

Sulfite-Activated Ferrate for Water Reuse Applications

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Highlights

- Sulfite-Activated Ferrate is viable option for water reuse treatment
- Activation can lead to improved disinfection, pollutant oxidation, and fewer Br-DBPs
- Activation results in a stable colloidal suspension requiring coagulation
- Br-DBP formation risk exists, especially when activating super stoichiometrically
- Sub-stoichiometric FeSAOP is most effective and efficient, accentuating the role of Fe(IV)/Fe(V)

Abstract

Ferrate is a promising, emerging water treatment technology. However, there has been limited research on the application of Ferrate in a water reuse paradigm. Recent literature has shown that ferrate oxidation of target contaminants could be improved by “activation” with the addition of reductants or acid. This study examined the impact of sulfite-activated Ferrate in laboratory water matrix and spiked municipal wastewater effluents with the goal of transforming organic contaminants of concern (e.g., 1,4-dioxane) and inactivating pathogenic organisms. Additionally, the formation of brominated disinfection byproducts by activated ferrate were examined and a proposed reaction pathway for byproduct formation is presented. In particular,

the relative importance of reaction intermediates is discussed. This represents the first activated ferrate study to examine 1,4-dioxane transformation, disinfection, and brominated byproduct formation. Results presented show that the sub-stoichiometric ($[\text{Sulfite}]:[\text{Ferrate}] = 0.5$) activated ferrate treatment approach can oxidize recalcitrant contaminants by >50%, achieve >4-log inactivation of pathogens, and have relatively limited generation of brominated byproducts. However, stoichiometrically excessive ($[\text{Sulfite}]:[\text{Ferrate}] = 4.0$) activation showed decreased performance with decreased disinfection and increased risk of by-product formation. In general, our results indicate that sub-stoichiometric sulfite-activated ferrate seems a viable alternative technology for various modes of water reuse treatment.

Keywords: Activated ferrate; Water reuse; Advanced oxidation processes; Coagulation; Disinfection.

1. Introduction

Increasing demand for potable water has stressed water systems, accelerating the need for additional sources of water (Brown et al., 2013; Kummu et al., 2016). Secondary wastewater (MWW) effluent is a viable alternative water source (Asano and Levine, 1996; Huertas et al., 2008; Nichols, 1988). Reclaiming MWW, i.e., water reuse, can increase the capacity of water systems and decrease anthropogenic influence on surface waters (Anderson, 2003). However, water reuse also presents risks including associated with organic contaminants of emerging concern (CECs) and pathogenic organisms found in nearly all MWW effluents (Hendricks and Pool, 2012; Jelic et al., 2011; Kasprzyk-Hordern et al., 2009). Failure to remove CECs or inactivate pathogens during water reuse treatment can pose major health risks, regardless of end

use (Gennaccaro et al., 2003; Weber et al., 2006). Furthermore, the presence of effluent organic matter (EfOM), which can be detected even in effectively-treated MWW discharges (Shon et al., 2006), may result in downstream generation of disinfection by-products (DBPs) during reuse disinfection and oxidation processes. Water reuse systems must minimize these potential health risks to safely increase water supply.

As one of the largest global water reuse markets (Lassiter and Gleick, 2015), the state of California Department of Public Health has developed a framework to help mitigate risks from water reuse entitled Title 22 “Regulations Related to Recycled Water” (CA22). Many of the water reuse risks covered in CA22 can be addressed by adding strong oxidants, such as ozone (O_3), chlorine dioxide (ClO_2), or permanganate (MnO_4), to the treatment process. O_3 in particular is a widely deployed strong oxidant in water treatment, and has been shown to mitigate several risks associated with water reuse (Pisarenko et al., 2012). Although O_3 is generally effective, several disadvantages exist such as relatively complex equipment for onsite generation which challenges smaller municipalities that may benefit from water reuse (Daigger, 2009). Furthermore, oxidation with O_3 may result in compounds more toxic than target compounds (Dar et al., 2019), and may produce brominated DBPs if bromine (Br^-) is present in the system influent (Richardson et al., 1999; F. Wang et al., 2014). This is concerning for potential O_3 -based (and other strong-oxidants) water reuse systems in water-scarce, coastal areas (e.g. southern and eastern Mediterranean, southwestern United States) where seawater intrusion leads to higher levels of Br^- in water systems (Barlow and Reichard, 2010; Demirel, 2004; Ged and Boyer, 2014).

High-valent iron species, specifically ferrate ($Fe(VI)$), are viewed as an alternative oxidant to O_3 and other strong oxidants (Jiang et al., 2019; Sharma et al., 2015; Yang et al.,

2013). Fe(VI) also offers associated operational advantages for water reuse systems including flexibility of being produced off-site by commercial Fe(VI) manufacturers as a stable salt (K_2FeO_4) (Monzyk et al., 2013), or generated on-site by an electrochemical method using commonplace water treatment chemicals (Ding et al., 2013; Jiang, 2014). Fe(VI) selectively oxidizes compounds generally considered CECs (Jiang, 2014; Sharma et al., 2016), inorganic contaminants (Goodwill et al., 2016; Virender K. Sharma, 2010), and inactivates pathogens (Daer et al., 2021; Hu et al., 2012; Schink and Waite, 1980). Fe(VI) can be “activated” yielding an advanced oxidation process (AOP) by addition of a reducing agent to generate an unknown combination of Fe(VI)-decay intermediates (i.e., “Fe(IV)/Fe(V)”) and other radical species. The activation process enables greater transformation of recalcitrant CECs without increasing Fe(VI) dose (Sharma et al., 2021). Fe(VI) activation has been demonstrated via addition of various chemical reductants (e.g., thiosulfate), acids (e.g., HCl), UV light, silica gel, or carbon nanotubes (Ghosh et al., 2019; Manoli et al., 2018, 2017b, 2017a; Yang et al., 2021). Sulfite (SO_3^{2-}) has gained attention due to its relatively fast kinetics with Fe(VI) [$k = 10^{12} M^{-2} s^{-1}$] (Johnson and Bernard, 1992) and is proposed to activate Fe(VI) (i.e., “FeSAOP”) in water treatment contexts due to high (>80%) transformation of CECs (Shao et al., 2019; Sun et al., 2018; Zhang et al., 2017). Some existing literature utilized sulfur-containing reductants for activation presumably due to broad acceptance of sulfite in wastewater treatment systems. The FeSAOP mechanism is believed to generate a combination of high-valent ephemeral iron intermediates (Fe(IV)/Fe(V)) plus certain radical species (e.g., $SO_4^{\cdot-}$, $\cdot OH$), likely as a function of $[SO_3^{2-}]:[Fe(VI)]$ (Shao et al., 2020). As $[SO_3^{2-}]:[Fe(VI)]$ increases, so does the amount of $SO_4^{\cdot-}/\cdot OH$ formation relative to Fe(IV)/Fe(V). FeSAOP also changes the size distribution of resultant particles (Bzdyra et al., 2020), although this impact has been relatively under studied.

