

Dynamic Promotion of the Oxygen Evolution Reaction via Programmable Metal Oxides

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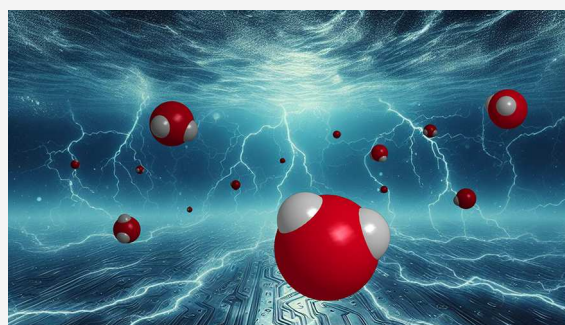


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Supporting Information

ABSTRACT: Hydrogen gas is a promising renewable energy storage medium when produced via water electrolysis, but this process is limited by the sluggish kinetics of the anodic oxygen evolution reaction (OER). Herein, we used a microkinetic model to investigate promoting the OER using programmable oxide catalysts (i.e., forced catalyst dynamics). We found that programmable catalysts could increase current density at a fixed overpotential (100–600× over static rates) or reduce the overpotential required to reach a fixed current density of 10 mA cm⁻² (45–140% reduction vs static). In our kinetic parametrization, the key parameters controlling the quality of the catalytic ratchet were the O*₂-to-OOH* and O*₂-to-OH* activation barriers. Our findings indicate that programmable catalysts may be a viable strategy for accelerating the OER or enabling lower-overpotential operation, but a more accurate kinetic parametrization is required for precise predictions of performance, ratchet quality, and resulting energy efficiency.



Development of carbon-neutral energy sources and energy storage mechanisms is the major challenge of the 21st century required to address climate change. Hydrogen gas is a promising energy storage medium when produced via water electrolysis to store renewable energy in reversibly formed chemical bonds.^{1,2} However, water electrolysis is not yet cost-competitive with fossil-derived H₂.^{3,4} One of the major contributors to the high cost of green H₂ is the slow kinetics of the anodic oxygen evolution reaction (OER), which transforms water into O_{2(g)} via a four electron transfer.^{1,2} Slow kinetics require large overpotentials to achieve industrially relevant current densities ($\eta > 0.5$ V at 0.3–10 A cm⁻²),¹ and state of the art catalysts are comprised of rare and expensive precious metal oxides such as IrO₂.^{4,5}

Despite intensive research efforts over the past two decades, the intrinsic activity of OER catalysts has only modestly improved.^{2,6} Activities are limited by linear free energy relationships (LFERs) that couple the binding energies of the OER intermediates (i.e., O*, OH*, and OOH*) on metals and oxides.^{7–13} Reported for the OER by Nørskov^{9,10} and Koper¹⁴ via density functional theory (DFT) calculations, LFERs constrain catalyst design such that each reaction intermediate cannot be independently stabilized, preventing the design of a catalyst with thermodynamically ideal reaction energies of 1.23 eV/step.

We propose using programmable catalysts (i.e., forced dynamics) as a strategy to accelerate the OER. Programmable

catalysts bypass the limitations conventionally imposed by LFERs by varying the properties of a catalyst during reaction with application of an oscillating stimulus (e.g., light,¹⁵ voltage,^{16–23} ferroelectric polarization,²⁴ etc.) on the time scale of a catalytic turnover.²⁵ Microkinetic models of programmable catalysts applied to both model reactions^{26–29} and ammonia synthesis³⁰ have predicted that reaction rates can be increased by one or more orders of magnitude over a range of applied frequencies. Regarding the OER specifically, switchable ferroelectric polarization has been proposed as a programmable catalyst,^{31,32} but no studies have analyzed the kinetics of promoting the OER via programmable catalysis.

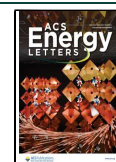
In this work, programmable oxide catalysts were evaluated using a mean-field microkinetic model to assess the viability for accelerating the OER. The model is schematically represented in Figure 1a, and the model equations and computational methods are described in section S1 of the Supporting Information (see SI, Tables S1 and S2 for nomenclature and model parameters). The elementary steps were written based on the acidic Eley–Rideal type adsorbate evolving mechanism

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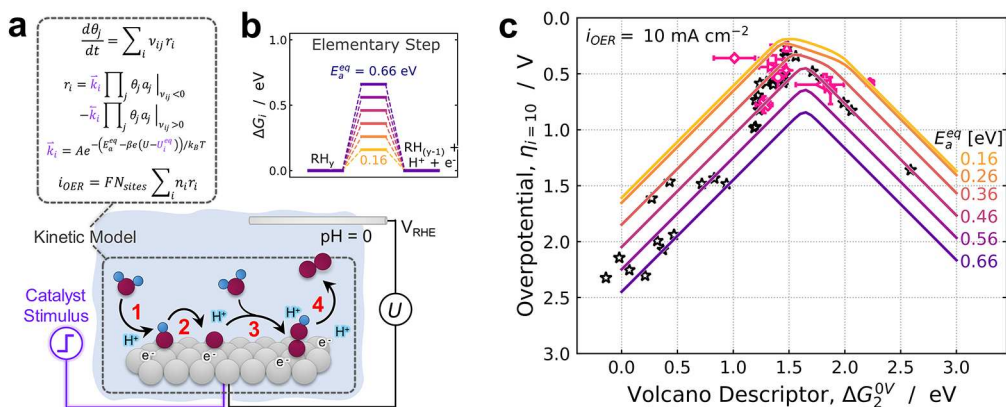


