

# Corrosion Protective Coatings from Poly(heterocyclic diphenylamine): Polyaniline Analogues

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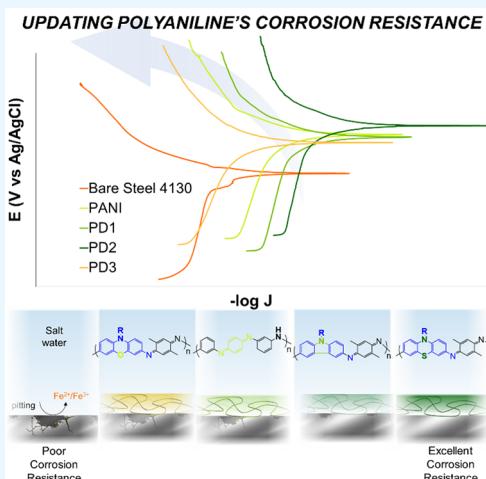
Supporting Information

**ABSTRACT:** This study explores conducting polymers with side chains containing long, branched alkyl groups as candidates for corrosion suppression coatings. These polymers, containing carbazole, phenothiazine, and phenoxazine cores, may be considered as analogues to polyaniline, which is often employed in corrosion control applications. The polymers are prepared from the corresponding dibrominated carbazole, phenothiazine, and phenoxazine monomers with 2,5-dimethyl-1,4-phenylenediamine by the Buchwald–Hartwig coupling reaction. The effectiveness of these coatings for corrosion suppression was tested by potentiodynamic polarization studies and electrochemical impedance spectroscopy. The morphology of the coatings was characterized by scanning electron microscopy (SEM) and atomic force microscopy (AFM). Corrosion testing of coated AISI 4130 steels in 3.5 wt % NaCl showed that the phenothiazine- and carbazole-containing polymers display excellent corrosion resistance. The protection efficiency (PE) of 95.9% for phenothiazine outperformed the other polymers, including polyaniline coating. SEM images indicate that the polymers are still uniformly coated with stable morphology after 24 h of exposure to corrosive media. These results suggest that phenothiazine- and carbazole-based PANI analogues may be candidates for protective organic coatings in transportation, aviation, marine, and oil and gas industrial applications.

**KEYWORDS:** corrosion, polyaniline, polyaniline analogues, poly(heterocyclic diphenylamine), phenothiazine, carbazole, phenoxazine, conducting polymer

## 1. INTRODUCTION

The ability of conducting polymers (CPs) to impart corrosion resistance to some metals has attracted researchers for many years.<sup>1,2</sup> Conducting polymers such as polypyrrole (PPy), polythiophene (PTh), poly(3,4-ethylenedioxythiophene) (PEDOT), polyaniline (PANI), poly(*p*-phenylene) (PPP), poly(*p*-phenylenevinylene) (PPV), and polycarbazole (PCz) have all been proposed as components of corrosion protection coatings.<sup>2–6</sup> PANI is one of the most studied conducting polymers to date due to its exceptional environmental stability in the doped state, good mechanical properties, and high electrical conductivity.<sup>1,6–8</sup> Since DeBerry reported using PANI as a protective coating for stainless steels, PANI-based coatings have been used to improve the corrosion protection of many metals, including aluminum, titanium, magnesium, aluminum alloys, steel, copper, and zinc.<sup>5,9–15</sup> The redox activity of PANI is implicated in providing anodic corrosion protection because it shifts the equilibrium potential of the coated substrate in a positive (i.e., anodic) direction.<sup>6,12,16,17</sup> PANI exists in three interconvertible forms depending on the redox state: the partially oxidized emeraldine base (EB), fully oxidized pernigraniline base (PB), and fully reduced leucoemeraldine



base (LB) form. All of these forms of PANI are insulators. Moreover, PANI has been used as an anticorrosion coating in diverse corrosive media. The EB form is the most common structure of PANI due to its high chemical stability and is widely employed as anticorrosion coating for ferrous and non-ferrous metals and alloys.<sup>4,5</sup> The EB form, for instance, is very effective in combating corrosion from NaCl.<sup>4,5</sup> EB is converted to conducting emeraldine salt (ES) by acid doping, which leads to effective corrosion control in acidic solutions.<sup>18,19</sup> PANI's protective coating for metallic surfaces provides high corrosion resistance<sup>14</sup> by forming adjacent layers of passive metallic oxide such as  $\text{Fe}_3\text{O}_4$ ,  $\alpha\text{-Fe}_2\text{O}_3$ , and  $\gamma\text{-Fe}_2\text{O}_3$ <sup>2,6,20,21</sup> or forming nitrides<sup>22</sup> and by promoting the passivation of the coated substrates. The metal surface is shielded from further corrosion by these thick oxide layers that serve as physical barrier

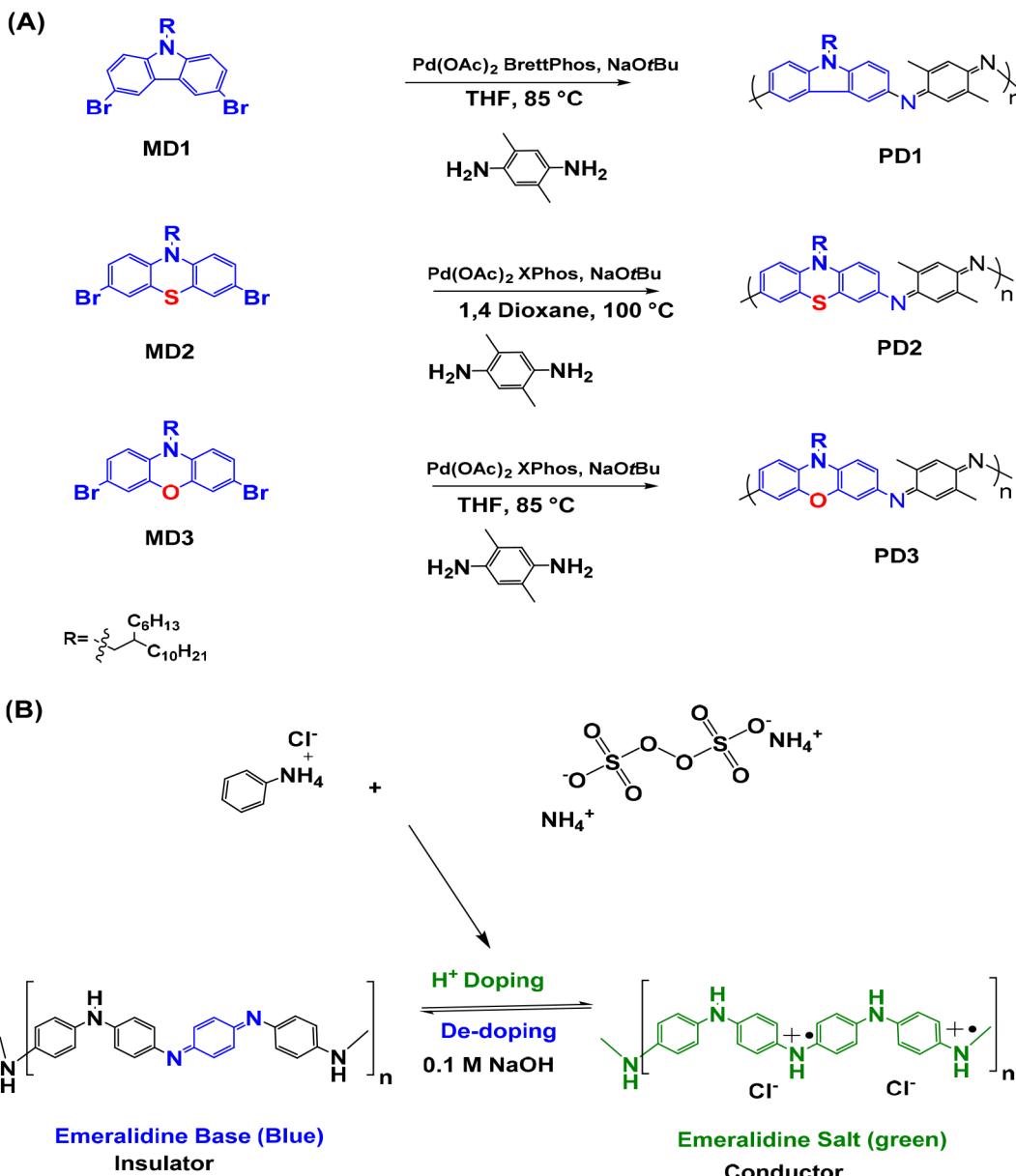
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**Figure 1.** (A) Synthetic route of PANI analogues. (B) Synthetic route to PANI nanofibers from aniline hydrochloride.

protection.<sup>2,5,6</sup> The effectiveness of barrier protection can be increased by enhancing PANI coating's bonding (adhesion) abilities to the metal–polymer interface.<sup>2,6,17,20</sup>

Despite its wide use for corrosion protection, PANI has limitations as a material. One of these limitations is the reported poor adhesion of PANI to metal surfaces.<sup>3,23,24</sup> The poor solubility of PANI in most organic solvents limits its processability for industrial applications.<sup>6,25</sup> Consequently, electrochemical oxidative polymerization of aniline may be used to form PANI films on metals and alloys.<sup>2,6</sup> Developing conducting polymers with improved electrochemical and mechanical stability compared to PANI is needed to improve coating application from organic solvents.<sup>26,27</sup> Methods such as the modification of monomer structure, use of soluble precursors, and formation of copolymers or composites have been introduced to improve PANI's properties (conductivity, solubility, etc.).<sup>3,15,23,24,28–34</sup> Our efforts are to incorporate large, branched alkyl chains into the polymer and replace the

aniline backbone with precursors (carbazole, phenothiazine, and phenoxazine) that can improve solubility (e.g., by derivatization with alkyl or other solubilizing groups) in common organic solvents, thereby enhancing their processability for wide organic coating application, explicitly investigating their anticorrosion properties with a view of projecting these materials as promising candidates for corrosion control coatings.

