

# Low-Temperature Plasma-Assisted Catalytic Dry Reforming of Methane over CeO<sub>2</sub> Nanorod-Supported NiO Catalysts in a Dielectric Barrier Discharge Reactor

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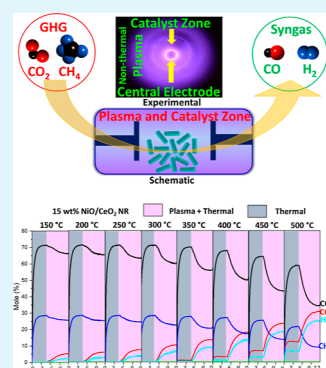
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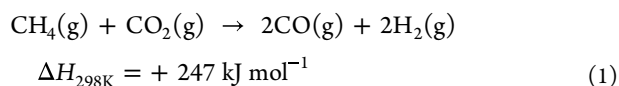
**ABSTRACT:** Nonthermal plasma (NTP)-assisted catalytic dry reforming of methane (DRM) is considered a powerful single-stage reaction mechanism because of its ability to activate normally stable CO<sub>2</sub> and CH<sub>4</sub> at a low temperature under ambient conditions. The thermodynamic barrier of DRM requires a high operating temperature (>700 °C), which can be reduced by nonequilibrium plasma. Herein, we present a method for the wet-impregnation synthesis of CeO<sub>2</sub> nanorod (NR)-supported 5 and 15 wt % NiO catalysts for efficient NTP-promoted DRM with an applied power in the range of 24.9–25.8 W (frequency: 20 kHz), a CH<sub>4</sub>:CO<sub>2</sub> feed gas ratio of 100:250 sccm, and a total flow rate of 350 sccm. The presence of NTP dramatically increased the reaction activity, even at 150 °C, which is usually inaccessible for thermally catalyzed DRM. The CH<sub>4</sub> and CO<sub>2</sub> conversion reaches a maximum of 66 and 48%, respectively, at 500 °C with the 15 wt % NiO/CeO<sub>2</sub> NR catalyst, which are much higher than the values obtained for the 5 wt % NiO/CeO<sub>2</sub> NR catalyst under the same conditions. According to the X-ray photoelectron spectroscopy profile for 15 wt % NiO/CeO<sub>2</sub> NR, a higher concentration of NiO on CeO<sub>2</sub> increases the proportion of Ce<sup>3+</sup> in the catalyst, suggesting enhanced oxygen vacancy concentration with an increased amount of NiO loading. Additionally, a higher NiO loading promotes a higher rate of replacement of Ce<sup>4+</sup> with Ni<sup>2+</sup>, which generates more oxygen vacancies due to the induced charge imbalance and lattice distortion within the CeO<sub>2</sub> lattice. As a result, it can be inferred that the incorporation of Ni ions into the CeO<sub>2</sub> structure resulted in inhibited growth of CeO<sub>2</sub> crystals due to the creation of a Ni<sub>x</sub>Ce<sub>1-x</sub>O<sub>2-α</sub> solid solution and the production of oxygen vacancies.

**KEYWORDS:** nonequilibrium plasma, nonthermal plasma, dry reforming of methane, nickel, CeO<sub>2</sub> nanorods



## 1. INTRODUCTION

Global warming and threatening climatic changes due to the increasing emission rate of greenhouse gases (GHG) have attracted considerable attention from scientists. The dry reforming of methane (DRM) reaction is regarded as a new strategy for simultaneously converting CO<sub>2</sub> and CH<sub>4</sub>, two dominant GHGs, into valuable syngas (H<sub>2</sub> and CO) and/or liquid hydrocarbons. In recent years, nonthermal plasma (NTP) has demonstrated itself as a powerful platform due to its ability to induce the highly endothermic DRM reaction shown in eq 1, even at lower temperatures.



While conventional thermal catalysis of DRM at high temperatures (>700 °C) leads to massive carbon deposition (coking) and catalyst poisoning, plasma with an efficient catalyst showed more significant potential for low-temperature DRM and boasts easy installation, lower cost, and higher efficiency. NTP technology overcomes the thermodynamic barrier of the endothermic DRM reaction at lower temperatures and generates highly energetic species such as electrons,

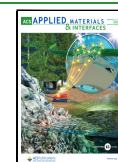
radicals, ions, and metastable species.<sup>1</sup> The coupling of plasma and a catalyst leads to plasma-catalytic synergism that allows for more energy-efficient CH<sub>4</sub> and CO<sub>2</sub> conversion with numerous advantages when compared with conventional thermal catalysis.

Although noble metals such as Ru, Pt, and Rh demonstrate excellent catalytic activity via their C–H bond cracking capability and coke resistance properties, their uneconomical costs prevent them from being used commercially.<sup>2–5</sup> Ni-based catalysts show good catalytic activity of DRM with mild coke resistance comparable with that of many earth-abundant and low-cost transition-metal oxide catalysts, making them promising and suitable for large-scale commercial applications. Khoja et al.<sup>6</sup> reported that a 10 wt % Ni/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>–MgO catalyst showed a maximum of 74.5% CH<sub>4</sub> and 73% CO<sub>2</sub>

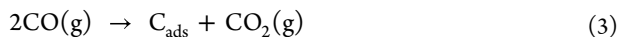
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conversion in thermal DRM testing, which was attributed to its high Lewis basicity, solid metal–support interaction, dispersion, and stability. Unfortunately, Ni as an active catalyst is still limited to lab-scale research because of the quick deactivation of the active material due to catalyst poisoning from methane decomposition and CO disproportionation, as shown in eqs 2 and 3.<sup>7</sup>



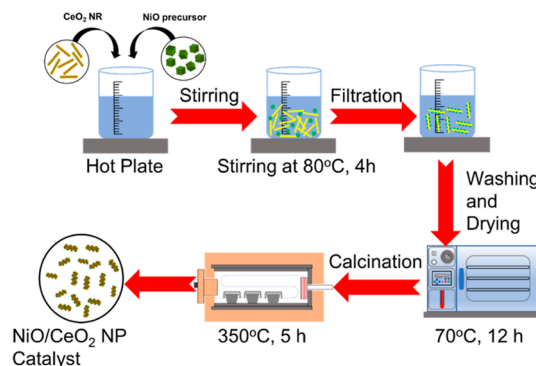
For the DRM reaction, the researcher conducted multiple experiments with Ni-based catalysts supported on metal oxides, including alumina ( $\text{Al}_2\text{O}_3$ ), silica ( $\text{SiO}_2$ ), ceria ( $\text{CeO}_2$ ), and zirconia ( $\text{ZrO}_2$ ), or a mixture of two or more of these oxides.<sup>8</sup> Among these supports,  $\text{CeO}_2$  received the most attention due to its unique reduction properties, its oxygen storage and release capacity, and its strong metal–support interaction (SMSI). In addition, the defects and oxygen vacancies present in  $\text{CeO}_2$  enhance the adsorption and desorption behavior of the catalyst for  $\text{CO}_2$  activation as well as facilitate the detachment of carbon from the catalyst surface.<sup>9</sup> Shape-controlled and surface-engineered  $\text{CeO}_2$  has found widespread applications in a variety of catalytic fields due to the fact that  $\text{CeO}_2$  nanocrystals contain highly reactive surface oxygen vacancies and other defects that promote the reduction of adjacent  $\text{Ce}^{4+}$  to  $\text{Ce}^{3+}$ .<sup>10</sup> In the literature, Ni/ $\alpha$ - $\text{Al}_2\text{O}_3$ , Ni/ $\text{TiO}_2$ , Ni/ $\text{ZrO}_2$ , Ni/ $\text{SiO}_2$ , and Ni/ $\text{MgO}$ , which was attributed to higher Ni dispersion and a SMSI between  $\text{NiO}_x$  and  $\text{CeO}_2$ . SMSI promotes oxygen vacancy formation and enhances surface coverage by  $\text{CO}_2$  species.<sup>11</sup> As a result, the interface and interaction of Ni and surface-engineered  $\text{CeO}_2$  could be a promising approach for enhancing catalyst stability and promoting anticoking properties. In this work, we prepared 5 and 15 wt % NiO-doped  $\text{CeO}_2$  nanorod (NR)-supported catalysts via the wet impregnation method to investigate the effect of NiO deposition with  $\text{CeO}_2$  NR on DRM performance in an atmospheric pressure dielectric barrier discharge (DBD) plasma environment. The reason for choosing the 5 and 15 wt % NiO loadings is to establish an adequate understanding of the activity of the supported catalyst across a representative composition range. In the literature, for thermal- and plasma-assisted DRM, numerous scientific papers have reported experimental studies fitting within this specified range.<sup>12–14</sup> In addition, an excess amount of NiO loading over the  $\text{CeO}_2$  NR support will result in the formation of bulk NiO, which will weaken the metal–support interaction.<sup>15</sup> X-ray diffraction (XRD), Raman spectroscopy,  $\text{H}_2$ -temperature programmed reduction ( $\text{H}_2$ -TPR),  $\text{CO}_2$ -temperature-programmed desorption ( $\text{CO}_2$ -TPD), and X-ray photoelectron spectroscopy (XPS) were used to analyze the morphological and chemical characteristics of catalysts in order to investigate the metal–support interaction and the factors influencing the DRM activities.

