

# All-Dielectric Terahertz Metasurfaces for Multi-Dimensional Multiplexing and Demultiplexing

Wanying Liu, Xiaohan Jiang, Quan Xu,\* Fan Huang, Quanlong Yang, Yongchang Lu, Yangfan Gu, Jianqiang Gu,\* Jiaguang Han, and Weili Zhang\*

Terahertz (THz) communication is an up-and-coming technology for the sixth-generation wireless network. The realization of ultra-high-speed THz communication requires the combination of multi-dimensional multiplexing schemes, including polarization division multiplexing (PDM), mode division multiplexing (MDM), and wavelength division multiplexing, to increase channel capacity. However, most existing devices for MDM in the THz regime are single-purpose and incapable of multi-dimensional modulation. Here, all-dielectric metasurfaces are designed for 2D multiplexing/demultiplexing, which takes the lead in combining orbital angular momentum (OAM) MDM and PDM in the THz regime. The multi-functional wavefront phase modulations and interleaved meta-atom arrangements are used to realize polarization-selective multichannel OAM mode (de)multiplexing, in which the linear-polarized 4-channel and circular-polarized 6-channel demultiplexing are experimentally demonstrated. Between different linear-polarized channels, the measured maximum crosstalk is  $-16.88$  dB, and the isolation of each channel can be greater than 10 dB in a range wider than 0.1 THz. This study paves the way for multi-dimensional multiplexing in the THz regime, which may benefit extremely high-capacity and integrated THz communication systems. The proposed design strategy is readily applied to multi-functional metasurfaces for microwaves and far infrared light, facilitating the development of multiplexing technology and OAM-related applications.

and high-speed 6G communication need THz devices for high-performance beam steering,<sup>[4-5]</sup> modulation,<sup>[6-7]</sup> and multiplexing. More recently, a series of studies on THz multiplexing, including polarization division multiplexing (PDM), wavelength division multiplexing (WDM), and mode division multiplexing (MDM), have received considerable interest.<sup>[8-11]</sup> Among these, MDM that explores the orthogonality of modes<sup>[12-14]</sup> can establish multiple distinguishable data paths using the orthogonal orbital angular momentum (OAM) modes.<sup>[15]</sup> The OAM determines the spiral phase front of the vortex beam proportional to  $\exp(il\varphi)$ , here  $\varphi$  is the azimuthal angle,  $l$  represents the topological charge, and the value of  $l$  can take any integer. OAM-MDM has been extensively discussed in optical and quantum communications.<sup>[16-19]</sup> In recent years, it has gradually garnered attention as an efficient candidate to increase the spectral efficiency of communication systems in the THz regime.<sup>[20]</sup>

The realization of high-quality MDM relies on the convenient and efficient (de)multiplexer for the orthogonal

modes.<sup>[21-25]</sup> Spatial light modulators and spiral phase plates are two straightforward methods for OAM mode conversion.<sup>[26-27]</sup> However, multiple converters and additional beam combiners are required to realize coaxial transmission of orthogonal modes for (de)multiplexing. Metasurfaces composed of sub-wavelength meta-atoms exhibit extraordinary wavefront manipulation

## 1. Introduction

Terahertz (THz) photonics is an emerging field with significant potential for the 6th generation wireless systems (6G), enabling broadband features and good directivity.<sup>[1-3]</sup> The large capacity

W. Liu, X. Jiang, Q. Xu, F. Huang, Y. Lu, Y. Gu, J. Gu, J. Han  
Center for Terahertz Waves and College of Precision Instrument and  
Optoelectronics Engineering  
Key Laboratory of Optoelectronic Information Technology  
Ministry of Education  
Tianjin University  
Tianjin 300072, P. R. China  
E-mail: [quanxu@tju.edu.cn](mailto:quanxu@tju.edu.cn); [gjq@tju.edu.cn](mailto:gjq@tju.edu.cn)

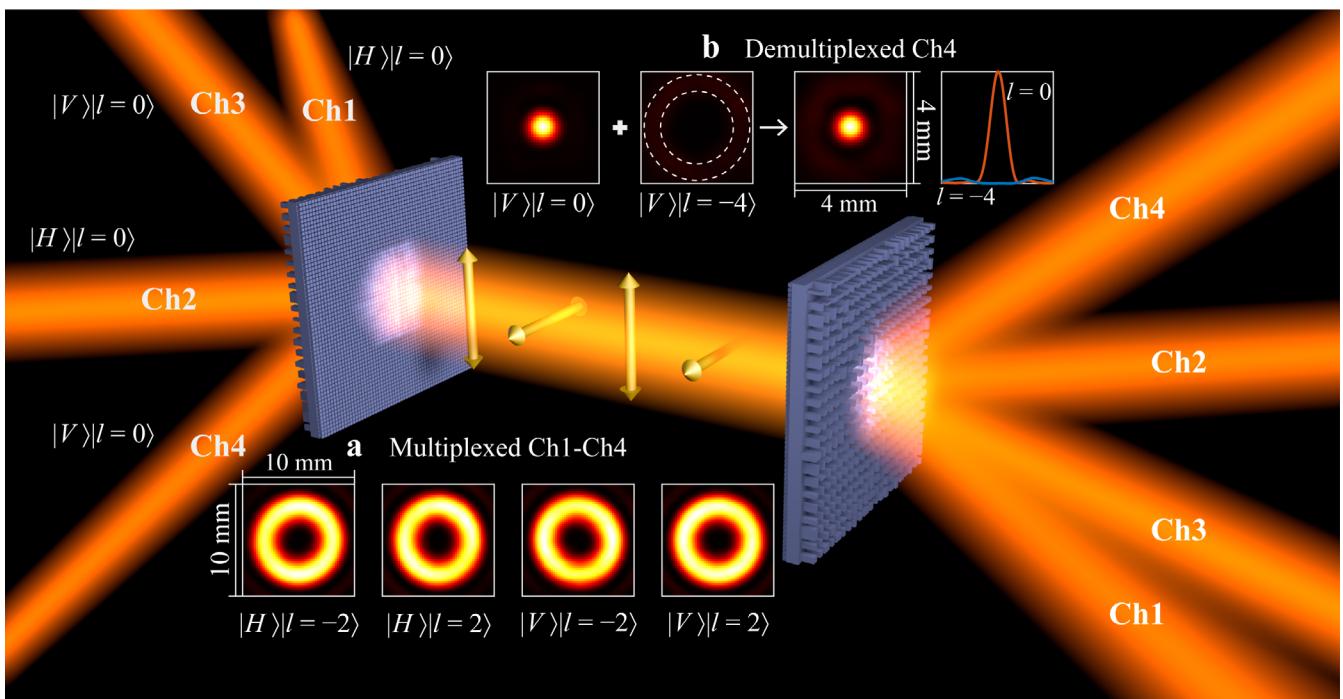
Q. Yang  
Hunan Key Laboratory of Nanophotonics and Devices  
School of Physics and Electronics  
Central South University  
Changsha, Hunan 410083, P. R. China

J. Han  
Guangxi Key Laboratory of Optoelectronic Information Processing  
School of Optoelectronic Engineering  
Guilin University of Electronic Technology  
Guilin 541004, P. R. China

W. Zhang  
School of Electrical and Computer Engineering  
Oklahoma State University  
Stillwater, OK 74078, USA  
E-mail: [weili.zhang@okstate.edu](mailto:weili.zhang@okstate.edu)

 The ORCID identification number(s) for the author(s) of this article can be found under <https://doi.org/10.1002/lpor.202301061>

DOI: 10.1002/lpor.202301061



**Figure 1.** Schematic of 2D MDM based on a pair of multi-functional metasurfaces. The Ch1-Ch4 represent four data-carrying channels. The orthogonal yellow arrows in the figure represent horizontal and vertical polarization, respectively. a) Four multiplexed OAM channels. b) The demultiplexed Ch4, whose intensity distribution is the same as the superposition of the correct-demultiplexed Gaussian beam ( $|V\rangle|l=0\rangle$ ) and incorrect-demultiplexed OAM beam ( $|V\rangle|l=-4\rangle$ ). The figure on the far right shows the normalized intensity distribution of the fundamental-mode Gaussian beam (orange line) and OAM beam with  $l = -4$  (blue line) at the y-axis.

applications such as abnormal refraction, beam modulation, perfect absorption, and mode conversion,<sup>[28–32]</sup> providing a customizable design method for the high-performance OAM mode generators and multiplexers.<sup>[33–38]</sup> Notably, by taking advantage of shared-aperture arrangement<sup>[39]</sup> and polarization-dependent meta-atoms,<sup>[40]</sup> a single metasurface can implement the 2D multiplexing of polarization and mode to increase the spectral efficiency immensely.<sup>[41–44]</sup> Meanwhile, the deflection and focusing of the converted beam can also be integrated into this metasurface, which can significantly benefit the compactness and efficiency of the MDM system.<sup>[45]</sup> Recent pioneering reports in the THz regime have shown encouraging advances in metasurfaces for multichannel vortex beam generation<sup>[46–48]</sup> and OAM mode multiplexing.<sup>[49–50]</sup> Moreover, combining OAM-based MDM and PDM can enhance spectral efficiency and system integration, enabling THz communications to support massive device connections and achieve ultra-high-rate data transmission. Significantly, the working bandwidth of the multi-functional metasurfaces used in multi-dimensional multiplexing and the crosstalk between adjacent channels have not been investigated, which is vital to compact THz wireless communication systems with extremely high data capacity.

