



# Hydrodynamic Simulations for Trash Loading in Southern California's Dense Urbanized Watersheds

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**Abstract:** Waterways and water bodies worldwide are impacted by anthropogenic litter (hereafter “litter” or “trash”), generated from nonpoint sources. This study analyzes litter loads across various land uses within two Los Angeles County watersheds: the Ballona Creek and the Los Angeles River. Our objective is to present a methodology to develop buildup and washoff parameters for densely populated urban areas, such as the coastal metropolitan area of Los Angeles, California. An assessment is also made to test how these model parameters perform when applied to another urbanized watershed with similar rainfall and climate patterns (i.e., the San Diego River Watershed in California). Using extensive litter collection data from small drainages (approximately 572 locations, each draining 0.05–8.5 ha), we estimate buildup and washoff model parameters. These parameters are used to simulate the buildup of litter and subsequent washoff (load) of litter in our selected watersheds. Simulated results are validated against observed data from different years in all three watersheds. To date, no study has used litter washoff data to develop these parameters for stormwater models and applied them on a regional scale. We compared linear and nonlinear power functions of litter buildup during interstorm periods. Although there were limited data to develop washoff parameters, an exponential washoff function was used and calibrated to the observed washoff. Generally, storm events with the greatest antecedent dry days had the largest litter loading. Buildup rates varied among land uses, and key calibration parameters included the maximum buildup, buildup rate constant, washoff exponent, and washoff coefficient. A parameter sensitivity analysis was conducted to reveal the washoff exponent as the most sensitive parameter. Annual litter loading estimates were 4.60 kg/ha for the Ballona Creek and 11.50 kg/ha for the Los Angeles River. Litter loading estimates for Ballona Creek were validated and calibrated to align with observed data from the Ballona Creek Trash Interceptor, resulting in an annual washoff load of 2.1 kg/ha. The estimated annual litter loading for the Lower San Diego River was 2.15 kg/ha falling between the mean (0.77 kg/ha) and the maximum (3.56 kg/ha) observed values. When applying model parameters from one watershed to another, models require extensive calibration and validation data, as extrapolating data between watersheds can introduce errors. DOI: [10.1061/JOEEDU.EEENG-7474](https://doi.org/10.1061/JOEEDU.EEENG-7474). This work is made available under the terms of the Creative Commons Attribution 4.0 International license, <https://creativecommons.org/licenses/by/4.0/>.

**Practical Applications:** This research can inform stormwater modelers about the process for developing parameters to estimate water quality in numerical modeling software. We demonstrate how data from field sampling can be directly used to develop model parameters. Results show that with proper validation data, stormwater models can accurately simulate annual litter loads in modeled watersheds. Future studies can test model parameters in other urbanized watersheds to validate the potential for standardized buildup values. Field studies can be done in conjunction with the results from this survey to investigate and further validate litter loads mobilized by stormwater. This study highlights the need for long-term monitoring to improve and update models in the future. Although there is a risk of inaccurate results when extrapolating model parameters from one watershed to another, this research indicates the potential for developing buildup and washoff parameters that can be used as a starting point for parameter selection across urban watersheds.

## Introduction

Aquatic environments are heavily impacted by litter from nonpoint sources (Alam et al. 2018; Hossain et al. 2012; Kim and Kang 2004;

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Note. This manuscript was submitted on June 13, 2023; approved on January 29, 2024; published online on May 25, 2024. Discussion period open until October 25, 2024; separate discussions must be submitted for individual papers. This paper is part of the *Journal of Environmental Engineering*, © ASCE, ISSN 0733-9372.

Liang et al. 2019; Wicke et al. 2012). Trash on beaches and in waterways is aesthetically unappealing and poses potential dangers to marine organisms, causing economic impacts and potential long-term harm to the marine environment (Gold et al. 2015; Moore et al. 2016) and possibly human health (Prata et al. 2020). Litter or trash can be defined as any improperly discarded waste material, including, but not limited to, convenience food, beverage, product packages, or containers constructed of steel, aluminum, glass, paper, plastic, and other natural and synthetic materials (California Regional Water Quality Control Board Los Angeles Region 2001).

Estimation and control of litter loads is being increasingly incorporated into policy and management, including in California. Under Clean Water Act section 303(d), states are required to establish total maximum daily loads (TMDLs), the maximum amount of a pollutant that a waterbody can receive and still meet water quality standards, for any body of water that is impaired (Kim 2002). The California State Water Resources Control Board established TMDLs for trash or litter in some of Southern California's urbanized watersheds, while allocating pollutant loadings to point and nonpoint sources (California Regional Water Quality Control



washoff was found to be controlled by local factors such as topography, slope, infiltration capacity, and antecedent moisture, which influence runoff rate (Tu and Smith 2018). The studies with information on the buildup rates by land uses and estimates of annual litter loading (Armitage 2007; Armitage and Rooseboom 2000; BASMAA 2014; Hadiuzzaman et al. 2022; Martinez and Griffiths 2023; Weideman et al. 2020; Winston et al. 2023) have not been directly applied and calibrated in stormwater modeling software.

### Sensitivity Analysis and Calibration

A sensitivity analysis (SA) is conducted to determine how the sensitivity of certain parameters can impact the model output (Lehtinen 2014). In the case of a buildup and washoff model, a SA can determine which parameters can influence litter loading the most. Both local and global methods exist for SA of hydrological models, such as screening methods, regression-based methods, and variance-based methods (Hong et al. 2019). Local SA methods or one-at-a-time methods determine the changes in model outputs from incremental changes in a single input parameter (Sun et al. 2012). A local SA is inefficient when more than one parameter controls the model output, because each parameter can directly affect the model output and indirectly effect other parameters. Local SA also fails to analyze the effect of large parameter changes (Sun et al. 2012). The Morris method ranks different parameters according to their sensitivities, while avoiding high computational cost of regression-based and variance-based methods. The Morris method averages local sensitivity measurements taken at different points of evenly spaced increments over a portion of the parameter range. This method is therefore a global method, as it explores a region of the parameter space (Chen et al. 2019; Vanrolleghem et al. 2015). The modified Morris method has been widely accepted as the standard for screening exercises (Hao et al. 2021; Li et al. 2016, 2020; Ma et al. 2021; Mohammed et al. 2022; Peng et al. 2020; Zhong et al. 2023).

