

# Impact of Local Microenvironments on the Selectivity of Electrocatalytic Nitrate Reduction in a BPM-MEA System

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**Electrochemical nitrate reduction reaction (NO<sub>3</sub>RR) has garnered increasing attention as a pathway for converting a harmful pollutant (nitrate) into a value-added product (ammonia). However, high selectivity toward ammonia (NH<sub>3</sub>) is imperative for process viability. Optimizing proton availability near the catalyst is important for achieving selective NH<sub>3</sub> production. Here, the aim is to systematically examine the impacts of proton availability on NO<sub>3</sub>RR selectivity in a bipolar membrane (BPM)-based membrane electrode assembly (MEA) system. The BPM generates a proton flux from the membrane toward the catalyst during electrolysis. Thus, the BPM-MEA system can modulate the proton flux during operation. The impact of interposer layers, proton scavenging electrolytes (CO<sub>3</sub><sup>2-</sup>), and catalyst configurations are also examined to identify which local microenvironments favor ammonia formation. It is found that a moderate proton supply allows for an increase in ammonia yield by 576% when compared to the standard MEA setup. This also results in a high selectivity of 26 (NH<sub>3</sub> over NO<sub>2</sub><sup>-</sup>) at an applied current density of 200 mA cm<sup>-2</sup>.**

## 1. Introduction

Nitrogen-based fertilizer is essential for agriculture, however, nitrate runoff into groundwater results in serious health issues such as infant methemoglobinemia and cancer.<sup>[1]</sup> Due to the rising demand for fertilizer use, the treatment of nitrate-contaminated waters is a growing concern. Nitrate removal occurs using physicochemical methods like ion exchange resins,

which are effective in extracting nitrate from the feed stream. These physicochemical methods however generate a significant amount of waste brines that contain high concentrations of nitrate (ranging from 1000 to 9000 ppm NO<sub>3</sub><sup>-</sup>-N).<sup>[2]</sup> Disposal of this concentrated waste stream is a significant challenge. In this context, catalytic or electrocatalytic conversion of nitrate to harmless (N<sub>2</sub>) or value-added (NH<sub>3</sub>), has garnered great attention.<sup>[1d,3]</sup> The appeal of electrocatalysis is in the seamless integration with renewable energy sources, providing a means to remediate nitrogen waste with non-fossil-based energy sources.

Electrocatalytic conversion depends on fully understanding the nitrate reduction reaction (NO<sub>3</sub>RR). There has been significant progress in understanding the NO<sub>3</sub>RR reaction mechanisms, and in tuning selectivity. Reports have also

suggested that ammonia can be produced at Faradaic efficiencies (FE) exceeding 90%.<sup>[4]</sup> However, most investigations are conducted under restrictive conditions, including low current density (H-type cell), strong alkaline conditions (pH > 14), and with elevated nitrate concentration.<sup>[5]</sup> There have been limited investigations to assess the feasibility of NO<sub>3</sub>RR under high currents, in flow cells, and with wastewater-like conditions.<sup>[6]</sup> In addition, most flow-cell studies involve the use of monopolar ion exchange

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DOI: [10.1002/aenm.202304202](https://doi.org/10.1002/aenm.202304202)

membranes (Table S1, Supporting Information), namely anion exchange membranes (AEM) and cation exchange membranes (CEM). The use of AEM can result in the crossover of anions (e.g., nitrate and nitrite), while the use of CEM can result in crossover of cations (e.g.,  $K^+$ ,  $H^+$ , and  $NH_4^+$ ). These unintended ionic crossovers can have detrimental impacts on the overall efficiency and economic viability of the electrochemical process.<sup>[6a,7]</sup> These challenges underscore a significant knowledge gap that must be addressed before  $NO_3$ RR can progress towards commercialization.

The conversion of  $NO_3^-$  to  $NH_3$  involves a stepwise reduction process with multiple intermediates, resulting in the production of various reduced nitrogen compounds (e.g.,  $NO_2^-$ ,  $N_2$ , and  $NH_3$ ).<sup>[3a]</sup> Thus it is challenging to achieve high selectivity towards  $NH_3$ . Most research attempts to address this via material design.<sup>[8]</sup> However, recent studies suggested that the concentration of protons is important for  $NO_3$ RR to be selective  $NH_3$  production, especially in alkaline or neutral conditions.<sup>[9]</sup> Under these conditions, the direct reduction pathway (driven by  $H^+$  from the electrolyte) is suppressed, which is detrimental to  $NH_3$  formation. These findings indicate that maintaining a stable and well-regulated supply of protons is essential for achieving highly selective  $NH_3$  production in wastewater conditions. Nevertheless, the impact of proton availability in  $NO_3$ RR has not yet been widely examined, even though wastewater typically has a pH between 7 and 12.<sup>[2]</sup>