Figure 1. Microkinetic model description. (a) Schematic representation of our microkinetic model of the OER (nomenclature, SI, Table S1). Parameters in purple text are controlled by the catalyst stimulus. Inset (b) illustrates the definition of E_a^{eq} . (c) OER overpotential volcano at a current density of $i_{\text{OER}} = 10 \text{ mA cm}^{-2}$. Solid lines show microkinetic model results as a function of the reversible activation barrier ($E_a^{\text{eq}} \in [0.16, 0.66] \text{ eV}$); black $\star^9$ are theoretical overpotentials predicted via DFT; pink markers^{73–77} are experimentally measured overpotentials in acidic electrolyte (details, SI, Table S7).

(AEM, SI, equations S1–S4), which features four proton-coupled electron transfer (PCET) steps.^{1,9,10} This mechanism has been used in numerous OER modeling studies,^{8,33–36} and there exists supporting experimental evidence.^{37,38} Additionally, recent experiments excluded the meaningful participation of lattice oxygen on IrO_2 ³⁹ and RuO_2 ,^{39,40} providing evidence against alternate mechanisms such as the lattice evolving mechanism (LOM) on those materials. However, we acknowledge that the precise mechanistic details of the OER remain debated.^{37,38,41–44}

For this kinetic study, a continuum descriptor space was needed to model and optimize a generic (*i.e.*, unspecified external stimulus) programmable OER catalyst. However, parameters for both thermodynamic and kinetic scaling relations are currently unknown for this system. Periodic trends of monometallic oxides⁹ were thus used as a first approximation of the thermodynamic scaling behavior of programmable OER catalysts. Following convention, the reaction free energy of step 2 at zero applied potential (ΔG_2^{OV}) was used as the catalyst descriptor.^{2,45} We acknowledge that it is likely that programmable catalysts will feature scaling parameters distinct from those of periodic trends because methods of implementing programmable catalysts change a property of the catalyst rather than the material itself. For example, programmable catalysts based on semiconductor devices tune the electron density, not nuclear composition, of metal,^{16–18} oxide,^{19–21} and transition metal dichalcogenide^{22,46} catalysts. However, the results presented herein provide insights into the design of programmable OER catalysts and motivation for future analyses that will further refine their precise behaviors.

To parametrize the activation barriers of the OER elementary steps, we adopted the strategy used by Nørskov⁴⁷ and Mavrikakis⁴⁸ in which all PCET reactions were assumed to have the same reversible activation barrier (E_a^{eq} , see Figure 1b), independent of catalyst material; the catalyst identity was incorporated into the reaction kinetics through the elementary reversible potential. This strategy was utilized because there is no widely accepted method for calculating electrochemical activation barriers;^{49,50} kinetic information also cannot be simply extracted from Tafel slopes for the OER.^{5,51–53} This leads to large variation in reported activation barriers (SI,

Figures S1–S3) and scant Brønsted–Evans–Polanyi relations for the OER (SI, Table S3).^{54,55} Therefore, E_a^{eq} was treated as an adjustable model parameter and varied between 0.16 and 0.66 eV; these bounds were approximated from a literature review of calculated kinetic barriers for the OER on oxide catalysts (details, SI, section S2 discussion and Tables S4 and S5).^{34,36,54,56–67} The kinetics of the OER were then evaluated using the Butler–Volmer framework with symmetry coefficient β of 0.5 (Figure 1a),^{68,69} and the microkinetic model was solved at differential conversion conditions at pH = 0 in Julia.^{70,71} Mass transport effects were not considered.

To assess the values of the reversible activation barrier (E_a^{eq}) used in the model, simulations were conducted at static (*i.e.*, nonoscillating) conditions to determine the minimum overpotential ($\eta_{i=10}$) required to reach a current density of 10 mA cm^{-2} , a common benchmark value.⁷² Figure 1c depicts these simulated overpotential volcanoes (see SI, Figures S4 and S5 for reaction coordinates, coverages). Markers overlaid on the volcano plot compare both theoretical (black)⁹ and experimental (pink)^{73–77} overpotentials for various oxide catalysts (see SI, Figure S6 for a magnified view near the volcano peak). Models with E_a^{eq} between 0.26 and 0.46 eV returned peak overpotentials ($\eta_{i=10}^{\text{peak}}$) of 229–451 mV (SI, Table S6), which is in the range of experimentally measured overpotentials of highly active OER catalysts in highly acidic electrolyte at this current density (*e.g.*, 220–260 mV for RuO_2 ,^{73,74} 373–458 mV for IrO_2 ,^{73–75} and 468 mV for CoO_x ,⁷⁶ see SI, Table S7). These E_a^{eq} values are also within the range of DFT calculations for AEM steps 3 and 4 on IrO_2 (0.36–0.54 eV and ~0.4–0.5 eV, respectively),^{58,60,63} but lower than reported for step 3 on RuO_2 (~0.6 eV).⁵⁷ In our model, E_a^{eq} of 0.56–0.66 eV returned peaks between 645 and 845 mV, far larger than experimental values; at E_a^{eq} of 0.16 eV, the model underpredicted both theoretical and experimental overpotentials.

