

# Yaw-Adjusted Wind Power Curve Modeling: A Local Regression Approach

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## Abstract

Accurate estimation of wind power curves using field data is instrumental to several wind farm operations including productivity assessment, power output estimation, operations and maintenance, among others. Existing methods for estimating wind power curves mainly rely on environmental variables (e.g., wind speed, direction, density) as inputs to construct the wind-to-power relationship. This paper attempts to integrate yaw misalignment as an additional input to power curve models, constructing what is referred to hereinafter as “yaw-adjusted wind power curves.” Our analysis shows that integrating yaw misalignment into power curves is non-trivial, largely due to the overwhelming impact of environmental variables (mainly wind speed) on a turbine’s power output, which obscures the secondary effect of yaw errors on power production. In response, we propose a local-regression-based method which reconstructs the yaw-to-power relationship *conditional* on an effective neighborhood of environmental variables. Tested on operational data from two onshore wind turbines in France, our proposed approach achieves significant improvements, in terms of power estimation accuracy, relative to a set of prevalent statistical- and machine-learning-based power curve models.

*Keywords:* Local Regression, Power Curve, Wind Energy, Yaw Error

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## 1. Introduction

Wind power continues to be one of the fastest growing sources of clean energy worldwide. Despite its rapid growth, the uncertainty associated with generating electricity from wind remains a fundamental barrier that impedes its large-scale penetration into modern-day power systems. This uncertainty

stems from two main sources: (i) uncertainty in the wind resource, which is, arguably, one of the most challenging meteorological processes to predict, especially at the turbine level [1, 2]; and (ii) uncertainty in the wind-to-power conversion process, i.e. the conversion of the hub-height wind conditions experienced by a wind turbine into power output [3, 4, 5]. This work focuses on the latter, i.e., to develop accurate models for turbine-specific power output estimation. In the wind energy industry, an accurate estimation of a turbine’s power production is important to several key wind farm operations, including performance assessment [6, 7], power output prediction [8, 9], asset monitoring and prognostics [10, 11], and maintenance scheduling [12, 13].

Theoretically, the wind power,  $P$ , produced by a wind turbine is expressed as in (1), where  $\rho$  denotes the air density,  $A_w$  is the rotor swept area,  $v$  is the hub-height wind speed, and  $C_p$  is the power coefficient, which, in turn, depends on the tip speed ratio  $\lambda$  and the blade pitch angle  $\beta$ .

$$P = \frac{1}{2}\rho A_w C_p(\lambda, \beta) v^3. \quad (1)$$

From (1), it is clear that the power production of a wind turbine is primarily dependent on wind speed, as evident by the cubic speed-to-power relationship, but also on other environmental variables such as air density. Moreover, (1) assumes that the turbine’s rotor plane is perfectly perpendicular to the wind flow. In reality, this perfect alignment seldom happens, and the power produced by a wind turbine is further dependent on the yaw error (or misalignment), denoted hereinafter by  $\gamma$  [14].

In practice, the actual wind-to-power conversion process, however, does not fully adhere to the physical relationship in (1), but instead, follows the so-called “power curve”, which is typically defined as the functional mapping relating the hub-height wind speed with the associated wind power, and comprises four main regions, as shown in Figure 1(a). In the first region, the turbine barely produces any power, as the wind speed is less than the so-called cut-in speed,  $v_{cut-in}$ . In modern-day wind turbines, cut-in speeds range between 3 m/s to 5 m/s. In the second region, the power output rapidly increases, first in a convex-shaped pattern, which then turns into a concave-shaped pattern. The wind speed in this region ranges between  $v_{cut-in}$  and the rated speed, denoted in Figure 1(a) by  $v_{rated}$ , which refers to the minimum wind speed at which the maximal turbine capacity,  $P_{rated}$ , is reached. This second region is further divided into two sub-regions: Regions II-a (Maximum power point tracking or MPPT control) and II-b (Fixed speed control). In

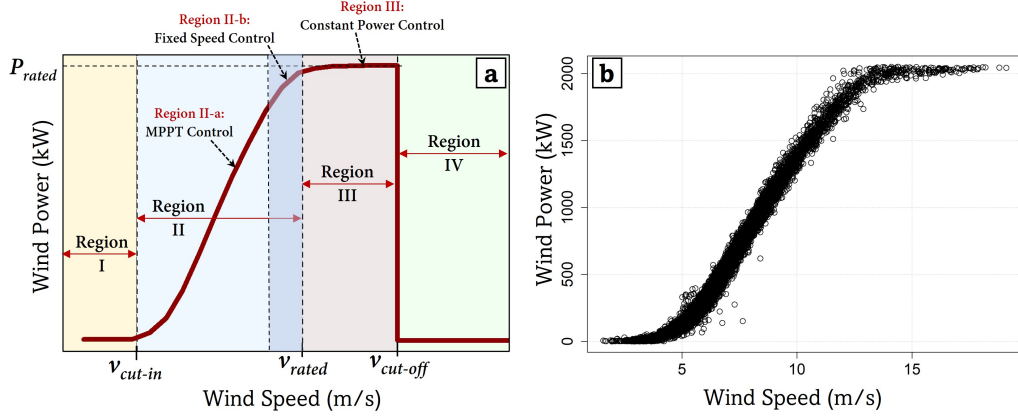


Figure 1: (a) Power curve of a typical wind turbine, with four regions defined by  $v_{cut-in}$ ,  $v_{rated}$ , and  $v_{cut-off}$ ; (b) Actual wind speed versus power for a typical wind turbine.

the former, both the power output and the rotor speed are within their permissible operational limits, while in the latter, the rotor speed operates at its maximum limit, until the turbine reaches its rated power,  $P_{rated}$ . In the third region, the power produced is maintained at the rated power level for damage-mitigating purposes. This rated power is maintained until the cut-off speed,  $v_{cut-off}$ , is reached, after which the turbine shuts down to protect its components and structures from extreme wind conditions (Region IV).

In practice, estimating a turbine's power curve using field data is challenging, because the actual power curve is rarely deterministic as the one displayed in Figure 1(a). Instead, as shown in Figure 1(b), it is contaminated by large uncertainties which are attributed to multiple sources that can be broadly categorized into *environmental* and *operational* factors. Environmental factors refer to the impact of additional weather variables (other than wind speed) that may impact a turbine's power output, such as air density, wind direction, turbulence, among others. Operational factors refer to the parameters related to the response of the turbine to its external environment, such as yaw errors, wake effects, aging and degradation, and measurement noise. An accurate power curve estimation should therefore seek to construct a functional relationship which accurately links the power output of a turbine to a set of environmental and operational factors, while taking into account the observational noise [4].

Towards that end, there is an extensive literature on estimating power curves using field data. Broadly, those efforts can be classified into paramet-

ric versus nonparametric approaches [4, 15]. Parametric power curve models assume a pre-determined functional form with a fixed set of parameters. Prior efforts in parametric power curve modeling include but are not limited to piecewise linear models [16], polynomial regression models [3], and logistic functions [7]. Nonparametric models, on the other hand, impose little assumptions about the functional form of the input-output relationship. Nonparametric power curve modeling approaches include copula-based methods [17], cubic splines [18], artificial neural networks [19], Gaussian Processes [11], and k-nearest neighbors (k-NN) [7].

To date, the large majority of the literature, whether using parametric or nonparametric methods, primarily uses wind speed as the sole input to wind power curve models [20]. The main limitation of those univariate models is that they largely overlook the impact of other environmental variables apart from wind speed. Recent efforts have investigated the potential of integrating additional environmental variables into power curve models [21, 22, 23, 24], such as air density, direction, and turbulence intensity. Those efforts concluded that multivariate power curve models, i.e. those that consider the impact of several environmental variables, are superior, in terms of estimation accuracy, to those that rely on wind speed as the sole input.