The incorporation of bipolar membrane (BPM) with the membrane electrode assembly (MEA) system represents a potential strategy to overcome the obstacles associated with the current development of  $NO_3$ RR for  $NH_3$  production. Compared to H-type cells, MEAs allow for higher current density studies and closely resemble commercial electrochemical cells, making MEA cell performance more representative of real-world applications.<sup>[6a,10]</sup> The BPM consists of a polymeric cation-exchange layer (CEL) and a polymeric anion-exchange layer (AEL), which has been proven to effectively prevent the crossover of ions and products during electrolysis.<sup>[6,11]</sup> By applying voltage, water dissociation occurs at the interface of the CEL and AEL, generating protons ( $H^+$ ) and hydroxide ions ( $OH^-$ ) simultaneously. Once generated, these ions undergo selective transport in the opposite direction, with  $H^+$  passing through the CEL and  $OH^-$  passing through the AEL. Recently, the use of BPM has gained increasing attention in the field of (bi)carbonate electrolysis.<sup>[12]</sup> By operating the BPM-MEA system in a “reverse bias” fashion, with the CEL oriented towards the cathode, it enables the construction of stable proton flux from the BPM toward the cathode. This proton flux can be controlled by the introduction of gaps or additive layers between the BPM and electrode.<sup>[13]</sup> This adjustable proton flux could serve as a regulator to modify the product selectivity in  $NO_3$ RR. Nevertheless, research exploring the application of BPM-MEA systems for  $NO_3$ RR remains limited.<sup>[6b]</sup>

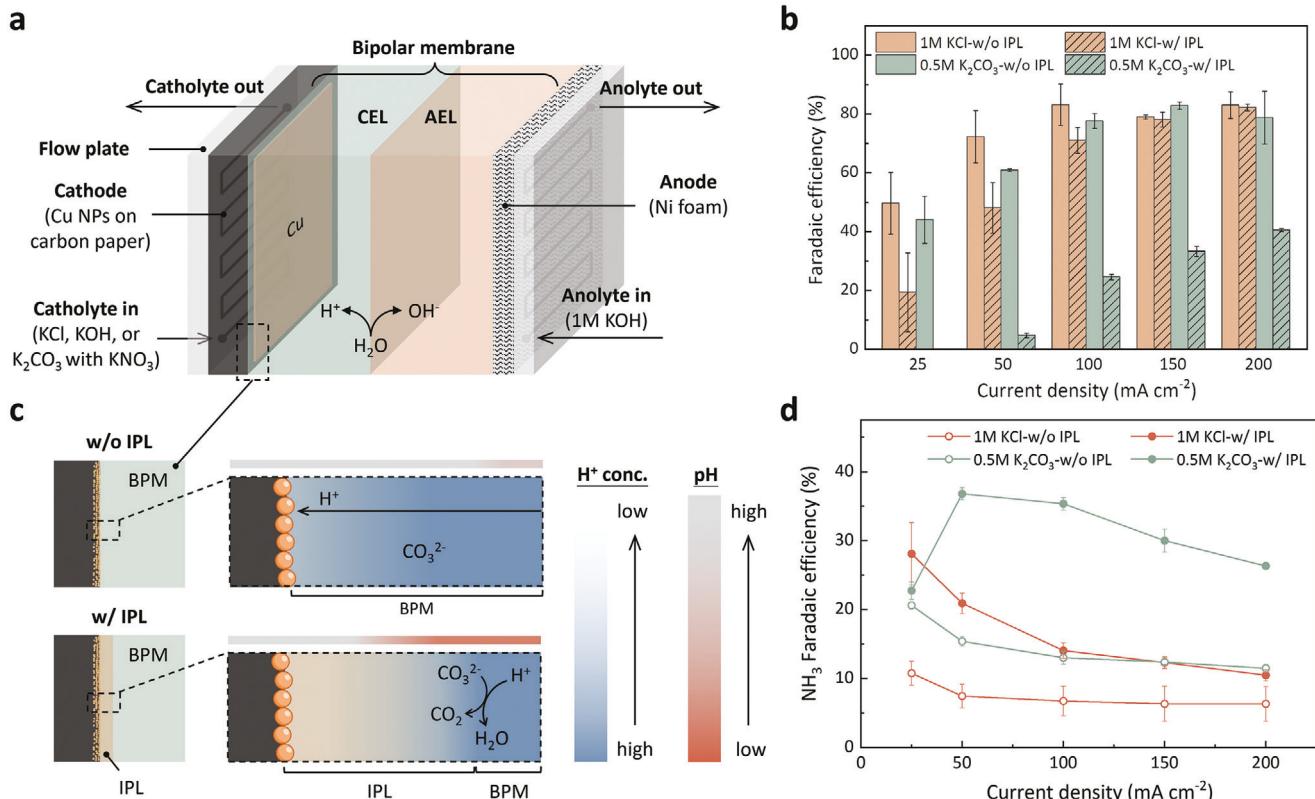
Here, we examined the  $NO_3$ RR within a BPM-MEA cell and specifically investigated how the proton availability can be tuned within the reactor to attain varied selectivity ( $NH_3$  vs  $NO_2^-$  vs  $H_2$ ). We investigate the impacts of an interposer layer (IPL) between the catalyst and membrane can have on the suppression of the hydrogen evolution reaction (HER).<sup>[13a]</sup> We also investigate the use of carbon capture-based solutions (0.5 M  $K_2CO_3$ ), which function as a proton scavenger through the conversion of

carbonate to  $CO_2$  ( $CO_3^{2-} + 2H^+ \rightarrow CO_2 + H_2O$ ). The integration of carbonate and IPL demonstrates synergistic effects in controlling proton flux, with the IPL creating a local pH gradient near the BPM that enhances both the conversion of carbonate to  $CO_2$  and the consumption of protons. We also examine various reactor configurations to tune the mass transfer of reactants (e.g.,  $NO_3^-$ ,  $H^+$ , and  $CO_2$ ). Finally, we carried out  $NO_3$ RR using an electrolyte that mimics wastewater conditions to assess the applicability of our BPM-MEA system in real-world scenarios. We demonstrate the feasibility of  $NO_3$ RR within a BPM-MEA system and propose a new MEA cell configuration that is favorable for  $NO_3$ RR under wastewater-like conditions. Through precise control of protons and the rational design of the cell configuration, high-selectivity  $NH_3$  production can be achieved.