Even with prior research demonstrating promising Fe(VI)-based (i.e., activated and non-activated) oxidation and disinfection results, there is little research covering FeSAOP in water reuse applications relative to CA22 benchmarks. The overarching objective of this research was to demonstrate that sulfite-activated Fe(VI) (i.e., FeSAOP) can mitigate risks associated with pathogens and CECs, and serve as an appropriate option for water reuse systems. Specific aims were to: (1) assess oxidation performance on a relatively recalcitrant CEC specified by CA22, 1,4-Dioxane (14D), in varying water matrices; (2) quantify activation impacts on coagulation mechanisms; (3) evaluated some FeSAOP byproducts, specifically brominated byproducts (Br-DBPs), due to their higher associated health risks (Chu et al., 1982) and elevated formation potential in EfOM (Sirivedhin and Gray, 2005a); and (4) establish suitability as a disinfectant. These represent the novel contributions to advancement of FeSAOP in water reuse systems. Benchmarks for success were based upon the CA22 indirect potable reuse requirements.

2. Materials and methods

2.1. Chemicals and reagents

All chemicals and reagents used were commercially sourced and reagent grade. High purity (>92%), electrochemically generated potassium ferrate (K_2FeO_4) powder was obtained from Element 26 Technology (League City, TX), a commercial supplier of Fe(VI) (Monzyk et al., 2013, US Patent 8.449,756 B2). Reagent grade water (RGW) with resistivity of 18.2 M Ω .cm was generated by a Direct-Q 5 UV Milli-Q water system (MilliporeSigma; Burlington, MA).

2.2. Oxidation experiments

All experiments were performed in triplicate. 1L solutions were prepared of RGW with 5 μ M 14D buffered at pH 8.0 (± 0.1) with either 10mM phosphate or 10 mM tetraborate. Oxidation experiments were performed in 2-L rectangular batch-reactors (PB-900 Programmable Jar Tester, Phipps & Bird). The reactors were rapidly mixed ($G \sim 150 \text{ s}^{-1}$) for 60 s, and dosed with 150 μ M Fe(VI) from a stock solution. Rapid mixing time and intensity was minimized to balance sample homogeneity and 14D volatilization ($H_{14D} = 0.005 \text{ atm}/(\text{mol/L})$). The 10mM Fe(VI) stock solution, prepared immediately before each experiment, was buffered at pH 9.2 with 5mM phosphate/0.3mM tetraborate with the Fe(VI) concentration confirmed spectrophotometrically at 510 nm (Rush et al., 1996). Each trial had a control (i.e., no Fe(VI)), Fe(VI)-alone, and an FeSAOP reaction. The FeSAOP reactors were dosed with SO_3^{2-} 30 seconds after Fe(VI) had been added. SO_3^{2-} was dosed in one sub-stoichiometric and one stoichiometrically excessive activation ratio ($[\text{SO}_3^{2-}]:[\text{Fe(VI)}]$) of either 0.5 or 4.0, respectively, to demonstrate the impact of varying the activation ratio. The $[\text{Fe(VI)}]$ represents the molar Fe(VI) concentration at the time of activation (30 s), not the initial Fe(VI) dose. The solutions were slow mixed ($G \sim 50 \text{ s}^{-1}$) for 60 minutes until $\text{Fe(VI)} < 5 \mu\text{M}$ in each reactor, which was confirmed by the ABTS method (Lee et al., 2005). Samples were passed through a 0.20 μm membrane filter (Whatman, Maidstone, U.K.) placed into 20-mL headspace-free volatile organic analysis vials and stored at $\sim 4^\circ\text{C}$ until analysis. To simulate a water reuse scenario, experiments were repeated using two unchlorinated, filtered (0.45 μm , nylon membrane, Whatman) secondary MWW effluents in place of RGW. Connecticut wastewater (CTWW) was collected at the Mattabassett District Water Pollution Control Facility (Cromwell, CT) and Iowa wastewater (IAWW) was collected at the Ames Water Pollution Control Facility (Ames, IA). Typical effluent water quality is given in Table SI-1. The

CTWW and IAWW samples were each buffered to pH 8.0 (± 0.1) with 10mM tetraborate and contained 7.7 and 4.1 mg/L EfOM, respectively.

2.3. Brominated by-product generation

Solutions of RGW were buffered to pH 7.0 (± 0.1) or 8.0 (± 0.1) with 10mM tetraborate and contained dissolved ($< 0.45 \mu\text{M}$) organic carbon (DOC) concentrations of either 2.2 or 5.1 mg/L (Suwanee River natural organic matter (NOM), RO Distillate, IHSS). Solutions also contained 200 μM Br⁻ intended to represent a worst-case scenario (similar to values tested by Huang et al., 2016 and Jiang et al., 2016). 250mL amber-glass jars (pre-washed with 10% acetone and rinsed with RGW) were filled with 200 mL of solution and sealed with threaded caps during experimentation. Experiments proceeded in the same manner explained in Section 2.2, having Fe(VI) dose of 150 μM and $[\text{SO}_3^{2-}]:[\text{Fe(VI)}]$ of 0, 0.5 and 4.0, each tested in triplicate. Each reaction was allowed to run for 60 minutes, quenched with 2mM hydroxylamine, and then analyzed for Total THMs (i.e., chloroform, bromodichloromethane, dibromochloromethane, and bromoform) (TTHMs) immediately. TTHM experiments were repeated using the same CTWW and IAWW in place of RGW. Bromate was generated by dosing Fe(VI) at 150 μM with $[\text{SO}_3^{2-}]:[\text{Fe(VI)}]$ of 0, 0.5 and 4.0 in solutions of RGW containing 200 μM Br⁻ and buffered at pH 7.0 (± 0.1) or 8.0 (± 0.1) with 1mM tetraborate.

2.4. Analytical and statistical methods

14D analysis was performed using a gas-chromatograph (GC) with a mass-spectrometer detector (QP2010-SE, Shimadzu Corp.; Kyoto, Japan), following EPA 8270-E. The GC contained a 30-m Restek RxiR-624Sil column. Pre-filtered samples were injected and pre-

concentrated with a purge and trap (O-I-Analytical; College Station, TX) according to EPA method 5030-C and similar to those used by M. Sun et al. (2016). Quantification was performed by comparing 14D peak areas directly to the control samples (i.e., no oxidant added). Samples for non-purgeable organic carbon concentrations (DOC and EfOM) were quantified using a TOC-L (Shimadzu Corp.; Kyoto, Japan), calibrated with a potassium hydrogen phthalate standard per Standard Method 5030 (APHA, 2012). TTHMs were quantified using a GC with a surface acoustic wave (SAW) detector (THM-1000, Parker Hannifin Corp.; Huntsville, AL), following the approach of Ahmadi and Wu (2017). The THM instrument was externally calibrated with standards prepared from a 2,000 µg/mL THM-mix reference standard (Restek Corp.; Bellefonte, PA). Bromate was quantified by liquid chromatography-mass spectrometry (LCMS-8060, Shimadzu Corp.; Kyoto, Japan) equipped with an Aquasil C18 column. LCMS-8060 operating conditions followed a method optimized for this instrument in Shimadzu LCMS Application Note number C144 (Jiang et al., 2016; Tanaka and Horiike, 2017). Active bromine (HOBr/OBr⁻) was determined using the Hach DPD Method 8016 (adapted from Standard Method 4500-Cl G, APHA, 2012). Values reported in figures represent the average of experimental replicates with error bars demonstrating two standard deviations (i.e., 95% confidence interval), unless noted otherwise.