Little research, however, has been conducted to explore the merit of integrating operational variables into power curve modeling. Barring few works which studied the integration of rotor speed and pitch angle in power curve estimation [25, 26], our work, up to our knowledge, constitutes the first attempt to formally integrate yaw misalignment in estimating wind power curves, yielding what we refer to hereinafter as “yaw-adjusted power curves.”

We summarize the main contributions of this work as follows:

- We investigate the impact of yaw errors on power using field data. We discover that, counter-intuitively, a direct integration of yaw misalignment as an additional regressor into a multivariate power curve model does *not* improve the power curve estimation accuracy. We postulate that this is mainly due to the overwhelming impact of the environmental conditions (mainly wind speed) on a turbine’s power output, which obscures the secondary effect of yaw errors on a the power output, and prevents classical statistical models from leveraging such finer-scale yaw-to-power correlations for improved power output estimation.
- Motivated by this observation, we propose a power curve estimation method based on local regression which reconstructs the yaw-to-power

relationship *conditional* on an effective neighborhood of environmental variables. We show that this approach in integrating yaw misalignment into wind power curves unearths its underlying impact on power generation, therefore enabling the power curve model to leverage it as a significant predictor of wind power production.

- We perform a series of extensive tests using real-world data from a wind farm in France to demonstrate the merit of our proposed approach relative to prevalent statistical- and machine-learning-based power curve models, eventually concluding that significant improvements in power estimation accuracy, ranging from 3.21% to 32.13% are realizable.

## 2. Data Description and Analysis

The data used herein comprises 10-min measurements collected in 2013 from the La Haute Borne-Vaudeville-le-Haut wind farm in north eastern France. The wind farm comprises four wind turbines, as shown in Figure 2, and is operated by Engie Green (a subsidiary of Engie), which provides open access to its data [27]. The turbines have a rated capacity of 2050 kW, 80-m hub height, and rotor diameter of 82 m. Of interest to us are the following SCADA variables: wind speed  $v$  (m/s), wind power  $P$  (kW), wind direction  $\theta$  ( $^\circ$ ), nacelle angle  $\phi$  ( $^\circ$ ), and air temperature  $T$  (K). Note that the wind direction and nacelle angle measurements have been pre-corrected in the dataset (we used the corrected versions of those variables) since SCADA measurements collected behind the turbine’s rotor can be fairly noisy [28]. We also obtain co-located hourly air pressure measurements from Meteoblue [29], which we linearly interpolate to 10-min resolution. We filter the combined 10-min dataset by removing outliers (e.g., when  $P$  is negative or smaller than a certain threshold for a given wind speed).

The focus of our analysis is on two wind turbines (Turbine ID#: R80711 and R80721) for the period of September to December 2013. The turbines and time coverage were selected so that the turbines under study are up-stream relative to the prevailing wind, which is found to be dominantly south westerly during this time of the year—See Figure 2.

We also compute two additional environmental variables: air density, denoted by  $\rho$  and determined as in (2), and turbulence intensity, denoted by  $I$  and computed as the ratio of the 10-min standard deviation of the wind

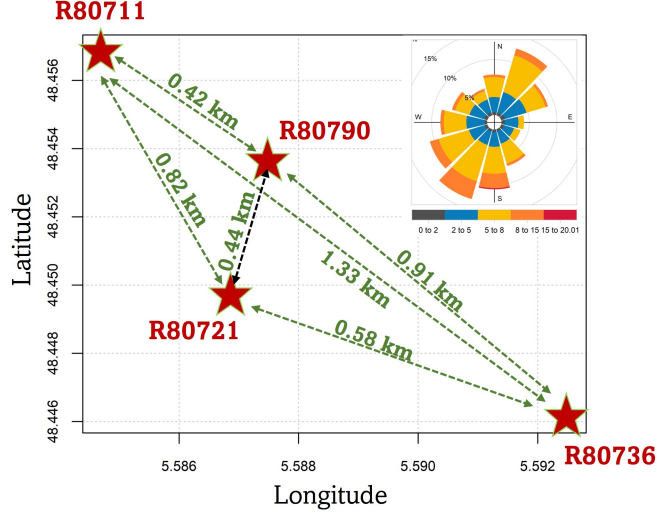


Figure 2: Map of the La Haute Borne-Vaudeville-le-Haut wind farm operated by Engie. Turbine locations are depicted by red stars. Numbers on arrows denote inter-turbine distances. The top right inset shows the wind rose plot at R80711, indicating a dominant south westerly wind during that time of the year.

157 speed (denoted by  $\sigma_v$ ) to its 10-min average  $v$ , such that  $I = \frac{\sigma_v}{v}$ .

$$\rho = 1.225 \times \frac{288.15}{T} \times \frac{B}{1013.3}, \quad (2)$$

158 where  $B$  denotes the interpolated 10-min air pressure in mbar.

159 In constructing power curves, the wind energy industry utilizes an air  
160 density correction, wherein the raw 10-min wind speed  $v$  is transformed to  
161 its air-density-corrected counterpart  $\tilde{v}$ , through the following expression:

$$\tilde{v} = v \times \left( \frac{\rho}{1.225} \right)^{\frac{1}{3}}. \quad (3)$$

162 The yaw misalignment,  $\gamma$ , is computed as the absolute difference between  
163 the corrected wind direction  $\theta$ , and the corrected nacelle angle  $\phi$ . The large  
164 majority of data points (96.16%) are found to have yaw errors in the  $[0^\circ, 20^\circ]$   
165 interval, as shown in Figure 3a. Figure 3b shows a scatter plot of wind speeds,  
166 yaw errors, and power measurements, color-coded with the yaw misalignment  
167 values (only for  $\gamma \leq 20^\circ$ ). Looking at Figure 3, there does not seem to

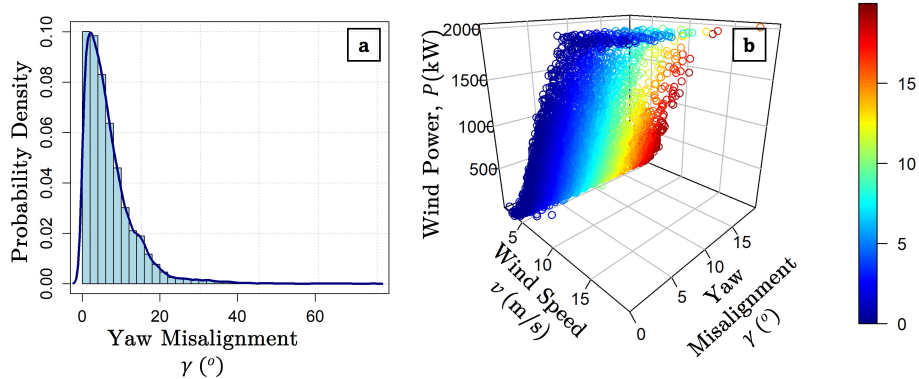


Figure 3: (a): Histogram of yaw misalignment values for turbine R80711. (b): 3D scatter plot of wind speed, yaw misalignment, and power for turbine R80711, color-coded by the yaw misalignment values ( $\gamma \leq 20^\circ$  is considered).

168 be stark negative correlations between the yaw error and the power output  
 169 ( $-0.24$  on a Pearson’s correlation scale).