## 2. Results and Discussion

To date, there has been no systematic study of the  $NO_3$ RR within a BPM-MEA cell. We first evaluated the performance of the  $NO_3$ RR using a standard BPM-MEA reactor configuration (Figure 1a). In this cell, the BPM is flush with the anode and cathode. Commercial copper nanoparticles were chosen as the cathodic catalysts since copper is a widely discussed catalyst for  $NO_3$ RR,<sup>[8,14]</sup> which can ensure the reproducibility of our results. Scanning electron microscopy (SEM) and energy-dispersive X-ray spectroscopy (EDX) mapping revealed a uniform and well-distributed deposition of copper nanoparticles on carbon paper, as detailed in Figures S1 and S2, Supporting Information. A Ni foam serves as the anode (Figure 1a). Given that wastewater typically has a pH in the neutral to weak alkaline range (pH = 7-12) and contains 1000–9000 ppm of nitrate ( $NO_3$ -N),<sup>[2]</sup> 1 M KCl (pH = 7) was chosen as the catholyte, with the addition of approximately 1000 ppm  $NO_3$ -N ( $70 \times 10^{-3}$  M  $KNO_3$ ) to serve as the nitrogen source. Meanwhile, 1 M KOH was added to the counterpart as the anolyte. On the cathode side, the nitrate-containing electrolyte flows along the flow pattern, with nitrate permeating through the carbon paper to reach the copper catalyst where the  $NO_3$ RR occurs.

When conducting electrolysis in 1 M KCl, the HER dominates catalytic activity ( $FE_{HER} = 49.7\%$  at 25 mA cm<sup>-2</sup>). With an increase in current density, this selectivity toward hydrogen plateau around 80% in the range of 100 to 200 mA cm<sup>-2</sup> (Figure 1b). The high HER competes with  $NO_3$ RR, leading to low  $NH_3$  FE (Figure S3, Supporting Information) and indicating an excessive proton concentration in this condition. To identify the origin of HER, we conducted electrolysis in a higher pH environment (pH 12 and 14). The results show that, unless the bulk electrolyte is extremely alkaline (e.g., pH 14), the bulk pH does not strongly affect the HER in this BPM-MEA system, which suggests that the proton flux from BPM is the primary hydrogen source that leads to high HER (Figure S4, Supporting Information). To mitigate the excessive proton flux from BPM, we introduced a mixed cellulose ester (MCE) membrane filter between the BPM and Cu electrode as an IPL, a recognized approach in BPM-based  $CO_2$  electrolysis for suppressing HER (Figure 1c).<sup>[13a]</sup> This additive layer functions by inhibiting proton transfer from the BPM to the Cu catalyst, resulting in varying levels of HER suppression at different current densities in 1 M KCl (Figure 1b). However, as the proton flux increases when applying higher current densities



**Figure 1.** a) Schematic representation of a bipolar membrane (BPM) based membrane electrode assembly (MEA) electrolyzer. b) Hydrogen evolution reaction (HER) Faradaic efficiency (FE) in 1 M KCl and 0.5 M K<sub>2</sub>CO<sub>3</sub> electrolytes containing  $70 \times 10^{-3}$  M KNO<sub>3</sub> across applied current densities ranging from 25 to 200 mA cm<sup>-2</sup>. Bars with diagonal stripes indicate electrolysis with the presence of an interposer layer (IPL). c) Simplified illustration of the pH gradient within the IPL and its impact on proton inhibition in the BPM-MEA system. d) Ammonia FE in 1 M KCl and 0.5 M K<sub>2</sub>CO<sub>3</sub> electrolytes containing  $70 \times 10^{-3}$  M KNO<sub>3</sub> with and without the presence of IPL across applied current densities ranging from 25 to 200 mA cm<sup>-2</sup>. Error bars represent standard deviations from three repeated measurements.

(100–200 mA cm<sup>-2</sup>), the inhibitory effect of the IPL on proton transfer becomes less pronounced. To tackle the issue of high HER at elevated currents, we introduced carbonate (in the form of K<sub>2</sub>CO<sub>3</sub>) into our system as a proton scavenger. In a proton-rich environment, carbonate undergoes conversion into CO<sub>2</sub> (CO<sub>3</sub><sup>2-</sup> + 2H<sup>+</sup> → CO<sub>2</sub> + H<sub>2</sub>O), which consumes protons and potentially aids in the suppression of HER. The results indicate that the proton-blocking effects of both IPL (denoted as 1 M KCl-w/ IPL) and carbonate (denoted as 0.5 M K<sub>2</sub>CO<sub>3</sub>-w/ IPL) are limited at high current densities (Figure 1b). However, when combining IPL with carbonate (denoted as 0.5 M K<sub>2</sub>CO<sub>3</sub>-w/ IPL), the proton flux is notably suppressed. The HER is controlled at around 40% FE at 200 mA cm<sup>-2</sup>, representing a 50% reduction in HER compared to 1 M KCl-w/o IPL. The pronounced strengthening of the proton-blocking effect can be ascribed to the synergistic effect arising from the incorporation of K<sub>2</sub>CO<sub>3</sub> and an IPL. The implementation of the IPL not only hinders proton transfer but also introduces a local pH gradient near the BPM.<sup>[13a]</sup> This acidic microenvironment facilitates the proton scavenger effect by promoting the conversion of carbonate into CO<sub>2</sub>, which aids in the consumption of protons. (Figure 1c). The result is consistent with findings in the field of CO<sub>2</sub> reduction reaction (CO<sub>2</sub>RR), where a prior study reported that a significant pH shift occurs near the BPM when applying IPL to the BPM electrolysis system.<sup>[13a]</sup> This