Calibration of storm water management models (SWMM) washoff models can be difficult due to the variability among storm events, and reproducing the time variation of washoff concentration may be too difficult of a task given the simplified representation of the washoff process in SWMM. This simplified approach only considers how a given runoff rate can washoff available pollutants, ignoring aspects of the land surface and differences in pollutant size or structure. It is more realistic to calibrate against the total mass of washoff produced over a number of storm events rather than focus on individual storm events (Rossman and Huber 2016). Tetra Tech (2010) utilized this approach and adjusted model parameters until a target annual load was simulated within an acceptable percent difference from observed data.

### Main Objectives

This paper addresses the research questions:

1. What is the process to develop buildup and washoff parameters to model litter loading in an urban area?
2. How are antecedent days and storm magnitude incorporated into buildup and washoff parameter development?

Our objective is to present a methodology to develop buildup and washoff parameters for densely populated urban areas. Using localized litter collection data at a small catchment scale, we develop and test the performance of these parameters for two watersheds within LA County, a coastal metropolitan area that meets the above criteria. An assessment is also made to test how these model parameters perform when applied to another

urbanized watershed with similar rainfall and climate patterns, such as the San Diego River Watershed.

### Data and Methods

The following section introduces the study areas, the incorporated datasets used for buildup and washoff parameter development, and the governing equations used for parameter development. Following the parameter development section, information on hydrologic verification and validation of the developed parameters is presented. Last, a brief section presents the street sweeping functionality within PCSWMM.

### Study Areas

Three watersheds were analyzed for the purpose of this study: the Los Angeles River Watershed (LARW), Ballona Creek Watershed (BCW), and Lower San Diego River Watershed (LSDRW) (Fig. 1). These watersheds were selected due to data availability, similarity in rainfall patterns (short and episodic in the fall and winter months), and common levels of urbanization. The episodic nature of rainfall in these areas, combined with the increase in imperviousness across urban surfaces, leads to a flushing of pollutants into receiving waters (Holt et al. 2017). Mean annual rainfalls for the BCW, LARW, and LSDRW are 411 mm, 528 mm, and 498 mm, respectively. The LARW and BCW are adjacent. LARW covers approximately 216,000 ha and its main stem is approximately 82-km long from the Santa Monica Mountains to the Pacific Ocean. The river channel is 94% concrete banks and about 75% hard concrete bottom (Boroon and Coo 2015). The LARW is characterized by steep mountainous headwaters and low-lying flat sections in the San Fernando Valley. The LARW has a population of approximately 9 million people, with 43 cities plus unincorporated communities. The land uses are 37% residential, 8% commercial, 11% industrial, and 44% open space (Los Angeles County Public Works 2023b).

The BCW covers approximately 33,600 ha and is one of the most heavily developed watersheds in Southern California, with 61% impervious land cover (Gold et al. 2015). Due to channelization and imported water use, Ballona Creek has shifted from naturally ephemeral to perennial (Gold et al. 2015). The BCW also extends into the Santa Monica Mountains, and spans major cities: Beverly Hills, West Hollywood, unincorporated areas of LA County, parts of Culver City, and Inglewood. The BCW drains into Santa Monica Bay (Fig. 1). The BCW has approximately 1.5 million people and the following land uses: 64% residential, 4% industrial, 24% open space/other, and 8% commercial (Los Angeles County Public Works 2023a).

The entire San Diego River Watershed drains 111,628 ha to its discharge point at the Pacific Ocean. Two large dams hydrologically separate the upper watershed from the LSDRW, which drains 41,908 ha. According to 2010 US Census data, there are approximately 520,000 residents in the entire San Diego River Watershed (Project Clean Water 2022). The LSDRW has the following land uses: 31% residential, 2.5% industrial, 56.5% open space, and 10% commercial. The following land uses were used in PCSWMM for the LSDRW: commercial, residential, and industrial (Fig. 1). Due to lack of validation data, open space land use is not included for litter buildup and washoff; however, open space areas did contribute to the surface runoff.

**Fig. 1.** (a) Map of California showing BCW, LARW, and the LSDRW; (b) elevation data for LSDRW with rain gages and monitoring stream gages (source: Esri, CONANP, TomTom, Garmin, FAO, NOAA, USGS, EPA); and (c) LSDRW divided into subcatchments, also showing land use data within each subcatchment. Datum North American 1983.

### Hydrologic Modeling Input

PCSWMM models were developed for each watershed (LARW, BCW, and LSDRW). Input data used for PCSWMM include rainfall data from NOAA's National Center for Environmental Information (NCEI), elevation data from the United States Geological Survey (USGS), soil data from United States Department of Agriculture, evaporation zones from the California Irrigation Management Information System (CIMIS), and land use data from the San Diego Department of Associated Governments (SANDAG). Due to limited geographic information, land use data at the entire watershed scale from the LA County Public Works database was used for LARW and BCW. The digital elevation models (DEM) for Los Angeles County and San Diego were downloaded from the USGS Earth Explorer database. We used data from the Shuttle Radar Topography Mission (SRTM, 30-m resolution). These DEM layers were utilized in ArcGIS to delineate subwatersheds or subcatchments. Six subwatersheds were delineated within the BCW as well as six in the LARW. Seven subwatersheds were delineated within the LSDRW. NOAA's NCEI provided hourly precipitation data. A total of six rain gages were used for modeling the three watersheds (Table S1 in the Supplemental Materials). The Green-Ampt method was used in PCSWMM to simulate infiltration. Infiltration parameters include suction head (mm), conductivity

(mm/h), and initial deficit (unitless). These parameters are determined from the hydrologic soil group (Geosyntec Consultants 2016). Due to the variability of hydrologic soil types in our watersheds, spatially weighted average infiltration rates were calculated (Table S1 in the Supplemental Materials). Hydrologic soil groups were determined for each subwatershed using the soil survey geographic database, SSURGO (NRCS, n.d.). The studied watersheds fell within evaporation zones 4, 6, 9, and 14 (Table S1 in the Supplemental Materials).