In this paper, we demonstrate the synthesis of processable PANI analogues incorporating long branched alkyl chains by the copolymerization of 2,5-dimethyl-*p*-phenylenediamine (PPDA) with 3,6-dibromo-9-(2-hexyldecyl)carbazole, 3,7-dibromo-10-(2-hexyldecyl)phenothiazine, and 3,7-dibromo-10-(2-hexyldecyl)phenoxazine by the Buchwald/Hartwig reaction for anticorrosion coatings. Specifically, the polymers are poly(10-(2-hexyldecyl)carbazole-3,7-diyl-*alt*-2,5-dimethyl-*p*-phenylenediamine) (**PD1**), poly(10-(2-hexyldecyl)-phenothiazine-3,7-diyl-*alt*-2,5-dimethyl-*p*-phenylenediamine) (**PD2**), and poly(10-(2-hexyldecyl)phenoxazine-3,7-diyl-*alt*-

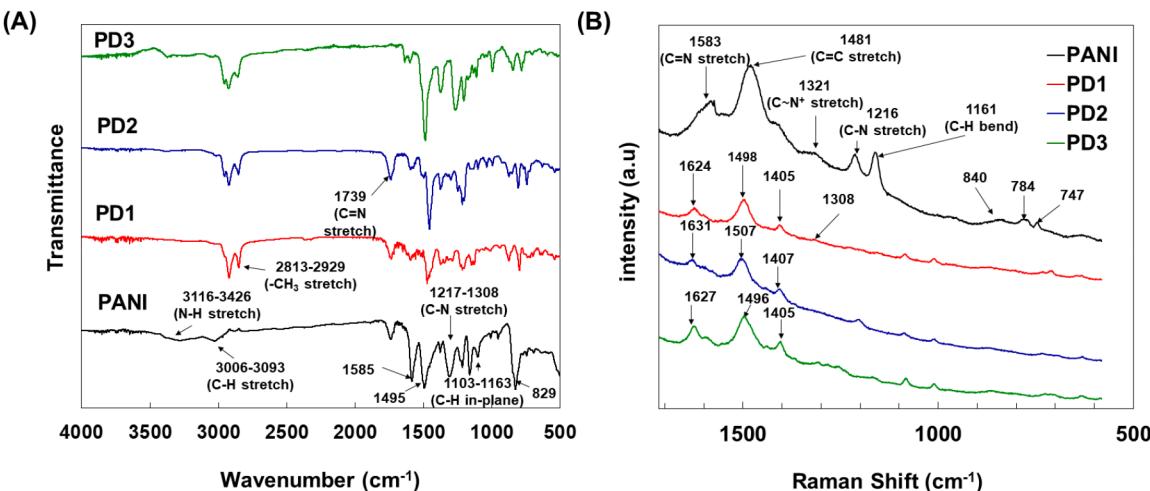


Figure 2. (A) ATR-IR spectra of PANI, PD1, PD2, and PD3. (B) Raman spectra of PANI, PD1, PD2, and PD3.

2,5-dimethyl-*p*-phenylenediamine) (PD3). The polymers were successfully characterized by ATR-IR, UV, and <sup>1</sup>H NMR spectroscopy, and solution was deposited from various common organic solvents. These polymers were then examined as corrosion-protective barrier coatings and compared to PANI coatings, as the EB form for both PANI analogues and PANI was used in this study. Corrosion resistance efficiency is tested for the films on steel in 3.5 wt % NaCl solution using potentiodynamic polarization and electrochemical impedance spectroscopy (EIS). Superior corrosion inhibition by the phenothiazine-core coating on steel in comparison to PANI was demonstrated in this work, introducing it as an option for corrosion control applications. To our knowledge, this work is the first report on these PANI analogues for use as in corrosion protection.

## 2. EXPERIMENTAL SECTION

**2.1. Materials.** All chemicals used in this study were reagent grade and used without further purification unless otherwise stated. A solvent purification system was used to obtain dry, degassed tetrahydrofuran (THF), dichloromethane (DCM), and toluene. Aniline hydrochloride and ammonium persulfate (APS, 99%) were purchased from Fisher Scientific (Princeton, NJ), and acetone (HPLC grade), *N*-methyl-2-pyrrolidone (NMP), and *N,N*-dimethylformamide (DMF) (ACs reagent grade, 99.8%) were purchased from Sigma-Aldrich Chemicals (USA). Deionized water with resistivity of not less than 18.0 MΩ cm was used throughout the analysis.

**2.2. Substrate Preparation.** Chromium–molybdenum alloy steel (AISI 4130AQ) coupons of dimensions 5.08 cm × 5.08 cm × 0.16 cm were obtained from [OnlineMetals.com](http://OnlineMetals.com). The steel is specified as 6345ASTM A505/S06 normalized or otherwise heat-treated with the following reported composition (wt %) of 0.32 C, 0.46 Mn, 0.008 P, 0.001 S, 0.19 Si, 0.039 Al, 0.03 Cu, 0.02 Ni, 0.91 Cr, 0.15 Mo, 0.006 Sn, 0.005 V, 0.001 Nb, 0.0002 B, 0.0040 Ti, 0.0027 Ca, 0.0050 N, and Fe, the balance. The steel coupons were polished using SiC paper in the order of 240, 400, and 800 grit. After polishing, the coupons were sonicated in acetone for 15 min, air-dried, and immediately coated with the polymer.

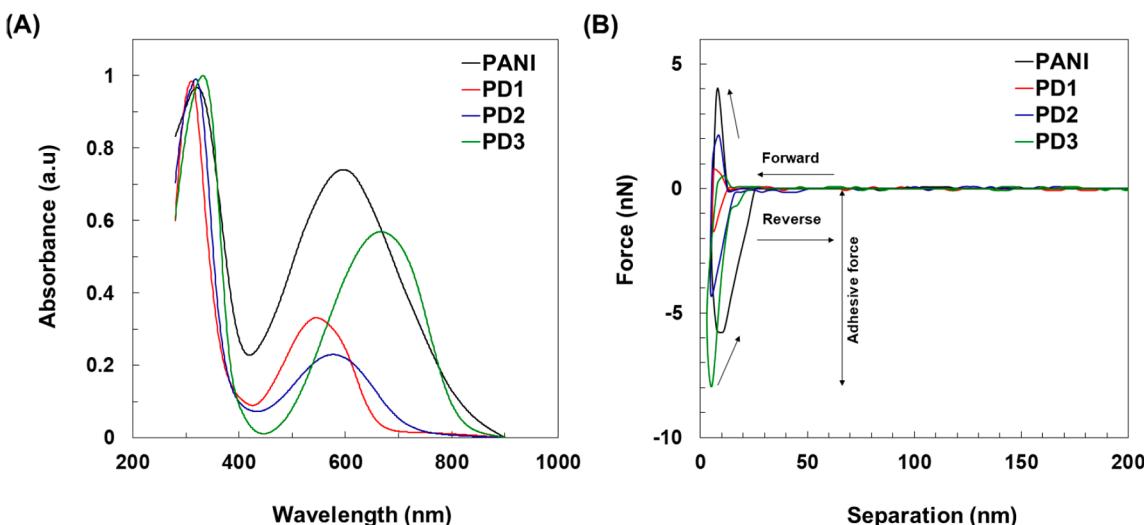
**2.3. Synthesis of Polyaniline Analogues.** The monomers 3,6-dibromo-9-(2-hexyldecyl)carbazole (MD1), 3,7-dibromo-10-(2-hexyldecyl)phenothiazine (MD2), and 3,7-dibromo-10-(2-hexyldecyl)phenoxazine (MD3) were prepared using a previously reported method for similar monomers.<sup>27,35</sup> Synthesis of the polymers followed previously reported methods (Figure 1A).<sup>26–28,35</sup> MD1, MD2, and MD3 (1 equiv), 2,5-dimethyl-*p*-phenylenediamine (1.05 equiv), NaOtBu (2.8 equiv), Pd(OAc)<sub>2</sub> (0.05 equiv), and Brettphos

(0.075 equiv for MD1)/Xphos (0.075 equiv for MD2 and MD3) were all added into an oven-dried microwave vial containing a magnetic stir bar, which was capped before being removed from the glovebox. For the product desired, either 5 mL of freshly distilled THF or dioxane (5 mL) was added to the mixture, and the vial was placed in an oil bath at 85 or 100 °C and stirred vigorously for 24 h. The reaction mixture was cooled to room temperature and diluted with DCM. The mixture was then filtered through diatomite and the filtrate concentrated under reduced pressure to give the crude polymer. The crude polymer was purified using a Soxhlet extractor with ethanol, acetone, hexane, and finally collected in chloroform. Polymers PD1, PD2, and PD3 were concentrated under reduced pressure to give 81%, 70%, and 52% yield, respectively.