initiated a pH swing process that generated CO<sub>2</sub> from the carbonate solution (near the interface of IPL and BPM) while maintaining an alkaline environment at the catalyst side (i.e., the bulk pH).<sup>[13a]</sup> It is worth noting that the in situ generated CO<sub>2</sub> may also participate in the electrolysis (15.7% FE toward carbon products at 200 mA cm<sup>-2</sup>) (Figure S5, Supporting Information). However, once generated CO<sub>2</sub> encounters the bulk electrolyte (alkaline solution), it converts back into carbonate, as supported by the detection of only trace levels of CO<sub>2</sub> during the experiment.

Due to the suppression of HER, the formation of NH<sub>3</sub> increased, with samples containing IPLs (1 M KCl-w/ IPL & 0.5 M K<sub>2</sub>CO<sub>3</sub>-w/ IPL) exhibiting higher NH<sub>3</sub> production than samples without the presence of IPLs (1 M KCl-w/o IPL & 0.5 M K<sub>2</sub>CO<sub>3</sub>-w/o IPL), and 0.5 M K<sub>2</sub>CO<sub>3</sub>-w/ IPL demonstrates the highest NH<sub>3</sub> FE (Figure 1d). The NH<sub>3</sub> FE decreases as the current density increases in all cases, except for 0.5 M K<sub>2</sub>CO<sub>3</sub>-w/ IPL. In 0.5 M K<sub>2</sub>CO<sub>3</sub>-w/ IPL, NH<sub>3</sub> production experiences a notable improvement from 25 to 50 mA cm<sup>-2</sup>, reaches a plateau, and gradually decreases with higher current density. The low NH<sub>3</sub> production at low current density can be attributed to the limited availability of protons, aligned with the observation of no HER when applying 25 mA cm<sup>-2</sup> (Figure 1b). The sharp increase in NH<sub>3</sub> production at 50 mA cm<sup>-2</sup> supports the hypothesis that a moderate proton supply is essential for ammonia synthesis.

The results suggest that the product selectivity of  $\text{NO}_3\text{RR}$  in the BPM-MEA system is highly dependent on the local environment, and we have demonstrated that the reactants (i.e., proton flux and in situ generated  $\text{CO}_2$ ) associate with undesired side reactions exhibit strong directionality (from BPM to flow plate) within the BPM-MEA system. Based on these findings, we reconfigured the MEA cell with the Cu electrodes facing away from the BPM (toward the flow plate), denoted as the reverse configuration (Figure 2a), and carried out electrolysis to investigate the influences of electrode orientation on  $\text{NO}_3\text{RR}$  performance (Figure 2b–d). The reverse configuration demonstrates a remarkable ability to suppress HER (Figure 2b). Without the presence of an IPL, the reverse configuration (reverse-w/o IPL) exhibits  $\text{H}_2$  production similar to the forward configuration with the presence of IPL (forward-w/ IPL), while no  $\text{H}_2$  formation can be observed from 25 to 150  $\text{mA cm}^{-2}$ , and the HER FE is <9% at 200  $\text{mA cm}^{-2}$  when applying IPL (reverse-w/ IPL). The Cu electrodes remain stable after electrolysis in both configurations, confirmed by SEM, EDX mapping, and X-ray photoelectron spectroscopy (XPS) (Figures S1, S2, and S6, Supporting Information).

Such a configuration and the associated performance changes may seem counterintuitive at first glance; however, this is related to the transfer of ions and/or reactants during electrochemical reactions (Figure 2a). In a standard electrochemical cell setup, the cathode and anode face each other (forward configuration), reducing the distance for ion transfer and thus lowering the ohmic resistance in the cell for electrochemical energy storage applications.<sup>[10,15]</sup> In electrocatalysis research using an H-type cell, the diffusion of reactants is, in principle, non-directional, so the performance will not be markedly affected whether in a reverse or forward configuration. However, in the BPM-MEA system, the reactants (for example, nitrate in  $\text{NO}_3\text{RR}$ ) are supplied from the flow plate, while protons are sourced from the BPM, creating a divergent transport path. In a standard setup (forward configuration), nitrate needs to diffuse through the substrate (in this case, carbon paper) to reach the Cu catalyst where the reduction reaction occurs, which, in turn, increases its diffusion resistance (Figure 2a). In the reverse setting, the resistance of nitrate diffusion decreases, while the diffusion length for protons and  $\text{CO}_2$  increases, which is beneficial for  $\text{NO}_3\text{RR}$ . As a result, both HER and  $\text{CO}_2\text{RR}$  were highly inhibited (Figure 2c), with  $\text{CO}_2\text{RR}$  nearly vanishing. Furthermore, the cell voltage decreases when compared to the forward configuration, which serves as direct evidence that the resistance for  $\text{NO}_3\text{RR}$  is reduced in a reverse fashion (Figure S7, Supporting Information).

