD overcoating. In Figure 7b, the H_2/CO ratio for uncoated $\text{Ni}/\text{Al}_2\text{O}_3$ and $60\text{CeO}_x\text{-Ni}/\text{Al}_2\text{O}_3$ was higher than the value based on the stoichiometric combination (i.e., $\text{H}_2/\text{CO}=2$) or the equilibrium ratio, especially at low temperatures. On one hand, the deviation between the practical H_2/CO ratio of BRM products and the equilibrium H_2/CO ratio might be explained by the severe water gas shift reaction. On the other hand, BRM is based on the catalytic dissociation of CH_4 on Ni sites and the following oxidation by H_2O or CO_2 , so the H_2/CO ratio in the products should be directly related to the activation process of H_2O or CO_2 . Therefore, the difference of H_2/CO ratio for the reaction catalyzed by $\text{Ni}/\text{Al}_2\text{O}_3$ and $60\text{CeO}_2\text{-Ni}/\text{Al}_2\text{O}_3$ indicated

that CeO_x overcoating could affect the reactant activation. Therefore, the lower H_2/CO ratio for $60\text{CeO}_x\text{-Ni/Al}_2\text{O}_3$ indicated that the CeO_x overcoating could have a better capability in CO_2 activation, which was ascribed to the oxygen vacancies of CeO_x ALD.

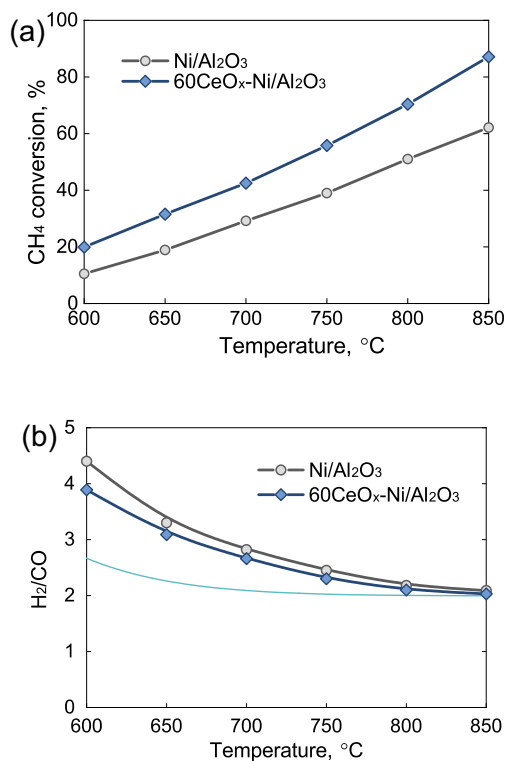


Figure 7. (a) CH_4 conversion and (b) H_2/CO ratio of BRM as a function of reaction temperature using $\text{Ni/Al}_2\text{O}_3$ and $60\text{CeO}_x\text{-Ni/Al}_2\text{O}_3$. Reaction conditions: 50 mg catalyst, 30 mL/min CH_4 , 10 mL/min CO_2 , and 20 mL/min H_2O (gas phase).

Figure 8 shows the catalytic performance of uncoated $\text{Ni/Al}_2\text{O}_3$ and $60\text{CeO}_x\text{-Ni/Al}_2\text{O}_3$ at 750 °C and 850 °C with different ratios of $\text{H}_2\text{O}/\text{CO}_2/\text{CH}_4$ but $(\text{H}_2\text{O}+\text{CO}_2)/\text{CH}_4=1$ in the feed as the combination of DRM and SRM. In Figure 8a, the CeO_x ALD overcoating significantly enhanced the CH_4 conversion for $60\text{CeO}_x\text{-Ni/Al}_2\text{O}_3$, as compared to the uncoated $\text{Ni/Al}_2\text{O}_3$ under different feed conditions. For instance, the CH_4 conversion was 62.6% for $\text{Ni/Al}_2\text{O}_3$ and 87.6% for $60\text{CeO}_x\text{-Ni/Al}_2\text{O}_3$.