**2.4. Preparation of PANI.** PANI was synthesized by first dissolving aniline hydrochloride (1.3 g, 0.1 mol) in 70 mL of deionized water. This solution was cooled to 0 °C in an ice bath and oxidized with aqueous APS (2.28 g in 30 mL) added dropwise over 20 min with vigorous stirring during the initial oxidation and then with continuous stirring for 24 h. The resulting product was filtered and washed with deionized water until a clear filtrate was observed. The polyaniline was dedoped with 0.1 M sodium hydroxide (NaOH) in a 2-neck flask with vigorous stirring and subsequent stirring for 24 h (Figure 1B). The resulting solid was then filtered and dried under vacuum at 50 °C for 24 h to yield blue needle-shaped crystals.

**2.5. Coating Preparation.** The polymer coating solution was made by dissolving the polymer in 10 mL of a 1:3 toluene/chloroform mixture at a concentration of 190 mg/mL. About 1 mL of the resulting solution was dropped on the metal test coupon prior to being spin-coated at 300 rpm for 3 min (WS-400 Spin Processor, Laurell Technologies, Lansdale, PA). A PANI coating was prepared by dropping 1 mL of a PANI solution (190 mg/mL in NMP) on the steel substrates prior to spin-coating as described above. The PANI-coated steel was vacuum-dried for 36 h at 95 °C.

**2.6. Characterizations and Instrumentation.** XRD analyses of the samples (powder) were acquired by a Bruker D8 Advance X-ray diffractometer (Germany) using Cu K $\alpha$  radiation (30 kV, 20 mA, and  $\lambda$  = 1.54 Å). Data were acquired with 4 s steps of 0.02° in the range of  $2\theta$  = 5°–60°. The ratio between the intensity of the crystalline peaks to the sum of the crystalline and amorphous intensities was used in calculating the percentage crystallinity of the samples. A Bruker Dimension Icon atomic force microscope (AFM) using the PeakForce quantitative Nanoscale Mechanical Characterization Mode (QNM) was used to quantify the surface energy of the rough coated surfaces and to measure the adhesion force of the coated steels. The surface morphology of the coated substrates was acquired with a scan area of 5  $\mu$ m × 5  $\mu$ m. Field emission SEM (FESEM, JEOL 6500F) images were acquired at 5 kV to measure the surface morphologies of the uncoated and coated substrates. Samples were coated with  $\approx$ 15 nm Pt for the FESEM/



**Figure 3.** (A) UV-vis spectra of the various undoped polymers. (B) AFM force–distance curve of PANI, PD1, PD2, and PD3.

EDX analysis. Elemental analysis was performed by the X-max 80 EDX detector (Oxford Instruments) at 20 kV.

FTIR spectra were collected using a diamond ATR instrument (iD7 ATR-FTIR Nicolet iS5, ThermoFisher Scientific). Each spectrum is an average of 400 scans with a nominal resolution of  $4\text{ cm}^{-1}$ . Raman spectra were acquired with a Yvon Horiba Raman spectrometer using a 632 nm laser source in microscope mode. UV-vis spectra of undoped polyaniline analogues and dedoped PANI were acquired with an Agilent Cary 60 spectrometer using a 1 cm quartz cell. The spectra of the polymer in NMP was corrected by subtracting the blank spectrum of NMP. Thermograms of the samples were acquired (TGA Q50 thermogravimetric analyzer, TA Instruments) under a  $\text{N}_2$  flow of 20 mL/min and a heating rate of  $10\text{ }^{\circ}\text{C}/\text{min}$ . Contact angles were measured using a Tantec contact angle micrometer using the half-angle method. The coating thickness was measured by using a digital-readout caliper.

Electrochemical measurements were performed with a Solartron Analytical 1470E potentiostat/galvanostat using a three-electrode cell with a Ag/AgCl (saturated KCl) reference, a platinum auxiliary, and a steel coupon working electrode in 3.5 wt % aqueous NaCl electrolyte. The metal test electrode was mounted vertically with an exposed circular area of  $12.8\text{ cm}^2$ . Potentiodynamic scans were from  $-0.25$  to  $+0.25\text{ V}$  versus Ag/AgCl (saturated KCl) electrode about the open-circuit potential (OCP) at a scan rate of  $0.2\text{ mV s}^{-1}$ . Multistat software (Scribner Associates) was used to acquire and evaluate the data. Electrochemical impedance spectroscopy (EIS) data were acquired from  $100\text{ mHz}$  to  $60\text{ kHz}$  with a  $10\text{ mV}$  AC signal about the OCP using a Solartron SI 1250 frequency response analyzer. Impedance data were fitted to equivalent circuits with ZView 4.0 (Scribner Associates).

Accelerated corrosion tests were performed by exposing the samples for 24 h to a 6 wt % ferric chloride/0.1 M hydrochloric acid solution at  $40\text{ }^{\circ}\text{C}$  (ASTM G48-11).<sup>36</sup> Weight loss was determined after the sample was rinsed with deionized water and dried in a vacuum oven to a constant weight.