170 Based on Figure 3, one may mistakenly rush to the conclusion that yaw  
 171 errors do not have a notable impact on the power output and should perhaps  
 172 be dropped from power curve modeling. We conjecture, however, that this  
 173 mainly attributed to the overwhelming impact of environmental variables  
 174 (largely wind speed) on wind power, which obscures the secondary effect of  
 175 yaw error on power output. Literature suggests that the power gain (or loss)  
 176 due to yaw misalignment is typically in the  $\sim 0\text{-}3\%$  range and is a function  
 177 of wind speed [30]. This means that slight changes in wind speed can easily  
 178 “mask” the power variations caused by yaw errors. For example, if both  
 179 wind speed and yaw error change by 1%, then the variation in power output  
 180  $P$  due to the change in wind speed alone will be much larger than that due  
 181 to yaw error. This confounding effect statistically obscures the underlying  
 182 impact of yaw errors on the turbine’s power output.

183 To reveal the impact of yaw errors on the power output, we have to  
 184 “marginalize” the effect of wind speed on power. To do so, we partition the  
 185 wind speed domain into narrow intervals of  $0.1$  m/s, and examine the yaw-  
 186 to-power relationship within each of those wind speed intervals. Within each  
 187 interval, the variation in wind speed is small, thereby allowing us to “zoom  
 188 in” and explore potential yaw-to-power correlations. Figure 4(a-c) shows the  
 189 results of this partitioning exercise for three selected wind speed intervals:  
 190  $[4.00, 4.10]$  m/s,  $[5.60, 5.70]$  m/s, and  $[7.30, 7.40]$  m/s. Within each wind

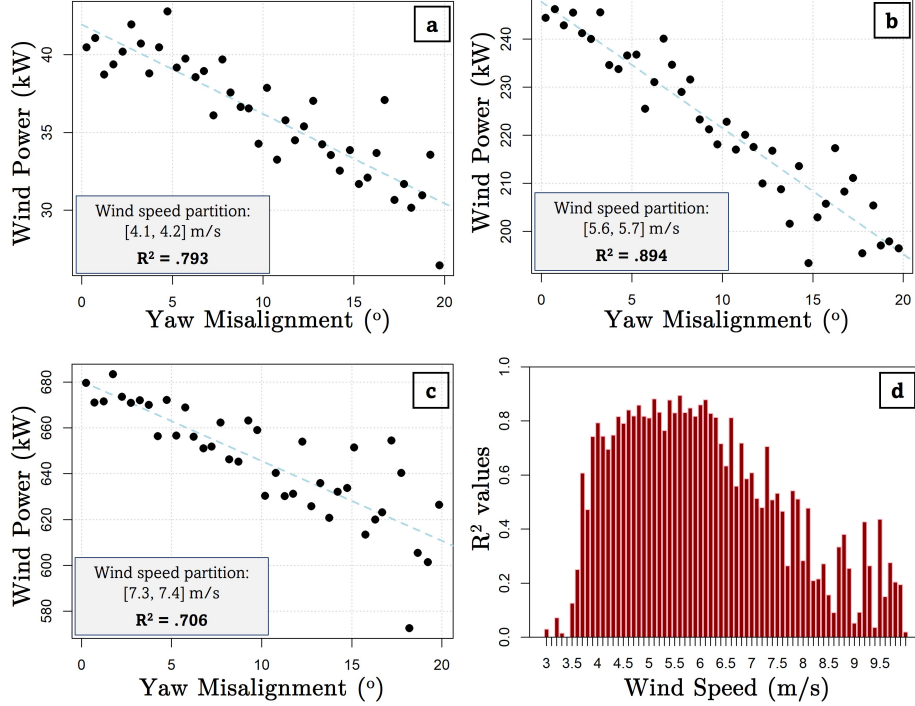


Figure 4: The yaw-to-power relationship for turbine R80711 within wind speed partitions of (a): [4.00, 4.10] m/s, (b): [5.60, 5.70] m/s, and (c): [7.30, 7.40] m/s, showing a strong negative linear association (yaw errors binned into  $0.5^\circ$  intervals) (d):  $R^2$  values of the yaw-to-power linear fits for all wind speed partitions between 3.00 and 10.00 m/s.

191 speed interval, the data suggest strong negative linear association between  
 192 yaw errors and power output (with  $R^2$  mostly in the 0.7-0.9 range). Figure  
 193 4d shows the  $R^2$  values over all wind speed intervals considered.

194 The analysis suggests that yaw error has a notable impact on power out-  
 195 put, particularly in the early and middle portions of Region II in a turbine's  
 196 power curve. However, such impact is only noticeably revealed when condi-  
 197 tioned on an effective neighborhood of environmental variables, or in other  
 198 words, once the impact of other environmental variables (primarily wind  
 199 speed) has been marginalized. A natural follow up question is how can we  
 200 leverage such yaw-to-power correlations in estimating a turbine's power curve  
 201 without relying on arbitrary partitions like those assumed in Figure 4. We  
 202 address this question in Section 3 by proposing a neighborhood-based ap-  
 203 proach for yaw-adjusted power curve estimation.



### 204 3. A Local Regression Model for Yaw-adjusted Wind Power Curves

205 Our yaw-adjusted power curve model builds on a recently proposed multi-  
 206 variate power curve method called “the additive multivariate kernel” (AMK)  
 207 [23]. This section therefore starts with a brief overview of the AMK method  
 208 and then proceeds to show how we extend it using a local regression formu-  
 209 lation in order to construct yaw-adjusted wind power curves.

#### 210 3.1. Overview of The Additive Multivariate Kernel (AMK) Method

211 Let  $\mathbf{x}^T = \{x_1, x_2, \dots, x_q\}$  be a set of explanatory variables which will be  
 212 used as inputs to the power curve model. For instance,  $\mathbf{x}$  can contain wind  
 213 speed, direction, air density, among others. Broadly speaking, our power  
 214 curve estimation task is to learn a functional mapping  $f : \mathbb{R}^q \rightarrow \mathbb{R}$  which  
 215 relates  $\mathbf{x}$  to the power output  $P$ , given a set of training data denoted by  
 216  $\mathcal{D} = \{\mathbf{x}_i^T, P(\mathbf{x}_i)\}_{i=1}^n$ . The estimated response surface,  $\hat{f}$ , constitutes the final  
 217 power curve which will be used to make turbine-specific power predictions.

218 To integrate additional environmental variables beside wind speed (e.g.,  
 219 wind direction, air density) into wind power curves, kernel regression (KR)  
 220 has been proposed in the past, due to its simplicity and attractive local  
 221 modeling capabilities [31]. KR is essentially a nonparametric local regression  
 222 model which uses the Nadaraya-Watson estimator [32], expressed in (4), to  
 223 obtain a localized, yet smooth estimate of  $f(\mathbf{x}^*)$  at a target input  $\mathbf{x}^*$ .

$$\hat{f}(\mathbf{x}^*) = \frac{\sum_{i=1}^n K(\mathbf{x}^*, \mathbf{x}_i) P(\mathbf{x}_i)}{\sum_{i=1}^n K(\mathbf{x}^*, \mathbf{x}_i)}, \quad (4)$$

224 where  $K(\mathbf{x}^*, \mathbf{x}_i)$  is a kernel function, which, in essence, is a measure of similar-  
 225 ity between the target input  $\mathbf{x}^*$  and the  $i$ th training data point  $\mathbf{x}_i$ , thereby  
 226 dictating the contribution of the latter in determining  $\hat{f}(\mathbf{x}^*)$ . A popular  
 227 choice for  $K(\mathbf{x}^*, \mathbf{x}_i)$  is the multivariate Gaussian kernel defined as in (5).

$$K(\mathbf{x}^*, \mathbf{x}_i) = \prod_{j=1}^q K(x_j^*, x_{ij}) = \prod_{j=1}^q \exp\left(-\frac{1}{2} \frac{\|x_{ij} - x_j^*\|^2}{\lambda_j^2}\right), \quad (5)$$

228 where  $x_{ij}$  is the  $i$ th observation of the variable  $x_j$ , while  $x_j^*$  is the value of  
 229 the  $j$ th variable in  $\mathbf{x}^*$ . The set of parameters,  $\lambda_1, \dots, \lambda_q$  dictate the width  
 230 of the univariate kernels, or in other words, the size of the effective local  
 231 neighborhood, whereas  $\|\cdot\|$  denotes the Euclidean distance.