During reaction, a programmable catalyst will be held at a constant working electrode potential (*i.e.*, constant overpotential); the application of an *additional* stimulus oscillates the properties of the catalyst and thus surface energetics. This additional stimulus can be a voltage applied to a catalytic condenser^{16–19} or transistor,^{20–22,46} strain,³⁰ ferroelectric polarization,^{24,31,32} *etc.*; this mechanism is not specified in our model. To generate a performance baseline, we simulated

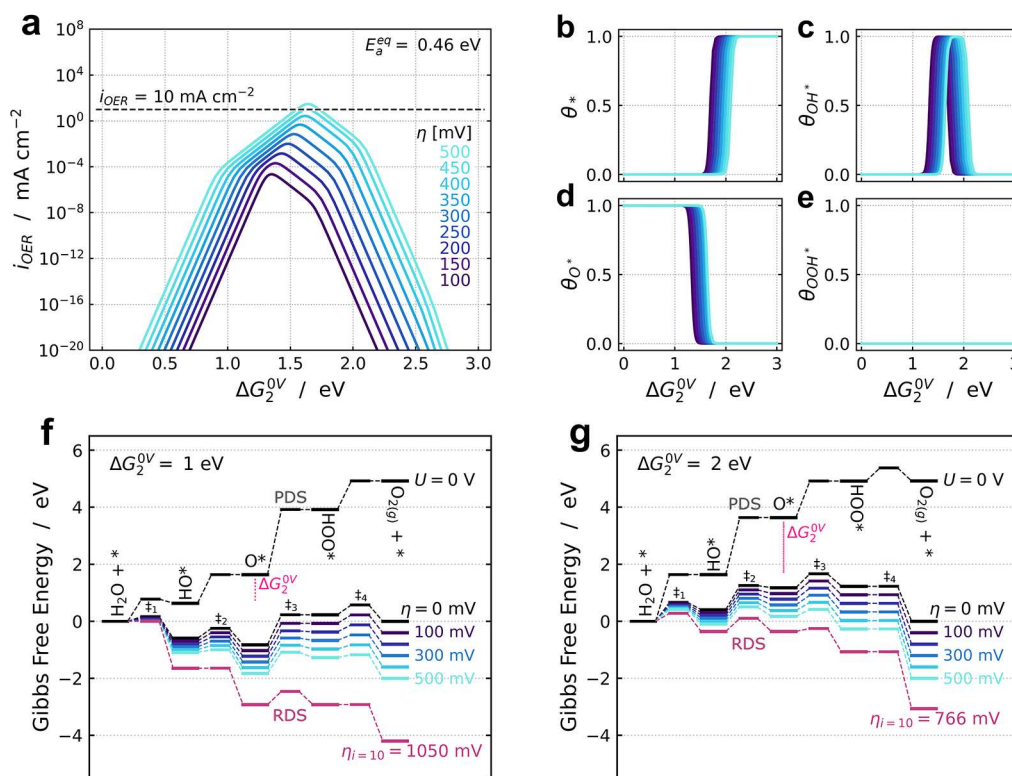


Figure 2. Static OER simulation results. (a) OER current density volcano and (b–e) surface coverages for $E_a^{\text{eq}} = 0.46$ eV at overpotentials $\eta \in [100, 500]$ mV. (f,g) Reaction coordinates at $E_a^{\text{eq}} = 0.46$ eV as a function of the electrochemical potential at $\Delta G_2^{0V} = 1$ and 2 eV, respectively. The black line shows the reaction coordinate at zero applied potential; purple $\rightarrow$ blue lines correspond to the constant-potential simulation results (a–e), and pink to the overpotential volcano (Figure 1c), depicting the reaction coordinate at the minimum overpotential ($\eta_{i=10}$) required to reach $i_{\text{OER}} = 10 \text{ mA cm}^{-2}$. Note that each step involves the transfer of an H^+/e^- pair (not illustrated).

OER current density volcanoes at a constant overpotential for an intermediate E_a^{eq} value of 0.46 eV, which featured close agreement between the model and experimental $\eta_{i=10}^{\text{peak}}$; the results are shown in Figure 2. Each current density volcano has several distinct regions (Figure 2a): to the left of the peak, step 3 (OOH* formation) was the potential determining step (PDS) for all simulated overpotentials (see e.g., Figure 2f) and the surface is covered by O^* (Figure 2d). To the right of the peak, the PDS was step 2 (O^* formation) (see e.g., Figure 2g) and the dominant coverage transitioned from O^* to OH^* to empty sites as ΔG_2^{0V} increased (Figures 2b,c). Step 4 ($\text{O}_{2(\text{g})}$ formation) was essentially barrierless at $\eta > 0$ V across most of the descriptor space, so there was never any appreciable coverage of OOH^* (Figure 2e). A degree of rate control analysis (SI, Figure S7) revealed that the rate-determining step (RDS) at the high- ΔG_2^{0V} side of the volcano was step 2; to the immediate left of the peak, the RDS switched to step 3. While only steps 2 and 3 are considered relevant from a purely thermodynamic viewpoint,⁹ recent studies considering kinetic barriers have proposed that O_2 formation can be rate limiting on IrO_2 ^{41,42,78} and RuO_2 .^{79,80} Our model predicted $X_{\text{RC},4} \sim 1$ at $\Delta G_2^{0V} \lesssim 1$ eV, which is lower than the DFT-calculated ΔG_2^{0V} of IrO_2 (1.3–1.5 eV) and RuO_2 (1.47–1.49 eV). Similar trends were observed for constant-potential simulations at other E_a^{eq} values (SI, Figures S8–S12).