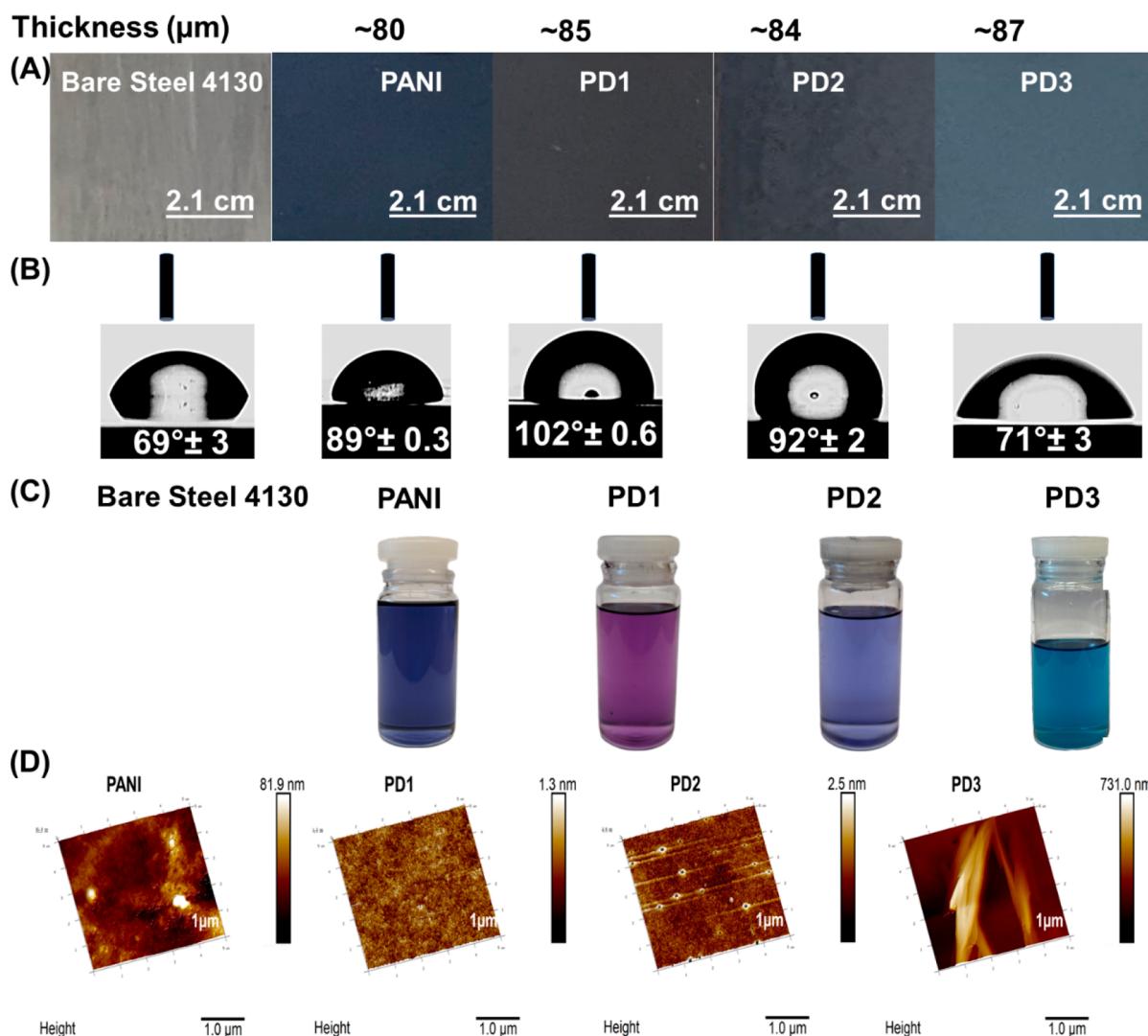
### 3. RESULTS AND DISCUSSION

**3.1. ATR-IR Studies.** ATR-IR spectra of PD1, PD2, PD3, and PANI are shown in Figures 2A and S10–S13. The broad peaks of the PANI spectrum at  $\approx 3116\text{--}3426\text{ cm}^{-1}$  are attributed to stretching vibrations of the secondary amine N–H bond. The peaks at  $\approx 3006\text{--}3093\text{ cm}^{-1}$  are attributed to the stretching of the aromatic C–H bond. The aliphatic C–H stretch is seen at  $\approx 2813\text{--}2929\text{ cm}^{-1}$ .<sup>31,37–40</sup> Peaks at  $\approx 1585$  and  $\approx 1495\text{ cm}^{-1}$  are attributed to the quinoid and benzenoid ring C=C bond stretch, respectively.<sup>29,37,39,41</sup> The C–N stretching vibration is assigned to  $\approx 1217\text{--}1308\text{ cm}^{-1}$ .<sup>32,41</sup>

The band at  $\approx 1103\text{--}1163\text{ cm}^{-1}$  is attributed to –C–H in-plane bending for the 1,4-disubstituted aromatic ring, while the band appearing at  $\approx 829\text{ cm}^{-1}$  can be assigned to the out-of-plane C–H bend in the benzenoid ring.<sup>32,37,39</sup>

Spectra of PD1, PD2, and PD3 can be compared to PANI. The secondary amine N–H bond stretching vibration is present in all the three polyaniline analogues but not very prominent as they are very weak while the aromatic C–H stretching bond is more prominent in PD1, PD2, and PD3 when compared to PANI. The quinoid ring C=C stretching peak near  $1585\text{ cm}^{-1}$  is present in all the polymers.<sup>27,42,43</sup> Other major peaks of PANI are also present in the polyaniline analogues but with lower intensity. The imine (C=N) stretching peak is present in all the polymers at  $1735\text{ cm}^{-1}$  for both PD1 and PD3 and  $1739\text{ cm}^{-1}$  for PANI and PD2, respectively.

**3.2. Raman Spectral Studies.** Figures 2B and S14–S17 show the Raman spectra of PANI, PD1, PD2, and PD3 in the range from  $500$  to  $1700\text{ cm}^{-1}$ . The band at  $1583\text{ cm}^{-1}$  in PANI corresponds to the C=N stretching vibration in the benzenoid ring, which was shifted to  $1624$ ,  $1631$ , and  $1627\text{ cm}^{-1}$  in PD1, PD2, and PD3, respectively.<sup>3,44–46</sup> The intense peak at  $1481\text{ cm}^{-1}$  in PANI can be assigned to a C=C stretching vibration in the quinoid structures. This peak shifts to  $1498$ ,  $1507$ , and  $1496\text{ cm}^{-1}$  in PD1, PD2, and PD3, respectively.<sup>3,45,46</sup> The band of phenazine-like structures is assigned to  $1328\text{ cm}^{-1}$  in PANI,  $1405\text{ cm}^{-1}$  in PD1 and PD3, and  $1407\text{ cm}^{-1}$  in PD2. The band at  $1321\text{ cm}^{-1}$  can be assigned to C–N<sup>+</sup> vibrations of delocalized polaronic structures in PANI. This peak is absent in PD2 and very diminished in PD1 ( $1308\text{ cm}^{-1}$ ).<sup>45</sup> The C–N stretching vibration in PANI is assigned to the band at  $1216\text{ cm}^{-1}$ , and the band at  $1161\text{ cm}^{-1}$  was attributed to C–H bending vibration of quinonoid rings.<sup>45</sup> Both peaks are shifted to longer wavelengths and are much diminished in PD1 to PD3. The alterations in peak positions and intensities indicate the impact of electronic effects (inductive and mesomeric effects) from functional groups, underscoring the intricate interplay influencing the vibrational characteristics of the polymer.<sup>47–49</sup> The peaks at  $840$ ,  $784$ , and  $747\text{ cm}^{-1}$  observed in the PANI spectrum are attributed to benzene-ring deformations of substituted aromatic rings, which includes phenazine-like structures.<sup>44,45,50</sup> These peaks are also present in PD1, PD2, and PD3 but again at longer wavelengths.



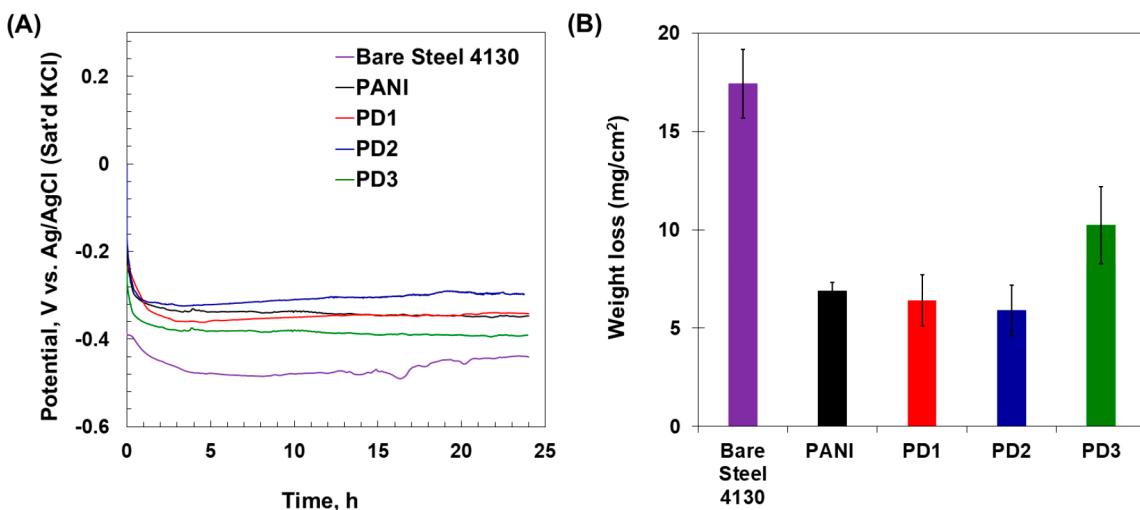
**Figure 4.** (A) Optical images of the uncoated AISI 4130 steel, PANI, and polyaniline analogue coated steels. (B) Static water contact angles of the polyaniline analogues. (C) Images of the polymers when dissolved in chloroform. (D) 3D AFM height images.

**3.3. UV/Vis Spectroscopy.** The UV-vis absorption spectra of PANI and polyaniline analogues (PD1–PD3) in chloroform are shown in Figure 3A. Strong peaks appear at 326 and 597 nm; 311 and 545 nm; 319 and 577 nm; and 333 and 668 nm for PANI, PD1, PD2, and PD3, respectively. The peaks from 311 to 333 nm indicate the  $\pi-\pi^*$  transition in the benzenoid ring of the polymers, while the broad peaks of 545–668 nm for all the polymers have been assigned to the  $n-\pi^*$  transition from the benzenoid ring to the quinoid moiety of the polymers.<sup>27,33,38,40,46</sup> There is a hypsochromic shift in both the  $\pi-\pi^*$  transitions in the benzenoid ring and the  $n-\pi^*$  transition from the benzenoid ring to the quinoid moiety for both PD1 and PD2 when compared to PANI. In contrast, a bathochromic shift is seen for both peaks of PD3 compared to PANI.<sup>27,40</sup>

**3.4. Thermogravimetric Analysis.** Thermograms from thermogravimetric analysis (TGA) of PD1, PD2, PD3, and PANI under  $N_2$  are shown in Figure S1. A small decrease in the weight of PANI below 100 °C is noted and assigned to dehydration and evaporation of absorbed water.<sup>32,41,51</sup> In general, the thermograms in Figure S1 suggest a one-stage weight loss process for all of the polymers except for PANI,

which exhibits a two-step degradation process. PANI has the highest onset of decomposition temperature,  $T_d$ , at 474 °C, followed by PD1 at 438 °C and PD3 at 343 °C. In contrast, PD2 has the lowest  $T_d$  onset at 343 °C. All the polyaniline analogues are thermally stable up to 350 °C. It was suggested in previous reports that the second degradation process of PANI at 600 °C is associated with the breaking of C–N, N–H, aromatic C–H bonds, and carbonization of aromatic rings, resulting in charring.<sup>41,51,52</sup> The thermal stability of the PANI analogues may arise from the rigidity of the fused ring systems in their structure.