Here, we propose all-dielectric metasurfaces for multi-dimensional multiplexing and demultiplexing in the THz regime. The multi-functional phase-modulated metasurfaces function as versatile (de)multiplexers in the MDM and PDM systems. As shown in Figure 1, the Gaussian beams with different

incident angles and polarizations are first converted to coaxially transmitted vortex beams with different OAM modes, and each incident beam serves as a data-carrying channel for information transmission. At the receiving terminal, the demultiplexer recovers the coaxial OAM modes to the corresponding Gaussian beams and focuses the demultiplexed beams on different positions. In the experiment, we demonstrated the demultiplexing process of 4-channel and 6-channel coaxial beams using multi-functional metasurfaces. The low crosstalk and high isolation of the demultiplexed channels show good performance of the fabricated metasurface samples at 0.75 THz. Notably, both two types of metasurfaces with linearly polarized (LP) responses and circularly polarized (CP) responses exhibit broadband responses and have the potential to be compatible with integrated WDM. The multi-functional metasurfaces demonstrated here can benefit the development of compact and broadband platforms for multi-dimensional multiplexing in the THz communication system.

## 2. Results

### 2.1. Preparation of Multi-Functional Metasurfaces

Figure 1 illustrates 4-channel 2D multiplexing and demultiplexing based on a pair of multi-functional metasurfaces. Two horizontally polarized (HP) and two vertically polarized (VP) Gaussian beams with various incident angles are converted into high-order OAM beams by the designed metasurface. Here, the state

of the four orthogonal channels can be described by  $|H\rangle|l = -2\rangle$ ,  $|H\rangle|l = 2\rangle$ ,  $|V\rangle|l = -2\rangle$  and  $|V\rangle|l = 2\rangle$ . The coaxial OAM modes with orthogonal polarizations can serve as independent channels to carry digital signals for high-capacity and high-speed data transmission, the intensity distributions of these four channels are shown in Figure 1a. After coaxial transmission over a specific distance, the vortex beams with different topological charges can be recovered to the Gaussian beams ( $|H\rangle|l = 0\rangle$  and  $|V\rangle|l = 0\rangle$ ) and deflected to different directions using the demultiplexing metasurface. It is worth mentioning that the demultiplexed metasurface can focus the output beam and thus optimize the beam divergence angle to obtain the high-quality Gaussian beam at the receiving terminal. As shown in Figure 1b, the demultiplexed beam corresponding to Channel 4 (Ch4) can be focused on the aim terminal. As the interleaved method is adopted in our metasurface design, this demultiplexed beam is the superposition of correct-demultiplexed  $|V\rangle|l = 0\rangle$  and incorrect-demultiplexed  $|V\rangle|l = -4\rangle$ . The detailed analysis is shown in Section S.1 (Supporting Information). However, we can efficiently receive the energy of the fundamental Gaussian mode by adjusting the diameter of the receiving device because the spot diameter of the OAM beam with the topological charge of  $l = -4$  is much larger than that of the fundamental-mode Gaussian beam and the intensity distribution of the OAM beam is a hollow ring, as shown in the dotted ring in the figure. Similarly, the electric fields of the other three channels are also a superposition of beams with  $l = 0$  and  $|l| = 4$ . We can identify the energy of the correct-demultiplexed fundamental mode without additional mode filters. The designed two metasurfaces can replace many bulky devices, such as  $q$ -plates, beam deflectors, and Fourier transform lenses, thus providing an efficient, versatile, and compact platform for multi-dimensional (de)multiplexing.

The same design method can be used to design multiplexers and demultiplexers according to the reversibility of the light path. Two different phase distributions corresponding to the HP and VP components are required to implement polarization and mode multiplexing/demultiplexing simultaneously. As shown in Figure 2a,b, for the HP component, the transmission function can be expressed as:

$$\Phi_{\text{HP}} = A \exp \left[ i(l\theta + m \frac{2\pi x}{T} + k(f - \sqrt{f^2 + x^2 + y^2})) \right] \quad (1)$$

where  $A$  is the transmission amplitude of the metasurface and is assumed to be 1 when only phase modulation is considered,  $l$  is the topological charge,  $\theta = \arctan(y/x)$  is the azimuthal coordinate,  $T$  is the period of phase gradient,  $m$  is the diffraction order and  $m = \pm 1$  for the 4-channel MDM. Here, we adopt the checkboard-like interleaving method to spatially sample the phase distribution (abbreviated to PD) for OAM mode multiplexing with the topological charge of  $l = +2$  (PD1+PD3 in Figure 2a) and  $l = -2$  (PD2+PD4 in Figure 2). The last term in the phase is for focusing, corresponding to the PD5 in the figure. Here,  $k = 2\pi/\lambda$  is the wavevector,  $\lambda$  represents the wavelength, and  $f$  is the focal length. Similarly, for the VP component, the transmission function is:

$$\Phi_{\text{VP}} = A \exp \left[ i(l\theta + m \frac{2\pi y}{T} + k(f - \sqrt{f^2 + x^2 + y^2})) \right] \quad (2)$$