Land use data in the LSDRW were from SANDAG. Land use for LARW and BCW was determined from the LA County Public Works website. The GIS data for the LA County land uses had several gaps; therefore, regional land use estimates across the entire watersheds were used for land use classification. Land use data for San Diego were simplified to match the data from the County of Los Angeles Department of Public Works Watershed Management Division (2004). Schools, retail, and urban parks were grouped with commercial land use. This allowed for all litter loading to be simulated with the same land uses across the three watersheds. Open space land use was excluded from the LSDRW due to lack of validation data and the dissimilarity between the sampled open space areas in the LA County watersheds compared to the open space areas in the LSDRW. Subwatersheds were not created at

the land use scale, so a single subwatershed had multiple land uses. The limitation of this approach with regard to developing washoff parameters is discussed in later sections.

### Buildup Parameter Development

Buildup and washoff parameters are used to simulate accumulation rates and rates of mobilization for pollutants (in this case litter) in stormwater simulation models. Local data are needed to correctly calibrate these values to match observed data and ensure model effectiveness. Datasets provided by the LACBS (2004) for the LARW and BCW were used to develop buildup and washoff parameters. The data from LA County include washoff loads in mass/area categorized into each major contributing land use: HDSFR, LDSFR, commercial, industrial, and open space. For our analysis, we combine the data from the high- and low-density residential land use into a single category.

Our method provides regional estimates based on the average rates of washed-off litter (kg/ha) from each storm across all sites observed in LA County. A technical memorandum for the Bay Area Stormwater Management Agencies presented a method to estimate baseline trash loads from field investigations (BASMAA 2011). The LACBS was analyzed as part of the BASMAA study. They determined litter generation rates for LA County by dividing the total reported washed-off litter (mass/area) by the days leading up to the storm. This created various buildup rates [mass/(area-days)] varying with each storm event and each land use. We implemented a different methodology to arrive at these buildup rates, using average washoff loads. For example, for the LARW, the total litter over the entire drainage area for industrial land use was 18.87 (kg/ha); however, the estimated annual loading based on the average washoff loads per storm event was 66.28 (kg/ha). Within their own data, BASMAA (2014) found there to be significant relationships ( $p < 0.05$ ) between trash and median income with retail and residential land uses. BASMAA (2014) found neither strong ( $r > 0.7$ ) nor statistically significant ( $p < 0.05$ ) relationships between trash generation and factors such as rainfall, household income, property value, population density, level of education, and other demographics in the LACBS. Therefore, socioeconomic and demographic information was excluded from our analysis when developing buildup and washoff parameters for the LA County Watersheds.

We utilize the LACBS (2004) as the basis of our parameter development. In the LACBS (2004), washed-off litter was collected and weighed at drainage points after each storm event over a period of roughly 2 years (November 2002 to April 2004). Drainage areas were delineated with only one land use per subcatchment. In our analysis, average washoff loads were plotted against dry days preceding the start of the storm events. Average loads were used to establish trends to overcome the variability in washoff loads with respect to site location. These data work well to establish buildup and washoff parameters, because there is a clear distinction of contributing land uses, the number of antecedent dry days, and runoff that produced a given washoff load.

To apply the principles of litter accumulation and washoff on a regional scale, we used PCSWMM, a computational hydrodynamic modeling software, where a user must define pollutants and rates of pollutant generation for different land uses (Rossman and Huber 2016). According to the Rossman and Huber (2016), buildup of traditional water quality constituents is a nonlinear function of dry days; however, there is no obvious proper functional form to describe pollutant buildup over time, and trash may follow different patterns from other constituents. There are three different functional options for developing surface buildup: power function (of which linear is a special case), exponential, and saturation. We

develop parameters for a linear power function [Eq. (1)] and a nonlinear power function [Eq. (2)]

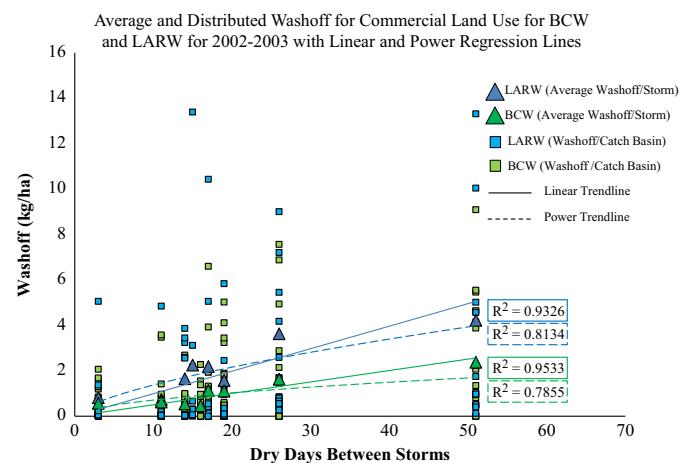
$$b = \min(B_{\max}, K_B t^1) \quad (1)$$

$$b = \min(B_{\max}, K_B t^{N_B}) \quad (2)$$

where  $b$  = buildup (kg/ha);  $t$  = buildup time interval (days);  $B_{\max}$  = maximum buildup possible (kg/ha);  $K_B$  = buildup rate constant [kg/(ha days)]; and  $N_B$  = buildup time exponent, dimensionless.