## 2. EXPERIMENTAL SECTION

**2.1. Catalyst Preparation.** **2.1.1. Materials.** Cerium(III) nitrate hexahydrate [ $\text{Ce}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$ ] (99.5% pure) was purchased from Acros Organics. Sodium hydroxide [ $\text{NaOH}$ ] (99% pure) and ammonium hydroxide [ $\text{NH}_3 \cdot \text{H}_2\text{O}$ , BDH, 28–30 vol %] were purchased from VWR. Nickel(II) nitrate hexahydrate [ $\text{Ni}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$ ] (99.9% pure) from Alfa Aesar was used as the precursor for the Ni catalysts. The chemicals were used without further purification.

**2.1.2. Preparation of the  $\text{CeO}_2$  NR Support.** 3.8403 g amount of  $\text{Ce}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$  was dissolved in 88 mL of deionized (DI) water to prepare 88 mL of 0.1 M  $\text{Ce}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$  solution. An 8 mL aqueous solution of 6 M  $\text{NaOH}$  was prepared by dissolving 1.93 g of  $\text{NaOH}$  in 8 mL of DI water. Then, 8 mL of 6.0 M  $\text{NaOH}$  solution was added dropwise to 88 mL of 0.1 M  $\text{Ce}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$  and mixed vigorously in a 200 mL Teflon autoclave liner. The solution was stirred for 15 s, and then the closed Teflon liner was transferred into a stainless-steel autoclave and sealed tightly. The temperature of the stainless-steel autoclave was maintained at 90 °C for 48 h. Afterward, the autoclave was cooled to ambient temperature, and the obtained precipitate was washed thoroughly with 500 mL of DI water to remove any residual ions ( $\text{Na}^+$ ,  $\text{NO}_3^-$ ). The product was then washed with 50 mL of ethanol and finally dried in air at 60 °C for 12 h to avoid hard agglomeration of the  $\text{CeO}_2$  nanoparticles. Then, the dried sample was collected and ground gently with a mortar and pestle.<sup>10,16</sup>

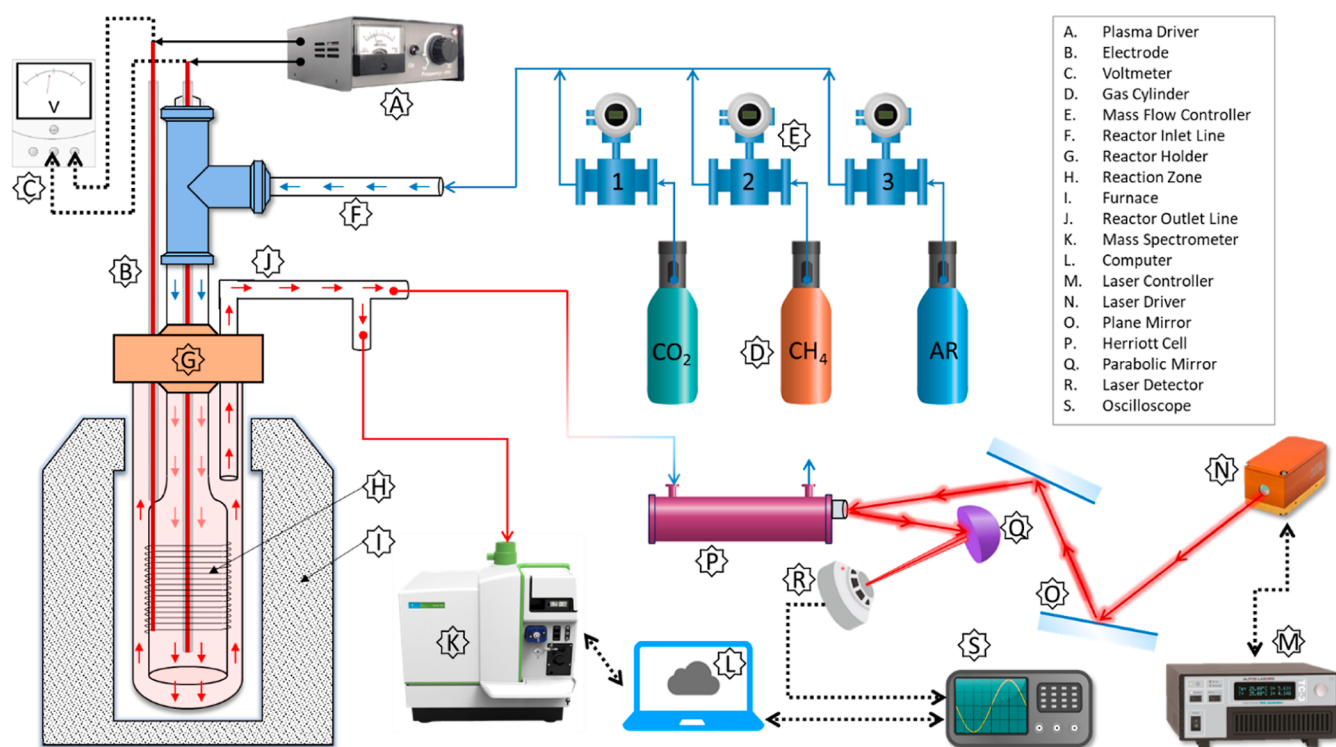
**2.1.3. Preparation of NiO/ $\text{CeO}_2$  NR Catalysts.** NiO/ $\text{CeO}_2$  NR catalysts were prepared using a wet impregnation method with two different NiO loadings. 0.95 g of  $\text{CeO}_2$  NR powder and 0.85 g of  $\text{CeO}_2$  NR powder, respectively, were put into 100 mL of DI water in 200 mL beakers.  $\text{Ni}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$ , equivalent to 5 and 15 wt % Ni, respectively, was added to the suspension solutions of the  $\text{CeO}_2$  NR support powders under stirring. The suspension solutions were mixed vigorously using magnetic stirring followed by dropwise addition of 0.5 M aqueous solution of ammonium hydroxide ( $\text{NH}_3 \cdot \text{H}_2\text{O}$ , BDH, 28–30 vol %) to maintain the pH value of the suspension to ~9. The stirring (400 rpm) continued for 4 h at 80 °C. Finally, the precipitates were transferred into a drying oven at 80 °C and kept overnight. A fine powder of the collected samples was obtained using a mortar and pestle and left in an air furnace for calcination at a rate of 10 °C/min up to 350 °C and maintained at this temperature for 5 h. Figure 1 shows the pictorial presentation of the complete NiO/ $\text{CeO}_2$  NR catalyst preparation method.



**Figure 1.** Synthesizing steps of NiO/ $\text{CeO}_2$  NR catalysts using a wet impregnation method.

**2.2. Catalyst Characterization.** The crystal structures of the synthesized catalysts were observed via powder XRD using a Phillips X'Pert MPD diffractometer operated at 40 kV and 40 mA with a copper K $\alpha$  radiation source ( $\lambda = 0.154$  nm). Each scanned profile used a 0.5° min<sup>-1</sup> scan rate with a  $2\theta$  range between 10 and 90°. Jade software was used to analyze each catalyst's lattice parameters and average crystal size from the recorded XRD patterns.

The Brunauer–Emmett–Teller (BET) surface area was obtained with a Micromeritics AutoChem II 2920 chemisorption analyzer using a nitrogen adsorption–desorption isotherm at 77 K. The same instrument was used to characterize  $\text{H}_2$ -TPR and  $\text{CO}_2$ -TPD. For  $\text{H}_2$ -TPR analysis, the powder samples (85–95 mg) were placed in a quartz U-tube sandwiched between two pieces of quartz wool and then heated at a rate of 10 °C/min from 30 to 900 °C. During  $\text{H}_2$ -TPR analysis, the samples were reduced at a flow rate of 50 mL/min in a 10 vol %  $\text{H}_2$ –90 vol % Ar gas mixture. A thermal conductivity



**Figure 2.** Schematic diagram of the DBD plasma reactor with accessories for DRM.

detector (TCD), which was calibrated using a quantitative reduction of CuO to metallic copper, was used to monitor the quantity of H<sub>2</sub> uptake during the reduction. For the CO<sub>2</sub>-TPD analysis, the sample was placed in a quartz U-tube and heated from room temperature to 400 °C with a helium (He) stream (flow rate: 50 mL/min) to remove residual moisture. After the system was cooled to room temperature, 10 vol % CO<sub>2</sub>–90 vol % He mixture gas was supplied with a flow rate of 50 mL/min through the sample for 60 min. The sample was then heated to 900 °C at a linear ramping rate of 10 °C/min under He gas. A TCD was used to evaluate the desorption behavior of CO<sub>2</sub> at elevated temperatures.