**3.5. Visual Images of the Samples and Contact Angle.** Optical images of the uncoated and coated substrates are provided in Figure 4A. In a comparison of the color of the polymer-coated steel with a chloroform solution of the polymer, it is seen that the PD1 coating is dark gray, while magenta color is seen in a chloroform solution (Figure 4C). PD2 coatings are ash colored but are violet in chloroform. PD3 is an ocean blue color as a coating and in an NMP solution. The PD3 film coating is more brittle than the PD1 and PD2 coatings, implying



**Figure 5.** (A) Time-dependent OCP plots after 24 h of immersion in 3.5 wt % NaCl solution. (B) Weight losses of the substrates after 24 h immersion in 40 °C, 6 wt % FeCl<sub>3</sub>/0.1 M HCl solution. The error bar indicates one SD,  $n \geq 3$ .

increased crystallinity. PANI is a dark blue amorphous coating on steel with a similar color when dissolved in NMP.

Thickness is an important factor in the efficiency of a barrier coating.<sup>53</sup> Improved barrier properties and corrosion resistance are found by optimizing coating thickness. The thickness of our coatings is estimated to be in the range 80–87  $\mu\text{m}$ , which is significantly thinner than the  $\approx 150 \mu\text{m}$  thickness typical of protective coatings used in industrial applications and compared well to similar studies.<sup>53–58</sup> Still, some demanding applications could call for thicker coatings. Thin coatings lead to more rapid failure than in a typical application. Contact angle (CA) measurements examined the wettability of the coated steels and the uncoated alloy steel samples (Figure 4B). Uncoated steel samples had a CA of  $69 \pm 3^\circ$ , indicating a hydrophilic surface with a high surface energy. PANI-coated steels show a slightly higher CA of  $89 \pm 0.3^\circ$ ; this increase is likely due to nonpolar aromatic rings in the polyaniline structure. PD1 was the most hydrophobic surface, with a CA value of  $102^\circ$ , again, due to nonpolar aromatic rings and alkyl groups within the matrix of the polymer. PD2 has a contact angle of  $92^\circ$ . While PD3 is hydrophilic with a CA value of  $71^\circ$ , it is likely from polar oxygen functional groups within the polymer. PD1 is a carbazole without the second heteroatom, whereas PD2 and PD3 have S and O in their backbone, respectively.

**3.6. Force–Distance Curve Analysis.** The effect of the surface coating force required to withdraw an AFM (atomic force microscope) tip from our coated substrates is illustrated in Figure 3B. The adhesion force is directly proportional to the surface energy of the coated surface: an increased adhesion force indicates an increased surface energy, which is quantified by AFM.<sup>59,60</sup> Figure 3B shows the force–distance curves when an AFM cantilever tip approaches and retracts from the coated polyaniline (PANI) and polyaniline analogues (PD1, PD2, and PD3) surfaces in air. These curves reveal that PD1 has the lowest maximum adhesion force of  $1.68 \pm 0.03 \text{ nN}$  of PD1 ( $\mu \pm \text{sd}$ ,  $n \geq 3$ ) among the tested PANI analogues. The maximum adhesion forces for PANI, PD2, and PD3 are approximately  $5.69 \pm 0.37$ ,  $4.20 \pm 0.12$ , and  $8.10 \pm 1.49 \text{ nN}$ , respectively. Compared to PANI, the low adhesion forces exhibited by the PD2 and PD3 coatings show that they have a lower surface energy and satisfactory nonstick behavior performance. The excellent result

exhibited by carbazole-based PD1 is likely due to the lack of electronegative atoms able to form hydrogen bonds with water. This result supports the data from the contact angle measurements.

AFM imaging is used to characterize the surface morphology and topography of the coated samples (Figures 4D, S2, and S3). PD3 is distinct in showing a fibrous structure erupting from the surface (Figures 4D, S2, and S3). These features seen in PD3 could be attributed to self-assembly and aggregation of the polymer strands during the synthesis or processing method used to prepare the polymer.<sup>61–63</sup> The AFM images of PD3 show pores in the coating, perhaps due to solvent evaporation during film formation with this polymer. The AFM images show areas that resemble aggregated polymers that formed sheets with heights around 82, 1.3, 2.5, and 731 nm for PANI, PD1, PD2, and PD3, respectively (Figures 4D and S2). Surface roughness ( $R_{\text{RMS}}$ ), average roughness ( $R_a$ ), and the maximum peak depth to height are provided in Table S1. The PD1 sample had the lowest  $R_{\text{RMS}}$  of 0.370, while PD2 has the lowest maximum peak depth of 8.22 nm. PD3 had the largest roughness of all of the coatings.

**3.7. XRD Analysis.** XRD data for PD1, PD2, PD3, and PANI are shown in Figure S4. The  $d$  spacing is found from Bragg's law (eq 1), and the crystallite size ( $D$ ) was determined from the Scherrer equation (eq 2).

$$n\lambda = 2d \sin \theta \quad (1)$$

$$D = \frac{K\lambda}{\beta \cos \theta} \quad (2)$$

where  $\Theta$  is the Bragg angle of the XRD peak,  $\beta$  is the width at half-maximum (FWHM) of crystallite peak (in radians),  $K$  is the shape factor for an average crystallite (0.94) depending on the Miller index of the reflecting plane and the shape of the crystal, and  $\lambda$  is the Cu  $\text{K}\alpha$  wavelength (here 0.154 nm), giving  $D$ , the crystallite size, in nm. The crystallite size of PANI is found to be 1 nm, while those of PD1, PD2, and PD3 are 2 nm each (Table S2). This confirms the formation of PANI nanofibers and nanofibers for the synthesized polyaniline analogues.

The percentage crystallinity in the PANI nanofibers is 17.04%, implying that the undoped polyaniline is mainly amorphous. This agrees with earlier reports that emeraldine base polyaniline

is an amorphous polymer.<sup>32,64–66</sup> The polyaniline analogues are also mainly amorphous polymers with crystallinity ranging from 15% (PD1) to 23% (PD3). The repeating benzenoid and quinoid moieties in these polymers is responsible for their high amorphicity.<sup>32</sup>

The broad diffraction peaks between 5° and 30° seen in all the polyaniline and polyaniline analogues have been attributed to the periodicity parallel and perpendicular to the polyaniline chain in the polymers.<sup>30,32,67</sup> Figure S4 shows the diffracted PANI peaks with their corresponding *d*-spacing at  $2\theta = 9.5953^\circ$  ( $d = 9.2110 \text{ \AA}$ ),  $18.7119^\circ$  ( $d = 4.7383 \text{ \AA}$ ),  $23.4108^\circ$  ( $d = 3.7968 \text{ \AA}$ ), and  $40.2769^\circ$  ( $d = 2.2374 \text{ \AA}$ ), as reported previously.<sup>31,66,68,69</sup> PD1 shows 2 reflections at  $2\theta = 8.2475^\circ$  and  $20.2635^\circ$  with corresponding interplanar distances of  $d = 10.7119$  and  $4.3789 \text{ \AA}$ . Overall, the polyaniline analogues gave similar diffraction patterns to PANI except for PD1 with a significantly lower peak in relation to PANI. Table S2 shows the peak angles and their corresponding *d*-spacings.

**3.8. Electrochemical Measurements/Corrosion Studies.** Results from the OCP, potentiodynamic polarization, and EIS tests are discussed below.

**3.8.1. Open-Circuit Potential Measurements.** Figure 5A shows the variation in open-circuit potential (OCP) during a 24 h period after immersion of the samples in 3.5 wt % NaCl solution. OCP values of the PANI and polyaniline analogues are more positive than the uncoated steels ( $\mu \pm 95\%$  confidence interval,  $n \geq 3$ , and % relative standard deviation RSD  $\leq 5\%$ ).