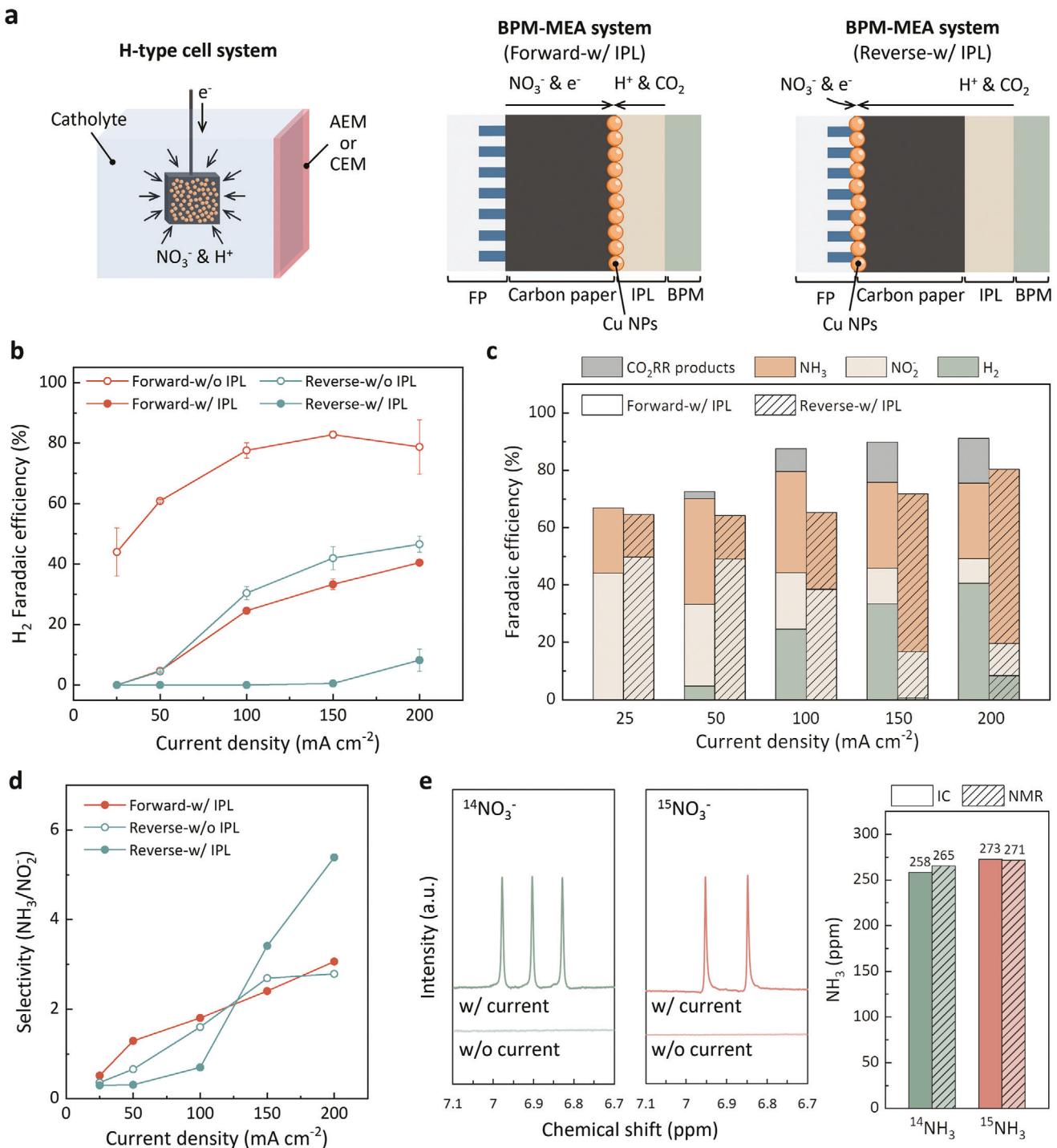
We have developed different methods (i.e., forward-w/ IPL, reverse-w/o IPL, and reverse-w/ IPL), which show varying degrees of HER suppression (Figure 2b). We then explore how the configurations alter  $\text{NO}_3\text{RR}$  selectivity for  $\text{NH}_3$  over  $\text{NO}_2^-$  (Figure 2d). In all configurations, the selectivity increases with increasing current density. This can be attributed to the higher current density, where proton flux increases and creates proton-rich environments, promoting the formation of  $\text{NH}_3$  over  $\text{NO}_2^-$  despite the elevated HER.<sup>[16]</sup> In the reverse-w/ IPL configuration, in the low current density region (<100  $\text{mA cm}^{-2}$ ), the selectivity is exceptionally low, primarily due to the excessive suppression of protons (Figure 2b), resulting in a more favorable formation of  $\text{NO}_2^-$ . Similar low selectivity performance can also be observed in other configurations when HER is low (both forward-w/ IPL

and reverse-w/o IPL at 25  $\text{mA cm}^{-2}$ ). Subsequently, as the current density increases, the selectivity increases significantly in the reverse-w/ IPL configuration. This serves as strong evidence that moderate proton supply is crucial for  $\text{NH}_3$  production. It is noteworthy that both the forward-w/ IPL and reverse-w/o IPL configurations exhibit comparable trends in selectivity (Figure 2d) as well as HER (Figure 2b), which further supports the notion that hydrogen plays an important role in selective  $\text{NH}_3$  production.