We lacked data on the litter retained in the watershed following a storm; therefore, we assumed that the minimum buildup available equals the observed washoff for a given event. The actual buildup may have been greater than our assumed values, as our data only show the amount washed off, and some litter may be stored in the watershed. For linear buildup, the slope of the linear regression line was used as  $K_B$ . Parameters for all land uses for each watershed are presented in the results section. Preliminary tests of an exponential function to model buildup gave lower  $R^2$  values when washoff was plotted against dry days, and was therefore excluded from further analysis. A saturation function for pollutant buildup was not tested, given that this function requires a clearly defined asymptote or upper limit. Typically, the fitted time exponent  $N_B$  is less than or equal to 1 so that the rate of buildup decreases with time. This was confirmed from the equations of the power regression lines tested against our data. For a linear buildup function,  $N_B$  was set to 1.  $B_{\max}$  can also be implemented with the buildup function to limit the total available load.  $B_{\max}$  was found to be useful during calibration to match observed washoff data when using constant buildup rates.

The washoff data from the LACBS shows an increased washoff load with an increasing number of dry days. A linear regression line and a power regression line were fit to the average washoff loads across all sites for each storm event. The intercept of the regression line was fixed at zero. This improved the linear correlation in some cases, and followed the framework of the SWMM reference manual (Rossman and Huber 2016). An example of this approach is shown in Fig. 2, with the coefficient of determination ( $R^2$ ) for the trendlines. The washoff loads were analyzed against dry days in the program R, with a Pearson Correlation test, using the “cor.test” function from the “stats” package (R Core Team 2023).



**Fig. 2.** Average washoff loads per storm event and individual washoff for each monitoring site for commercial land in the BCW and LARW for 2002–2003 with linear and power regression line.

This determined that there is weak positive relationship ( $r = 0.09$ ) and the relationship is not significant ( $p$ -value = 0.1827), when analyzing the washoff loads across all sites per storm event. However, when comparing the average washoff load across all sites against dry days, there is strong positive correlation ( $r = 0.89$ ) and the relationship is significant ( $p$ -value = 0.002). The same approach was implemented for all land uses for each year of sampling in both the LARW and the BCW.

Additional graphs for each land use type are provided in the Supplemental Materials. The  $R^2$  values for all land uses are presented in the results section.

### Washoff Parameter Development

Washoff parameters were developed to match observed data for individual storm events and the overall loading from a group of storm events, given changes in mean runoff. A constant buildup rate was desired to be used across multiple years for a given land use, so that the only variables affecting washoff load were the available buildup load, and rainfall-runoff for a given storm. Fig. 3 shows average washoff loads for all land uses, with both rainfall and buildup days before storm events plotted for both years of sampling

$$w = K_w q^{N_w} B \quad (3)$$

where  $w$  = rate of washoff (mg/h);  $K_w$  = washoff coefficient ( $\text{mm}^{-1}$ );  $N_w$  = washoff exponent (unitless);  $q$  = runoff rate per unit area ( $\text{mm}/\text{h}$ ); and  $B$  = pollutant buildup (kg).

When comparing events with similar simulated buildup, in some cases increased rainfall correlated with increased washoff. Other correlations that could have resulted in the deviations from the expected washoff loads are in the discussion section.

The washoff equation in SWMM has three different possible forms: exponential, rating curve, and event mean concentration (EMC). The EMC approach produces washoff concentrations that are uniform within-storm and the loading rate for the entire storm will vary in direct proportion to the runoff rate. By using either a rating curve or exponential function, washoff rates can be simulated to increase and decline proportional to storm runoff. The rating curve is typically used for natural catchments and rivers, where sediment load is proportional to flow raised to a power

(Rossman and Huber 2016). Based on these criteria, the exponential washoff function [Eq. (3)] was chosen.

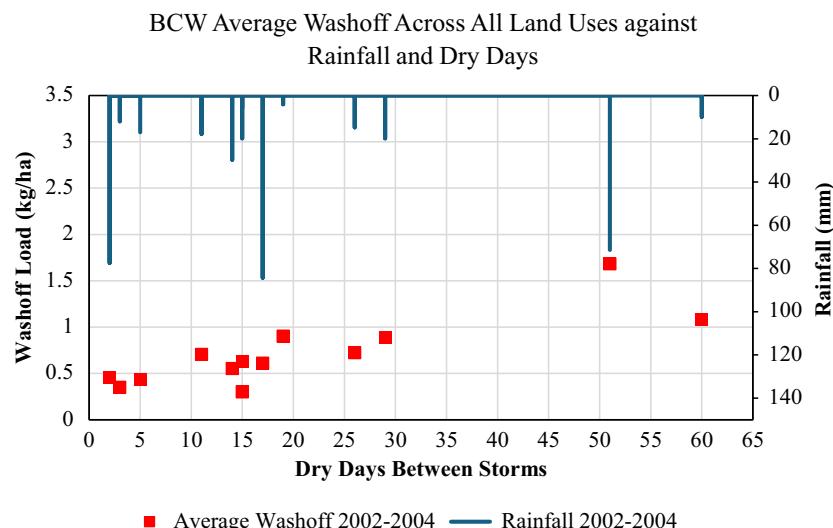
The parameters  $K_w$  and  $N_w$  were developed based on storm events with similar buildup days but different runoff rates per unit area. We assume that if buildup rates are constant, then two events with similar buildup days would have approximately the same buildup at the start of the storm, but the differences in observed washoff could be correlated to differences in rainfall. Using this assumption, Eq. (3) was rearranged to determine  $K_w$ . For example, if a given runoff rate per unit area washed off only a percentage of the presumed available load, and a value for  $N_w$  was selected based on the literature, then Eq. (3) could be used to determine  $K_w$ . This method was used to provide an initial estimate of a possible value for  $K_w$  and was adjusted further to match target loading during calibration.