The potentials at 24 h are  $-442 \pm 6$ ,  $-344 \pm 27$ ,  $-342 \pm 42$ ,  $-326 \pm 30$ , and  $-385 \pm 21$  mV for bare steel 4130, PANI, PD1, PD2, and PD3, respectively. After an initial negative shift, the OCP values stabilized to distinct values, with all the polymers settling to values more positive than bare steel. This positive OCP shift (i.e., in the noble direction) is an indication of a lower corrosion susceptibility. PD2 has the largest shift; at about 116 mV more positive than the uncoated steel substrate. The polyaniline analogues contain cross-linked aryl and alkyl groups within its structure reducing their permeability and rate of electrolyte uptake.<sup>70</sup> Thus, the coatings exhibit a passivation effect, forming a protective layer on the substrates resulting in higher OCP values and high resistance to a corrosive media.<sup>6</sup>

**3.8.2. Tafel Test/Potentiodynamic Polarization Test.** Potentiodynamic polarization testing was done after the 24 h of the OCP experiment to indicate the anticorrosion performance of the samples. Tafel plots—plots of potential against the logarithm of the current density ( $\log J$ ) are shown in Figure 6. The corrosion potential ( $E_{\text{corr}}$ ) and corrosion current ( $I_{\text{corr}}$ )

values are extracted by fitting the Tafel plot to the Butler–Volmer equation.<sup>71</sup> The protection efficiency (PE%) estimates the ability of the coating to minimize corrosion and is calculated from eq 3.

$$\text{PE (\%)} = \frac{I_{\text{corr,uc}} - I_{\text{corr,c}}}{I_{\text{corr,uc}}} \times 100 \quad (3)$$

where  $I_{\text{corr,uc}}$  and  $I_{\text{corr,c}}$  are the corrosion current densities of the uncoated and coated samples. The corrosion parameters extracted from the Tafel plots are given in Table 1.

As expected, the uncoated substrate displays significantly higher cathodic and anodic current values compared to the coated substrates (PD1, PD2, PD3, and PANI). Lower metal corrosion rates are indicated by smaller  $I_{\text{corr}}$  values. Additionally, as in the OCP tests, a more positive  $E_{\text{corr}}$  value implies a smaller corrosion tendency.<sup>72</sup> The  $E_{\text{corr}}$  values of the uncoated substrate are more negative than those of the coated substrates. Organic coatings may not always provide the best barrier against corrosive media, but the diffusion pathways of coatings made of higher density materials or polymers with cross-linked structures are more constrained, resulting in a lower permeability. Higher OCP values and greater tolerance to corrosive environments are outcomes of this lower permeability.<sup>73–75</sup> Further, data from contact angle and AFM adhesion tests show that PANI and PANI analogues possess low surface energy and act as a hydrophobic barrier to diffusion of the corrosive electrolytes across the coating–metal surface. PD2 has the most positive  $E_{\text{corr}}$  at  $-300 \pm 6.6$  mV and the smallest  $I_{\text{corr}}$  value at  $0.129 \pm 0.11 \mu\text{A}/\text{cm}^2$ , giving this material a PE% value of 95.9%—higher than the PANI coating. In contrast, PD3 with an  $I_{\text{corr}}$  value of  $1.656 \pm 0.16 \mu\text{A}/\text{cm}^2$ , and an  $E_{\text{corr}}$  value of  $-343.7 \pm 10.69$  mV has a PE % value of 47.6%, performing well below PANI and the other polyaniline analogue polymers. These results indicate that PD1 and PD2 should perform better than PANI in anticorrosion applications.

**3.9. SEM/EDX Analysis.** Figure 7 shows the morphologies of the samples before and after 24 h exposure to 3.5 wt % NaCl solution. Corresponding EDX spectra are also presented in Figure S5. The EDX spectrum showed peaks for Fe, C, Cr, Al, Si, Ti, and Mn elements present in the bare and coated steel samples. The presence of Fe, C, Cr, and Mn peaks in the EDX spectrum of the coated substrates is due to the ability of the high-energy electron beams to penetrate the coating and interact with the metal surface. Pt is present from the conductive Pt coatings applied to the substrates to avoid charging artifacts during SEM. The EDX spectra of PD2 and PD3 additionally had S and O peaks, respectively, from the polymer composition.

After 24 h exposure to the 3.5% NaCl solution, uncoated steel shows irregular pores with deep cavities on the surface media due to corrosion.<sup>40</sup> Prior to exposure, the surface is smooth, showing only polishing scratches. The EDX spectrum indicates an increase in O on the postexposure sample.

In the coated samples, the ability of polyaniline to reduce corrosion rate is attributed to the interaction of metallic cations with the imine nitrogen atom in PANI, which produces a change in the morphology and structure of PANI.<sup>15,24</sup> This change is evident in the SEM of PANI before and after exposure to NaCl; the initial feathery structures condense to a more cohesive film after exposure. Some delamination of the PANI coating is also noted after immersion in NaCl solution for 24 h. PD1 produces a uniform and very smooth layer on steel surfaces. However, the film typically forms cracks a few days after PD1 coatings were

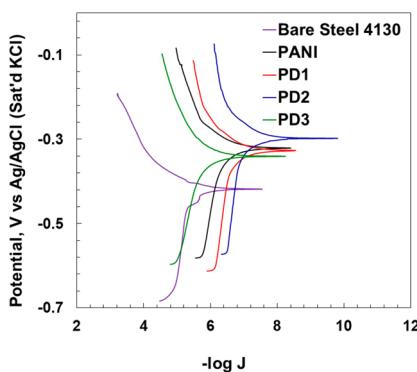


Figure 6. Tafel plot after 24 h of immersion in 3.5 wt % NaCl solution.

Table 1. Corrosion Parameters Extracted from the Tafel Plots

	bare steel	PANI	PD1	PD2	PD3
$I_{corr}$ ( $\mu\text{A}/\text{cm}^2$ )	$3.16 \pm 0.62$	$0.38 \pm 0.17$	$0.35 \pm 0.19$	$0.13 \pm 0.11$	$1.66 \pm 0.16$
$E_{corr}$ (mV vs Ag/AgCl (satd))	$-413 \pm 4$	$-335 \pm 13$	$-338 \pm 17$	$-300 \pm 7$	$-344 \pm 11$
corrosion rate ( $\mu\text{m} / \text{year}$ )	37.5	4.6	4.1	1.5	19.7
protection efficiency (%)		87.8	89.0	95.9	47.6

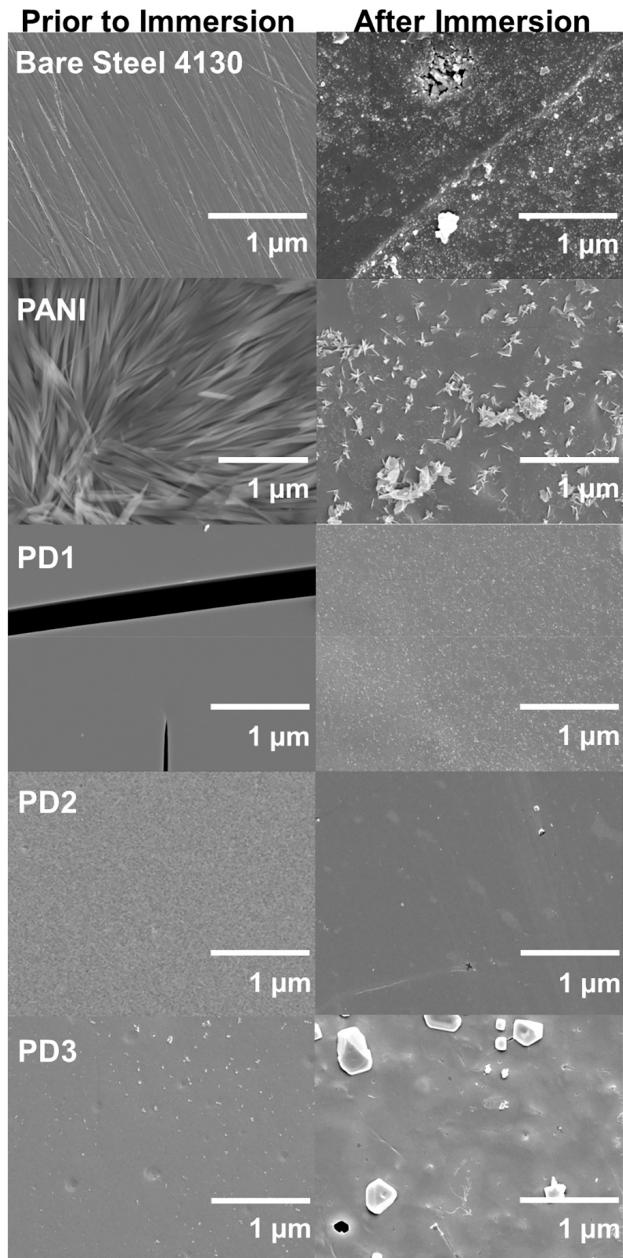


Figure 7. SEM pattern of uncoated steels, PANI, PD1, PD2, and PD3 before and after 24 h of exposure to NaCl solution.

applied, as seen in the SEM. Only a slight roughening of the PD1 surface is noted after exposure to 24 h of NaCl. The coated surface also only showed slight surface changes seen after immersion in NaCl. In contrast, the PD3 surface shows the presence of corrosion products (i.e., lighter particles seen on the surface of the polymer) and pits after exposure. There is also a change in the surface texture of PD3, which can be attributed to the absorption and percolation of water into the coating,

resulting in swelling. The EDX spectrum for PD3, postexposure, shows a large increase in Cl, likely due to the presence of chloride-containing corrosion products.<sup>76</sup> In contrast, PD1 and PD2 coatings show only minimal formation of white corrosion product particles and pits after 24 h in corrosive media.