232 KR has been successfully used to model bivariate power curves, with  
 233 wind speed and direction as inputs [31]. If more variables beyond speed and  
 234 direction are introduced, the multiplicative form of the kernel in (5) can cause  
 235 the KR method to run into the so-called “curse of dimensionality,” wherein  
 236 the number of data points within each high-dimensional neighborhood does  
 237 not allow for a reliable (or in some cases, even feasible) estimation of  $\hat{f}(\mathbf{x}^*)$ .  
 238 To remedy this limitation, the Additive Multivariate Kernel (AMK) method  
 239 was proposed by Lee *et al.* [23] to integrate several environmental variables  
 240 (in their paper, up to seven variables) like wind speed, direction, air density  
 241 into a multivariate power curve model.

242 Instead of relying on the multiplicative form of (4), AMK proposes to  
 243 compute  $\hat{f}(\mathbf{x}^*)$  as in (6).

$$\hat{f}(\mathbf{x}^*) = \frac{1}{q-2} \left[ \hat{f}_1(x_1^*, x_2^*, x_3^*) + \dots + \hat{f}_{q-2}(x_1^*, x_2^*, x_q^*) \right], \quad (6)$$

244 wherein  $\hat{f}_1(x_1^*, x_2^*, x_3^*)$ , ...,  $\hat{f}_{q-2}(x_1^*, x_2^*, x_q^*)$  are defined as in (4) using three-  
 245 dimensional Gaussian kernels. AMK chooses to always fix the two variables  
 246  $x_1$  and  $x_2$  in each of the multiplicative kernels as the wind speed and direction  
 247 respectively, such that  $x_1 = \tilde{v}$  and  $x_2 = \theta$ , while  $x_3, \dots, x_q$  denote additional  
 248 environmental variables such as density, humidity, or turbulence intensity.  
 249 Using the formulation in (6), AMK still uses multiplicative kernels to cap-  
 250 ture interactions in the input space, but restricts them to be the product of  
 251 three univariate kernels in order to ensure scalability in higher dimensions.  
 252 As a result, AMK was shown to yield significant improvements in estimat-  
 253 ing turbine-specific power relative to univariate and bivariate power curve  
 254 models. Readers can refer to [23, 33] for more details of the AMK method.

### 255 3.2. Towards Yaw-adjusted Power Curves: The YAMK Method

256 Our method, the Yaw-adjusted Additive Multivariate Kernel, or in short  
 257 YAMK, extends the AMK modeling framework to effectively integrate yaw  
 258 misalignment into a multivariate wind power curve. The idea behind YAMK  
 259 is to construct localized yaw-to-power regression models within the local  
 260 neighborhoods defined by AMK. This formulation is inspired by the prelim-  
 261 inary analysis in Section 2 wherein the effect of  $\gamma$  on  $P$  is only unearthed  
 262 once the impact of other environmental conditions has been marginalized.

263 In our work, we let  $\mathbf{x} := \{\tilde{v}, \theta, \rho, I\}$ , that is, the set of all environmental  
 264 variables. YAMK starts with a similar formulation to that of AMK expressed

in (6). The fundamental difference between YAMK and AMK, however, lies in how  $f_1, \dots, f_q$  are defined. Instead of relying on locally weighted averages as in (4), YAMK defines them as locally weighted polynomial regression models which take the yaw misalignment,  $\gamma$ , as a direct input. That is,  $\hat{f}_j(\mathbf{x}^*)$ ,  $\forall j = 1, \dots, q - 2$  is defined as in (7).

$$\hat{f}_j(\mathbf{x}^*) = g(\mathbf{x}^*)^T (\mathbf{G}^T \mathbf{K} \mathbf{G})^{-1} \mathbf{G}^T \mathbf{K} \mathbf{P}, \quad (7)$$

where  $\mathbf{P}$  is the  $n \times 1$  vector of power outputs, defined as  $\mathbf{P} = \{P(\mathbf{x}_1), \dots, P(\mathbf{x}_n)\}$ . We define  $g(\mathbf{x})^T := (1, \tilde{v}, \gamma)$ , while  $\mathbf{G}$  is the  $n \times 3$  regression matrix whose  $i$ th row corresponds to  $g(\mathbf{x}_i)^T$ . The  $n \times n$  diagonal matrix  $\mathbf{K}$  contains the kernel weights obtained via the AMK kernel structure. Including  $\tilde{v}$  as input to  $\mathbf{G}$  is motivated by its unique importance in estimating power output, while the inclusion of  $\gamma$  allows us to capture its localized impact on power output, conditional on the environmental conditions within its neighborhood.

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**Algorithm 1** The YAMK method for Power Curve Modeling

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- 1: *Input* training data  $\mathcal{D}^{tr} = \{\tilde{v}_i, \theta_i, \rho_i, I_i, \gamma_i, P_i\}_{i=1}^n$
  - 2: *Input* target inputs  $\mathcal{D}^{ts} = \{\tilde{v}_s^*, \theta_s^*, \rho_s^*, I_s^*, \gamma_s^*\}_{s=1}^S$
  - 3: *Determine* the kernel parameters  $\lambda_v, \nu_\theta, \lambda_\rho$ , and  $\lambda_I$ .
  - 4: **for**  $s \in \{1, \dots, S\}$  **do**
  - 5:     Construct  $\mathbf{K}_1$  and  $\mathbf{K}_2$  using the AMK kernel weights, such that their  $i$ th diagonal entries are computed as  $K(\tilde{v}_s^*, \tilde{v}_i)K(\theta_s^*, \theta_i)K(\rho_s^*, \rho_i)$  and  $K(\tilde{v}_s^*, \tilde{v}_i)K(\theta_s^*, \theta_i)K(\rho_s^*, I_i)$ , respectively.
  - 6:     Set  $g(\mathbf{x}_s^*) = \{1, \tilde{v}_s^*, \gamma_s^*\}$ , and  $\mathbf{G}$  as the correspondent  $n \times 3$  training input matrix, for which the  $i$ th row is defined as  $\{1, \tilde{v}_i, \gamma_i\}$ .
  - 7:     Estimate  $\hat{f}_1(\mathbf{x}_s^*)$  and  $\hat{f}_2(\mathbf{x}_s^*)$  using (7).
  - 8:     Predict at  $\mathbf{x}_s^* = \{\tilde{v}_s^*, \theta_s^*, \rho_s^*, I_s^*, \gamma_s^*\}$  using (9).
  - 9: **end for**
  - 10: **return** the final yaw-adjusted power curve, defined by  $\hat{\mathbf{P}} = \{\hat{f}(\tilde{v}_s^*, \theta_s^*, \rho_s^*, I_s^*, \gamma_s^*)\}_{s=1}^S$
- 

Algorithm 1 summarizes the framework of the YAMK method. At our disposal is a training dataset, denoted as  $\mathcal{D}^{tr} = \{\mathbf{x}_i, \gamma_i, P(\mathbf{x}_i)\}_{i=1}^n$ , and a set of target inputs, denoted by  $\mathcal{D}^* = \{\mathbf{x}_s^*, \gamma_s^*\}_{s=1}^S$ , for which a set of predictions are needed,  $\{\hat{f}(\mathbf{x}_s^*, \gamma_s^*)\}_{s=1}^S$ . For each variable in  $\mathbf{x}$ , we first find the set of univariate kernel bandwidth parameters. For wind speed, air density, and turbulence intensity, we use univariate Gaussian kernels. Since wind direction

283 is a circular variable, we use the Von Mises kernel, which is defined as in (8).

$$K_\nu(\theta^*, \theta_i) = \frac{\exp\{\nu \cos(\theta^* - \theta_i)\}}{2\pi I_0(\nu)}, \quad (8)$$

284 where  $I_0(\cdot)$  is the modified Bessel function of order 0, and  $\nu$  is the concentra-  
 285 tion parameter. The parameters for all the kernels, namely  $\lambda_v$ ,  $\nu_\theta$ ,  $\lambda_\rho$ , and  
 286  $\lambda_I$  are found using the direct plug-in (DPI) method [34, 35].