2.5. Coagulation and flocculation of EfOM

Coagulation and flocculation processes used similar laboratory-prepared (5.1 mg/L DOC) and IAWW EfOM solutions at pH 7.0 as previously described in section 2.3. Pre-oxidation of EfOM by Fe(VI) and two activation ratios (similar to section 2.3) occurred in covered 600-mL glass beakers and mixed for 30 minutes. Resultant suspensions were then titrated with Nalcolyte

8100 (Nalco Water, Saint Paul, MN) cationic polyquaternary-amine-chloride polymer (specific gravity = 1.16) until suspended particle negative surface charge had been titrated. Polymer was diluted 1:200 immediately before coagulation experiments, and the volume of polymer solution added was always <3% of total volume. Suspended particle surface charge was quantified *in situ* via streaming current (Dentel et al., 1989) using a laboratory charge analyzer (Chemtrac LCA-01, Norcross, GA). Once streaming current values were ~ 0, samples were allowed to flocculate under gentle mixing ($G < 40 \text{ s}^{-1}$) for 30 minutes. Flocs were then counted using the light obscuration method on a PC5000 particle counter (Chemtrac, Norcross, GA) using predefined size-range channels. The range of countable particle diameters was between 2 and 125 μm .

2.6. *E. coli* disinfection and Fe(VI) activation

Escherichia coli K-12 cultures were grown in minimal media (MM) at room temperature (22-23°C) with continuous orbital shaking at 160 rpm and allowed to reach late exponential growth phase (optical density (OD) at 600nm = 0.5-0.6). MM details are described in Text SI-1. Cells were harvested by centrifugation (8000 $\times g$, 2 min), washed twice using 10 mM tetraborate buffer (pH 8.0 $\pm$ 0.1), and subsequently resuspended in 10 mM tetraborate buffer (pH 8.0 $\pm$ 0.1) or MWW (CTWW or IAWW) for disinfection experiments. A 50 mM Fe(VI) stock solution was prepared in 10 mM borate buffer (pH 9.0 $\pm$ 0.1) prior to *E. coli* disinfection experiments and utilized within 5 min of preparation to minimize Fe(VI) auto-decomposition. *E. coli* cell suspensions were dosed with Fe(VI) and aliquots were subsequently withdrawn to quantify Fe(VI) concentrations using the same ABTS method as previously mentioned. After 15 seconds of Fe(VI) addition, cultures were dosed with SO_3^{2-} at $[\text{SO}_3^{2-}]:[\text{Fe(VI)}]$ of 0, 0.2, 0.4, 0.8, and 3.0. The time of SO_3^{2-} activation with respect to Fe(VI) addition was varied by introducing SO_3^{2-}

after 15, 30, 45 and 60 seconds of Fe(VI) addition. For all cell inactivation measurements, *E. coli* cell concentrations were measured at 0 and 60 minutes of exposure by heterotrophic plate counting following Standard Method 9215. Losses in culturable cells was considered inactivation and calculated based on Equation SI-1.

3. Results and discussion

3.1. Dioxane Oxidation

Figure 1A presents the transformation of 14D by 150 μ M Fe(VI) in two different buffers. Results demonstrate limited transformation of 14D by Fe(VI) alone, with < 40% of 14D oxidized. The phosphate-buffered sub-stoichiometric activation experiments yielded the most significant ($p < 0.01$) improvement in transformation, increasing from 33% to 64%. Resultant 14D concentrations under these conditions approach the 0.5-log removal (69%) requirement set under CA22. The transformation of 14D with increasing activation ratio showed no improvement in borate and notably decreased performance in phosphate (< 20% transformation).

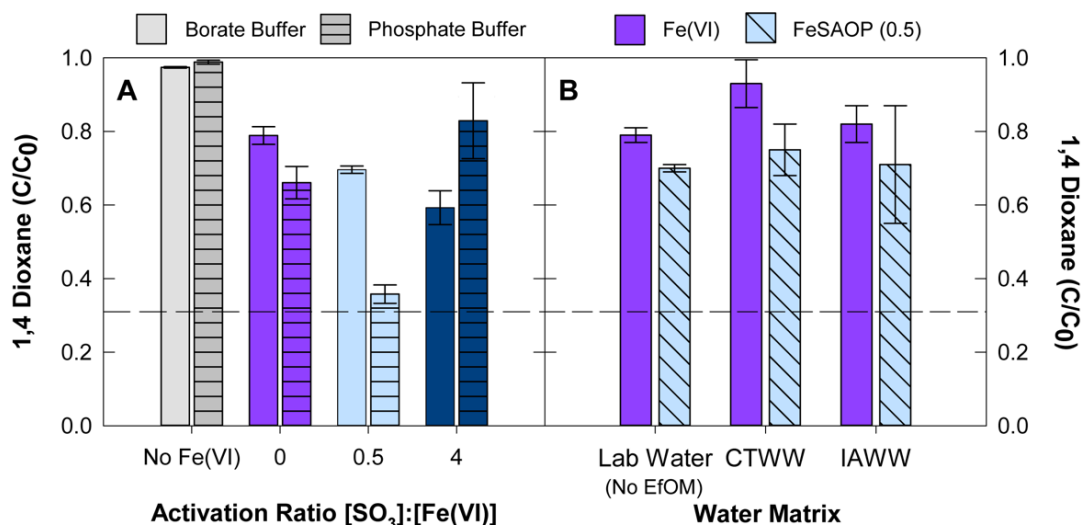


Figure 1: (A) Transformation of 5 μM 14D by 150 μM Fe(VI) at pH 8.0 (± 0.1) in 10mM Borate (solid bars) or 10 mM Phosphate (striped bars) buffer with increasing activation ratio. (B) Transformation of 5 μM 14D by Fe(VI) (solid bars) and FeSAOP (striped bars) in two MWWs, buffered with 10mM Borate at pH 8.0, and compared with RGW (no NOM) performance. FeSAOP [SO₃²⁻]:[Fe(VI)] = 0.5:1. Dashed lines represents oxidation target set by CA22.

The buffer significantly impacted 14D oxidation during activation. Huang et al. (2018) concluded borate-buffered Fe(VI) solutions yielded higher transformation of several CECs compared to phosphate buffered solutions due to nucleophilic complexation of Fe-species by phosphate ligands. However, this phenomenon noted by Huang et al. was not seen in our study where the 0.5 activation in phosphate yielded the highest oxidation, with only ~35% 14D remaining. In borate-buffered experiments both Fe(VI)-alone and 0.5-activation had significantly ($p < 0.02$) decreased oxidation performance compared to the same conditions with phosphate. Improved performance under 0.5 activation could imply 14D is more susceptible to oxidation by ephemeral iron species Fe(V)/Fe(IV) ($E^0 > 1.8$ V, Sharma, 2010) than SO₄^{•-}/•OH ($E^0 \approx 2.5$ V/2.7V, Giannakis et al., 2021) or Fe(VI) alone. The lower oxidation seen in borate buffers is

likely due to the formation of particulate Fe(III), which would have been sequestered in phosphate buffer, accelerating autocatalytic Fe(VI) decay in a way that does not lead to 14D transformation (Jiang et al., 2015). The decreased performance seen in stoichiometrically-excessive activation in phosphate buffer may be associated with the formation of phosphate radicals (e.g., $\text{HPO}_4^{\cdot-}$) during activation. Both $\text{SO}_4^{\cdot-}$ and $\cdot\text{OH}$ react rapidly with buffer HPO_4^{2-} ($k = 10^5$ and $10^6 \text{ M}^{-1}\text{s}^{-1}$, respectively) to form $\text{HPO}_4^{\cdot-}$ (Mártire and Gonzalez, 2001; Maruthamuthu and Neta, 1978) and likely would only have occurred during 4.0 FeSAOP conditions. Phosphate radicals are shorter lived and generally 1-2 orders of magnitude less reactive with organics than $\text{SO}_4^{\cdot-}$ and $\cdot\text{OH}$ at circumneutral pH, implying a decreased oxidative performance (Bosio et al., 2005; Criado et al., 2012; Mártire and Gonzalez, 2001). However, the phosphate buffered experiments hold little practical implications for a water reuse scenario as the buffer phosphate concentration was two orders of magnitude higher than typical MWW influent phosphate concentrations (0.1-0.2mM, Metcalf & Eddy et al., 2013). For this reason, the use of a strong (10mM) phosphate buffer was not utilized in further experiments as the complete sequestration of resulting Fe(III) by phosphate does not offer an accurate representation of a typical water reuse matrix.