High-resolution transmission electron microscopy (HRTEM) images were obtained using an FEI Tecnai F20 instrument with an acceleration voltage of 200 kV to observe microstructures. A JEOL 7000 FE SEM instrument was used to obtain surface morphology and assess elemental distribution (energy-dispersive X-ray spectroscopy data or EDX). For transmission electron microscopy (TEM) sample preparation, powder samples went through ultrasonic dispersion in ethanol. One or two drops of the suspension solution were deposited on an ultrathin carbon film supported by a 400-mesh copper grid (Ted Pella Inc.) and then dried for 2 h before analysis.

The surface chemical composition of the synthesized samples was measured using a Kratos Axis Ultra DLD spectrometer with a monochromatic Al K $\alpha$  ( $h\nu = 1486.6$  eV) source under ultrahigh vacuum ( $10^{-10}$  Torr). For XPS analysis, carbon (C) 1s at 284.8 eV was used for calibration of binding energies (BE). The fitting and deconvolution of the spectra were conducted using CasaXPS software.

For nondestructive characterization, Raman experiments of the catalysts were conducted using a HORIBA LabRAM HR 800 Raman spectrometer (equipped with a 100 $\times$  long working distance objective, NA = 0.60) in the spectral range from 100 to 1200 cm<sup>-1</sup>. Before each analysis, the spectrometer was calibrated using a single-crystal Si wafer. A diode-pumped solid-state laser system (Laser Quantum MPC6000) tuned at  $\lambda = 532$  nm was used for excitation.

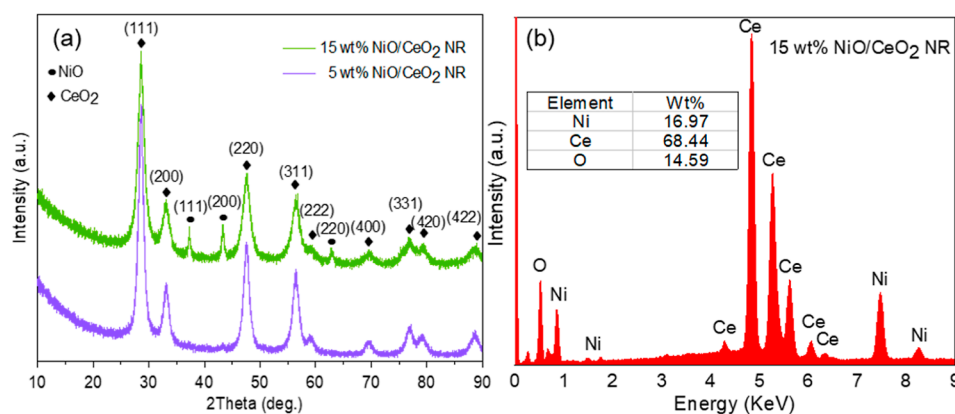
**2.3. Reactor Setup.** Figure 2 displays the schematic diagram for the plasma DRM catalyst testing system together with a gas flow diagram and analysis system. The testing system can be divided into three sections: flue gas analysis, the DBD reactor, and the gas supply. CH<sub>4</sub>, CO<sub>2</sub>, and Ar gases from Airgas (purity >99.99%) are fed to the

reactor by mass flow controllers (Brooks GF040 MultiFlo MFC, response time 1 s) in the gas supply section. The DBD reactor consists of two concentric quartz tubes, which are placed inside the furnace (ATS 3210, max. temp. 1200 °C). The outer quartz tube has a constant outer diameter (OD) of 25.4 mm, while the inner quartz tube (OD = 6.35 mm) features an expansion portion (inner diameter = 9.53 mm, length = 50 mm). In order to generate plasma, one electrode (Kanthal A-1 wire, 24 g), which is covered with a ceramic tube, is placed at the center axis of the quartz tubes. Another thin wire (Kanthal A-1 wire, 32 g) is wrapped around the inner tube expansion section as the other electrode. Both electrodes are connected to a plasma generator (PVM/DDR plasma driver). The catalyst material is positioned inside the inner expansion part of this reactor and distributed with quartz wool; the plasma is created in this expansion section.

Flue gases are analyzed in the flue gas analysis system where some gases (CO, H<sub>2</sub>, CH<sub>4</sub>, CO<sub>2</sub>, and Ar) are detected by a mass spectrometer (Extrel QMS, MAX300-EGA, 300 ms, 1–250 amu detectability) and other gases (higher hydrocarbon like C<sub>2</sub>H<sub>6</sub>) are detected using an infrared (IR) laser absorption spectrometer system. The IR laser absorption spectroscopy portion is a specially designed system that includes a quantum cascade laser (Alpes Lasers, sbcw6200 DN) with a controller and laser supply, a handmade Herriott cell to extend the gas adsorption length, an IR detector (Vigo, PVMI-4TE) to detect laser signals, an oscilloscope (Tektronix TBS1154, 150 MHz) to visualize the signal, and a waveform generator (B&K Precision, 4055B, 1  $\mu$ Hz to 60 MHz) to trigger the laser. The same setup has been used before for the oxidative coupling of methane, and its accuracy was confirmed.<sup>17</sup>

In the DRM analysis, CH<sub>4</sub> and CO<sub>2</sub> were used at a total flow rate of 350 sccm (CH<sub>4</sub>/CO<sub>2</sub> molar ratio = 100:250 = 0.4). Ar gas was used to purge or neutralize the reactor from other contaminated gases before starting the experiment for each observation. The catalyst was regenerated using a mixed supply of Ar and CO<sub>2</sub> (Ar/CO<sub>2</sub> molar ratio = 100:250 = 0.4). Each type of gas flow was controlled by a separate MFC and mixed before pumping into the reactor. The reaction zone temperature was regulated using the furnace, where the temperature ranged from 150 to 500 °C with a 4 °C/min ramp, and the plasma supply was controlled manually. The DBD reactor was linked to an





**Figure 3.** (a) XRD patterns of 5 wt % NiO/CeO<sub>2</sub> NR and 15 wt % NiO/CeO<sub>2</sub> NR and (b) EDS analysis of 15 wt % NiO/CeO<sub>2</sub> NR.

AC high-voltage power supply (PVM500–2500 from <http://Amazing1.com>) with a peak-to-peak voltage of 40 kV and a frequency of 20–70 kHz. In this work, the power supply frequency was fixed at 20 kHz. The electrical signals (applied voltage and current) were recorded by a four-channel digital oscilloscope (Tektronix, TBS1154) using a high-voltage probe (Tektronix P6015A) and a current transformer (Magnetlab, CT-E 0.5 BNC). A discharge power in the range of 24.9–25.8 W was calculated for this work. The gas sample was collected from the reactor in both the QMS and QCL systems, where the flue gas was continuously analyzed and data were logged into the incorporated data acquisition system.

**2.4. Performance Parameters.** The conversion of CH<sub>4</sub> and CO<sub>2</sub> is expressed as the ratio of the moles of reactants converted to the moles of reactants initially present. The yield of a reaction is the proportion of the desired product produced (in moles) to the maximum possible yield, assuming complete conversion of the limiting reactant and no side reactions. The selectivity refers to the ratio of the desired product formed to the amount of undesired products formed. The equations used for the calculation of conversion, yield, and selectivity in a DRM reaction are presented below

$$C_{\text{CH}_4} = \frac{\text{moles of CH}_4 \text{ converted}}{\text{moles of CH}_4 \text{ input}} \times 100\% \quad (4)$$

$$C_{\text{CO}_2} = \frac{\text{moles of CO}_2 \text{ converted}}{\text{moles of CO}_2 \text{ input}} \times 100\% \quad (5)$$

$$Y_{\text{H}_2} (\%) = \frac{\text{moles of H}_2 \text{ produced}}{2 \times \text{moles of CH}_4 \text{ input}} \times 100\% \quad (6)$$

$$Y_{\text{CO}} (\%) = \frac{\text{moles of CO produced}}{\text{moles of CH}_4 \text{ input} + \text{moles of CO}_2 \text{ input}} \times 100\% \quad (7)$$

$$S_{\text{H}_2} (\%) = \frac{\text{moles of H}_2 \text{ produced}}{2 \times \text{moles of CH}_4 \text{ converted}} \times 100\% \quad (8)$$

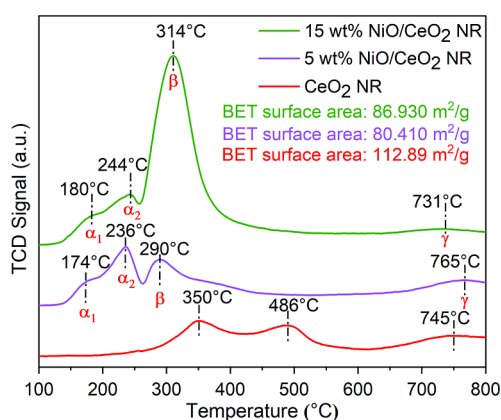
$$S_{\text{CO}} (\%) = \frac{\text{moles of CO produced}}{\text{moles of CH}_4 \text{ converted} + \text{moles of CO}_2 \text{ converted}} \times 100\% \quad (9)$$