287 Once the kernel parameters have been estimated, we estimate the coeffi-  
 288 cients of the locally weighted polynomial regression models using (7), which  
 289 are then plugged in to make a prediction  $\hat{f}(\mathbf{x}^*)$  as in (9).

$$\hat{f}(\mathbf{x}^*) = \frac{1}{2} \left[ \hat{f}_1(\tilde{v}^*, \theta^*, \rho^*) + \hat{f}_2(\tilde{v}^*, \theta^*, I^*) \right]. \quad (9)$$

## 290 4. Results and Discussions

291 We test the performance of the YAMK method on the dataset described in  
 292 Section 2. Two case studies are presented, one for each wind turbine (Turbine  
 293 ID#: R80711 and R80721). We begin by describing the benchmarks, the  
 294 evaluation procedure, then present the numerical results and analyses.

### 295 4.1. Benchmarks

296 We compare the predictive performance of the YAMK approach to a  
 297 number of power curve modeling benchmarks, listed below as B1-B5:

298 (B1) *The Method of Bins* ( $BIN_{v,\rho}$ ) is a non-parametric approach for power  
 299 curve modeling described in the IEC 61400-12-1 standard [36]. It discretizes  
 300 the density-corrected wind speed domain into a number of bins, each with  
 301 bin width of 0.5 m/s, and then takes the average of the power values within  
 302 each bin as the estimated power, as expressed in (10).

$$\bar{v}_k = \frac{1}{n_k} \sum_{i=1}^{n_k} \tilde{v}_{ik} \quad \text{and} \quad \bar{P}_k = \frac{1}{n_k} \sum_{i=1}^{n_k} P(\tilde{v}_{ik}), \quad (10)$$

303 where  $n_k$  is the number of data points within the  $k$ th wind speed bin, while  
 304  $\bar{v}_k$  and  $\bar{P}_k$  are the average wind speed and power output within the  $k$ th bin,  
 305 respectively. The prediction for a target input,  $\mathbf{x}_s^*$ , is obtained as in (11).

$$\hat{f}(\mathbf{x}_s^*) = \sum_{k=1}^{\mathcal{K}} \mathbb{I}(\tilde{v}_s^* \in \mathcal{B}_k) \bar{P}_k, \quad (11)$$

where  $\mathcal{K}$  is the total number of bins,  $\mathbb{I}(\cdot)$  is the indicator function, and  $\mathcal{B}_k$  is the set of density-corrected wind speed values within the  $k$ th bin.

(B2-B3) *k nearest neighbors (kNN)*: kNN is widely used for power curve modeling [7]. It computes a local prediction at the  $s$ -th target input as the average of the outputs of its  $k$ -nearest neighbors, as expressed in (12).

$$\hat{f}(\mathbf{x}_s^*) = \frac{1}{k} \sum_{\mathbf{x}_i \in \mathcal{N}(\mathbf{x}_s^*)} P(\mathbf{x}_i). \quad (12)$$

We implement two variants of kNN. The first variant constructs a one-dimensional power curve by solely using the density-corrected wind speed as input, that is, in (12), we set  $\mathbf{x} := \{\tilde{v}\}$ . We call this method as  $\text{kNN}_{v,\rho}$  because it takes wind speed and air density (through the density correction) as inputs. The second variant, which we call  $\text{kNN}_{v,\rho,\gamma}$  directly integrates yaw misalignment  $\gamma$  as an additional input beside the density-corrected wind speed, that is, in (12), we set  $\mathbf{x} := \{\tilde{v}, \gamma\}$ .

We implement kNN using the `caret` package in the statistical programming language `R`. The number of nearest neighbors,  $k$ , has a significant impact on the final predictive performance, and is selected by heuristically searching for the value of  $k$  that minimizes the out-of-sample error [37].

(B4-B5) *Additive Multivariate Kernel (AMK)*: This is the kernel-based regression method proposed by Lee *et al.* [23] and explained in Section 3.1. Two variants of AMK are implemented. The first variant, denoted by  $\text{AMK}_{v,\theta,\rho,I}$ , is the same model proposed in [23], and uses  $\mathbf{x} := \{\tilde{v}, \theta, \rho, I\}$  in (6). Its kernel structure comprises the addition of two trivariate kernels (one for  $\{\tilde{v}, \theta, \rho\}$ , and another for  $\{\tilde{v}, \theta, I\}$ ), that are obtained as the product of three univariate kernels. This variant does not take yaw error into account, and unlike YAMK, computes the prediction as a local neighborhood average. The second variant,  $\text{AMK}_{v,\theta,\rho,I,\gamma}$ , augments this input set by  $\gamma$ , such that  $\mathbf{x} := \{\tilde{v}, \theta, \rho, I, \gamma\}$  in (6). Its kernel structure comprises the addition of three trivariate kernels (one for  $\{\tilde{v}, \theta, \rho\}$ , one for  $\{\tilde{v}, \theta, I\}$ , and one for  $\{\tilde{v}, \theta, \gamma\}$ ), that are formed by the product of three univariate kernels.

#### 4.2. Evaluation and Results

For evaluation, we implement  $K$ -fold cross validation, where we set the number of folds  $K = 5$ , as is typical in machine learning practice. Predictions are evaluated using the normalized root mean squared error (NRMSE),

Table 1: 5-fold average NRMSE of power curve models for turbines R80711 and R80721. Bold-faced values indicate best performance. Percentage improvements, denoted as % IMP, are computed relative to the best-performing method.

Method	Number of Inputs	Turbine 1 (R80711)	Turbine 2 (R80721)	Avg.	% IMP
$\text{BIN}_{v,\rho}$	2	2.585	2.260	2.423	32.13%
$\text{kNN}_{v,\rho}$	2	2.078	1.713	1.896	13.27%
$\text{kNN}_{v,\rho,\gamma}$	3	2.193	1.729	1.961	16.16%
$\text{AMK}_{v,\theta,\rho,I}$	4	1.827	1.570	1.699	3.21%
$\text{AMK}_{v,\theta,\rho,I,\gamma}$	5	1.890	1.588	1.739	5.46%
$\text{YAMK}_{v,\theta,\rho,I,\gamma}$	5	<b>1.780</b>	<b>1.508</b>	<b>1.644</b>	-

expressed as in (13). For  $S_k$  testing data points within the  $k$ th fold, the NRMSE of a power curve model  $\mathcal{M}$ , is given by:

$$\text{NRMSE}(\mathcal{M}) = \frac{1}{K} \sum_{k=1}^K \left[ \frac{100\%}{P_r} \sqrt{\frac{\sum_{s=1}^{S_k} [P(\mathbf{x}_s^*) - \hat{f}(\mathbf{x}_s^*)]^2}{S_k}} \right], \quad (13)$$

where  $P_r$  refers to the rated power. For both R80711 and R80721, the rated power is  $P_r = 2050$  kW.