### Litter Loading Validation for LA County Watersheds

Two forms of validation were conducted for the LA County watersheds. The first analysis was conducted using the second year of data from the LACBS. These data were collected from 2003 to 2004 in the same manner as the previous year. A key factor was the reduction in rainfall for this validation year, which was approximately half of the previous year. Observed data were scaled up from the average values from LACBS, taking the average washoff/storm ( $\text{kg}/\text{ha}$ ), and multiplying it by the total land use area. Scaled-up values were used for comparison with simulated results. The second validation was conducted using data from the Ballona Creek Trash Interceptor, developed by The Ocean Cleanup. The Ballona Creek Trash Interceptor collected litter from the outlet of the Ballona Creek Watershed from October 2022 through May 2023. Data were published on their website and the total annual loading for the 2022–2023 wet season was used to validate the buildup and washoff parameters (The Ocean Cleanup 2023).

### Hydrologic Verification and Litter Loading Validation for the Lower San Diego River Watershed

Two USGS stream gages were used to verify the hydrologic modeling in the LSDRW (Fig. 1). An upstream gage and downstream



**Fig. 3.** Average washoff load for all land uses plotted with dry days and rainfall for both years of sampling. Top x-axis shows each storm plotted against the number of dry days leading up the storm, with rainfall (mm) for the storm on the right y-axis.

gage were used. Flow rate data were acquired from the USGS National Water Information System. These data were then imported into PCSWMM as a time series and compared with simulated results. A total of 13 rain events were used for hydrologic verification. The average value for the maximum (peak) flow of the 13 rain events was calculated and compared. These storms were within the time range used for litter loading validation (presented below).

Buildup and washoff parameters developed for the LA County watersheds were applied to the LSDRW and validated with data from a Technical Report by Michael Baker International, Regional Trash Generation Rates for Priority Land Uses in San Diego County (Michael Baker International 2018). Their research determined regional trash generation rates for priority land uses in San Diego County, which involved installing full capture devices in 36 drain inlets throughout the county. Collection from these drain inlets was conducted quarterly. After validating the LARW and BCW, the BCW parameters were used for the LSDRW, due to more recently available validation data. Simulated results were compared with observed data for each land use. Litter generation rates for each land use were scaled up in the same manner as the LA County watersheds to compare total simulated litter load with observed data.

### Street Sweeping

Due to lack of data, street sweeping was excluded from the LARW and BCW PCSWMM models. Street sweeping is included in the LSDRW model, reducing the available buildup load. Within PCSWMM, a user can define a sweeping interval, buildup available for removal, and removal efficiency. Based on data from the City of San Diego, the street sweeping interval was set to be weekly. The buildup available was determined by estimating the area associated with roads in each land use type. A GIS shape file was used to determine the lengths of roads within each land use type, an average width was used to convert the lengths into an area. This average width (15 m) was based on information from the City of San Diego Transportation Manual (Millard-Ball 2022). A percentage of the total land use area that is roads is used as the buildup available to be swept. Lacking sufficient data on removal efficiencies for litter, three different scenarios were tested: 70%, 80%, and 90% removal efficiency (Selbig and Bannerman 2007). Street sweeping analyses were conducted in ideal scenarios where all streets that are capable of being swept are, meaning cars or other obstructions did not stop the sweeper.

Please see the Supplementary Materials for more information on sensitivity analysis, model calibration, and validation.

## Results

### Hydrologic Verification

Table 1 shows the verification of hydrologic data between simulated and observed data. Table 1 shows the values associated with the downstream (Fashion Valley) and upstream (Santee) USGS stream gages. The model was run with a continuous simulation from July 2016 to November 2017, and the following error

functions were tested: Nash–Sutcliffe efficiency (NSE) and integral square error (ISE). NSE and ISE values were calculated for total inflow ( $m^3/s$ ) between simulated and observed data. Depending on the NSE value, model performance is considered to be very good ( $NSE > 0.75$ ), good ( $NSE$  between 0.65 and 0.75), satisfactory ( $NSE$  between 0.5 and 0.65), or unsatisfactory ( $NSE < 0.5$ ) (Moriasi et al. 2007; Pachepsky et al. 2016). ISE values are good if the value is between 6.0 and 10.0, very good if between 3.0 and 6.0, and excellent if less than 3.0 (Sarma et al. 1973). The relatively low percent error between observed and simulated average peak flow (<20%), the NSE values in the very good (0.79) and satisfactory (0.54) ranges, and the excellent rating for ISE allow this verification to be satisfactory for hydrologic performance.

### Buildup Parameter Comparison

The buildup rates ( $K_B$ ) associated with the linear buildup function are presented in Table 2. The  $K_B$  and buildup time exponent ( $N_w$ ) associated with the power buildup function are also presented in Table 2. Initial maximum buildup values ( $B_{max}$ ) values were taken as the greatest observed washoff load for each land use.

Values for linear buildup rates across all land use types ranged from 0.016 to 0.38 ( $kg/ha\cdot day$ ), with a mean of 0.068 ( $kg/ha\cdot day$ ). Values for power buildup rates ranged from 0.046 to 0.64 (mean of 0.25), and exponents in the range of 0.18 to 1.4 (mean 0.54). Maximum buildup values ranged from 0.57 to 17.5 ( $kg/ha$ ), with a mean of 3.1 ( $kg/ha$ ). Our mean buildup rates are slightly higher than those reported in BASMAA (2014), with a mean of 0.0175 ( $kg/ha\cdot day$ ) and a maximum of 0.131 ( $kg/ha\cdot day$ ). Winston et al. (2023) reported a buildup loading rate in the range of 0.10 to 5.22 ( $kg/ha\cdot day$ ) with a mean value of 0.79 ( $kg/ha\cdot day$ ). Their higher values are impacted by the fact that approximately 80% of the collected material was natural litter (leaf litter, etc.).

### Buildup/Washoff Calibration and Validation for LA County Watersheds

Based on our initial estimates from using Eq. (3), when  $N_w$  was set to equal 0.5,  $K_w$  ranged from 0.6 to 2.0, depending on which two storms with similar buildup periods were being analyzed. These initial values worked well to estimate washoff loads for some storm events, but over- or underestimated the values for others. Fig. 4 presents simulated washoff loading rate ( $kg/h$ ) compared with observed data converted to ( $kg/h$ ). Observed washoff data are presented as the total loading ( $kg$ ) for a given storm and divided by the duration (h) of the simulated storm event. Table 3 provides additional context about the presented storm events in Fig. 4.