### 3. CHARACTERIZATION

**3.1. X-ray Diffraction.** The XRD patterns in Figure 3a exhibit the peaks of the cubic fluorite structure of CeO<sub>2</sub>, confirmed by JCPDS# 34–0394, space group *Fm3m*. According to the XRD database and literature, the peaks with  $2\theta$  values at 28.5, 33.1, 47.5, 56.3, 59.1, 69.4, 76.7, and 79.1° correspond to the planes (111), (200), (220), (311),

(222), (400), (331), (420), and (422), respectively.<sup>18</sup> The results demonstrated that the CeO<sub>2</sub> NRs maintained their crystal structure after the wet impregnation of NiO and calcination at 350 °C for 5 h. The XRD pattern of 5 wt % NiO/CeO<sub>2</sub> NR showed no significant NiO peaks, suggesting that NiO was highly dispersed on CeO<sub>2</sub> NR or that there was a low metal content.<sup>19</sup> As NiO peaks are very weak and mixed with the background, it is nearly impossible to determine the crystal size by using the Scherrer formula. The XRD pattern of 15 wt % NiO-doped CeO<sub>2</sub> had three additional peaks besides the CeO<sub>2</sub> peaks. These XRD peaks had  $2\theta$  values of 37.2, 43.2, and 62.8°, which correspond to the (111), (200), and (220) planes of NiO, respectively.<sup>20</sup> Figure 3b depicts the EDS line scanning result of 15 wt % NiO/CeO<sub>2</sub> NR, illustrating the approximate similarity of NiO loading of the prepared sample. The average crystallite size was determined by using the highest peak associated with the CeO<sub>2</sub> (111) plane. Using the Scherrer formula, the average crystallite sizes of 5 wt % NiO/CeO<sub>2</sub> NR and 15 wt % NiO/CeO<sub>2</sub> NR were found to be 8.74 and 7.14 nm, respectively. The reduction of crystallite size was due to the replacement of Ni<sup>2+</sup> ions (0.055 nm) with Ce<sup>3+</sup> or Ce<sup>4+</sup> ions (0.114 or 0.097 nm).<sup>21</sup> As a result, it can be assumed that the integration of Ni ions with Ce ions inhibited the growth of CeO<sub>2</sub> crystals by forming Ni<sub>x</sub>Ce<sub>1-x</sub>O<sub>2- $\alpha$</sub>  which is a solid solution with ample oxygen vacancies. Increased NiO loading led to a minor shift in the diffraction peaks of NiO and CeO<sub>2</sub> toward a higher Bragg's angle, indicating the presence of diffusion-made solid solution on the catalyst surface.<sup>22</sup> In the 15 wt % NiO/CeO<sub>2</sub> NR, the peak intensity of NiO increased relative to the background, suggesting probable agglomeration of NiO, as reported by Zhao et al.<sup>19</sup> Their work explored the relationship between higher NiO concentrations and higher intensity of NiO peaks and found that NiO agglomeration can occur when the NiO concentration exceeded 4%.

**3.2. H<sub>2</sub>-Temperature Programed Reduction.** As shown in the H<sub>2</sub>-TPR profiles in Figure 4, the three reduction peaks observed for CeO<sub>2</sub> NR at 350, 486, and 745 °C are attributed to the surface reduction (350 and 486 °C) and bulk reduction (745 °C), which are consistent with the literature reports.<sup>23,24</sup> Figure 4 also exhibits three reduction peaks  $\alpha$ ,  $\beta$ , and  $\gamma$  for 5 wt % NiO/CeO<sub>2</sub> NR and 15 wt % NiO/CeO<sub>2</sub> NR. In general, the reduction peaks of CeO<sub>2</sub>-supported NiO catalysts are observed in the temperature range of 200–600 °C.<sup>25</sup> Thus, these high-temperature reduction peaks at 731, 745, and 756 °C for these three samples are ascribed to the bulk reduction of CeO<sub>2</sub> support.<sup>26,27</sup> The addition of NiO has a significant influence on



**Figure 4.**  $\text{H}_2$ -TPR profiles of pure  $\text{CeO}_2$  NR, 5 wt %  $\text{NiO}/\text{CeO}_2$  NR, and 15 wt %  $\text{NiO}/\text{CeO}_2$  NR.

the low-temperature surface reducibility (i.e., reduction temperature and hydrogen consumption) of  $\text{CeO}_2$ , as shown in Figure 4. The low-temperature peaks ( $\alpha_1$  and  $\alpha_2$ ) observed below 250 °C were caused by the reduction of surface oxygen, which are possibly attached to the oxygen vacancies generated by the partial substitution of  $\text{Ce}^{4+}$  ions with  $\text{Ni}^{2+}$  ions. Another peak was observed in the 250–400 °C region, labeled as the  $\beta$  peak for 5 wt %  $\text{NiO}/\text{CeO}_2$  NR and 15 wt %  $\text{NiO}/\text{CeO}_2$  NR. The 15 wt %  $\text{NiO}/\text{CeO}_2$  NR catalyst possessed a distinct  $\beta$  peak with an extra-high intensity when compared to the 5 wt %  $\text{NiO}/\text{CeO}_2$  NR catalyst. The  $\beta$  peak is attributed to reduction of  $\text{NiO}_x$  incorporated in the  $\text{CeO}_2$  lattice or the  $\text{Ni}-\text{Ce}-\text{O}$  solid solution. The solid solution of  $\text{Ni}_x\text{Ce}_{1-x}\text{O}_{2-\alpha}$  is formed by replacing  $\text{Ce}^{4+}$  with  $\text{Ni}^{2+}$ , which generates a charge imbalance and lattice distortions within the  $\text{CeO}_2$  lattice, resulting in a high concentration of oxygen vacancies. The solid solution of  $\text{Ni}-\text{Ce}-\text{O}$  includes both weak and strong  $\text{NiO}_x/\text{CeO}_2$  interactions, which govern the reduction of highly dispersed  $\text{NiO}$  and cause the agglomeration of  $\text{NiO}$  on the  $\text{CeO}_2$  surface as represented by the  $\beta$  peak. Hence, the  $\beta$  peak plays a key role in enhancing the catalytic activity in low-temperature catalytic DRM. In contrast, the  $\gamma$  and  $\alpha$  peaks are considered insignificant for catalytic improvement (Table 1).<sup>28</sup>

**3.3. X-ray Photoelectron Spectroscopy.** XPS was conducted to analyze the surface composition and chemical state of the  $\text{Ni}/\text{CeO}_2$  catalysts. Figure 5 displays the XPS spectra along with the fitted deconvolution of the 3d orbital of Ce, the 1s orbital of O, and the 2p orbital of Ni for both  $\text{CeO}_2$  NR-supported 5 and 15 wt %  $\text{NiO}$  catalysts, respectively. Figure 5a,d demonstrate the Ce 3d XPS analysis for 5 wt %  $\text{NiO}/\text{CeO}_2$  NR and 15 wt %  $\text{NiO}/\text{CeO}_2$  NR. Here, the peaks at 915.5, 906.4, 900.1, 897.5, 886.4, and 881.4 eV are assigned to the  $\text{Ce}^{4+}$  states, denoted by  $\text{U}'''$ ,  $\text{U}''$ ,  $\text{U}'$ ,  $\text{V}'''$ ,  $\text{V}''$ , and  $\text{V}'$ , respectively.<sup>29</sup> The final states of Ce 3d<sub>3/2</sub> and Ce 3d<sub>5/2</sub> are represented by letters U and V, respectively. In contrast, the peaks  $\text{U}^\circ$  and  $\text{V}^\circ$  are located at 895.2 and 876.7 eV,

respectively, and correspond to  $\text{Ce}^{3+}$ . It is noted that the peaks at 895.2 and 876.7 eV represent the concentration of the  $\text{Ce}^{3+}$  state, which is more vital for the 15 wt %  $\text{NiO}/\text{CeO}_2$  NR catalyst than for the 5 wt %  $\text{NiO}/\text{CeO}_2$  NR catalyst.<sup>30,31</sup> This is because each Ni ion substitution in the  $\text{CeO}_2$  lattice creates an oxygen vacancy with two electrons to make up for the charge difference between  $\text{Ce}^{4+}$  and  $\text{Ni}^{2+}$ , leading to the formation of  $\text{Ce}^{3+}$  ions, which is a key factor that influences the catalytic performance of the DRM reaction.<sup>8</sup> Therefore, it is reasonable to conclude that 15 wt %  $\text{NiO}/\text{CeO}_2$  NR contains more oxygen defects than 5 wt %  $\text{NiO}/\text{CeO}_2$  NR. The XPS profiles of the O 1s given in Figure 5b,e strongly support this hypothesis. The peaks were fitted using the Gaussian function at BE = 529.1 and 532.4 eV, respectively, for the  $[\text{O}]_{\text{Ce}^{4+}}$  and  $[\text{O}]_{\text{Ce}^{3+}}$  oxygen.<sup>32</sup> The oxygen-bound peak for  $\text{Ce}^{3+}$  is stronger at 15 wt %  $\text{NiO}/\text{CeO}_2$  NR than at 5 wt %  $\text{NiO}/\text{CeO}_2$  NR. Consequently, a large amount of oxygen vacancies may accumulate on the catalyst surface of 15 wt %  $\text{NiO}/\text{CeO}_2$  NR and modulate the  $\text{CO}_2$  reforming process. The  $\beta$  peak of the  $\text{H}_2$ -TPR profile for 15 wt %  $\text{NiO}/\text{CeO}_2$  NR corresponds with these observations. Figure 5c,f demonstrate the XPS spectra of Ni 2p for 5 wt %  $\text{NiO}/\text{CeO}_2$  NR and 15 wt %  $\text{NiO}/\text{CeO}_2$  NR, respectively. The multi-split peaks at BE = 863.2 and 861.6 eV and the satellite at 868.7 eV are attributed to Ni 2p<sub>3/2</sub> which determine the  $\text{Ni}^{3+}$  and  $\text{Ni}^{2+}$  concentration. The higher concentration of NiO on  $\text{CeO}_2$  increases the proportion of  $\text{Ce}^{3+}$  present on the 15 wt %  $\text{NiO}/\text{CeO}_2$  NR catalyst. Thus, the amount of NiO doping is shown to have a substantial effect on charge imbalance, defects, and oxygen vacancy density, all of which are also confirmed by the RAMAN profile (Figure S3) and promote DRM reaction activation.