Table 1 and Figure 5 show the averages and boxplots of the 5-fold NRMSE, respectively, across all methods for turbines R80711 and R80721. Looking at Table 1 and Figure 5, we can draw few key insights. First, one of the key findings is that a direct integration of yaw misalignment as an additional input to a multivariate power curve model does not lead to any improvement in the predictive performance (if any, it actually leads to a slight deterioration). This is evident by how  $\text{kNN}_{v,\rho,\gamma}$  and  $\text{AMK}_{v,\theta,\rho,I,\gamma}$  perform worse than  $\text{kNN}_{v,\rho}$ , and  $\text{AMK}_{v,\theta,\rho,I}$ , respectively.

The YAMK method, on the other hand, outperforms all of the benchmarks, with percentage improvements, on average, reaching up to 32.13% over the method of bins, and at least 3.21% relative to its closest competitor,  $\text{AMK}_{v,\theta,\rho,I}$ . The improvements appear to be more pronounced for turbine R80721 than R80711, which may be partly explained by the higher-on-average yaw errors for R80721 relative to R80711. Hence, the merit of leveraging the yaw-to-power correlations becomes more substantial.

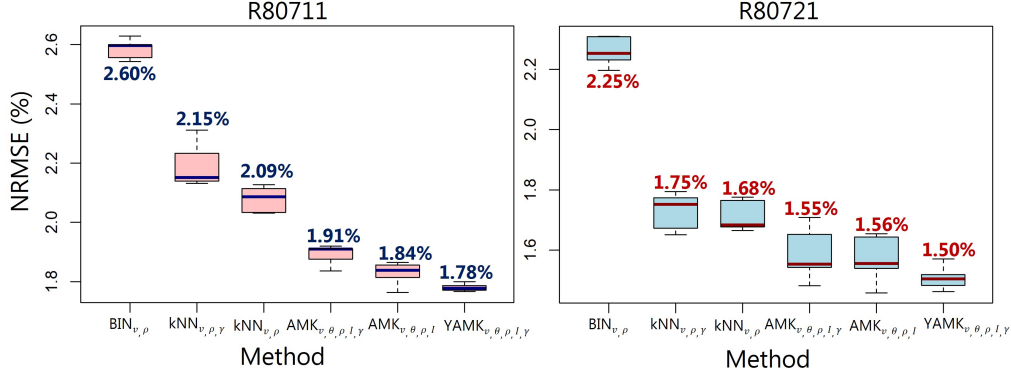


Figure 5: Boxplots of the NRMSE values across the five folds, for different methods. The numbers on top of the boxplots denote the median NRMSE value.

Figure 6 shows the estimated power curves for R80711 (left) and R80721 (right) separated into two groups: Group 1 (red circles) represents power predictions for testing observations that had yaw errors below the median yaw misalignment value ( $5.17^\circ$  for R80711 and  $5.51^\circ$  for R80721), while Group 2 represents those for which the yaw errors were higher than the median values. In both R80711 and R80721, the predicted power curves for the first group's data appear to dominate those for the second group, suggesting that YAMK effectively takes into account the influence of yaw errors on power predictions. The power gains (in %) of Group 1 relative to Group 2 are 1.73% and 3.18% for Turbines R80711 and R80721, respectively, which aligns with what has been shown in the literature [30].

The distribution of the prediction errors of the wind power reveals the accuracy of the prediction approach, wherein a power curve model with poor accuracy will have its prediction errors distributed widely, as opposed to a sharper, concentrated distribution for an accurate power curve model. Figure 7 shows the probability density distributions of the wind power prediction errors for three models:  $BIN_{v,\rho}$ ,  $AMK_{v,\theta,\rho,I,\gamma}$ , and  $YAMK_{v,\theta,\rho,I,\gamma}$ . As we can observe, the distribution of the prediction errors from  $BIN_{v,\rho}$  is relatively spread out. AMK's distribution of prediction errors is better than that of  $BIN_{v,\rho}$  highlighting the merit of integrating additional environmental variables. YAMK's error distribution is the sharpest among the three models, suggesting the importance of effectively integrating yaw as an additional operational input. This is further confirmed in Figure 7(b) and (d) which show

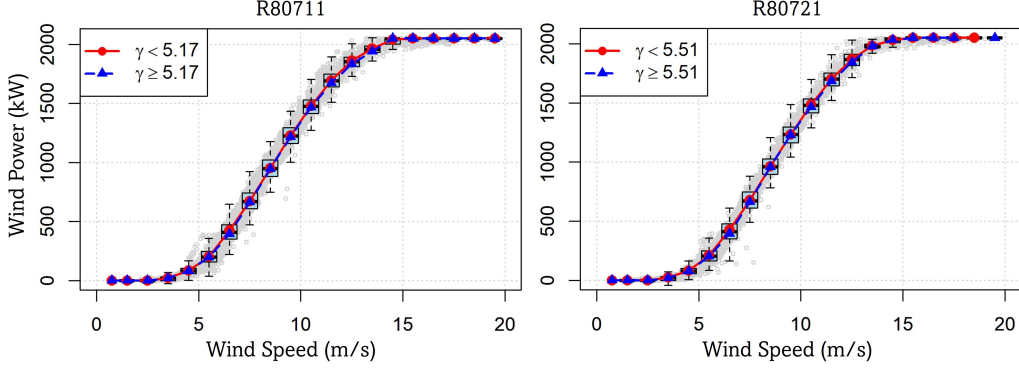


Figure 6: Final power curves for R80711 (left) and R80721 (right), separated into two groups: Group 1 (red circles): yaw errors below the median yaw misalignment value ( $5.17^\circ$  for R80711 and  $5.51^\circ$  for R80721); Group 2 (blue squares): yaw errors above the median yaw misalignment value ( $5.17^\circ$  for R80711 and  $5.51^\circ$  for R80721). Predicted power gains (in %) between the two groups are 1.73% and 3.18% for R80711 and R80721, respectively.

the actual versus predicted wind power values from  $\text{YAMK}_{v,\theta,\rho,I,\gamma}$ , which closely match with the  $45^\circ$  line, indicating closeness to a perfect prediction.

Finally, we would like to assess the performance of  $\text{YAMK}$  across different wind speed values. Figure 8 shows the median absolute error (scaled by  $P_r$ ) versus the corresponding wind speed values (wind speed bins of 1 m/s are used), for four methods:  $\text{YAMK}_{v,\theta,\rho,I,\gamma}$  (black circles),  $\text{AMK}_{v,\theta,\rho,I,\gamma}$  (red triangles),  $\text{kNN}_{v,\rho}$  (green squares), and  $\text{BIN}_{v,\rho}$  (blue diamonds). Errors from both turbines have been pooled to produce this analysis. Again, we can immediately see that  $\text{YAMK}$  significantly improves over all methods across almost all wind speed ranges. A closer look reveals that  $\text{YAMK}$ 's largest improvements over its closest competitor,  $\text{AMK}$ , manifests itself in the early and middle portions of Region II of a turbine's power curve (between 3.5 and 11 m/s). As the wind speed approaches the rated power region (Region III), the performance of  $\text{YAMK}$  gradually converges towards that of  $\text{AMK}$  (especially noticeable at wind speeds higher than 12 m/s). This finding is in line with the analysis in Figure 4 which suggests that the impact of yaw on power is more articulated for the early and middle portions of Region II in a turbine's power curve. We also note that the relative improvements of  $\text{YAMK}$  over methods that do not take the yaw as an input in first place (namely,  $\text{kNN}_{v,\rho}$  and  $\text{BIN}_{v,\rho}$ ) are maintained across all wind speed values.