Ni/Al₂O₃ with a feed of H₂O/CO₂/CH₄=3/0/3 (which is the case of SRM) at 850 °C. Besides, it was noted that the H₂O/CO₂ ratio in the feed influenced the CH₄ conversion. For instance, the CH₄ conversion for 60CeO_x-Ni/Al₂O₃ with feed H₂O/CO₂/CH₄=0/3/3 (which is the case of DRM) was 86.2% at 850 °C, and a higher CH₄ conversion was achieved with a higher H₂O content ratio in the feed, reaching CH₄ conversion of 87.2% with a feed of H₂O/CO₂/CH₄=2/1/3, and 87.6% with a feed of H₂O/CO₂/CH₄=2/1/3. The higher conversion for high-content H₂O in feed is more significant for Ni/Al₂O₃, with CH₄ conversion at 750 °C reaching CH₄ conversion of 57.7% with H₂O/CO₂/CH₄=0/3/3 (DRM), 62.1% at H₂O/CO₂/CH₄=2/1/3, and 62.6% at H₂O/CO₂/CH₄=3/0/3 (SRM). The influence of H₂O in the feed is more significant at lower temperatures. At 750 °C, 60CeO_x-Ni/Al₂O₃ had a CH₄ conversion of 47.9% for DRM and 52.1% for SRM, and Ni/Al₂O₃ had a CH₄ conversion of 32.7% for DRM and 41.1% for SRM, indicating that the effects of H₂O on CH₄ conversion were less significant for 60CeO_x-Ni/Al₂O₃. The better performance with a higher H₂O content in the feed might be ascribed to the activation of CO₂. The H₂/CO ratio at 850 °C for both catalysts was close to the equilibrium value, whereas the H₂/CO ratio at 750 °C was far from the equilibrium value, especially for Ni/Al₂O₃. Similar to the previous discussion, the H₂/CO ratio might be affected by the water-gas shift reaction and the activation process for H₂O or CO₂. It seems that the CeO_x overcoating could enhance the CO₂ activation and achieve a H₂/CO ratio which was close to the equilibrium value.