**3.10. EIS Study.** An EIS study was used to understand the electrochemical behavior and anticorrosion performance of the polyaniline analogues on AISI 4130 steel in 3.5 wt % NaCl solution.<sup>2,33</sup> EIS data were acquired by excitation with a 10 mV rms sine wave over the frequency range of 0.1 Hz–60 kHz. Figures 8A–E show the Nyquist plots (real impedance  $Z'$  vs the imaginary impedance  $Z''$ ) of bare AISI 4130 steel and various coatings. The uncoated steel shows a single depressed semicircle in Figure 8A. The depressed semicircle indicates an imperfect capacitance with a resistive component. The Nyquist plots for PANI, PD1, PD2, and PD3 coated substrates in Figures 8B–E also contain depressed semicircles in the high-frequency region and an incomplete semicircle at low frequency.

A Randles electrical model (Figure 8F, model A) with solution resistance ( $R_s$ ) in series with a parallel constant phase element (CPE<sub>dl</sub>– $T$ ) and charge-transfer resistance  $R_{ct}$  (or polarization resistance  $R_p$ ) element provides a good fit to the bare steel sample. A constant phase element (CPE) is used to model the nonideal behavior of the double-layer capacitor.<sup>2,77</sup> The impedance of the CPE is

$$Z_{CPE} = \frac{1}{(2j\pi f)^n Y_0} \quad (4)$$

where  $Y_0$  is the capacitance;  $n$  accounts for the nonideal behavior of the capacitor and ranges from  $n = 1$  (purely capacitive) to 0.<sup>2,23,77,78</sup>

The simple Randles model is inadequate for the coated substrates. Thus, there is a need to account for the heterogeneity of the protective coating and mass transfer processes producing time constant variations and other deviations.<sup>2,28,53,79–81</sup> The two electrochemical interphases that exist between the substrate surface and the electrolyte solution were accounted for by model B in Figure 8F. The charge transfer at the interphase between the metal and the coat is represented by  $R_{ct}$ –(CPE<sub>dl</sub>– $T$ ), while the coating interphase is accounted for by  $R_c$ –(CPE<sub>c</sub>– $T$ ). The model thus accounts for the two-time constants observed in the experimental Bode magnitude ( $\log |Z|$  vs  $\log f$ ) and phase angle ( $\theta$  vs  $\log f$ ) plots for the bare steel and the coated steels which are displayed in Figure S6.<sup>53,76,81</sup> The region above 1 kHz in the Bode magnitude and the phase angle plots gives the coating barrier performance, while the formation of corrosion products, due to failure of the barrier coatings, is indicated below 1 kHz.<sup>28,53,82,83</sup>

Electrochemical parameters from fitting the EIS data to the models are listed in Table 2. Note that  $R_s$  for the bare steel was  $19 \pm 0.56 \Omega \text{ cm}^2$ , which was much lower than the other samples, reflecting an increase in ion concentration in solution as the metal corrodes. At low frequencies, the impedance modulus ( $|Z|$ ) for bare steel is  $141.7 \pm 1.1 \Omega \text{ cm}^2$ , which is very small. The bare steel exhibited a single time constant below 10 Hz, arising

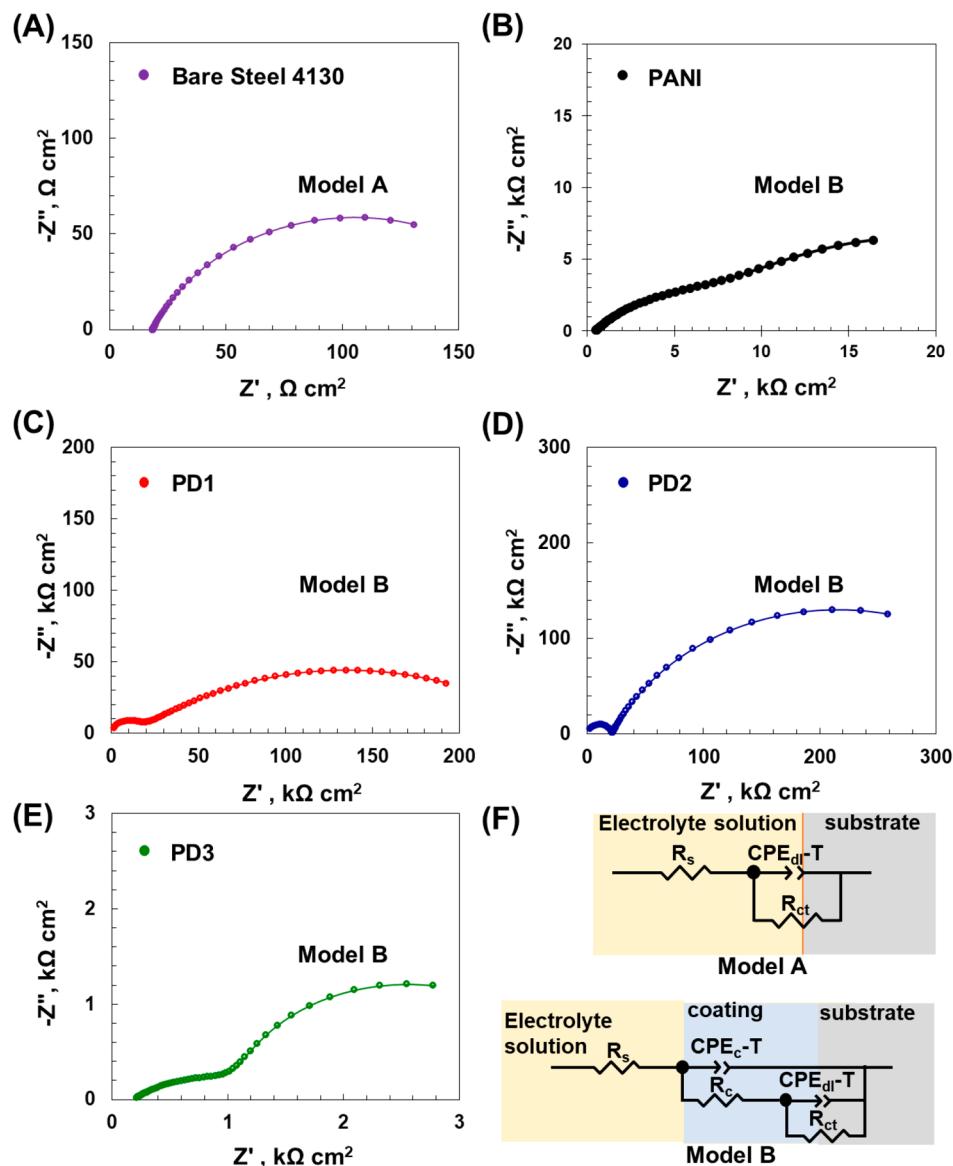


Figure 8. Nyquist plots for (A) bare steel 4130, (B) PANI, (C) PD1, (D) PD2, and (E) PD3 and (F) equivalent electrical circuit (EEC) models.

Table 2. EIS Parameter Values Obtained from Fitting the EIS Data of the Uncoated and Coated Substrates after 24 h Immersion in 3.5 wt % NaCl Solution

	bare steel 4130	PANI	PD1	PD2	PD3
$R_s$ ( $\Omega$ cm $^2$ )	$19 \pm 0.6$	$450 \pm 6$	$550 \pm 20$	$570 \pm 10$	$190 \pm 4$
$CPE_c-T$					
$Y_0$ ( $\mu\Omega^{-1}$ s $^n$ cm $^{-2}$ )		$14 \pm 1.3$	$(7.2 \pm 0.5) \times 10^{-4}$	$(6.3 \pm 0.9) \times 10^{-4}$	$108 \pm 4$
$n$		$0.55 \pm 0.01$	$0.99 \pm 0.01$	$0.97 \pm 0.01$	$0.43 \pm 0.01$
$R_c$ (k $\Omega$ cm $^2$ )		$11.0 \pm 0.9$	$15.0 \pm 0.4$	$21 \pm 2.1$	$1.3 \pm 0.04$
$CPE_{dl-T}$					
$Y_0$ (m $\Omega^{-1}$ s $^n$ cm $^{-2}$ )	$4.7 \pm 0.46$	$(6.8 \pm 0.09) \times 10^{-2}$	$(1.9 \pm 0.5) \times 10^{-2}$	$(2.3 \pm 0.5) \times 10^{-3}$	$0.24 \pm 0.01$
$n$	$0.75 \pm 0.01$	$0.63 \pm 0.01$	$0.45 \pm 0.02$	$0.75 \pm 0.01$	$0.93 \pm 0.02$
$R_{ct}$ (k $\Omega$ cm $^2$ )	$0.17 \pm 0.01$	$20 \pm 2.2$	$240 \pm 49$	$390 \pm 38$	$3.3 \pm 0.19$
$\chi^2$	$2.4 \times 10^{-4}$	$1.5 \times 10^{-3}$	$8.3 \times 10^{-4}$	$2.7 \times 10^{-4}$	$2.6 \times 10^{-3}$