The analysis above shows how our yaw-adjusted power curve is able to



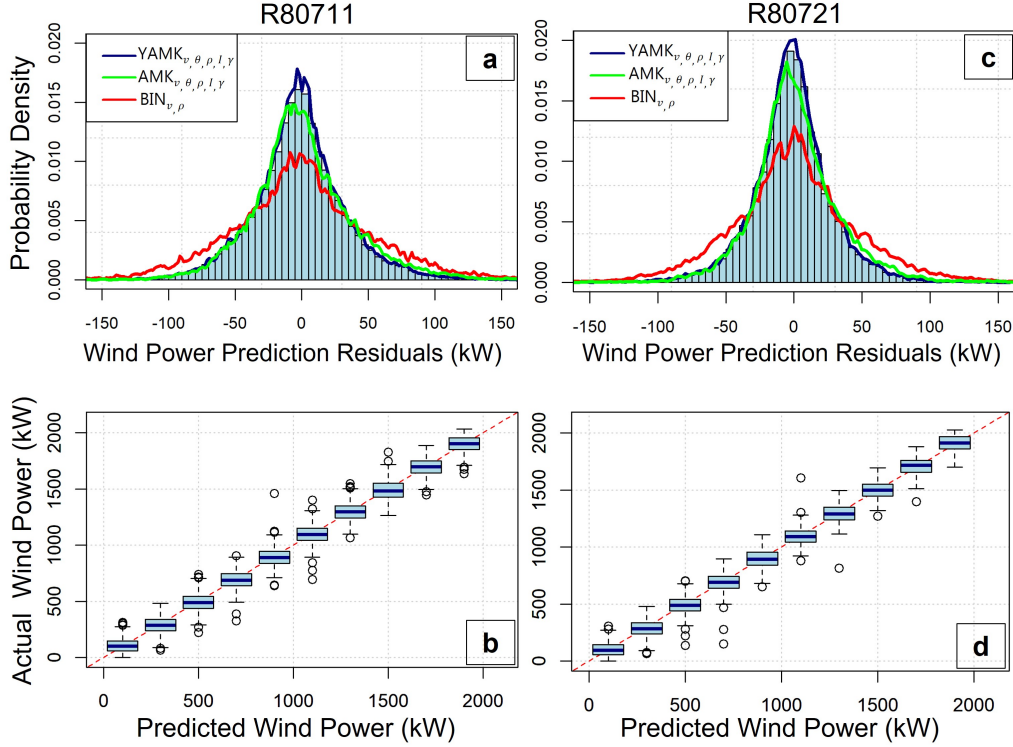


Figure 7: (a) and (c): Residuals of wind power prediction for three models:  $\text{BIN}_{v,\rho}$  (red),  $\text{AMK}_{v,\theta,\rho,I,\gamma}$  (green), and  $\text{YAMK}_{v,\theta,\rho,I,\gamma}$  (blue), on top of the histograms of YAMK’s residuals. (b) and (d): Actual versus predicted wind power values (in kW) for the YAMK method, lying closely to the 45° line suggesting high-quality predictive performance.

401 (1) leverage the AMK special kernel structure to scalably integrate several  
 402 environmental parameters, and (2) effectively harness the yaw-to-power cor-  
 403 relations in order to make significant predictive improvements, on top of those  
 404 provided by the AMK and other nonparametric power curve models. Those  
 405 results affirm our hypothesis: yaw is indeed a significant predictor of power,  
 406 but its significance may only be statistically leveraged in a power curve model  
 407 once *conditioned on* a neighborhood of environmental parameters.

## 408 5. Conclusions

409 In this paper, we proposed the notion of a “yaw-adjusted power curve.”  
 410 Instead of directly adding yaw error as an additional input to a multivariate

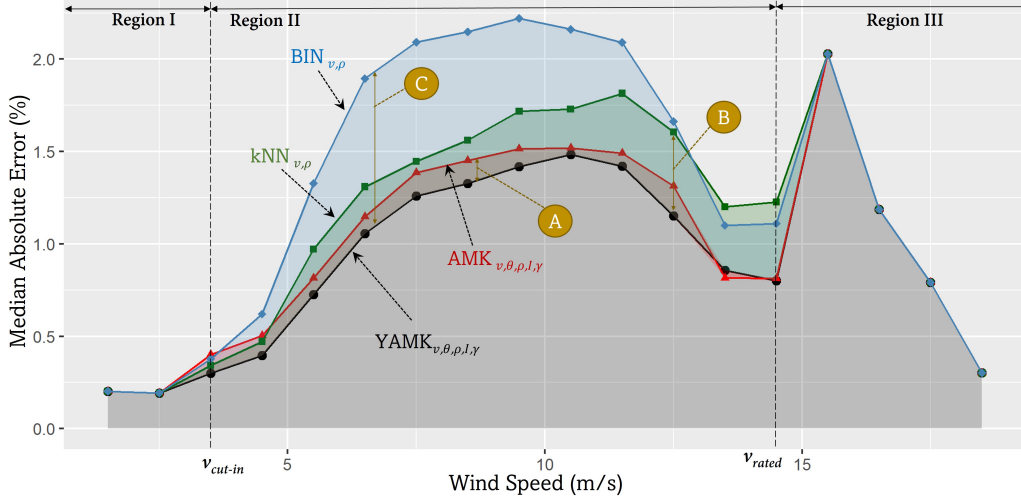


Figure 8: Performance of  $\text{YAMK}_{v,\theta,\rho,I,\gamma}$  (black circles),  $\text{AMK}_{v,\theta,\rho,I,\gamma}$  (red triangles),  $\text{kNN}_{v,\rho}$  (green squares), and  $\text{BIN}_{v,\rho}$  (blue diamonds), in terms of median absolute error (scaled by  $P_r$ ). Points (A), (B), and (C) show the maximum differences in performance of each method relative to  $\text{YAMK}_{v,\theta,\rho,I,\gamma}$ . Those correspond to percentage improvements of 9.35% (point A), 28.3% (point B), and 44.3% (point C), respectively.

power curve model, which is found not to result in any competitive advantage, our approach learns the local yaw-to-power relationship conditional on an effective neighborhood of environmental variables defined using a special kernel structure which was recently proposed in the literature. Our experiments on a real-world dataset suggest that such approach results in significant improvements, in terms of power output estimation accuracy, relative to several existing power curve models.

We believe that the proposed yaw-adjusted power curve model can be valuable to several wind farm operations that primarily rely on wind power curves such as wind power prediction, asset monitoring and prognostics, maintenance scheduling, among others. In addition, such yaw-adjusted wind power curves can be highly relevant to the emerging area of yaw-based power production optimization in wind farms. Recent studies suggest that yaw-based production optimization can significantly improve power production. A pivotal assumption in such optimization routines, however, is the perfect knowledge about how yaw errors impact the power output of a wind turbine. Without a reliable method to accurately estimate the yaw-to-power response surface, as the one proposed herein, the power gains from such emerging

429 and promising efforts may be forfeited or largely compromised. An area of  
430 future research is to explore the impact of the improvement in power curve  
431 estimation from our model on such power production optimization routines.

432 Another interesting line of future research is to consider turbine-to-turbine  
433 dependencies. It is known that a turbine’s yaw error does not only impact  
434 its power output, but also that of its neighbors in a wind farm. In this  
435 research, we have only considered a period of time when the turbines un-  
436 der study were upstream relative to the incoming winds. Future research  
437 may therefore look into modeling turbine dependencies when constructing  
438 the yaw-to-power relationship.

## 439 Data Availability

440 The wind turbine dataset used in this work has been made publicly  
441 available by Engie through its website and can be accessed at [https://](https://opendata-renewables.engie.com/)  
442 [opendata-renewables.engie.com/](https://opendata-renewables.engie.com/) [27]. Air pressure measurements, co-  
443 located with Engie’s dataset, have been obtained from Meteoblue [29].