Programmable catalysts were simulated by defining two states between which the catalyst oscillated according to a square waveform with tunable frequency (f), amplitude ($\Delta \Delta G_2$), center point (ΔG_2^{ctr}), and duty cycle (ϕ , fractional time at state 1). All waveform parameters were defined with

respect to the zero applied potential reaction coordinate. One set of rate constants was calculated for each catalyst state, and the programmable catalyst was modeled by switching the rate constants at the specified time points (determined by the waveform frequency and duty cycle) during ODE integration using callbacks in Julia (details, SI section S1).^{70,71} After the model reached a dynamic steady state (i.e., limit cycle), the time-averaged OER current density was calculated by averaging over five oscillations.

We note that oscillation of a working electrode potential has been experimentally demonstrated to accelerate formic acid electro-oxidation rates 20–30 $\times$,^{81,82} improve the Faradaic efficiency of CO_2 electrolysis,^{83,84} and even increase the rate of ethylene hydrogenation (which is not promoted by static potentials) by $\sim 550\%$.⁸⁵ However, it should be emphasized that *oscillating the electrode potential is conceptually distinct from the type of programmable catalyst modeled in this study*.²⁹ When a potential is oscillated to a higher value, all (electrochemical) steps proceed with a larger thermodynamic driving force and lower activation energies (see e.g., the purple $\rightarrow$ blue reaction coordinates in Figure 2f). The low-overpotential state is slower for all steps and, as shown by Holewinski and co-workers, oscillation to this state does not provide any net benefit for Faradaic series reactions.²⁹ Conversely, application of an oscillating stimulus to a programmable catalyst (represented in our model as oscillating the catalyst descriptor) modifies adsorbate energetics nonuniformly. Some steps become more energetically favorable, and others less so (compare e.g., reaction coordinates in Figure 2f,g at $U = 0$ V; the PDS switches from step 3 to step 2, respectively). This biases the