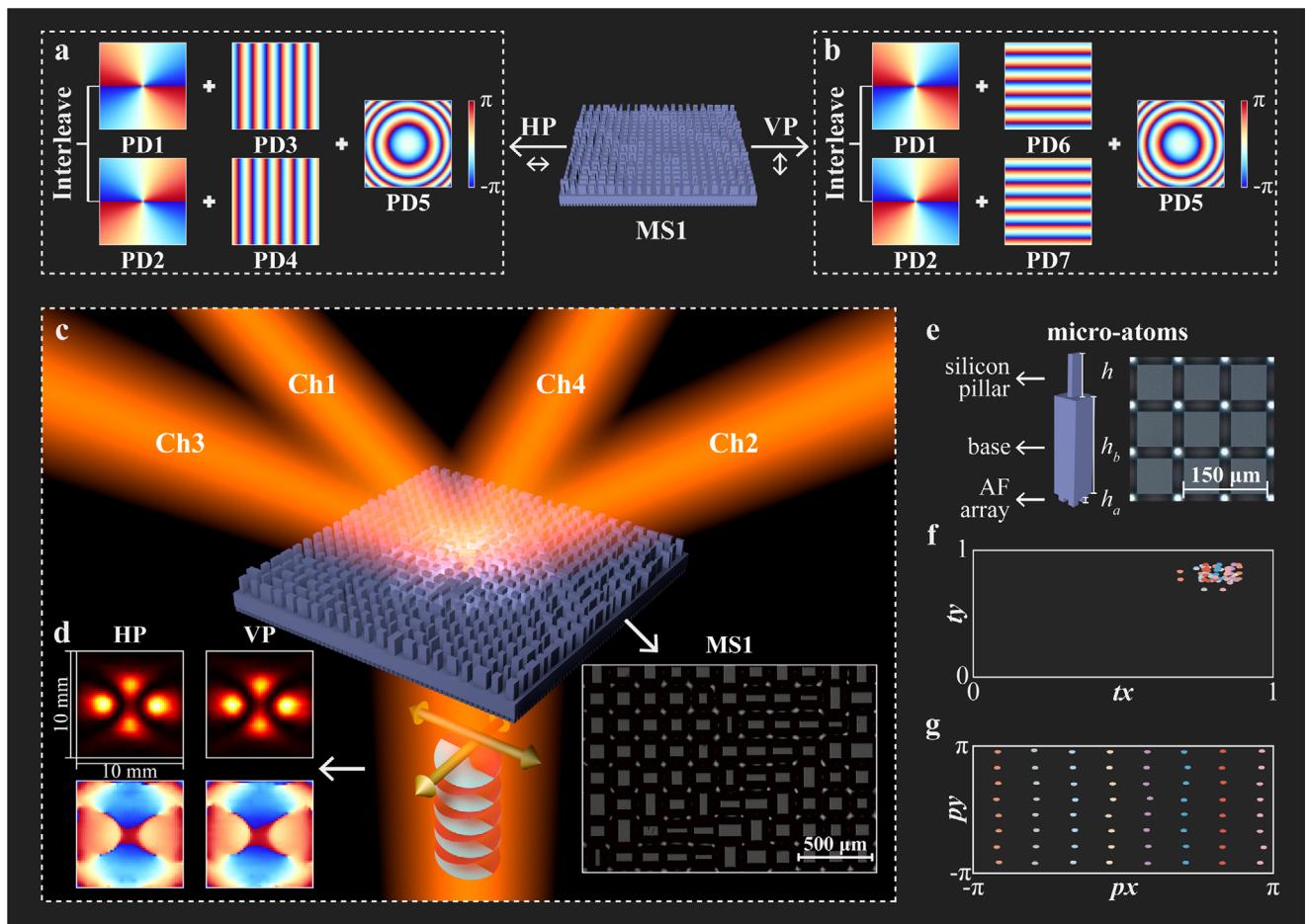
To obtain the different transmission responses for HP and VP components, the phase modulation of the metasurface at each point should satisfy the  $\Phi_{\text{HP}}$  and  $\Phi_{\text{VP}}$  in the two formulas above. As shown in Figure 2e, we used polarization-dependent silicon meta-atoms to compose the metasurface. The high-resistive silicon wafer exhibits a non-dispersive refractive index ( $\sim 3.45$ ) and low absorption loss in the THz band. Sixty-four meta-atoms with a period of  $160 \mu\text{m}$  ( $0.4\lambda$  at  $0.75 \text{ THz}$ ) were selected to achieve independent phase modulation for HP and VP with a phase interval of  $45^\circ$ . Details of the chosen pillars can be seen in Table S1 (Supporting Information). The metasurface contains three layers: a silicon pillar with a thickness of  $h = 260 \mu\text{m}$ , a  $688\text{-}\mu\text{m}$ -thick silicon substrate, and a periodic anti-reflection layer with  $h_a = 52 \mu\text{m}$  thickness. As shown in the right image of Figure 2e, the anti-reflection layer<sup>[51]</sup> consists of the periodic quadrate pillars with side length  $l_x = l_y = 48 \mu\text{m}$  and the period  $p = 63 \mu\text{m}$ . The phase accumulation of the selected meta-atoms under HP and VP incidence simulated by CST Microwave Studio is shown in Figure 2g. Figure 2f shows the simulated transmission amplitude of the selected meta-atoms. The average  $t_x(t_y)$  of the chosen meta-atoms is 0.815, and the transmissivity of the ordinary silicon wafer is  $\approx 0.7$ , which indicates that the anti-reflection layer can effectively improve transmission efficiency. We fabricated the proposed metasurface by double-sided registration lithography and deep reactive ion etching. The details can be found in the “Method” section. For the fabricated MS1 sample, the optical image of the upper layer is shown in the lower right corner of Figure 2c.

## 2.2. Two-Dimension Demultiplexer with LP Responses

The performance of the multi-functional metasurface was first investigated by the Rayleigh–Sommerfeld (RS) diffraction integration<sup>[52–53]</sup> in theory. The RS diffraction formula we used in the calculation is described by:

$$E(P_1) = \sum \sum \frac{d}{i\lambda} E_0(P_0) \frac{e^{-ikr_{01}}}{r_{01}^2} dx dy \quad (3)$$

where  $E(P_1)$  and  $E_0(P_0)$  represent the electric field at point  $P_1$  on the objective plane and point  $P_0$  on the metasurface, respectively.  $d$  is the distance between the metasurface and the objective plane;  $r_{01}$  is the distance between the points  $P_0$  and  $P_1$ . For OAM mode multiplexing, the complex amplitude  $E_0$  can be expressed as  $E_0 = E_{\text{in}} \cdot \exp(i\Phi_m)$ . Here,  $E_{\text{in}} = A_0 \cdot \exp(i\Phi_g)$  is defined as the initial incident Gaussian beam,  $A_0 = \exp[-(x^2 + y^2)/w^2]$  is the amplitude, and  $\Phi_g$  is the phase gradient due to oblique incidence,  $\Phi_m$  represents the phase distribution for metasurface serving as OAM mode multiplexer. For OAM mode demultiplexing, the  $E_0$  in Equation 3 can be defined by:  $E_0 = E_{\text{OAM}} \cdot \exp(i\Phi_{\text{dem}})$ ,  $E_{\text{OAM}}$  is the complex amplitude of coaxial OAM beams, and  $\Phi_{\text{dem}}$  represents the phase distribution for metasurface serving as mode demultiplexer. The period of phase gradient in  $\Phi_{\text{dem}}$  is set to  $T = 2.02 \text{ mm}$  for separating the different channels with a refractive angle of  $11.42^\circ$ . The calculated intensity distributions of demultiplexed beams at the focal plane of  $f = 20 \text{ mm}$  are shown in Figure 3a. The focus points corresponding to the correct-demultiplexed fundamental mode can be observed at four different positions, indicating that the four coaxial channels have been demultiplexed and separated successfully.