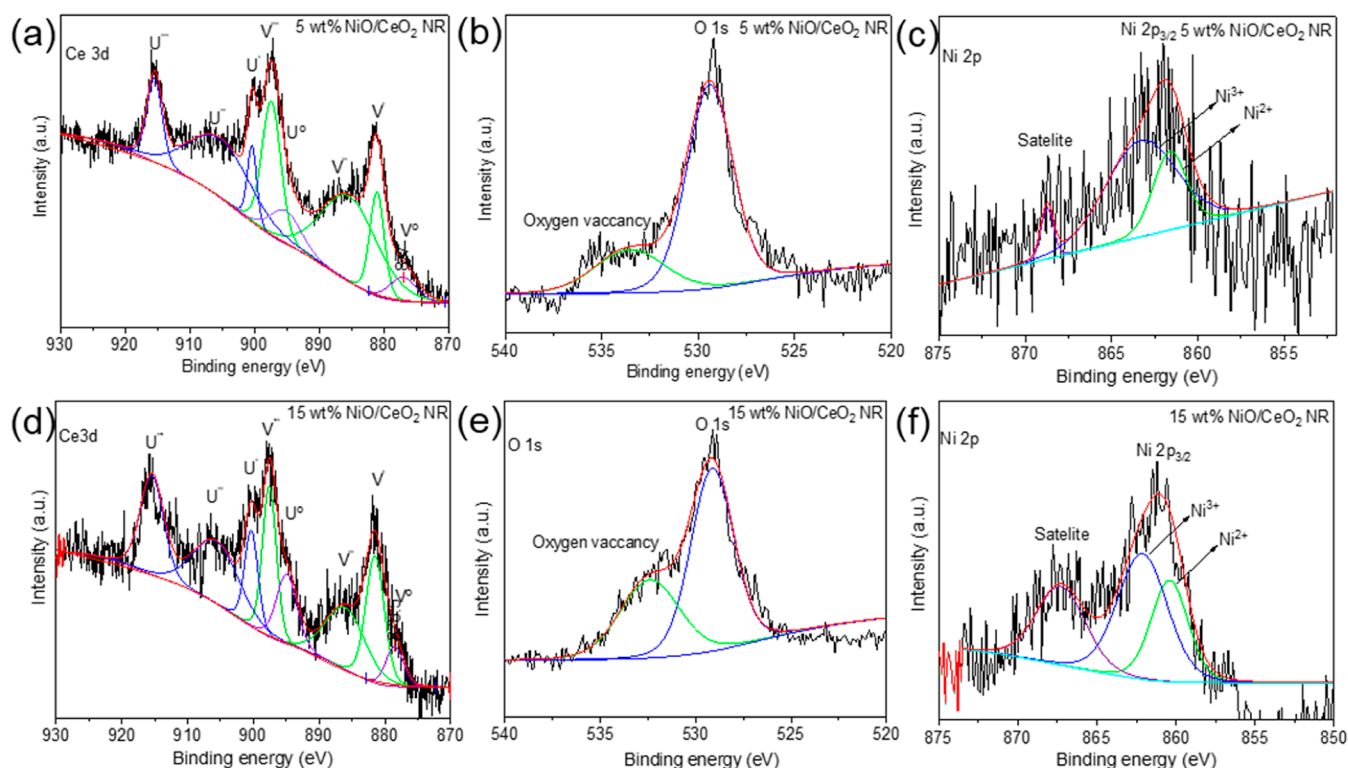
**3.4. Transmission Electron Microscopy.** Figure 6 shows low- and high-magnification TEM images of the  $\text{CeO}_2$  NR-supported 15 wt %  $\text{NiO}$  catalyst, as well as the selected area electron diffraction (SAED) pattern of  $\text{CeO}_2$  and  $\text{NiO}$ . It is evident that the  $\text{CeO}_2$  shape remains unchanged after  $\text{NiO}$  loading and calcination. The length and diameter of the  $\text{CeO}_2$  NRs are in the ranges of 60–80 and 5–10 nm, respectively. The SAED patterns in Figure 6b,c exhibit four well-defined diffraction rings for  $\text{CeO}_2$  and one diffraction ring for the  $\text{NiO}$  crystal. These rings correspond to the (111), (200), (220), and (311) crystalline planes of  $\text{CeO}_2$ , along with the (200) crystalline plane of  $\text{NiO}$ . The  $d$ -spacing value of 0.301 nm demonstrated by  $\text{CeO}_2$  corresponds to the (111) plane, while the  $d$ -spacing value of 0.207 nm shown by  $\text{NiO}$  corresponds to the (200) plane. The same crystalline plane was observed in the lattice fringes of the TEM images. In Figure 6d, the HRTEM image clearly revealed the existence of lattice distortion and other defects.

## 4. RESULTS AND DISCUSSION

Figure 7 shows the molar fraction of  $\text{CO}_2$ ,  $\text{CH}_4$ ,  $\text{CO}$ , and  $\text{H}_2$  obtained from QMS for DRM at eight different temperatures

**Table 1.**  $\text{H}_2$  Consumption and Reduction Temperature of the Prepared Samples and Their Crystallite Size from the  $\text{H}_2$ -TPR Profiles and XRD Patterns

samples	crystallite size (nm)	reduction temperature (°C)			$\text{H}_2$ consumption ( $\mu\text{mol g}^{-1}$ )		total surface $\text{H}_2$ consumption ( $\mu\text{mol g}^{-1}$ )
		$\alpha_1$	$\alpha_2$	$\beta$	$\alpha$	$\beta$	
5 wt % $\text{NiO}/\text{CeO}_2$ NR	8.74	174	236	290	8.45	7.77	16.22
15 wt % $\text{NiO}/\text{CeO}_2$ NR	7.41	180	244	314	2.96	26.59	29.55



**Figure 5.** XPS spectra of Ce 3d, O 1s, and Ni 2p, respectively, for (a–c) 5 wt % NiO/CeO<sub>2</sub> NR and (d–f) 15 wt % NiO/CeO<sub>2</sub> NR.

ranging from 150 to 500 °C with 50 °C intervals for the 15 wt % NiO/CeO<sub>2</sub> NR catalyst. The plasma was introduced for 7 min, whereas thermal-only DRM was tested for 5 min. The thermal-only DRM was measured for the first 5 min, with the plasma starting on the 6th and stopping on the 12th minute. These two zones were distinguished in the figure by differently colored shading. The results from the introduction of plasma suggest that the thermodynamic barrier of DRM is easily surpassed, a phenomenon that is not possible with thermal-only DRM. For thermal catalytic DRM, no detectable CO and H<sub>2</sub> gases were observed for the first five min until the temperature reached 300 °C. However, with the initiation of plasma at the sixth minute, there were detectable 6% CO (red line) and 3% H<sub>2</sub> (sky-blue line) gases observed at temperatures as low as 150 °C, corresponding with a sudden decrease in mole concentration of CO<sub>2</sub> (black line) and CH<sub>4</sub> (blue line) in the exhaust gas. A small molar concentration of CO and H<sub>2</sub> was detected in the thermal catalysis region at 350 °C, with these concentrations increasing to 12 and 9%, respectively, at 500 °C. Comparatively, in the plasma catalytic region at 500 °C, there were 33 and 25% molar concentrations of CO and H<sub>2</sub>, respectively. These results indicate that the introduction of plasma is crucial for initiating and promoting low-temperature DRM to produce syngas.