Large volumes of runoff and highest rainfall did not always produce large washoff loads. Runoff combined with a long period of dry weather resulted in the greatest washoff loads. Large washoff loads were also observed with relatively low rainfall when there was a longer period of dry weather (Alam et al. 2017).

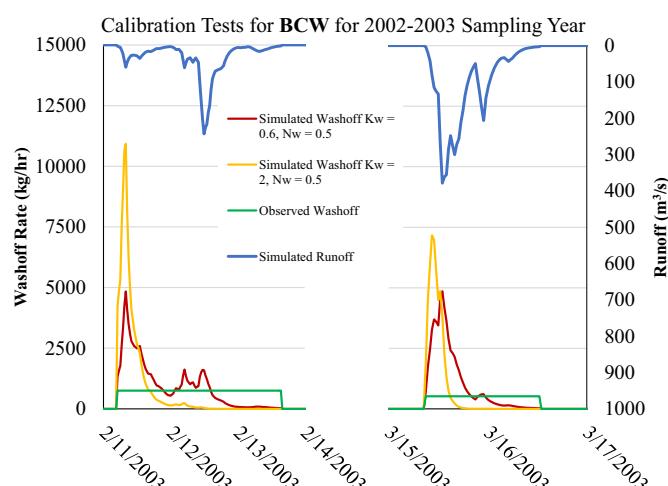
The preliminary estimates for the washoff parameters were calibrated to match observed washoff for all land uses. The final values were selected as  $K_w$  (1.25) and  $N_w$  (0.925). Table 4 shows

**Table 1.** Hydrologic verification for downstream (USGS Fashion Valley) and upstream (USGS Santee) locations

Stream gage	Date range	Number of storm events	Observed average peak flow ( $m^3/s$ )	Simulated average peak flow ( $m^3/s$ )	% error between average peak flow	NSE	ISE
Fashion Valley	July 2016–Nov 2017	13	29.41	24.57	16	0.79	1.54
Santee			17.98	18.93	-5	0.54	1.86

**Table 2.** Buildup rates and maximum buildup for land uses in LA County watersheds

Watershed	Sampling year	Land use	Maximum buildup possible		Linear buildup		Power buildup		
			$B_{\max}$ (kg/ha)	$K_B$ (kg/ha-day)	$R^2$	$K_B$ (kg/ha-day)	$N_w$	$R^2$	
LARW	2002–2003	Commercial	4.2	0.099	0.93	0.35	0.65	0.95	
		Residential	0.96	0.025	0.56	0.048	0.78	0.04	
		Industrial	17.5	0.38	0.91	0.11	1.4	0.70	
		Open space	0.57	0.022	0.55	0.25	0.23	0.02	
BCW	2002–2003	Commercial	2.7	0.056	0.95	0.24	0.52	0.66	
		Residential	0.85	0.016	0.85	0.11	0.33	0.20	
		Industrial	1.47	0.032	0.91	0.13	0.56	0.62	
		Open space	2.6	0.050	0.82	0.23	0.48	0.31	
LARW	2003–2004	Commercial	2.7	0.062	0.88	0.39	0.47	0.74	
		Residential	0.73	0.021	0.69	0.097	0.53	0.95	
		Industrial	7.7	0.19	0.70	0.64	0.60	0.64	
		Open space	3.9	0.049	0.71	0.046	0.83	0.29	
BCW	2003–2004	Commercial	1.1	0.018	0.94	0.15	0.45	0.95	
		Residential	0.97	0.019	0.84	0.26	0.30	0.98	
		Industrial	1.1	0.022	0.74	0.48	0.18	0.95	
		Open space	1.3	0.029	0.75	0.47	0.25	0.75	


**Fig. 4.** Calibration test for varying washoff parameters during first year of sampling. Two storm events shown as subplots. Simulated runoff shown on the top axis.

calibrated values for  $K_B$  and  $B_{\max}$  for a linear buildup function, using a constant  $K_w$  and  $N_w$ . Table 5 shows the target value of washoff load (kg/ha) used for calibration, the simulated washoff load using calibrated values from Table 4, and the error between the annual loads. The decision to use a single set of parameters to define washoff for all land uses is elaborated in the discussion

section. Table 6 shows validation of the calibrated buildup and washoff parameters when applied to the following year of data in the LA County Watersheds, where rainfall depth decreased by nearly half.

The constant washoff parameters estimated washoff more closely in the LARW compared to the BCW. By design, the model was set to produce less washoff load when runoff decreased. The highest error occurred when washoff loads increased during the second year. High error also occurred for commercial land use in the BCW. From year 1 to year 2, there was approximately a 70% decrease in washed-off litter for commercial land use. Model parameters were unable to simulate this decrease based on runoff alone, indicating that other factors may have reduced observed washoff. The washoff exponent was the most sensitive parameter (Table 7). The maximum buildup and washoff coefficients were classified as sensitive, where the buildup rate constant was moderately sensitive.

#### Regional Estimates of Litter Loading for LA County Watersheds from Simulations

Regional estimates of litter transported by stormwater can inform municipalities of the scale and method of collection needed to capture and reduce the amount of litter entering waterways. Regional estimates based on calibrated parameters are presented in Table 8. These estimates were developed based on simulations for the 2002–2004 sampling events conducted by LA County. Our results provide regional estimates based on the average rates of washed-off litter (kg/ha) from each storm across all sites observed in LA County.