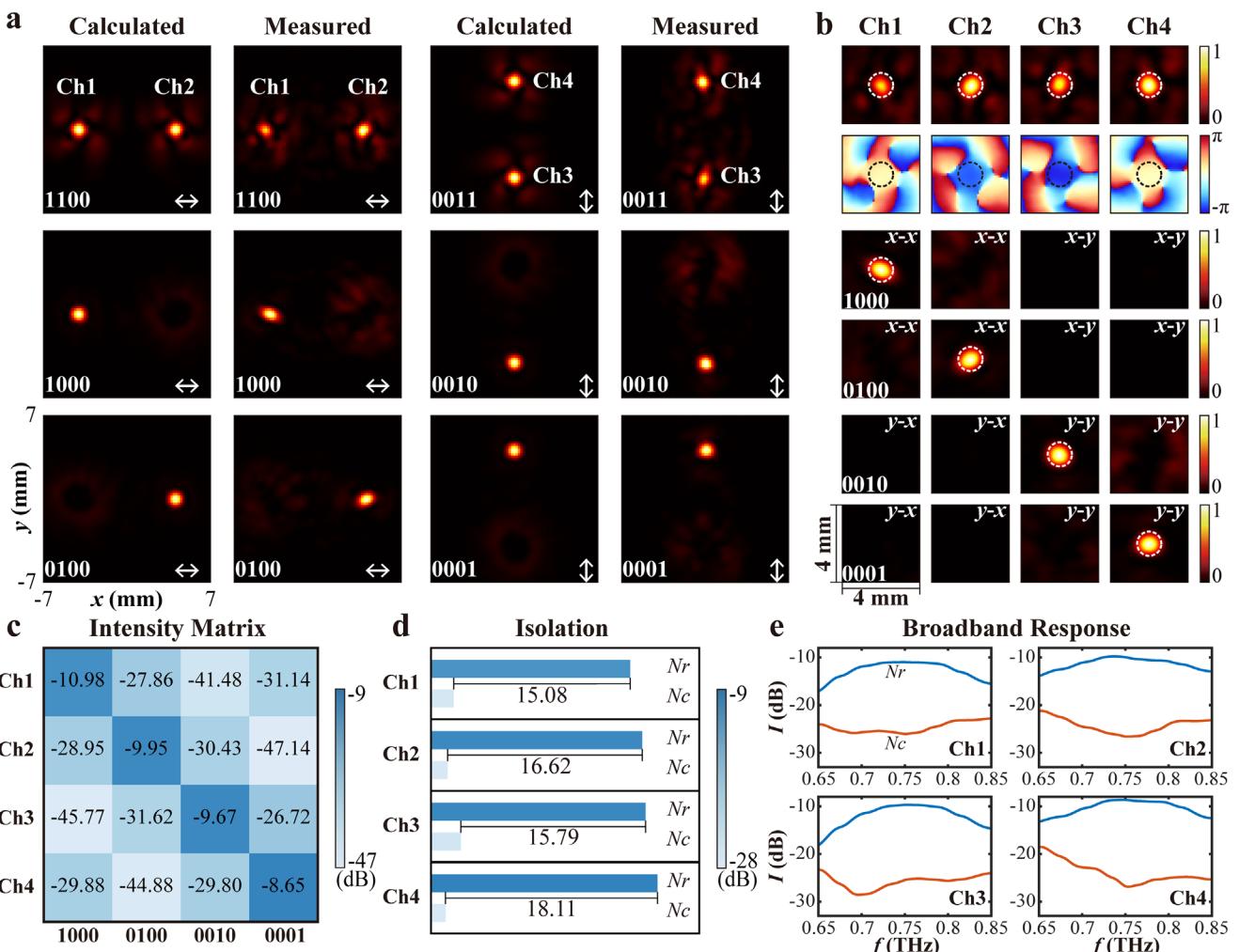


**Figure 2.** Design and demonstration of the 2D demultiplexer with LP responses. a,b) Phase response of HP and VP components. The PD1-PD7 represents the phase distributions of functional devices. PD1-2 are OAM mode converters. PD3-4 and 6-7 are different deflectors. PD5 represents the focusing lens. MS1 is the device for multi-functional multiplexing/demultiplexing. c) Schematic of 2D demultiplexing using the fabricated MS1 (the optical image is shown in the lower right corner). The yellow arrows are the orthogonal linear polarizations. The blue and red spirals refer to the different topological charges ( $l = \pm 2$ ) that the beams carry. Ch1-Ch4 represents four independent channels. d) Measured superimposed OAM beams with horizontal and vertical polarizations. e) Left: the schematic of the meta-atom. Right: the image of the anti-reflection layer. f) Simulated transmission amplitude of the selected meta-atoms. g) Simulated phase accumulation under HP and VP incidence.

The characteristics of the fabricated metasurfaces were experimentally investigated by the THz near-field time-domain spectroscopy (NF-TDS) system. Details of the experimental setup are shown in Figure S2 (Supporting Information). Since it was difficult to tilt the transmit antenna in our NF-TDS system, we fabricated the mode converter to replace the multiplexer used for oblique incidence, which can convert the normal-incident THz beam into OAM beams with the topological charge of  $l = \pm 2$ , the details of the design method are shown in Section S.4 (Supporting Information). The intensity and phase distributions of converted superimposed vortex beams with HP and VP can be seen in Figure 2d. We use the fabricated multi-functional metasurfaces as the 2D demultiplexer. Figure 3 shows the measured and calculated results of demultiplexed channels at four receive positions, verifying the 2D modulation of the metasurface. A 4-bit binary code is used to simulate incident beams that carry different information. Out of the demultiplexer, the spatially co-propagated OAM beams carried different information that could be recovered to Gaussian beams and be focused to four positions,

as shown in Figure 3a. The result scanned by the NF-TDS system in Figure 3a is the  $x$ - $y$  plane perpendicular to the  $z$ -axis. But in practice, the detector should be placed in the plane perpendicular to the wavevector of the demultiplexed beam. Here, we process the measured data by RS integration to obtain the intensity and phase distributions in the plane perpendicular to the wavevector of the demultiplexed channels. The results for each channel are shown in Figure 3b, and the data processing details are in Section S.5 (Supporting Information). When the incident beams carry 1100, the clear focus spots and uniform phase distributions can be observed in two symmetric positions on the  $x$ -axis. If the incident beams carry 0011, the two focus spots can be seen on the  $y$ -axis.

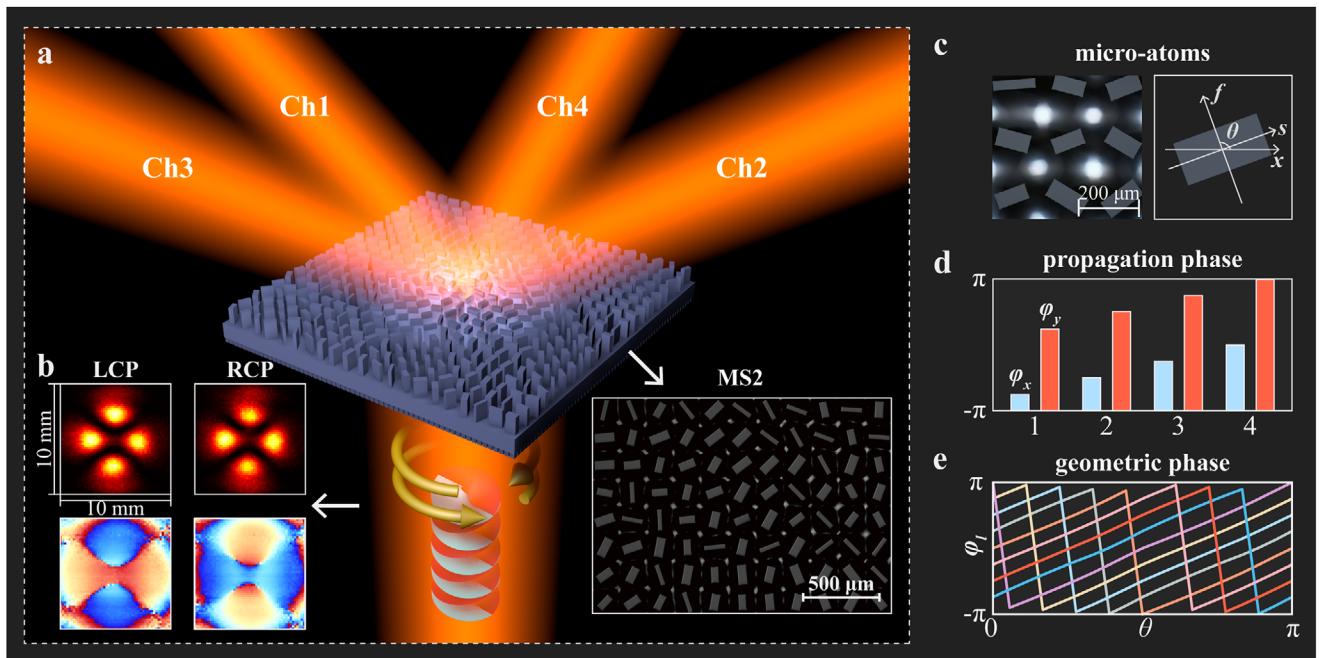
Based on the measurement results in Figure 3b, we can quantitatively analyze the crosstalk and isolation of four channels, where the aperture of the receiver is set to 1.36 mm (white dashed circles in the figure), the same as the diameter (calculated by  $1/e^2$ ) of the focused spot. The intensity matrix of the four demultiplexed channels is shown in Figure 3c, where the values



**Figure 3.** Measurement results for the 2D demultiplexer with LP responses. a) Calculated and measured intensity distributions at the demultiplexed focal plane. The horizontal and vertical arrows represent HP and VP components. Ch1-Ch4 represent the four independent channels. The 4-bit binary number at the bottom left represents the information carried by the four channels. b) The intensity and phase distributions of demultiplexed channels at four receive positions. The results are obtained at the plane perpendicular to the beam wavevector of the demultiplexed channel. The label in the upper right corner represents the incident and measured polarization states., E.g.,  $x$ - $x$  means the polarization state of the incident vortex beam is  $x$ -polarization (same as HP), and the measured electric field is  $y$ -polarized (same as VP). The white dashed circles represent the receiver aperture. c,d) Measured intensity matrix and isolation of four channels. Nr and Nc represent the intensity of the correct-demultiplexed beam and the crosstalk, respectively. All the numbers in the figure are in units of dB. e) The performance of the designed MS1 over the broadband range of 0.65–0.85 THz.

are calculated by  $N_{dB} = 10 \cdot \lg (I_r/I_i)$ ,  $I_r$  is the intensity of the correct-demultiplexed Gaussian beam within the receiving aperture, and  $I_i$  represents the intensity of the corresponding incident beam. The diagonal of the matrix is the value of the correct-demultiplexed beam, and the others are crosstalk. The maximum crosstalk among all channels is  $-16.88$  dB. The isolation of each channel is shown in Figure 3d, which is calculated by  $N_{is} = N_r - N_c$ ,  $N_r$  is the intensity of the correct-demultiplexed beam in the diagonal of the intensity matrix.  $N_c = 10 \cdot \lg (I_c/I_i)$ ,  $I_c$  represents the sum of the intensities of all crosstalk aroused by incorrect-demultiplexed beam within the receive aperture, and the measured isolation of the demultiplexed channels at 0.75 THz can be greater than  $15.08$  dB. We also analyzed the performance of the designed devices over the broadband range of 0.65–0.85 THz based on the measured results. It is worth mentioning that we

used broadband mode convertors in the experiment, and the normalized intensity of all incident OAM modes in the measured frequency range is greater than 83%. The details of incident vortex beams can be found in Figure S5 (Supporting Information). The isolation of the four channels in the whole interested range is shown in Figure 3e, while the crosstalk is analyzed in Section S.7 (Supporting Information). Due to the dispersion, the wavelength deviation will decrease in the received intensity. However, the proposed metasurface still exhibits wideband performance. The 3 dB bandwidth of all correct-demultiplexed channels is 0.13 THz, and the isolation of each channel can be greater than 10 dB over a range of 0.15 THz. Considering that isolation and insertion loss are two critical factors in multiplexing systems, we defined the adequate working bandwidth (AWB) of the devices as the frequency range in which the received energy attenuates



**Figure 4.** Design of two-dimension demultiplexer with CP responses. a) Schematic of 2D demultiplexing. The lower right corner is the optical image of the fabricated MS2 sample. The two yellow arrows represent the LCP and RCP, respectively. b) LCP and RCP components of the coaxial OAM beams. c) The top views of the meta-atoms.  $\theta$  is the orientation angle. d) Simulated propagation phase of the selected meta-atom.  $\varphi_x$  and  $\varphi_y$  are the phase delays under the horizontally and vertically polarized incidences. e) Simulated geometric phase of the chosen meta-atom.  $\varphi_l$  is the phase delay for LCP incidence.