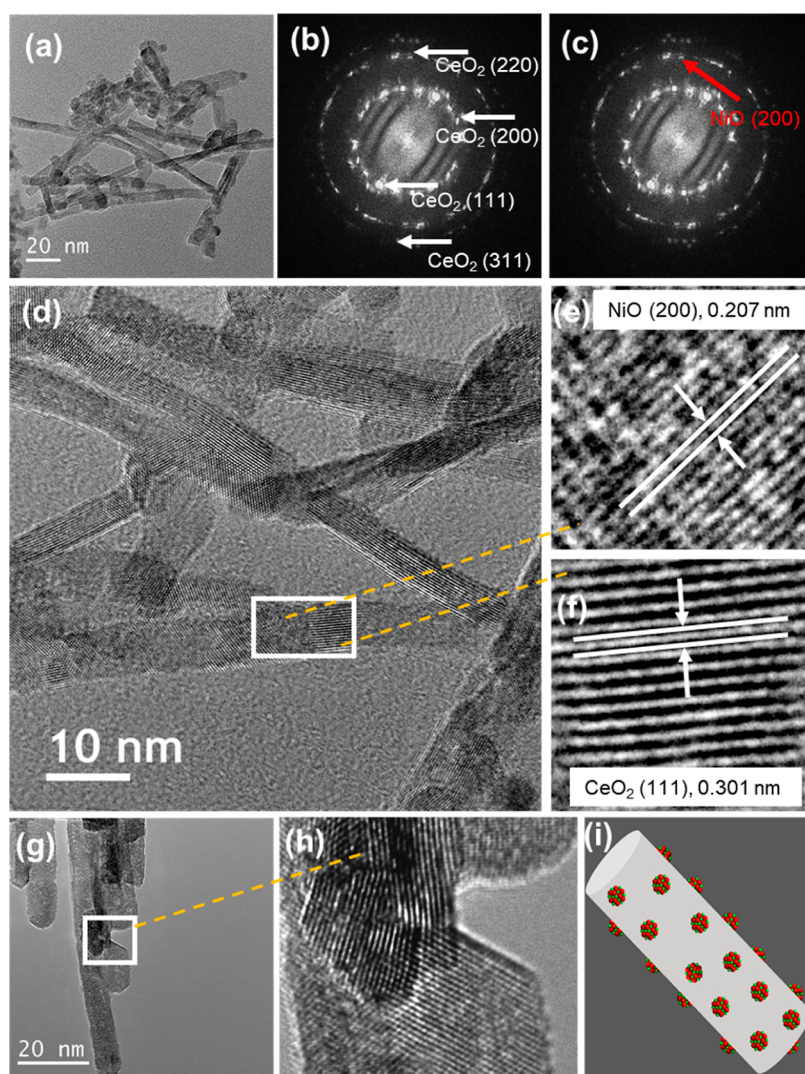
The conversion of the DRM reaction with only plasma, a plasma-assisted only CeO<sub>2</sub> NR support, a thermal-assisted catalyst, and a plasma-assisted catalyst is illustrated in Figure 8 for three different temperatures (350, 400, and 450 °C). Compared to thermally driven DRM, plasma-assisted DRM conversions are shown to occur at a much higher rate for both catalysts. In addition, neither catalyst showed any thermally assisted DRM reaction below 350 °C. Furthermore, the CH<sub>4</sub> and CO<sub>2</sub> conversion percentages with the plasma-only and CeO<sub>2</sub> NR-only conditions were less than 5%. It should be

noted that the CH<sub>4</sub> conversion percentage was higher than the CO<sub>2</sub> conversion percentage in all circumstances, which can be attributed to the differences in bond energy. Due to the lower bond dissociation energy (BDE) of CH<sub>4</sub> (440 kJ/mol) compared to that of CO<sub>2</sub> (523 kJ/mol), the addition of plasma promotes more CH<sub>4</sub> conversion than CO<sub>2</sub>.<sup>33</sup> In the case of thermally assisted DRM, the CH<sub>4</sub> is adsorbed on the Ni catalyst surface, which controls CH<sub>4</sub> conversion. Increasing the Ni content (from 5 to 15 wt %) consequently increases CH<sub>4</sub> conversion.

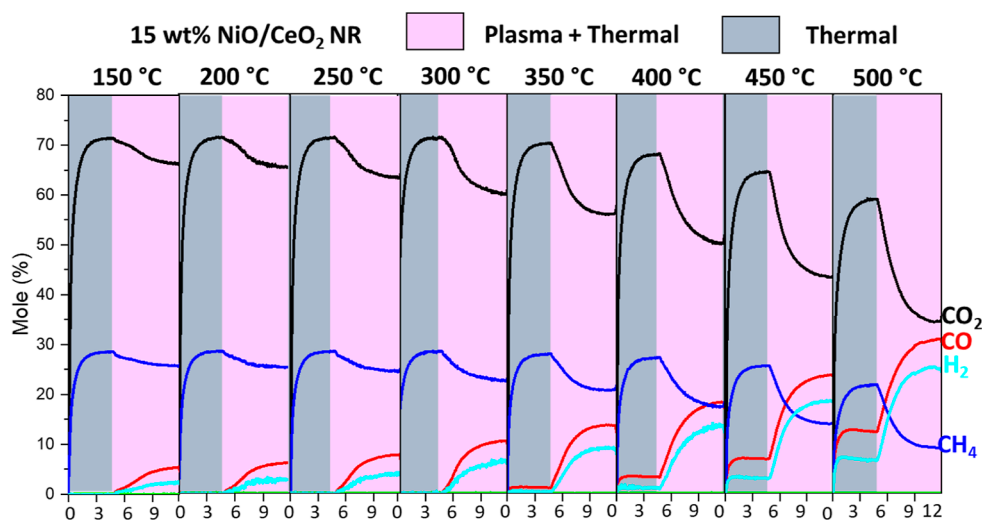
**4.1. Conversion of Input Gases and Efficiency of Syngas Production.** The performance of the NiO catalyst on CeO<sub>2</sub> NR support for DRM application in a NTP environment was investigated at temperatures ranging from 150 to 500 °C with a total flow rate of 350 sccm (CH<sub>4</sub>: CO<sub>2</sub> molar ratio = 100:250 sccm) without inert gas dilution. The experimentally observed DRM effect for various temperatures is shown in Figures 9 and 10.

Figure 9 represents the experimentally obtained conversion of CH<sub>4</sub> and CO<sub>2</sub> for both pure thermal- and plasma-assisted DRM experiments across a range of temperatures. When using the 5 wt % NiO/CeO<sub>2</sub> NR catalyst, the CH<sub>4</sub> conversion rate ranges from 5%–15% (pure thermal) and 14%–50% (plasma-thermal synergy) over the temperature range of 150–500 °C. At the same temperature range, the CH<sub>4</sub> conversion rate is 8–29% (pure thermal) and 21–66% (plasma-thermal synergy) when using the 15 wt % NiO/CeO<sub>2</sub> NR catalyst. On the other hand, CO<sub>2</sub> conversion changes from 3 to 13% (pure thermal) and 10 to 40% (plasma-thermal synergy) for the 5 wt % NiO/CeO<sub>2</sub> NR catalyst and from 3–24% (pure thermal) to 15–48% (plasma-thermal synergy) for the 15 wt % NiO/CeO<sub>2</sub> NR catalyst. The plasma-assisted DRM began converting gases at temperatures as low as 150 °C, whereas the thermal DRM began working at roughly 350 °C. It is also noticeable that the