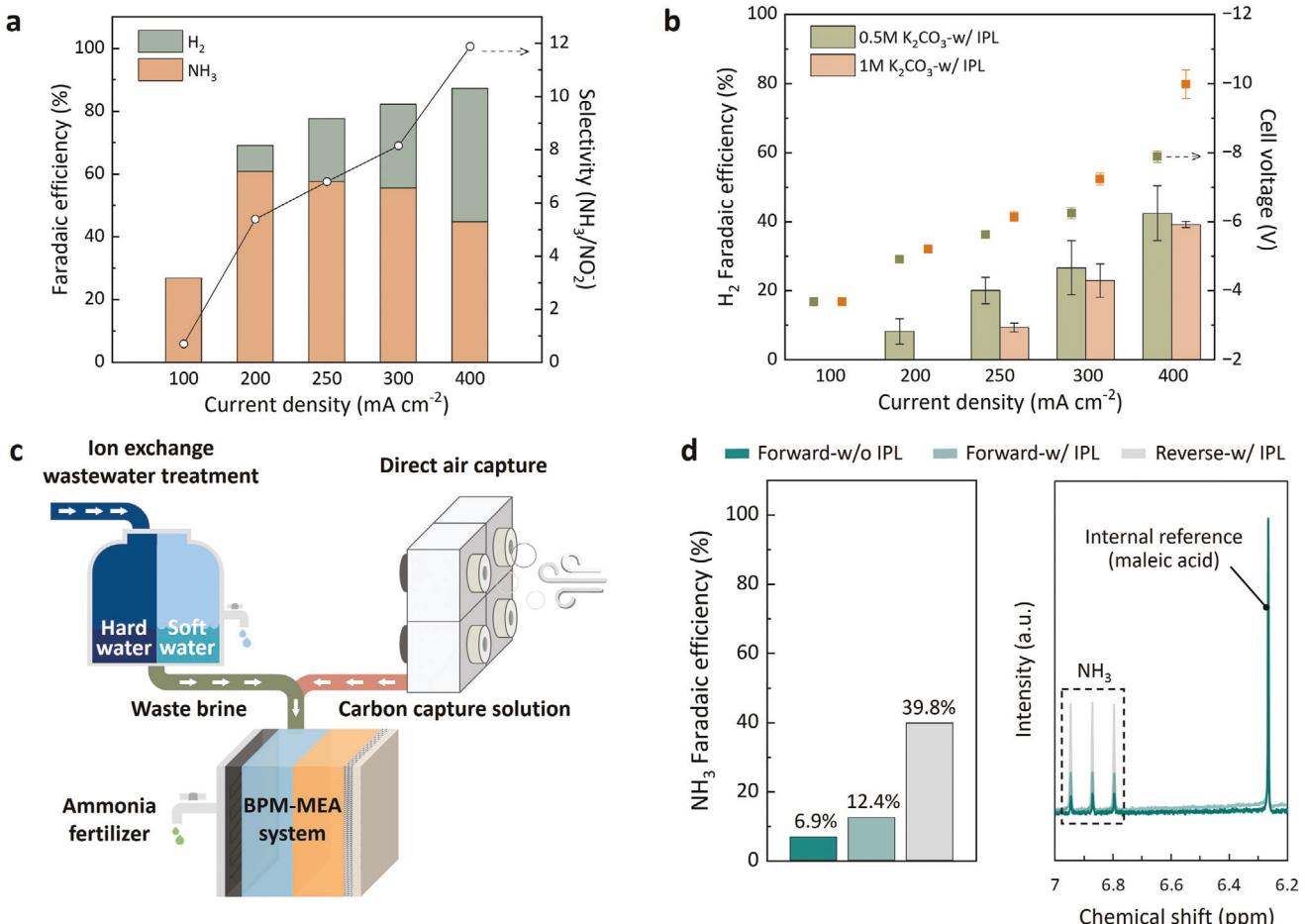
To exclude the possibility of adventitious ammonia contamination that could lead to false positive results, the experiments were conducted rigorously, and all equipment (e.g., BPM, flow pattern, tubing, gasket, etc.) that might come into contact with the samples were rinsed with DI water before use.<sup>[17]</sup> Isotope labeling  $^1\text{H}$  NMR spectroscopy was conducted (see Experimental Section). Due to its ability to distinguish between different isotopes (in this case,  $^{14}\text{NH}_3$  and  $^{15}\text{NH}_3$ ), isotope labeling NMR measurement is considered the most robust method to verify the nitrogen source for the measured  $\text{NH}_3$ .<sup>[18]</sup> The electrolytes for NMR measurement were collected after electrocatalytic reduction in the reverse-w/ IPL configuration. The NMR spectra show triplet peaks, which correspond to  $^{14}\text{NH}_3$ , when current is applied (200  $\text{mA cm}^{-2}$ ) and  $^{14}\text{NO}_3^-$  was used as the nitrogen source (Figure 2e). When switching the nitrogen source to  $^{15}\text{NO}_3^-$ , the NMR spectra show clear doublet peaks, which correspond to the formation of  $^{15}\text{NH}_3$ , and no  $^{14}\text{NH}_3$  peaks can be observed in this case. This indicates that the contamination level in our setup is low. To support this, control experiments without applying current were conducted (Figure 2e). The NMR spectra show that neither  $^{14}\text{NH}_3$  nor  $^{15}\text{NH}_3$  was detected, suggesting that contamination from nitrate and the system can be disregarded. Quantitative NMR measurements were performed using maleic acid as the internal reference. The  $\text{NH}_3$  concentrations are very similar (<2% difference) when using either  $^{15}\text{NO}_3^-$  or  $^{14}\text{NO}_3^-$  as the nitrogen source and are consistent with the  $\text{NH}_3$  measured by IC, further suggesting that the  $\text{NH}_3$  measured in our experiments solely originates from  $\text{NO}_3\text{RR}$ .