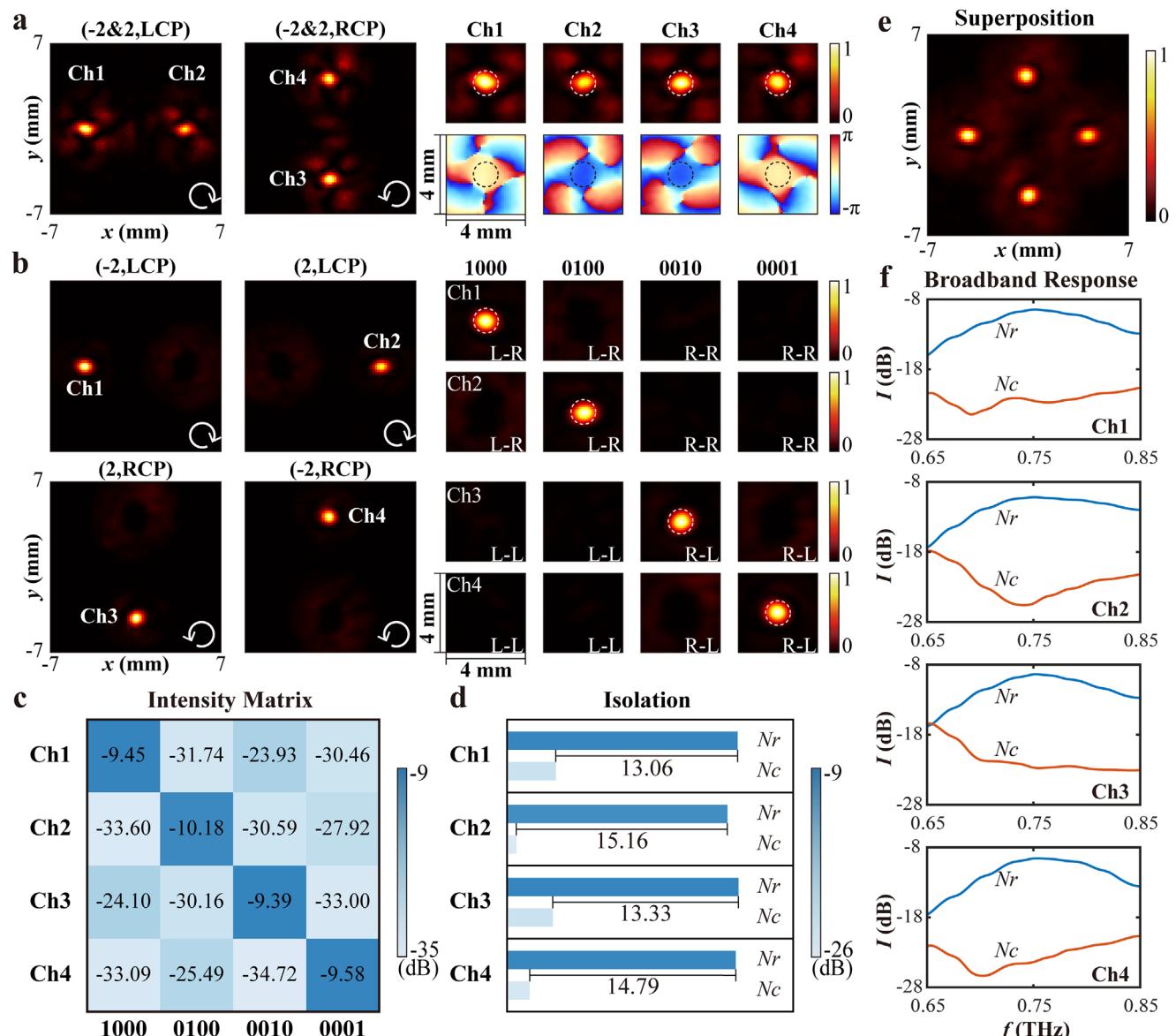
less than 3 dB with respect to the center frequency and the isolation of each channel is greater than 10 dB. Thus, the AWB of the designed MS1 is 0.13 THz. The results indicate that the proposed 2D demultiplexer is promising for THz communication compatible with WDM. As two cascaded metasurfaces are adopted in our MDM strategy, the misalignment issues may influence the performance of the devices. We provide a theoretical analysis and discussion on this issue in Section S.8 (Supporting Information). The calculated results show that as long as the displacement is less than  $\pm 2$  mm (31% of the side length of the metasurface), the decrease of received intensity and isolation can be less than 3 dB and 8 dB respectively, indicating that the multiplexing system can still perform well under minor displacement. Meanwhile, the calculated results show that the devices can be robust to the minor rotation if the diffraction orders are designed to be symmetric.

### 2.3. Two-Dimension Demultiplexer with CP Responses

The HP and VP are two essential and commonly used orthogonal polarization states for the PDM technique used in optical communications. Besides HP and VP, the left-circular polarized (LCP) and right-circular polarized (RCP) components also can be used as two orthogonal polarization channels. Using the circularly polarized components can decrease the alignment difficulty of the polarization coordinates of the transmitter and the receiver, and the polarization degree of a circularly polarized beam can maintain better performance in the free space transmission compared with that of a linearly polarized beam.<sup>[54]</sup> Therefore, we designed MS2 with CP responses. Similar to MS1, the designed

MS2 needs to provide two independent phase profiles for the LCP and RCP components, and the transmission functions of  $\Phi_{LCP}$  and  $\Phi_{RCP}$  are the same as  $\Phi_{HP}$  and  $\Phi_{VP}$  we mentioned above, respectively. Here, we obtain the target phase profiles by combining geometric phase and propagation phase modulation<sup>[55]</sup> in the design method. The phase modulation of the metasurface at each point should satisfy  $\Phi_{LCP} = \exp[i(\varphi_l)] = \exp[i(\varphi_p + \varphi_g)]$  and  $\Phi_{RCP} = \exp[i(\varphi_r)] = \exp[i(\varphi_p - \varphi_g)]$ , here  $\varphi_p$  and  $\varphi_g$  represent propagation phase and geometric phase, respectively. To design a metasurface with arbitrary phase distribution  $\varphi_l$  and  $\varphi_r$ , the propagation phase at each point should satisfy  $\varphi_p(x, y) = (\varphi_l + \varphi_r)/2$ , and the orientation angle  $\theta$  is defined by  $\theta(x, y) = \varphi_g/2 = (\varphi_l - \varphi_r)/4$ . As shown in Figure 4c, we used the anisotropic silicon pillars to compose the metasurface. The image of the fabricated MS2 sample is shown in the bottom right corner of Figure 4a. We selected eight pillars with a propagation phase interval of  $45^\circ$ , four of them are displayed in Figure 4d. The other four structures can be obtained by rotating these four pillars with an angle of  $90^\circ$ . For the chosen meta-atoms, the phase difference between the geometric phase  $\varphi_x$  and  $\varphi_y$  is very close to  $\pi$ , thereby implementing efficient conversion of the two orthogonally circular polarizations, and the average conversion efficiency  $\eta_{lr}(\eta_{rl})$  is 0.8244. Figure 4e shows the geometric phase of eight meta-atoms, which illustrates that the phase delay  $\varphi_l$  can cover the range of  $0$  to  $2\pi$  when rotating the pillars from  $0$  to  $\pi$ . The details of the selected meta-atoms are shown in Table S2 (Supporting Information).