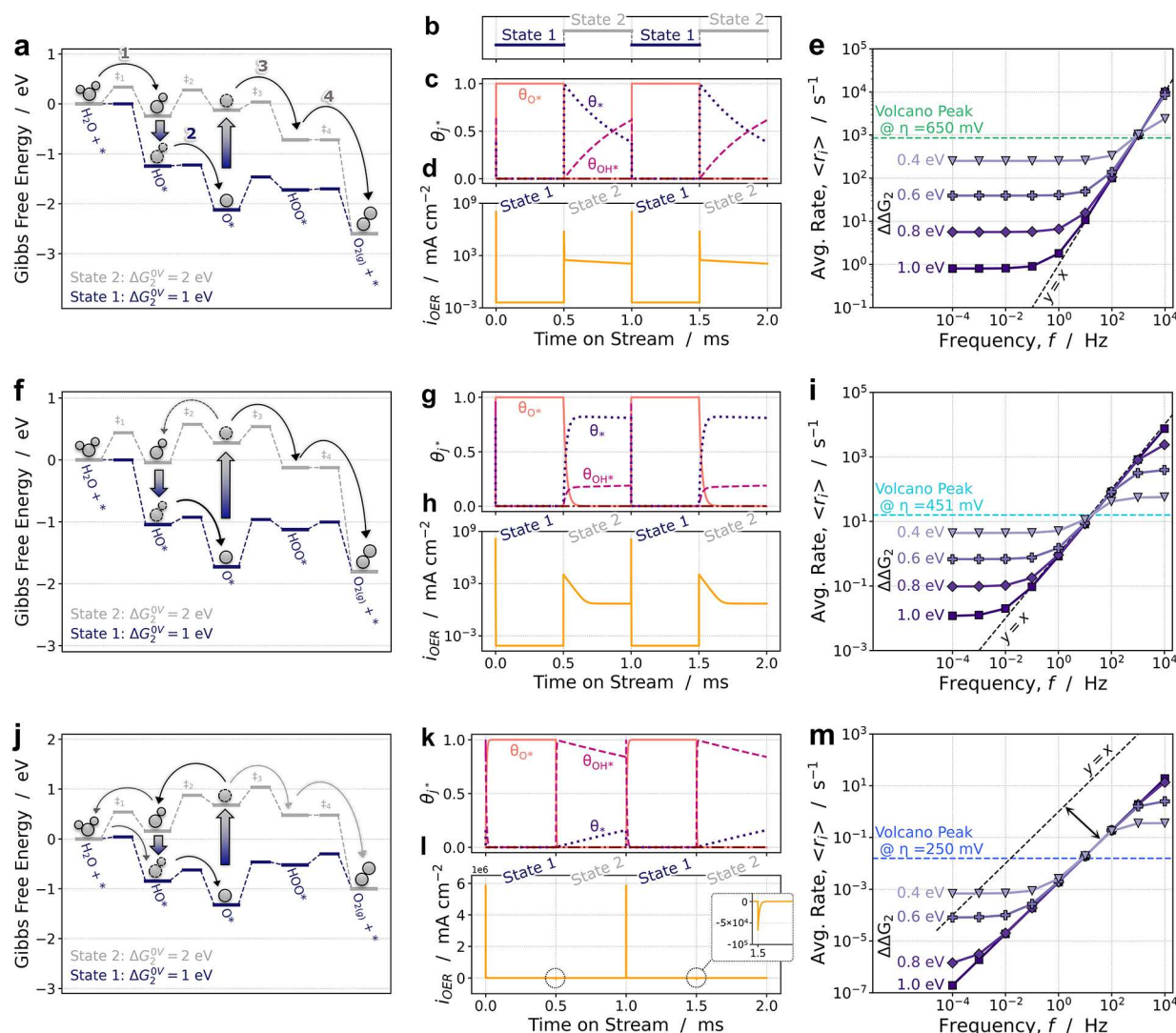


Figure 3. Selected programmable catalyst simulations for $E_a^{\text{eq}} = 0.46$ eV at different overpotentials corresponding to different quality ratchets. All panels have the same waveform parameters (center point $\Delta G_2^{\text{tr}} = 1.5$ eV, duty cycle $\phi = 50\%$, amplitude $\Delta \Delta G_2 = 1$ eV, and frequency $f = 1$ kHz). (a) Reaction coordinate of an “effective” forward ratchet at $\eta = 650$ mV. (b) Catalyst waveform and corresponding (c,d) time on stream data for surface coverages and current density; (e) frequency response plot. The frequency response traces overlap the parity line, indicating there is ~ 1 catalytic turnover per catalyst oscillation, corresponding to an efficient ratchet. (f) Reaction coordinate of an “intermediate” ratchet at $\eta = \eta_{\text{peak}}^{\text{peak}} = 451$ mV; (g,h) time on stream data for surface coverages and current density; (i) frequency response plot. (j) Reaction coordinate of a “reverse” ratchet at $\eta = 250$ mV; (k,l) time on stream data for surface coverages and current density; (m) frequency response plot where traces are far from the parity line, indicating an inefficient programmable catalyst.

reaction coordinate from one state to another, creating a series of local minima and maxima that directionally drive (“ratchet”) molecules from reactant to product.

Figure 3 depicts three examples of programmable catalyst simulations for an intermediate reversible activation barrier (E_a^{eq}) of 0.46 eV, with fixed waveform parameters (center point $\Delta G_2^{\text{tr}} = 1.5$ eV, amplitude $\Delta \Delta G_2 = 1$ eV, frequency $f = 1$ kHz, and duty cycle $\phi = 50\%$). Parts a–e of Figure 3 show the results of a simulation at $\eta = 650$ mV, which yields an effective state 2 forward ratchet for O^* (i.e., O^* prefers to react forward to OOH^* rather than backward to OH^*). The dominant reaction pathway of surface molecules is shown in Figure 3a as the catalyst oscillates between the two states. In state 1 (navy), water dissociates to form OH^* and then O^* , which covers the surface (Figure 3c) because it cannot react further due to the large barrier of step 3. Upon switching the catalyst to state 2

(gray), the majority of surface O^* followed the more kinetically facile pathway to produce $\text{O}_{2(\text{g})}$; this created open sites on the catalyst surface, which were slowly populated with OH^* (Figure 3c). Upon switching back to state 1, the OH^* and any remaining empty sites were rapidly converted to O^* , completing the catalytic cycle. The relative rates of surface coverage changes were determined by the forward activation barriers (Figure 3a): formation of O^* is barrierless in catalyst state 1, while formation of both OH^* and OOH^* in state 2 has small barriers (0.34 and 0.16 eV, respectively). Rapid change in surface coverages was also apparent in the magnitude of the current density spikes that occurred when switching catalyst states (Figure 3d), with the switch from state 2 to state 1 (barrierless O^* formation) featuring the larger spike due to the faster catalytic rate. SI, Figures S13 and S14 depict similar