The impact on 14D oxidation due to MWW EfOM is presented in Figure 1B. Sub-stoichiometric activation showed no improvement in transformation in IAWW compared to Fe(VI) alone, but significantly improved ($p = 0.02$) oxidation by 18% in CTWW. Transformation was far from meeting CA22 0.5-log transformation goals in all conditions. Dosing Fe(VI) alone in CTWW was less effective compared to lab water, resulting in $< 10\%$ degradation, likely a result of the high EfOM (7.1 mg/L). These results imply that all oxidation conditions are impacted similarly by the presence EfOM and would not be appropriate for pre-oxidation of

certain recalcitrant MWW contaminants. These results agree with prior work suggesting the effectiveness of $\text{SO}_4^{\cdot-}/\cdot\text{OH}$ -based oxidation is impeded in the presence of EfOM, likely due to sorption of target CECs to EfOM (Lian et al., 2017). However, similar impacts from EfOM were also noted with O_3 -based advanced oxidation processes (Pisarenko et al., 2012). Furthermore, EfOM does not impact all contaminants equally. For example, oxidation of Mn(II) by Fe(VI) was shown to be independent of NOM due to the Mn(II)-Fe(VI) reactions rapid kinetics (Goodwill et al., 2016).

3.2. EfOM Coagulation

Figure 2A demonstrates the surface charge neutralization of laboratory Suwannee River NOM and resultant iron particles by cationic polymer in RGW. NOM with no pre-oxidation required 3.1 mg of polymer for complete negative charge titration, as indicated by the streaming current results, while particles after pre-oxidation (all conditions) required greater than 4 mg of polymer. The polymer required for complete titration varied only slightly (4.1-4.3 mg) between the three methods of pre-oxidation. Polymer addition after pre-oxidation is in agreement with prior studies where higher coagulant doses required after Fe(VI) pre-oxidation of NOM, due to the cleaving of large molecules forming smaller hydrophilic molecules (Graham et al., 2010). This phenomenon is not limited to Fe(VI) pre-oxidation, and has been noted with other pre-oxidants (e.g., ozone) (Edwards et al., 1994; Schneider and Tobiasson, 2000). However, significantly higher (~1.5 to 3x) doses of polymer were required to obtain the point of zero charge in MWW EfOM samples (Figure 2B). Converse to results in the lab water matrix, EfOM absent of pre-oxidation demanded a higher polymer dose at 7.3 mg while the Fe(VI) pre-oxidation required the lowest coagulant dose of 5.9 mg to achieve complete surface charge neutralization. EfOM and Fe(VI) resultant particles after FeSAOP pre-oxidation were less

conductive to charge destabilization compared to Fe(VI) oxidation, similar to previously reported charge titrations (Bzdyra et al., 2020). Activation conditions each demanded nearly double the dose of polymer at 11.8 and 12.4 mg for $[\text{SO}_3^{2-}]:[\text{Fe(VI)}]$ 0.5 and 4.0, respectively.

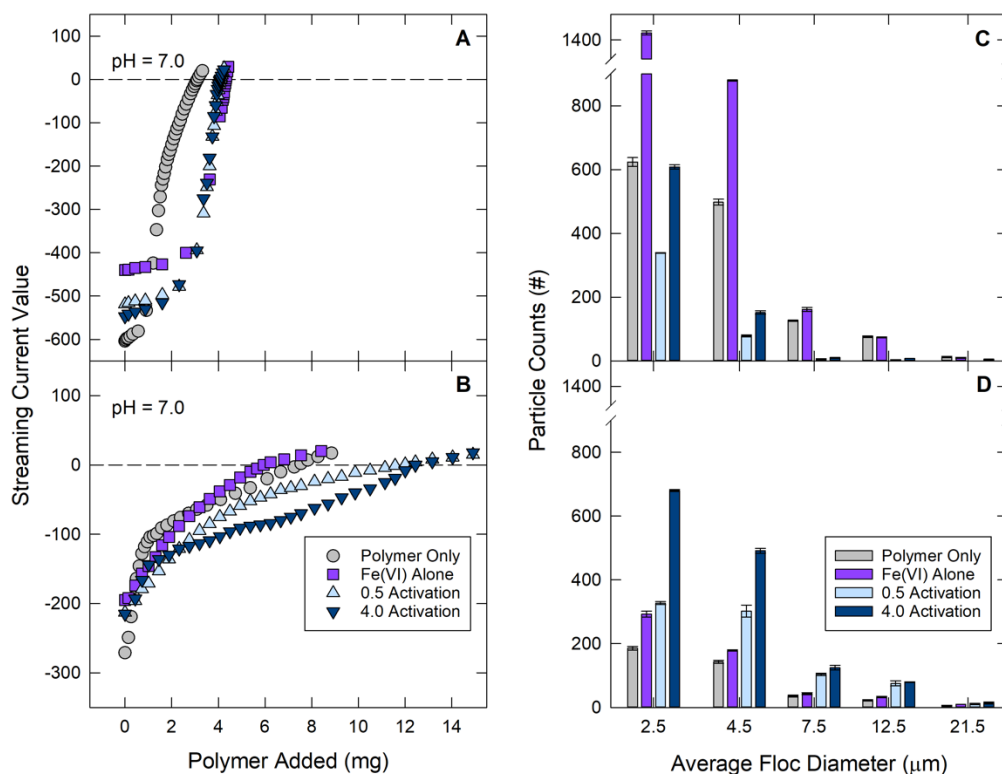


Figure 2: Polymer mass required for particle destabilization of lab NOM (A) and EfOM (B) surface charge in 0.5 L of pH 7 suspensions using cationic polymer with and without pre-oxidation, and the resulting floc size after 30-min for lab NOM (C) and MWW sample (D).