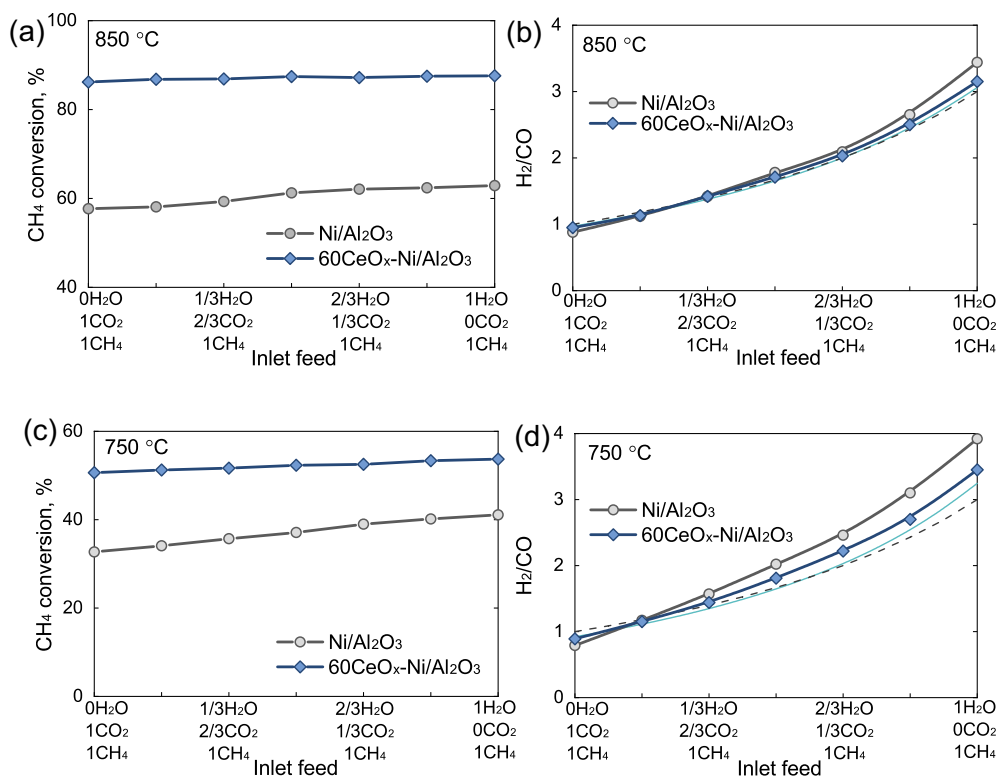


Figure 8. (a) CH_4 conversion and (b) H_2/CO ratio of BRM as a function of feed conditions using $\text{Ni}/\text{Al}_2\text{O}_3$ and $60\text{CeO}_x\text{-Ni}/\text{Al}_2\text{O}_3$ as catalysts at 850°C . (c) CH_4 conversion and (d) H_2/CO ratio of BRM as a function of feed conditions using $\text{Ni}/\text{Al}_2\text{O}_3$ and $60\text{CeO}_x\text{-Ni}/\text{Al}_2\text{O}_3$ as catalysts at 750°C . Reaction conditions: 50 mg catalyst and inlet feed $(\text{H}_2\text{O}+\text{CO}_2)/\text{CH}_4=1$.

H_2 pulse chemisorption was conducted to demonstrate the confinement effects and the promoting effects of CeO_x overcoating on $\text{Ni}/\text{Al}_2\text{O}_3$ for BRM reaction, as shown in Figure 9. With the increase in the cycle number of CeO_x ALD overcoating, the Ni surface area exhibited a decreasing trend, which indicates that the CeO_x overcoating partially covered the Ni surface and confined the Ni sites. The turnover frequency (TOF) was also calculated to investigate the intrinsic reaction activity with the order as follows: $90\text{CeO}_x\text{-Ni}/\text{Al}_2\text{O}_3 \approx 60\text{CeO}_x\text{-Ni}/\text{Al}_2\text{O}_3 > 30\text{CeO}_x\text{-Ni}/\text{Al}_2\text{O}_3 >$

Ni/Al₂O₃. The increasing TOF value with the increase in the ALD cycle number indicates that the CeO_x overcoating enhanced the intrinsic reaction rate.

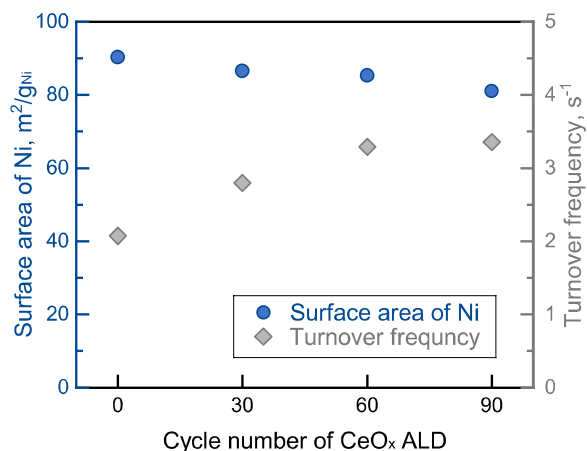


Figure 9. Ni surface area based on H₂-chemisorption and turnover frequency of methane on Ni sites for bi-reforming of methane as the function of CeO_x ALD cycle number on Ni/Al₂O₃.

3.3. Characterizations of spent catalysts

The sintering of Ni NPs is generally one of the main reasons for catalyst deactivation. TEM was used to investigate the Ni NPs size for the spent catalysts in Figure 10. For the spent Ni/Al₂O₃ catalyst in Figure 10a, the average size for Ni NPs was 24.6 ± 5.2 nm. For the spent 60CeO_x-Ni/Al₂O₃ catalyst in Figure 10b, the average size for Ni was 18.4 ± 3.8 nm. The presence of CeO_x ALD overcoating greatly prevented the mobilization of Ni NPs, possibly due to the Ni-CeO_x interaction or the geometric confinement effect of CeO_x coating [45], thus preventing the sintering of Ni NPs and enhancing the stability of the Ni NPs.