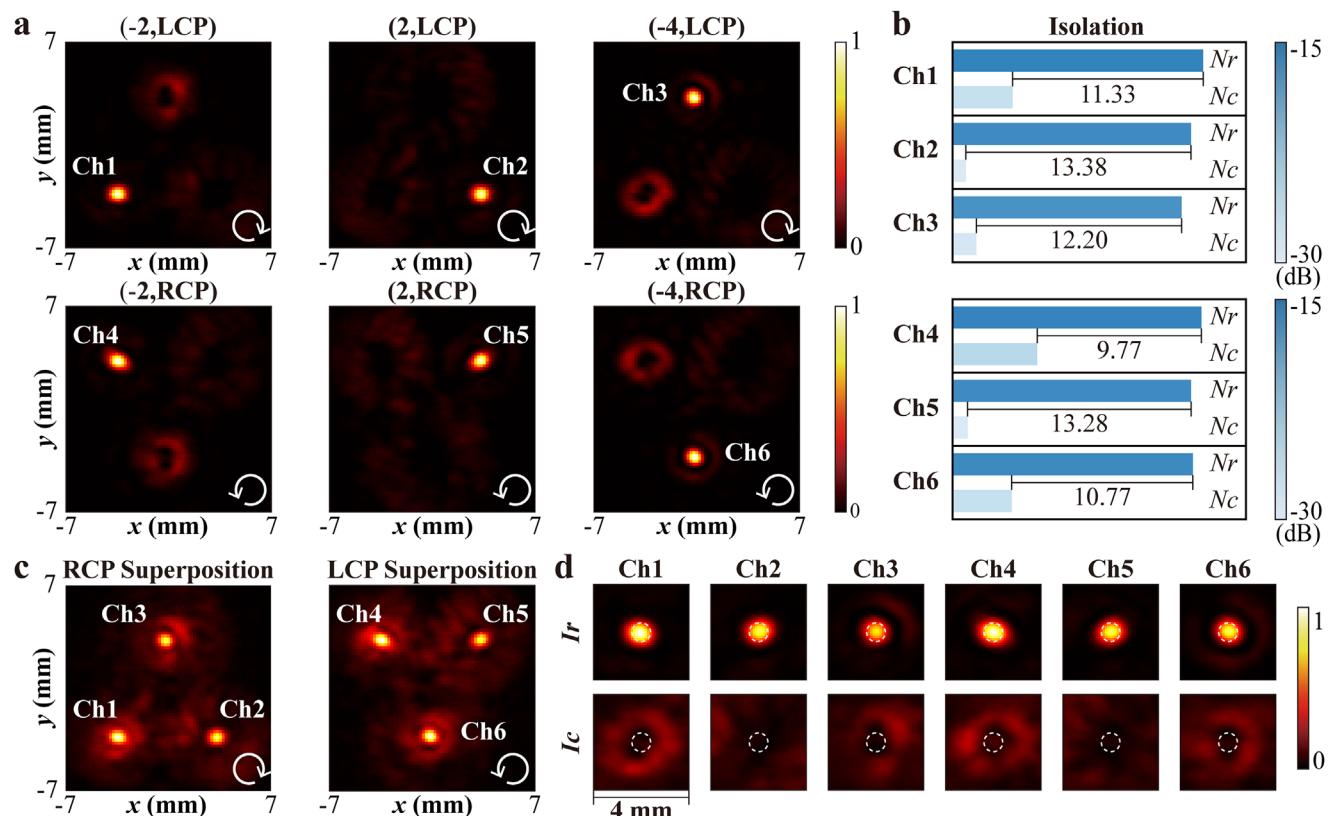
Figure 4b illustrates the measured intensity and phase distributions of the coaxial beams with superimposed OAM modes of  $l = \pm 2$  for LCP and RCP, respectively, which was obtained by another mode converter. As illustrated in Figure 4a, MS2 is used as



**Figure 5.** Performance of the 2D demultiplexer with CP responses measured by NF-TDS. a) Left: LCP and RCP components of the demultiplexed channels under multiple mode incidence. Right: Intensity and phase distributions of the demultiplexed Ch1-Ch4 in the plane perpendicular to the wavevector of the demultiplexed channels. b) Left: Intensity distributions in demultiplexed focal plane illuminated by different vortex beams. Right: The intensity distributions of demultiplexed channels at four receive positions. c,d) Measured intensity matrix and isolation of four channels. e) The superposition of measured intensity at the demultiplexed focus plane under four incidences (1000, 0100, 0010, and 0001). f) The performance of the designed MS2 over the broadband range of 0.65–0.85 THz.

a 2D demultiplexer with CP responses, and the intensity distributions of the demultiplexed channels are shown in Figure 5a. The right of Figure 5a shows the intensity and phase distribution at the focused positions of the four channels, demonstrating that the OAM modes with different polarizations are successfully demultiplexed into spatially separated fundamental Gaussian modes by the MS2. Figure 5b shows the measured intensity distribution in demultiplexed focal plane illuminated by different OAM beams, respectively, and the intensity distributions at four focal positions in the plane perpendicular to the wavevector of correct-demultiplexed beams are shown on the right of

Figure 5b. Figure 5c represents the intensity matrix of the four demultiplexed channels. It can be seen that the crosstalk between the orthogonal polarization channels is greater than that between different OAM mode channels with the same polarization. The former of crosstalk can be attributed to fabrication errors because the small deviation of element size will cause the reduction of polarization conversion efficiency, and the incomplete conversion of energy can increase the crosstalk. However, the fabricated MS2 still shows good performance. The maximum crosstalk among all channels is  $-14.48$  dB, and the measured isolation of the channels is above  $13.06$  dB (as shown in Figure 5d). Figure 5e



**Figure 6.** Performance of the designed MS3 for 6-channel 2D demultiplexing measured by NF-TDS. a) The intensity distributions of the demultiplexed channels illuminated by different vortex beams. b) Measured isolation of six channels. c) The superposition of measured RCP components (left) and LCP components (right). d) Measured intensity distributions of correct-demultiplexed Gaussian mode (up) and superposed intensity of all the crosstalk (down).

obtained by superposing the intensity distribution in the focal plane of demultiplexed beams under four incident vortex beams carrying the codes 1000, 0100, 0010, and 0001, respectively. We also evaluate the performance of the designed MS2 over the broadband range of 0.65–0.85 THz, and details of the broadband incident vortex beams are shown in Figure S6 (Supporting Information). As shown in Figure 5f, the 3 dB bandwidth of the demultiplexed channels is 0.13 THz, and the measured isolation of each channel can be greater than 10 dB over a range of 0.12 THz, which means that the AWB of MS2 can exceed 0.1 THz. These indicate that the designed metasurface can perform 2D demultiplexing in a broadband regime.

### 3. Discussion

The design method we used here can be extended to realize multiplexing and demultiplexing for more OAM channels or other orthogonal mode channels, such as Hermite-Gaussian modes and vector modes. As a proof of concept, we designed MS3 for 6-channel multi-dimensional demultiplexing, and the states of the six coaxial channels can be described by  $|LCP\rangle|l = \pm 2, l = -4\rangle$  and  $|RCP\rangle|l = \pm 2, l = -4\rangle$ . Figure 6a shows the intensity distribution of the demultiplexed channels illuminated by different vortex beams. The superposition results of all the LCP and RCP components in Figure 6c indicate that MS3 could also show good per-

formance under the incidence with multiple modes. As interleaving is a kind of shared-aperture design method, the increase of demultiplexed channels inevitably leads to decreased energy received by each channel and the introduction of extra crosstalk.<sup>[56]</sup> Designing the anti-reflection layer is an effective way to improve device efficiency, as demonstrated here before. In addition, using the optimization algorithm to optimize the phase distribution of the meta-devices can increase the power received in each channel.<sup>[57]</sup> In the experiment, we adjusted the aperture of the receiving terminal to decrease crosstalk, and the diameter of the receiving aperture was set to be the same as the full width at half maximum of correct-demultiplexed Gaussian mode in the top row of Figure 6d. The bottom row of Figure 6d shows the superposed intensity distribution of all the crosstalk aroused by the five incorrect-demultiplexed beams. A significant intensity difference between the Gaussian mode and crosstalk within the receiving aperture can be observed. The measured isolation of Ch1–Ch6 is shown in Figure 6b. Except for Ch4, whose isolation is 9.77 dB, the isolation of other channels is greater than 10 dB. According to our definition of device bandwidth, the MS3 can only be used as a narrow-band device. The results in Figure 6d show that the isolation of Ch2 and Ch4 is greater than that of other channels as the minimum interval of the topological charges between these two channels and adjacent channels is  $|4|$  comparing  $|2|$  of other channels, which indicates that the crosstalk can be reduced by

increasing the intervals of the topological charges between adjacent channels. In a multiplexing system, isolation and insertion loss are two critical factors. In theory, it is difficult to accurately predict the deterioration of these two factors as the number of channels increases due to the complexity of the 2D multiplexing system. Our measured results demonstrated that, under the given experimental conditions, a 6-channel metasurface-based demultiplexing setup can achieve an isolation of nearly 10 dB and an insertion loss of  $\approx$ 15 dB. This indicates that the few-channel (6 or less) MDM+PDM strategy holds high promise to be integrated into broadband THz modulation systems. Moreover, we analyze the sensitivity of the MDM system to the angle error of the transmitter and receiver in Section S.10 (Supporting Information). The results indicate that the error of the angle should be less than  $\pm 1^\circ$ . Reconfigurable and intelligent metasurfaces<sup>[58–61]</sup> can be utilized to design multiplexers that respond rapidly to wide-range incident angles and realize self-adaptive beamforming, which hold promise to increase the flexibility of THz demultiplexer.