The polymer doses required for neutralization were similar to doses predictions based on the charge densities of the experimental solutions and the polymer. The charge density of the polymer was assumed to be $7.3 \mu\text{eq/mg}$ as previously reported for a quaternary polyamine polymer (Bolto and Gregory, 2007). The lab NOM solution was assumed to have an average charge density of $10.5 \mu\text{eq/mg-DOC}$ based on a previously determined value for Suwanee River NOM (Driver and Perdue, 2015) while the approximate average EfOM density was $25 \mu\text{eq/mg}$

based on a previously reported range for EfOM of 19-31 $\mu\text{eq}/\text{mg}$ (Cho et al., 2000). It was estimated that the lab NOM and MWW, absent of Fe(VI), should require 3.5 and 7.1 mg doses of polymer, respectively. The modeled estimates had good agreement with lab data, having an over estimation by $\sim 10\%$ for lab NOM and only a 3% under estimation for EfOM. The required dose was within 1.0 mg/L of the expected dose. The difference in polymer dose and rate of destabilization between NOM and EfOM (< 5 mg vs > 8 mg polymer, respectively) is likely due to the differing organic matter make ups. Surface water NOM generally contains a high fraction of aromatic compounds (Mao and Schmidt-Rohr, 2004) while anthropogenically-influenced EfOM typically contains more high-carbon aliphatic compounds along with a high fraction of nitrogenated organics (Sirivedhin and Gray, 2005b). The aliphatic and nitrogenous compounds increased the stability of Fe-particles in the EfOM suspension. The coating (i.e., adsorption) of long aliphatic compounds unto Fe-oxides was demonstrated to alter particles electrostatic forces resulting in re-stabilization of Fe-particles (Liang and Morgan, 1990), thus counteracting the addition of polymer. Furthermore, organic nitrogen was shown to be less-emendable to Fe-based coagulation mechanisms (Hu et al., 2016; Pietsch et al., 2001) and requires cationic polymer dosing to destabilize particles complexed with organic nitrogen (Lee and Westerhoff, 2006). Our results show both Fe(VI) alone and FeSAOP pre-oxidation resulted in stable colloidal suspensions requiring further coagulation, regardless of organic matter type, to achieve aggregation. However, all pre-oxidation methods used in a water reuse context (i.e., with EfOM) required a higher polymer dose to achieve complete coagulation, likely due to the functional nature of EfOM complexed with resultant particles.

The size of the resulting coagulated flocs are shown in Figure 2C and D. Generally, all flocs formed had Z-average diameters $< 5.5 \mu\text{m}$ under all conditions. All conditions were absent

of large-diameter (45-125 μm) NOM/EfOM particles before pre-oxidation and coagulation experiments. In RGW EfOM, Fe(VI) pre-oxidation produced the highest concentration of coagulated floc particles and the 0.5 activated resulted in the fewest. RGW EfOM flocs formed absent of Fe(VI) had the largest z-average diameter at 4.5 μm . Meanwhile both FeSAOP samples formed the smallest average floc size at 3.1-3.2 μm . These results are supported by prior work demonstrating FeSAOP results in a more polydisperse size distribution compared Fe(VI) (i.e., non-activated) particles, with FeSAOP particles smaller (and larger) than those generated by Fe(VI) (Bzdyra et al., 2020). These results differ from those obtained in MWW water trials. In MWW, the 4.0 activation resulted in the highest particle counts. The 0.5 activated resultant particles formed flocs with the largest z-average diameter (5.1 μm) while all other conditions resulted in flocs of similar, slightly smaller diameter ($\sim 4.5 \mu\text{m}$). It is important to note that under all pre-oxidation conditions the resulting iron-based flocs (assuming $\rho = 1500 \text{ kg/m}^3$, per Bache and Gregory, 2010) would have sufficient settling velocities ($> 0.75 \text{ m/hr}$) to be removed via sedimentation within a recommended 4-hour settling time (10 State Standards). Remaining unsettlable small particles ($d < 1.0 \mu\text{m}$), likely in higher abundance under activation conditions (Bzdyra et al., 2020), would need to be removed via subsequent dual-media or membrane/ultra-filtration.

3.3. Disinfection performance

The results presented in Figure 3 show the $\log_{10}$ inactivation of *E. coli* by Fe(VI) and FeSAOP. Sub-stoichiometric activation led to notable improvements (28%) to inactivation in buffered RGW, similar to improvements demonstrated in oxidation experiments (i.e., Figure 1). Enhancement in *E. coli* disinfection using FeSAOP is likely due to generation of Fe(V)/Fe(IV)

and $\text{SO}_4^{\cdot-}/\cdot\text{OH}$ (Ghosh et al., 2006; Hu et al., 2012; Manoli et al., 2017a). Elevated inactivation by FeSAOP may be due to limited gene expression (i.e., downregulation) during exposure which differs from more conventional disinfectants (Daer et al., 2021). However, it is noteworthy that stoichiometrically excessive FeSAOP significantly ($p=0.0003$) decreased *E. coli* inactivation by 75% compared to Fe(VI) alone, suggesting Fe(V)/Fe(IV) drive Fe(VI) disinfection. The decreased inactivation may be a result of elevated cellular upregulation of oxidative-stress response genes when exposed to $\text{SO}_4^{\cdot-}/\cdot\text{OH}$ that is not seen when exposed to Fe(V)/Fe(IV) (Daer et al., 2021) in addition to no contact time with ephemeral iron species. Kazama (1994) showed that the addition of sodium thiosulfate with Fe(VI) led to a similar decrease in disinfection capacity of Fe(VI) against F-specific RNA coliphage(Q β), likely due to quenching of disinfecting Fe(V)/Fe(IV) by the excess reductants. The average *E. coli* log inactivation by Fe(VI) alone in IAWW and CTWW was 6.2 ± 0.4 and 7.7 ± 0.2 , respectively, two orders of magnitude higher than the average inactivation in RGW. These results are in agreement with Manoli et al. where a 2-log improvement in murine norovirus inactivation by Fe(VI) was also noted in MWW effluent compared to a lab matrix, possibly due to unintentional activation by MWW constituents, such as NH_3 , and subsequent formation of Fe(V)/Fe(IV) (Manoli et al., 2020). Although still higher compared to RGW experiments, use of FeSAOP in IAWW and CTWW resulted in a significant drop in *E. coli* inactivation by 20 and 11%, respectively (Figure 3). Results presented here are dissimilar to from 14D oxidation results, where FeSAOP had slight improvements in MWW, but overall transformation was not better in MWW compared to RGW. Some differences may have resulted from reaction kinetics. Although specific rates were not determined in this study, inactivation of *E. coli* by Fe(VI) is understood to be relatively fast (i.e., minutes, Gilbert et al., 1976), while oxidation of 14D by Fe(VI)-alone appears to be much slower

(e.g., < 20% transformation in RGW after 60 minutes, Figure 1) allowing for quenching by EfOM. Although FeSAOP appears to be a viable option for disinfection in water reuse, further examination, especially on role the Fe(VI)-derived intermediates during disinfection in MWW matrices, is needed to identify active species and their involvement in the FeSAOP-specific disinfection mechanism.