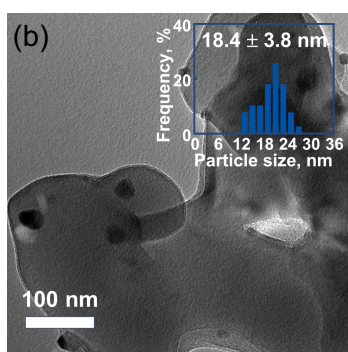
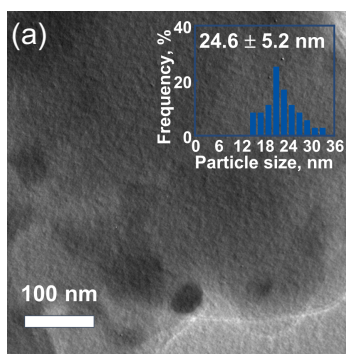
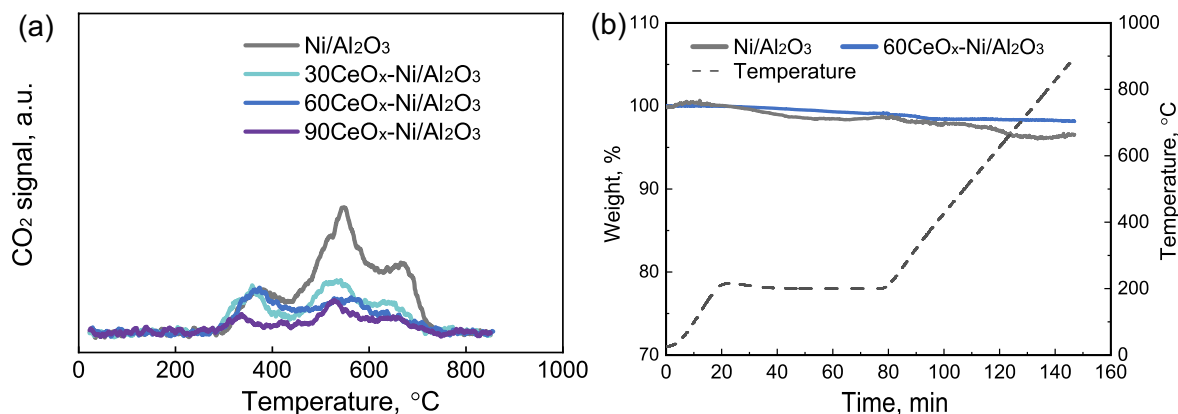


Figure 10. TEM images of (a) spent Ni/Al₂O₃ and (b) spent 60CeO_x-Ni/Al₂O₃ after bi-reforming of methane reaction at 850 °C for 72 h. The inset images show the size distribution of Ni NPs.

During SRM or DRM, the catalytic dissociation of methane on metal sites is generally considered as the initial step to generate H and CH_x (x=0-3) and the oxidants (H₂O or CO₂) will undergo dissociation and activation for the oxidation of CH_x. However, the side reactions (CH₄ cracking and Boudouard reaction) share the same species as carbon intermediates in the elementary step and inevitably result in carbon growth [10, 13]. During methane reforming, the carbon formation resulted from the side reactions and the low oxidation rate of coke by the reactants (i.e., H₂O and CO₂). To determine the carbon growth rate during the bi-reforming of methane, O₂-TPO was conducted on the spent catalysts. As shown in Figure 11a, spent Ni/Al₂O₃, spent 30CeO_x-Ni/Al₂O₃, spent 60CeO_x-Ni/Al₂O₃, and spent 90CeO_x-Ni/Al₂O₃ after bi-reforming of methane at 850 °C for