We then investigated the  $\text{NO}_3\text{RR}$  performance of the reverse-w/ IPL configuration at elevated currents (Figure 3a). In line with the above discussion, as the current increases, the selectivity for  $\text{NH}_3$  over  $\text{NO}_2^-$  continues to rise, as well as the production of  $\text{H}_2$ . As the competition between  $\text{NO}_3\text{RR}$  and HER intensified with the rising current, the performance reached its peak with an optimal  $\text{NH}_3$  selectivity of 60.8% FE at an applied current density of 200  $\text{mA cm}^{-2}$ , and the highest  $\text{NH}_3$  partial current density achieved was 178.84  $\text{mA cm}^{-2}$  at  $-7.89\text{ V}$  (Figure S8, Supporting Information).

The impact of carbonate concentration on  $\text{NO}_3\text{RR}$  was examined (Figures S9 and S10, Supporting Information), as carbonate solution plays an important role in our BPM-MEA system. As a proton scavenger, increasing the carbonate concentration leads to a decrease in  $\text{H}_2$  formation (Figure 3b), which can be ascribed to the higher concentration of carbonate likely generating more  $\text{CO}_2$ , resulting in the consumption of more protons.<sup>[13a]</sup> Due to the superior proton regulation of 1  $\text{M}$   $\text{K}_2\text{CO}_3$  compared to 0.5  $\text{M}$   $\text{K}_2\text{CO}_3$ , the peak of  $\text{NH}_3$  FE shifts from 60.8% at 200  $\text{mA cm}^{-2}$  to 61.0% at 250  $\text{mA cm}^{-2}$  (Figure S10, Supporting Information). The claims that higher carbonate concentration generates more  $\text{CO}_2$  can be supported by the observation of higher cell voltage in 1  $\text{M}$   $\text{K}_2\text{CO}_3$  compared to 0.5  $\text{M}$   $\text{K}_2\text{CO}_3$  (Figure 3b). The increased



**Figure 2.** a) Simplified schematic of the mass transfer of reactants in different electrolyzer configurations. AEM: anion exchange membrane. CEM: cation exchange membrane. FP: flow plate. b)  $H_2$  FE in  $0.5\text{ M}$   $K_2CO_3$  electrolyte containing  $70 \times 10^{-3}\text{ M}$   $KNO_3$  with electrode facing towards (forward-w/o IPL and forward-w/ IPL) and away (reverse-w/o IPL and reverse-w/ IPL) from the BPM. Error bars represent standard deviations from three repeated measurements. c) Product distribution of  $NO_3$ RR done with forward-w/ IPL and reverse-w/ IPL at varying applied current densities ranging from 25 to  $200\text{ mA cm}^{-2}$ . The electrolysis was conducted in  $0.5\text{ M}$   $K_2CO_3$  containing  $70 \times 10^{-3}\text{ M}$   $KNO_3$ . The  $CO_2$ RR products include  $C_2H_4$ ,  $CH_4$ ,  $HCOO^-$ , and  $CO$ . d) Ammonia-to-nitrite selectivity at forward and reverse configurations in  $0.5\text{ M}$   $K_2CO_3$  containing  $70 \times 10^{-3}\text{ M}$   $KNO_3$ . e) Quantitative ammonia measurements using ionic chromatography (IC) and  $^1H$  nuclear magnetic resonance (NMR) spectroscopy. The samples were collected after electrolysis with and without the applied of current ( $200\text{ mA cm}^{-2}$ ) in electrolytes containing  $70 \times 10^{-3}\text{ M}$   $K^{14}NO_3$  and  $K^{15}NO_3$ .



**Figure 3.** a) Performance metrics for ammonia and hydrogen production using the reverse-w/ IPL configuration at higher current densities ranging from 100 to 400 mA cm<sup>-2</sup> in a 0.5 M K<sub>2</sub>CO<sub>3</sub> solution containing 70 × 10<sup>-3</sup> M KNO<sub>3</sub>. The right-hand y-axis indicates the selectivity of ammonia to nitrite. b) H<sub>2</sub> FE and corresponding cell voltages measured in 0.5 and 1 M K<sub>2</sub>CO<sub>3</sub> electrolytes with a nitrate concentration of 70 × 10<sup>-3</sup> M using the reverse-w/ IPL system. Error bars represent standard deviations from three repeated measurements. c) Simplified diagram illustrating NO<sub>3</sub>RR using the BPM-MEA system with nitrate-concentrated brine from ion exchange water treatment plants and carbon capture solution from the direct air capture facilities. d) Performance of ammonia production using synthetic wastewater as the catholyte in different electrolyzer configurations under applied current density at 200 mA cm<sup>-2</sup>.

overpotential can be attributed to the in situ generation of CO<sub>2</sub>, which forms tiny bubbles near the interface of IPL and BPM, leading to higher resistance.<sup>[13a]</sup> It is worth noting that even in the 1 M K<sub>2</sub>CO<sub>3</sub> electrolyte, the electrolysis produces negligible carbon products (about 1% FE toward carbon products; Figure S11, Supporting Information). This finding suggests that CO<sub>2</sub> is well regulated in the reverse-w/ IPL configuration and reinforces the role of carbonate as a co-catalyst (proton scavenger) rather than a reactant, as it does not participate in the NO<sub>3</sub>RR.