**Table 3.** Additional information for storm events in Fig. 4, and comparison of total washoff load for calibration scenarios with scaled-up observed data

Storm event	Antecedent dry days	Rainfall (mm)	Max rainfall intensity	Scenario	Washoff load (kg)
2/11/2003–2/14/2003	50	91	12.20	$K_w = 2, N_w = 0.5$	52,596
				$K_w = 0.6, N_w = 0.5$	55,510
				Observed	44,104
3/15/2003–3/17/2003	17	108	21.59	$K_w = 2, N_w = 0.5$	30,659
				$K_w = 0.6, N_w = 0.5$	25,570
				Observed	14,578

**Table 4.** Calibrated buildup parameters (buildup rate constant, maximum buildup)

Watershed	Land use	$K_B$	$B_{\max}$
LARW	Commercial	0.1	4.5
	Residential	0.03	1.5
	Industrial	0.4	13
	Open space	0.025	3
BCW	Commercial	0.09	2
	Residential	0.02	1.25
	Industrial	0.05	2
	Open space	0.08	2.5

**Table 5.** Target washoff load compared with simulated washoff load (kg/ha-year) for calibration

Watershed and sampling year	Land use	Target (kg/ha)	Simulated (kg/ha)	% error
LARW	Commercial	17.02	17.06	0.20
2002–2003	Residential	4.82	5.33	10.70
Nov 10–May 5	Industrial	60.70	57.30	5.61
	Open space	4.63	4.92	6.30
BCW	Commercial	9.41	6.80	27.74
2002–2003	Residential	2.69	2.65	1.25
Nov 10–May 5	Industrial	5.57	6.01	8.05
	Open space	8.80	8.27	6.11

**Table 6.** Target washoff load compared with simulated washoff load (kg/ha-year) for validation

Watershed and sampling year	Land use	Target (kg/ha)	Simulated (kg/ha)	% error
LARW	Commercial	10.82	10.91	0.83
2003–2004	Residential	3.58	3.57	0.31
Nov 3–April 4	Industrial	30.65	32.79	6.98
	Open space	5.79	3.85	33.46
BCW	Commercial	2.74	4.14	51.02
2003–2004	Residential	3.01	1.87	37.92
Nov 3–March 4	Industrial	3.84	3.86	0.58
	Open space	4.84	4.97	2.78

**Table 7.** Modified Morris screening method SA results

Parameter	Modified Morris sensitivity value	Ranking
$N_w$	1.29 (very sensitive)	1
$B_{\max}$	0.83 (sensitive)	2
$K_w$	0.51 (sensitive)	3
$K_B$	0.19 (moderately sensitive)	4

The values developed for the BCW were validated against an additional year because there was an available dataset from the Ballona Creek Trash Interceptor. The values developed for the 2002–2004 year produced washoff estimates that were 2.6 times greater than the collected trash loads for 2022–2023 year. Therefore, BCW parameters were recalibrated to match the data for

the 2022–2023 year (Table 9).  $K_B$  values from Table 4 were scaled down by approximately 70% to match annual load with observed data.

### Street Sweeping Analysis

Street sweeping was tested for the same simulation year as hydrologic verification and litter loading validation, with the following removal efficiencies: 70%, 80%, and 90%. These removal efficiencies can collect 21%, 23%, and 25% of the available surface buildup, respectively.

### Results and Validation for Lower San Diego River Watershed

Using the updated  $K_B$  values (Table 9) and the  $B_{\max}$  values for the BCW (Table 4), regional estimates for the LSDRW were simulated. Table 10 shows the results for the 2016–2017 simulation year compared with data from Michael Baker International (2018). The annual washoff values were converted from lbs/acre to kg/ha.

The sample size for the validation is relatively low ( $n = 13$ ) and the distribution of sample sites does not fully represent the entire LSDRW watershed. These are some factors that could affect the validation. Other factors not captured in the model—such as topography, population density, climatic conditions such as wind, and the volume of vehicle and pedestrian traffic—can also impact the litter loading in an urbanized watershed.

The annual loading rates determined for the LSDRW fall within the range presented in BASMAA (2014). BASMAA (2014) estimates a production of litter of 0.5 to 150 (gallons/acre/year), which converts to approximately 0.38 to 114 (kg/ha/year), depending on the land use and the median household income level (conversion made using their relationship of 0.68 lbs to each gallon of material). They split these estimates into low, moderate, high, and very high categories. Our estimation for the LSDRW for the year of July 2016 to November 2017 is 2.15 kg/ha. This falls in the range of the low estimate for the Bay Area, where low is less than 3.8 kg/ha, moderate is 3.8–7.6 kg/ha, and high estimates are 7.6–38 kg/ha. Alam et al. (2017) reported total pollutant load for wet seasons with the following values (kg/ha): 4.5 ( $\pm 0.8$ ), 0.7 ( $\pm 0.5$ ), 3.7 ( $\pm 2.4$ ), 3.5 ( $\pm 6.3$ ). Weideman et al. (2020) quantified litter loading as 0.377 (kg/ha-day) for industrial land use, 0.115 (kg/ha-day) in commercial areas, and 0.0024 (kg/ha-day) for residential areas. This equates to an annual loading of 137 (kg/ha) for industrial, 41.5 (kg/ha) for commercial, and 0.876 (kg/ha) for residential. The values for industrial and commercial land uses are much higher than our estimated loading for the LSDRW; however, the value for residential land use is only slightly higher than our estimated loading.