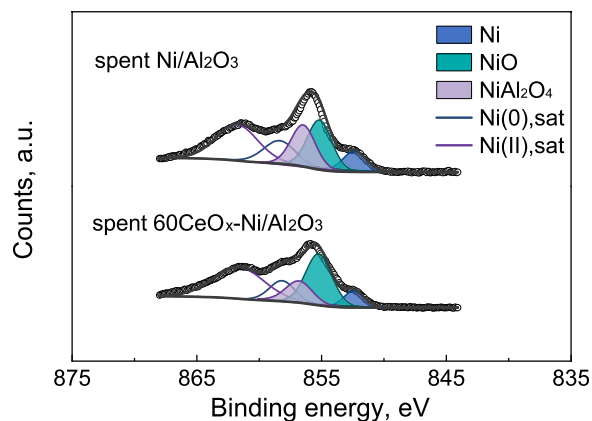
72 h ($\text{H}_2\text{O}/\text{CO}_2/\text{CH}_4=2/1/3$) were tested. The oxidation temperature of the surface carbon on these catalysts ranged from 300 to 750 °C, indicating different carbon species. According to the oxidation temperature, the chemical composition and crystallization of carbon can be determined. The carbon peak at <400 °C was assigned to the carbidic carbon (C_α), the carbon peak at 400-600 °C was assigned to the amorphous carbon (C_β), and the carbon peak at > 600 °C was assigned to the graphitic carbon (C_γ) [46, 47]. In this work, all three carbon species resulted from the bi-reforming of methane reaction, especially for the amorphous carbon and graphitic carbon. As for the catalysts with CeO_x ALD overcoating, there exhibited a great decrease in the carbon amount, mainly for the amorphous carbon and graphitic carbon. Studies showed that further graphitization growth was catalyzed on the large Ni NPs and insufficient oxidation rate. The CeO_x overcoating on Ni NPs by made the Ni sites discontinuously exposed, then limited the graphitization growth. Besides, the oxygen sites on CeO_x , especially the oxygen vacancies, provided the activation sites for CO_2 or H_2O and enabled the high concentration of surface O for carbon oxidation. Therefore, a decreasing amount of carbon deposition was found with the increase in the number of CeO_x ALD cycles. TGA was also conducted to determine the carbon deposition on spent $\text{Ni}/\text{Al}_2\text{O}_3$ and spent $60\text{CeO}_x\text{-Ni}/\text{Al}_2\text{O}_3$, as shown in Figure 11b. The catalysts first underwent a preheating process at 200 °C to remove any moisture. When the temperature ramped from 200 to 900 °C, the weight of $\text{Ni}/\text{Al}_2\text{O}_3$ decreased from 98.6% to 96.5%, indicating that 2.1 wt.% coke was detected. Besides, the decrease at ~120 min indicates the existence of graphitic carbon. In comparison, the weight of $60\text{CeO}_x\text{-Ni}/\text{Al}_2\text{O}_3$ decreased from 99.0% to 98.2%, indicating 0.8 wt.% coke was detected. The lower coke amount was ascribed to the activation sites of H_2O and CO_2 on Ni-CeO_x interface. Therefore, the suppressing effects of CeO_x overcoating on coking was confirmed for $\text{Ni}/\text{Al}_2\text{O}_3$ in the methane reforming.

515



516

517 Figure 11. (a) O₂-TPO of spent Ni/Al₂O₃, 30CeO_x-Ni/Al₂O₃, 60CeO_x-Ni/Al₂O₃, and 90CeO_x-
 518 Ni/Al₂O₃, (b) TGA of the spent Ni/Al₂O₃ and spent 60CeO_x-Ni/Al₂O₃. Spent catalysts underwent
 519 bi-reforming of methane at 850 °C for 72 h (H₂O/CO₂/CH₄ = 2/1/3).



520

521 Figure 12. XPS spectra of Ni 2p_{3/2} of spent Ni/Al₂O₃ and spent 60CeO_x-Ni/Al₂O₃ after bi-
 522 reforming of methane at 850 °C for 72 h (H₂O/CO₂/CH₄ = 2/1/3).

523 XPS spectra were collected using the spent Ni/Al₂O₃ and spent 60CeO_x-Ni/Al₂O₃ catalysts after
 524 bi-reforming of methane at 850 °C for 72 h, as shown in Figure 12 and Figure S6. For Ni 2p_{3/2},
 525 there was 19.9% NiAl₂O₄ for spent Ni/Al₂O₃ and 13.2% NiAl₂O₄ for spent 60CeO_x-Ni/Al₂O₃. This
 526 indicates that the CeO_x overcoating enhanced the reducibility of NiAl₂O₄. Besides, it was noticed

that there was more metallic Ni for the spent 60CeO_x-Ni/Al₂O₃ catalyst than that of spent Ni/Al₂O₃, which demonstrates that the CeO_x overcoating enhanced the reducibility and helped prevent the Ni nanoparticles from oxidation. The more metallic Ni sites by CeO_x overcoating means better utilization of Ni sites and better catalytic performance. Besides, for the O 1s spectra, the 60CeO_x-Ni/Al₂O₃ catalyst still had a high amount of surface oxygen after the reaction process, indicating that the oxygen species of CeO_x overcoating was stable during the reaction.