from the formed metallic oxide layer. The polymer-coated samples show much higher  $R_s$ , indicating a small increase in the number of ions present in the electrolyte solution due to corrosion. The parallel combination of  $R_{ct}$  and  $CPE_{dl-T}$ , which models the electrochemical reaction occurring at the coating–

metal interface in model B, estimates the electron transfer rate between the coatings and the metal. A lower  $R_{ct}$  value implies a high electron transfer rate.<sup>2</sup> The  $R_{ct}$  value for the bare steel was  $0.17 \pm 0.01$  k $\Omega$  cm $^2$  while higher values of  $20 \pm 2.2$ ,  $240 \pm 49$ , and  $390 \pm 38$  k $\Omega$  cm $^2$  were obtained for PANI, PD1, and PD2,

respectively. **PD2** and **PD1** gave a superior barrier performance, with  $|Z|$  values of  $2.9 \pm 0.9$  and  $2.0 \pm 0.3 \text{ M}\Omega \text{ cm}^2$ , respectively, when compared to **PD3** and even **PANI** with a  $|Z|$  value of  $17.6 \pm 6.1 \text{ k}\Omega \text{ cm}^2$ . **PD2** and **PD1** have lower  $\theta$  values of  $-26^\circ$  and  $-10^\circ$ , respectively, at low frequencies, which suggests minimal coating damage. At high frequency, both **PD2** and **PD1** have phase angles of  $-65^\circ$  and  $-68^\circ$ , respectively. This implies that the coatings reduce the corrosion rate of the substrates in the corrosive media. **PD3** has two time constants: one at a mid-frequency due to the protective ability of the polymer and another time constant at low frequency with a  $|Z|$  value of  $3.0 \pm 0.3 \text{ k}\Omega \text{ cm}^2$  with phase angle ( $\theta$ ) =  $-23^\circ$ , indicating minimal coating damage. **PD3** gave low resistance values, indicating poor corrosion protection. Studies have revealed that lower values of  $\text{CPE}_{\text{dl}}\text{-}T$  predict lowered corrosion rates, indicating a reduction in the distribution of electrical charges between the metal–solution interphase, thus delaying the production and dissolution of hydrophilic corrosion products (e.g., hydrated metal oxides and hydroxides).<sup>28,82–84</sup> The  $R_c$  values of the coated samples tracks the  $R_{\text{ct}}$  values. Larger  $R_c$  values can delay the movement of corrosive electrolytes to the metallic substrate. **PD1** and **PD2** display larger  $R_c$  values and lower  $\text{CPE}_c\text{-}T$  values [ $(7.2 \pm 0.5) \times 10^{-4}$  and  $(6.3 \pm 0.9) \times 10^{-4} \mu\Omega^{-1} \text{ s}^\text{n} \text{ cm}^{-2}$ ] when compared to **PD3** and even **PANI**. This is consistent with the lack of major damage and evidently low water absorption in the coatings after exposing the coated substrates to the corrosive media, as noted in the SEM images (Figure 7), where in comparison, the surface texture of **PD3** looks swollen.<sup>77,82</sup> The increase in rigidity from the carbazole and the phenothiazine cores in **PD1** and **PD2** may account for the reduction of porosity—reducing the percolation of ions through the coating.<sup>27,35</sup> The use of these polymers as coating barriers helps to increase the impedance modulus values. In contrast, the low  $R_c$  ( $1.28 \pm 0.04 \text{ k}\Omega \text{ cm}^2$ ) and much higher  $\text{CPE}_c\text{-}T$  ( $108.3 \pm 3.9 \mu\Omega^{-1} \text{ s}^\text{n} \text{ cm}^{-2}$ ) values of **PD3** support water adsorption producing the change in the surface texture of the coating in the SEM image (Figure 7) after being exposed to the corrosive media. This EIS result agrees with the data from the OCP and Tafel experiment where both **PD1** and **PD2** gave a superior performance in comparison to **PANI** and **PD3** coatings.

**3.11. Accelerated Corrosion Test.** An accelerated corrosion test was performed by immersing the coated substrates in an aggressively corrosive solution of 6 wt %  $\text{FeCl}_3$  in 0.1 M HCl at 40 °C to evaluate the robustness of the coatings and their resistance on long-term use in an aggressive electrolyte solution.<sup>36</sup> Figure 5B shows the mass loss of these substrates after 24 h immersion in this solution.

The results support the potentiodynamic, EIS, and SEM/EDX experiments. The high weight loss of  $10.2 \text{ mg cm}^{-2}$  of **PD3** is consistent with the damage seen in the SEM image (Figure 7) after exposure to the less aggressive NaCl solution. The poor performance of **PD3** may be ascribed to hydrolysis of weakly bound O atoms in the phenoxazine-based polyaniline analogue polymers, thus doping the polymer, which initiates damage of the polymer coating, noted by the presence of corrosion products, crevices, and cracks appearing on the coated surface.<sup>53</sup> The lowest weight loss of  $5.9 \text{ mg cm}^{-2}$  in **PD2** may be due to the presence of a C–S bond in the polymer matrix, which makes its bond less polar compared to the C–O bonds in the phenoxazine polymer. These phenothiazine-based polyaniline analogues display superior barrier property as it delays corrosion of the substrates.

## 4. CONCLUSIONS

Our initial study of polyaniline analogues as corrosion-protection coatings has demonstrated that they offer a noticeable enhancement of corrosion protection for AISI 4130 steel in 3.5 wt % NaCl. The phenothiazine and carbazole based polyaniline analogues performed nearly as well as the commercial polymer **PANI** with this initial corrosion testing. The carbazole and phenothiazine (**PD1** and **PD2**) based polymers are good hydrophobic barriers to protect metal surfaces from ingress of corrosive media. Based on this investigation, these polymers provide low corrosion rates, high impedance values from the EIS, and very high protection efficiency. Results from the Tafel plot, EIS, SEM/EDS, AFM, and accelerated corrosion test support the observations seen with 24 h immersion times used in related studies.<sup>3,24,40,53,55–58,85,86</sup> The superior performance of corrosion resistance in the carbazole and phenothiazine based polymers might be attributed to the absence of polar functional groups and the presence of nonpolar covalent bonds (e.g., C–C, C–H, and C–S bonds for phenothiazine), which increases hydrophobicity, corrosion resistance, and stability in aggressive media. **PD1** and **PD2** can be used as standalone barrier coatings due to their good adhesion and hydrophobicity. **PD3**, on the other hand, with lower impedance values, can serve as a primer for contributing to enhanced corrosion resistance within a comprehensive paint matrix. All the polymers may also find use as additives to paint primer coatings to enhance corrosion resistance of the paint matrix. **PD1** and **PD2** have the highest corrosion resistance among the tested **PANI** analogues in this study and may prove valuable as an alternative polymeric barrier coating. Further investigation into their suitability will require the production of thinner coatings to match commercial applications. Moreover, we must investigate protection over longer terms with prolonged exposure to corrosive media and accelerated aggressive corrosion testing (e.g., the salt–fog method) to validate this assertion. In addition, enhancement of the protective ability of these polymers will be investigated by adding nanofillers and additives (such as montmorillonite, silica, carbon nanotubes, graphene oxide, titania, etc.), which are likely to act as barriers by increasing tortuosity against electrolyte intrusion, further improving corrosion, adhesion, and mechanical protection. All the **PANI** analogues were studied in their undoped nonconductive state. As with **PANI**, there may be significant advantages to using these polymers in their conducting state, such as particulate additives to paint, epoxy, or primer formulations.<sup>33,87</sup>

## ■ ASSOCIATED CONTENT

### ● Supporting Information

The Supporting Information is available free of charge at <https://pubs.acs.org/doi/10.1021/acsapm.3c02347>.

Thermograms of the polymers; XRD pattern of the polymers; EDX pattern of the bare steel and the uncoated steels; AFM images of coated images; Bode magnitude and phase angle plots of the bare and coated steel; calculation of the equivalent weight of AISI 4130 steel; calculation for corrosion rate from corrosion current;  $^1\text{H}$  NMR spectra of **PD1**, **PD2**, and **PD3**; ATR-IR spectrum of **PD3** (PDF)

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R.F.A.: conceptualization, investigation, data curation, writing—original draft, visualization, writing—review and editing. M.A.: investigation, writing—review and editing. H.G.: investigation, data curation, writing—review and editing. C.N.S.: writing—review and editing supervision, resources. D.O.W.: writing—review and editing, supervision, resources.

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### Notes

The authors declare no competing financial interest.

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