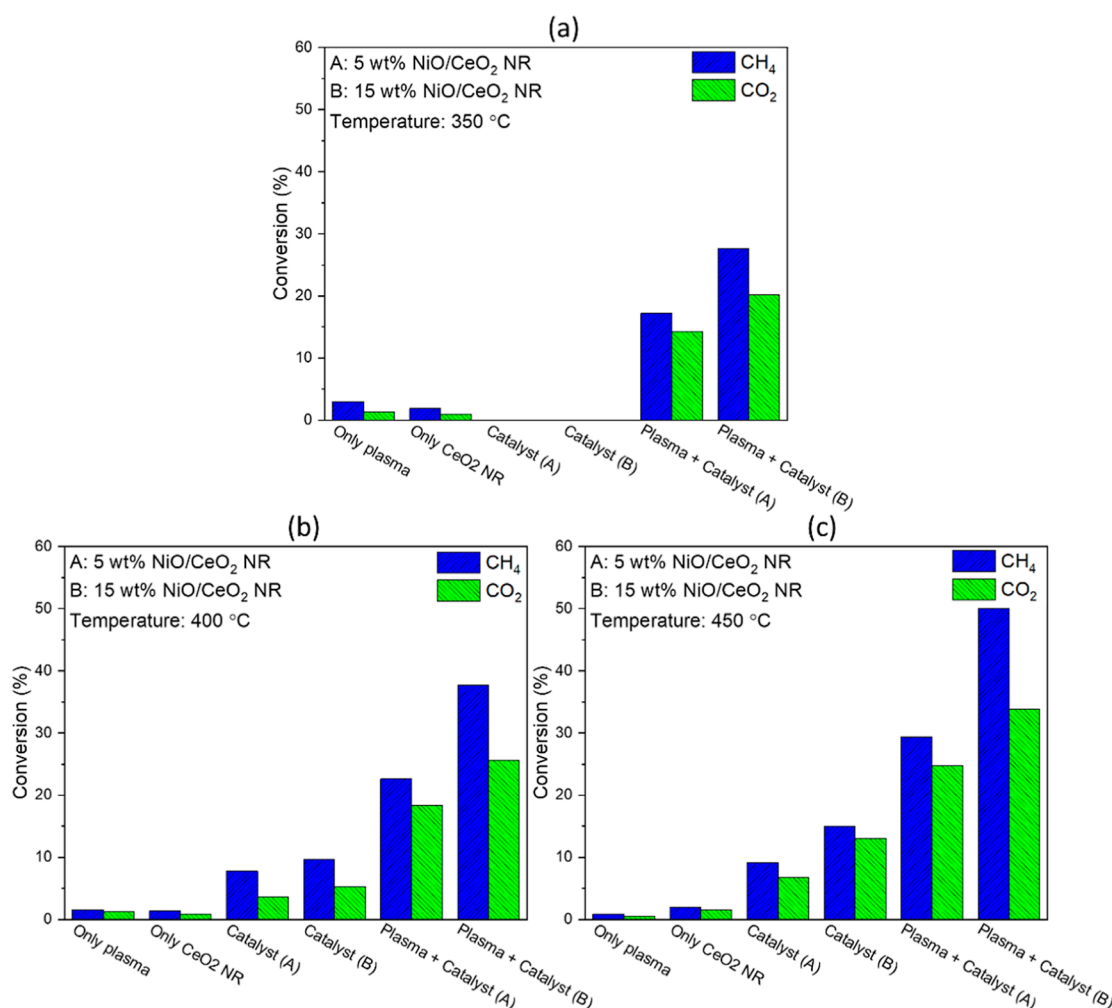




**Figure 6.** (a,d,g,h) HRTEM images of 15 wt % NiO/CeO<sub>2</sub> NR with different magnification, (b,c) SAED patterns of 15 wt % NiO/CeO<sub>2</sub> NR, (e,f) *d* spacing of NiO and CeO<sub>2</sub>, and (i) NiO-coated CeO<sub>2</sub> catalyst model.



**Figure 7.** Measured time-resolved species mole fraction for thermal and thermal + plasma regions from 150 to 500 °C, 1 atm pressure (5 min for thermal catalysis only and 7 min for thermal + plasma catalysis) (catalyst wt: ~200 mg, power: 24.9–25.8 W, frequency: 20 kHz, flow rate: CO<sub>2</sub>: 250 sccm and CH<sub>4</sub>: 100 sccm).

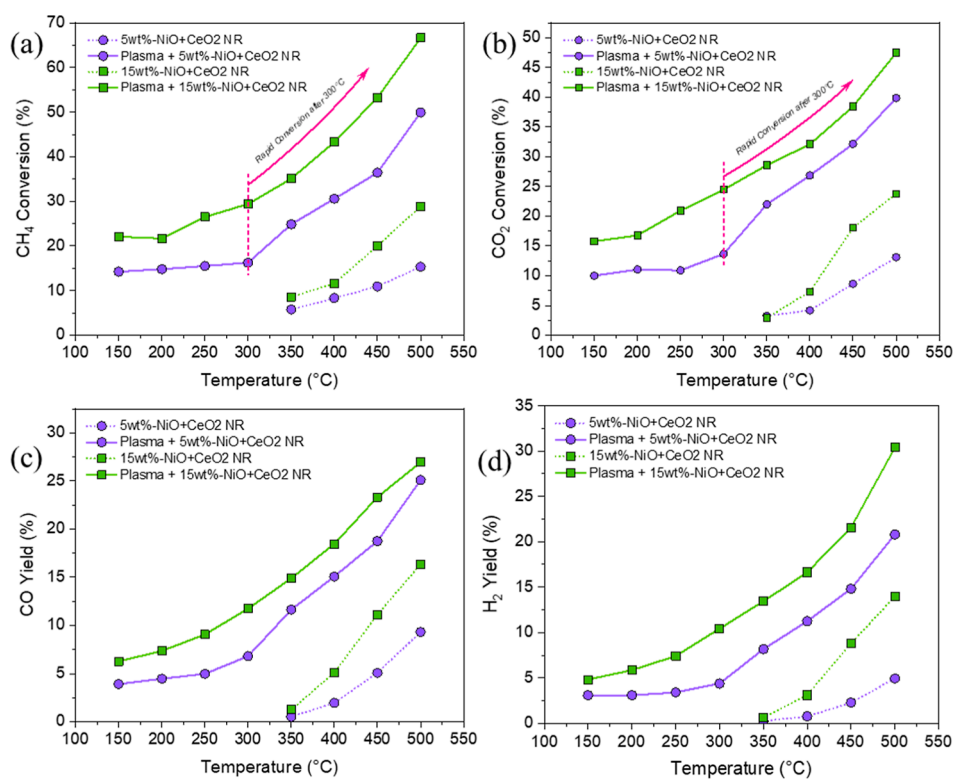


**Figure 8.** Comparison of CO<sub>2</sub> and CH<sub>4</sub> conversion in only plasma, only plasma + support (CeO<sub>2</sub> NR), thermal-assisted DRM with catalysts, and plasma-assisted DRM with catalysts for three different temperatures: (a) 350, (b) 400, and (c) 450 °C (catalyst wt: ~200 mg, power: 24.9–25.8 W, frequency: 20 kHz, flow rate: CO<sub>2</sub>: 250 sccm and CH<sub>4</sub>: 100 sccm).

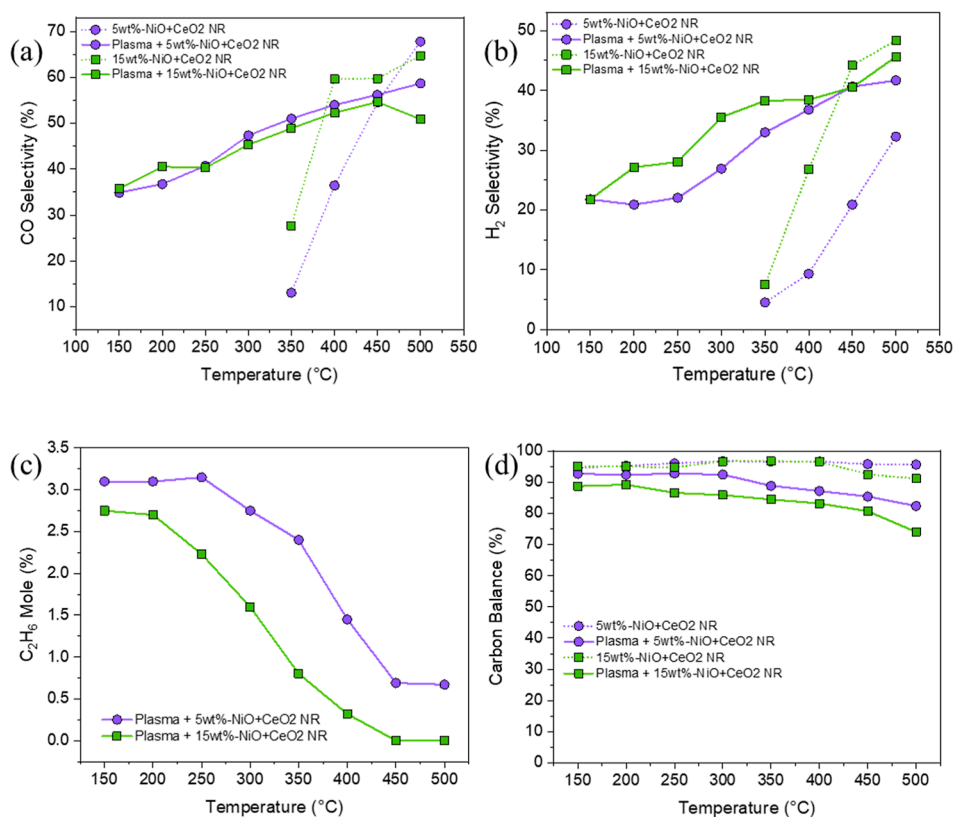
CO<sub>2</sub> conversion percentage is comparatively lower than the CH<sub>4</sub> conversion percentage. As was previously mentioned, the plasma aids in breaking down CH<sub>4</sub> more readily than CO<sub>2</sub> since CH<sub>4</sub> has a smaller BDE than CO<sub>2</sub>, which increases its adsorption on NiO surfaces, hence enhancing CH<sub>4</sub> conversion. Additionally, the quantity of Ni present in the catalyst and the lower supply of CH<sub>4</sub> relative to that of CO<sub>2</sub> can be seen as factors influencing this result. As NiO adsorbs CH<sub>4</sub>, a catalyst with a higher Ni content (15 wt % in this case) absorbs and breaks down more CH<sub>4</sub> than a catalyst with a lower Ni content (5 wt %), resulting in a greater CH<sub>4</sub> conversion rate. Others have previously investigated the effect of smaller CH<sub>4</sub>/CO<sub>2</sub> molar ratios on thermal DRM using Ni–CeO<sub>2</sub>/MgO,<sup>13</sup> Ni–WC, and Ni–Mo<sub>2</sub>C.<sup>34</sup> They discovered that, for thermal DRM, CH<sub>4</sub> conversion is higher when the CH<sub>4</sub>/CO<sub>2</sub> molar ratio is less than unity, which could be attributed to an excess amount of CO<sub>2</sub>. In another research review,<sup>35</sup> the authors noted that the presence of a higher CO<sub>2</sub> concentration increases CH<sub>4</sub> conversions in plasma catalytic synergy. According to their hypothesis, the plasma zone produces methyl/hydrocarbon radicals from CH<sub>4</sub> due to reactive metastable O(<sup>1</sup>D) produced by CO<sub>2</sub> dissociation, thus allowing the cofeed to promote each other's conversions.