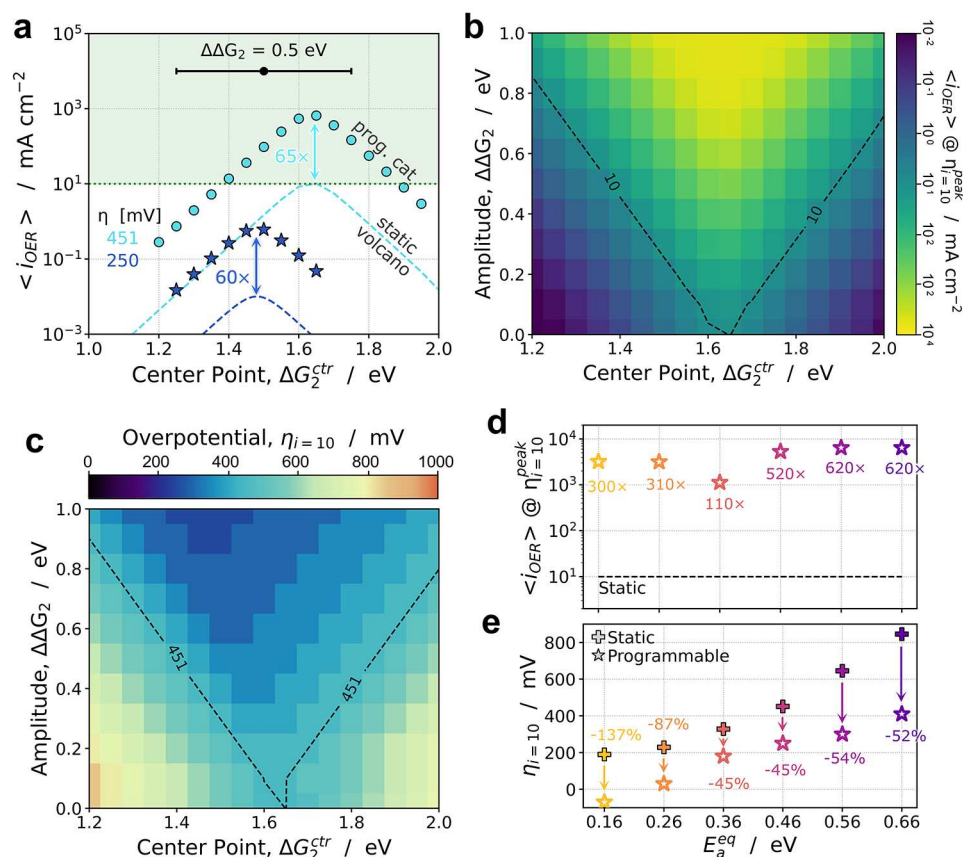


Figure 4. Programmable OER simulation results. Unless noted otherwise, results are shown for $E_a^{\text{eq}} = 0.46$ eV with waveform parameters duty cycle $\phi = 50\%$ and frequency $f = 10$ kHz. (a) Comparison of static (dashed lines) and programmable (markers) OER catalysts at overpotentials η of 250 and 451 mV with waveform amplitude $\Delta\Delta G_2 = 0.5$ eV. At both η values shown, the programmable catalyst achieves current densities $\sim 60\times$ above the corresponding volcano peak. (b) Heatmap showing the current density achieved by a programmable catalyst operating at $\eta_{i=10}^{\text{peak}}$ (451 mV) as a function of waveform center point and amplitude. $\Delta\Delta G_2 = 0$ eV represents static results. (c) Heatmap showing the minimum overpotential ($\eta_{i=10}$) needed to achieve $i_{\text{OER}} = 10$ mA cm $^{-2}$ as a function of waveform center point and amplitude. $\Delta\Delta G_2 = 0$ eV represents static results (see Figure 1c). (d) Maximum current density achieved by optimized programmable catalysts operating at $\eta_{i=10}^{\text{peak}}$ as a function of the reversible activation barrier E_a^{eq} (see SI, Table S8 for corresponding waveform parameters). Numbers represent the enhancement over the static volcano peak. (e) Reduction in $\eta_{i=10}$ by programmable catalysts as a function of the reversible activation barrier E_a^{eq} . Static values correspond to volcano peaks of Figure 1c, and programmable values to optimized waveforms (see SI, Table S9 for corresponding waveform parameters).

time-on-stream results obtained at different waveform frequencies and duty cycles.

The example of Figure 3a–e is characterized as an “effective” forward ratchet due to small forward activation barriers and simultaneously large backward activation barriers. For every catalyst cycle between states ($1 \rightarrow 2 \rightarrow 1$), each site predominately yields one turnover to form the ligand-free $\text{O}_{2(\text{g})}$. This is apparent in the frequency response plot of Figure 3e, which shows the time-averaged catalytic rates (s^{-1}) relative to applied waveform frequency ($\text{Hz} [=] \text{s}^{-1}$) at oscillation amplitudes ($\Delta\Delta G_2$) between 0.4 and 1.0 eV. At $\Delta\Delta G_2 > 0.4$ eV, each trace overlaps with the parity line ($y = x$), indicating an efficient dynamic catalyst of one catalytic turnover per oscillation.

Parts f–i of Figure 3 depict an intermediate quality catalytic ratchet in state 2 (gray), which results from a simulation at $\eta = 451$ mV ($\eta_{i=10}^{\text{peak}}$ for E_a^{eq} of 0.46 eV). As shown in Figure 3f, the forward barrier for O^* -to- OOH^* formation in state 2 (gray) is only slightly smaller than the reverse barrier of the O^* -to- OH^* formation (0.26 vs 0.3 eV, respectively). Thus, as the catalyst switches from state 1 to state 2, a small fraction of the O^* reacts backward to form OH^* instead of following the forward

pathway to produce $\text{O}_{2(\text{g})}$ (Figure 3g,h; see also SI, Figures S15 and S16 for varied f and ϕ). However, the majority of molecules still proceed forward such that frequency response traces (Figure 3i) are comparable to the parity line, indicating that one catalyst oscillation ($1 \rightarrow 2 \rightarrow 1$) still yields about one catalytic turnover.