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## 448 References

- 449 [1] C. Sweeney, R. J. Bessa, J. Browell, P. Pinson, The future of forecast-  
450 ing for renewable energy, Wiley Interdisciplinary Reviews: Energy and  
451 Environment 9 (2) (2020) e365.
- 452 [2] A. Ezzat, Turbine-specific short-term wind speed forecasting considering  
453 within-farm wind field dependencies and fluctuations, Applied Energy  
454 269 (2020) 115034.
- 455 [3] C. Carrillo, A. O. Montaña, J. Cidrás, E. Díaz-Dorado, Review of power  
456 curve modelling for wind turbines, Renewable and Sustainable Energy  
457 Reviews 21 (2013) 572–581.

- 458 [4] M. Lydia, S. S. Kumar, A. I. Selvakumar, G. E. P. Kumar, A com-  
459 prehensive review on wind turbine power curve modeling techniques,  
460 Renewable and Sustainable Energy Reviews 30 (2014) 452–460.
- 461 [5] Y. Wang, Q. Hu, L. Li, A. M. Foley, D. Srinivasan, Approaches to  
462 wind power curve modeling: A review and discussion, Renewable and  
463 Sustainable Energy Reviews 116 (2019) 109422.
- 464 [6] B. Niu, H. Hwangbo, L. Zeng, Y. Ding, Evaluation of alternative power  
465 production efficiency metrics for offshore wind turbines and farms, Re-  
466 newable Energy 128 (2018) 81–90.
- 467 [7] A. Kusiak, H. Zheng, Z. Song, On-line monitoring of power curves, Re-  
468 newable Energy 34 (6) (2009) 1487–1493.
- 469 [8] P. Pinson, Wind energy: Forecasting challenges for its operational man-  
470 agement, Statistical Science 28 (4) (2013) 564–585.
- 471 [9] A. Ezzat, M. Jun, Y. Ding, Spatio-temporal asymmetry of local wind  
472 fields and its impact on short-term wind forecasting, IEEE Transactions  
473 on Sustainable Energy 9 (3) (2018) 1437–1447.
- 474 [10] Y. He, A. Kusiak, Performance assessment of wind turbines: data-  
475 derived quantitative metrics, IEEE Transactions on Sustainable Energy  
476 9 (1) (2017) 65–73.
- 477 [11] P. Guo, D. Infield, Wind turbine power curve modeling and monitoring  
478 with Gaussian process and SPRT, IEEE Transactions on Sustainable  
479 Energy 11 (1) (2018) 107–115.
- 480 [12] P. Papadopoulos, D. W. Coit, A. A. Ezzat, STOCHOS: Stochastic  
481 opportunistic maintenance scheduling for offshore wind farms, arXiv  
482 preprint arXiv:2207.02274 (2022).
- 483 [13] P. Papadopoulos, D. Coit, A. Ezzat, Seizing opportunity: Maintenance  
484 optimization in offshore wind farms considering accessibility, production,  
485 and crew dispatch, IEEE Transactions on Sustainable Energy (2021).
- 486 [14] P. A. Fleming, A. Scholbrock, A. Jehu, S. Davoust, E. Osler, A. D.  
487 Wright, A. Clifton, Field-test results using a nacelle-mounted lidar for  
488 improving wind turbine power capture by reducing yaw misalignment,

- 489 in: Journal of Physics: Conference Series, Vol. 524, IOP Publishing,  
490 2014, p. 012002.
- 491 [15] V. Sohoni, S. Gupta, R. Nema, A critical review on wind turbine power  
492 curve modelling techniques and their applications in wind based energy  
493 systems, Journal of Energy 2016 (2016).
- 494 [16] M. G. Khalfallah, A. M. Koliub, Suggestions for improving wind turbines  
495 power curves, Desalination 209 (1-3) (2007) 221–229.
- 496 [17] B. Stephen, S. J. Galloway, D. McMillan, D. C. Hill, D. G. Infield, A  
497 copula model of wind turbine performance, IEEE Transactions on Power  
498 Systems 26 (2) (2010) 965–966.
- 499 [18] V. Thapar, G. Agnihotri, V. K. Sethi, Critical analysis of methods for  
500 mathematical modelling of wind turbines, Renewable Energy 36 (11)  
501 (2011) 3166–3177.
- 502 [19] A. Marvuglia, A. Messineo, Monitoring of wind farms’ power curves  
503 using machine learning techniques, Applied Energy 98 (2012) 574–583.
- 504 [20] S. Shokrzadeh, M. J. Jozani, E. Bibeau, Wind turbine power curve  
505 modeling using advanced parametric and nonparametric methods, IEEE  
506 Transactions on Sustainable Energy 5 (4) (2014) 1262–1269.
- 507 [21] T. Ouyang, A. Kusiak, Y. He, Modeling wind-turbine power curve: A  
508 data partitioning and mining approach, Renewable Energy 102 (2017)  
509 1–8.
- 510 [22] R. K. Pandit, D. Infield, J. Carroll, Incorporating air density into a  
511 Gaussian process wind turbine power curve model for improving fitting  
512 accuracy, Wind Energy 22 (2) (2019) 302–315.
- 513 [23] G. Lee, Y. Ding, M. G. Genton, L. Xie, Power curve estimation with  
514 multivariate environmental factors for inland and offshore wind farms,  
515 Journal of the American Statistical Association 110 (509) (2015) 56–67.
- 516 [24] B. Golparvar, P. Papadopoulos, A. Ezzat, R.-Q. Wang, A surrogate-  
517 model-based approach for estimating the first and second-order moments  
518 of offshore wind power, Applied Energy 299 (2021) 117286.

- 519 [25] R. K. Pandit, D. Infield, A. Kolios, Gaussian process power curve mod-  
520 els incorporating wind turbine operational variables, *Energy Reports* 6  
521 (2020) 1658–1669.
- 522 [26] D. Astolfi, Wind turbine operation curves modelling techniques, *Elec-*  
523 *tronics* 10 (3) (2021) 269.
- 524 [27] Engie’s Open Data, <https://opendata-renewables.engie.com/>.
- 525 [28] T. Duc, G. Giebel, T. Göçmen, M. Korpås, O. Coupiac, Optimization of  
526 wind farm power production using innovative control strategies (2017).
- 527 [29] Meteoblue Official Website, [https://www.meteoblue.com/en/](https://www.meteoblue.com/en/weather/week/passaic_united-states-of-america_5102443)  
528 [weather/week/passaic\\_united-states-of-america\\_5102443](https://www.meteoblue.com/en/weather/week/passaic_united-states-of-america_5102443).
- 529 [30] K. A. Kragh, M. H. Hansen, Potential of power gain with improved yaw  
530 alignment, *Wind Energy* 18 (6) (2015) 979–989.
- 531 [31] J. Jeon, J. W. Taylor, Using conditional kernel density estimation for  
532 wind power density forecasting, *Journal of the American Statistical As-*  
533 *sociation* 107 (497) (2012) 66–79.
- 534 [32] E. A. Nadaraya, On estimating regression, *Theory of Probability & Its*  
535 *Applications* 9 (1) (1964) 141–142.
- 536 [33] Y. Ding, *Data Science for Wind Energy*, CRC Press, 2019.
- 537 [34] D. Ruppert, S. J. Sheather, M. P. Wand, An effective bandwidth selector  
538 for local least squares regression, *Journal of the American Statistical*  
539 *Association* 90 (432) (1995) 1257–1270.
- 540 [35] C. C. Taylor, Automatic bandwidth selection for circular density estima-  
541 tion, *Computational Statistics & Data Analysis* 52 (7) (2008) 3493–3500.
- 542 [36] Wind Energy Generation Systems - Part 12-1: Power Performance  
543 Measurements of Electricity Producing Wind Turbines, IEC 61400-12-  
544 1International Electrotechnical Commission (2017).
- 545 [37] M. Kuhn, Building predictive models in R using the caret package, *Jour-*  
546 *nal of Statistical Software* 28 (2008) 1–26.