## 4. Conclusion

In conclusion, we proposed a multi-functional metasurface to realize the 2D MDM-PDM in the THz domain. 4-channel LP demultiplexing and 6-channel CP demultiplexing were experimentally demonstrated by the NF-TDS system. For the 4-channel LP demultiplexing, a low crosstalk of  $-16.88$  dB between different channels is achieved. Moreover, the 3 dB bandwidth of the metasurfaces is 0.13 THz, and the measured isolation of each channel can be greater than 10 dB over a range of 0.1 THz, which indicates that they have great potential to be compatible with WDM. This work provides an efficient and compact platform for integrated THz MDM and PDM, and the results will help to pave the way for multi-dimensional multiplexing in high-capacity THz communication systems.

## 5. Experimental Section

**Fabrication Steps:** The fabrication of the metasurface sample can be divided into three steps. First, a 3- $\mu$ m-thick AZ4620 photoresist is spin-coating on the 1-mm-thick silicon wafer, prebaked at 120 °C for 120 s, and subsequently exposed through UV to pattern the features of the designed meta-atoms in the mask aligner (SUSS MA4). The patterns are revealed after the development process in AZ400K liquid for 18 seconds. It is worth mentioning that the alignment marks on the photomask are used to calibrate the lithography area for double-layer processing. Next, the silicon sample is etched by the inductively coupled plasma reactive ion etching system with Bosch technology. This process consists of passivation and etching. During each period, we use SF<sub>6</sub> gas to etch the silicon for 4 s and C<sub>4</sub>F<sub>8</sub> gas to deposit fluorocarbon protective polymer for 2.2 s. The above period is repeated until the required etching depth is achieved. Finally, we removed the remaining photoresist with an acetone solution and cleand the silicon wafer with DI water.

## Supporting Information

Supporting Information is available from the Wiley Online Library or from the author.

## Acknowledgements

This work was funded by the National Natural Science Foundation of China (62027820, 61975143, 62375203, 62205380, 62025504, 61935015), the National Science Foundation (2114103).

## Conflict of Interest

The authors declare no conflict of interest.

## Author Contributions

W.L. and J.G. conceived the idea and initiated the project. Q.Y. joined the discussion of the notion. W.L. developed the theoretical calculation and performed the simulation with the help of X.J.. W.L. fabricated and characterized the samples with the help of F.H. and C.L.. W.L. carried out the experiment with the help of X. J. and Q.X.. W.L. analyzed the results with the help of the Q.X.. W.L. wrote the manuscript and produced the figures. J.G., Q.X., and Y.G. edited the manuscript. J.H. and W.Z. supervised the project.

## Data Availability Statement

The data that support the findings of this study are available from the corresponding author upon reasonable request.

## Keywords

multi-dimensional multiplexing, multi-functional metasurfaces, orbital angular momentum mode, terahertz

Received: October 20, 2023  
Revised: February 14, 2024  
Published online:

- [1] I. F. Akyildiz, J. M. Jornet, C. Han, *Phys. Commun.* **2014**, *12*, 16.
- [2] T. Nagatsuma, G. Ducournau, C. C. Renaud, *Nat. Photonics* **2016**, *10*, 371.
- [3] Y. H. Yang, Y. Yamagami, X. B. Yu, P. Pitchappa, J. Webber, B. L. Zhang, M. Fujita, T. Nagatsuma, R. Singh, *Nat. Photonics* **2020**, *14*, 446.
- [4] R. Jia, S. Kumar, T. C. Tan, A. Kumar, Y. J. Tan, M. Gupta, P. Sriftgiser, A. Alphones, G. Ducournau, R. Singh, *Sci. Adv.* **2023**, *9*, eadi8500.
- [5] A. Kumar, M. Gupta, P. Pitchappa, N. Wang, M. Fujita, R. Singh, *J. Appl. Phys.* **2022**, *132*, 140901.
- [6] H. Zeng, H. Liang, Y. Zhang, L. Wang, S. Liang, S. Gong, Z. Li, Z. Yang, X. Zhang, F. Lan, Z. Feng, Y. Gong, Z. Yang, D. M. Mittleman, *Nat. Photonics* **2021**, *15*, 751.
- [7] Y. Zhang, K. Ding, H. Zeng, W. Kou, T. Zhou, H. Zhou, S. Gong, T. Zhang, L. Wang, S. Liang, F. Lan, Y. Dong, Z. Feng, Y. Gong, Z. Yang, D. M. Mittleman, *Optica* **2022**, *9*, 1268.
- [8] J. Li, L. Zhang, M. Zhang, H. Su, I. L. Li, S. Ruan, H. Liang, *Adv. Opt. Mater.* **2020**, *8*, 2000068.
- [9] N. J. Karl, R. W. McKinney, Y. Monnai, R. Mendis, D. M. Mittleman, *Nat. Photonics* **2015**, *9*, 717.
- [10] W. Liu, Q. Yang, Q. Xu, X. Jiang, T. Wu, K. Wang, J. Gu, J. Han, W. Zhang, *Adv. Opt. Mater.* **2021**, *9*, 2100506.
- [11] A. Kumar, M. Gupta, P. Pitchappa, N. Wang, P. Sriftgiser, G. Ducournau, R. Singh, *Nat. Commun.* **2022**, *13*, 5404.
- [12] S. Randel, R. Ryf, A. Sierra, P. J. Winzer, A. H. Gnauck, C. A. Bolle, R.-J. Essiambre, D. W. Peckham, A. McCurdy, R. Lingle, *Opt. Express* **2011**, *19*, 16697.

[13] L.-W. Luo, N. Ophir, C. P. Chen, L. H. Gabrielli, C. B. Poitras, K. Bergmen, M. Lipson, *Nat. Commun.* **2014**, *5*, 3069.

[14] S. Kruk, F. Ferreira, N. M. Suibhne, C. Tsekrekos, I. Kravchenko, A. Ellis, D. Neshev, S. Turitsyn, Y. Kivshar, *Laser Photonics Rev.* **2018**, *12*, 1800031.

[15] R. C. Devlin, A. Ambrosio, N. A. Rubin, J. P. B. Mueller, F. Capasso, *Science* **2017**, *358*, 896.

[16] A. E. Willner, H. Huang, Y. Yan, Y. Ren, N. Ahmed, G. Xie, C. Bao, L. Li, Y. Cao, Z. Zhao, J. Wang, M. P. J. Lavery, M. Tur, S. Ramachandran, A. F. Molisch, N. Ashrafi, S. Ashrafi, *Adv. Opt. Photonics* **2015**, *7*, 66.

[17] N. Bozinovic, Y. Yue, Y. Ren, M. Tur, P. Kristensen, H. Huang, E. Willner Alan, S. Ramachandran, *Science* **2013**, *340*, 1545.

[18] T. Stav, A. Faerman, E. Maguid, D. Oren, V. Kleiner, E. Hasman, M. Segev, *Science* **2018**, *361*, 1101.

[19] Y. Yan, G. Xie, M. P. J. Lavery, H. Huang, N. Ahmed, C. Bao, Y. Ren, Y. Cao, L. Li, Z. Zhao, A. F. Molisch, M. Tur, M. J. Padgett, A. E. Willner, *Nat. Commun.* **2014**, *5*, 4876.