The third example in Figure 3j–m depicts a reverse O^* ratchet in state 2 for a simulation conducted at $\eta = 250$ mV. Consistent with the prior two examples, the catalyst surface is covered in O^* in state 1 (Figure 3k). However, as depicted in Figure 3j, the kinetically favorable reaction pathway for O^* in state 2 is the reverse reaction pathway from O^* to OH^* (0.2 eV barrier vs 0.36 eV for O^* to OOH^*). When the catalyst switches from state 1 to state 2, the surface coverage of OH^* immediately increases to ~ 1 (Figure 3k); after forming OH^* , the molecules continue along the reverse reaction pathway to produce empty sites. Because most molecules follow the reverse reaction pathway, the current density is negative in state 2 (Figure 3l). For this programmable catalyst, only a small fraction of the O^* molecules react to the OOH^* and follow the forward pathway to the $\text{O}_{2(\text{g})}$. However, because state 1 exhibits strong forward bias (promotes $\text{H}_2\text{O} \rightarrow \text{OH}^* \rightarrow$

O*), the programmable catalyst increased rates $\sim 1200\times$ above the corresponding static volcano peak when oscillated at sufficiently high frequencies (albeit inefficiently, as apparent in Figure 3m). Similar behaviors are observed for programmable catalysts operating at lower amplitudes (SI, Figure S17).

Programmable catalysts were then simulated with different waveform parameters to maximize the OER activity. Simulations were conducted at both $\eta_{i=10}^{\text{peak}}$, corresponding to an intermediate quality ratchet (e.g., Figure 3f–i), and at the minimum overpotential ($\eta_{i=10}$) required to reach 10 mA cm^{-2} , which typically corresponded to a “reverse O*” ratchet (e.g., Figure 3j–m). The key results from these simulations at an intermediate reversible activation barrier (E_a^{eq}) of 0.46 eV are shown in Figure 4a–c. Figure 4a compares static (dashed lines) and programmable (markers) catalyst performance at overpotentials (η) of 250 and 451 mV ($\eta_{i=10}^{\text{peak}}$) for a 50% duty cycle waveform with amplitude $\Delta\Delta G_2 = 0.5 \text{ eV}$ and frequency $f = 10 \text{ kHz}$. At both η values, the programmable catalyst achieved $\sim 60\times$ higher current densities than the respective static volcano maximum. The heatmap of Figure 4b shows the results of simulations at the larger overpotential (451 mV, $\eta_{i=10}^{\text{peak}}$) where the amplitude ($\Delta\Delta G_2$) was varied between 0.1 and 1.0 eV; static results are depicted at $\Delta\Delta G_2 = 0 \text{ eV}$. As $\Delta\Delta G_2$ increased, the current density also increased, as expected. The maximum current density achieved by this programmable catalyst was $\sim 5300 \text{ mA cm}^{-2}$ at $\Delta\Delta G_2 = 1.0 \text{ eV}$, corresponding to a $\sim 520\times$ increase over the static volcano peak.

Next, the ability of programmable catalysts to decrease overpotential was assessed by setting a target current density of 10 mA cm^{-2} and simulating the minimum overpotential ($\eta_{i=10}$) required to reach this target in 50 mV increments. The heatmap of Figure 4c shows the results at a reversible activation barrier (E_a^{eq}) of 0.46 eV as a function of waveform center point (ΔG_2^{ctr}) and amplitude ($\Delta\Delta G_2$) for a 50% duty cycle waveform oscillating at 10 kHz frequency; static results are again shown at $\Delta\Delta G_2 = 0 \text{ eV}$. A minimum $\Delta\Delta G_2$ of 0.3 eV was necessary to outperform the static volcano peak ($\eta_{i=10}^{\text{peak}} = 451 \text{ mV}$). Increasing $\Delta\Delta G_2$ to 0.4 eV further decreased $\eta_{i=10}$ to 350 mV, and at $\Delta\Delta G_2$ of 0.9 eV or higher, a minimum $\eta_{i=10}$ of 250 mV was achieved, corresponding to a 45% decrease from the static $\eta_{i=10}^{\text{peak}}$. Tuning the waveform duty cycle (ϕ) allowed a larger range of ΔG_2^{ctr} to reach the target current density at the minimum $\eta_{i=10}$ of 250 mV (details, SI, section S4.2 discussion, and Figures S18–S20).

Parts d and e of Figure 4 show how the reversible activation barrier (E_a^{eq}) value impacts the simulated performance of programmable catalysts. Figure 4d compares the maximum current densities achieved by optimized programmable catalysts within the bounds of sampled parameters (waveform parameters, SI, Table S8) operating at the respective static volcano peak overpotentials ($\eta_{i=10}^{\text{peak}}$, SI, Table S6). For E_a^{eq} of 0.16–0.26 eV, $\sim 300\times$ enhancement was achieved, corresponding to current densities $\sim 3200 \text{ mA cm}^{-2}$. E_a^{eq} of 0.36 eV returned the lowest performance at only $110\times$ enhancement (1100 mA cm^{-2}), and E_a^{eq} of 0.56–0.66 eV both achieved $620\times$ enhancement ($\sim 6400 \text{ mA cm}^{-2}$). For $E_a^{\text{eq}} \leq 0.26 \text{ eV}$, ratchets are of “intermediate” quality (SI, Figures S21d and S22d). However, barriers are almost nonexistent, resulting in resonance frequencies far above 10 kHz (SI, Figures S21b and S22b). For E_a^{eq} of 0.36 eV, which returned the lowest rate enhancement, the ratchet is a mild “reverse” ratchet (SI, Figure S23d) and resonance frequencies are above 10 kHz (SI, Figure

S23b); this combination hinders rate enhancement. Finally, for E_a^{eq} of 0.46 eV and larger, $\eta_{i=10}^{\text{peak}}$ results in “effective” forward ratchets with relevant forward barriers of $\sim 0.2 \text{ eV}$ (Figure 3f, and SI, Figures S24d, S25d). This leads to these systems experiencing close to maximal performance at the maximum oscillation frequency sampled (i.e., resonance frequencies on the order of 10 kHz, Figure 3i, and SI, Figures S24b and S25b).