3.4. Mechanism of performance enhancement by CeO_x ALD overcoating

In this work, the effects of CeO_x ALD overcoating on Ni/Al₂O₃ for bi-reforming of methane was systematically studied. The mechanism of performance enhancement was proposed, as shown in Figure S7. The CeO_x ALD overcoating was successfully deposited onto Ni/Al₂O₃ and a beneficial Ni-CeO_x interface was formed. The CeO_x ALD overcoating exhibited its unique chemical properties for enhanced performance as compared to the ALD Al₂O₃ or IW CeO₂ promoter. Compared to the lower reducibility of the Al₂O₃ ALD coated Ni/Al₂O₃ catalyst due to the formation of NiAl₂O₄ during Al₂O₃ ALD process, the CeO_x ALD overcoating greatly improved the reducibility of Ni(II) and prevented the oxidation of the active Ni NPs. Besides, CeO_x was oxygen-deficient in non-stoichiometric form, resulting in the high concentration of the oxygen vacancies. The high oxygen vacancies in CeO_x ALD overcoating CeO₂ promoter provided higher activity in the CO₂ activation process and promoted the catalytic performance.

4. Conclusion

In this work, Ni/Al₂O₃ catalyst was prepared by depositing Ni NPs on Al₂O₃ NPs by ALD, followed by CeO_x ALD overcoating on Ni/Al₂O₃ catalyst with different numbers of cycles (i.e.,

10, 30, 60, and 90). The catalytic performance of CeO_x-Ni/Al₂O₃ was investigated for the bi-reforming of methane reaction. Based on TEM analysis, the Ni NPs size for the pristine Ni/Al₂O₃ catalyst was about 2.7 nm and the Ni size for the 60CeO_x-Ni/Al₂O₃ catalyst was about 2.9 nm, which indicates that the CeO_x ALD coating didn't change the morphology of Ni NPs due to its mild temperature ALD conditions. Based on XPS and CO₂-TPD, CeO_x ALD overcoating was found to be in non-stoichiometric form with a high amount of Ce(III) and oxygen vacancies, which might be ascribed to the unique ALD growth process. Besides, the reduction process for the catalyst led to a further reduction of Ce(IV) to Ce(III) and generated more oxygen vacancies, which acted as the CO₂ activation sites and achieved a good balance between SRM and DRM. Based on TPR analysis, CeO_x ALD also enhanced the reducibility of Ni NPs and helped keep Ni in the metallic state. For the bi-reforming of methane, CeO_x ALD significantly improved the activity and stability and achieved a better control in the H₂/CO ratio at the designed H₂O/CO₂/CH₄ feed. For BRM at 850 °C with H₂O/CO₂/CH₄=2/1/3, which was intended to produce H₂/CO at 2, the CH₄ conversion was ~61.9% for pristine Ni/Al₂O₃ and 87.2% for 60CeO_x-Ni/Al₂O₃, with H₂/CO molar ratio at ~2.05 for both catalysts. For BRM at 750 °C with H₂O/CO₂/CH₄=2/1/3, the CH₄ conversion was ~39.4% with gradual deactivation for pristine Ni/Al₂O₃ and ~53.5% in a 150-h test for 60CeO_x-Ni/Al₂O₃. Besides, the H₂/CO varied from 2.45 to 2.88 for Ni/Al₂O₃ during a 75-h test and kept stable at 2.34 for 60CeO_x-Ni/Al₂O₃. Under the varying H₂O/CO₂/CH₄ feed conditions (keeping (H₂O+CO₂)/CH₄=1), the 60CeO_x-Ni/Al₂O₃ catalyst exhibited a closer H₂/CO value to the direct stoichiometric combination result of SRM and DRM than that of the Ni/Al₂O₃ catalyst. Based on TPO results of spent catalysts, CeO_x ALD significantly decreased the carbon formation, especially the amorphous carbon and graphitic carbon, because CeO_x ALD overcoating could

provide sufficient oxygen vacancies, which enhanced the oxidant activation to remove carbon intermediate and inhibited carbon formation.

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