### Discussion

Model parameters are uncertain because multiple values are needed to estimate them, and agencies may only collect data for some of the necessary values. Lacking knowledge of the initial or remaining buildup after storm events, it was difficult to develop washoff parameters. To develop more accurate washoff parameters, information is needed on the amount and material of available buildup at the start of a storm and residual buildup after a storm, to determine the effectiveness of a given rainfall-runoff to remove available litter load. A further investigation is also needed to assess the deposition of litter by other sources such as wind or direct dumping. LA County reported high litter loads in the storm drain outlets

**Table 8.** Regional estimates for litter loading for Los Angeles County

Watershed	Simulation year	Total load from PCSWMM (kg)	Total load based on LACBS (2004) (kg)	Total load per unit area from PCSWMM (kg/ha)	Total load per unit area based on LACBS (2004) (kg/ha)	Total runoff volume from PCSWMM (m <sup>3</sup> )	Total rainfall for simulation year (mm)
BCW	2002–2003 (Calibrated)	155,145	155,568	4.6	4.63	28,588,000	417.1
BCW	2003–2004 (Validated)	103,205	117,600	3.1	3.5	18,334,400	223.5
LARW	2002–2003 (Calibrated)	2,486,808	2,548,800	11.5	11.8	237,182,300	404.5
LARW	2003–2004 (Validated)	1,584,020	1,913,760	7.3	8.86	124,718,100	226.8

**Table 9.** Validation results with Ballona Creek trash interceptor for 2022–2023. Updated  $K_B$  values and updated annual load

Watershed	Simulation year	Updated buildup rate constants, $K_B$	Total trash collected by Ballona Creek trash interceptor (kg)	Total load from PCSWMM with initial $K_B$ values (kg)	Total load from PCSWMM with calibrated $K_B$ values (kg)	Total rainfall for simulation year (mm)
BCW	October 2022–May 2023	Commercial: 0.027 Residential: 0.006 Industrial: 0.015 Open space: 0.024	70,170	183,131	71,361	431.8

**Table 10.** Regional estimates for litter loading for San Diego compared with validation data

Land use	PCSWMM simulation for LSDRW with street sweeping (July 2016–November 2017) (kg/ha)	San Diego County special study mean values for litter generation rates (July 2016–November 2017) (kg/ha)	San Diego County special study maximum values for litter generation rates (July 2016–November 2017) (kg/ha)
Commercial	4.48	1.1	4.3
Industrial	3.7	0.73	5.0
Residential	1.3	0.53	2.7
Total	2.15	0.77	3.56

during the dry season, so litter is ending up in the storm system without runoff. This is not reflected in the present model.

There are contradictory findings related to correlation of rainfall-runoff and the amount of litter that is washed off in an urban catchment. In BAASMA (2014), washed-off trash did not correlate with rainfall intensity, runoff, or duration. This could indicate that buildup rates may vary throughout the year—i.e., buildup rates may be different in winter than in spring. If litter washoff is not strongly correlated with rainfall-runoff, then developing washoff parameters to estimate annual loading may not be the best method. Instead, buildup rates could vary, and once a threshold value of runoff is met, then the total available load is washed off. On the contrary, Winston et al. (2023) found that rainfall depth, duration, and peak rainfall intensity were significantly correlated to either macrodebris mass or volume. In the LA County washoff data, there is a clear reduction in rainfall-runoff and reduction in washoff load for both watersheds in the second year. This may reveal some correlation between rainfall-runoff quantities and washed off litter.

We developed washoff parameters from storm events with similar antecedent dry days where runoff correlated with washoff load. This assumption works well if the objective is to match total annual washoff loads. However, it does not work well if the objective is to assess the transportability of trash with respect to different rainfall intensities for select storm events. We assume that litter is generally composed of the same materials across watersheds; therefore, we use a single set of washoff parameters for all land uses. A more accurate approach would be to define varying washoff parameters based on the materials associated with the litter from specific land uses. This would require an understanding of the

typical density of each litter material and a more refined distribution of subcatchments in the PCSWMM model (i.e., each subcatchment would need to have only one land use).

Our simulation results suggest there is the potential to use washoff data at small catchment scales to estimate regional litter loading based on the relative similarity between final estimates with LA County. However, when applying parameters from one watershed to another, extensive data are needed for calibration and validation data. The calibration data are needed to adjust the washoff parameters, and the remaining data are needed to validate that the model reflects the conditions of the watershed. Additional litter may enter a watershed through direct deposition and storage in larger floodplains downstream of the small drainages monitored in the current available datasets. The washoff parameters could also be further optimized to more accurately represent the effectiveness of a given storm to washoff available litter.

## Conclusion and Future Work

We demonstrate the potential to develop standardized buildup and washoff parameters for urbanized watersheds. This work is aimed at improving estimates of litter loading from various land uses. Antecedent dry days were found to be a strong control on litter loads, and rainfall and runoff also impacted litter loads. Our model does not fully evaluate the impact of direct dumping; direct dumping could result in some of the unexplained large spikes of washed-off litter. We found the implementation of maximum buildup values effective to match simulated and observed data for

multiyear simulations and constant parameter values. Standardizing these parameters would allow for efficient estimations of litter loading based on readily available land use information.

Simulated litter generation rates in the BCW and LSDRW varied by about 2 to 5 times when compared to validation data from different years. This indicates that other factors must be considered when applying buildup and washoff parameters from one watershed to another (population density, climatic conditions, socioeconomic data, demographics, site visitation, and vehicular traffic). A pure modeling approach does not fully account for this variability because average values are used when setting maximum buildup values and calculating buildup rates. Additional field data can supplement the findings from our modeled results to model and manage litter more effectively. Ultimately, long-term datasets are needed to improve model performance. Field measurements that focus on areas where there were the greatest observed unexplained spikes in washed-off litter could determine if these spikes are truly outliers or if there is a trend of factors—such as location or socioeconomic factors—leading to an increase in litter spikes. These potential outliers can be seen in the Supplemental Materials related to the washoff loads across all sites per land use in the LARW and BCW. A deeper assessment of socioeconomic factors in certain areas would provide a better understanding of the factors contributing to trash generation. Similarly, dividing the residential category into its various subgroups, such as multifamily, would improve the accuracy of modeled results.

## Data Availability Statement

All software and data can be made available upon request from the corresponding author.

## Acknowledgments

This project was funded by the NOAA Marine Debris Program, award NA21NOS9990109. Thank you also to PCSWMM for their support of an educational research grant that made this project possible. The development of the computer model was also partially supported by NSF Award No. 2244837.

## Supplemental Materials

Eq. (S1), Figs. S1–S35, and Table S1 are available online in the ASCE Library ([www.ascelibrary.org](http://www.ascelibrary.org)).

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