[20] H. Zhou, X. Su, A. Miroofar, R. Zhang, K. Zou, H. Song, K. Pang, H. Song, N. Hu, Z. Zhao, A. Almaiman, S. Zach, M. Tur, A. F. Molisch, H. Sasaki, D. Lee, A. E. Willner, *Opt. Express* **2022**, *30*, 25418.

[21] R. Imai, N. Kanda, T. Higuchi, K. Konishi, M. Kuwata-Gonokami, *Opt. Lett.* **2014**, *39*, 3714.

[22] H. F. Zhang, X. Q. Zhang, Q. Xu, Q. Wang, Y. H. Xu, M. G. Wei, Y. F. Li, J. Q. Gu, Z. Tian, C. M. Ouyang, X. X. Zhang, C. Hu, J. G. Han, W. L. Zhang, *Photonics Res* **2018**, *6*, 24.

[23] A. Al Dhaybi, J. Degert, E. Brasselet, E. Abraham, E. Freysz, *J. Opt. Soc. Am. B* **2019**, *36*, 12.

[24] J. S. Li, L. N. Zhang, *Opt. Express* **2020**, *28*, 36403.

[25] X. Zang, Z. Li, Y. Zhu, J. Xu, J. Xie, L. Chen, A. V. Balakin, A. P. Shkurinov, Y. Zhu, S. Zhuang, *Appl. Phys. Lett.* **2020**, *117*, 171106.

[26] J. Wang, J.-Y. Yang, I. M. Fazal, N. Ahmed, Y. Yan, H. Huang, Y. Ren, Y. Yue, S. Dolinar, M. Tur, A. E. Willner, *Nat. Photonics* **2012**, *6*, 488.

[27] K. Miyamoto, K. Suizu, T. Akiba, T. Omatsu, *Appl. Phys. Lett.* **2014**, *104*, 261104.

[28] N. Yu, P. Genevet, M. A. Kats, F. Aieta, J.-P. Tetienne, F. Capasso, Z. Gaburro, *Science* **2011**, *334*, 333.

[29] S. Sun, Q. He, S. Xiao, Q. Xu, X. Li, L. Zhou, *Nat. Mater.* **2012**, *11*, 426.

[30] G. M. Akselrod, J. Huang, T. B. Hoang, P. T. Bowen, L. Su, D. R. Smith, M. H. Mikkelsen, *Adv. Mater.* **2015**, *27*, 8028.

[31] M. I. Shalaev, J. Sun, A. Tsukernik, A. Pandey, K. Nikolskiy, N. M. Litchinitser, *Nano Lett.* **2015**, *15*, 6261.

[32] X. Quan, S. Xiaoqiang, Z. Xueqian, D. Lijuan, L. Lifeng, S. Yunlong, W. Qiu, K. Ming, A. Andrea, Z. Shuang, H. Jianguang, Z. Weili, *Adv. Photonics* **2022**, *4*, 016002.

[33] Q. Feng, X. Kong, M. Shan, Y. Lin, L. Li, T. J. Cui, *Phys. Rev. Appl.* **2022**, *17*, 034017.

[34] W. Liu, Q. Yang, Q. Xu, X. Jiang, T. Wu, J. Gu, J. Han, W. Zhang, *Nanophotonics-Berlin* **2022**, *11*, 3631.

[35] F. Huang, Q. Xu, W. Liu, T. Wu, J. Gu, J. Han, W. Zhang, *Photonics Res* **2023**, *11*, 431.

[36] Z. H. Jiang, L. Kang, W. Hong, D. H. Werner, *Phys. Rev. Appl.* **2018**, *9*, 064009.

[37] S. Zhang, P. Huo, W. Zhu, C. Zhang, P. Chen, M. Liu, L. Chen, H. J. Lezec, A. Agrawal, Y. Lu, T. Xu, *Laser Photonics Rev.* **2020**, *14*, 2000062.

[38] Y. Li, X. Li, L. W. Chen, M. B. Pu, J. J. Jin, M. H. Hong, X. G. Luo, *Adv. Opt. Mater.* **2017**, *5*, 1600502.

[39] E. Maguid, I. Yulevich, D. Veksler, V. Kleiner, M. L. Brongersma, E. Hasman, *Science* **2016**, *352*, 1202.

[40] Y. Jin, L. Rong, C. M. u Ku, T. Din Ping, *Adv. Photonics* **2023**, *5*, 024001.

[41] K. Zhang, Y. Yuan, X. Ding, H. Li, B. Ratni, Q. Wu, J. Liu, S. N. Burokur, J. Tan, *Laser Photonics Rev.* **2020**, *15*, 2000351.

[42] S. Chen, Z. Xie, H. Ye, X. Wang, Z. Guo, Y. He, Y. Li, X. Yuan, D. Fan, *Light: Sci. Appl.* **2021**, *10*, 222.

[43] S. Li, X. Li, L. Zhang, G. Wang, L. Zhang, M. Liu, C. Zeng, L. Wang, Q. Sun, W. Zhao, W. Zhang, *Adv. Opt. Mater.* **2020**, *8*, 1901666.

[44] H. Wu, Q. Zeng, X. Wang, C. Li, Z. Huang, Z. Xie, Y. He, J. Liu, H. Ye, Y. Chen, Y. Li, D. Fan, S. Chen, *Nanophotonics-Berlin* **2023**, *12*, 1129.

[45] H. Chung, D. Kim, E. Choi, J. Lee, *Laser Photonics Rev.* **2022**, *16*, 2100456.

[46] X. He, Y. Yang, L. Deng, S. Li, B. Feng, *ACS Appl. Mater. Interfaces* **2021**, *13*, 20770.

[47] J. Liu, Y. Cheng, F. Chen, H. Luo, X. Li, *J. Opt. Soc. Am. B* **2023**, *40*, 441.

[48] F. Li, Y. Li, T. Tang, Y. Lu, X. Liu, Y. Liao, Q. Wen, *Photonics Res* **2023**, *11*, 485.

[49] H. Zhao, B. Quan, X. Wang, C. Gu, J. Li, Y. Zhang, *ACS Photonics* **2018**, *5*, 1726.

[50] H. Yang, S. Zheng, H. Zhang, N. Li, D. Shen, T. He, Z. Yang, Z. Lyu, X. Yu, *IEEE Trans. Antennas Propag.* **2023**, *71*, 4194.

[51] H. Zhang, X. Zhang, Q. Xu, C. Tian, Q. Wang, Y. Xu, Y. Li, J. Gu, Z. Tian, C. Ouyang, X. Zhang, C. Hu, J. Han, W. Zhang, *Adv. Opt. Mater.* **2018**, *6*, 1700773.

[52] V. Nasco, P. C. Logofătu, *Appl. Opt.* **2009**, *48*, 4310.

[53] Q. Wang, X. Zhang, Y. Xu, J. Gu, Y. Li, Z. Tian, R. Singh, S. Zhang, J. Han, W. Zhang, *Sci. Rep.* **2016**, *6*, 32867.

[54] X. Zhao, Y. Yao, Y. Sun, C. Liu, *J. Opt. Commun. Netw.* **2009**, *1*, 307.

[55] Y. Xu, H. Zhang, Q. Li, X. Zhang, Q. Xu, W. Zhang, C. Hu, X. Zhang, J. Han, W. Zhang, *Nanophotonics-Berlin* **2020**, *9*, 3393.

[56] E. Maguid, I. Yulevich, M. Yannai, V. Kleiner, M. L. Brongersma, E. Hasman, *Light: Sci. Appl.* **2017**, *6*, e17027.

[57] X. Zhang, L. Huang, R. Zhao, H. Zhou, X. Li, G. Geng, J. Li, X. Li, Y. Wang, S. Zhang, *Sci. Adv.* **2022**, *8*, eabp8073.

[58] J. C. Ke, X. Chen, W. Tang, M. Z. Chen, L. Zhang, L. Wang, J. Y. Dai, J. Yang, J. W. Zhang, L. Wu, Q. Cheng, S. Jin, T. J. Cui, *Natl. Sci. Rev.* **2022**, *9*, nwac225.

[59] F. Lan, L. Wang, H. Zeng, S. Liang, T. Song, W. Liu, P. Mazumder, Z. Yang, Y. Zhang, D. M. Mittleman, *Light: Sci. Appl.* **2023**, *12*, 191.

[60] L. Cong, R. Singh, *Adv. Mater.* **2020**, *32*, 2001418.

[61] Y. J. Tan, C. Zhu, T. C. Tan, A. Kumar, L. J. Wong, Y. Chong, R. Singh, *Opt. Express* **2022**, *30*, 27763.