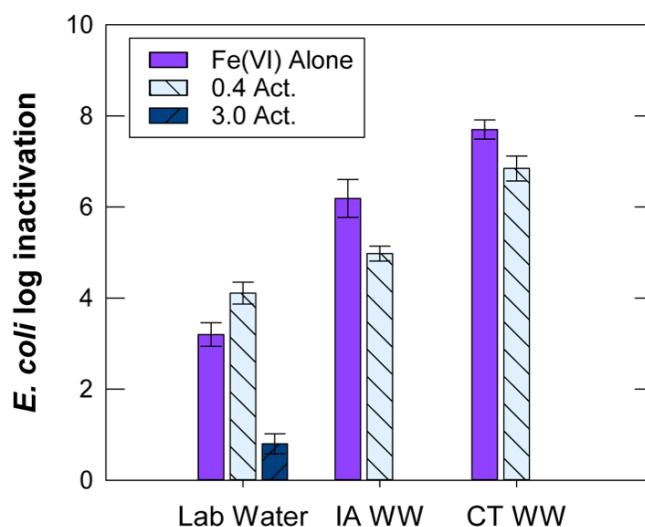


Figure 3: *E. coli* inactivation buffered lab water and MWW at pH 8.0 (± 0.1) at room temperature. Error bars represent 1 standard error of at least three biological replicates. Initial cell concentration $\sim 10^7$ CFU/mL. 3.0 activation was not performed in MWW samples

3.4. DBP Formation

The formation of select Br-DBPs were quantified under various Fe(VI) and FeSAOP oxidation conditions. Figure 4 presents the generation of active bromine (i.e., HOBr/OBr-), a key intermediate of Br-DBP formation, and bromate after Fe(VI) and FeSAOP oxidation. At neutral pH, all oxidation methods produced similar concentrations of active bromine (~ 200 $\mu\text{g/L}$). While activation may have been anticipated to generate more active bromine due to the presence of

Fe(V)/Fe(IV) and $\text{SO}_4^{\cdot-}/\cdot\text{OH}$, slightly faster production of H_2O_2 during FeSAOP (see Figure S1) likely suppressed active bromine formation (Jiang et al., 2016). 4.0 FeSAOP generated more than double the HOBr/OBr^- compared to Fe(VI) alone and 0.5 activation when under more basic conditions (i.e., at pH 8). This observed difference at elevated pH is likely due to an order of magnitude increase in solution OH^- , a precursor for $\cdot\text{OH}$ formation (e.g., OH^- oxidation by $\text{SO}_4^{\cdot-}$ only under 4.0 FeSAOP, Shao et al., 2020). The increased $\cdot\text{OH}$ would have reacted with H_2O_2 more rapidly than HOBr/OBr^- (10^7 vs $10^5 \text{ M}^{-1}\text{s}^{-1}$; Crittenden et al., 1999; Von Gunten and Oliveras, 1997) lowering the level of suppression and increasing HOBr/OBr^- yields. The level of HOBr/OBr^- formed suggests Br-DBP formation is an important consideration when treating elevated Br^- waters with 4.0 FeSAOP. Furthermore, the formation of $\text{Br}\cdot$ during FeSAOP in Br^- rich waters may also have impacts on the degradation of target contaminants (Dar et al., 2020).

All oxidation methods also produced BrO_3 (Figure 4B). Results show experimental conditions produced normalized BrO_3 yields (i.e., $\mu\text{g/L BrO}_3/\mu\text{M Fe(VI)}$) of 0.8 and 0.6 $\mu\text{g/L BrO}_3/\mu\text{M Fe(VI)}$ at pH 7 and 8, respectively. Comparatively, prior work in borate buffer with the same $[\text{Br}^-]_{\text{initial}}$ showed $\text{BrO}_3/\mu\text{M Fe(VI)}$ of 0.9 and 1.5 at pH 6.2 and 7.5, respectively (Jiang et al., 2016). FeSAOP yielded less BrO_3 compared to Fe(VI) at pH 7.0, with 4.0 FeSAOP producing the lowest overall BrO_3 concentrations. BrO_3 yields by FeSAOP trended with pH, consistent with prior radical-based oxidation results where BrO_3 formation increased with pH (Guan et al., 2020; Pinkernell and Von Gunten, 2001). The opposite pH-effect was noted for Fe(VI)-alone where increased BrO_3 formation was observed with decreasing pH, which was also noted in prior studies (Huang et al., 2016; Jiang et al., 2016), likely resulting from the higher reduction potential associated with higher abundance of protonated Fe(VI) species (e.g., $\text{H}_2\text{FeO}_4/\text{HFeO}_4^-$) at relatively lower pH values (Sharma et al., 2016). Formation of elevated BrO_3

is explained by the HOBr/OBr⁻ (a precursor to BrO₃) results previously presented, and due to the high [Br⁻]_{initial} used in this study as BrO₃ formation by Fe(VI) oxidation generally increases proportionately with increasing [Br⁻]_{initial} (Jiang et al., 2016). These results imply that reuse systems treating bromide-containing waters must use caution when implementing FeSAOP, as even with effective EfOM removal the formation of inorganic Br-DBPs remains. Decreasing pH in low-EfOM water may help decrease FeSAOP BrO₃ formation potential in water reuse systems. However, based on results from prior studies comparing Fe(VI) and O₃, yields from FeSAOP would likely be lower than BrO₃ resulting from O₃ under similar conditions (Jiang et al., 2019).

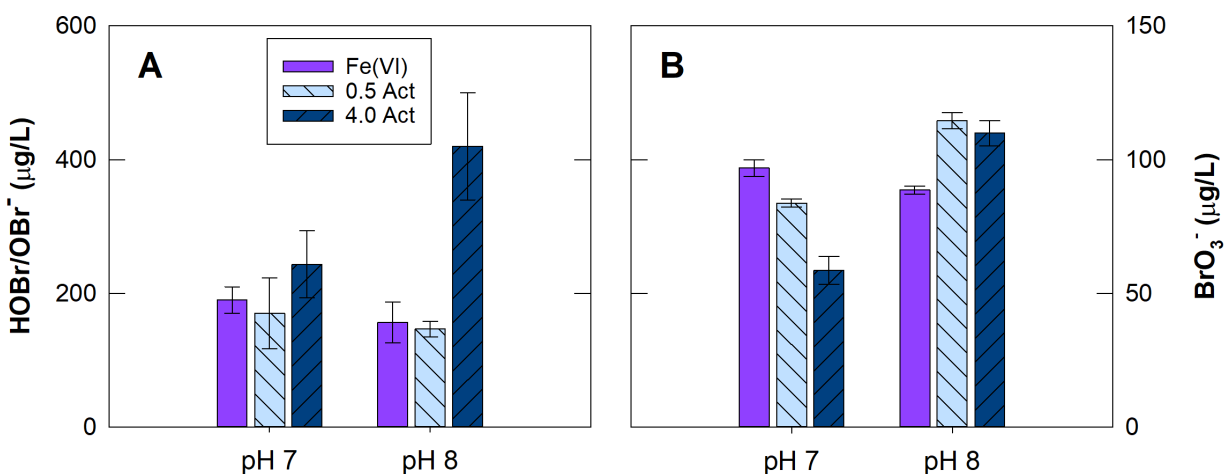


Figure 4: Generation of (A) active Bromine (HOBr/OBr⁻) in 10mM borate buffered RGW absent of NOM and (B) formation of Bromate in 1 mM borate buffer RGW absent of NOM.