To gain a better understanding of the performance of the BPM-MEA cell in real-world conditions, we conducted electrolysis in a mimic wastewater solution. As a proof of concept, synthetic wastewater was prepared by mixing nitrate-concentrated brine from ion exchange water treatment plants (containing Na<sup>+</sup>, K<sup>+</sup>, Mg<sup>2+</sup>, Cl<sup>-</sup>, SO<sub>4</sub><sup>2-</sup>, and NO<sub>3</sub><sup>-</sup>) and carbon capture solution (1.5 M K<sub>2</sub>CO<sub>3</sub>) from direct air capture facilities in a volume ratio of 2:1 (Figure 3c; See Experimental Section).<sup>[2e,13a,19]</sup> Due to the presence of highly concentrated Na ions (1.4 M) in the mimic wastewater, quantitative <sup>1</sup>H NMR was used to measure NH<sub>3</sub>, as the NH<sub>3</sub>

peak overlaps with the Na<sup>+</sup> peak in IC under this specific condition. Compared to the standard MEA setup (forward-w/o IPL), the reverse-w/ IPL configuration exhibits stronger NH<sub>3</sub> characteristic peaks in the NMR spectra, corresponding to 167 ppm and 29 ppm of NH<sub>3</sub> after 30 min electrolysis in the reverse-w/ IPL and forward-w/o IPL configurations, respectively. At a current density of 200 mA cm<sup>-2</sup>, the NH<sub>3</sub> FE, however, decreased to 39.8% compared to the 60.8% NH<sub>3</sub> FE achieved in pure 0.5 M K<sub>2</sub>CO<sub>3</sub> electrolyte, despite the higher nitrate contents supplied in the mimic wastewater solution (100 × 10<sup>-3</sup> M NO<sub>3</sub><sup>-</sup> in the synthetic wastewater compared to 70 × 10<sup>-3</sup> M NO<sub>3</sub><sup>-</sup> in the 0.5 M K<sub>2</sub>CO<sub>3</sub> electrolyte). The decrease in NH<sub>3</sub> FE may be associated with the detrimental effects of the complex interplay between the multi-ionic environment and active sites.<sup>[5b,20]</sup> Nevertheless, the results suggest that the reverse-w/ IPL configuration is more favorable for NH<sub>3</sub> production compared to the standard MEA setup (with an almost 6-fold increase in NH<sub>3</sub> yield) in wastewater-like conditions. This improvement can primarily be ascribed to the effective control of reactants transfer in the reverse-w/ IPL setup.

We expect that better performance can be achieved through optimization efforts, but the focal point of this work lies in emphasizing a fresh perspective: tackling the selective  $\text{NH}_3$  production of  $\text{NO}_3\text{RR}$  from a cell design standpoint.

### 3. Conclusions

In conclusion, our research highlights the critical importance of moderate proton supply for achieving selective  $\text{NH}_3$  production in  $\text{NO}_3\text{RR}$ . We employed various strategies (including IPL and proton scavenger) to modulate the proton flux and showcased their synergistic effect on proton regulation through integration. Furthermore, we proposed a new perspective on the configuration of BPM-based MEA cells for electrocatalytic studies, by evaluating the mass transfer limitations in current MEA setup. Quantitative isotope labeling NMR measurement was employed to ensure genuine ammonia production. By utilizing the new configuration,  $\text{NH}_3$  yield has increased by 576% compared to the standard BPM-MEA setup in mimic wastewater solution, marking a significant advancement in  $\text{NO}_3\text{RR}$ . Future efforts can focus on optimizing performances, such as stability (Figure S12, Supporting Information) and energy efficiency (Figure S13, Supporting Information). These can be done by catalyst or membrane optimization. Furthermore, the potential applications of this system can be explored by adjusting the interlayers. For example, we observed variations in product distribution when introducing the Ag layer on the back side of the Cu electrode (Figure S14, Supporting Information). The strategies we developed here are universal (Figure S15, Supporting Information) and serve to regulate reactant transfer and local environments in BPM-based MEA cell electrolysis, which can be challenging to achieve in the setups of other electrochemical cells. We hypothesize that the BPM-MEA system we proposed can be utilized to investigate and optimize other electrochemical synthesis processes, such as the electrosynthesis of urea.<sup>[21]</sup>

### Supporting Information

Supporting Information is available from the Wiley Online Library or from the author.

### Acknowledgements

P.-W.H. and H.S. contributed equally to this work. This material is based upon work supported by the National Science Foundation under Grant No. 1846611 and 1933646. This work was supported by the Gordon and Betty Moore Foundation (Award 10615). This work was supported by the National Science Foundation through the Center for Advancing Sustainable and Distributed Fertilizer Production (CASFER) under Grant No. EEC-2133576.

### Conflict of Interest

The authors declare no conflict of interest.

### Data Availability Statement

The data that support the findings of this study are available in the supplementary material of this article.

### Keywords

bipolar membrane, electrochemical nitrate reduction, hydrogen, membrane electrode assembly, product selectivity

Received: December 6, 2023

Revised: January 14, 2024

Published online:

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