Figure 4e compares overpotential-optimized programmable catalysts (waveform parameters, SI, Table S9) to the highest-performing static catalysts. For the most physically representative reversible activation barrier values sampled in this model (E_a^{eq} of 0.26–0.46 eV), $\eta_{i=10}$ of programmable catalysts was 30–250 mV (compare to $\eta_{i=10}^{\text{peak}}$ of 229–451 mV). At the larger end of E_a^{eq} values simulated, reductions of $\sim 50\%$ were achieved, corresponding to $\eta_{i=10}$ values of 300 and 410 mV for E_a^{eq} of 0.56 and 0.66 eV, respectively. For E_a^{eq} of 0.16 eV, the optimized programmable catalyst resulted in $\eta_{i=10}$ of $\sim 70 \text{ mV}$. While this may seem like an error in our model, the overall reaction free energy change does not necessarily dictate the net reaction direction if the reaction coordinate changes with time.⁸⁶ In fact, artificial molecular ratchets have been designed to drive endergonic reactions by coupling to an orthogonal energy source (one which does not impact the reaction coordinate of interest, but instead provides energy to drive the uphill reaction by, e.g., switching between potential energy surfaces with different local minima and maxima to directionally ratchet molecules).^{87–89} Programmable catalysts are an “energy ratchet”⁸⁸ where the work from an external oscillating stimulus enables chemical transformations not possible by conventional methods, such as supra-equilibrium conversion^{27,28} and imparting significant net turnover into a closed catalytic loop.⁹⁰

Kinetic models of prototype chemistries have predicted that optimized programmable catalysts can increase rates by several orders of magnitude^{26–29} while more complex models of ammonia synthesis³⁰ and steam methane reforming²³ predicted modest rate increases of $10\times$ ($f = 2 \text{ kHz}$) and 15% ($f \geq 10 \text{ MHz}$), respectively, for the initial catalyst perturbations modeled. In comparison, our model of the OER predicts approximately $100\text{--}600\times$ rate enhancement at oscillation amplitudes comparable to prototype chemistry models (1 eV), which decreases to $\leq 65\times$ (SI, Figure S26; waveform parameters, SI, Tables S10 and S11) at a lower amplitude of 0.5 eV ($f = 10 \text{ kHz}$). The kinetics in our model are more approximate than those of refs 23, and 30, as we are not modeling a specific stimulus, but our results nonetheless indicate that programmable catalysts may be a viable strategy for accelerating the OER beyond the Sabatier volcano peak.

In this work, microkinetic simulations of programmable OER catalysts were conducted using a simple kinetic parametrization in which all proton-coupled electron transfer (PCET) reaction steps featured the same reversible activation barrier (E_a^{eq}), which was varied between 0.16–0.66 eV. We found that volcano peak overpotentials ($\eta_{i=10}$) predicted by our model at intermediate values of E_a^{eq} (0.26–0.46 eV) featured closest agreement with literature. For this range of E_a^{eq} values, programmable catalyst simulations conducted at the volcano peak overpotential(s) achieved current densities $\sim 100\text{--}500\times$ higher than static, while programmable catalysts simulated at a benchmark current density of 10 mA cm^{-2} were able to operate at 45–90% lower overpotentials than static. Additionally, we found that this kinetic parametrization led to “effective” forward ratchets at high overpotentials, while the ratchets became less effective (even promoting backward

reaction) at low overpotentials. The key parameters controlling ratchet quality were the $\text{O}^*\text{-to-OOH}^*$ and $\text{O}^*\text{-to-OH}^*$ formation barriers at the high ΔG_2^{OV} catalyst state.

This simple kinetic model demonstrated that programmable catalysts are a potentially viable strategy to accelerate the rate of the OER or reduce the overpotential required to reach a specific current density. By accelerating the OER, programmable catalysts may enable the use of cheaper, more abundant catalyst materials. Alternately, programmable thin film IrO_2 -based catalysts may enable commercial PEM electrolyzers to operate at lower catalyst loadings, reducing cost and consumption of this rare precious metal. However, future work improving the parametrization of OER kinetics by replacing the assumed LFERs and single-valued reversible activation barrier is required to enable more accurate predictions of rate enhancement and ratchet quality for the programmable OER. This is requisite for determining the energy efficiency of programmable OER catalysts.

■ ASSOCIATED CONTENT

SI Supporting Information

The Supporting Information is available free of charge at <https://pubs.acs.org/doi/10.1021/acsenergylett.4c00365>.

List of variables; complete microkinetic model equations and computational methods; brief literature review of kinetic scaling relations and barriers reported for the OER; method for estimating bounds of the reversible activation barrier; additional static catalyst simulation results; additional programmable catalyst simulation results; additional refs 91–122 (PDF)

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