The formation of bromoform in RGW with NOM is presented in Figure 5A&B. Under all conditions, bromoform concentrations were below the 80 μg/L Maximum Contaminant Level (MCL) for TTHMs set by CA22 and the U.S. Safe Drinking Water Act. However, chlorine was not present in the system elimination formation of chlorinated THMs. Fe(VI) alone formed < 20 μg/L of bromoform in every test condition. Prior work has shown Fe(VI) pre-oxidation generally

results in similarly low bromoform yields. Work by Huang et al. (2016) yielded only ~1 µg/L bromoform with notably different experimental conditions (e.g., 70% smaller Fe(VI) dose, an order of magnitude lower $[Br^-]_{initial}$, etc.). FeSAOP sub-stoichiometrically at pH 7.0, bromoform yields were significantly ($p < 0.03$) lower when compared to Fe(VI) alone with changes of -39% and -32% in 2.2 and 5.1 mg/L NOM, respectively. This difference is also noted in Figure 4A (active bromine), and is likely a result of active oxidants shifting from Fe(VI) to primarily Fe(V)/Fe(IV) in the sub-stoichiometric FeSAOP mechanism (Shao et al., 2020). However, excess (i.e., 4.0) activation in lower NOM at pH 7 yielded more than double the bromoform concentration compared to Fe(VI) alone, and 3.5 times more than 0.5 activation. This is likely due to increased $SO_4^{\cdot-}/\cdot OH$ generation by 4.0 FeSAOP compared to 0.5 FeSAOP (Shao et al., 2020) that preferentially result in bromoform formation in the presence of low molecular weight carboxylic acids (Y. Wang et al., 2014), which are relatively abundant in the NOM source used in this study (Palma et al., 2021). More than doubling the NOM increased the bromoform generation six-fold (10.7 to 61.4 µg/L) under 4.0 activation at pH 7 (e.g., Figure 5B). There was limited formation (< 6 µg/L) of bromoform at pH 8.0, independent of DOC concentration and activation ratio. Prior studies have shown that bromoform formation by Fe(VI) changes inversely proportional with pH (e.g., bromoform not detected at higher pH by Huang et al., 2016). This is most likely a result of the lower reduction potential of Fe(VI) at elevated pH due to the larger fraction of deprotonated Fe(VI) (e.g., FeO_4^{2-}), which generally reacts slower with target compounds (Jiang et al., 2016; Sharma, 2011). Only FeSAOP 4.0 activation in the

presence of 5 mg/L NOM had significantly different results ($p < 0.01$), with less bromoform resulting compared to Fe(VI).

Bromoform formation was also determined in unchlorinated Br-spiked MWW samples (Figure 5C). Experiments in both real MWW samples yielded less than 10 $\mu\text{g/L}$ of TTHMs. Fe(VI) alone generated only 1.5 and 0.9 $\mu\text{g/L}$ bromoform in CT and IAWW, respectively. These yields are similar ($\sim 1 \mu\text{g/L}$) to those in aforementioned Fe(VI) studies (Huang et al., 2016). Activating at 0.5:1 produced negligible bromoform ($< 1 \mu\text{g/L}$) in either effluent. The higher activation ratio again yielded increased byproduct concentrations, showing 5-6 fold increased formation than Fe(VI) alone. This again is most likely due to shift in radical species during FeSAOP from Fe-based to $\text{SO}_4^{\cdot-}/\cdot\text{OH}$. Although the overall MWW yields were lower, the trend agrees with results in RGW matrix experiments. In general, these results suggest implementation of sub-stoichiometric FeSAOP at $\text{pH} \leq 7.0$ would generate fewer Br-DBPs when compared to other tested oxidation methods and may be most viable conditions for water reuse applications. A proposed reaction pathway for formation of the measured Br-DBPs by FeSAOP radical pre-oxidation in a water reuse context is given in Figure 6. It is important to note that anything exhibiting oxidant demand (e.g., 14D) may alter these proposed reaction pathways and resulting yields of certain DBPs.

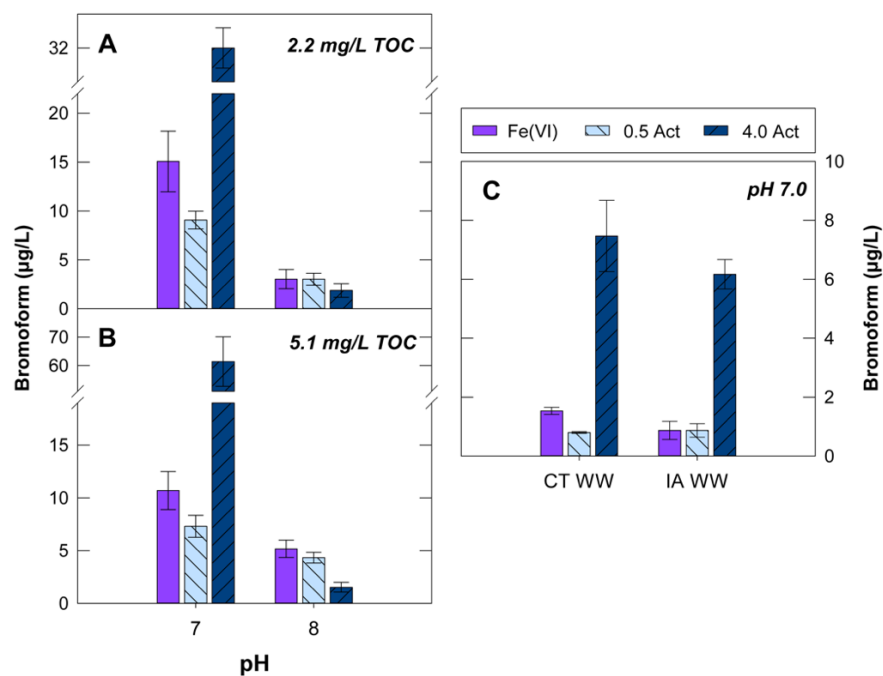


Figure 5: Formation of Bromoform at pH 7.0 and 8.0 (10mM borate buffer) with 2.2 (A) and 5.1 (B) mg/L of IHSS Suwannee River NOM. Bromoform was also quantified in pH 7.0 MWW (C). Other measured THMs (chloroform, bromodichloromethane, dibromochloromethane) accounted for < 2 µg/L in 5C.

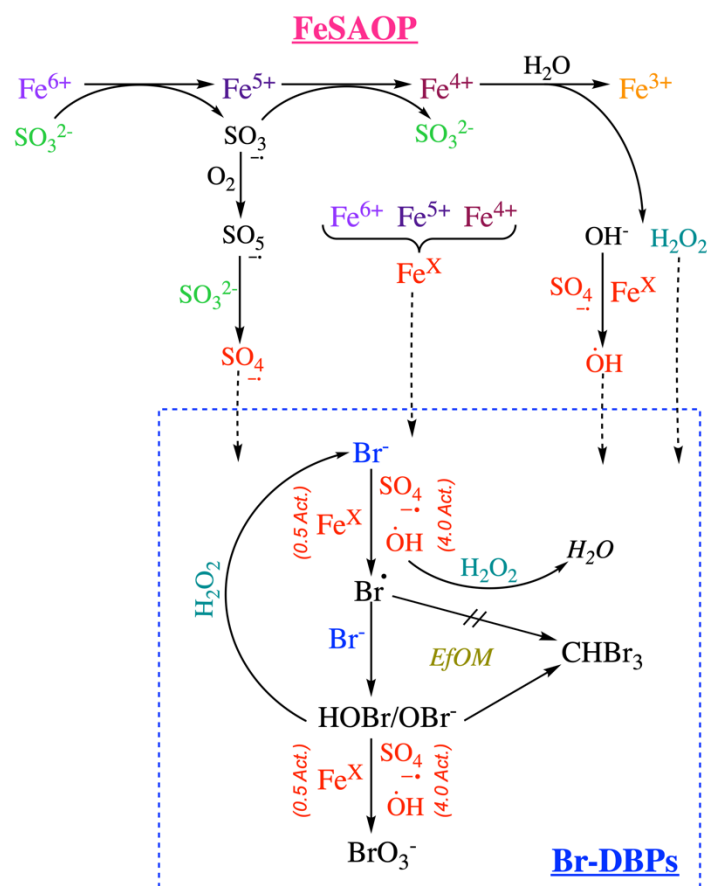


Figure 6: Proposed reaction mechanism for formation of measured Br-DBPs by FeSAOP in a water reuse paradigm