According to our investigation, the 15 wt % NiO/CeO<sub>2</sub> NR catalyst demonstrated the highest CH<sub>4</sub> and CO<sub>2</sub> conversion rates, which were 29 and 24%, respectively, for thermal DRM, and 67 and 48%, respectively, for plasma-assisted DRM. It is obvious that the plasma contribution enhanced the conversion rate by more than doubling it. The conversion rates for plasma thermal synergy employing our shaped 15 wt % NiO/CeO<sub>2</sub> NR catalyst are higher compared to those of other catalysts tested in different plasma environments. When compared to experiments employing nearly equal feed ratios and different Ni-based catalysts such as Ni/γ-Al<sub>2</sub>O<sub>3</sub> in a DBD reactor,<sup>30</sup> x-Ni/γ-Al<sub>2</sub>O<sub>3</sub> (x = 5, 10, 20) in a corona discharge reactor,<sup>31</sup> x-Ni/Al<sub>2</sub>O<sub>3</sub> (x = 15, 30) in a rotating gliding spouted bed reactor, structural and textural modified CaO,<sup>8</sup> and 15 wt % Ni/TiO<sub>2</sub>,<sup>32</sup> higher conversion rates were achieved by our shaped 15 wt % NiO/CeO<sub>2</sub> NR catalyst. Although certain conversions are possible at temperatures as low as 150 °C, the plasma thermal synergy effect becomes the most effective between 300 and 500 °C. The 15 wt % NiO/CeO<sub>2</sub> NR catalyst performs similarly to lanthanum-based catalysts with aluminum supports such as LaNiO<sub>3</sub>/γ-Al<sub>2</sub>O<sub>3</sub><sup>36</sup> and La–Ni/γ-Al<sub>2</sub>O<sub>3</sub><sup>37</sup> under almost identical circumstances and reaction environments.





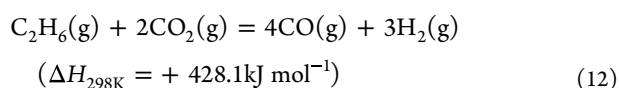
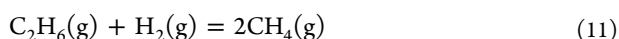
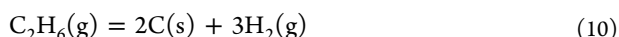
**Figure 9.** (a)  $\text{CH}_4$  conversion, (b)  $\text{CO}_2$  conversion, (c) CO yield, and (d)  $\text{H}_2$  yield using the 5 wt % NiO/CeO<sub>2</sub> NR and 15 wt % NiO/CeO<sub>2</sub> NR catalysts at various temperatures (catalyst wt: ~200 mg, power: 24.9–25.8 W, frequency: 20 kHz, flow rate:  $\text{CO}_2$ : 250 sccm and  $\text{CH}_4$ : 100 sccm).



**Figure 10.** (a) CO selectivity, (b)  $\text{H}_2$  selectivity, (c)  $\text{C}_2\text{H}_6$  production, and (d) carbon balances for the 5 wt % NiO/CeO<sub>2</sub> NR and 15 wt % NiO/CeO<sub>2</sub> NR catalysts at various temperatures (catalyst wt: ~200 mg, power: 24.9–25.8 W, frequency: 20 kHz, flow rate:  $\text{CO}_2$ : 250 sccm and  $\text{CH}_4$ : 100 sccm).

The yields of CO and H<sub>2</sub> as a function of temperature for both thermal- and plasma-assisted catalysis methods are shown in Figure 9c,d. The yields are proportional to temperature, with the maximum yields of 27% for CO and 31% for H<sub>2</sub> achieved at 500 °C when plasma is applied onto the 15 wt % NiO/CeO<sub>2</sub> NR catalyst. The results also show that the 5 wt % NiO/CeO<sub>2</sub> NR catalyst is more effective at producing CO than H<sub>2</sub>, while the 15 wt % NiO/CeO<sub>2</sub> NR catalyst produces H<sub>2</sub> more effectively than CO. However, in the thermal DRM scenario, both catalysts produce CO more effectively than H<sub>2</sub>. The addition of plasma to the experiment increases the quantity of CH<sub>4</sub> conversion, which, in turn, increases the amount of H<sub>2</sub> produced.

Figure 10a,b illustrates the trends in CO and H<sub>2</sub> selectivity, which reflect the formation of the desired CO and H<sub>2</sub> to the formation of secondary products. At 500 °C, pure thermal DRM achieves its maximum selectivity with values for CO and H<sub>2</sub> of 68 and 49%, respectively. In the case of plasma-assisted DRM, selectivity increases with increasing temperature, indicating that the process moves in the direction of the DRM reaction (eq 1). At lower temperatures, the plasma breaks down CH<sub>4</sub> into more CH<sub>x</sub><sup>+</sup> (x = 1, 2) radicals than H<sup>+</sup> radicals, leading to the generation of C<sub>2</sub> hydrocarbons (C<sub>2</sub>H<sub>6</sub> in this instance) rather than H<sub>2</sub>, which lowers the selectivity. On the other hand, when the temperature rises, the Ni catalyst becomes more active, able to adsorb gaseous C<sub>2</sub>H<sub>6</sub> on the surface and dissociate bonds via ethane cracking (eqs 10 and 11) or the ethane dry reforming process (eq 12), increasing the selectivity.<sup>38</sup> This claim is also verified by the C<sub>2</sub>H<sub>6</sub> production shown in Figure 10c, which depicts the reduction in C<sub>2</sub>H<sub>6</sub> formation with increasing temperature. The responsible Ni through adsorption slows down the production of C<sub>2</sub> hydrocarbons, causing the formation rate of C<sub>2</sub>H<sub>6</sub> to be comparably lower for 15 wt % NiO/CeO<sub>2</sub> NR (higher Ni content) than for 5 wt % NiO/CeO<sub>2</sub> NR (lower Ni content). The carbon balance in Figure 10d depicts the variation in the production of unwanted carbonaceous products and carbon deposition with temperature. As temperature rises, kinetic energy increases and dissociation energy decreases, and the plasma is able to break more bonds. This results in carbon deposition through CH<sub>4</sub> breakdown (eq 2) and CO desorption (eq 3). In both thermal- and plasma-assisted DRM, 15 wt % NiO/CeO<sub>2</sub> NR deposits more carbon than 5 wt % NiO/CeO<sub>2</sub> NR because the amount of Ni in the catalyst is directly related to the rate of carbon deposition. Finally, the SMSI of the 15 wt % NiO/CeO<sub>2</sub> NR catalyst produces a large number of oxygen vacancies, which improves the performance.



## 5. CONCLUSIONS

In summary, NTP-assisted catalytic DRM is considered an efficient approach for converting CO<sub>2</sub> and CH<sub>4</sub> to valuable chemicals and fuels. The prepared catalysts were analyzed qualitatively and quantitatively using XRD, H<sub>2</sub>-TPR, HRTEM, and XPS. The catalytic evaluation showed that the 15 wt % NiO/CeO<sub>2</sub> NR catalyst significantly improves the DRM

conversion compared to the 5 wt % NiO/CeO<sub>2</sub> NR catalyst. In addition, introducing NTP facilitates the conversion far more effectively than conventional thermal catalysis DRM. H<sub>2</sub>-TPR, XPS, and CO<sub>2</sub> TPD profiles of catalysts confirmed that an increase in NiO loading over CeO<sub>2</sub> NR support enhanced the oxygen vacancy density of the catalysts by replacing Ce<sup>4+</sup> with Ni<sup>2+</sup> ions. This method was shown to promote higher conversion, up to 66% for CH<sub>4</sub> and 49% for CO<sub>2</sub> at 500 °C.

## ■ ASSOCIATED CONTENT

### Supporting Information

The Supporting Information is available free of charge at <https://pubs.acs.org/doi/10.1021/acsami.3c09349>.

Additional material characterization and performance measurement details for the 5 and 15 wt % CeO<sub>2</sub> NR-supported NiO catalysts, including CO<sub>2</sub>/CO-TPD profiles, Raman spectroscopy, Rietveld analysis, power and temperature measurement of the reactor, and activation energy graph (PDF)

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### Notes

The authors declare no competing financial interest.

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