3.5. Implications For Water Reuse

FeSAOP as a water reuse technology that may address several aforementioned risks facing water reuse systems, including needs for inactivation of pathogenic organisms, destruction of residual suspended EfOM, and transformation of numerous CECs. Novel contributions from this study indicate that FeSAOP at [SO₃²⁻]:[Fe(VI)] 0.5 could serve as a feasible alternative technology for some water reuse systems due to the combined mode of action (i.e., ephemeral iron species and radicals) leading to oxidation of recalcitrant CECs, inactivation of pathogens, and decreased direct Br-DBP formation. 0.5 FeSAOP was comparable to, or an improvement

over, Fe(VI)-alone in nearly all experimental trials. Although 4.0 FeSAOP may produce stronger oxidative strength (due to $\text{SO}_4^{\cdot-}/\cdot\text{OH}$) resulting in oxidation of EfOM and certain CECs, it may not be effective against all CECs (e.g., 14D) and does not inactivate pathogenic organisms. Also stoichiometric-excessive activation leads to significantly elevated direct Br-DBP formation. Reuse systems with elevated levels of Br⁻ in raw water should use caution when implementing FeSAOP due to the potential risks of Br-DBPs. Furthermore, stoichiometric-excessive FeSAOP simply acts as a mode for generation of $\text{SO}_4^{\cdot-}$ and $\cdot\text{OH}$ which several existing technologies also accomplish (Giannakis et al., 2021; Miklos et al., 2018), while no existing technology provides the combined mode of action with ephemeral iron species. Rural areas, often most impacted by water scarcity, may especially benefit most from implementation of 0.5 FeSAOP due to certain installation and operational simplicities compared to other technologies such as O_3 (Bauer, 2020) and should be a point of focus in future research. Key remaining knowledge gaps include operational proof of concept through pilot studies.

4. Conclusions

- 0.5 FeSAOP can improve oxidation of a recalcitrant organics compared to Fe(VI) alone and may achieve CA22 benchmarks, but performance is highly dependent on water quality and chemistry (e.g., buffer, EfOM, etc.).
- FeSAOP results in stable colloidal suspensions requiring subsequent coagulation to a great extent than Fe(VI) alone, with FeSAOP requiring double the coagulant dose. However, measured flocs from all oxidating conditions could be removed via sedimentation.

- 0.5 FeSAOP leads to significantly less formation of measured Br-DBPs compared to 4.0 FeSAOP, likely through increased H₂O₂ formation resulting in suppression of HOBr/OBr⁻.
- Sub-stoichiometric Fe(VI) activation results in adequate disinfection, however, inactivation is noticeably decreased at a [SO₃²⁻]:[Fe(VI)] of 4.0, likely from instant quenching of all residual iron species leading to insufficient inactivation contact time.
- 0.5 FeSAOP may be the most advantageous option for water reuse systems, achieving improved transformation of contaminants and comparable disinfection performance to Fe(VI) while limiting direct formation of Br-DBPs.

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Supplementary Information

Sulfite activated Ferrate for Water Reuse Applications

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Table SI-1: Typical MWW Effluent Water Quality obtained from facility records. N/A denotes value was not available in facility records at time of publication.

<u>Parameter</u>	<u>CTWW</u>	<u>IAWW</u>
Facility Name	Mattabassett District Water Pollution Control Facility	Ames Water Pollution Control facility
EPA Facility Look-up ID #	110001404178	110002039918
Flow (x10⁶ gal/day)	24.4	10.1
pH	7.2	N/A
Biochemical Oxygen Demand (mg/L)	2.5	5.6
Total Suspended Solids (mg/L)	2.0	8.4
Nitrate (mg-N/L)	0.02	N/A
Total Phosphorus (mg/L)	0.77	4.7
Fecal Coliforms (#/100 mL)	2.7	N/A

Text SI-1: Additional Disinfection Methods

Bacteria media consisted of 0.3 g/L KH_2PO_4 ; 5.0 g/L K_2HPO_4 ; 0.5 g/L NaCl ; 1.0 g/L $(\text{NH}_4)_2\text{SO}_4$; 0.12 g/L $\text{MgSO}_4 \cdot 7\text{H}_2\text{O}$; 0.02 g/L $\text{CaCl}_2 \cdot 2\text{H}_2\text{O}$; 1.36 mg/L $\text{FeSO}_4 \cdot 7\text{H}_2\text{O}$; 0.24 mg/L $\text{NaMoO}_4 \cdot 2\text{H}_2\text{O}$; 0.10 mg/L $\text{NiSO}_4 \cdot 6\text{H}_2\text{O}$; 0.27 mg/L ZnCl_2 ; 14.6 mg/L EDTA (pH 8.0 ± 0.1) supplemented with 1 g/L glucose from a 20% (w/v) stock glucose solution.

Log inactivation was calculated by:

$$[\text{Eq. SI-1}] \quad \text{Inactivation} = \log_{10} \left(\frac{N_0}{N} \right)$$

where N_0 and N are *E. coli* cell concentrations (CFU/mL) present initially and following treatment, respectively.

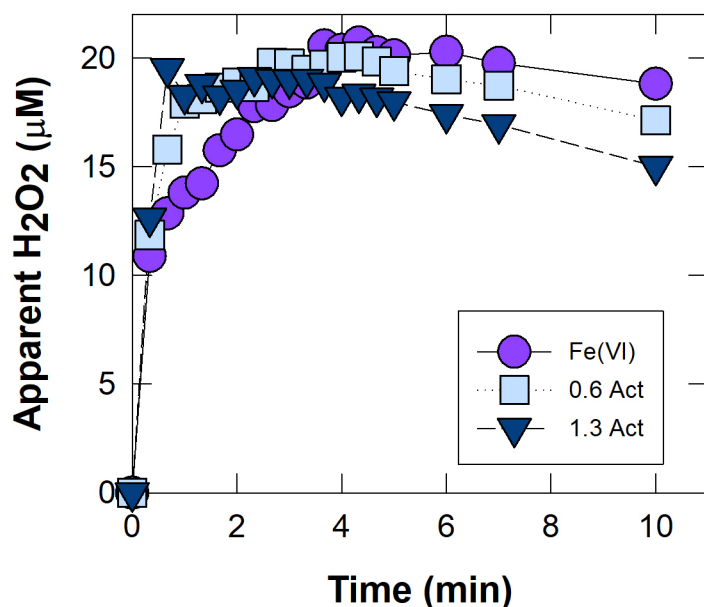


Figure S1: Apparent H_2O_2 formation over time after Fe(VI), 0.6, and 1.3 activation in pH 7.0 RGW, measured using the horseradish-peroxidase ABTS method, as described in Lee et al., 2014.

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